

5th Joint HiLumi LHC-LARP Annual Meeting 2015

Cryo infrastructures for Crab Cavities tests at SPS

Progress and perspectives



Features

- Introduction
- Main principles and basic process analysis for installation of the cold box at the surface or underground
- Proximity cryogenics for Crab Cavities modules
- Cryo schedule with main phases for SM18 tests & BA6
- Others & summary

Introduction

- Situation in last November'14: cryogenics for crab cavities in BA4

Significant part of equipment installation work at BA4 was done during LS1, regarding 2K cooling capability.

- The 2K helium pumps have been installed in the SPS cavern at BA4
 - Cooling water circuits installed for pumps cooling – EN/CV support
 - Electrical supply pulled from surface to TA4 and BA4 alcove –EN/EL support
 - Control racks installed in TA4 (shaft bottom area) – TE/CRG
 - Ethernet network pulled and installed underground for control system – IT support
- Decision to go to SPS-BA6 was thereafter taken => new integration study and impact on initial cryo planning

Main principles and basic process analysis

- 2 options studied to chose cold box location
 - Underground, in cavern – 60m horizontal transfer line from cold box to client
 - Surface, in BA6 – 120m vertical transfer line from cold box to client
- Compressor station location
 - In both cases, it stays at surface level in BA6
- About heat loads and refrigeration capacity requirements
 - They will be assessed and summarized in the following slide
 - They are coherent with analysis from KEK meeting / Nov'14
 - Since then:
 - Adding of a transfer line => slight increase in heat load budget
 - Screening done no more by LN₂, but by GHe @ 50K provided by the cold box

Heat loads and refrigeration capacity requirements

COLD BOX IN CAVERN						
Component	@ 2K		@ 4.5K		@ 50K-80K	
	Heat load	Refrigeration capacity requirement	Heat load	Refrigeration capacity requirement	Heat load	Refrigeration capacity requirement
Service Module	/	/	2.5W @ 4.5K	0.13 g/s of LHe @ 4.5K	30W @ 80K	0.19 g/s of GHe @ 50K
Buffer tank	/	/	1.5W @ 4.5K	0.08 g/s of LHe @ 4.5K	20W @ 80K	0.13 g/s of GHe @ 50K
Cryo Module Static	18.6W @ 2K	0.80 g/s of LHe @ 2K	/	/	286W @ 80K	1.84 g/s of GHe @ 50K
Cryo Module Dynamic	13.4W @ 2K	0.57 g/s of LHe @ 2K	/	/	30W @ 80K	0.19 g/s of GHe @ 50K
Transfer Lines	/	/	4W @ 4.5K	0.21 g/s of LHe @ 4.5K	/	/
60m-transfer line for remote location of cold box	/	/	6W @ 4.5K	0.32 g/s of LHe @ 4.5K	78W @ 80K	0.50 g/s of GHe @ 50K
TOTAL	32W @ 2K	1.37 g/s of LHe @ 2K	14W @ 4.5K	0.74 g/s of LHe @ 4.5K	444W @ 80K	2.85 g/s of GHe @ 50K
Equiv @ 4.5K	= 1.52 g/s of LHe @ 4.5K		= 0.74 g/s of LHe @ 4.5K		= 0.26 g/s of LHe @ 4.5K	
Required Cold box capacity			= 2.52 g/s of LHe @ 4.5K			
With security factor of 1.5			3.78 g/s of LHe @ 4.5K = 118 L/h of LHe @ 4.5K			

COLD BOX AT SURFACE						
Component	@ 2K		@ 4.5K		@ 50K-80K	
	Heat load	Refrigeration capacity requirement	Heat load	Refrigeration capacity requirement	Heat load	Refrigeration capacity requirement
Service Module	/	/	2.5W @ 4.5K	0.13 g/s of LHe @ 4.5K	30W @ 80K	0.19 g/s of GHe @ 50K
Buffer tank	/	/	1.5W @ 4.5K	0.08 g/s of LHe @ 4.5K	20W @ 80K	0.13 g/s of GHe @ 50K
Cryo Module Static	18.6W @ 2K	0.80 g/s of LHe @ 2K	/	/	286W @ 80K	1.84 g/s of GHe @ 50K
Cryo Module Dynamic	13.4W @ 2K	0.57 g/s of LHe @ 2K	/	/	30W @ 80K	0.19 g/s of GHe @ 50K
Transfer Lines	/	/	4W @ 4.5K	0.21 g/s of LHe @ 4.5K	/	/
120m-vertical line for remote location of cold box	/	/	12W @ 4.5K	0.64 g/s of LHe @ 4.5K	156W @ 80K	1.0 g/s of GHe @ 50K
TOTAL	32W @ 2K	1.37 g/s of LHe @ 2K	20W @ 4.5K	1.06 g/s of LHe @ 4.5K	522W @ 80K	3.35 g/s of GHe @ 50K
Equiv @ 4.5K	= 1.52 g/s of LHe @ 4.5K		= 1.06 g/s of LHe @ 4.5K		= 0.31 g/s of LHe @ 4.5K	
Required Cold box capacity			= 2.89 g/s of LHe @ 4.5K			
With security factor of 1.5			4.34 g/s of LHe @ 4.5K = 143.7 L/h of LHe @ 4.5K			

Scenario 1: cold box in cavern

Assumptions

- Cold box in cavern below BA6, producing He_{liq} @ 1.4bar / 4.58K
- Dewar underground, no subcooler
- 60m-long horizontal transfer line from CB to « clients »

Key values of \dot{m} , regarding heat load at 2K

- | | |
|-------------------------------------|---------------------------------------|
| 1: 1.37 g/s @ 2K / 30mbar | 5: 0.20 g/s @ 4.5K (saturated vapour) |
| 2: 1.52 g/s @ 4.5K / 1.3bar | |
| 3: 1.57 g/s @ 4.58K / 1.4bar | |
| 4: 1.37 g/s @ 2K (saturated vapour) | |

Required liquefaction rate @ 4.5K = 3.78 g/s (regarding all heat loads, and taking into account a contingency factor of 1.5)

Required Cold box capacity = 3.90 g/s = 118 L/h \Leftrightarrow 394W @ 4.5K

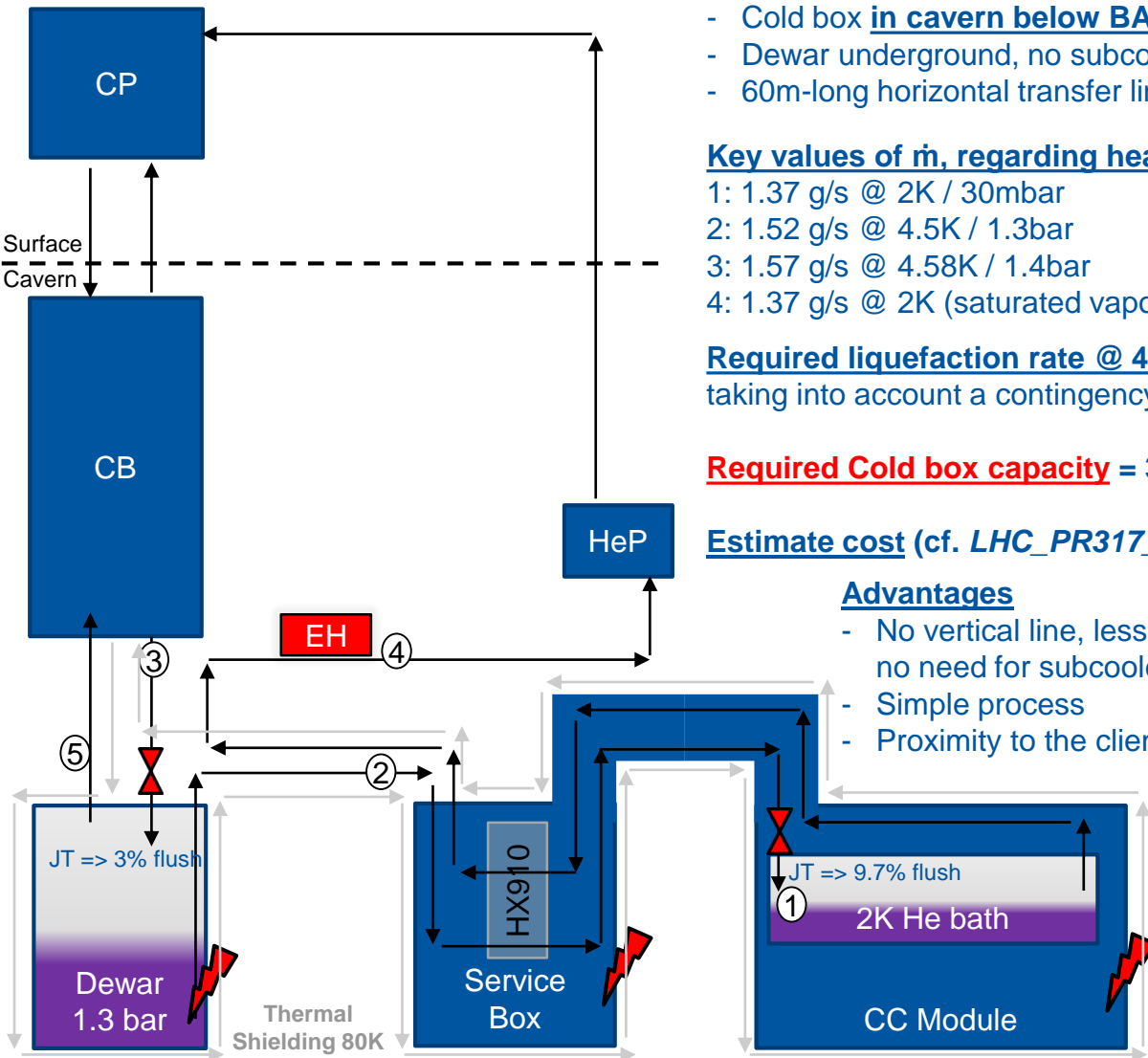
Estimate cost (cf. LHC_PR317_Economics & inflation): 1.40 MCHF

Advantages

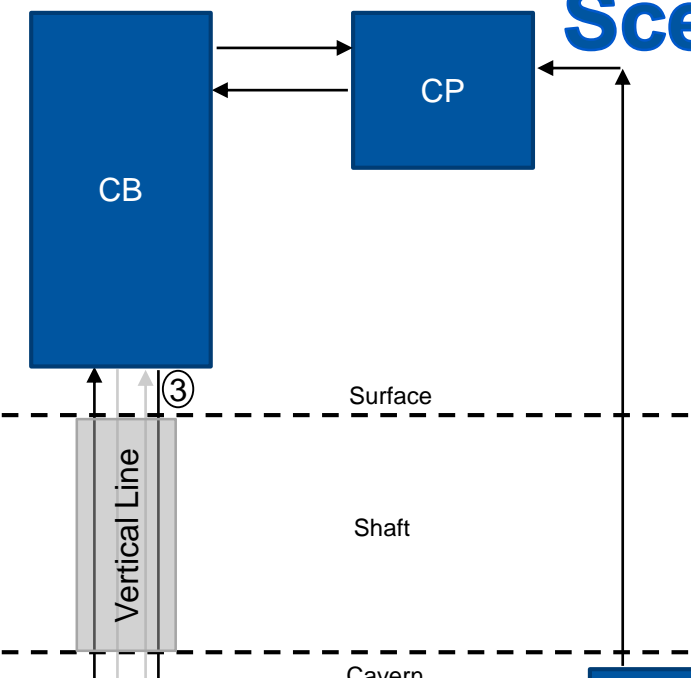
- No vertical line, less heat loads, no hydrostatic compression problem, no need for subcooler, no biphasic instabilities at cold box return
- Simple process
- Proximity to the client

Disadvantages

- Still reduced mobility, even in the cavern
- No use of LN_2 underground



Scenario 2: cold box at surface



Assumptions

- Cold box located at surface, producing He_{liq} @ 1.4bar / 4.58K
- Dewar underground, **no subcooler**
- 120m-long vertical transfer line

Key values of \dot{m} , regarding heat load at 2K

- | | |
|-------------------------------------|---------------------------------------|
| 1: 1.37 g/s @ 2K / 30mbar | 5: 0.40 g/s @ 4.5K (saturated vapour) |
| 2: 1.52 g/s @ 4.5K / 1.3bar | |
| 3: 1.63 g/s @ 4.58K / 1.4bar | |
| 4: 1.37 g/s @ 2K (saturated vapour) | |

Required liquefaction rate @ 4.5K = 4.34 g/s (regarding all heat loads, and taking into account a contingency factor of 1.5)

Required Cold box capacity = 4.66 g/s = 143.7 L/h \Leftrightarrow 471W @ 4.5K

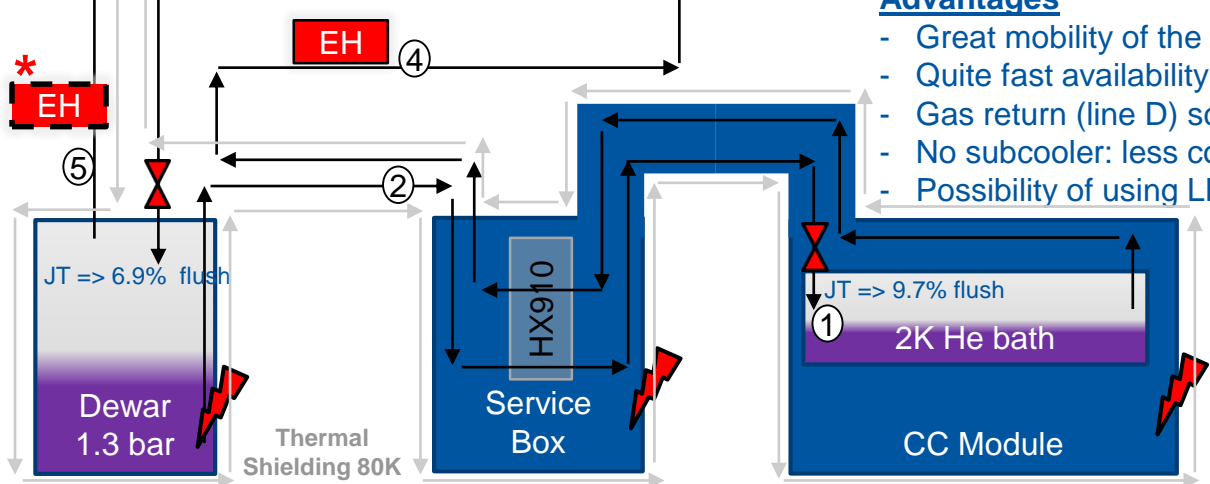
Estimate cost (cf. LHC_PR317_Economics & inflation): 1.56 MCHF

Advantages

- Great mobility of the CB as located at surface
- Quite fast availability for the manufacturer
- Gas return (line D) screening the inlet liquid flow (line C)*
- No subcooler: less complicated process
- Possibility of using LN_2

Disadvantages

- Vertical line in the shaft



Our needs for cold box integration

Minimal volume in one-piece (cold box): [L(2.6m) × W(1.8m) × H(2.6m)] = 12.2 m³ ; 2.5 tons

Accessibility: 1m width needed around cold box for operation/maintenance, + 1m above (removability of top plate for turbine maintenance in particular)

About horizontality: not for standard refrigerators, to be discussed with manufacturer

Utilities:

- Electricity (400V, and 24V for control-command)
- Water (cooling of 2 K pumping units, turbines circuits, raw water only)
- Compressed air (8 bar, dry air, mainly for regulation valves)

Cryo-line: 1 single vacuum-insulated transfer line for both liquid and screening He (+ gas returns)

Decision for final location of cold box still underway (wrt integration study – on-site visit at YETS the latest)

Selected from market existing standard design refrigerators (available from manufacturers)

Air Liquide: HELIAL Liquefiers (Helial LL)

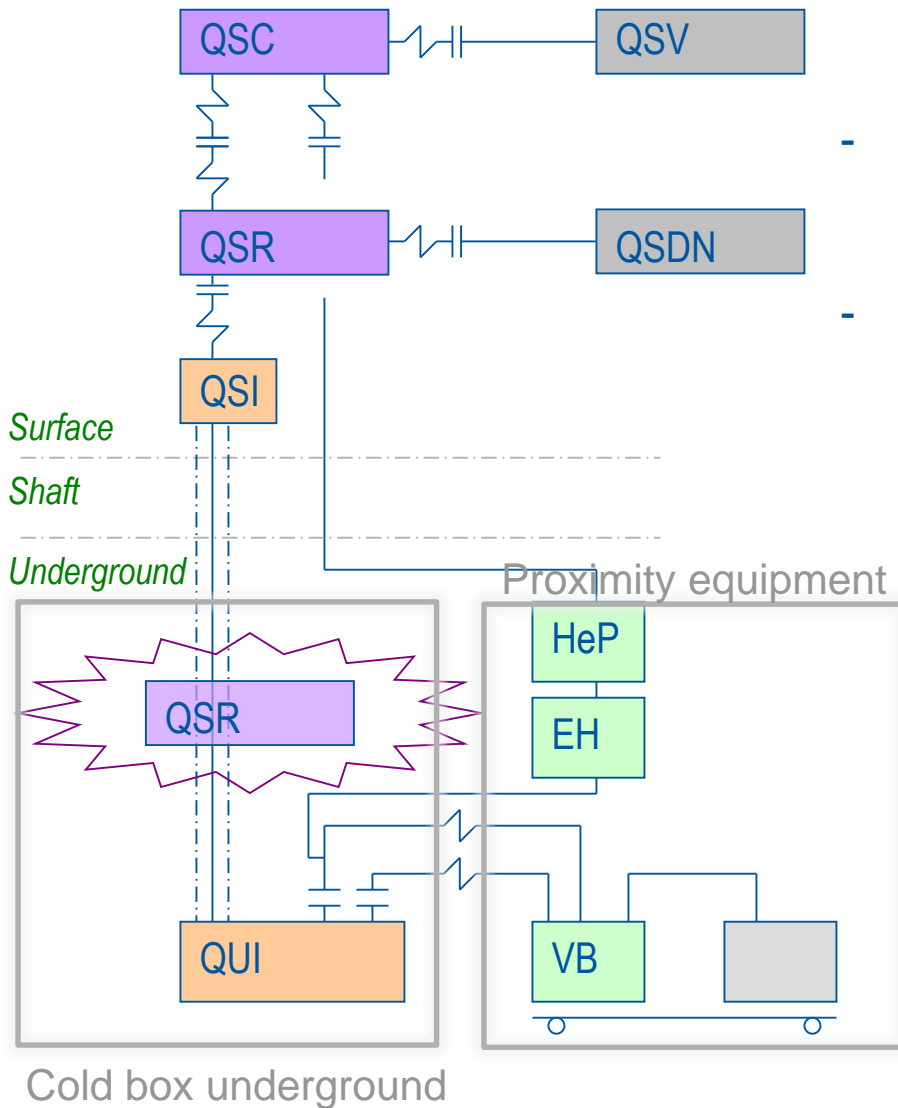
- from 110 to 145 L/h w/o LN₂ precooling
- from 215 to 300 L/h with LN₂ precooling
- *Beware: no thermal shielding circuit at 50-80K*

Linde Kryotechnik: L-Series (L280)

- from 100 to 145 L/h w/o LN₂ precooling
- from 200 to 290 L/h with LN₂ precooling
- *Thermal shielding circuit at 50-80K*



Proximity Cryogenics for Crab Cavities modules



- As cold box will require Dewar to be tested (reception test in SM18), both are grouped
- Proximity cryo equipment stands for the service module and the EH on VLP + He pumps

Proximity Cryogenics for Crab Cavities modules

Proximity equipment: CC service box, flexible double channel transfer line, VLP helium return heater.

Status:

- Technical specification advanced to 70-80%
- Equipment to be ordered by the beginning of 2016

Current work: interfaces design definition and “delicate” parts design e.g. top plate of the CC service box, safety devices

Next steps: definition and design of SM18 adaptation for three type of clients to be tested:

- first CC prototype module to be tested with CC service box,
- second CC prototype to be tested with direct connection to SM18 infrastructure,
- Final LHC design (with different interface than prototypes) to be tested with direct connection to SM18 infrastructure

Crab cavity cryo module – instrumentation

Recall: Crab cavities cryo-module will be operated in saturated helium bath at 2 K

Level measurement: 2 supra gauges installed in dedicated helium channel connected to the bath – the gauges will 100% of the bath depth measurement, connecting cables are planned to be routed in the double phase collector, connector to outside placed on CC service box side

Pressure measurement: 1 gauge connected on the double phase gas volume (possibly in the jumper)

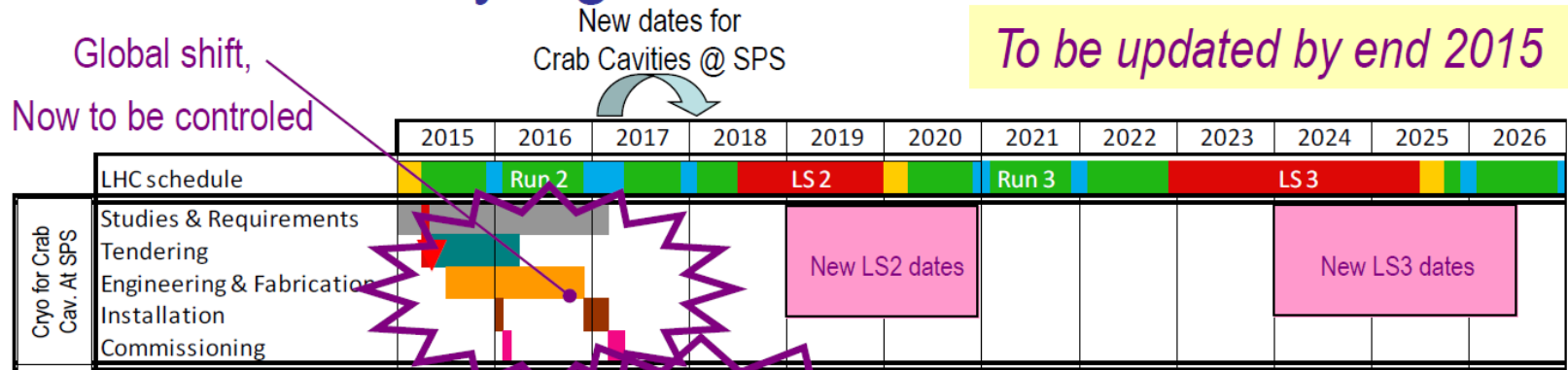
Temperature measurement: 12 CERNOX thermometers placed on the helium tanks and HOM – exact place to be defined, installed by means of screwing

Electrical heaters: 2 x 50 W electrical heaters glued on copper supports then screwed to the bottom of the helium tanks

More information will be given during next CC review on November, 10th and 11th by K. Brodzinski

Cryo Schedule

HL-LHC, Cryo general schedule C&S Review March'15



[see S.Claudet presentation](#)

- The change of SPS location from BA4 to BA6 has an impact on initial cryo planning
 - Modification of design of the main components
 - Relocation of already installed at BA4 equipment is necessary
 - New integration study crosschecked with technical solution is necessary for BA6
- Global planning update is necessary to fit cryogenic activities in the global schedule
- Work on SM18 test preparation to be integrated in planning with details with the first priority

Summary

- Integration study / work underway, progressing well
- Uninstallation of cryo equipment from BA4 this YETS (2015) (among them, He pumps, electrical cabinet, utilities cables, etc.)
- Installation in BA6 scheduled for next year end stop (EYETS 2016)
- Work on SM18 test preparation to be integrated in planning with details with the first priority

THANK YOU FOR YOUR ATTENTION



