

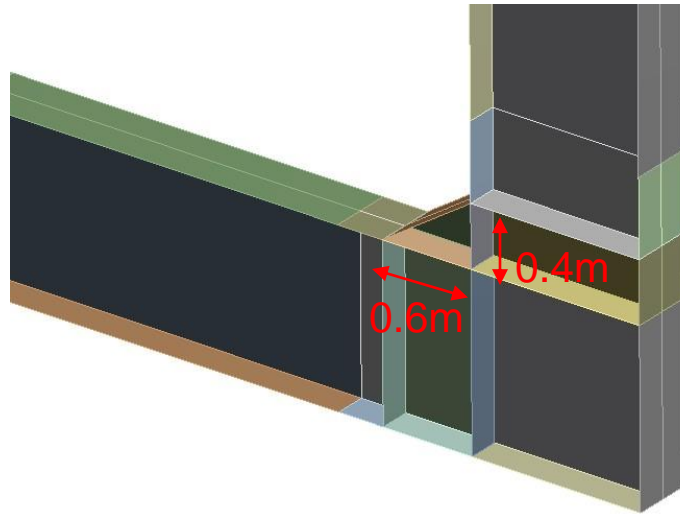
Connections: FEA

PH-DT Engineering Office, CERN

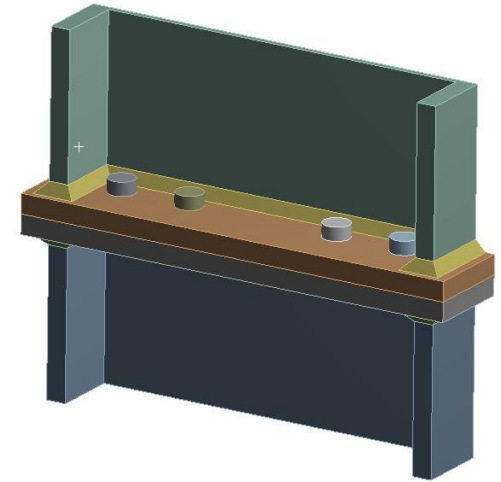
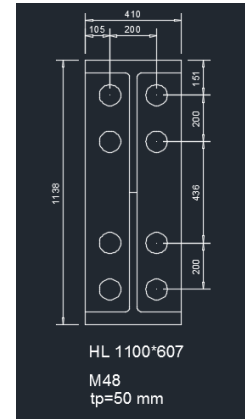
CERN, May 2015

Splice Connection

- Combination of two splice connections and a pre-manufactured L-shaped moment connection at the bottom



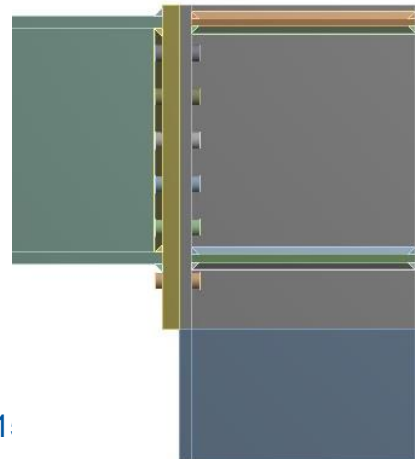
Pre-manufactured, L-Shaped Connection



Splice Connection

Vertical positions of the splice connections to be carefully selected so as to minimise the bending moment that they must withstand

- Top Connection: Pinned or Moment Connection?



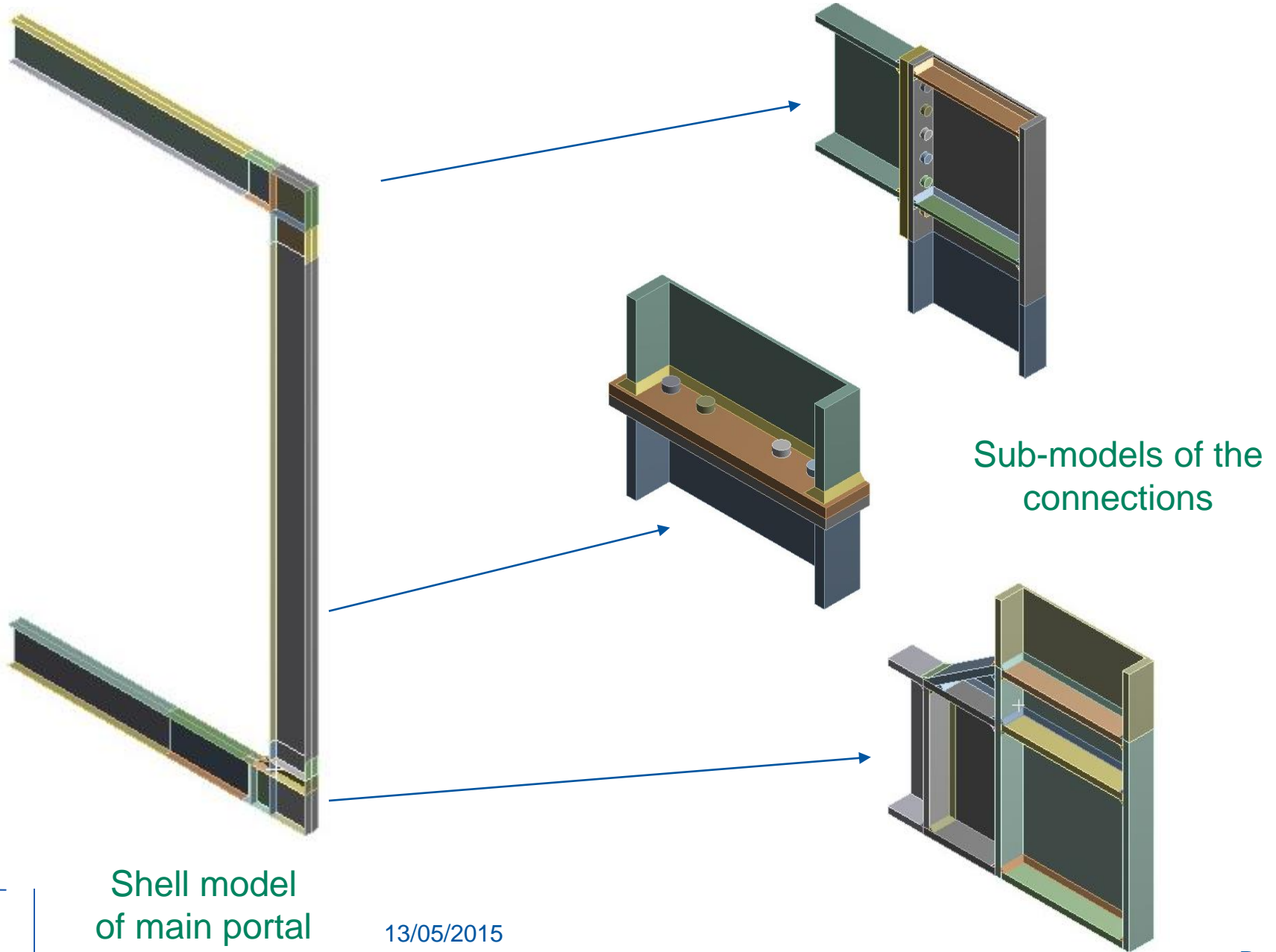
Joint Validation: Proposed FEA Methodology

1. Extract rotational stiffness of bottom (“pre-manufactured”) and top (bolted) connections (i.e. K_{bot} and K_{top} respectively) using detailed joint models or analytical EC3 calculations.
2. Introduce the values of K_{bot} and K_{top} in a beam model of the main frame to obtain the bending moment distribution along the main vertical beam.
 - Initial position for the splice connection corresponds to the location of the zero-bending moment.
3. Run a shell model of the main portal. (The bottom connection will be explicitly included in this model, but the imperfect nature of the top connection should be accounted for via a revolute joint with rotational stiffness equal to K_{top}).
4. Use the results of step 3 to run a **sub-model of the various connection** and evaluate the **stresses in the bolts/welds**. The nominal position of the splice connection would correspond to that extracted in step 2, but a sensitivity analysis should be performed to assess the effect of the positional error. Bolt pre-tension and **nominal** loads should be taken into account in this step.

Joint Validation: Proposed FEA Methodology

- The rotational stiffness of the top and bottom connections in the full shell model seems very close to that extracted from the detailed analysis (numerical and analytical) when they operate below their maximum capacity.
 - ↳ Bypass the beam model and work directly with the full shell model of the main portal to determine the optimum position of the splice connection and the imported BCs for the top and bottom joints (K_{bot} and K_{top} are directly included in the model).
1. Run a shell model of the main portal.
 - ↳ Determine the initial position of the vertical splice, which corresponds to the location of the zero-bending moment.
 2. Use the results of step 3 to run **sub-models of the various connection** and evaluate the **stresses in the bolts/welds**. The nominal position of the splice connection would correspond to that extracted in step 2, but a sensitivity analysis should be performed to assess the effect of the positional error. Bolt pre-tension and **nominal** loads should be taken into account in this step.

Joint Validation: Proposed FEA Methodology

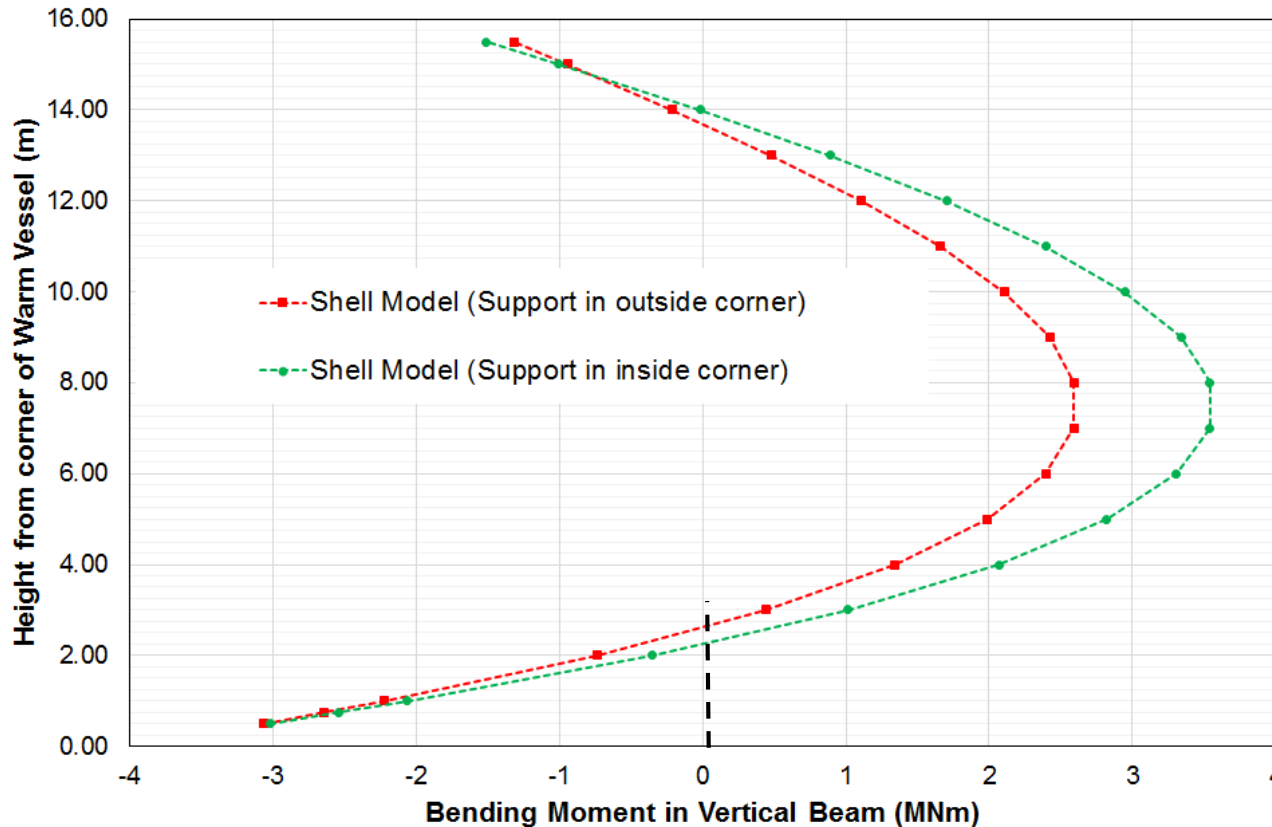
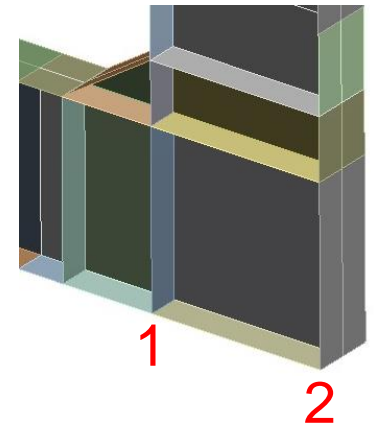


Shell model
of main portal

13/05/2015

Shell Frame: Preliminary Results

- Significant effect of the location of the local vertical support for the bottom corner
 - Case 1: Support inside corner → Optimum position ~2.25m
 - Case 2: Support outside corner → Optimum position ~2.65m

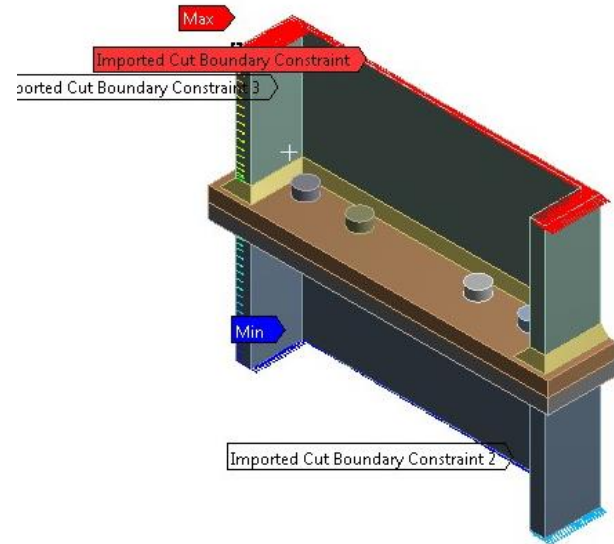
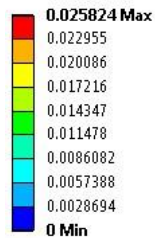


* The length shown in the graph is measured from the internal corner of the box. So, for 2.25m the total height of the bottom joint would be $2.25 + 1.138 = 3.388\text{m}$ from the floor (assuming that the bottom beam remains HL 1100x607)

Joint Validation: Shell Frame + Sub-modelling

- Analysis of the all-shell frame with nominal loads
- Sub-modelling of the various connections (.

A: Static Structural
Total Deformation
Type: Total Deformation
Unit: m
Time: 1
11/05/2015 22:55

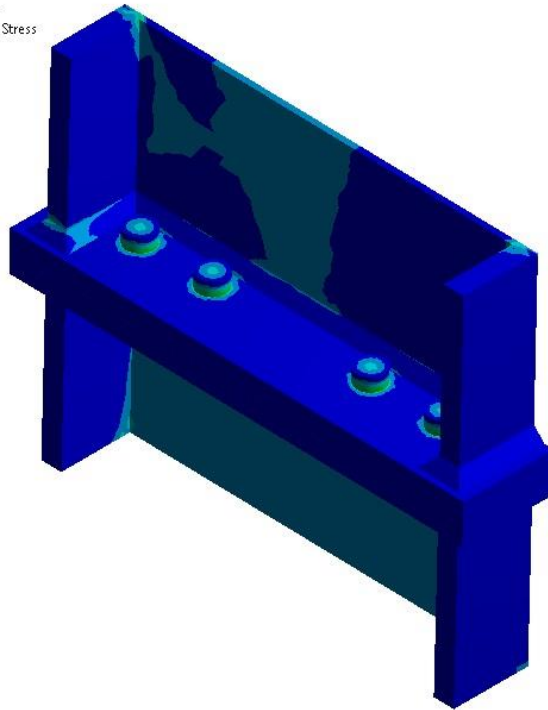
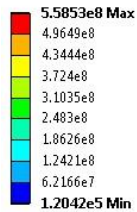


- Imported BCs for the corresponding position (parametric)
- Frictional contacts ($\mu=0.25$)
- Welds (30mm)
- Non-linear materials (S355 for beams, 10.9 for bolts)
- Bolt Pre-tension=625kN (M48)
- No washers

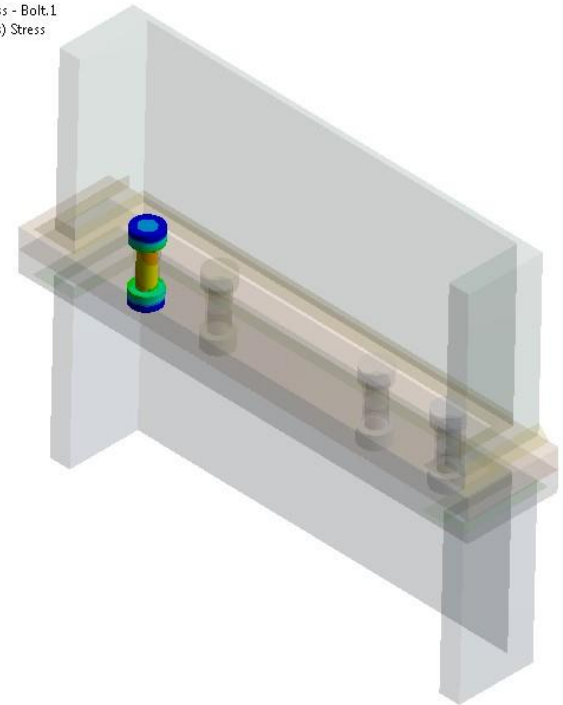
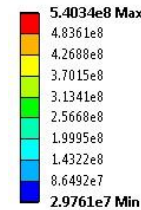
Case 1: Splice Connection Analysis

- Nominal Position: 2.25m from inside corner
- Good News!!
 - For the optimal position of the splice connection, even the peak stresses in the bolts & welds are below $2/3 \sigma_y$.
 - Average Stresses to be calculated next according to ASME

B: Model, Static Structural
Equivalent (von-Mises) Stress
Type: Equivalent (von-Mises) Stress
Unit: Pa
Time: 3
11/05/2015 23:11



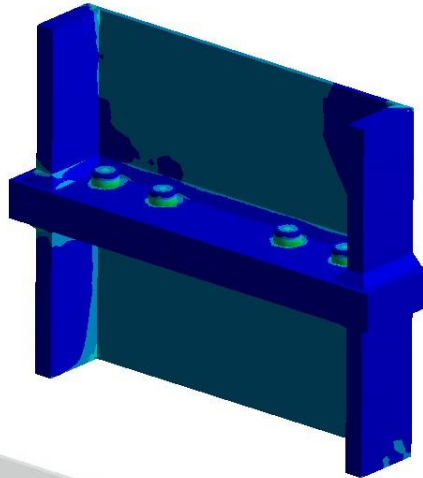
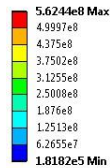
B: Model, Static Structural
Equivalent (von-Mises) Stress - Bolt.1
Type: Equivalent (von-Mises) Stress
Unit: Pa
Time: 3
11/05/2015 23:12



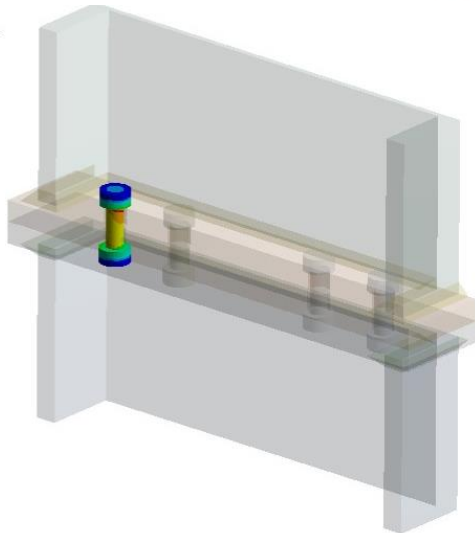
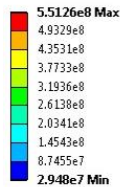
Case 1: Splice Connection Analysis

- Variation of the position of the spliced joint $\pm 500\text{mm}$ (i.e. position 1.75m and 2.75m) and repeated the analysis.
 - Even the peak stresses in bolts & welds remain below $2/3 \sigma_v$

B: Model, Static Structural
Equivalent (von-Mises) Stress
Type: Equivalent (von-Mises) Stress
Unit: Pa
Time: 3
11/05/2015 23:27



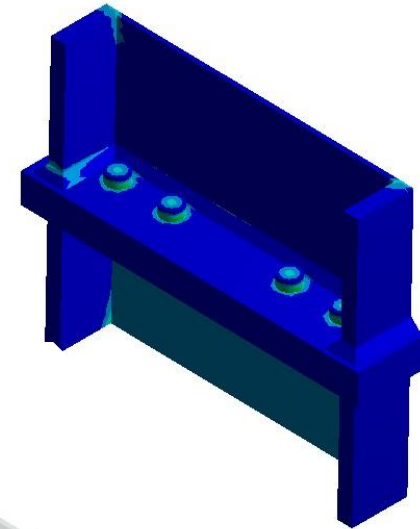
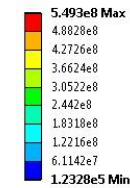
B: Model, Static Structural
Equivalent (von-Mises) Stress - Bolt.1
Type: Equivalent (von-Mises) Stress
Unit: Pa
Time: 3
11/05/2015 23:28



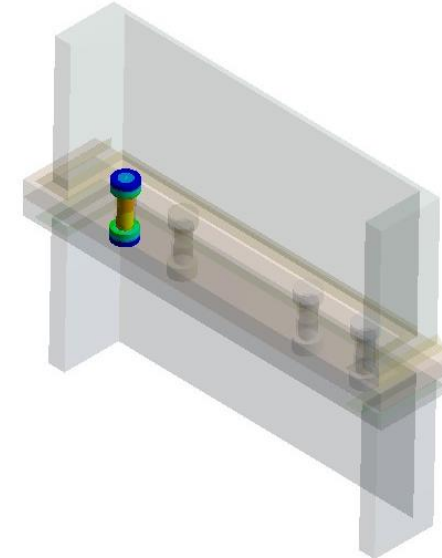
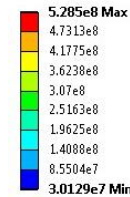
~1.75m

13/05/2015

B: Model, Static Structural
Equivalent (von-Mises) Stress
Type: Equivalent (von-Mises) Stress
Unit: Pa
Time: 3
11/05/2015 23:20



B: Model, Static Structural
Equivalent (von-Mises) Stress - Bolt.1
Type: Equivalent (von-Mises) Stress
Unit: Pa
Time: 3
11/05/2015 23:20



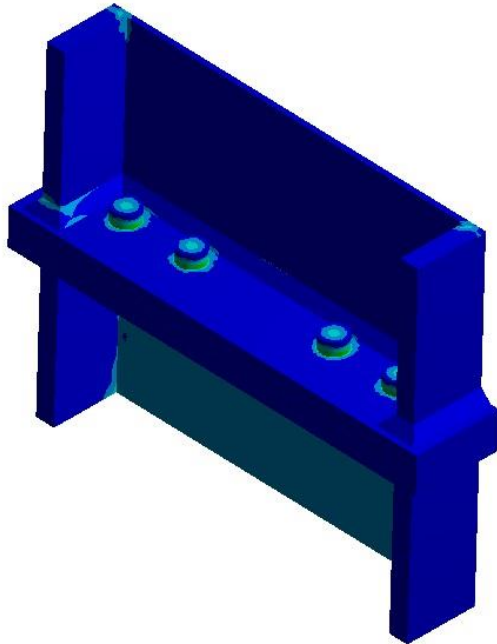
~2.75m

Case 2: Splice Connection Analysis

- Nominal Position: 2.65m from inside corner

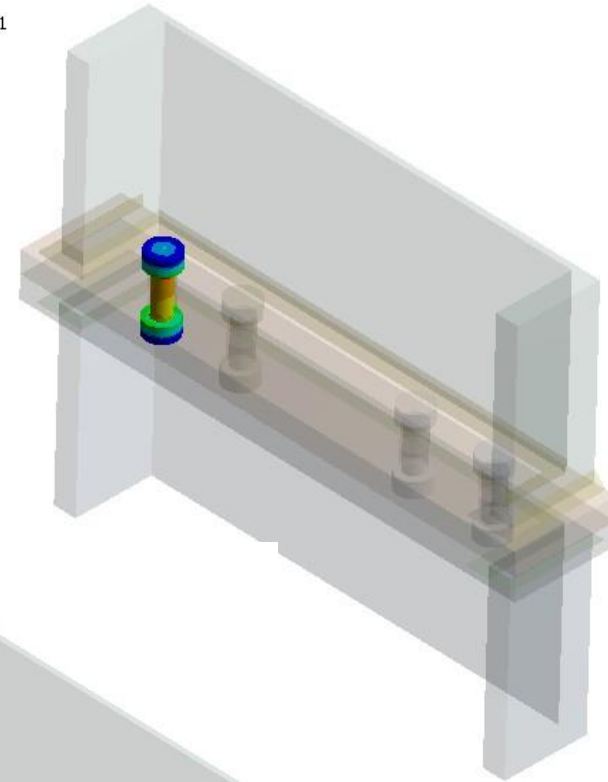
B: Splice Connection
Equivalent (von-Mises) Stress
Type: Equivalent (von-Mises) Stress
Unit: Pa
Time: 3
13/05/2015 16:50

5.3609e8 Max
4.7653e8
4.1698e8
3.5743e8
2.9787e8
2.3832e8
1.7876e8
1.1921e8
5.9652e7
97736 Min



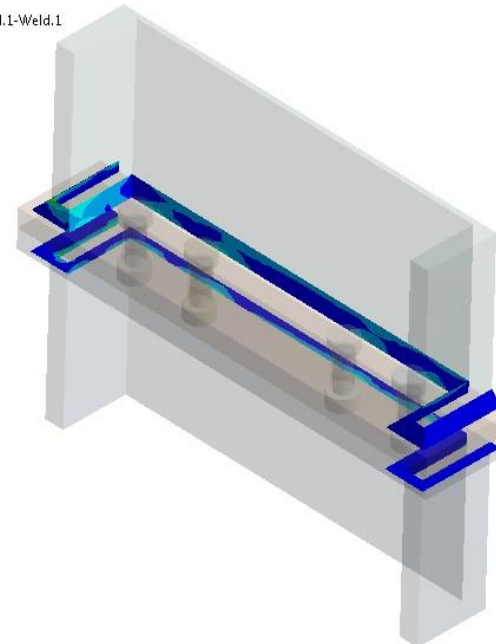
B: Splice Connection
Equivalent (von-Mises) Stress - Bolt.1
Type: Equivalent (von-Mises) Stress
Unit: Pa
Time: 3
13/05/2015 16:50

5.2599e8 Max
4.7092e8
4.1584e8
3.6076e8
3.0568e8
2.5061e8
1.9553e8
1.4045e8
8.5377e7
3.03e7 Min



B: Splice Connection
Equivalent (von-Mises) Stress - Weld.1-Weld.1
Type: Equivalent (von-Mises) Stress
Unit: Pa
Time: 3
13/05/2015 16:51

2.6851e8 Max
2.3872e8
2.0893e8
1.7913e8
1.4934e8
1.1954e8
8.9751e7
5.9958e7
3.0164e7
3.7086e5 Min



Case 2: Bottom Connection Analysis

C: L-Shape Connection

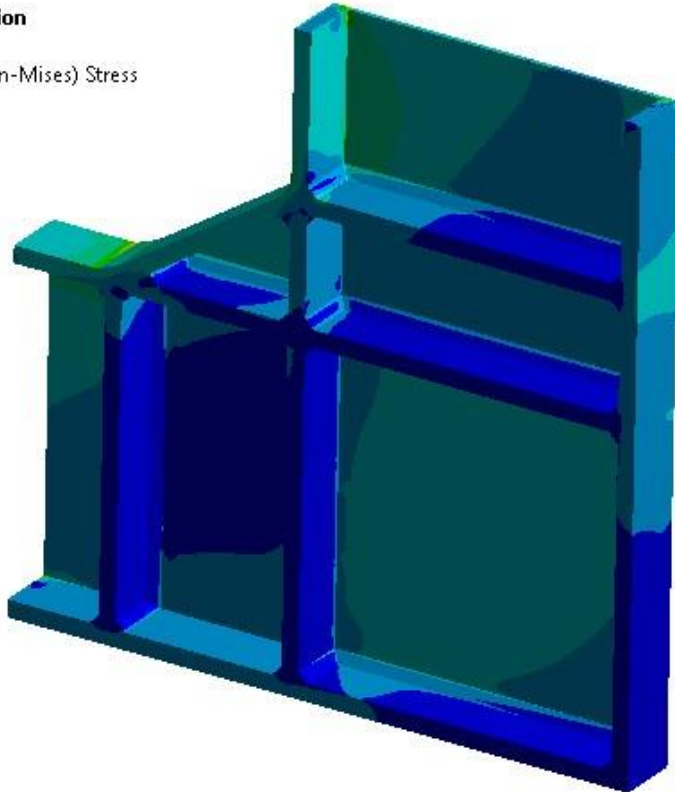
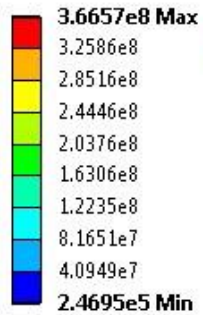
Equivalent Stress

Type: Equivalent (von-Mises) Stress

Unit: Pa

Time: 1

13/05/2015 16:53



C: L-Shape Connection

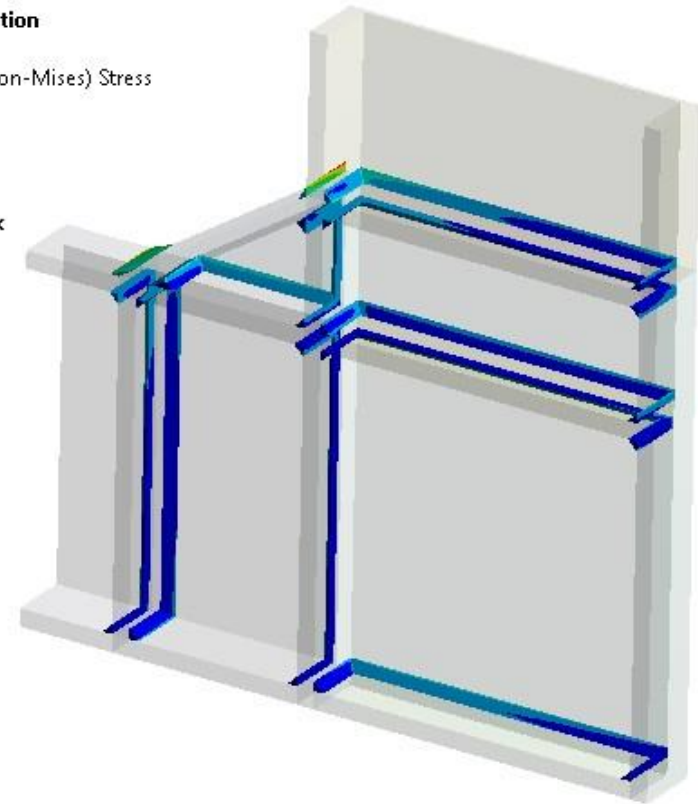
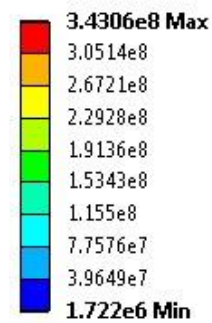
Equivalent Stress 2

Type: Equivalent (von-Mises) Stress

Unit: Pa

Time: 1

13/05/2015 16:54



Case 2: Top Connection Analysis

