

# Follow-up of the impedance of the crab cavities

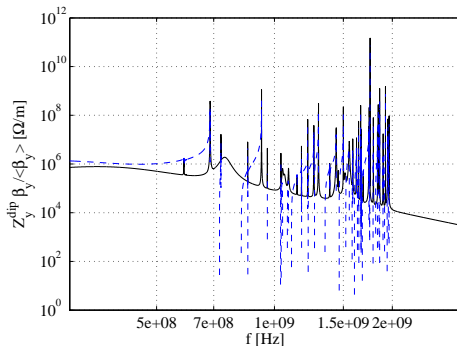
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# Outline

- 1 Introduction
- 2 Kick factor from Crab Cavities
- 3 Single bunch Vs Coupled Bunch
- 4 Conclusion and outlook

**Motivation:** We want to evaluate the effect of crab cavities focusing on their **single bunch** and **coupled bunch** kick factor in comparison with already existing equipment.



f (GHz)	Q	R (Ohm/m) per half cavity	plane	Deltaf in kHz
0.400	6.66E+09	5.98E+12	V	-
0.685	1880	4.67E+05	H	365
0.927	8600	1.38E+06	H	108
1.30	6540	3.73E+05	V	200
1.50	10800	2.67E+05	H	140
1.66	24200	3.14E+05	H	69
1.75	5800	2.57E+05	H	301
1.75	4160000	1.81E+08	H	0.4
1.84	9990	3.34E+05	V	185
1.86	26400	4.17E+05	H	70
1.86	88200	1.56E+06	V	21
1.92	102000	1.85E+06	H	18
1.96	54400	1.15E+05	H	36

Reminder:

- Crab cavities exhibit HOMs from  $\approx 500$  MHz up to 2 GHz in a location where the transverse  $\beta$  is  $\approx 3000$ .
- Some HOM reach the level of  $R_s = 10 \text{ G}\Omega/\text{m}$   $\rightarrow$  it might drive transverse CB instabilities!

# Kick factor from Crab Cavities

- We define the transverse kick factor as:

$$k_t = \frac{1}{2\pi} \int_{-\infty}^{+\infty} Z_t(\omega)h(\omega)d\omega, \quad (1)$$

where  $h(\omega) = \lambda(\omega)^2$  is the power spectrum of the current distribution,  $Z_t$  the transverse impedance (dipolar + quadrupolar). Given in units  $[k_t]=V/(mm \text{ pC})$ .

- For a Gaussian bunch we have:

$$h(\omega) = e^{-\omega^2\sigma_t^2}. \quad (2)$$

- The kick factor is related to the transverse kick  $\Delta y'$  a particle would get due to an impedance:

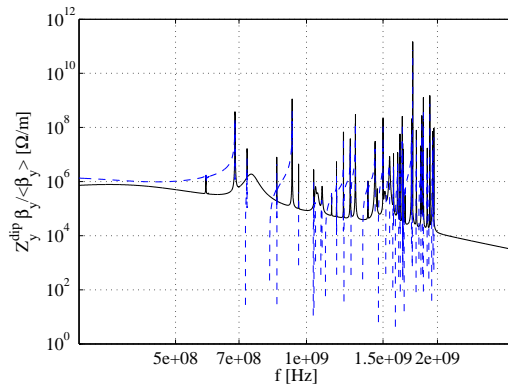
$$\Delta y' = -\frac{N_b q^2 y_0}{\beta^2 E} k_t. \quad (3)$$

with  $N_b$  bunch intensity,  $q$ ,  $v$  and  $m_p$ , proton particle charge, velocity and rest mass,  $y_0$  the closed orbit position at the impedance location.

- From the loss factor we can recover the usual tune shift formula (same as Sacherer for single bunch, azimuthal mode  $m = 0$ ):

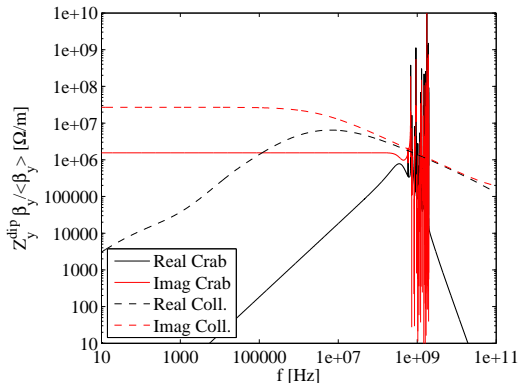
$$\Delta Q_y^{m=0} = \frac{1}{4\pi} \beta_k \Delta y' = -\frac{I_b q T_0}{4\pi \beta^2 E} \bar{\beta}_y k'_t, \quad \text{with } k'_t = \frac{\beta_k}{\bar{\beta}_y} k_t. \quad (4)$$

- Considering all the Crab Cavities (8 x plane x beam) we have



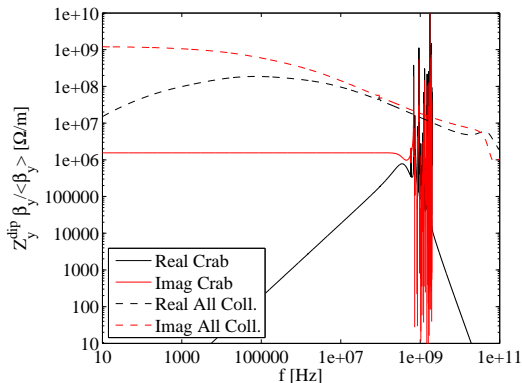
- $k_t' = 1.4 \text{ V/mm pC}$ .

- Considering all the Crab Cavities (8 x plane x beam) we have



- $k_t' = 1.4 \text{ V/mm pC.}$
- The TCP.D6L7.B1 with half gap at  $\approx 1 \text{ mm}$  would  $k_t' = 3.14 \text{ V/mm pC.}$

- Considering all the Crab Cavities (8 x plane x beam) we have



- $k'_t = 1.4$  V/mm pC.
- The TCP.D6L7.B1 with half gap at  $\approx 1$  mm would  $k'_t = 3.14$  V/mm pC.
- All the collimators would give  $k'_t = 45.3$  V/mm pC.

## Single bunch:

- For a single bunch displaced by  $y_0 = 1mm$  at the Crab cavities location, with  $N_b = 2.2 \cdot 10^{11}$  ppb, the induced voltage is  $V = N_b q k_t' y_0 = 50 kV$ . This is the voltage seen by the bunch passing through the impedance. The change in transverse energy  $\Delta E_t = qV$  will determine the bunch oscillations and tune shift.
- The effect looks negligible comparing with usual equipments like collimators.

## Coupled bunch:

- An HOM with shut impedance  $R_s$ , merit factor  $Q$  and resonant frequency  $f_r$  can drive unstable modes  $\rightarrow$  the M bunches start oscillating coherently.
- We suppose rigid bunch oscillations (azimuthal  $m = 0$ ) and derive the unstable frequency as  $f_p = (n_x + k_p M + Q_{y_0}) f_0$  with  $n_x \in (0..M - 1)$  coupled bunch number,  $k_p$  line number.
- We choose the **most unstable mode** ( $f_p \simeq f_r$ ).
- The kick factor can be defined extending the single bunch case as:

$$k_t = \omega_0 \sum_{p=-\infty}^{+\infty} Z_t(\omega_p) h(\omega_p), \quad (5)$$

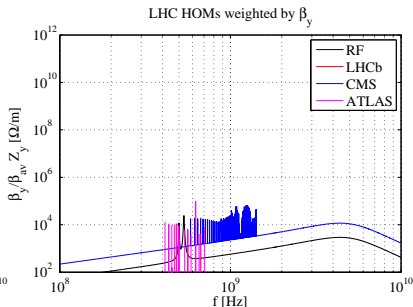
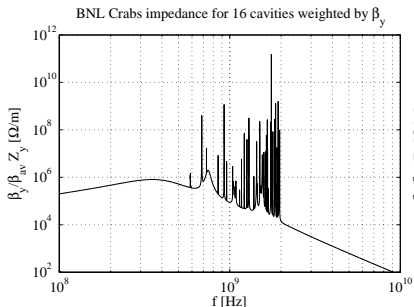
where  $\omega_p = (n_x + k_p M + Q_{y_0}) \omega_0$ .



- A transverse HOM can be characterized by shut impedance  $R_s$ , merit factor  $Q$  and resonant frequency  $f_r$ :

$$Z(f) = \frac{f_r}{f} \frac{R_s}{1 - jQ\left(\frac{f_r}{f} - \frac{f}{f_r}\right)};$$

- When falling on a CB line we have  $k_t = \omega_0 R_s h(\omega_r)$ .



- Comparison of HLLHC (round  $\beta^* = 15\text{cm}$ ) BNL-HOMs Vs main HOMs from nominal LHC ( $\beta^* = 60\text{cm}$ ).
- Several orders of magnitude difference  $\rightarrow$  not negligible effect (DELPHI).

## Conclusions

- We gave an overview of the effect of crab cavities in single bunch and coupled bunch.
- The **single bunch** effect of crab cavities **can be compared** with the one of a **single LHC collimator**.
- The **single bunch** effect of crab cavities **is negligible** comparing to the **total LHC collimators** contribution.
- The **coupled bunch** effect of crab cavities is driven by the equipment HOM → **orders of magnitude** above other machine equipment.

## Outlook

- Continuing improving the crab cavities design in order to damp the HOM.
- Studying possible configurations for safe and stable machine operation with this equipment (collide and squeeze).
- ...

Thanks for your attention!

# Backup

- Each CB line can be driven unstable in presence of an impedance.
- The rise-time and frequency shift can be approximately calculated by means of the Sacherer formula:

$$\Delta\omega_m^{x,y} = \frac{1}{|m| + 1} \frac{jq\beta I_b}{2 m_0 \gamma Q_{x_0,y_0} \Omega_0 L_b} (Z_{x,y}^{eff})_m$$

where  $\Delta\omega_m^{x,y}$  the CB line complex frequency shift,  $q$  is the proton charge,  $m_0$  the proton rest mass,  $I_b = e N_b / T_0$  the beam current,  $T_0$  the revolution frequency,  $\omega_0$  revolution radial frequency,  $Q_{x_0,y_0}$  the machine unperturbed tune,  $\beta$  and  $\gamma$  relativistic factors,  $L_b = 4\sigma_z$  with  $\sigma_z$  the rms bunch length,  $Z_{x,y}^{eff}$  the impedance weighted by the sinusoidal modes with

$$h(\omega) = \frac{8\tau_b^2}{\pi^4} (|m| + 1)^2 \frac{1 + (-1)^{|m|} \cos(\omega 4\tau_b)}{[(\omega 4\tau_b / \pi)^2 - (|m| + 1)^2]^2}$$

and

$$Z_{x,y}^{eff} = \frac{\sum_{p=-\infty}^{+\infty} Z(\omega_p)_{x,y} h(\omega_p)}{\sum_{p=-\infty}^{+\infty} h(\omega_p)}$$

- The chromatic frequency  $\omega_\xi = \frac{\omega\xi}{\eta}$  shifts the sinusoidal modes (replace  $\omega \rightarrow \omega - \omega_\xi$ ).
- NB: No damper is considered here.

# Backup

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$$Z(f) = \frac{f_r}{f} \frac{R_s}{1 - jQ\left(\frac{f_r}{f} - \frac{f}{f_r}\right)};$$

- If the bandwidth  $\Delta f = \frac{f_r}{Q} \geq f_0$ , the mode covers one or more CB lines that are driven unstable.
- If the bandwidth  $\Delta f = \frac{f_r}{Q} \ll f_0$ , the mode can fall between the CB lines  $\rightarrow$  complicated situation due to the many azimuthal modes spaced by  $f_s$ .

- **If falling on the CB line** we can simplify the Sacherer formula

$$\Delta\omega_m^{x,y} = \frac{1}{|m| + 1} \frac{jq\beta I_b}{2 m_0 \gamma Q_{x_0,y_0} \Omega_0 L_b} R_s \frac{h(\omega_r)}{\sum_{p=-\infty}^{+\infty} h(\omega_p)}$$

- **If not falling on the CB line** we are in principle stable.