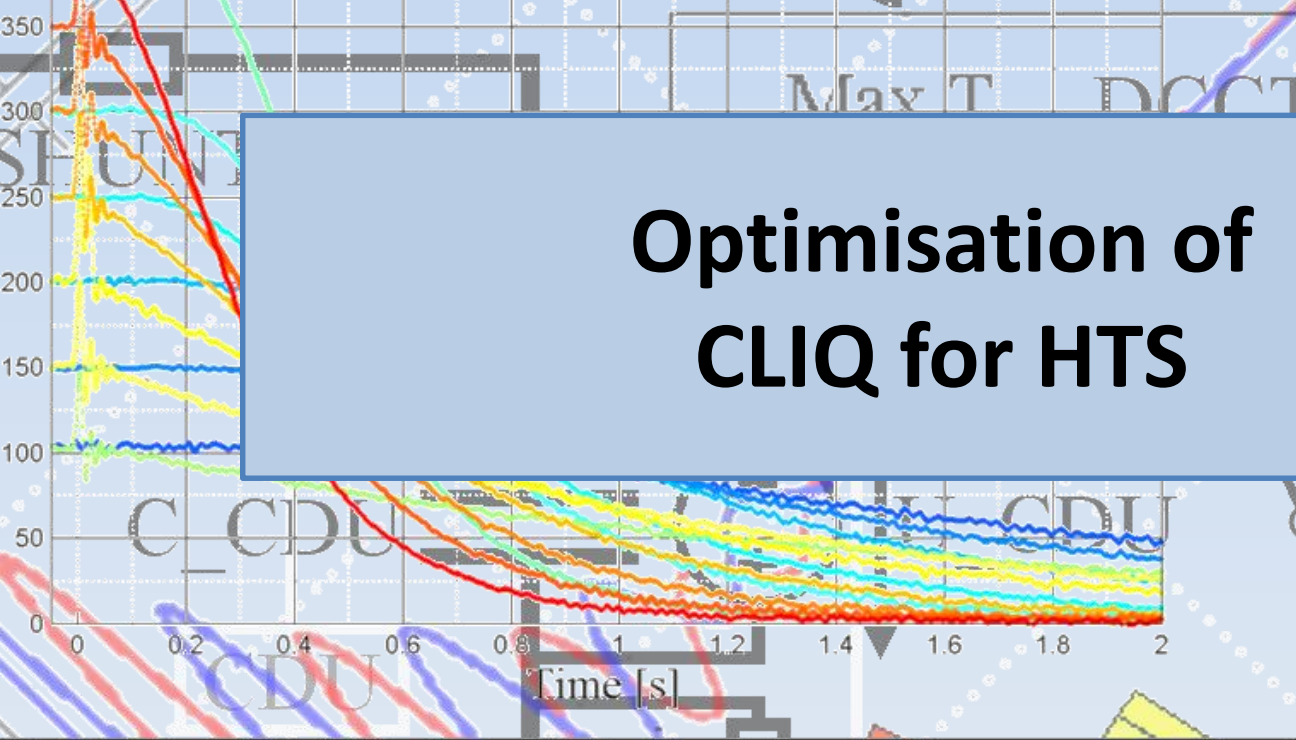


# Optimisation of CLIQ for HTS



11 September 2015

Emmanuele Ravaioli (CERN, University of Twente)  
Jeroen Van Nugteren (CERN, University of Twente)

Thanks to H.H.J. ten Kate, G. Kirby and A.P. Verweij



Before we begin..

**DISCLAIMER**

**I am not an expert of HTS!**

What  
is CLIQ

AC loss  
in HTS

CLIQ  
optimization  
(valid for  
any magnet)

Possible  
game  
changers

First study case  
of CLIQ on HTS  
(Ravaioli &  
Van Nugteren)

CLIQ with  
external  
excitation  
coils

# HTS – Challenges for effective quench protection

Very low normal-zone propagation velocity ( $\sim\text{cm/s}$ ): bad for detection, bad for protection

Very high margin to quench ( $\sim\text{J/cm}^3$ ): good for stability, bad for protection

Slower quench detection

Faster rise of the hot-spot temperature

Less homogeneous transition to the normal state:  
Thermal stress (?), Less uniform coil-to-ground voltages

# What is CLIQ

**What  
is  
CLIQ**

AC loss  
in HTS

CLIQ  
optimization  
(valid for  
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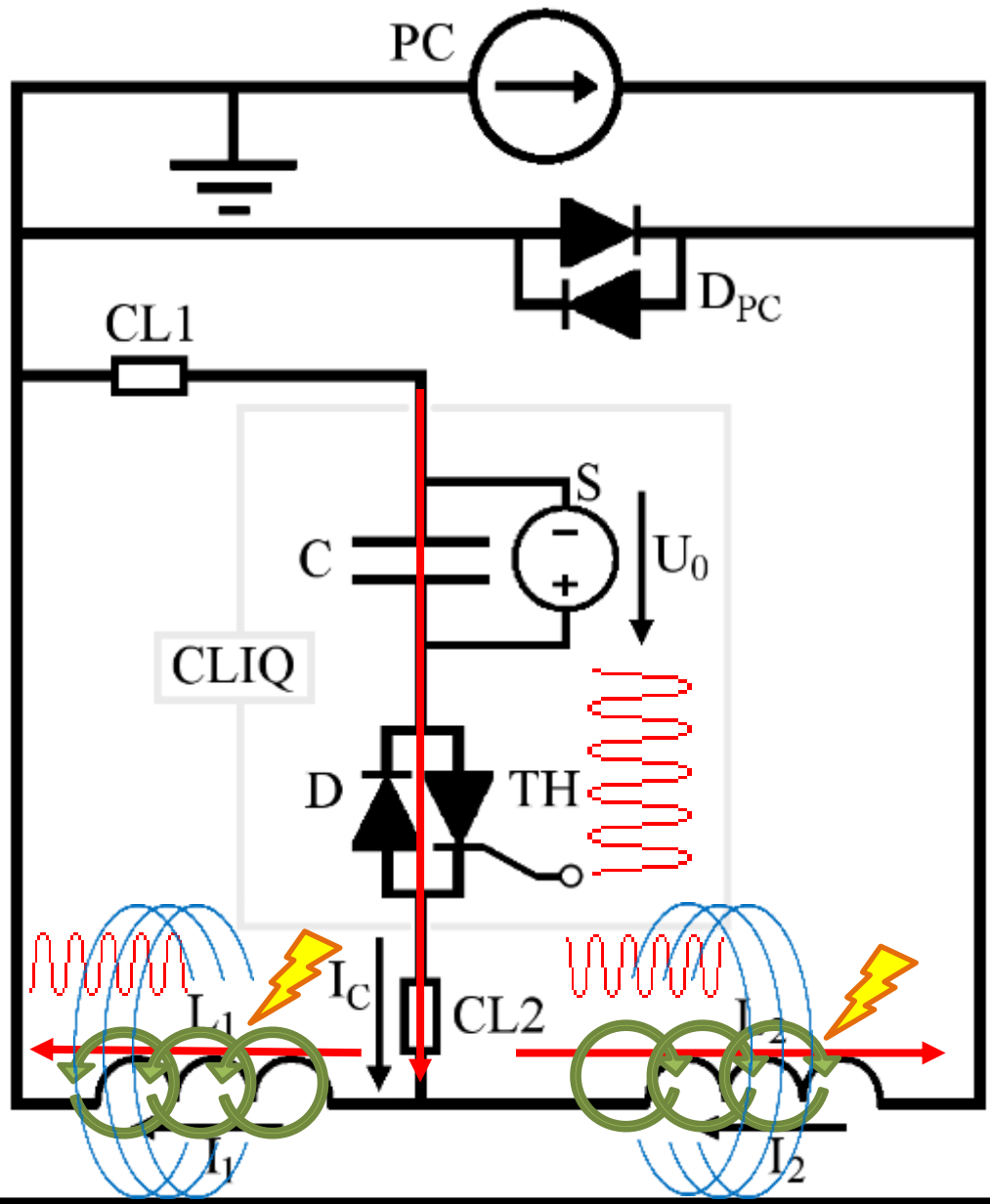
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# CLIQ – Coupling-Loss Induced Quench system

Patent  
EP13174323.9



Current change

Magnetic field change

Transitory losses (Heat)

Temperature rise

**QUENCH**

## What CLIQ offers...

A different mechanism for depositing heat in superconductors with respect to QH

(in multi-filamentary LTS strands, this mechanism is very effective)

An electrically robust system, mainly external to the coil, hardly interfering with the coil winding technology

## ...and what it requires

Study of complex interdependent electro-magnetic and thermal effects, on very different scales (filaments, strands, tapes, cables, main circuit)

Additional terminals connected to the coil to protect

...and “fast” transitory losses!! (i.e. with small time constant)

# AC loss in HTS

What  
is CLIQ

**AC  
loss in  
HTS**

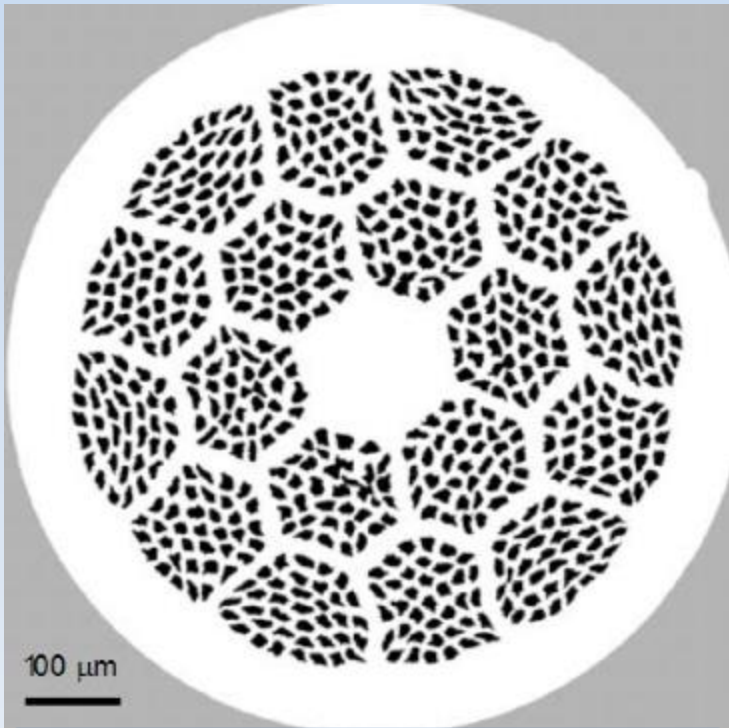
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# HTS strands/tapes



B-2212 strand (Ag matrix)



YBCO tape

MgB<sub>2</sub> strand (Cu matrix)



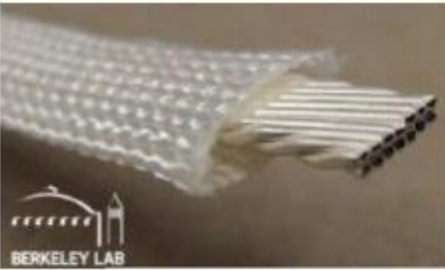
Figures and information from Luisa Chiesa's plenary talk at ASC 2014



# HTS cables (Slide from Luisa Chiesa's talk at ASC2014)

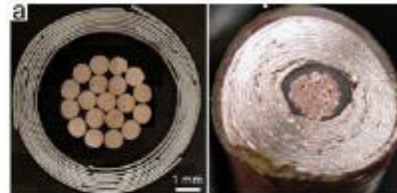
IEEE/CSC SUPERCONDUCTIVITY NEWS FORUM (global edition) October 2014  
 Plenary Presentation 4PLA-01 given at ASC 2014, Charlotte, August 10 - 15, 2014.

## HTS cables



BSCCO-2212 Rutherford cable

Advanced Conductor Technologies LLC



CORC-Conductor on Round Core

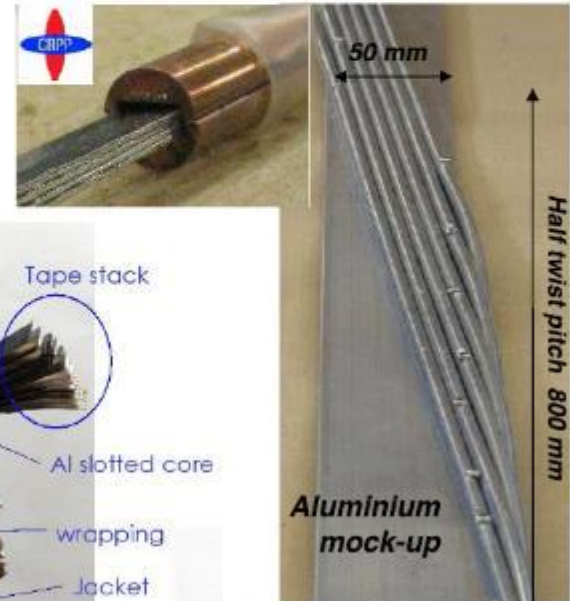


TSTC-Twisted Stacked-Tape Cable

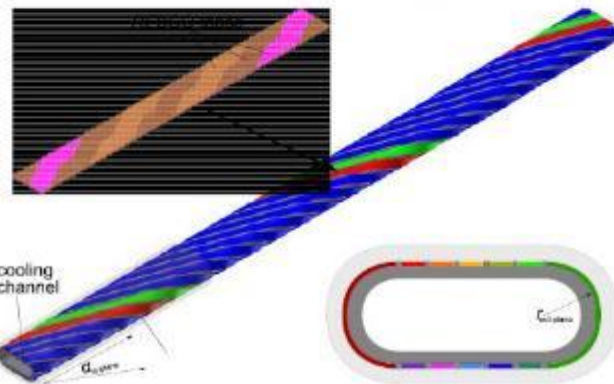
Twisted Pair



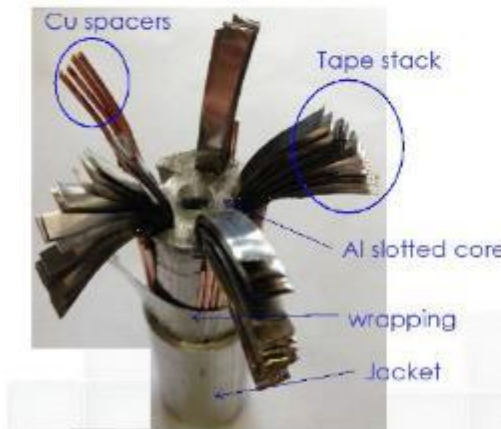
RACC-Roebel Assembled Coated Conductor



RSCCCT-Round Strands Composed of Coated Conductor Tapes



CCRC-Coated Conductor Rutherford Cables



Slotted core HTS CIC conductor

# Transitory losses in HTS conductors

The target of a CLIQ-based protection system is generating enough transitory losses to transfer most of the coil to normal state **in 10-20 ms**

**Hence, “fast” losses are needed**

**Inter-filament coupling loss**: Usually features an **ideal time constant** for heating up the superconductor very effectively with a CLIQ discharge  
**...but not present in tapes, by definition! (if not striated)**

**Inter-strand or inter-tape coupling losses**: Whilst often higher in amplitude, they are typically too slow for heating up the coil in <20 ms  
**Too slow**

**Hysteresis losses** (intentionally unspecific term here):  
No time constant involved, potential for effective mechanism, but the amplitude of the oscillating field must be high  
**To measure and/or model on a case-by-case basis**

# CLIQ optimization (valid for any magnet)

What  
is CLIQ

AC loss  
in HTS

**CLIQ  
optimization  
(valid for  
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Possible  
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CLIQ with  
external  
excitation  
coils

# Some rules of thumb for CLIQ power and energy deposition

Coupling losses per unit volume are proportional to  $(dB/dt)^2$

$dB/dt$  is proportional to  $U_0$

$dB/dt$  is proportional to  $N_{\text{CLIQ}}$

$dB/dt$  is proportional to  $1/L_{\text{eq}}$  and  $L_{\text{eq}}$  can be reduced by 10+ times by optimizing the discharge circuit

$dB/dt$  is independent of  $C$

$dB/dt$  distribution can be optimized

Hysteresis losses per unit volume are dependent on  $\Delta B$  ( $\propto \Delta B^3$ ?)

$\Delta B$  is proportional to  $U_0$

$\Delta B$  is proportional to  $(N_{\text{CLIQ}})^{0.5}$

$\Delta B$  is proportional to  $(1/L_{\text{eq}})^{0.5}$  and  $L_{\text{eq}}$  can be reduced by 10+ by optimizing the discharge circuit

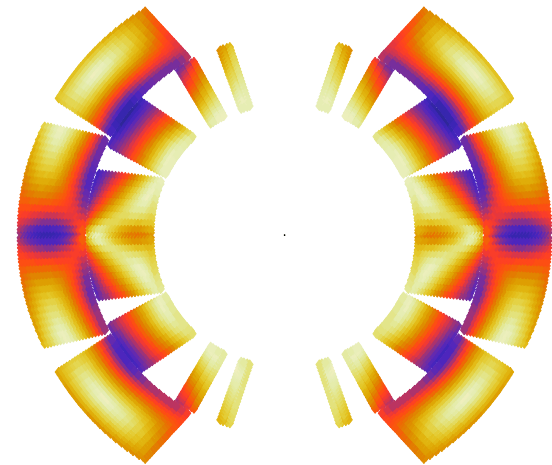
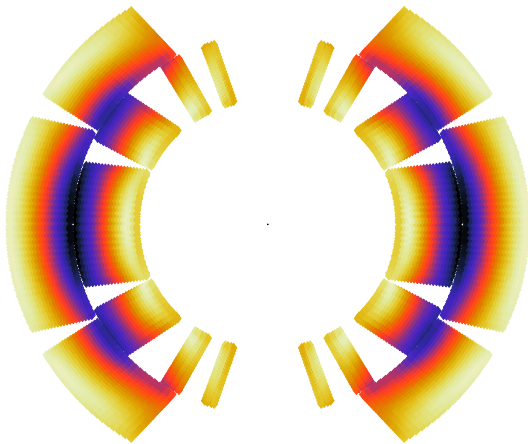
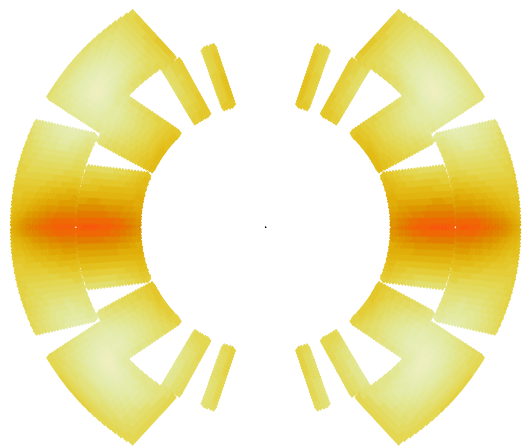
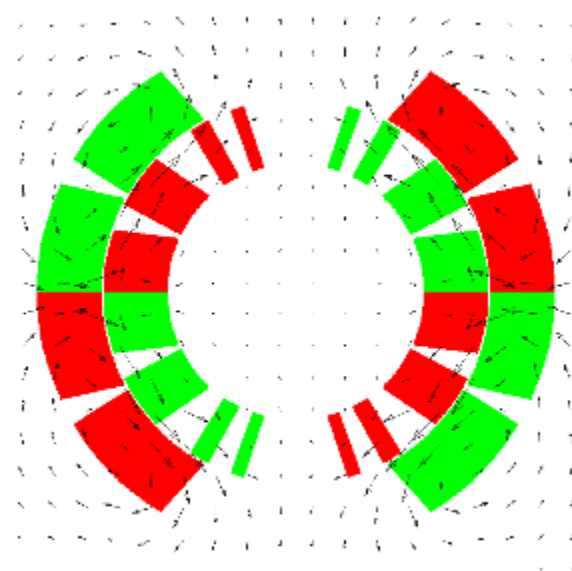
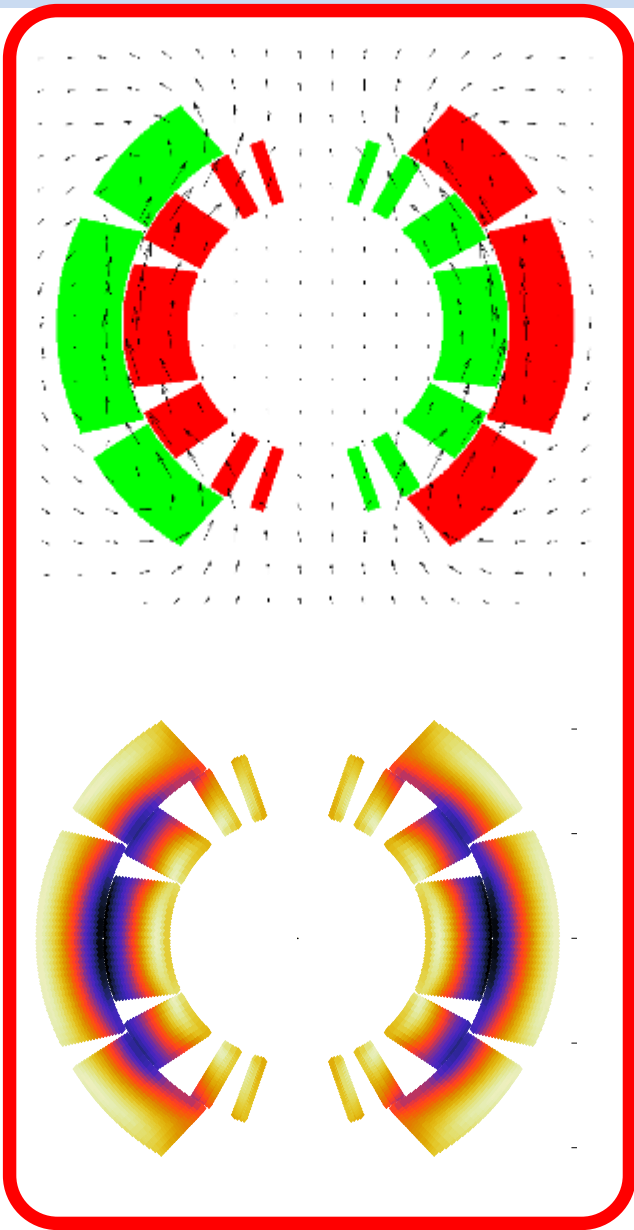
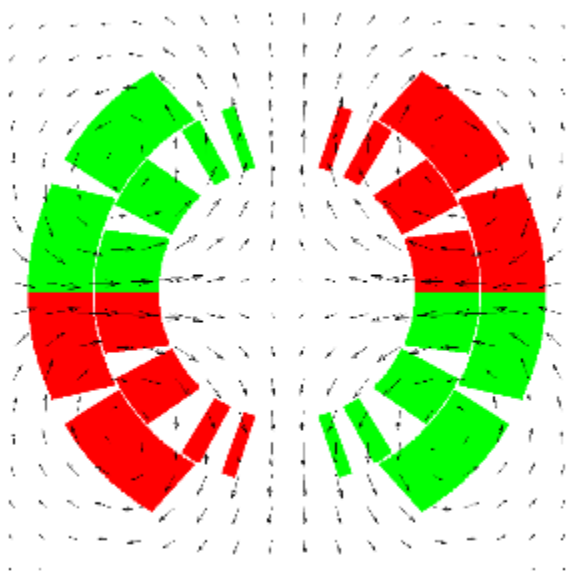
$\Delta B$  is proportional to  $C^{0.5}$

$\Delta B$  distribution can be optimized

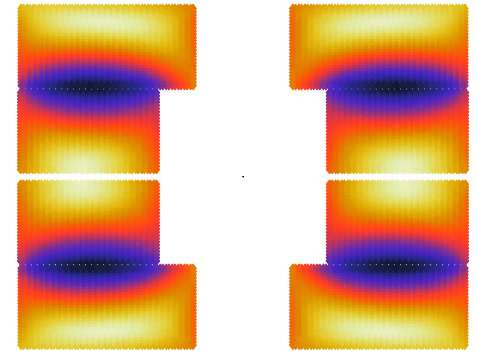
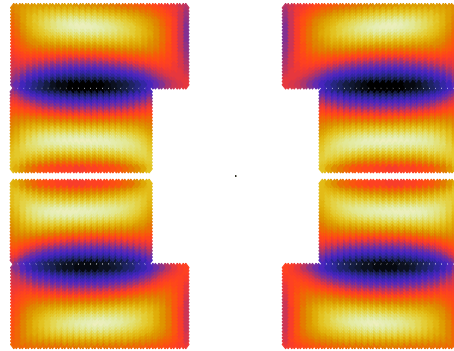
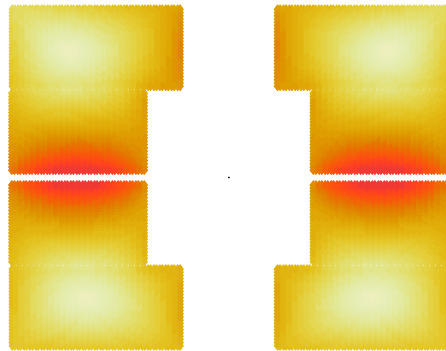
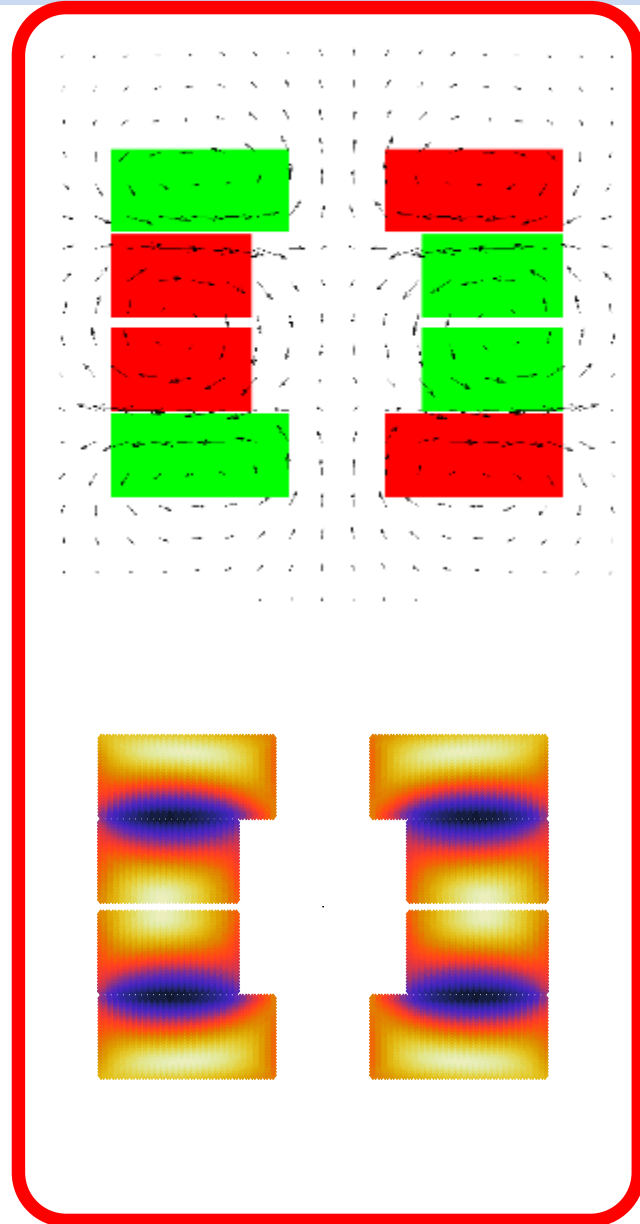
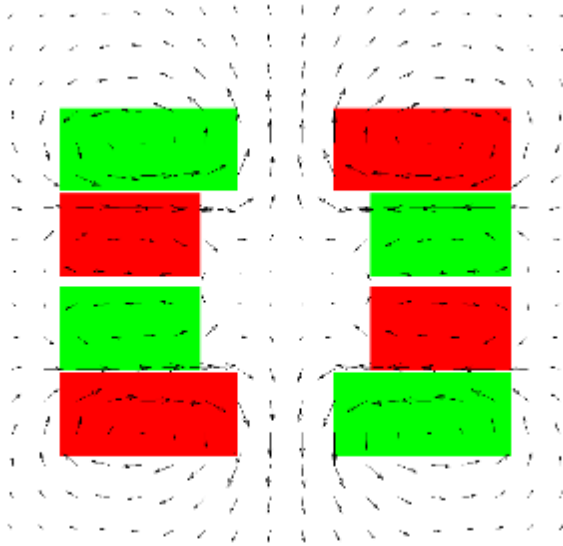
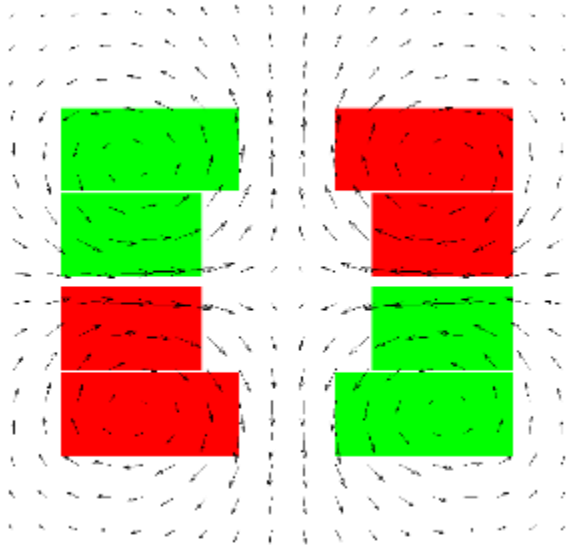
In any case, the total energy delivered to the coil is  $< 0.5 N_{\text{CLIQ}} C U_0^2$

CLIQ typically introduces up to  $dB/dt \sim 10^2 - 10^3$  T/s and  $\Delta B \sim 10^{-1} - 10^0$  T and orientation very different from the field lines when powering in DC

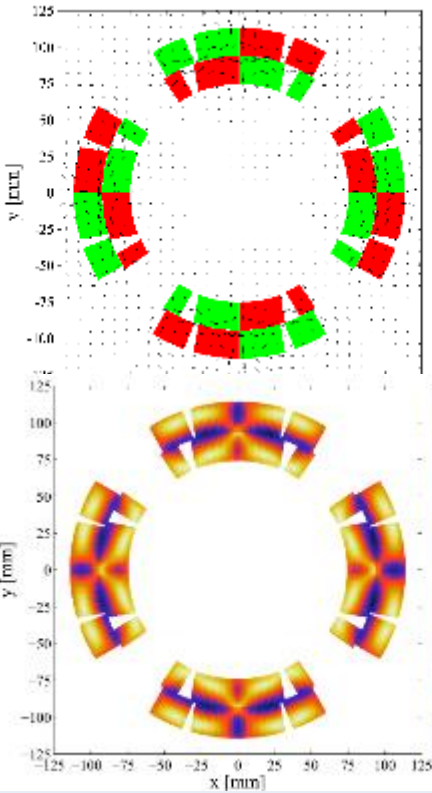
# Example of CLIQ optimization (Dipole geometry)



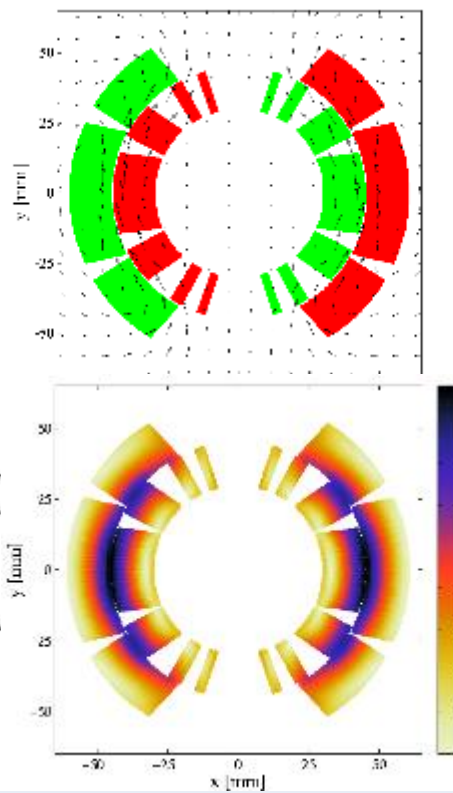
# Example of CLIQ optimization (Block-coil geometry)



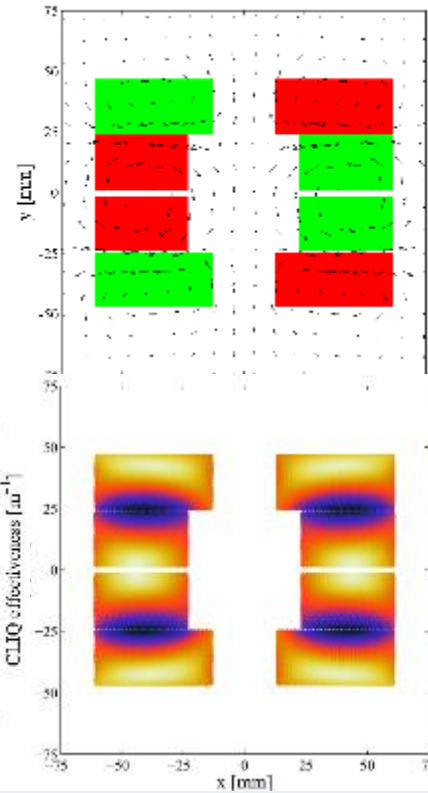
# Optimizing CLIQ – Different magnet geometries



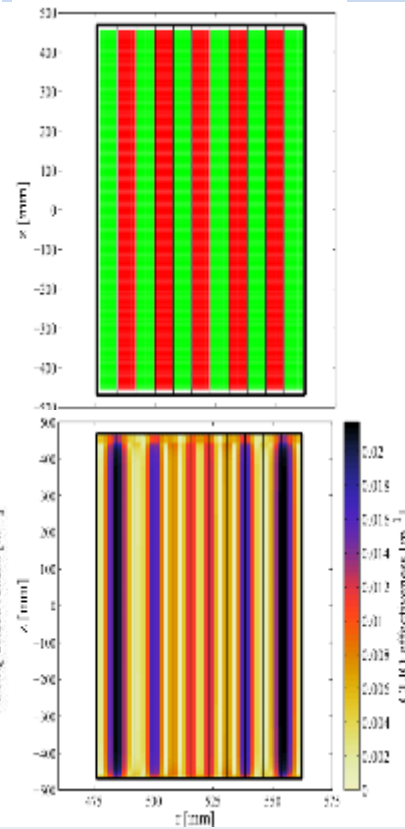
Quadrupole



Dipole



Block coil



Solenoid

**Golden rules**

Subdividing the coil in multiple sections

Introducing opposite current changes in coil sections that are physically adjacent

# This looks beautiful... but where's the catch?

Increase of  $U_0$

Increase of peak voltages to ground in the circuit (<1 kV?)

Addition of CLIQ units

Needs additional CLIQ terminals

Optimization of the discharge circuit (positioning of CLIQ leads, order of the coil sections, etc)

Typically requires addition of CLIQ terminals between magnet layers (less obvious to manufacture)

**No real bottleneck** for increasing dB/dt introduced with CLIQ by 10+ times, i.e. **increasing coupling loss by 100+ times** with respect to present CLIQ systems achieving very good performance on LTS coils

...providing the rules of the game don't change! →



# Possible game changers

What  
is CLIQ

AC loss  
in HTS

CLIQ  
optimization  
(valid for  
any magnet)

**Possible  
game  
changers**

First study case  
of CLIQ on HTS  
(Ravaioli &  
Van Nugteren)

CLIQ with  
external  
excitation  
coils

# Game changers

If filaments are present, but matrix has very high transverse resistivity, compensate with longer filament twist-pitch

If filaments are present, but matrix has very low transverse resistivity, not possible to compensate with shorter filament twist-pitch (IFCL time constant too large), compensate with filament-matrix barrier (?)

If filaments are not present, no inter-filament coupling loss

If very low/high hysteresis losses are generated for a given  $\Delta B$ , performance can change dramatically (you'll see an example soon)

If current density depends on the magnetic-field direction, the transition to the normal state can be achieved with smart field-changes

Use a different type of CLIQ system based on external excitation coils (see last part of the presentation)

# First study case of CLIQ on HTS (Ravaoli & Van Nugteren)

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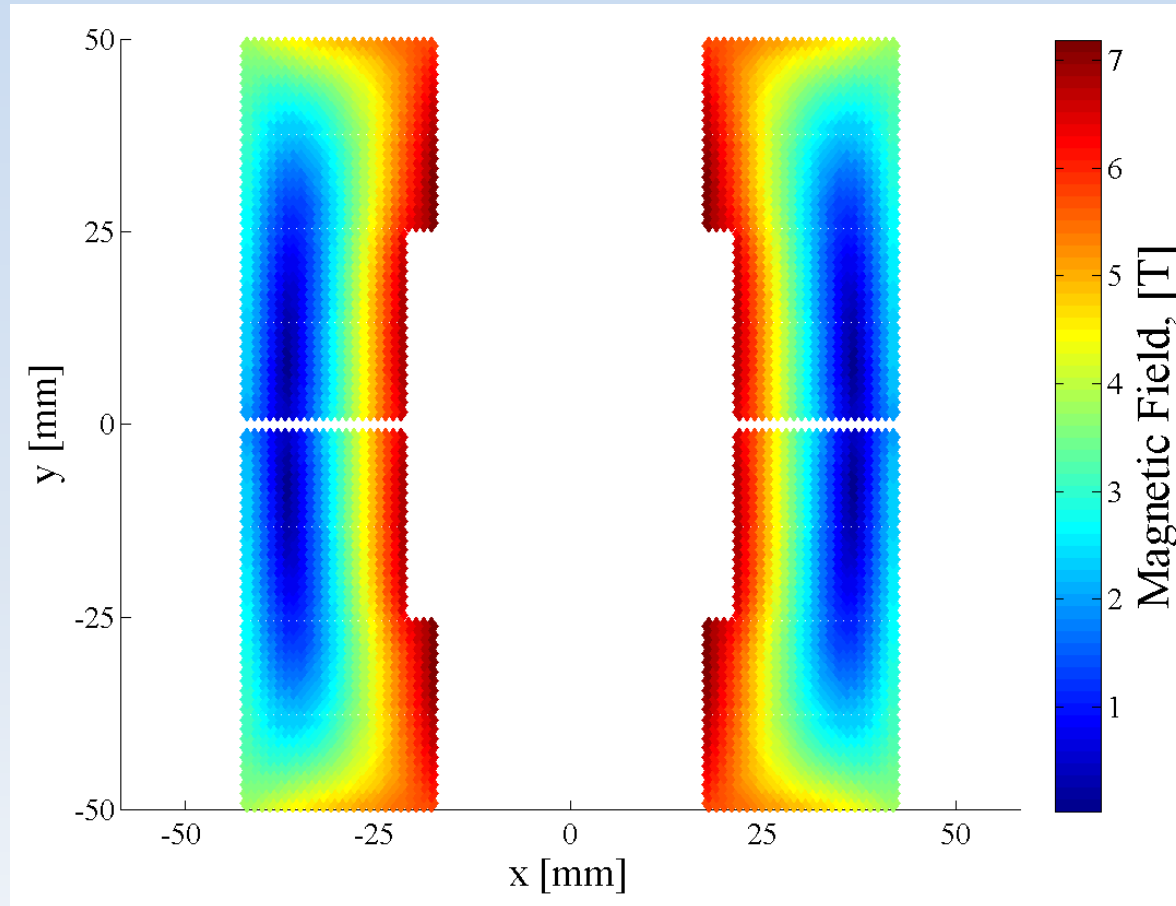
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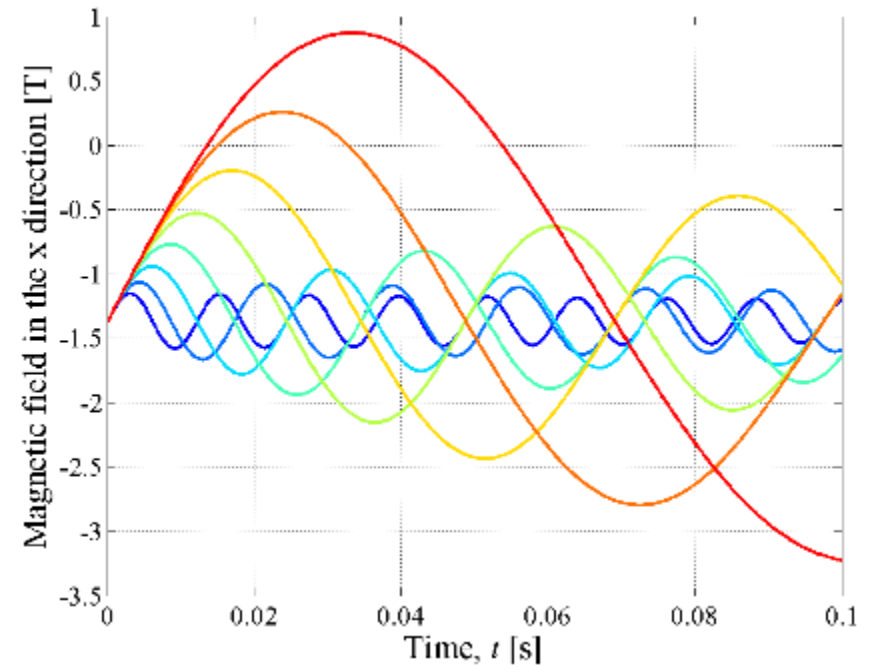
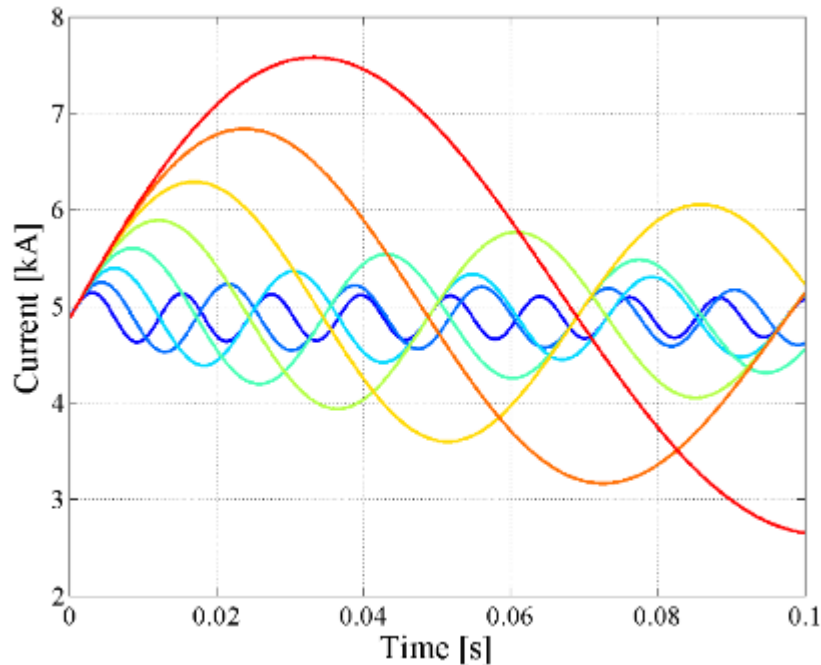
# Study case: 7 T block-coil dipole insert, YBCO Roebel cable

- Block-coil
- 4 layers
- $R=25$  mm aperture
- 5 meter long
- Nom current 4880 A
- Peak dipole field  $\sim 7$  T
- Background field 13 T
- Insulation 0.1 mm
- YBCO, Roebel cable
- 15 tapes
- $12 \times 0.8$  mm<sup>2</sup>
- $J_e=400$  A/mm<sup>2</sup>



Study jointly performed by  
E. Ravaioli and J. Van Nugteren

# Current and magnetic-field changes introduced by CLIQ

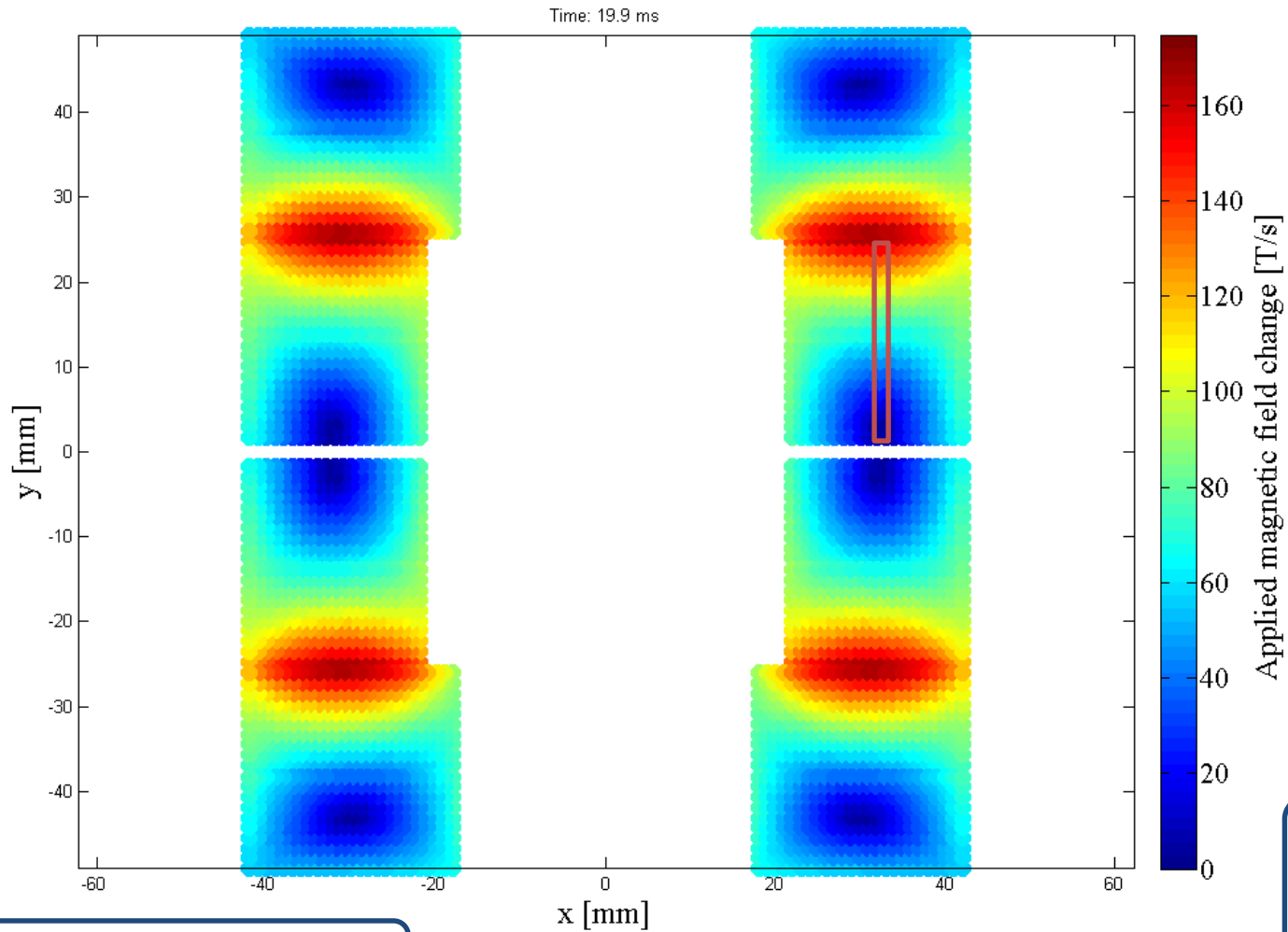


Only **1 CLIQ unit** and 2 CLIQ terminals  
 $U_0=1$  kV ( $\pm 500$  V to ground)  
C varying between 1 and 128 mF

**CLIQ configuration optimized** to maximize the **magnetic-field changes** in the direction **perpendicular** to the cable broad faces

Study jointly performed by  
E. Ravaioli and J. Van Nugteren

# Magnetic-field changes introduced by CLIQ

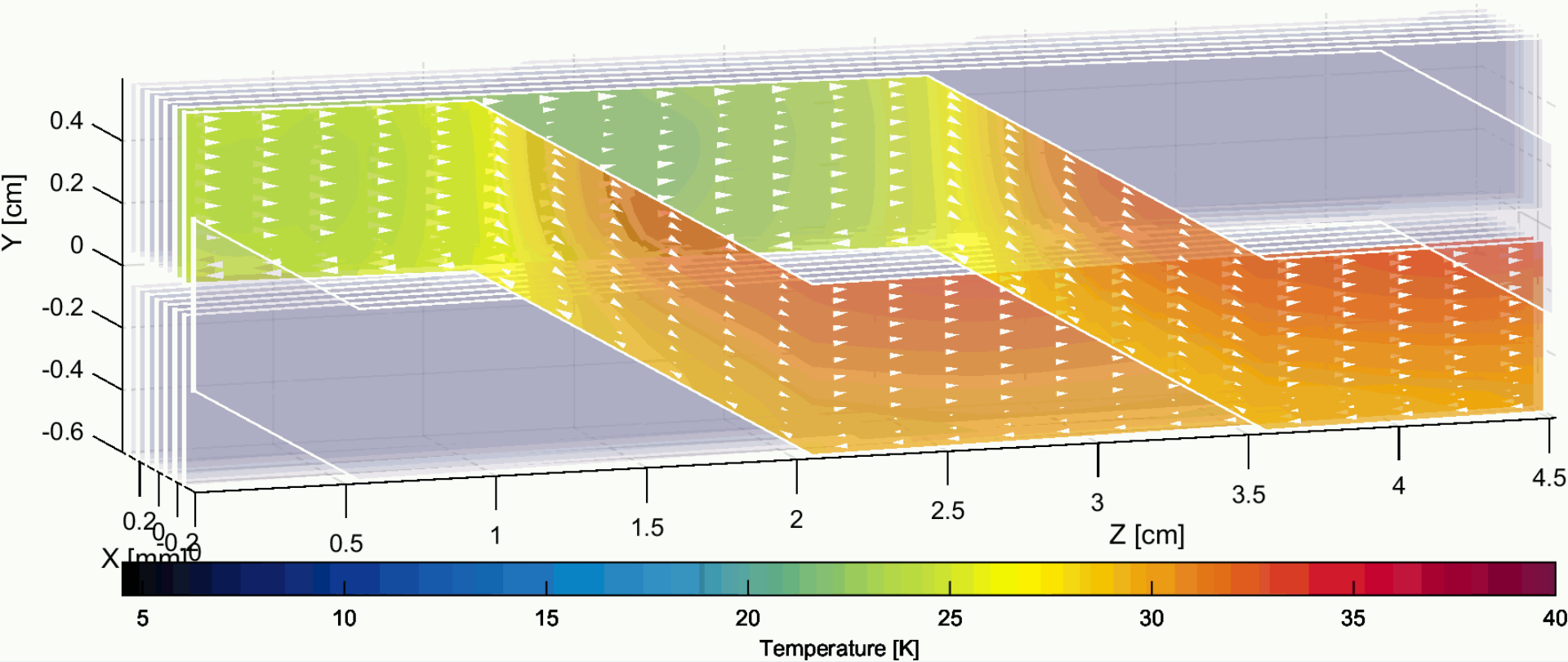


1 CLIQ unit  
 $U_0=1$  kV  
 $C=10$  mF

Study jointly performed by  
E. Ravaioli and J. Van Nugteren

# Temperature profile in two adjacent tapes

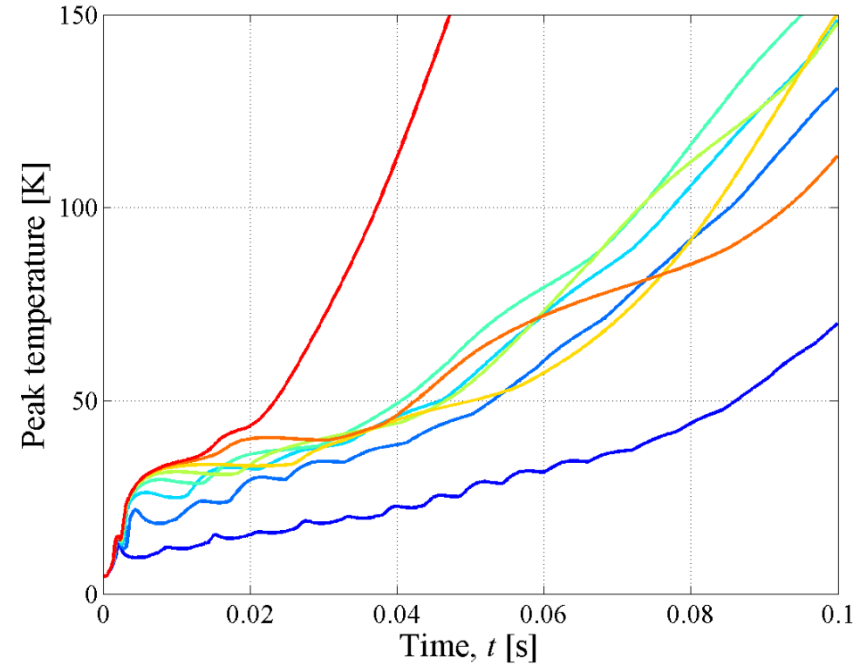
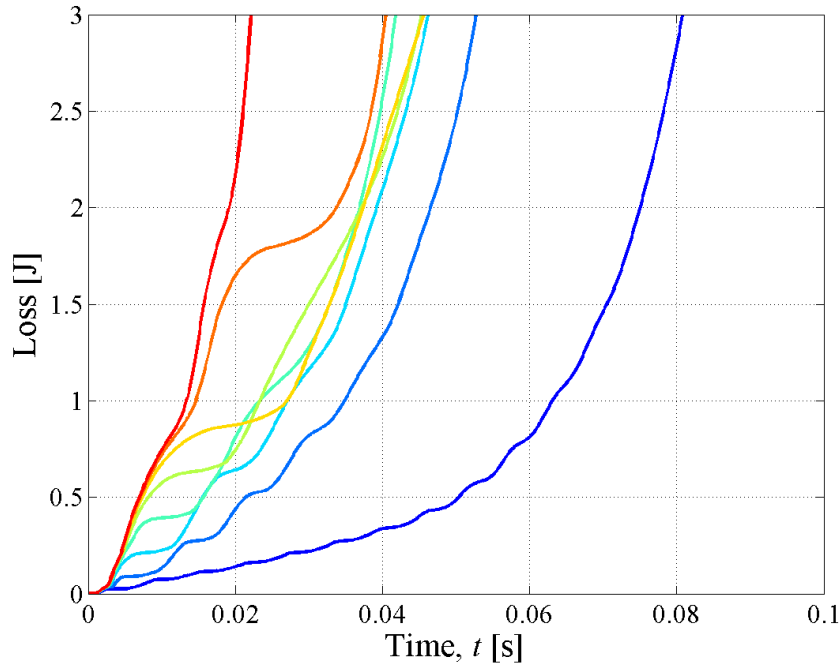
$t = 1250.02$  s,  $I = 5169.94$  A,  $B_x = -1.13$  T,  $B_y = -15.48$  T,  $B_z = 0.00$  T



Study jointly performed by  
E. Ravaioli and J. Van Nugteren

1 CLIQ unit  
 $U_0 = 1$  kV  
 $C = 10$  mF

# Deposited loss (Hysteresis+Ohmic) and Temperature



$U_0=1$  kV ( $\pm 500$  V to ground)  
C between 1 and 128 mF

Study jointly performed by  
E. Ravaioli and J. Van Nugteren

With reasonable charging  
voltage and capacitance, this  
HTS coil can be effectively  
quenched by CLIQ **in <20 ms**

...with only  
1 CLIQ unit and  
2 CLIQ terminals!



## Next steps to conclude the analysis

Study the interaction between stacked cables

Run similar simulations for tapes in different locations of the coil

Complete electro-thermal simulation

(Loss → Temperature → Quench → Resistance → Magnet discharge)

Study the effect of losses on the differential inductance

For LTS, all steps done and model validated

**For HTS, some work is still needed...**

# CLIQ with external excitation coils

What  
is CLIQ

AC loss  
in HTS

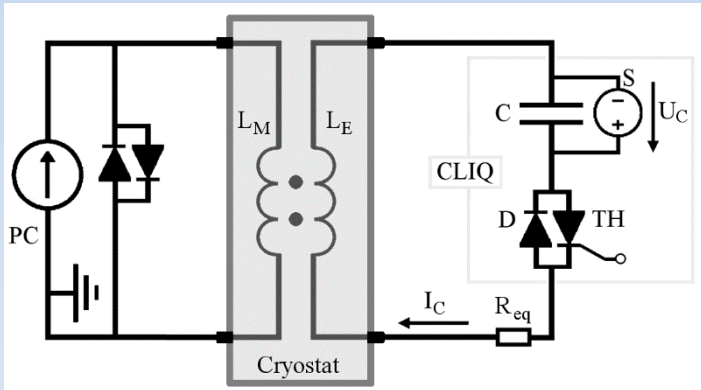
CLIQ  
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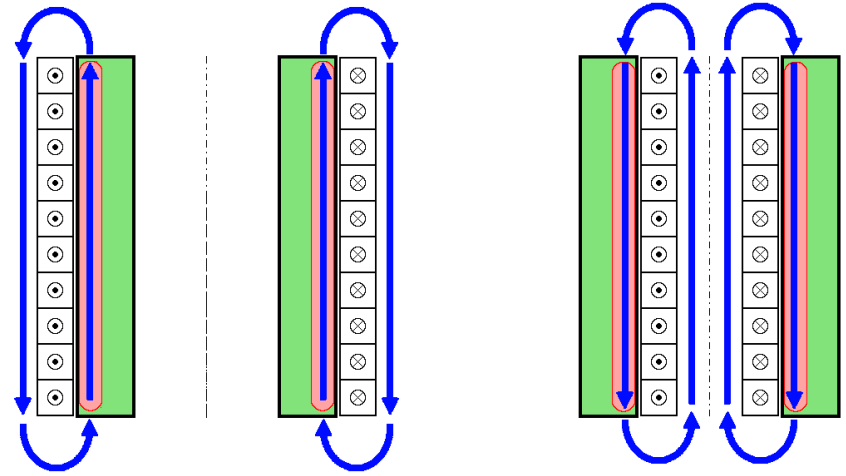
**CLIQ with  
external  
excitation  
coils**

# CLIQ with external excitation coils



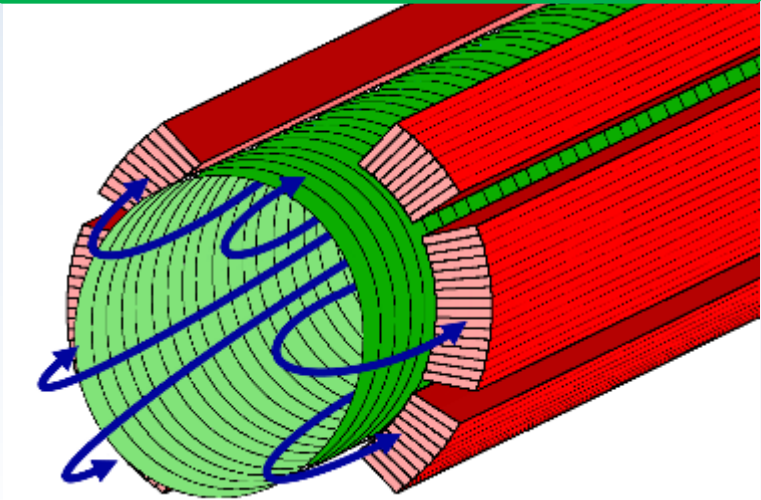
Tested  
in 2013  
on LTS

External or internal to the coil,  
or between layers

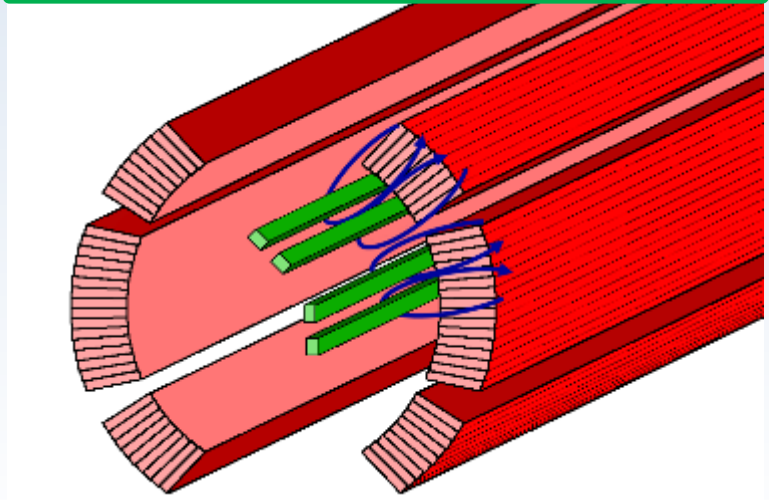


Advantages: Galvanically separated from the coil, High voltages can be introduced

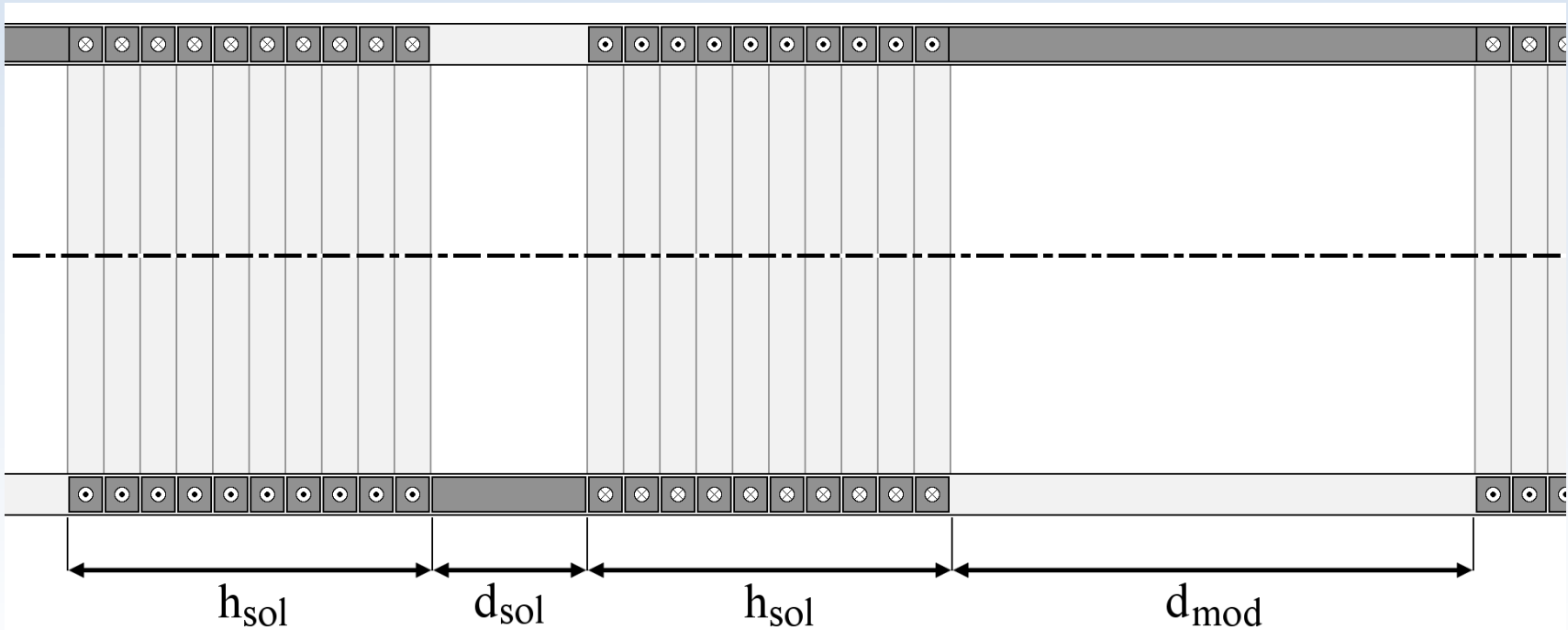
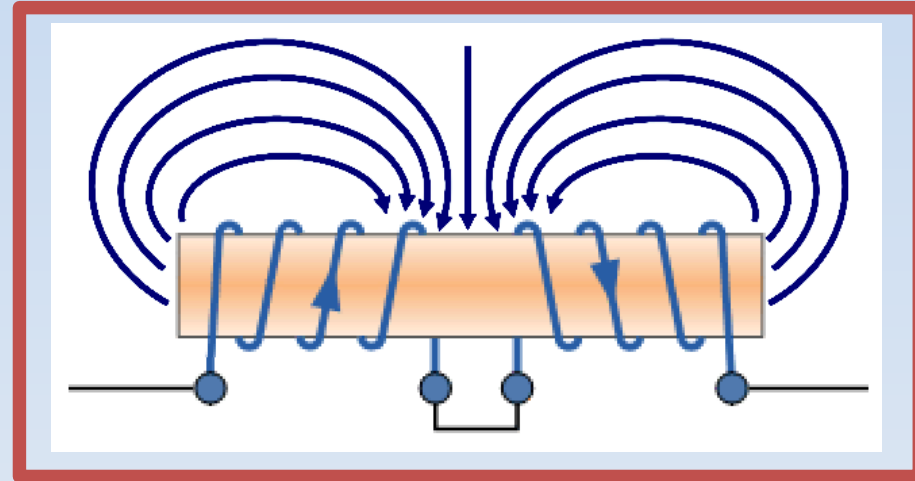
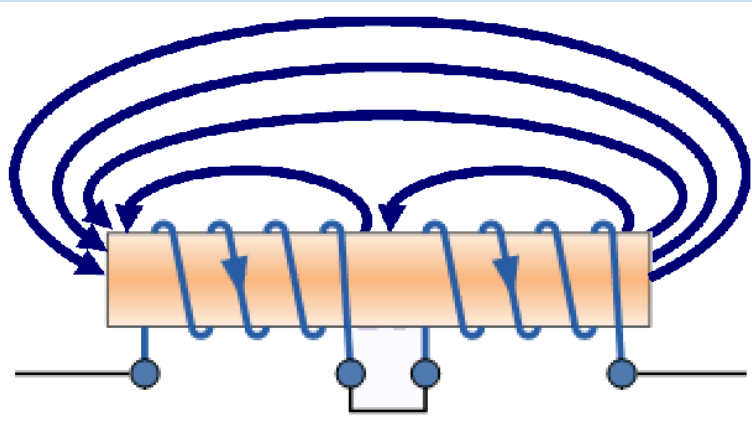
Solenoid coil



Multipole coil



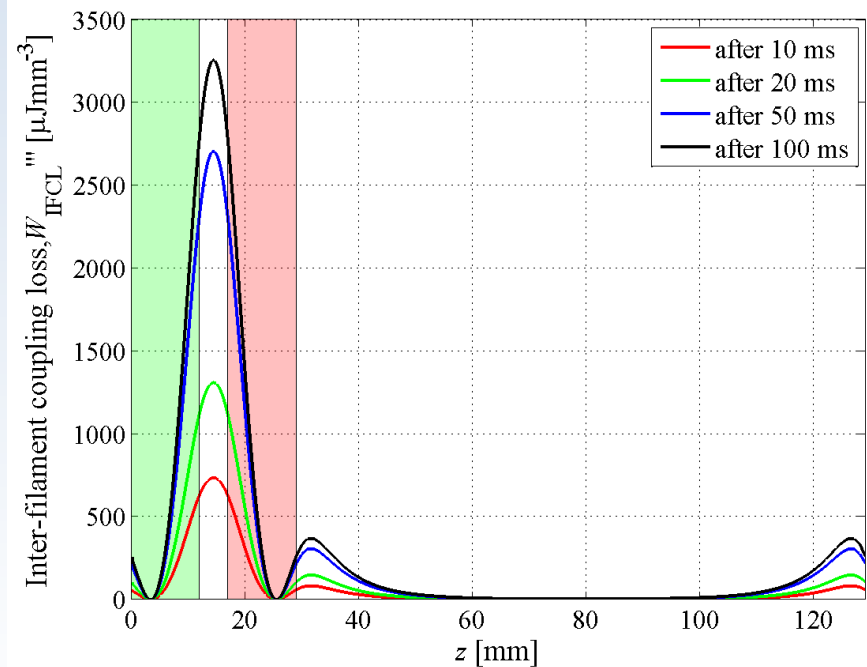
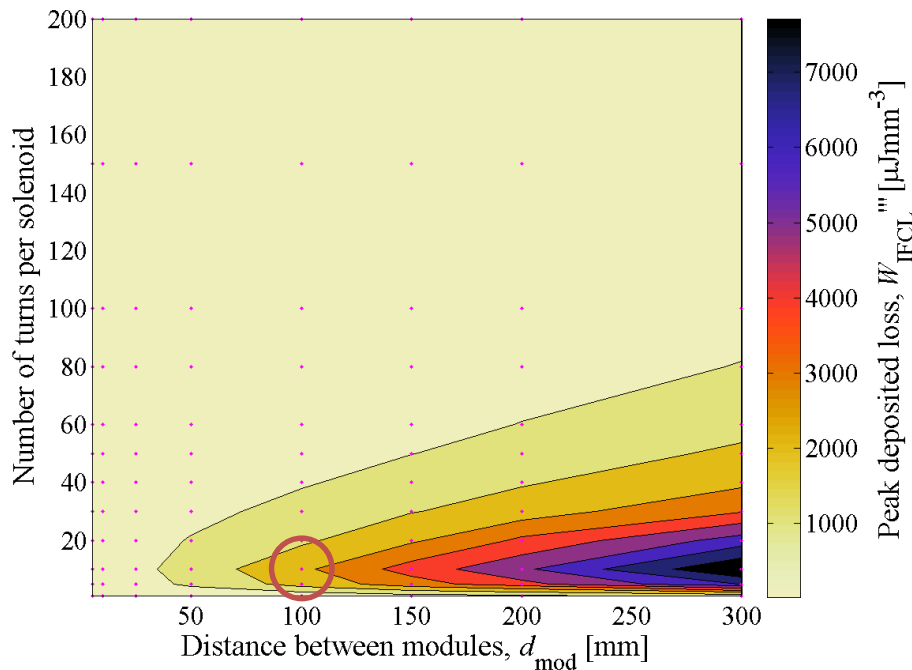
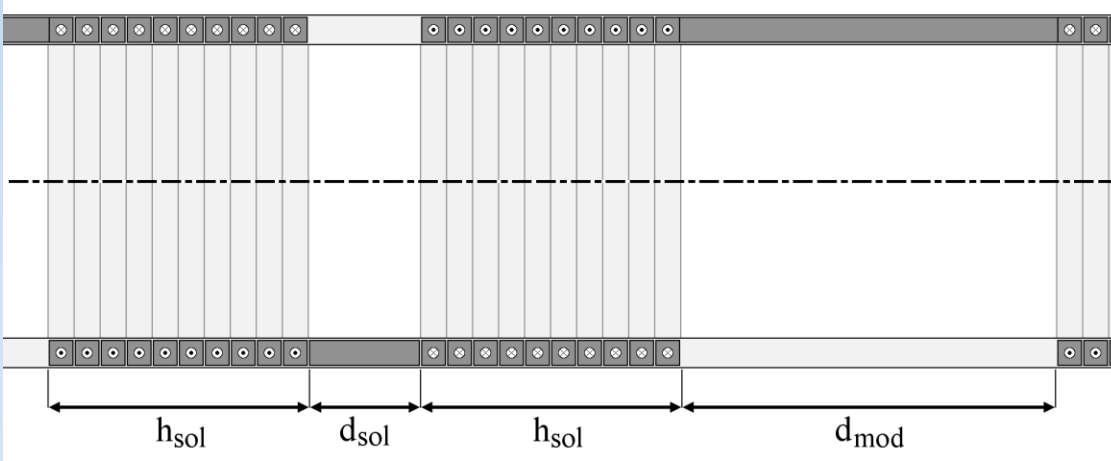
# CLIQ with external excitation coils – Multi-Solenoid



# CLIQ with Multi-Solenoid excitation coil

In my humble opinion, this seems a subject for a very interesting PhD..

Very high energy deposition achieved in effective “inductive heating stations” ( $\sim J/cm^3$  in  $<20$  ms)



CLIQ: Mature technology for LTS magnets

Optimization methods presented ( $U_0$ ,  $N_{\text{CLIQ}}$ , terminal positioning, C, excitation coils)

With inter-filament coupling loss, increasing the CLIQ power deposition by 100+ times with respect to present systems are within reach

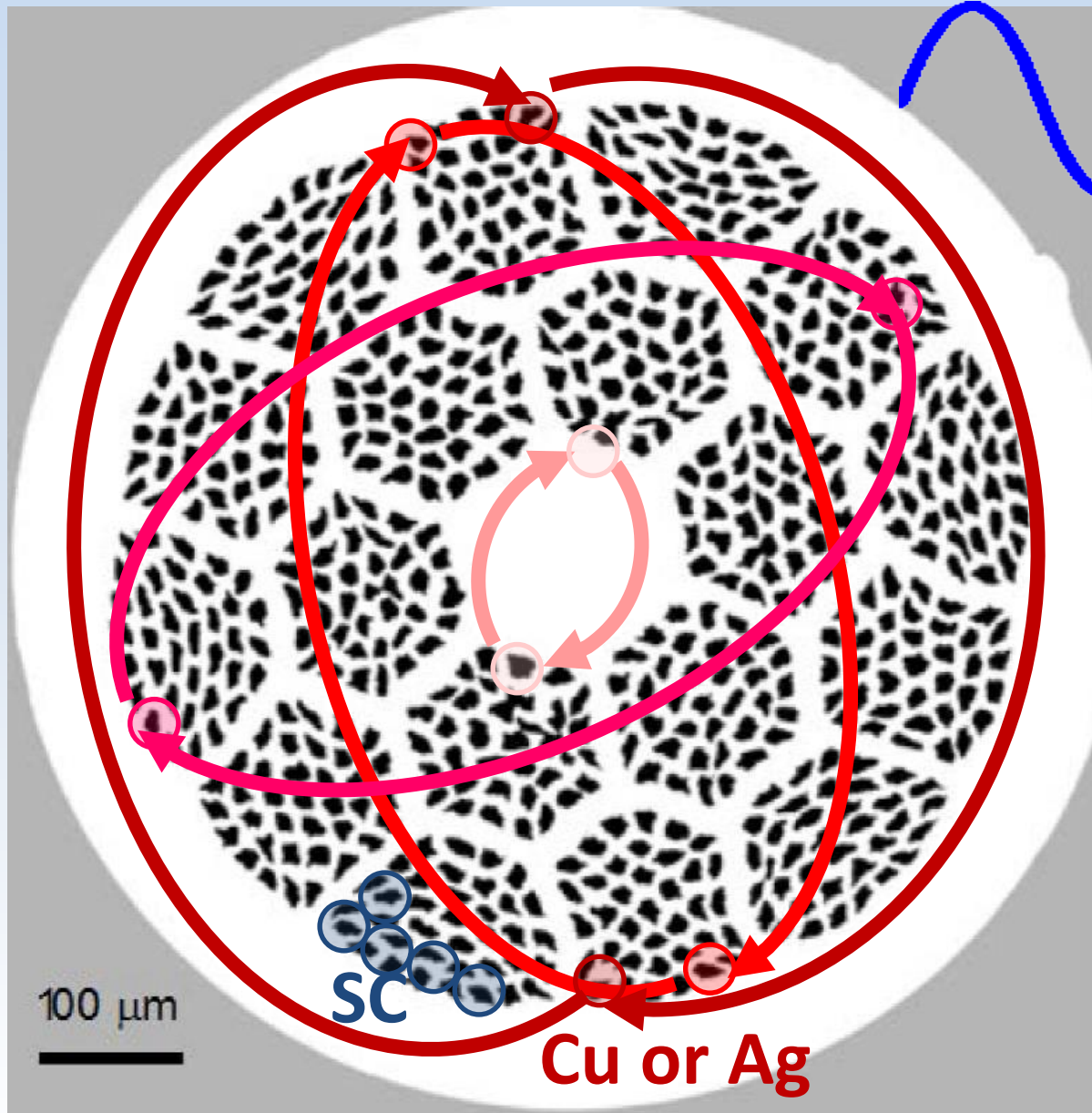
Different loss mechanisms (particularly in cables) could be game changers (either way..)

Way to go: Collaborations between experts of CLIQ protection and AC losses in HTS (loss measurements, modeling, CLIQ optimization, circuit simulations,...)

# QUESTIONS?

Emmanuele.Ravaioli@cern.ch

# Multi-filamentary wires/strand: inter-filament coupling loss



**Same physics** as inter-filament coupling loss in LTS, but different material properties

$$\frac{P_{IF}}{vol} = \left( \frac{l_p}{2\pi} \right)^2 \frac{1}{\rho_{eff}(B)} \left( \frac{dB}{dt} \right)^2$$

$$\tau_{IF} = \frac{\mu_0}{2} \left( \frac{l_p}{2\pi} \right)^2 \frac{1}{\rho_{eff}(B)}$$

**Filament twist-pitch** and effective **transverse resistivity of the matrix** are the key parameters



# Hysteresis loss