Ideas on MAPS design for ATLAS ITk

HV-MAPS challenges

Fast signal Good signal over noise ratio (S/N). Radiation tolerance (various fluences) Resolution and readout rate Filling factor and area coverage Power needs

Signal speed

 $\mathbf V$ ACHIEVED: provided that drift field is created (HV-CMOS technology) even with "large" technology node (AMS .35) the signal can be kept within < 50 ns. Smaller nodes allows for even shorter time performance. The imminent H35 submissions features pixel flavours with more aggressive time performance and will give further reassurance on this aspect.

- **Analog pixels (2 large arrays of 24 rows x 300 columns each)**
	- Flavour 1 (24 rows x 100 columns) \rightarrow mid-gain pre-amp. + low-speed
	- Flavour 2 (24 rows x 100 columns) \rightarrow high-gain pre-amp. + high-speed
	- Flavour 3 (24 rows x 100 columns) \rightarrow low-gain pre-amp. + very high-speed
- **Digital pixels (2 large arrays of 16 rows x 300 columns each)**
	- Flavour 4 (16 rows x 300 columns) \rightarrow CMOS comparator in the periphery
	- Flavour 5 (16 rows x 150 columns) \rightarrow nMOS comparator without TW compensation
	- Flavour 6 (16 rows x 150 columns) \rightarrow nMOS comparator with TW compensation
- **Test structures**
	- Single diodes & extra pixels

Good S/N ratio

The requirement for fast signal shaping limits the noise performance of the analogue stage. For this reason (besides the charge collection speed) the presence of strong electric field in the sensor p-bulk is demanded. Deep depletion operations (where deep is a variable number, but $>$ 50 μ m is a good number) will yield the S/N .

Radiation tolerance (various fluences)

Need to operate with near 100% tracking efficiency after the target irradiation fluence. These will change depending on the radial distance, but we should set ourself targets like 0.5, 1, 3, 5 x 10¹⁵ n_{eq} cm⁻² (displacement damage) and 10, 50, 100 and 250 Mrad (TID). A substantial impact on the performance is given by the biasing scheme.

E-field Lines Comparison

. HV top

- . HV back
- . More uniform field

E-field Value Comparison

Charge Collection Comparison

- . Mip enters at 1ns at width of 45um, 80eh pairs per um
- Deposits total charge of 4000e $\ddot{}$

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Back bias full charge collection at 2ns compared to ≈60% for HV top .

Colled Charge Comparison of 50μm thick sensors, resistivity=1000Ωcm, bias=-60V

The electric field keeps a similar shape with irradiation and the backplane biasing should allow violating the maximum applied bias allowed from the technology.

Radiation tolerance (various fluences)

Substrate resistivity is also a parameter for radiation tolerance. The depletion depth depends on both the resistivity and the applied bias voltage. It could be a parameter that is advantageous to optimise for the specified target fluence (layer). It should be notice that the effective space charge(N_{eff}) of p-type bulk silicon does not increase immediately with irradiation!

Edge-TCT

Chess1, not irradiated

1) charge: time integral of induced current pulse (25 ns) 2) velocity (in E-TCT): induced current immediately after the laser pulse

• charge collection region wider (diffusion)

 \rightarrow take into account non zero laser beam width (\approx 10 µm)

Edge-TCT

Chess1, irradiated with neutrons to 2e14 n/cm² in reactor in Ljubljana

- charge collection region narrower
- field region (velocity) increases \rightarrow acceptor removal
- no long tails of induced current pulses \rightarrow trapping, less diffusion

Edge-TCT

Chess1, irradiated with neutrons up to 5e15 n/cm2 Fluence steps: 2e14, 5e14, 1e15, 2e15, 5e15

• the depth with electric field (depleted depth) increases with fluence up to ~1e15

Soncentration of initial acceptors falls with irradiation faster than new acceptors are introduced \rightarrow space charge conc. falls

- depleted depth smaller at 5e15 than at 2e15
	- \rightarrow acceptor removal finished, space charge concentration increases with irradiation
- * after 5e15 depleted depth still much larger than before irradiation

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• charge collection region at 5e15 (4e15) smaller than after 2e15 but still much larger than before irradiation

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Edge-TCT

• from E-TCT measurements extract the charge collection width vs. Bias voltage

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MIP CC measurement

CHESS1 large passive HV-CMOS array - 3 devices irradiated with neutrons Fluences: 2e14, 5e14, 1e15, 2e15, 5e15

- . charge drops after first irradiation steps: smaller diffusion contribution
- charge increases with more irradiation \rightarrow depleted region increases due to acceptor removal
- \cdot charge drops at higher fluence \rightarrow acceptor removal finished, space charge conc. increases with fluence,

more charge trapping

Calculate CC for different resistivites:

The idea of tuning the resistivity to the radiation fluence is feasible mainly if backside biasing is implemented.

Resolution and readout rate

Compromise between the pixel size and the readout complexity.

- Small pixels can be achieved in CMAPS, analogue encoding can be used for improving granularity. All this adds to the digital circuitry.
- Part (if not all) of the digital activity is outside the sensitive area and it has impact on tiling.

Filling factor and area coverage

Filling factor has two aspects: in the active area (possible loss of efficiency in the inter-area between collecting n-wells) and periphery for digital circuits The first effect is strongly mitigated (aka solved) by "deep depletion" and collection by drift.

The second aspect depends on readout architecture and choices (e.g. In pixel discrimination).

LF15A is a modular 0.15 μ m RF CMOS process, offering up to 6 levels of AI plus thick metal (2 - 6 μ m), optionally a MIM capacitor, a polyimide passivation and I/O voltages of 1.8 V, 3.3V and 5.0 V.

- Substrate resistivity 1-2 $k\Omega$ cm
- Allow isolated NWELL within a DNWELL (Full CMOS)
- Large fill factor ~85% for 50x250 um^2 pixel
- Break down voltage ~120V

Thinned to 125um:

- full depletion from the back side should be feasible (80V at $2k\Omega$ cm)
- $Q_{MIP} \sim 10000e^{-t}$
- Cin ~ 400fF (70fF DNW to SUB, 330fF DNW to PW) for $50x250 \mu m^2$ pixel (worst case)
- Considering sharing a threshold around 1000e should give us reasonable efficiency. Required Noise ~100e⁻

Filling factor and area coverage

The reticule size with a maximum of \sim 2 x 2 cm² obliges to make a rather laborious tessellation work to produce large area systems. This could be improved if CMAPS detector can be diced in multiple reticules. The inter-reticule area could result in a non-sensitive region. This has to be minimised or made sensitive. Deep-depletion devices can allow to make the field extended laterally to cover the inter-reticule area. We need to study how strongly this mitigation factor improves the coverage using stitching methods (with the foundries that allow for it) or by dedicated crafting of the n-well geometry in the border pixels.

Routing demonstrator - Floorplan

• **Floorplan** (engineering run with maximum reticle size of 1.9 cm x 2.45 cm)

Filling factor and area coverage

The routing of channels to a readout pad area could allow to use a small readout chip for removing the digital circuits from periphery (this implies use of stitching and TSV on the readout chip).

HV-MAPS challenges

Fast signal √

Good signal over noise ratio (S/N). Improving if backplane biasing implemented. At CMOS foundry level or post processing.

Radiation tolerance (various fluences).). Improving if backplane biasing implemented. Possible playing with substrate resistivity. NOTE: deep depletion with high voltage better than deep depletion with high res substrate. Resolution and readout rate. System dependant. Optimisation exercise.

Filling factor and area coverage. Study stitching or multireticule dicing.

Power needs. System dependant.