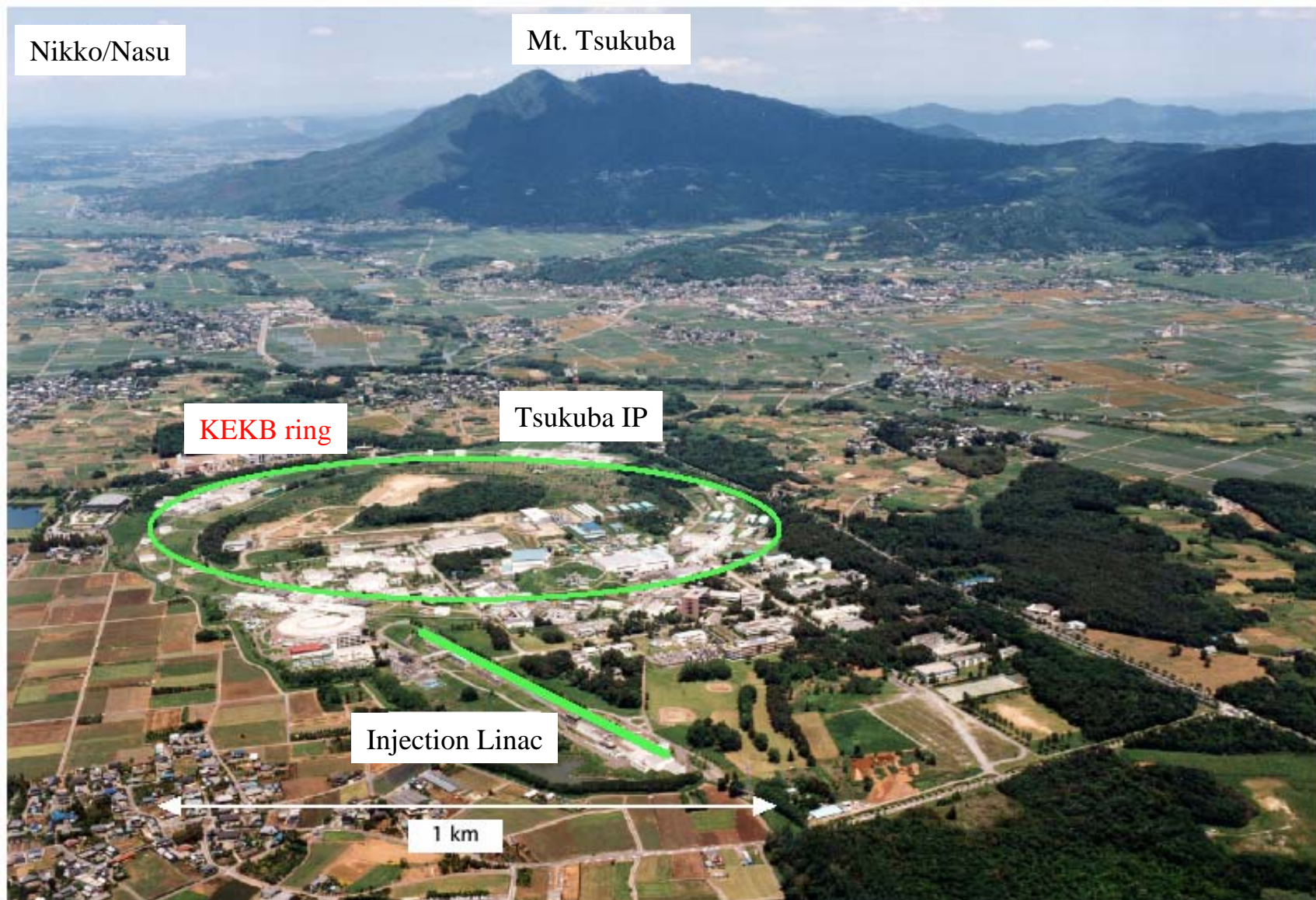


# *KEKB RF System*

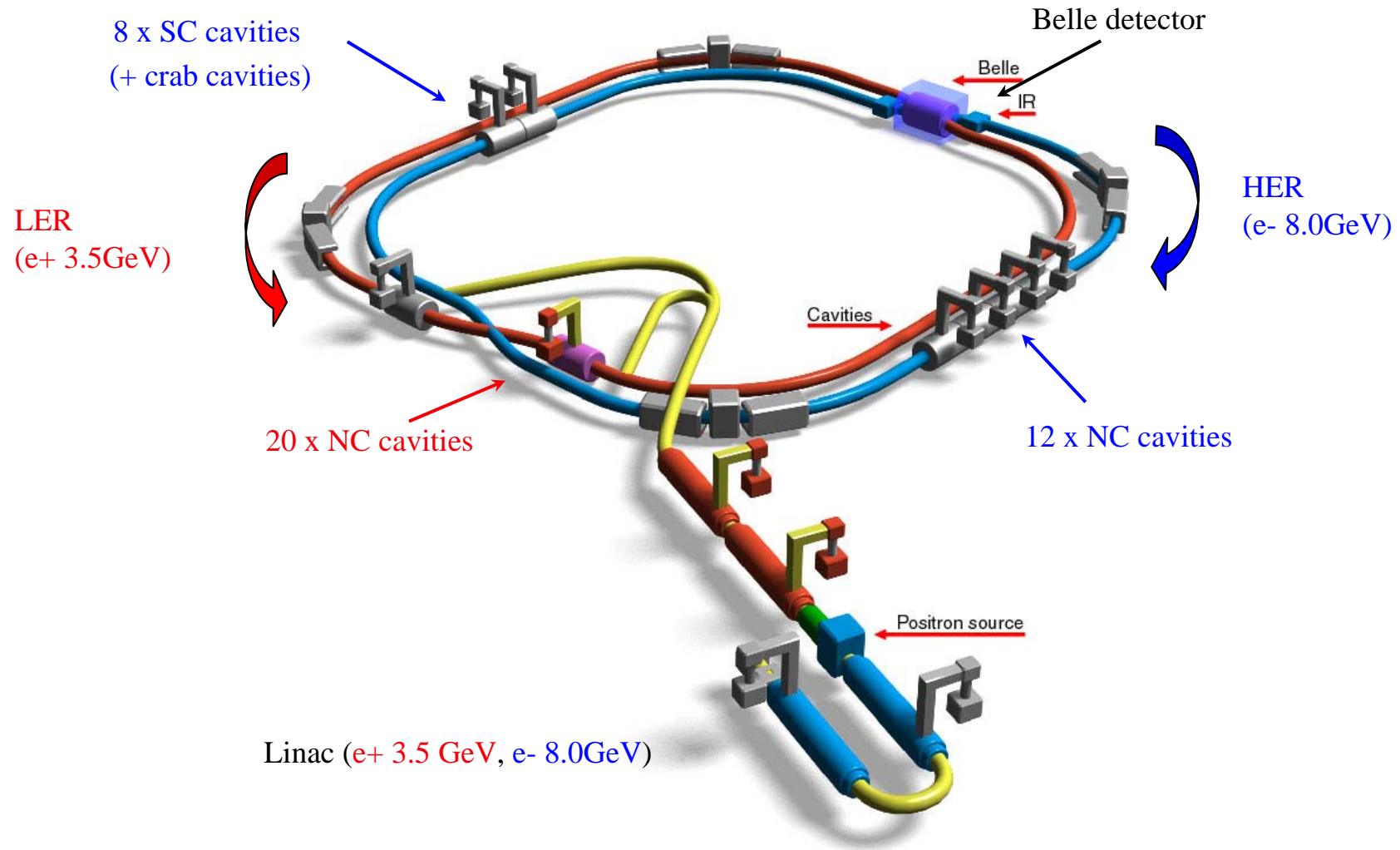
- 1. Overview of KEBB-RF*
- 2. Operational experience*
- 3. Upgrade projects*

K. AKAI for KEBB-RF group  
LLRF workshop, Oct. 10, 2005 at CERN



KEKB RF system (K. Akai)

# *KEKB factory and injector*



# *History of KEKB*

- 1994 Construction started
- 1995 Jun. Design report completed
- 1998 Dec. Beam commissioning started
- 1999 May Belle detector installed
- 2001 Apr. Reached record luminosity
- 2003 May Reached design luminosity ( $1 \times 10^{34} / \text{cm}^2 \text{s}$ )
- 2005 May Peak luminosity is  $1.58 \times 10^{34} / \text{cm}^2 \text{s}$

Number of RF cavities and RF stations

	LER	HER	
	ARES (Kly)	ARES (Kly)	SCC (Kly)
1998 Dec.	12 (6)	6 (3)	4 (4)
1999 Oct.	16 (8)	10 (5)	4 (4)
2000 Oct.	16 (8)	10 (5)	8 (8)
2001 Oct.	20 (10)	12 (6)	8 (8)
2005 Sep.	20 (10)	12 (7)	8 (8)
2006	Crab cavities will be installed.		

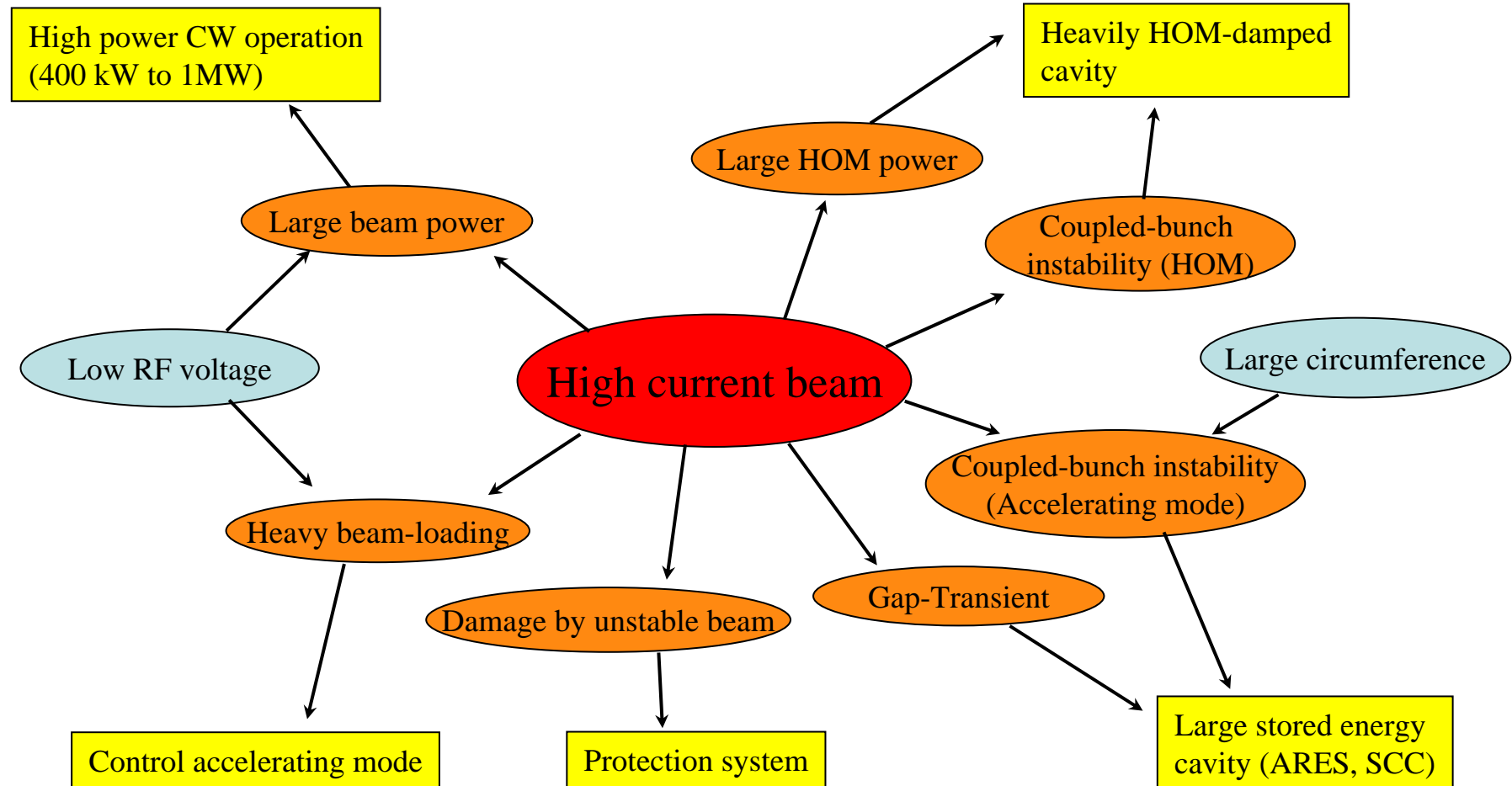
QuickTimeý Ç?  
TIFFÁià èkÇ»ÇuÁj êLiÉÈvÉçÉOÉaÉÄ  
Ç™Ç±ÇÄÉsÉNÉ`ÉÉÇ%â©ÇÉÇZÇ½Ç...ÇÖiKóvÇ-Ç`ÁB

## *RF-related parameters (design)*

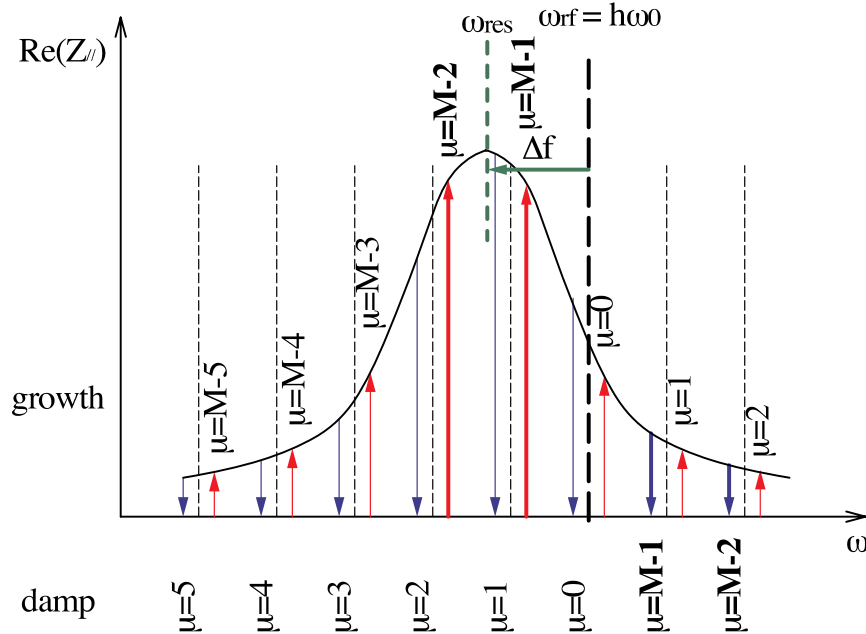
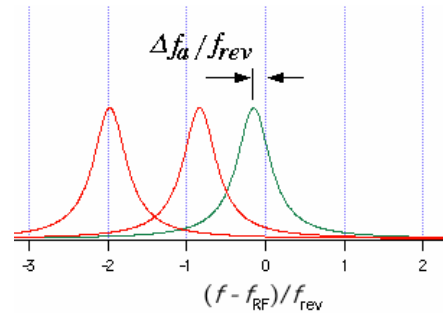
Ring	LER	HER	
Beam energy (GeV)	3.5	8.0	
<b>Beam current (A)</b>	<b>2.6</b>	<b>1.1</b>	
Wiggler magnets	yes	no	
Energy damping time (ms)	23	23	
Energy loss/turn (MeV)	1.6	3.5	
<b>Total beam power (MW)</b>	<b>4.5</b>	<b>4.0</b>	
Total RF voltage (MV)	10	17.9	
Bunch length (mm)	4	4	
<b>Cavity type</b>	<b>ARES</b>	<b>ARES</b>	<b>SCC</b>
<b>No. of cavities</b>	<b>20</b>	<b>12</b>	<b>8</b>
<b>Voltage /cav. (MV)</b>	<b>0.5</b>	<b>0.5</b>	<b>1.5</b>
<b>Input coupling</b>	<b>2.7</b>	<b>2.7</b>	<b>-</b>
<b>Loaded-Q value (x10E4)</b>	<b>3.0</b>	<b>3.0</b>	<b>7.0</b>
<b>Beam power /cav. (kW)</b>	<b>225</b>	<b>170</b>	<b>240</b>
<b>Wall loss /cav. (kW)</b>	<b>150</b>	<b>150</b>	<b>-</b>
<b>Klystron power (kW)</b>	<b>810</b>	<b>730</b>	<b>270</b>
<b>No. of klystrons</b>	<b>10</b>	<b>6</b>	<b>8</b>

# Requirements for KEKB-RF system

---



# CBI due to the accelerating mode



- Detuning in storage rings,
  - Resonant frequency of the accelerating mode should be detuned to match to beam (optimum tuning)

$$\Delta f = -\frac{I_b \sin \phi_s}{2V_a} \times \left( \frac{R}{Q} \right) \times f_{rf} = -\frac{P_b \tan \phi_s}{4\pi U}$$

- In a large circumference ring with high beam current,
  - Large detuning due to high beam current
  - Small revolution frequency
  - High impedance of the accelerating mode
- CBI of -1, -2, etc. modes can arise, growth rate can be very high.
- To reduce the detuning frequency,
  - Operate with high RF voltage
  - High stored energy in cavity
  - Reduce R/Q value of cavity



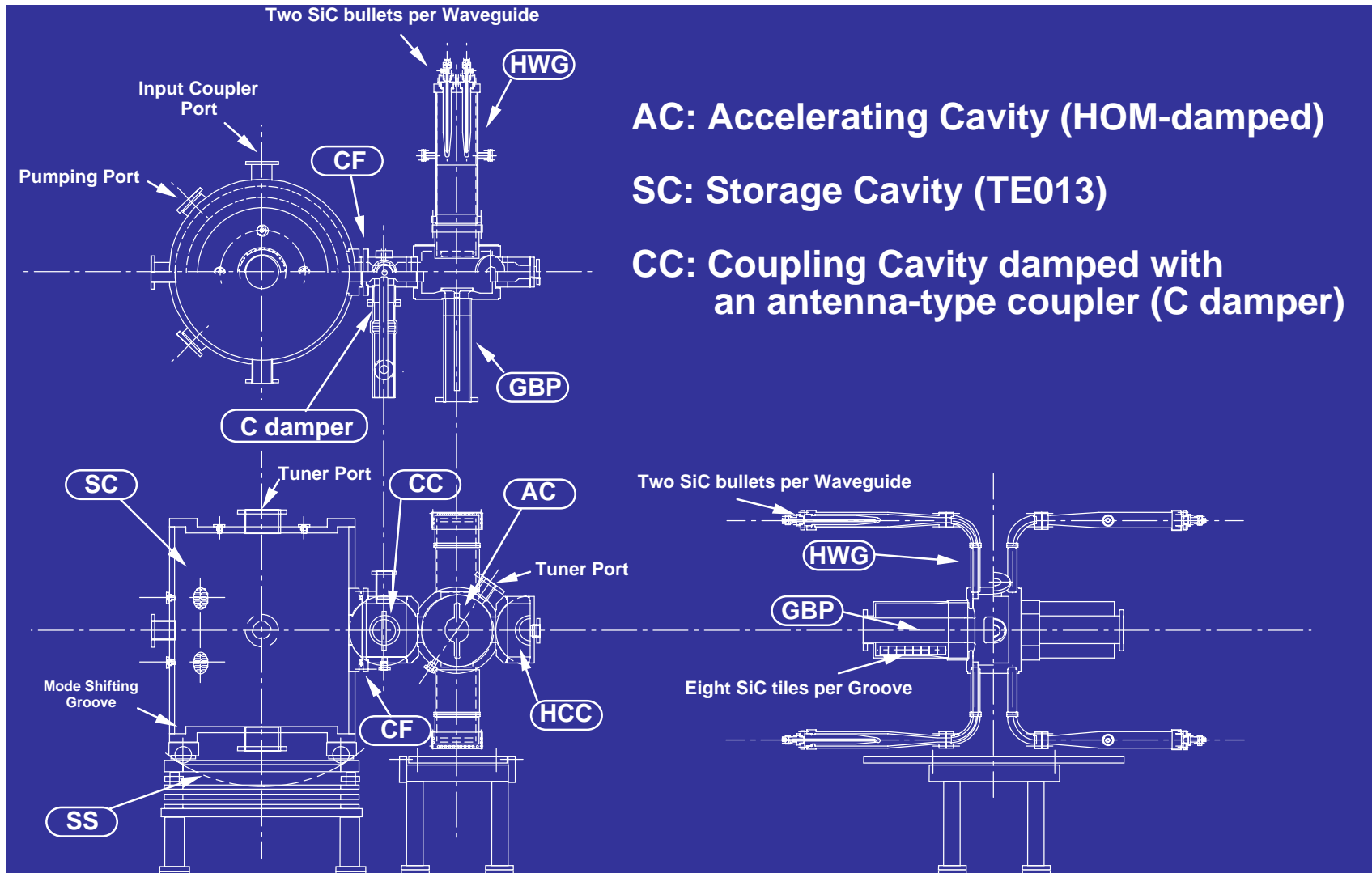
# *KEKB-RF cavities*

---

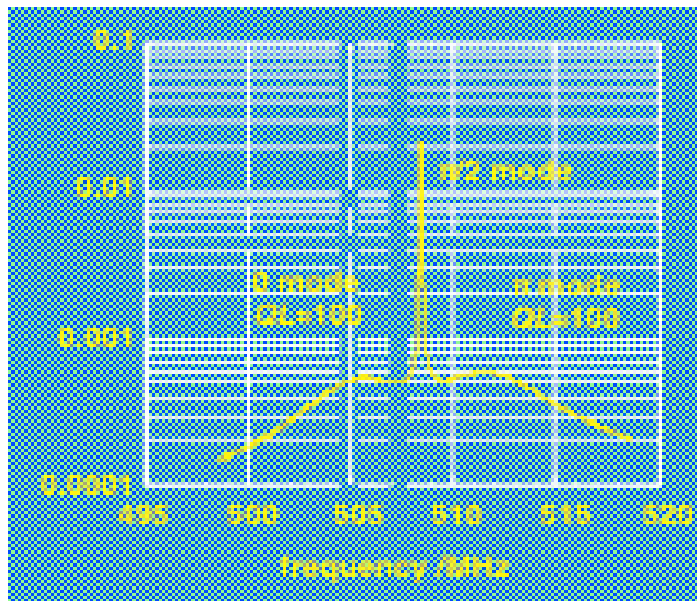
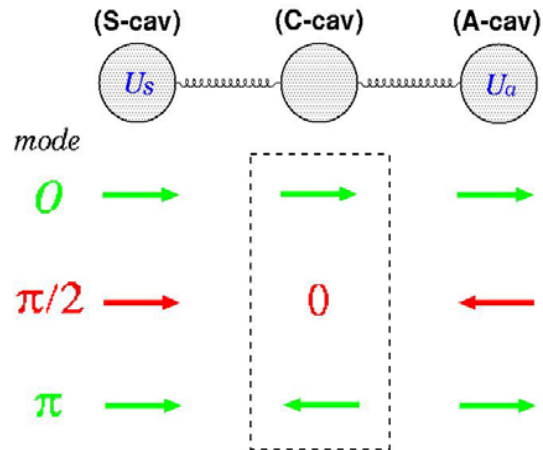
- Large stored energy (ARES, SCC)
  - Suppress the CBI associated with the accelerating mode.
  - Bunch gap transient effect is reduced.
- Heavily-damped structure
  - Suppress the CBI due to HOMs
- Operation
  - LER uses the ARES
    - More suitable for higher beam-loading
  - HER adopts hybrid of SCC and ARES
    - Most of the RF voltage is supplied by the SCC.
    - Phase of ARES is shifted w.r.t. SCC, so that the ARES supplies half of beam power (the other half by SCC).

*Accelerator Resonantly-coupled with Energy Storage*

**3-cavity system stabilized with the  $\pi/2$ -mode operation**

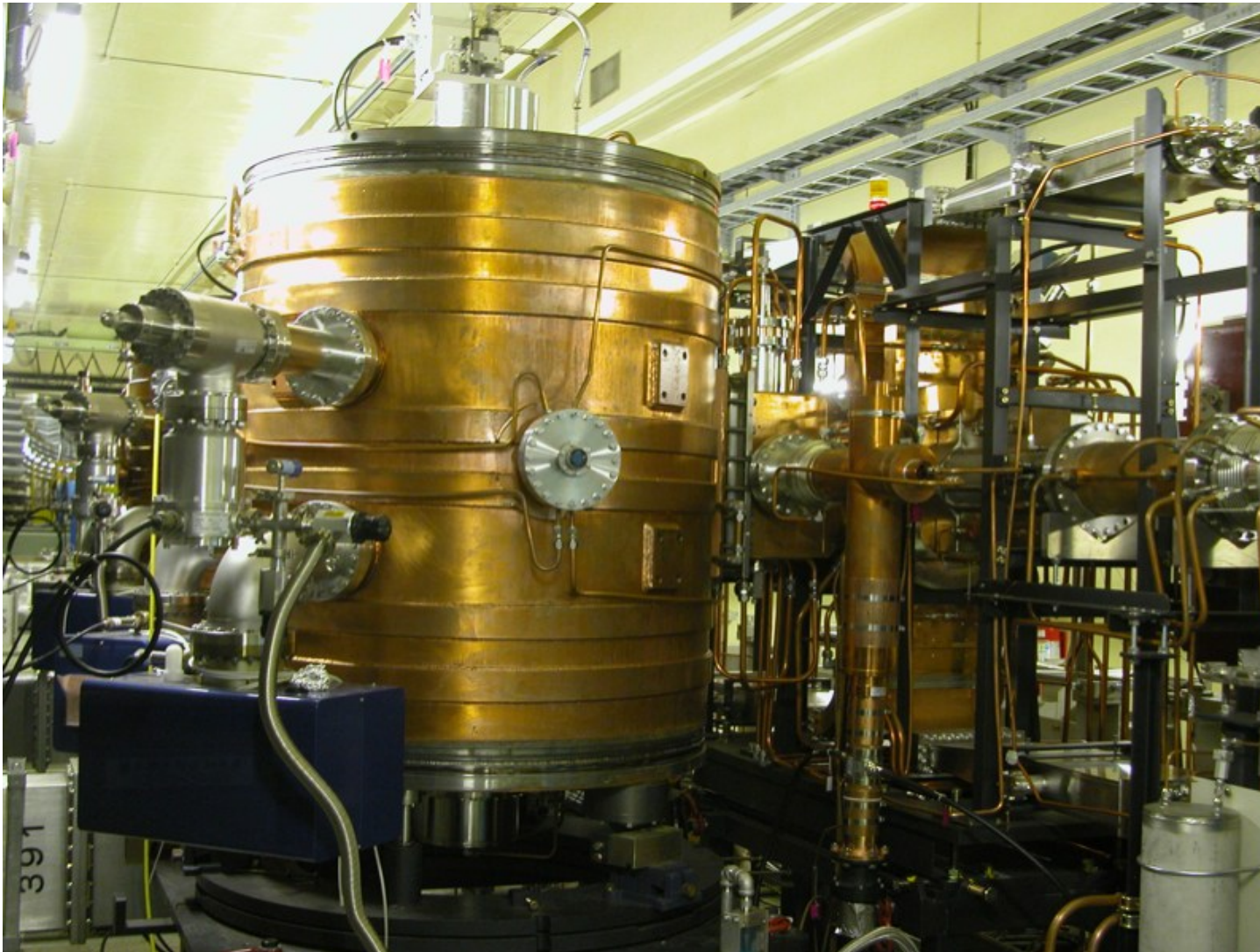


# Principle of ARES cavity

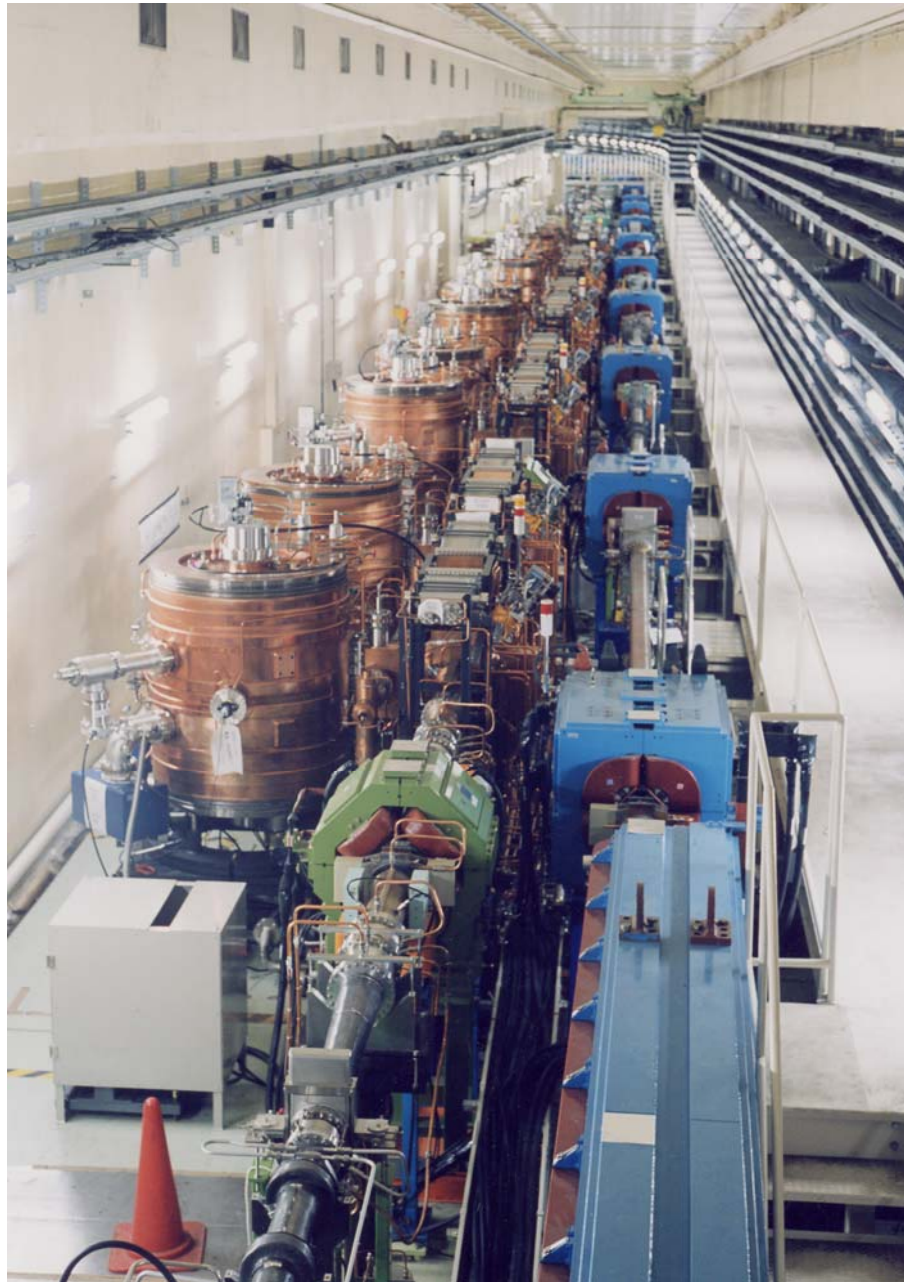


- High stored energy in the storage cavity operating at TE<sub>013</sub> mode.
- Three modes for the three-cavity system
  - The  $\pi/2$  mode: operating mode
    - $U_s:U_a=9:1$ . Ten times total stored energy compared to the accelerating cavity only. The detuning frequency is reduced to 1/10.
    - The  $\pi/2$  mode is more stable than other modes against beam-loading or errors.
  - 0 and  $\pi$  modes: parasitic
    - Damped to  $Q=100$  by an antenna at the coupling cavity.
    - The impedance of 0 and  $\pi$  modes is about symmetry w.r.t. the  $\pi/2$  mode. Growth rate due to these modes are almost cancelled.

# 1 set of ARES cavity in KEKB tunnel



ARES cavities  
in Fuji straight section

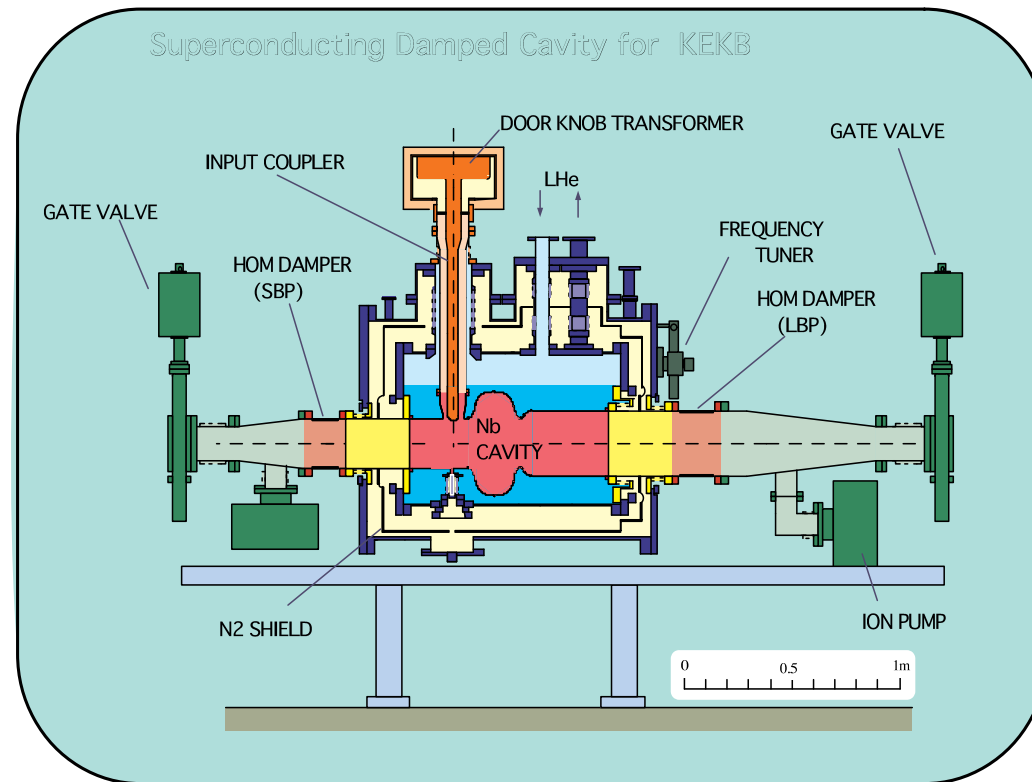


KEKB RF system (K. Akai)

# *KEKB superconducting cavity*

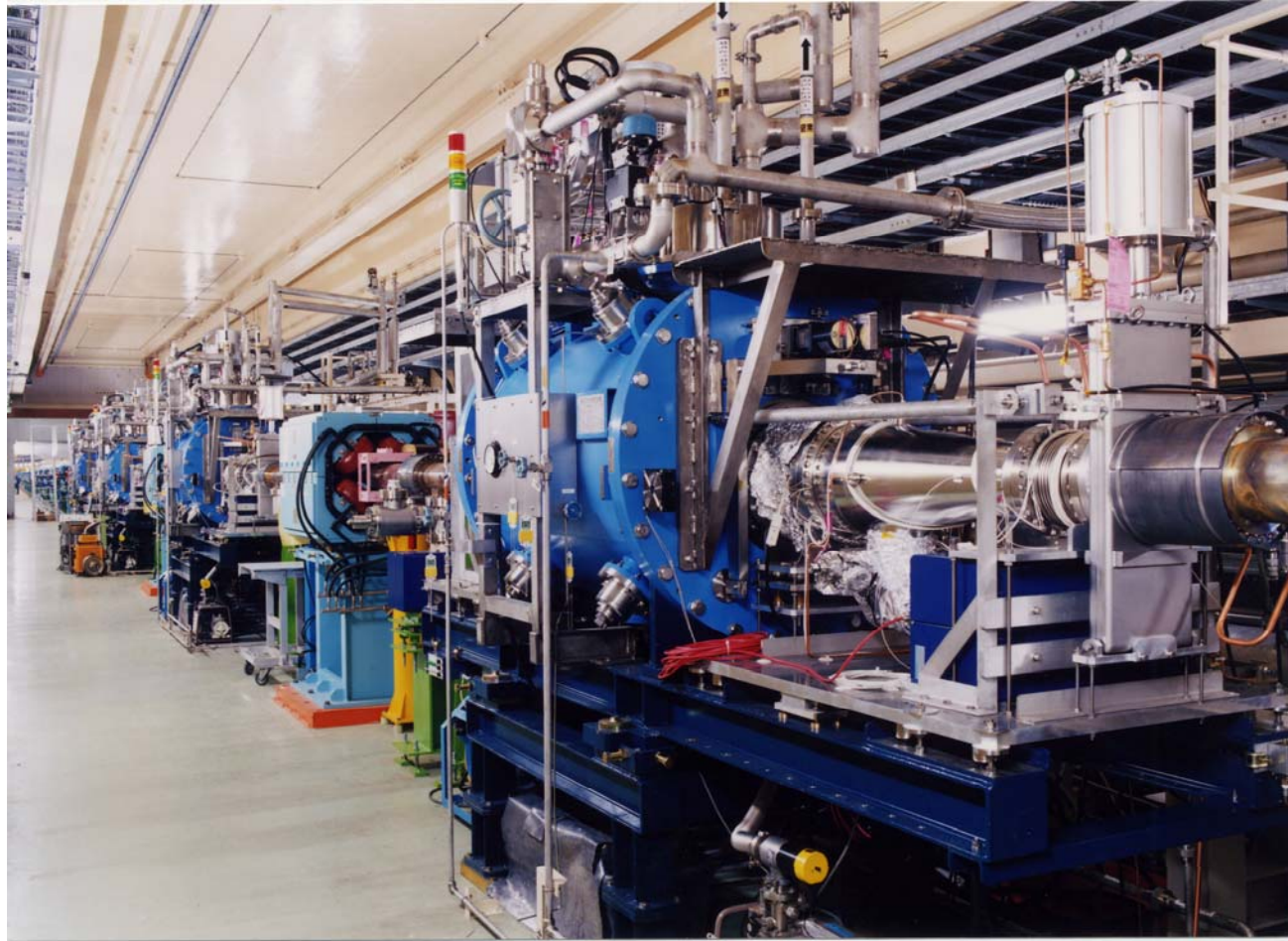
- Features

- Single-cell HOM damped cavity.
- Lower R/Q value and higher voltage than NC cavity: the CBI due to the accelerating mode can be suppressed.
- Ferrite is attached inside the beam pipe by Hot Isostatic Press method.



KEKB RF system (K. Akai)

## SC cavities in Nikko straight section

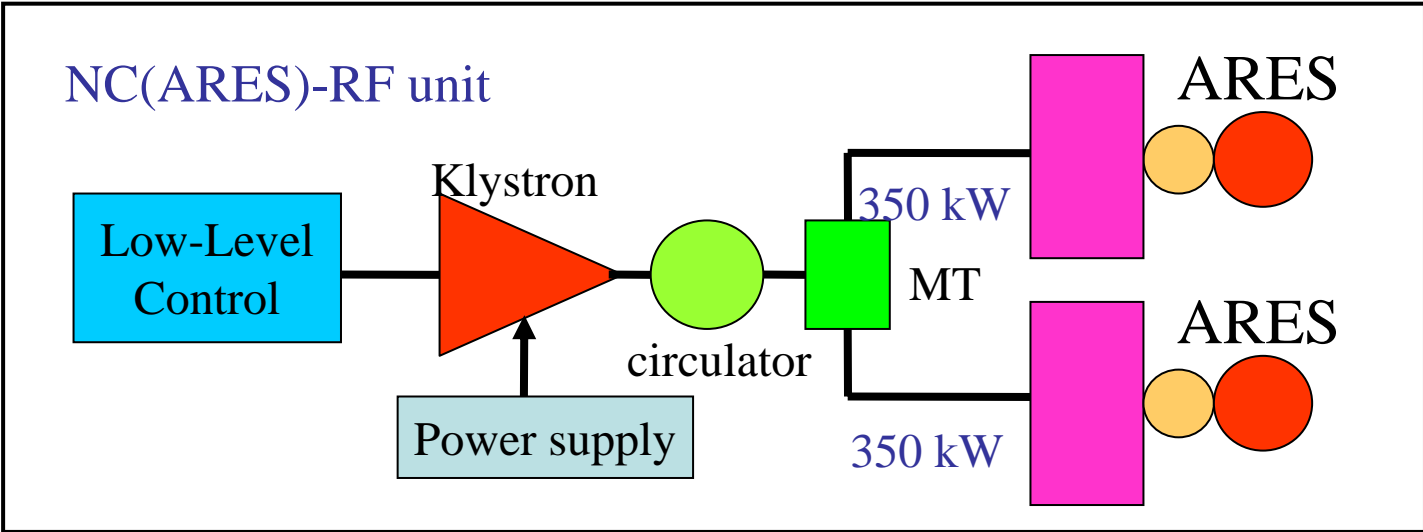


# *High power and LLRF system*

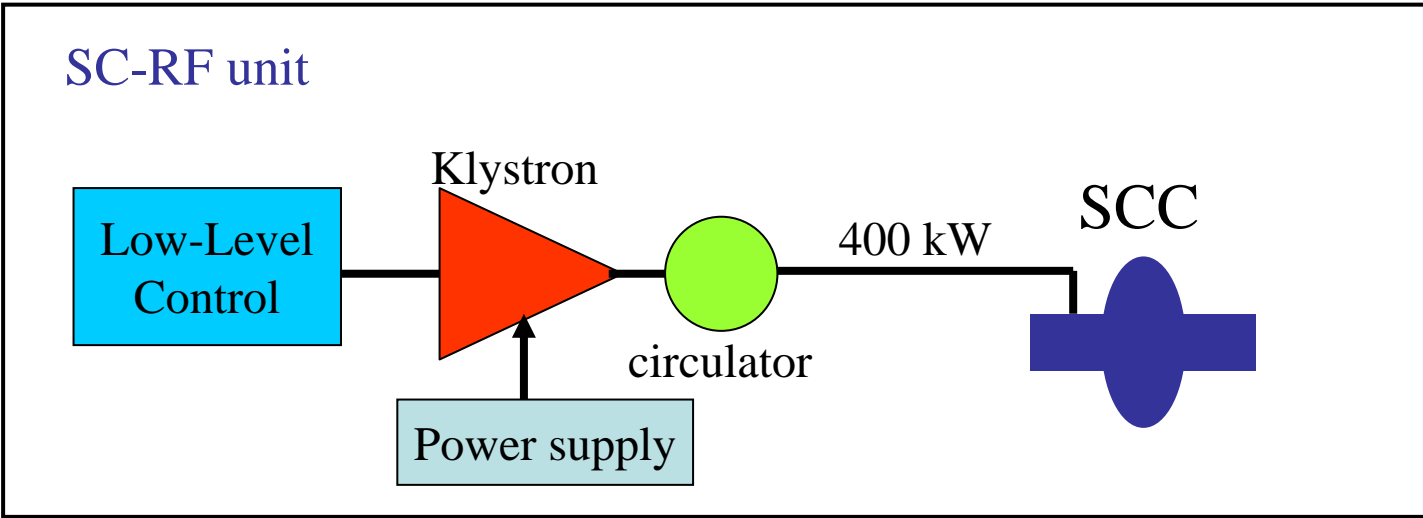
---

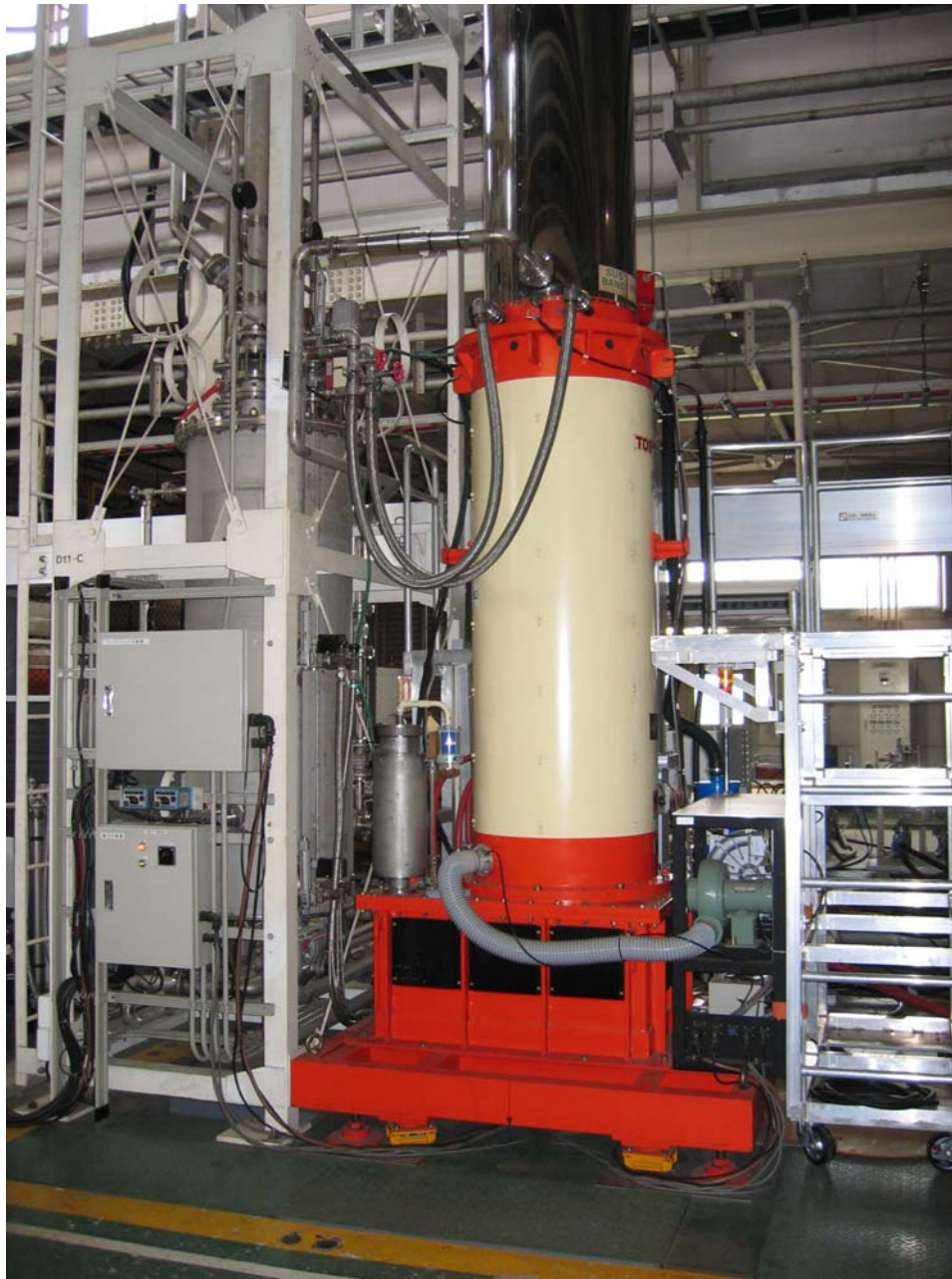
- From TRISTAN to KEKB
  - Same RF frequency (509 MHz).
  - Most of the high-power components such as klystrons, circulators and waveguides were taken from TRISTAN.
  - It reduces construction cost.
  - The RF system and its components have been re-examined to meet the increased demands associated with high luminosity of KEKB.
- As for LLRF
  - Most of control modules also taken from TRISTAN: mostly analog.
  - Incorporated new feedback loops including direct RFFB.
  - Zero-mode and the -1 mode stabilizer was added.
  - Interlock and beam abort trigger system has been improved.





(This year two ARES cavities have been changed to 1:1 configuration.)

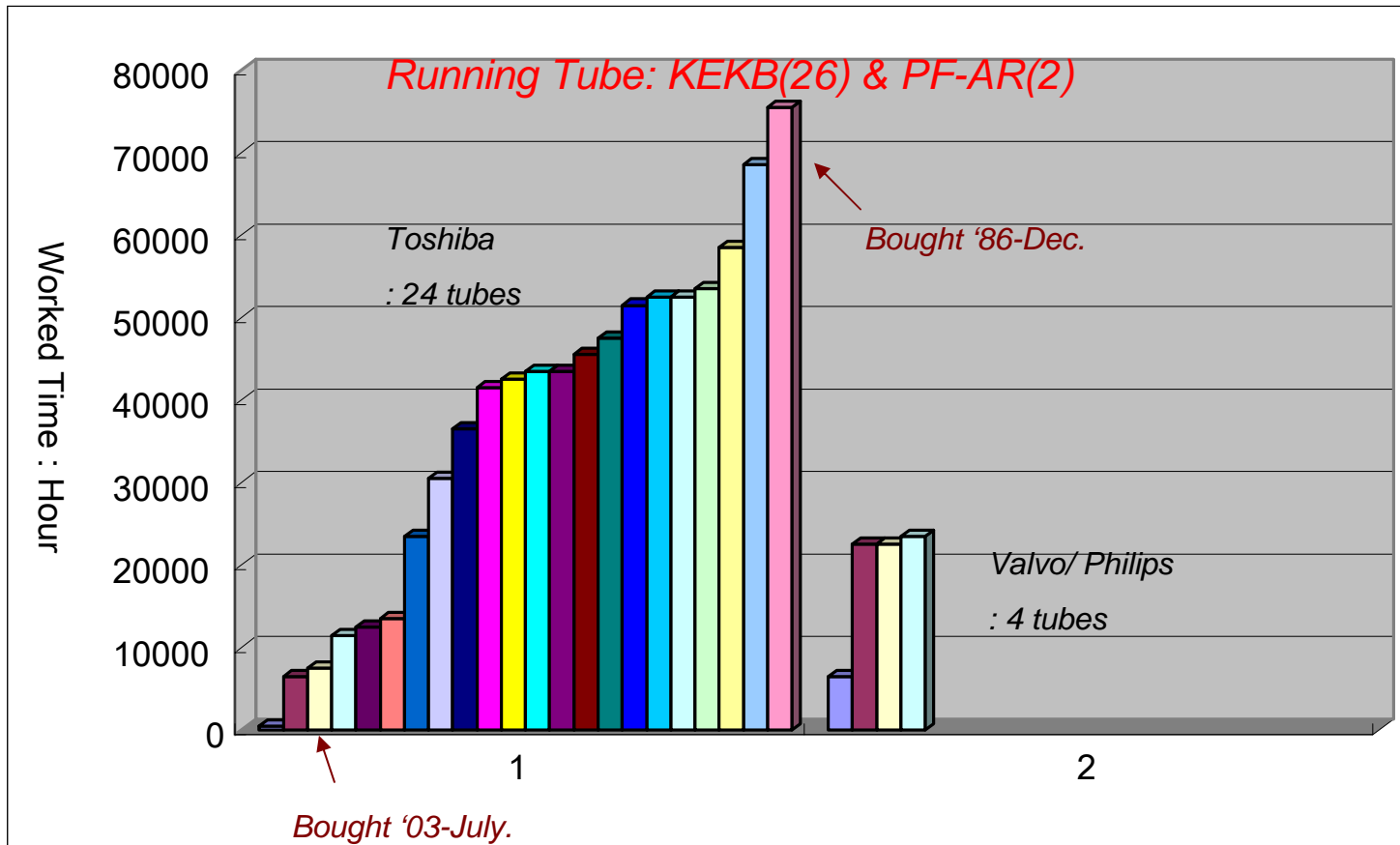




Toshiba 1.2 MW CW  
Klystron

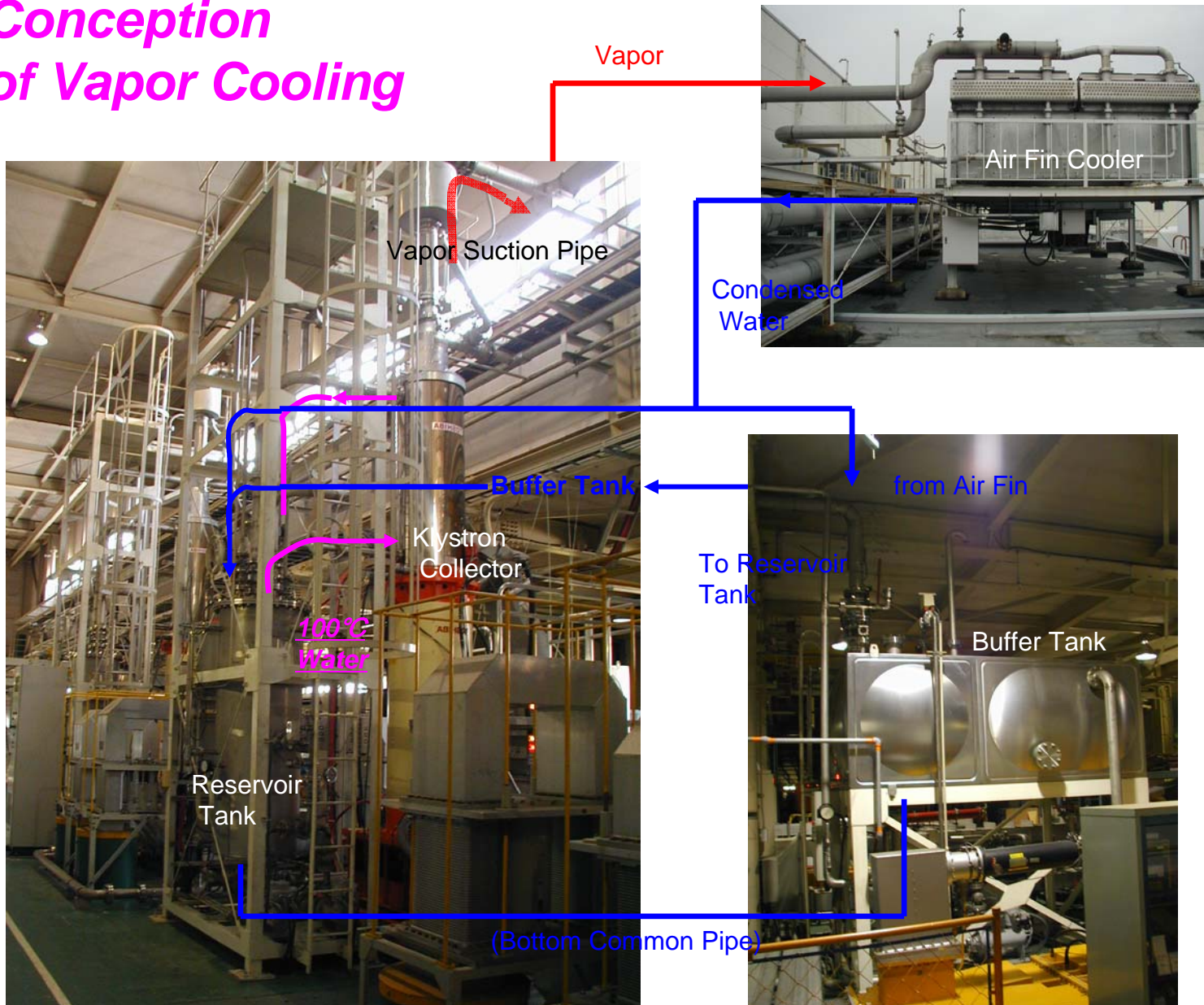
# Klystron worked time

: (S. Isagawa; 04/08/16)



*Reliable operation of Klystrons continued since TRISTAN.*

# Conception of Vapor Cooling



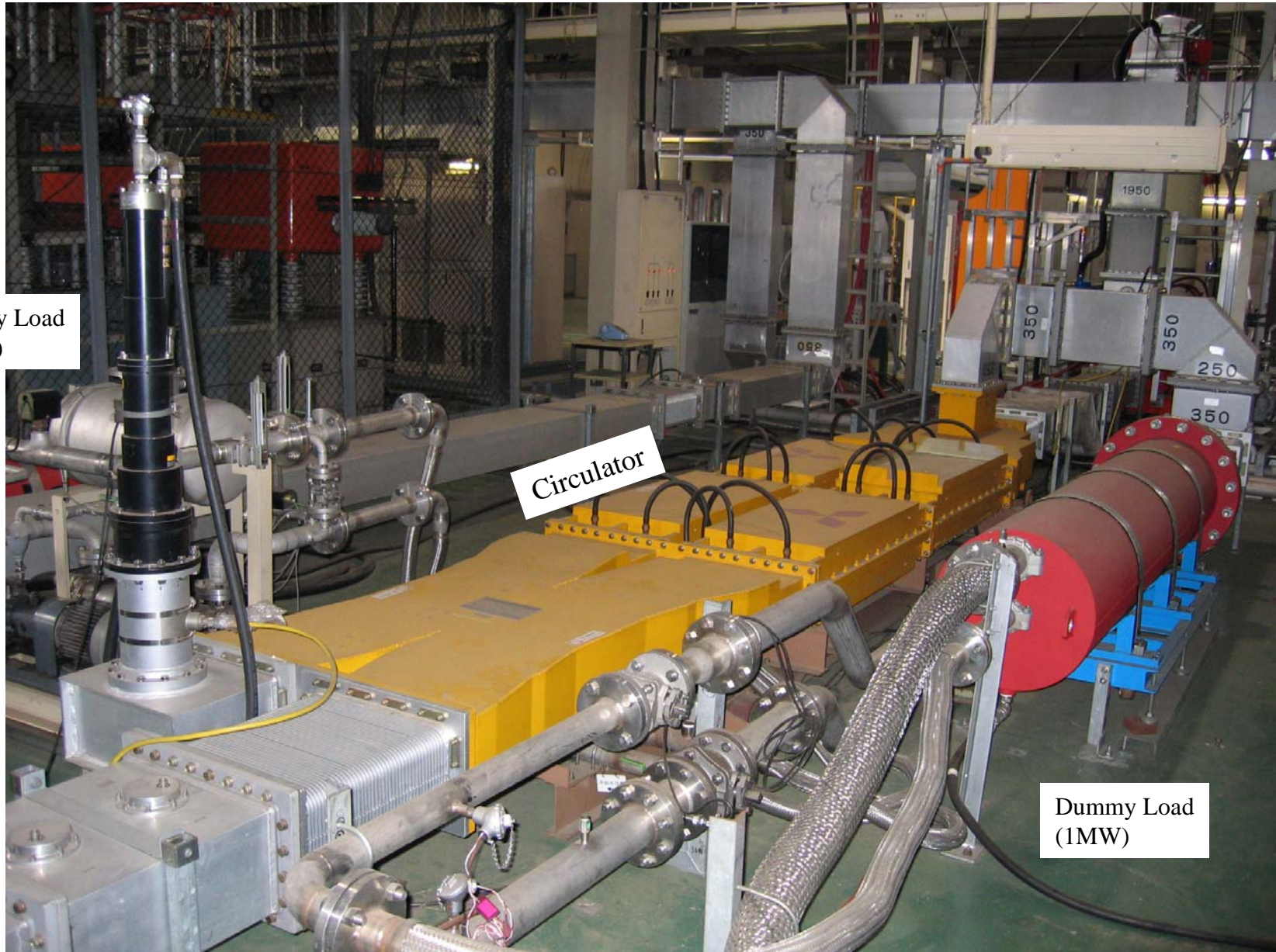
KEKB RF system (K. Akai)

# High power RF system (Circulator, Waveguide, Dummy-load)

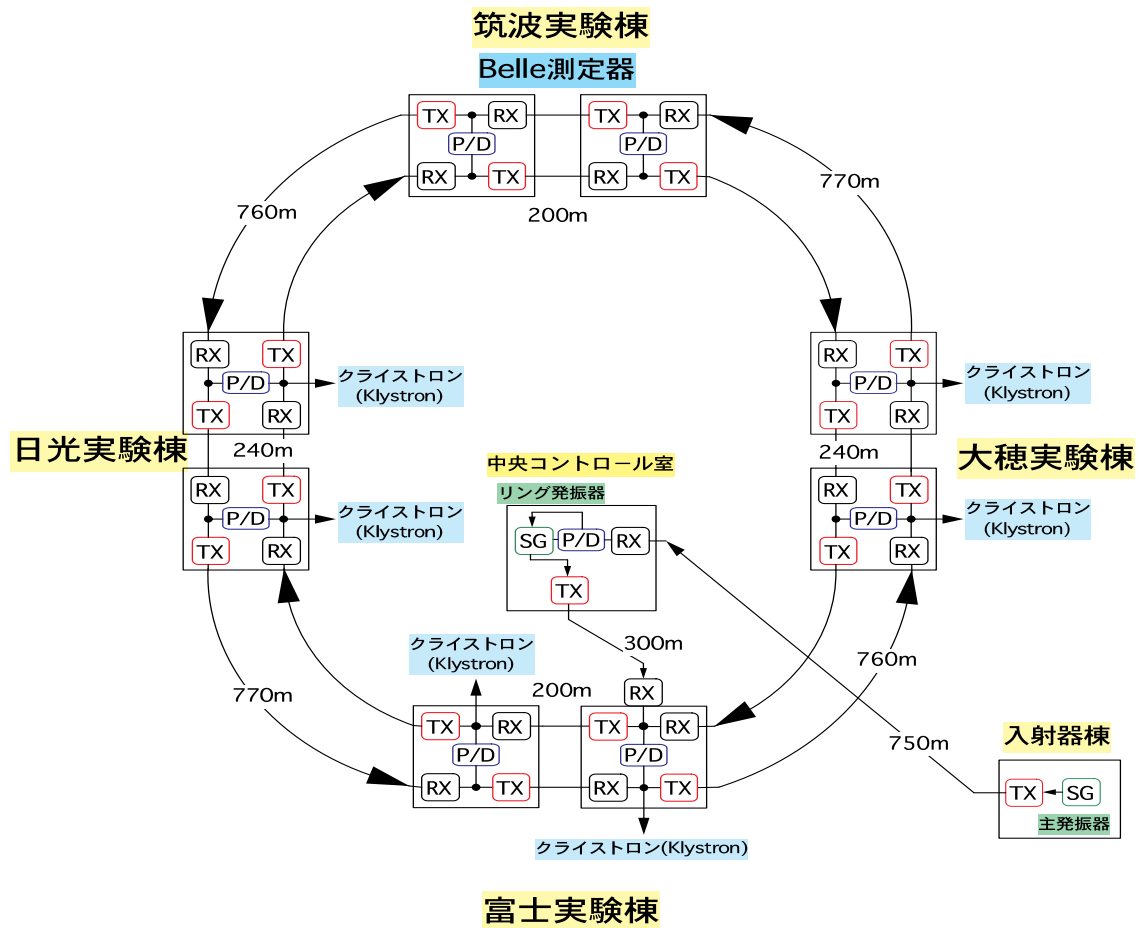
Dummy Load  
(40kW)

Circulator

Dummy Load  
(1MW)

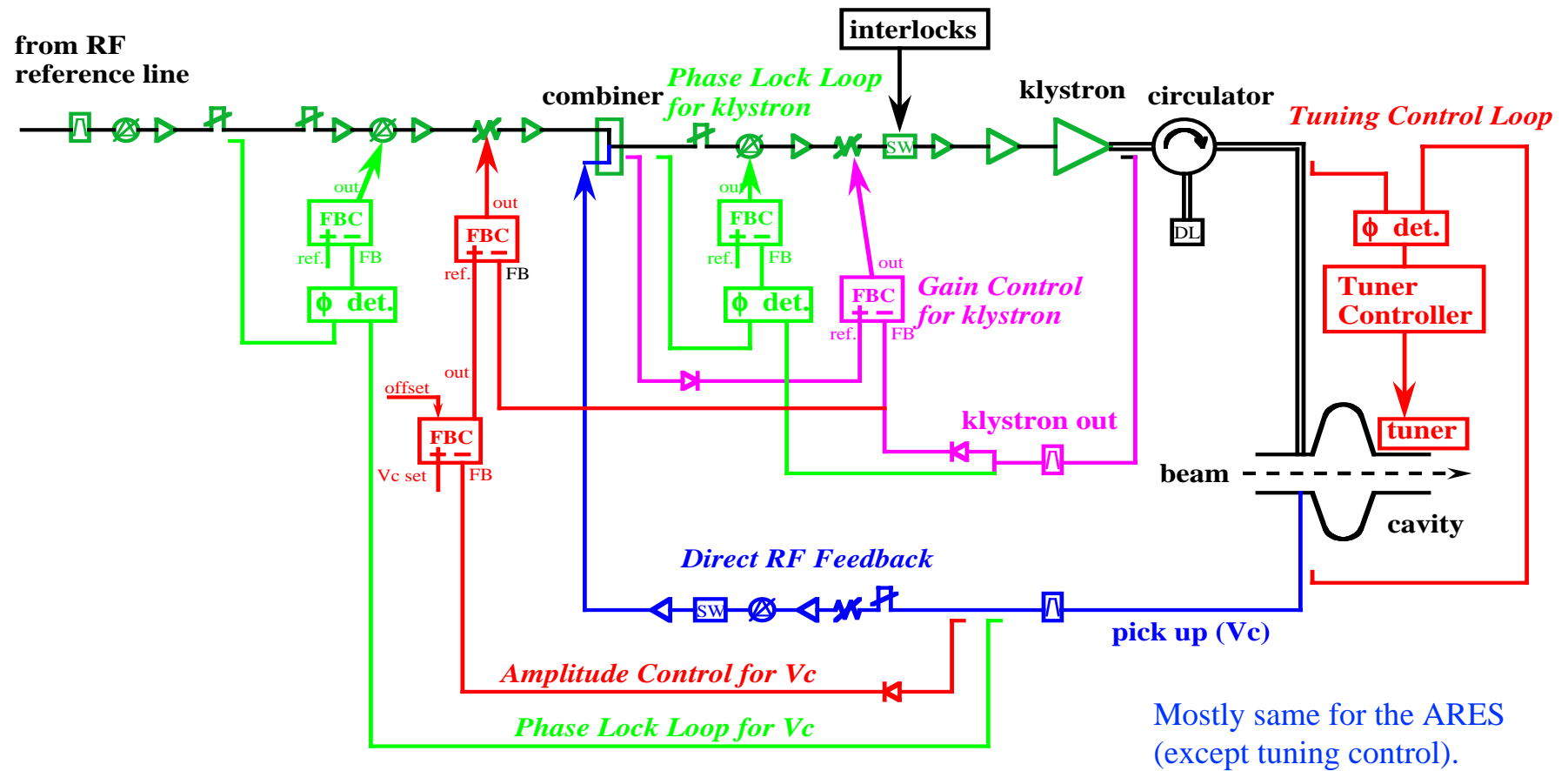


# RF reference line for KEKB ring

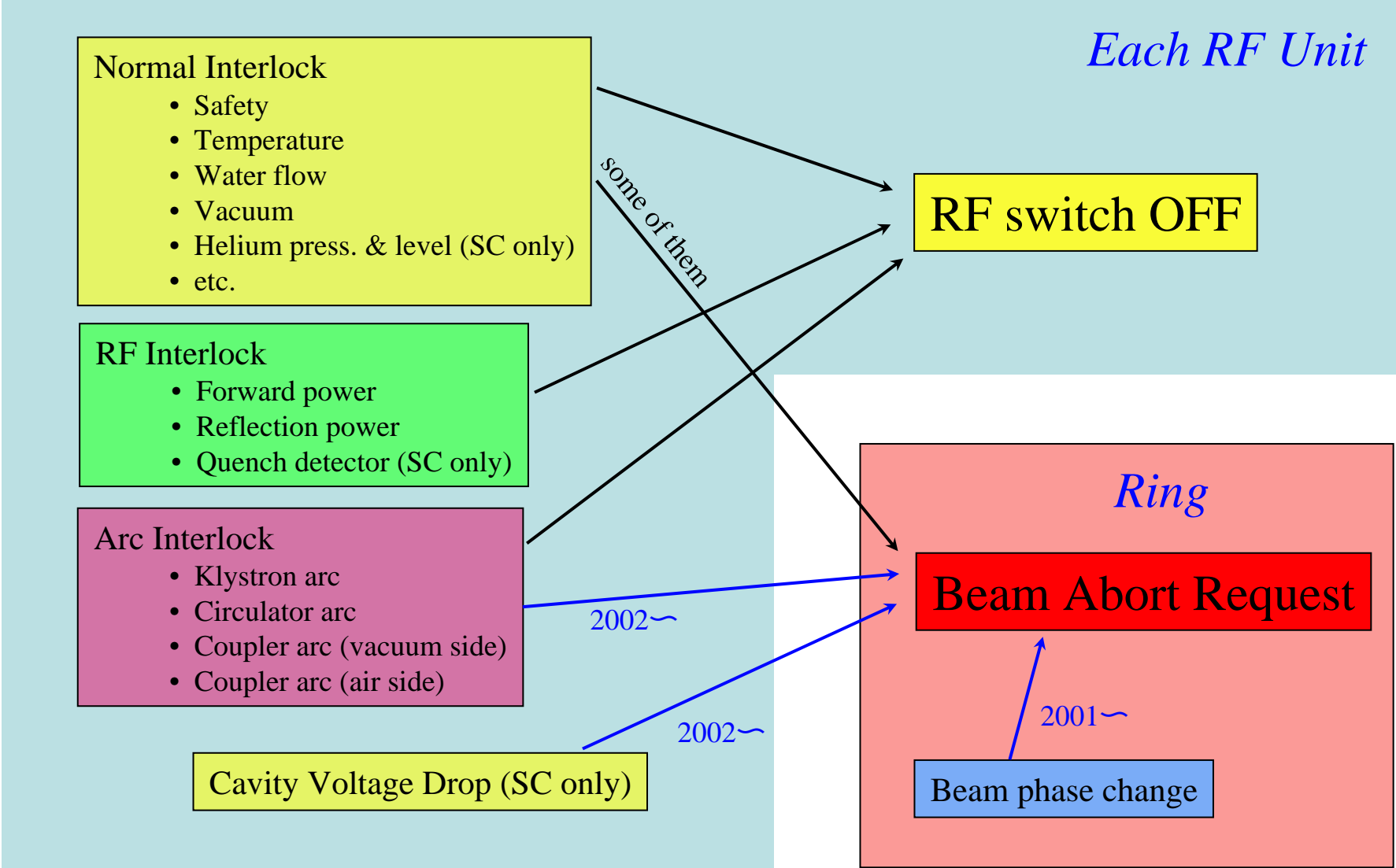


- TX 送信器(Transmitter)
- RX 受信器(Receiver)
- P/D 位相計(Phase detector)

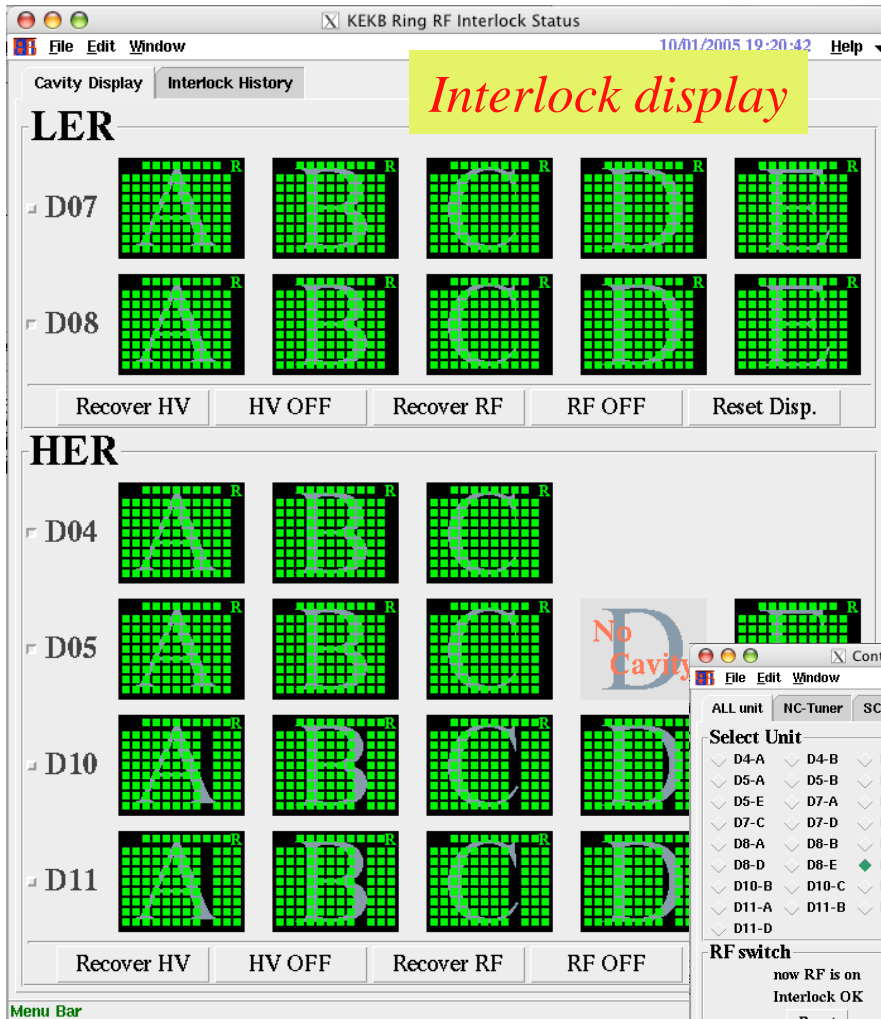
## Low-level RF for KEKB Superconducting cavity



# Interlock system

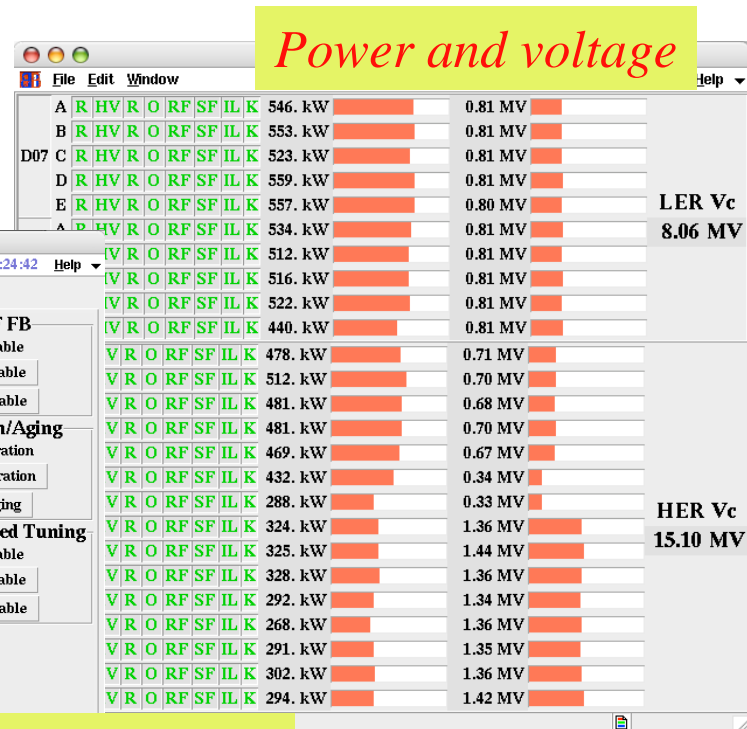




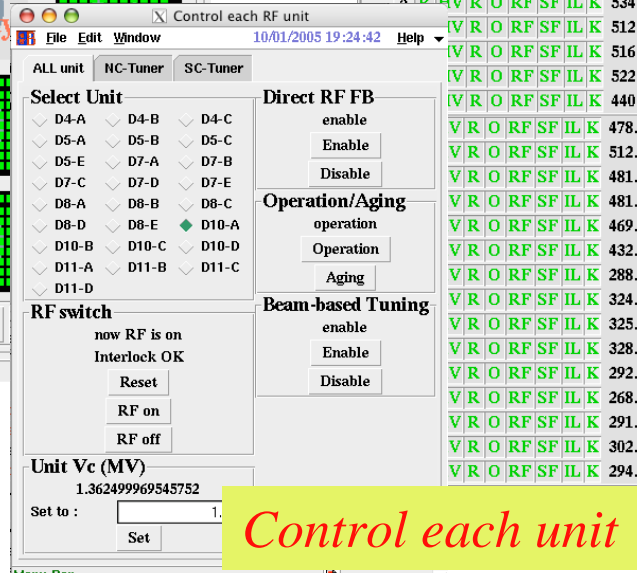


- Control software (EPICS/SAD)

- Status display
- Set operating parameters
- Control each components
- Recover RF after beam aborts
- Cavity conditioning
- etc.



And more . . .



# *Operational status*

---

- **Stable operation continues at high beam current and high RF power.**
  - Frequency of beam aborts due to any RF trip is only about 1/day.
- **No coupled-bunch instability due to HOMs has been observed.**
  - Excellent HOM damping scheme and reliable HOM damper.
- **Hardware troubles**
  - We had experienced several hardware troubles in the early period.
  - After 2002 we seldom have serious troubles that stop the beam operation for long time.
- **Stability of the accelerating mode**
  - Most of difficulties due to heavy beam-loading are eased by high stored energy of the ARES and SCC.
  - However, the 0-mode and -1 mode beam oscillation was stronger than expected. They are stabilized by corresponding dampers.

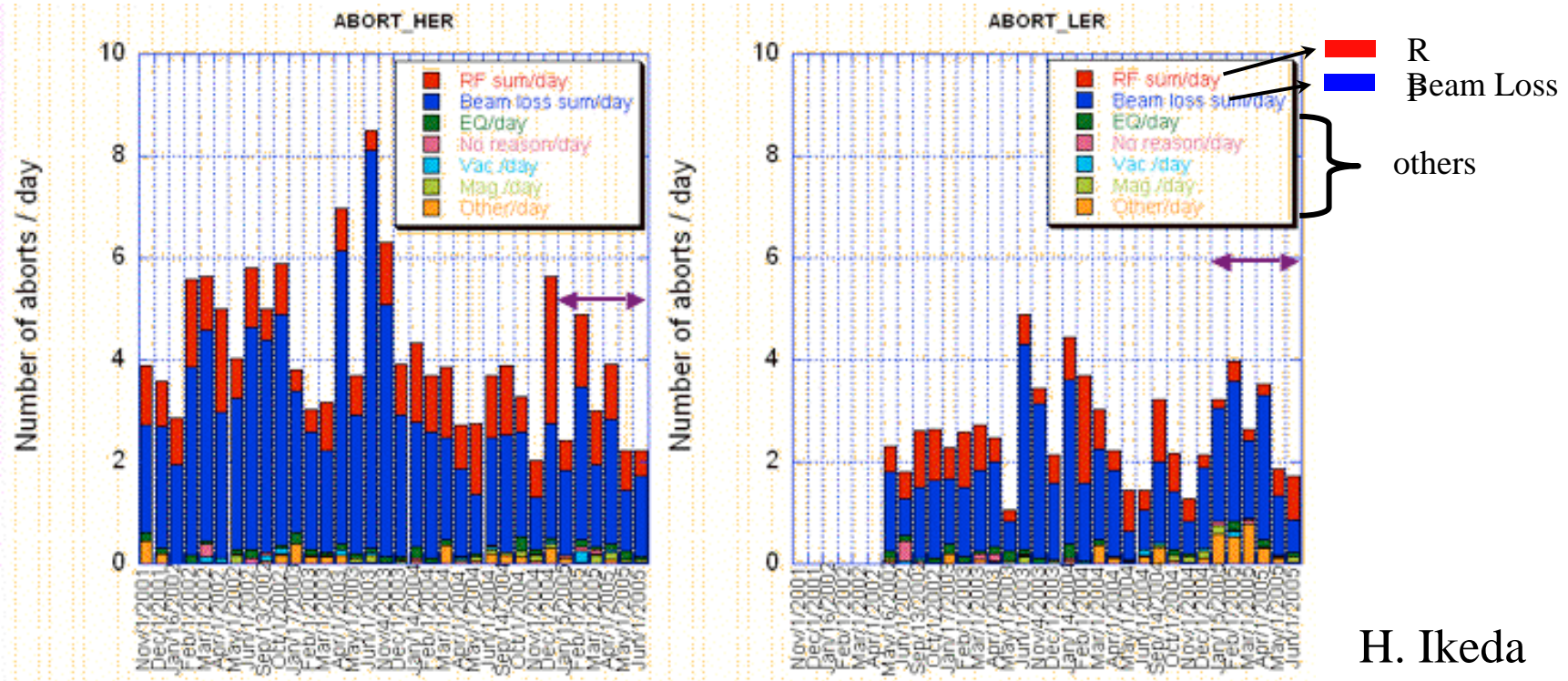
# *Design and achieved parameters*

	LER ARES	HER	
		ARES	SCC
Max. beam current (mA)	1860 (2600)	1340** (1100)	
Operating RF voltage (MV)	8 (5 ~ 10)	15 (10 ~ 18)	
RF voltage/cavity(MV): Operating Conditioned up to	0.4 0.55 (0.5)	0.34 0.475 (0.5)	1.36 >2.2 (1.5)
Total beam power (MW)	3.3 (4.5)	4.8 (4.0)	
Max. beam power/cavity (kW)	170 (225)	200 (170)	400** (250)
HOM power/cavity (kW)	6		13 (5)

( ) : design values

\*\* record of SC cavities

## Beam aborts (2001-2005, monthly)



H. Ikeda

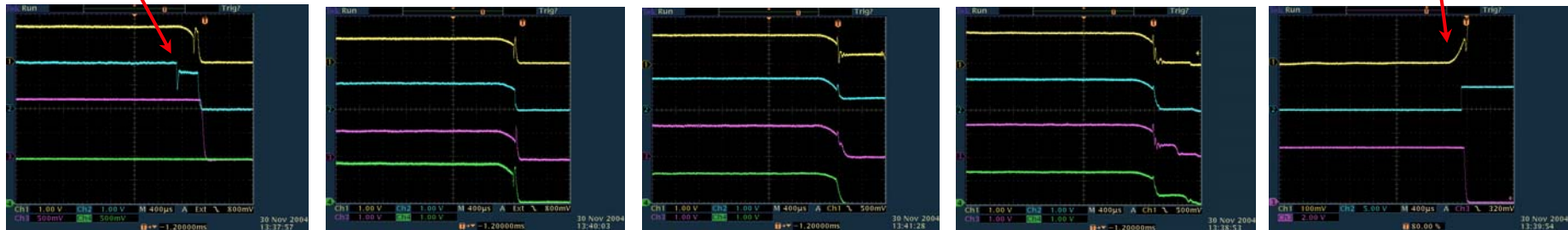
- We try to understand the cause of any beam abort.
- Statistics of frequency of beam aborts is routinely taken as above.
- Caused by beam loss (70%), RF (20%), others (<10%).
- Number of aborts in two rings caused by any RF reasons is about 1/day.

# RF Abort monitor

RF D04_1(ext. trig.)	RF D05_1(ext. trig.)	RF D10_1 (D10-A trig.)	RF D11_2 (D11-A trig.)	RF D11_1
D04-B cavity voltage D04-C cavity voltage HER DCCT LER DCCT	D05-A cavity voltage D05-B cavity voltage D05-C cavity voltage D04-A cavity voltage	D10-A Cavity voltage D10-B Cavity voltage D10-C Cavity voltage D10-D Cavity voltage	D11-A Cavity voltage D11-B Cavity voltage D11-C Cavity voltage D11-D Cavity voltage	HER Beam Phase HER BPA Req. HER Current (trig.) empty

D4-C trip

Beam phase



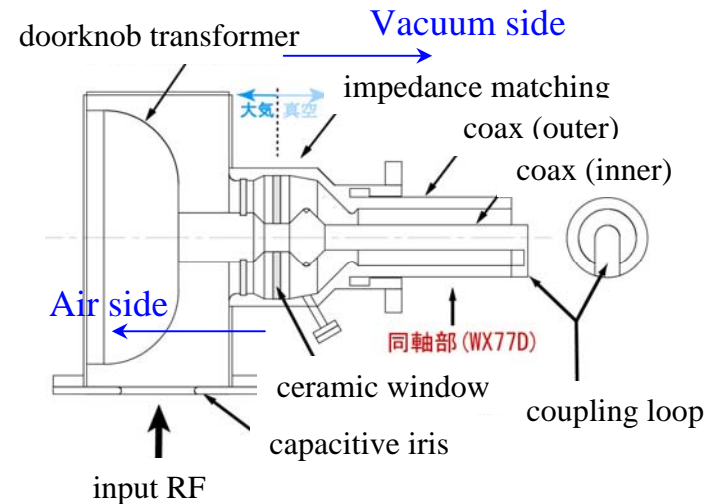
- Transient behavior of every RF station is monitored using oscilloscopes.
- Every beam abort triggers the oscilloscope and the data is automatically logged and displayed on the web so that the operator can judge the cause of abort: RF trips or other reasons? if RF trip, which unit?

## *Lessons we learned in operation*

- Arc sensor for input couplers
- Bad effects of beam aborts due to RF trips
- Zero mode and -1 mode oscillation

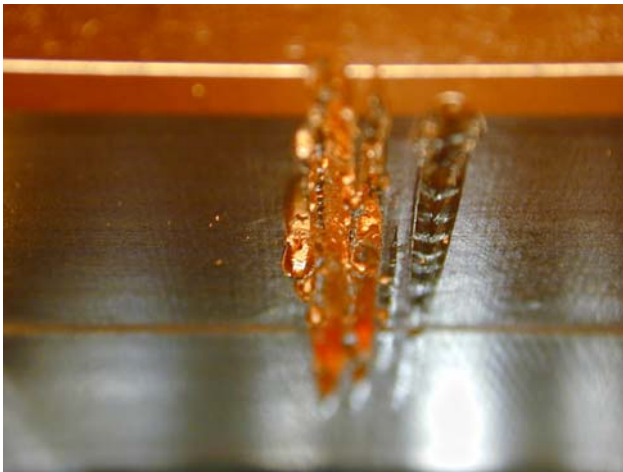
# Arc sensor for ARES input coupler

- Before 2000
  - An arc sensor was attached only on the vacuum side of ceramic window.
- Troubles
  - Doorknob transformer burned (Jan. 2000).
  - Ceramic window leaked due to discharge on the air side of the window (Nov. 2000).
  - Ceramic window leaked by circulating beam despite that the arc sensor switched off the RF (Oct. 2001).
- Measures taken
  - An arc sensor is added on the air side of the window.
  - Beam abort is triggered whenever any arc sensor works.
  - Since then no serious accident occurred at the input couplers.



# *Bad effects of RF trips*

- Unstable beam due to RF trip caused troubles (2001).
  - A large amount of radiation hit the Belle detector. (5 krad/shot worst case!)
  - Movable masks are damaged. Beam life is deteriorated.

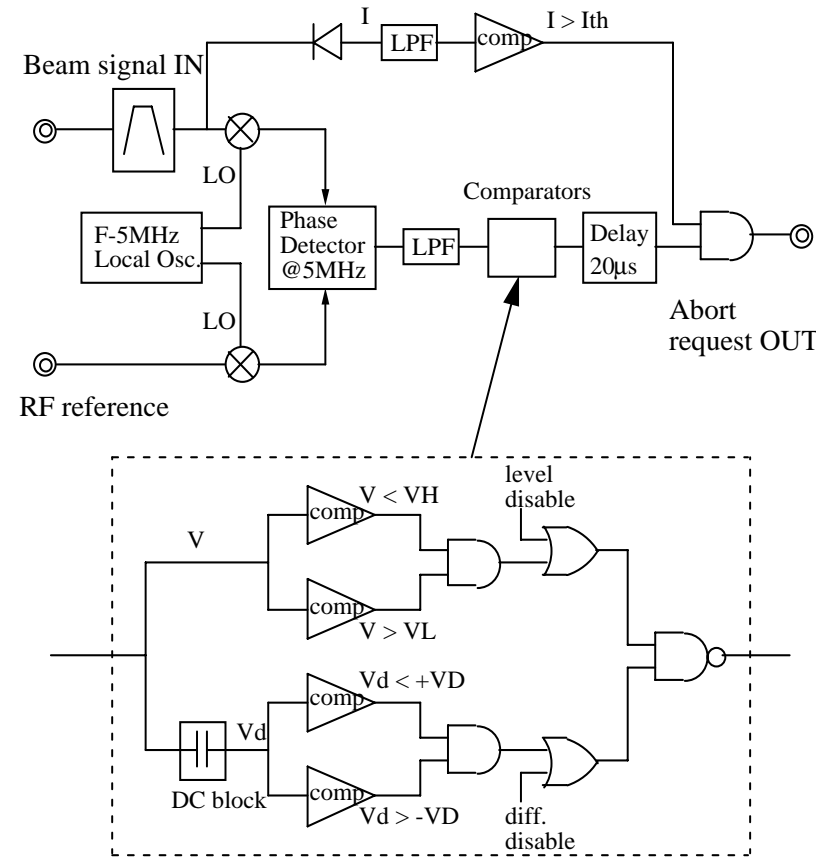
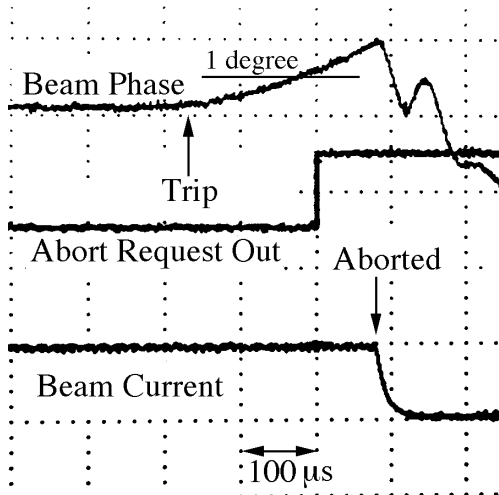


- Abort triggered by interlock system did not help all cases:
  - Some interlocks are not very fast.
  - RF field can become abnormal prior to any interlock work.
- Measures taken (2001~02):
  - Beam Phase Abort
  - Additional abort trigger by voltage drop and arc sensor
  - PIN diodes
  - Mask head changed from Cu to Ti.
- After 2002, no such bad effects was observed due to RF trips
  - Only one exception: misoperation of master oscillator could not be helped (phase change so fast).



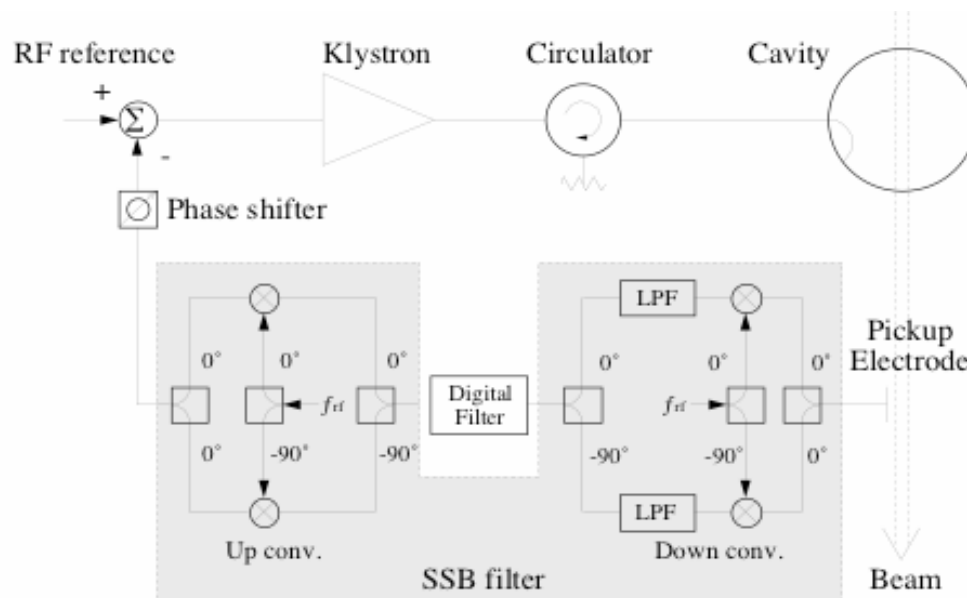
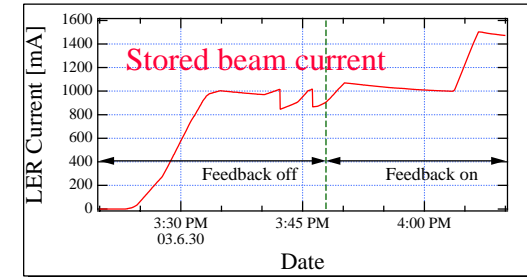
# Beam Phase Abort

- Relative phase between beam and reference RF is measured.
- Beam phase shift by 1 degree makes a trigger signal to the abort system.

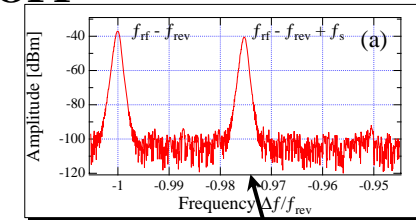


# The -1 mode feedback

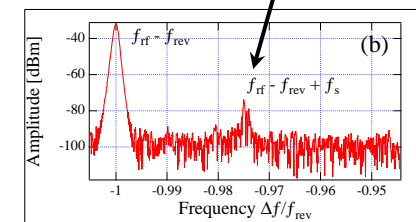
- Beam current was limited due to the -1 mode instability at 1 A in LER and 1.2 A in HER, much lower current than expected.
- The -1 mode digital feedback selectively reduces impedance at the driving frequency.
- After the -1 mode feedback was installed, the beam current could be successfully increased.



**FB OFF**



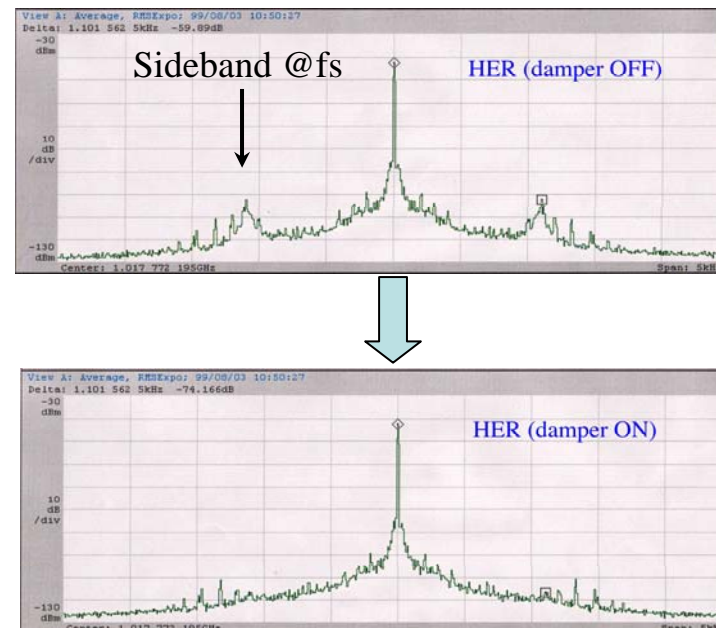
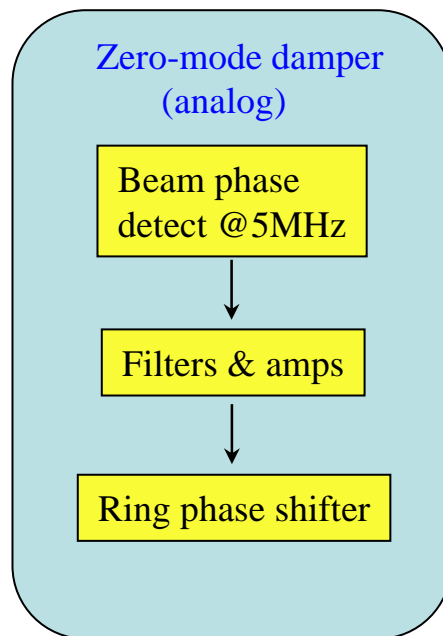
**FB ON**



-1 mode sideband

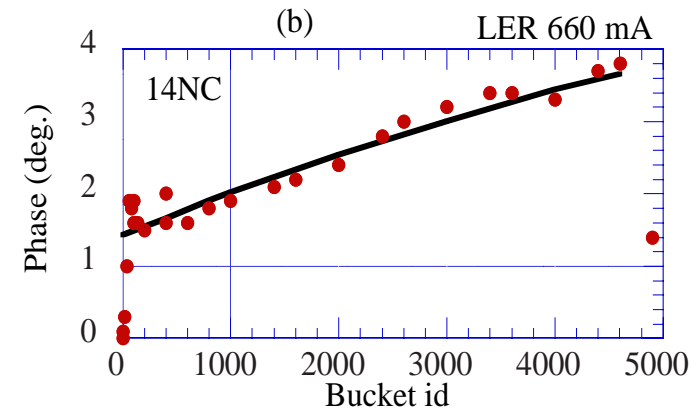
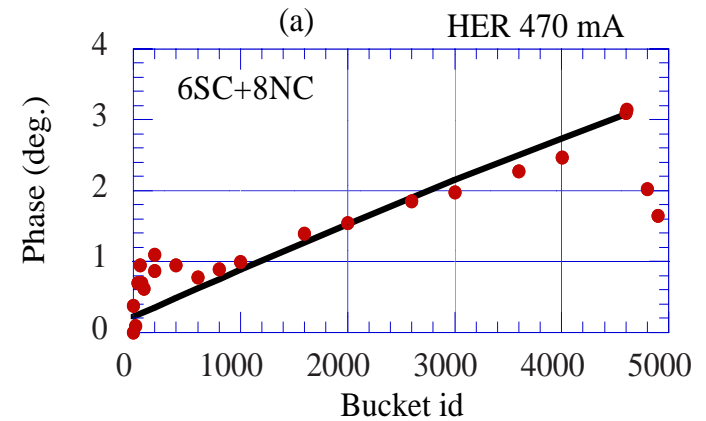
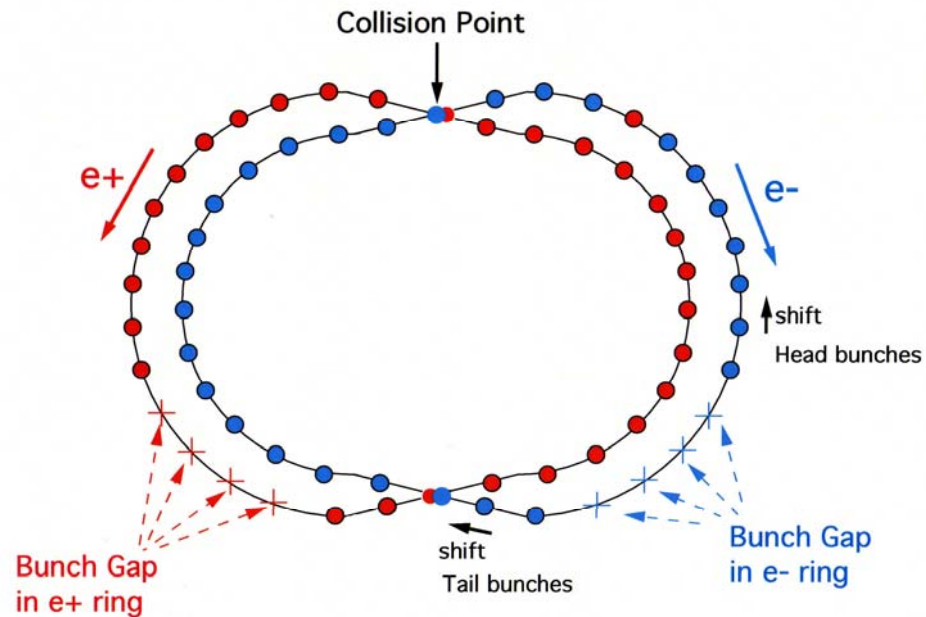
# Zero-mode oscillation

- At the beginning we observed zero-mode synchrotron oscillation even at a low beam current.
  - The amplitude was about 0.5 degree p-p.
  - It is probably caused by noise in the RF reference line system.
- The amplitude is reduced by 15dB by the zero-mode damper.



# Bunch-gap transient

- 5% of the ring is not filled with bunches (abort gap).
- Longitudinal position is modulated along the bunch train.



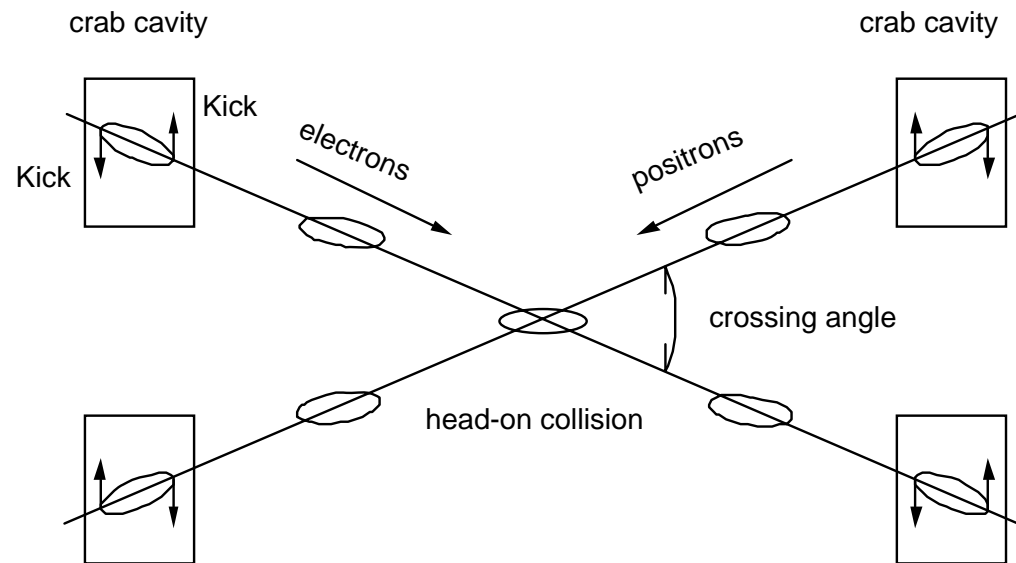
Phase modulation along the train  
(simulation and measurement).

# *Upgrade projects*

---

- **Crab crossing**
  - Superconducting crab cavities will be installed in KEKB next year to conduct crab-crossing experiment.
- **SuperKEKB**
  - Increase luminosity by 20~40 times.
  - Design report has been completed.
  - Letter Of Intent has been circulated.

# Crab crossing



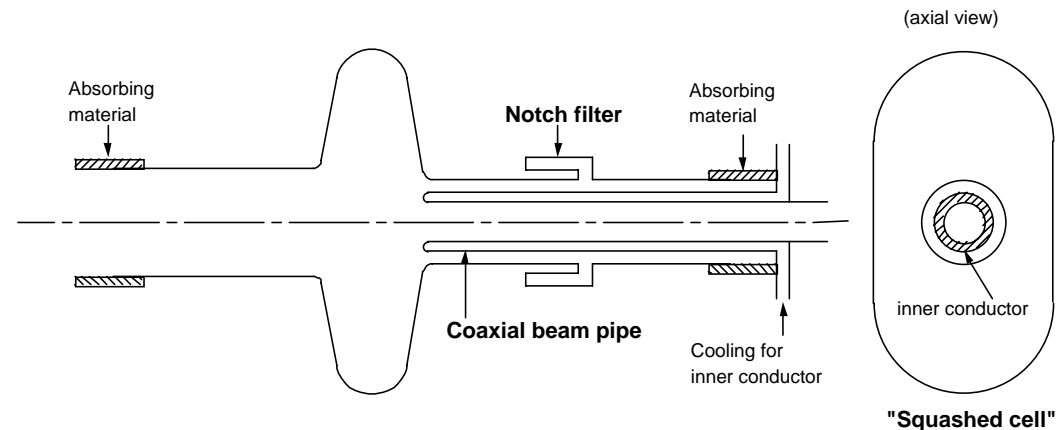
Palmer for LC (1988)

Oide and Yokoya for storage rings (1989)

Recent simulations showed significant increase of luminosity by several times with the crab-crossing.

# Crab cavity for KEKB

- Crab cavity for high current beam needs special damped structure.
  - The operating mode is not the lowest frequency mode.
  - Not only HOMs, but also the fundamental mode must be heavily-damped.
- The KEKB crab cavity has unique feature:
  - Squashed cell
  - Coaxial beam pipe + notch filter

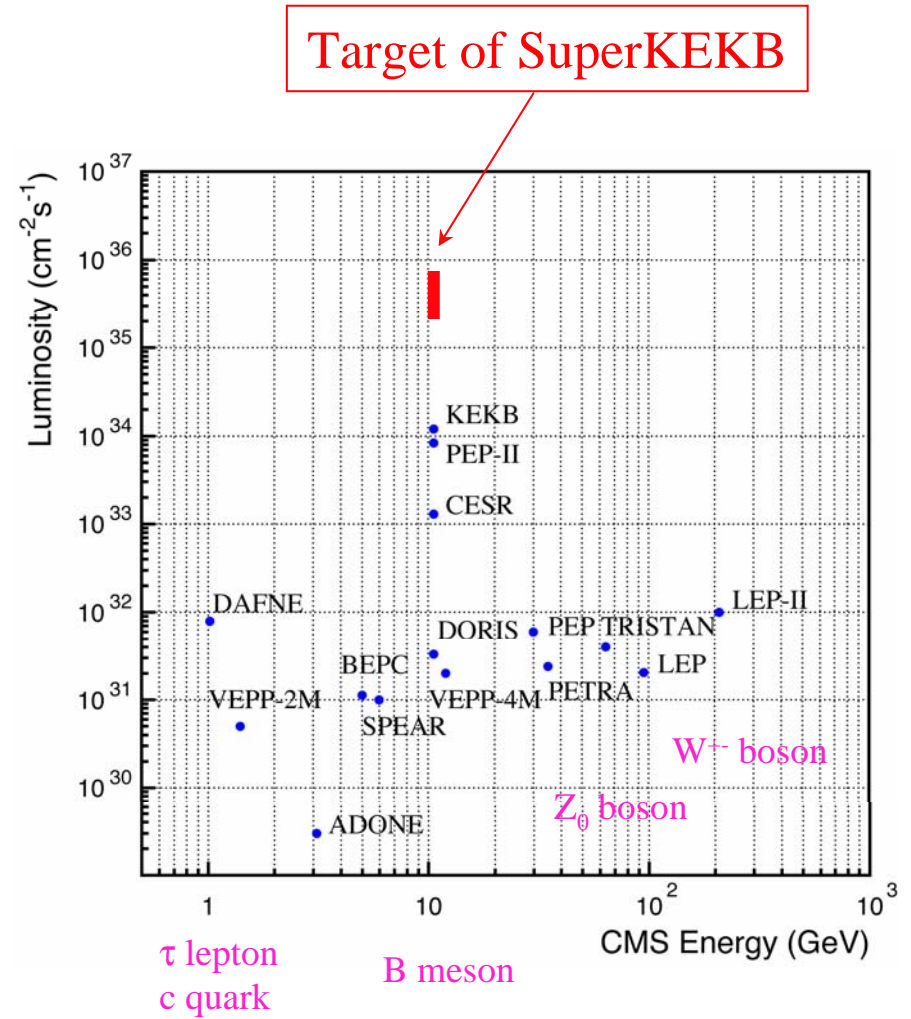
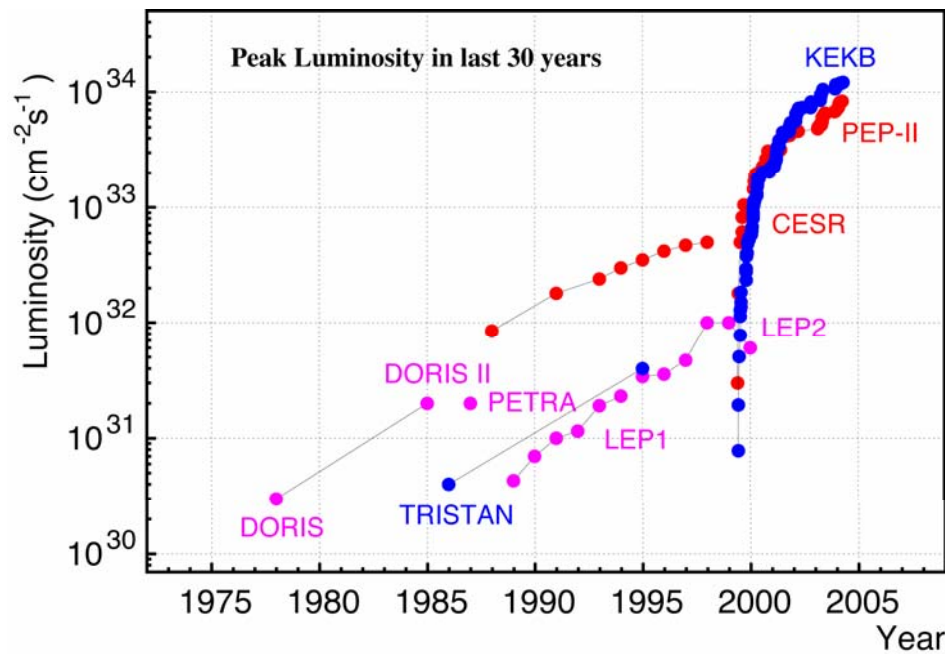


Squashed Crab cavity for B-factories

(K. Akai et al., Proc. B-factories, SLAC-400 p.181 (1992).)

Crabbing mode keeps high-Q value.  
All other modes are heavily-damped.

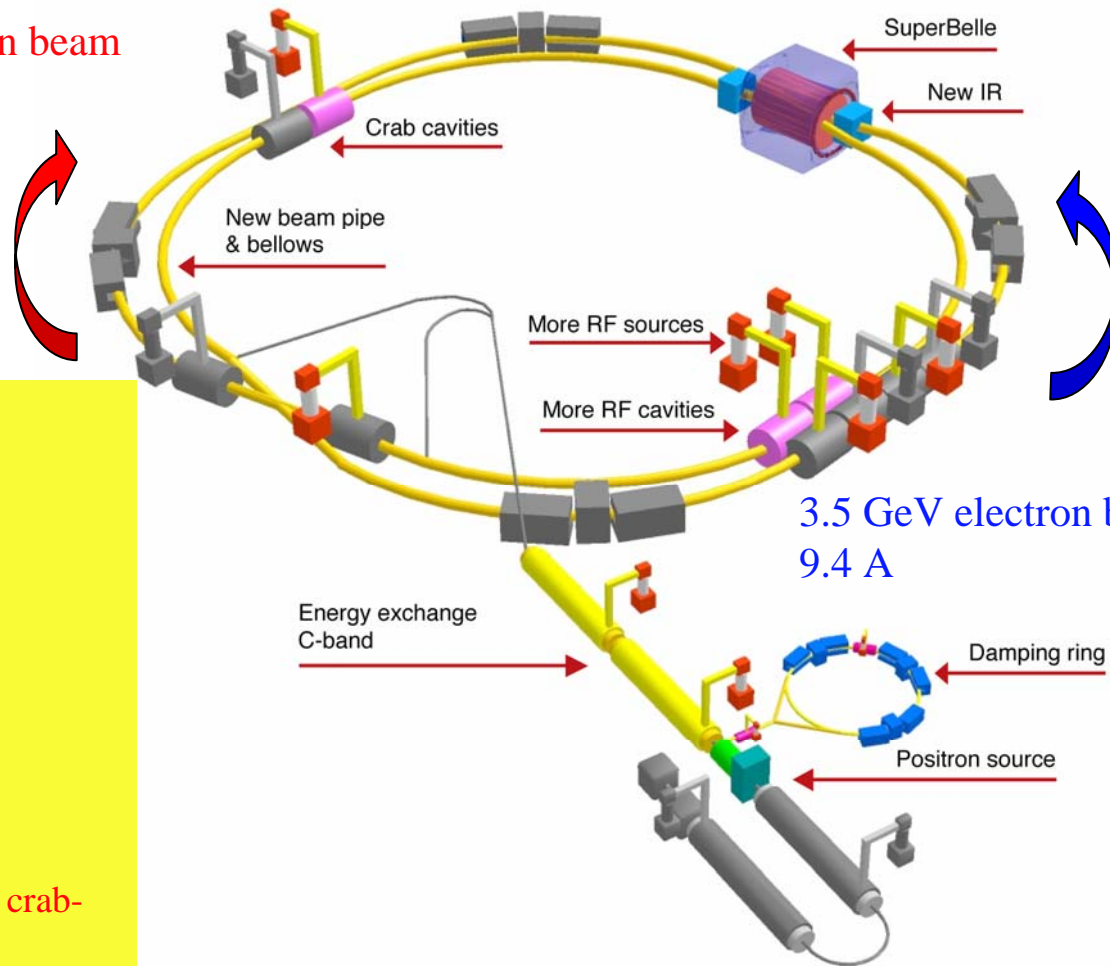
# Luminosity of $e^+e^-$ circular colliders





# Concept of SuperKEKB

8 GeV positron beam  
4.1 A



3.5 GeV electron beam  
9.4 A

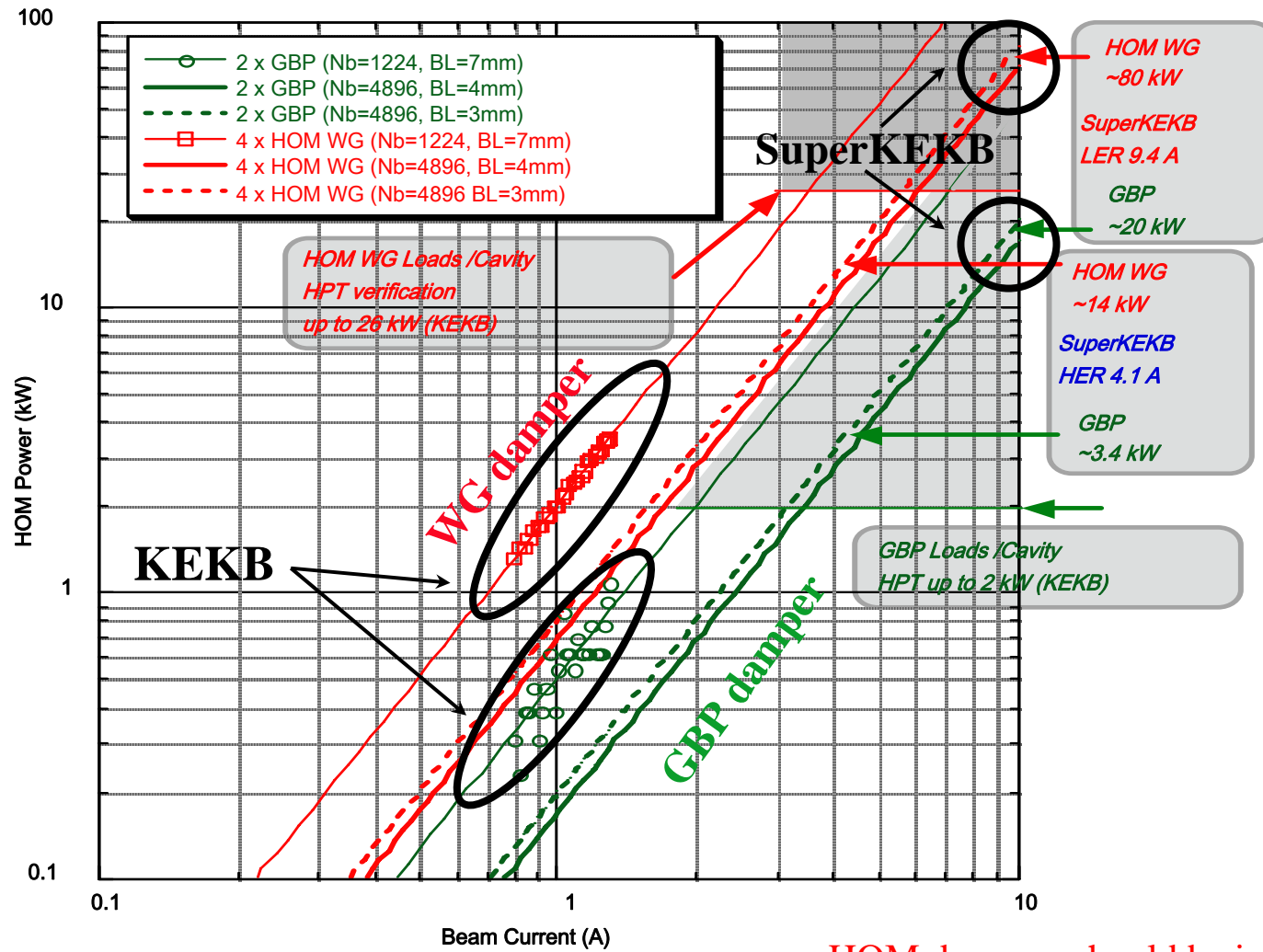
To get  $L = 4 \times 10^{35} / \text{cm}^2 \text{s}$ ,

- More beam current
  - LER/HER = 1.6A/1.3A → 9.6A/4.1A
- Squeeze  $\beta_y^*$ 
  - $\beta_y^* = 6\text{mm} \rightarrow 3\text{mm}$
  - $\sigma_z = 6\text{mm} \rightarrow 3\text{mm}$
- Beam-beam parameter
  - $\xi_y = 0.05 \rightarrow 0.14$  by adopting crab-crossing

# *Strategy for SuperKEKB-RF*

- 4 times large beam power
  - More than double RF stations are needed (24 → 56).
  - All ARES stations will be converted to (1 cavity) : (1 klystron).
- Modification of the ARES
  - Further increase the stored energy by changing the coupling between A- and S-cavities.
- Improve HOM dampers
  - 50~80 kW/cavity should be treated.
- Improve LLRF
  - May need to be converted to digital system.
  - Noise in the reference line should be reduced.
  - The -1 mode feedback system should be improved.
    - Even with the modification of ARES, the growth time of the -1 mode instability is as fast as 1 ms.
- Crab cavity for much higher beam current

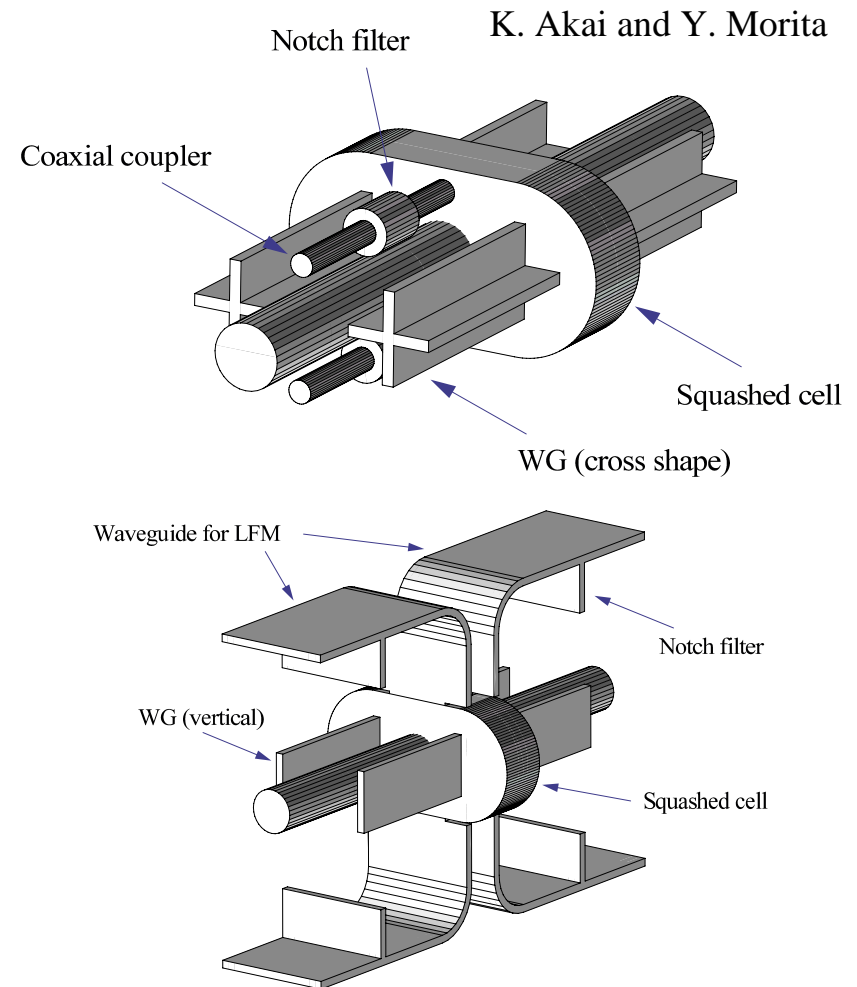
# HOM power of LER-ARES



HOM dampers should be improved.

# Crab cavity for SuperKEKB

- For SuperKEKB the crab crossing is adopted as a baseline design.
- Much higher beam current (10A)
  - Much heavier damping of HOM and the fundamental mode is needed.
  - Cure for a large amount of HOM power.
- We designed two types of new crab cavity for SuperKEKB.
  - Parasitic impedance is sufficiently reduced.
  - Loss factor is also reduced by less than half.



## *Summary*

- Continuous effort to improve stability of whole RF system has contributed to high performance of KEKB.
- Owing to high stored energy of cavities, requirements for LLRF is eased compared with conventional cavity system: for example, analog phase and amplitude feedback loops can work satisfactory.
- For upgrading to SuperKEKB, the LLRF may need to be changed including converting to more sophisticated digital system. We expect this LLRF workshop is a good chance to start for future improvements.