

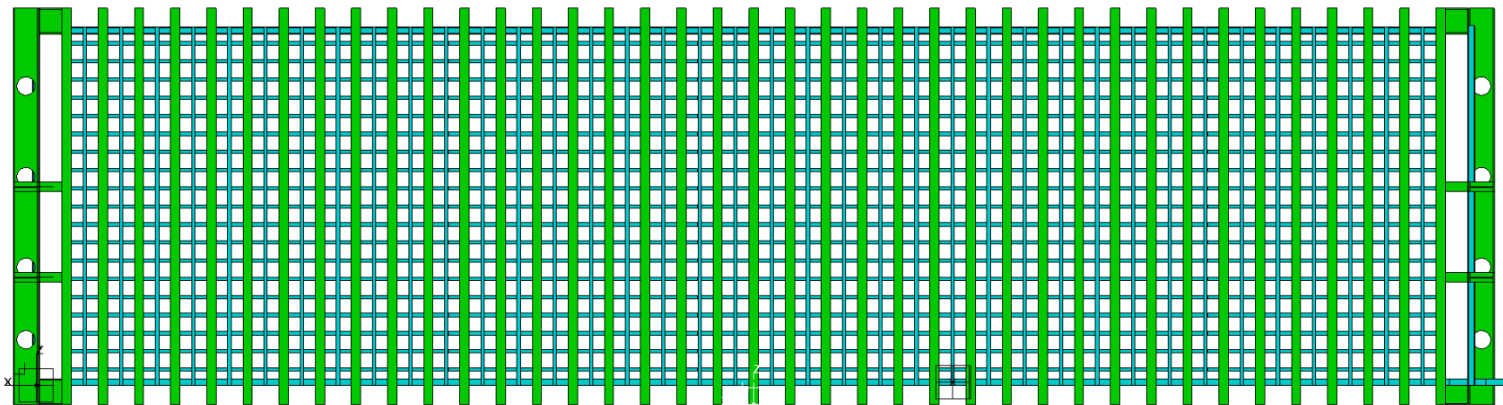
Modifications to baseline proposal

PH-DT Engineering Office, CERN

CERN, April 2015

Modified pitch and main beams

- Current baseline design doesn't match with requirements as:
 - Crane capacity exceeded (beams of 977 kg/m = 17 tons for 17.4 m length; crane capacity 10 tons)
 - Profiles are non-standard: composed girders are subject to strength capacity penalties
 - Splicing seems rather critical; size of possible preassembled corner joints limited by shaft size
- Alternative: more frequent and lighter standard beams (at shorter pitch of 1.6 m)



Similar beam (bridge) constructions



Advantages ... if it works

- Main beams are available off the shelf profiles and hot rolled
 - This can be a very important requirement for the review !
 - No capacity penalty as from composed/welded girders
 - Beam class is rather good – beams are available in different steel grades
 - HL 1100 x 607: confidence it could work (work is restarting on those)
 - HL 1100 x 548: first verifications shows it may work as well (TBC)
- Beam weigh within crane capacity (10 tons):
 - HL 1100 x 607: the longest vertical beams will (almost) cope the crane capacity: $607 \text{ kg} \times 17.4 \text{ m} = 10.56 \text{ tons}$
 - HL 1100 x 548: $548 \text{ kg} \times 17.4 \text{ m} = 9.5 \text{ tons} \rightarrow \text{OK for crane}$
- Both new beams (at new pitch) give some total weigh gain:
 - HL 1100 x 607: 37 units (instead of 25): $(37 \times 10.56) / (25 \times 17) = 8\%$
 - HL 1100 x 548: 17%
 - Plus saving on 1 grid vertical beam / unit cell
- More uniform pressure distribution on shorter grid (less bulging out)
- Moment connection at base better distributed
- Room left between main belts for access and inspection
- New beam profiles are slightly smaller in high (OK for cavern)

Shortcomings

- A new iteration on verifications is still required
- Manholes may force to adopt the heaviest of the two new beams proposed
- Some increase in the number of (bolted) joints at base and grid/belts connections
- Final unit beam weight will increase due to the above.

Work Ahead

- There is still a lot of work required for the review, and the current baseline does not cope with some main requirements (as mentioned earlier):
- We need to propose a solution without major flaws in which we have reasonable confidence.
- No time available x alternative design: this modification does not affect much the previous baseline design proposed and leaves time later for optimisation.
- Urgent no to cover the work still ahead for the review:
 - Still some verifications by FEA
 - Eurocode verifications (joints, beam capacity, stability, Scia complete model)
 - All design work: 3D model, members, joints, all details : LOT OF WORK THAT MUST START
 - All assembly / installation scenarios to be studied and documented

Poutrelles européennes à très larges ailes

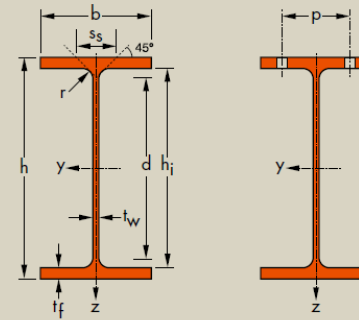
Dimensions: ASTM A 6/A 6M - 12
 Tolérances: ASTM A 6/A 6M - 12
 HL 1000 AA - M+HL 1100, EN 10034: 1993
 Etat de surface: conforme à EN 10163-3: 2004, classe C, sous-classe 1

European extra wide flange beams

Dimensions: ASTM A 6/A 6M - 12
 Tolerances: ASTM A 6/A 6M - 12
 HL 1000 AA - M+HL 1100, EN 10034: 1993
 Surface condition: according to EN 10163-3: 2004, class C, subclass 1

Europäische Träger mit besonders breiten Flanschen

Abmessungen: ASTM A 6/A 6M - 12
 Toleranzen: ASTM A 6/A 6M - 12
 HL 1000 AA - M+HL 1100, EN 10034: 1993
 Oberflächenbeschaffenheit: Gemäß EN 10163-3: 2004, Klasse C, Untergruppe 1



Désignation Designation Bezeichnung	Dimensions Abmessungen						Dimensions de construction Dimensions for detailing Konstruktionsmaße						Surface Oberfläche	
	G	h	b	t _w	t _f	r	A	h _i	d	Ø	p _{min}	p _{max}	A _L	A _G
kg/m	mm	mm	mm	mm	mm	mm	mm ²	mm	mm	mm	mm	mm	m ² /m	m ² /t
HL 1100 A*	343	1090	400	18,0	31,0	20	436,5	1028	988,0	M 27	116	294	3,710	10,83
HL 1100 B*	390	1100	400	20,0	36,0	20	497,0	1028	988,0	M 27	118	294	3,726	9,549
HL 1100 M*	433	1108	402	22,0	40,0	20	551,2	1028	988,0	M 27	120	296	3,746	8,657
HL 1100 R*	499	1118	405	26,0	45,0	20	635,2	1028	988,0	M 27	124	300	3,770	7,560
HL 1100 x 548**/A	548	1128	407	28,0	50,0	20	698,3	1028	988,0	M27	126	302	3,794	6,921
HL 1100 x 607**/A	607	1138	410	31,0	55,0	20	773,1	1028	988,0	M27	128	304	3,820	6,294

Notations pages 215-219 / Bezeichnungen Seiten 215-219

Désignation Designation Bezeichnung	Valeurs statiques / Section properties / Statische Kennwerte											Classification EN 1993-1-1: 2005											
	axe fort y-y strong axis y-y starke Achse y-y					axe faible z-z weak axis z-z schwache Achse z-z					Pure bending y-y			Pure compression									
	G	I _y	W _{el,y}	W _{pl,y} ♦	I _y	A _{ve}	I _z	W _{el,z}	W _{pl,z} ♦	I _z	s _s	I _t	I _w	S235	S355	S460	S235	S355	S460	EN 10025-2: 2004	EN 10025-4: 2004	EN 10225: 2009	
kg/m	mm ⁴	mm ³	mm ³	mm	mm ²	mm ⁴	mm ³	mm ³	mm	mm	mm ⁴	mm ⁶	x10 ³	x10 ³	x10 ³	x10 ³	x10 ³	x10 ³	x10 ³	x10 ³	x10 ³	x10 ³	x10 ³
HL 1100 A	343	867400	15920	18060	44,58	206,5	33120	1656	2568	8,71	103,4	1037	92710	1	1	2	4	4	4	✓	HI	HI	
HL 1100 B	390	1005000	18280	20780	44,98	230,6	38480	1924	2988	8,80	115,4	1564	108700	1	1	1	4	4	4	✓	HI	HI	
HL 1100 M	433	1126000	20320	23160	45,19	254,4	43410	2160	3362	8,87	125,4	2130	123500	1	1	1	4	4	4	✓	HI	HI	
HL 1100 R	499	1294000	23150	26600	45,14	300,4	49980	2468	3870	8,87	139,4	3135	143400	1	1	1	2	4	4	✓	HI		
HL 1100 x 548	548	1446000	25630	29510	45,50	325,3	56380	2771	4349	8,99	151,4	4205	163200	1	1	1	2	4	4	✓	HI		
HL 1100 x 607	607	1613000	28350	32790	45,68	361,2	63450	3095	4877	9,06	164,4	5628	185300	1	1	1	1	3	4	✓	HI		

HI = HISTAR®



Steel Grades

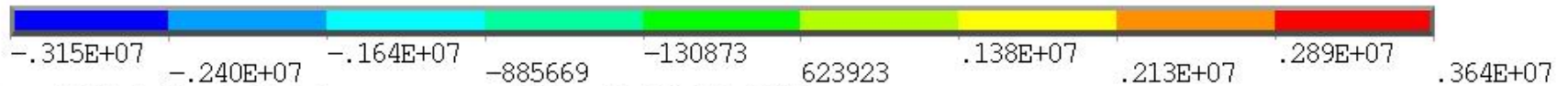
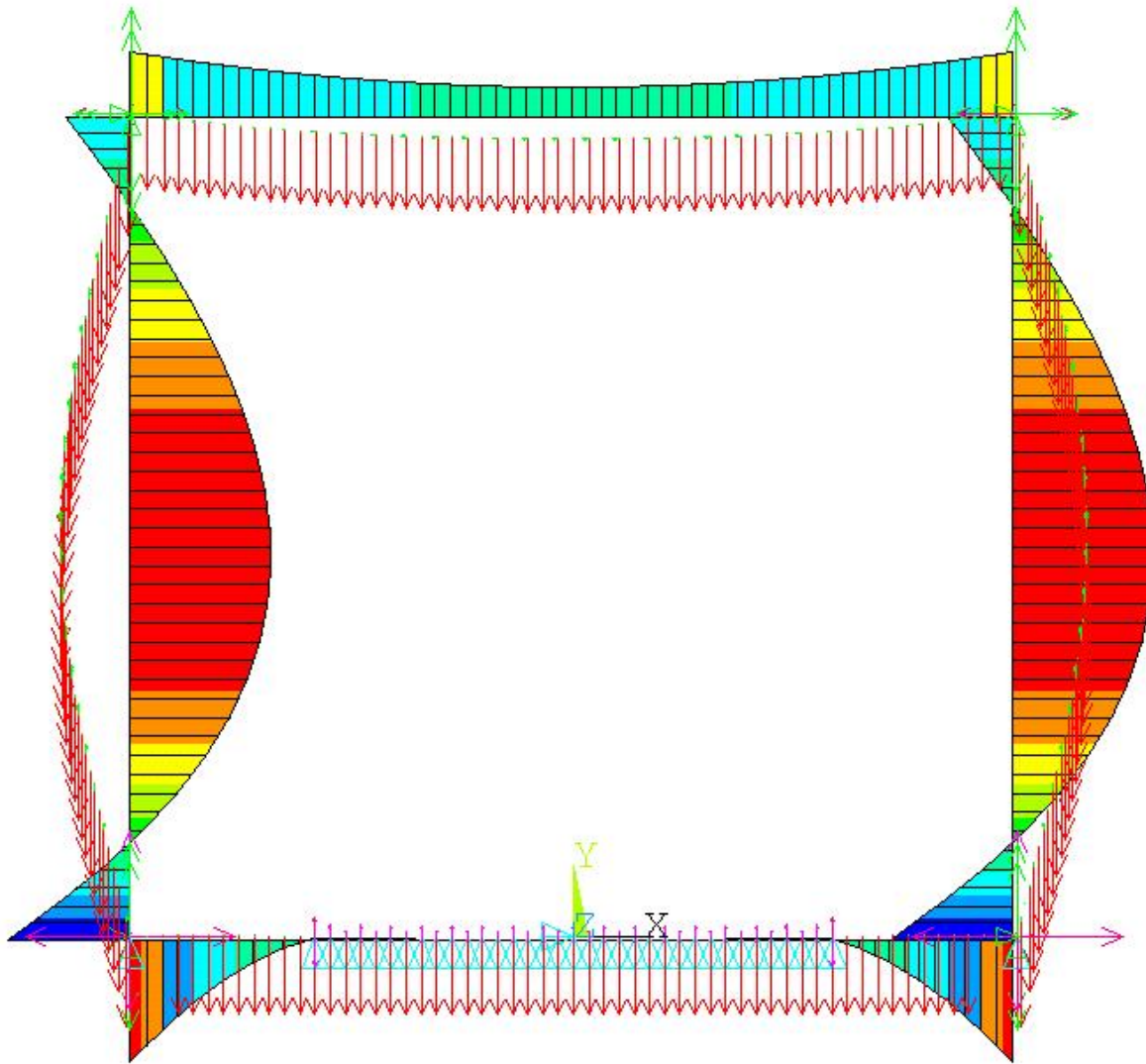
- Steel S355 (EC properties for $t > 40\text{mm}$)
 - $\sigma_y = 335\text{ MPa} \rightarrow \sigma_y/1.5 = 223\text{ MPa}$
 - $\text{UTS} = 470\text{ MPa} \rightarrow \text{UTS}/3.5 = 134\text{ MPa}$
- Small Improvements by moving to S450 (EC properties for $t > 40\text{mm}$):
 - $\sigma_y = 410\text{ MPa} \rightarrow \sigma_y/1.5 = 273.3\text{ MPa}$
 - $\text{UTS} = 550\text{ MPa} \rightarrow \text{UTS}/3.5 = 157\text{ MPa}$

APR 29 2015
15:55:49
PLOT NO. 1

1 LINE STRESS

STEP=1
SUB =1
TIME=1
MYI MYJ
MIN =-.315E+07
ELEM=1
MAX =.364E+07
ELEM=13

- U
- F
- CP
- NFOR
- NMOM
- RFOR



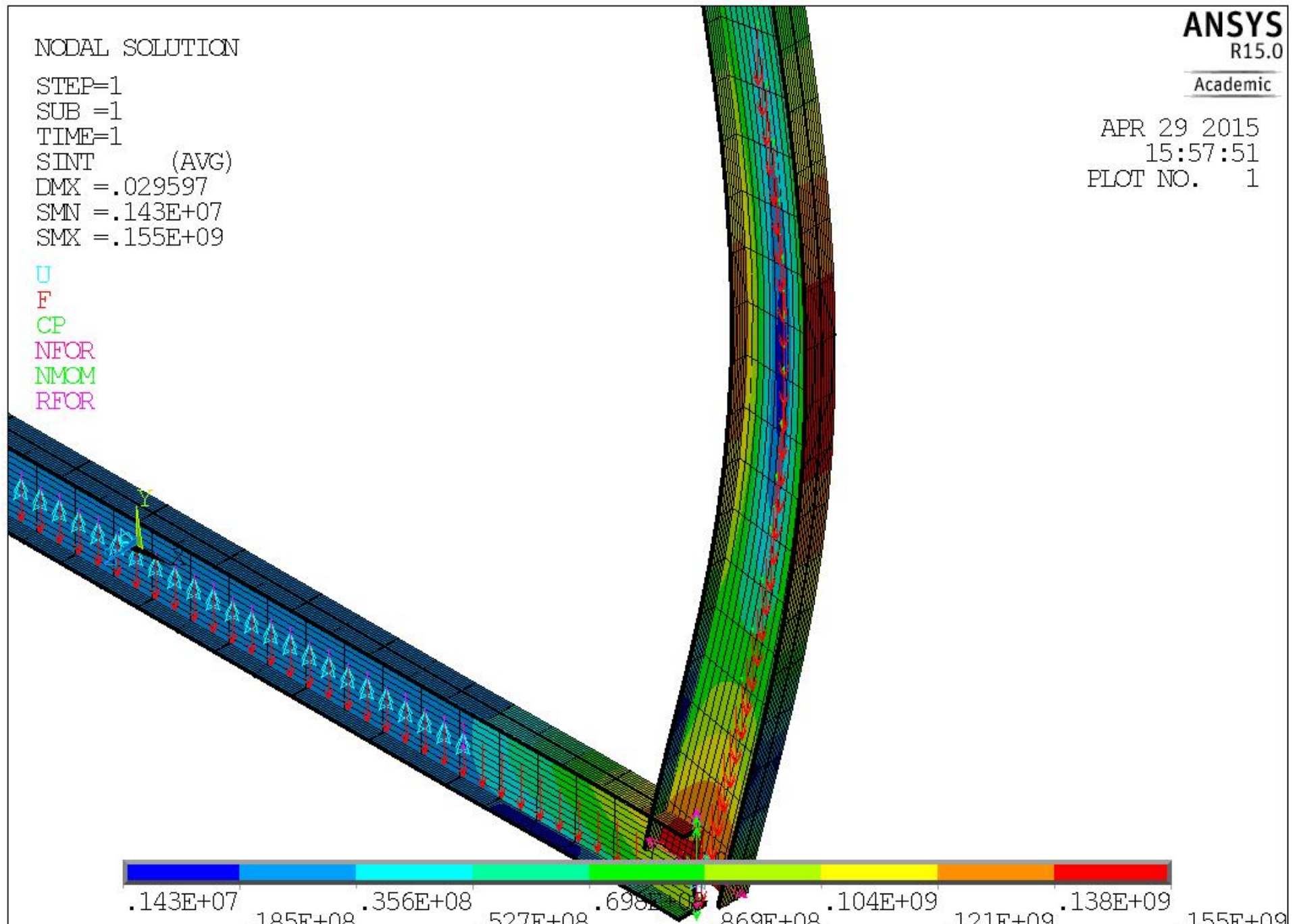
Neutrino LBNF Portal Frame - profile HL1100-548

APR 29 2015
15:57:51
PLOT NO. 1

NODAL SOLUTION

STEP=1
SUB =1
TIME=1
SINT (AVG)
DMX =.029597
SMN =.143E+07
SMX =.155E+09

U
F
CP
NFOR
NMOM
RFOR



.143E+07 .185E+08 .356E+08 .527E+08 .698E+08 .869E+08 .104E+09 .121E+09 .138E+09 .155E+09

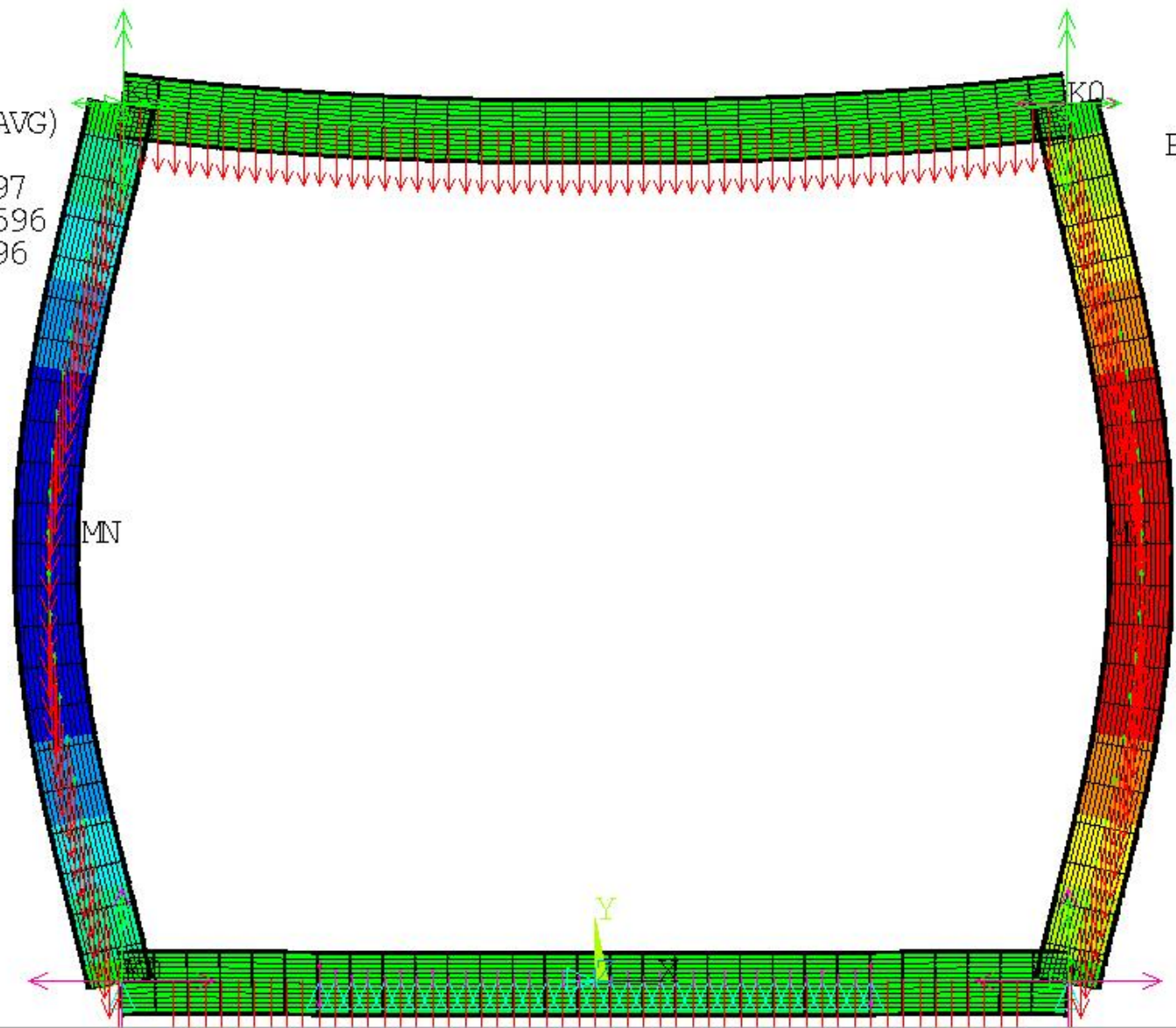
Neutrino LBNF Portal Frame - profile HL1100-548

APR 29 2015
15:58:34
PLOT NO. 1

1 NODAL SOLUTION

STEP=1
SUB =1
TIME=1
UX (AVG)
RSYS=0
DMX =.029597
SMN =-.029596
SMX =.029596

- U
- F
- CP
- NFOR
- NMOM
- RFOR

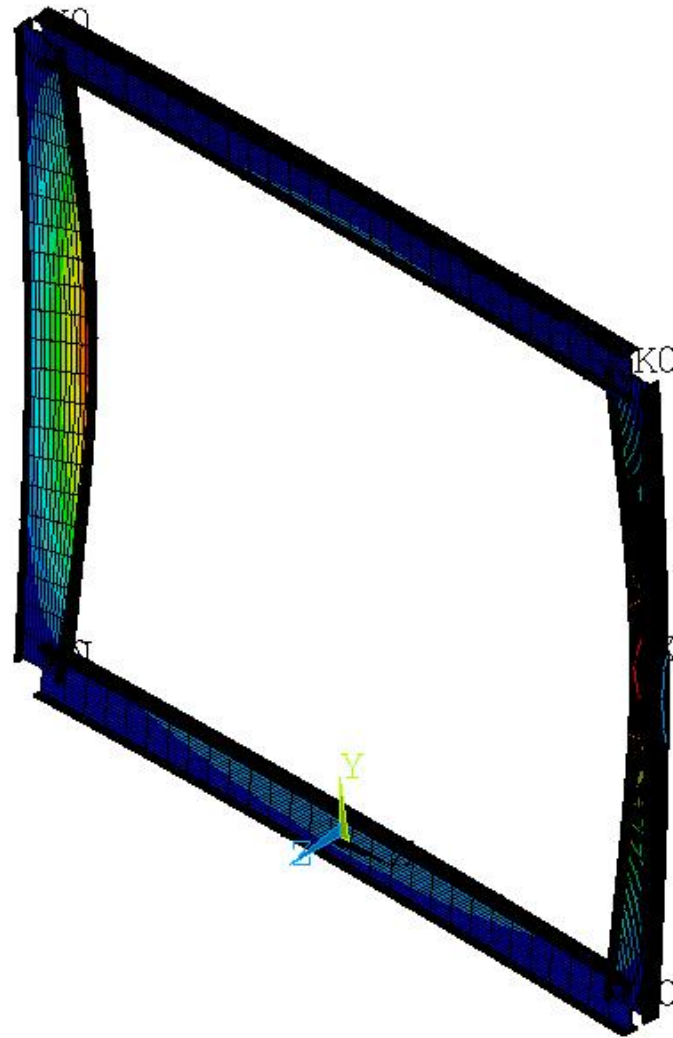


Neutrino LBNF Portal Frame - profile HL1100-548

APR 29 2015
16:05:07
PLOT NO. 1

1 NODAL SOLUTION

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SUB =1
FACT=1.15955
USUM (AVG)
RSYS=0
DMX =1.34087
SMN =.890E-12
SMX =1.34087



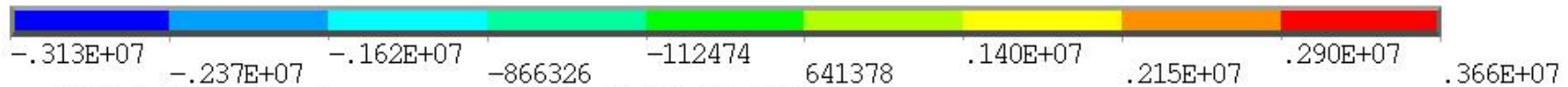
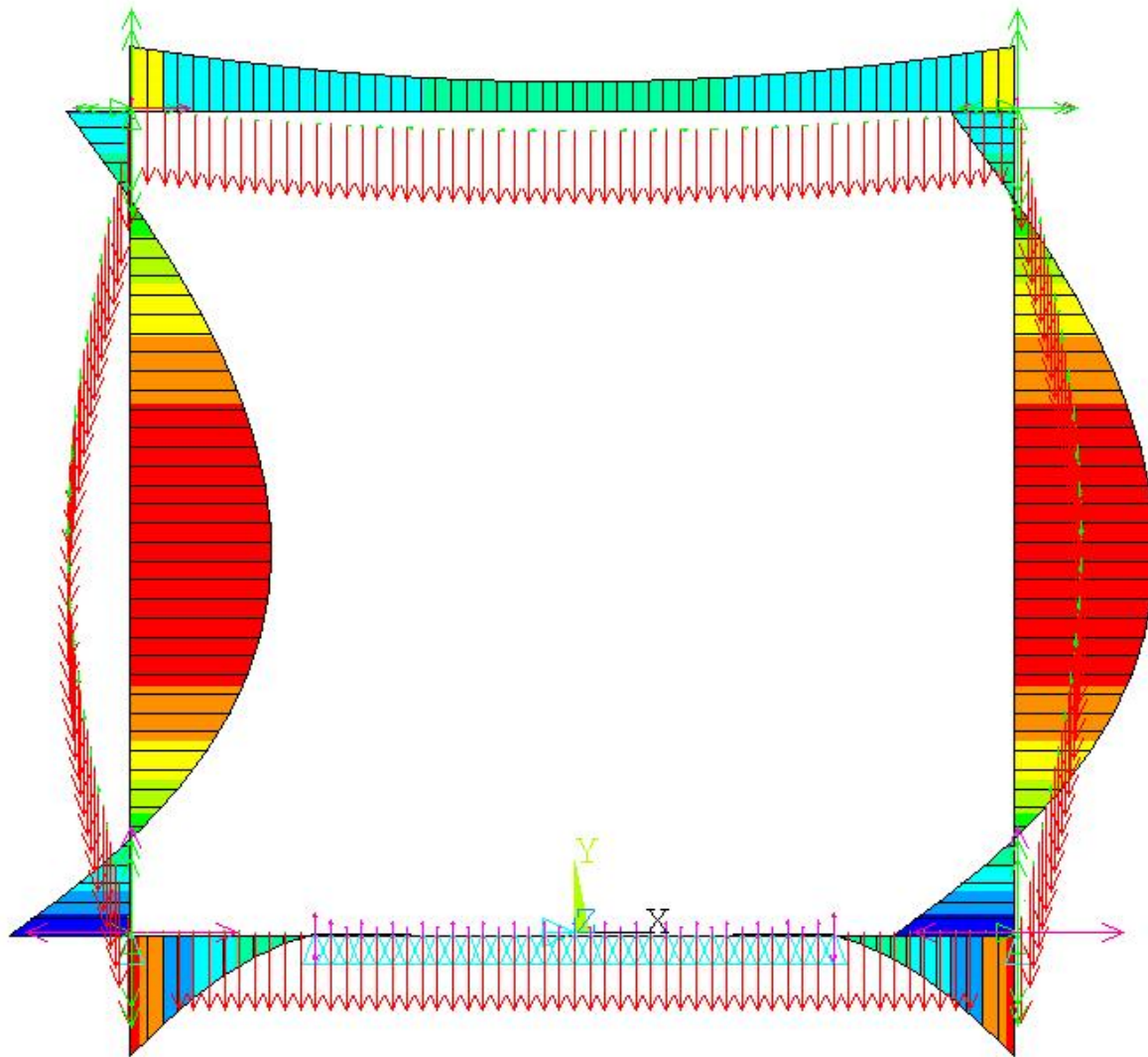
Neutrino LBNF Portal Frame - profile HL1100-548 - buckling

APR 29 2015
16:15:09
PLOT NO. 1

1 LINE STRESS

STEP=1
SUB =1
TIME=1
MYI MYJ
MIN =-.313E+07
ELEM=1
MAX =.366E+07
ELEM=13

- U
- F
- CP
- NFOR
- NMOM
- RFOR



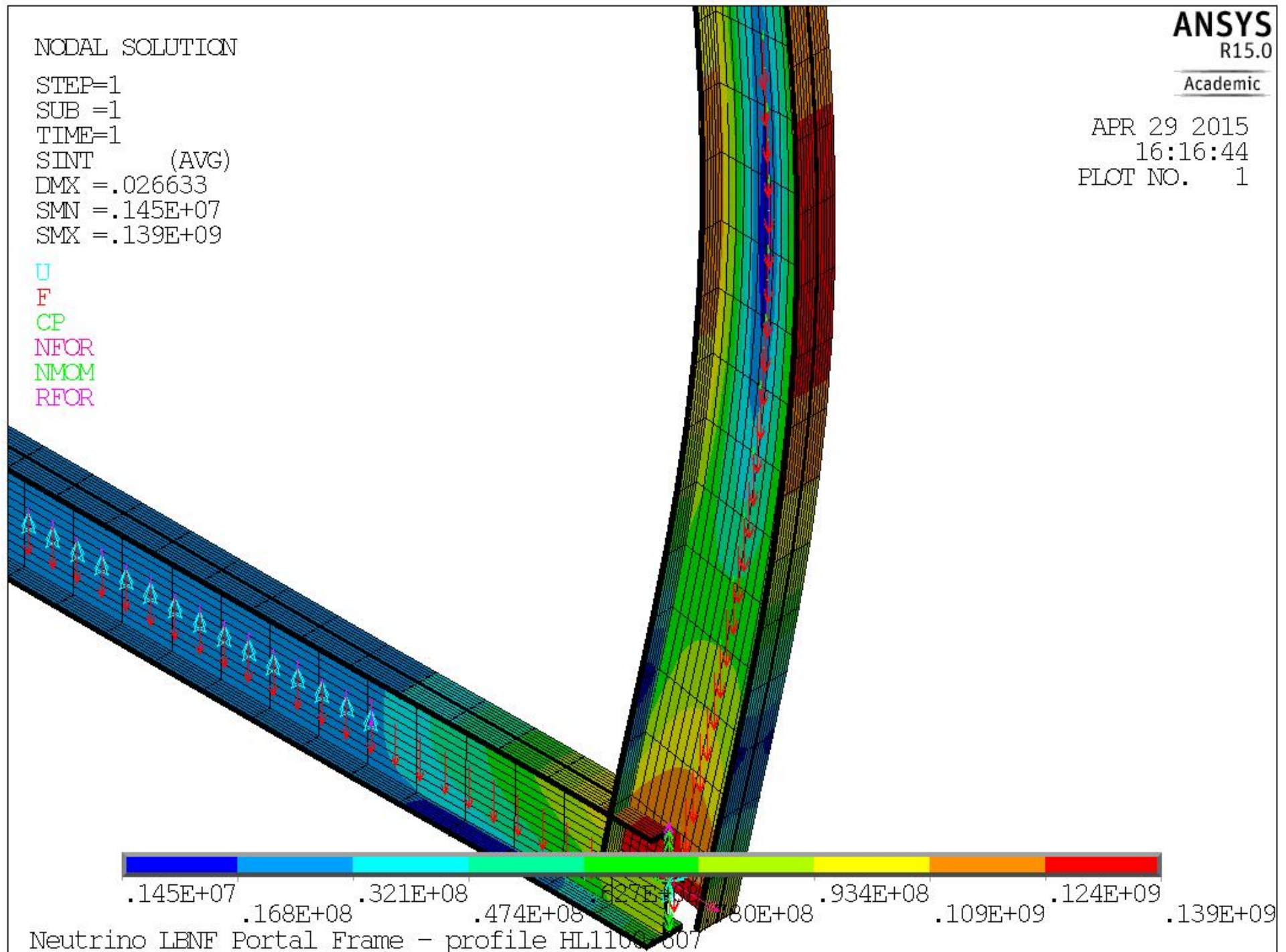
Neutrino LBNF Portal Frame - profile HL1100-607

APR 29 2015
16:16:44
PLOT NO. 1

NODAL SOLUTION

STEP=1
SUB =1
TIME=1
SINT (AVG)
DMX =.026633
SMN =.145E+07
SMX =.139E+09

- U
- F
- CP
- NFOR
- NMOM
- RFOR



.145E+07 .168E+08 .321E+08 .474E+08 .627E+08 .80E+08 .934E+08 .109E+09 .124E+09 .139E+09

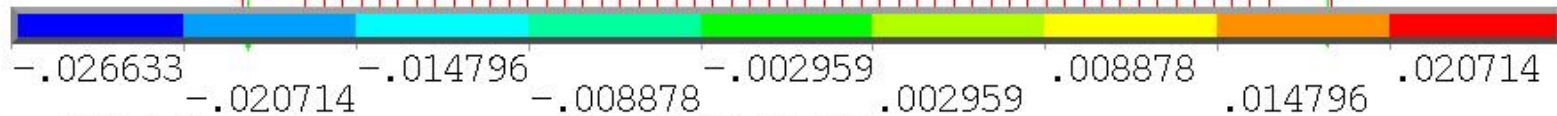
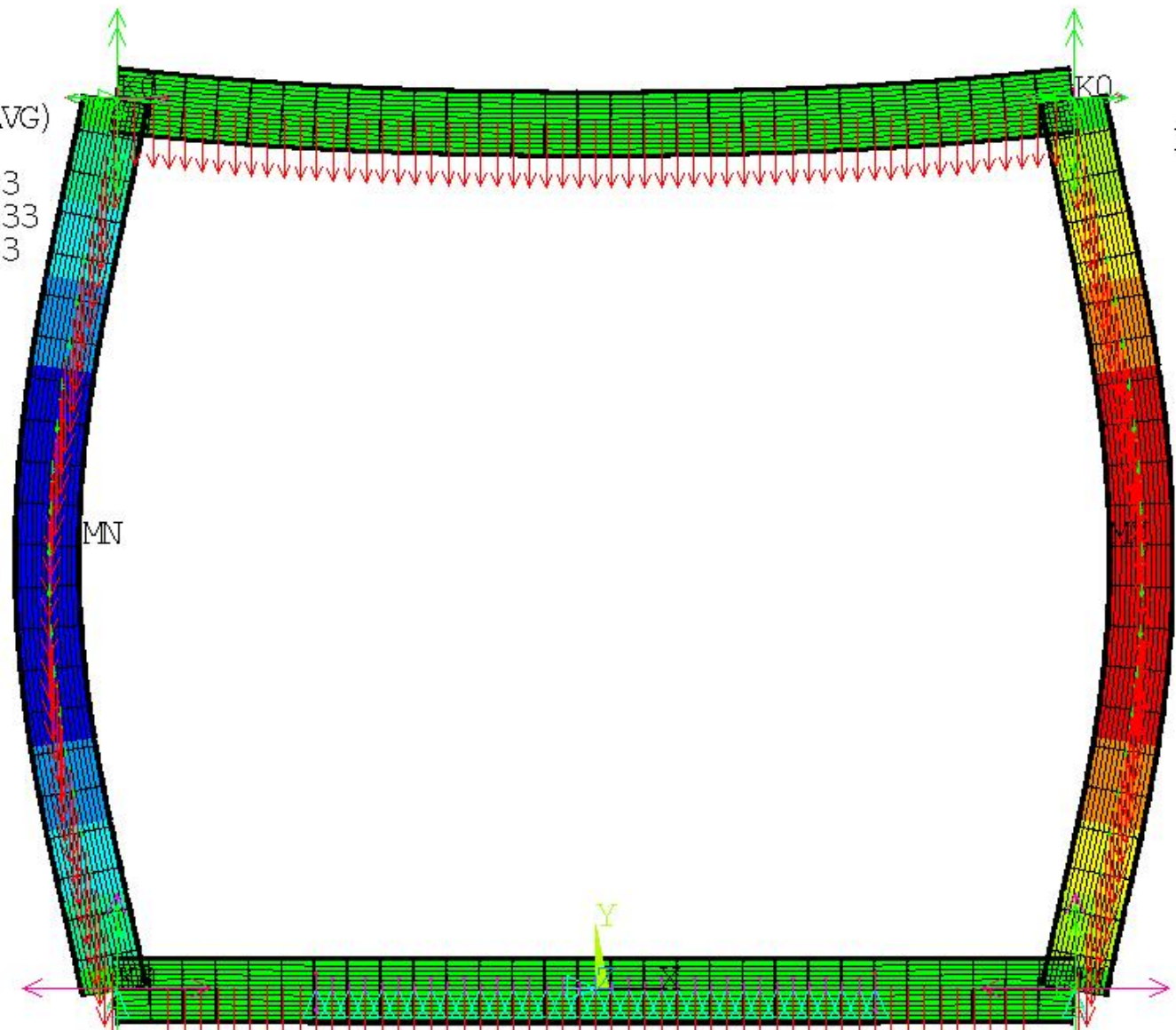
Neutrino LBNF Portal Frame - profile HL1100 507

APR 29 2015
16:15:39
PLOT NO. 1

1 NODAL SOLUTION

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SUB =1
TIME=1
UX (AVG)
RSYS=0
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SMN =-.026633
SMX =.026633

- U
- F
- CP
- NFOR
- NMOM
- RFOR

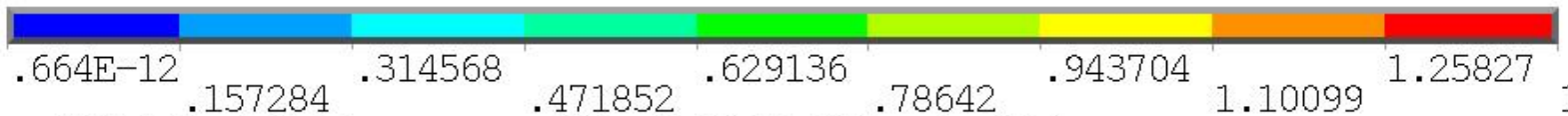
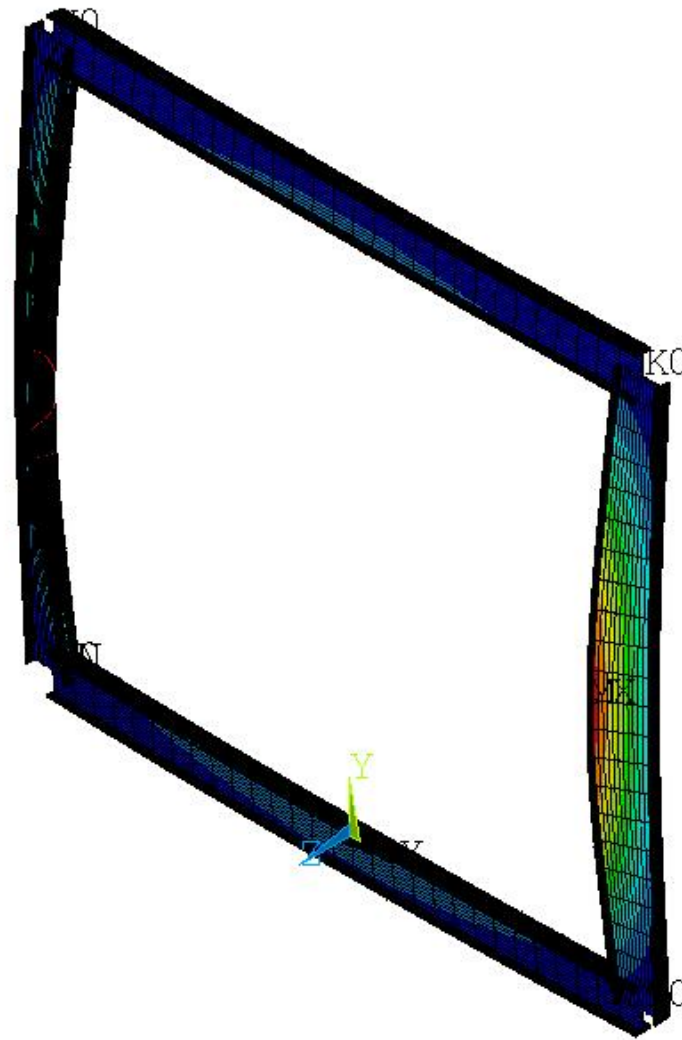


Neutrino LBNF Portal Frame - profile HL1100-607

APR 29 2015
16:19:35
PLOT NO. 1

1 NODAL SOLUTION

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SUB =1
FACT=1.40968
USUM (AVG)
RSYS=0
DMX =1.41556
SMN =.664E-12
SMX =1.41556



.664E-12 .157284 .314568 .471852 .629136 .78642 .943704 1.10099 1.25827 1.41556

Neutrino LBNF Portal Frame - profile HL1100-607 - buckling