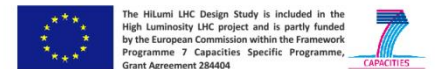


# Magnetic measurements and analysis on 11-T models at CERN



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O. Dunkel, S. Russenschuck, G. Willering, J. Feuvrier  
22<sup>nd</sup> September 2015



# Outline

- MM systems
  - ambient temperature tests
  - cryogenic temperature tests
- MM test strategy
- Tested magnets
- Results
  - TF
  - Multipoles
  - Comparison with ROXIE model
  - Cold/Warm correlation
  - Inverse analysis
  - Ramp-rate dependency
- Conclusions

# Measurement system 300 K

- Motor + encoder + slip-ring unit (MRU)
- Fast Digital Integrator (FDI)
- FuG low voltage power supply (40 V, 20 A)
- DCCT Hitec MACC-plus
- Search coil shafts (radius 22 mm, length 1.2 m)
- Flexible software Framework for Magnetic Measurements (FFMM)

Number of turns	(-)	256
Inner width	(mm)	13.41
Inner length	(mm)	1195.6
Groove thickness	(mm)	1.4
Magnetic surface	(m <sup>2</sup> )	3.37
Center radius	(mm)	21.33

A measurement is an average over 1.2 m

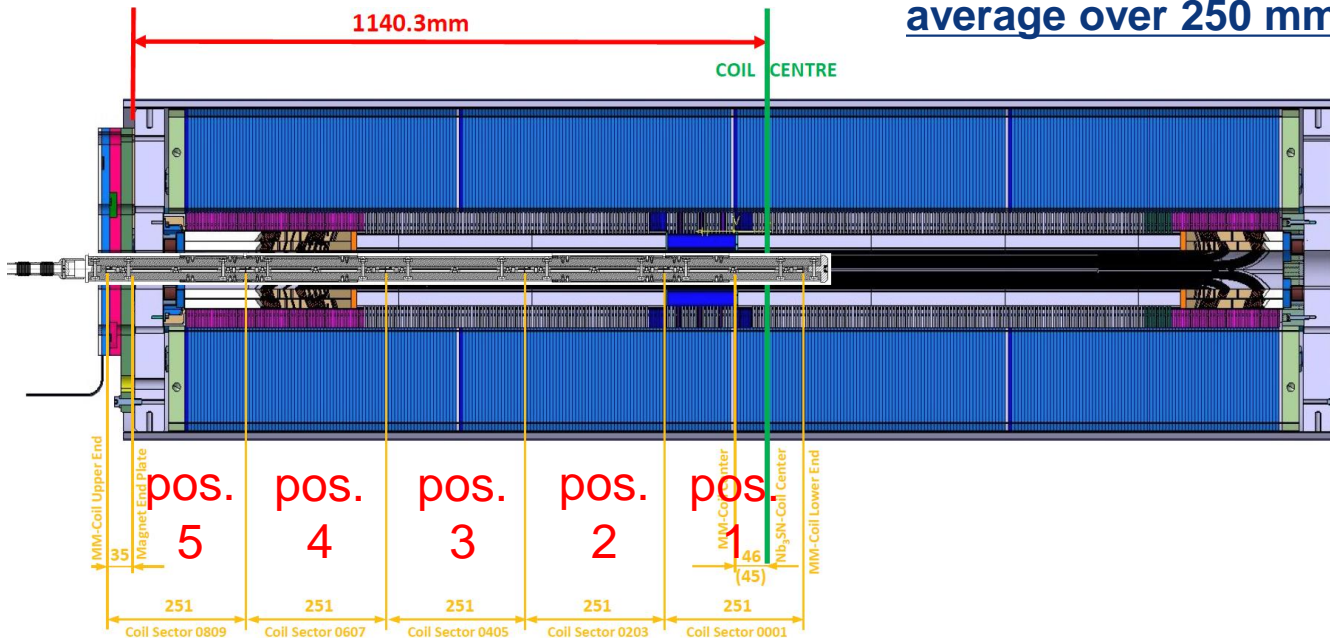


# Measurement system 1.9 K

- Flexible software Framework for Magnetic Measurements (FFMM)
- Fast Digital Integrators (FDI)
- Motor + encoder + slip-ring unit (MRU)
- Vertical rotating shaft in liquid He

Number of turns	(-)	150
Inner width	(mm)	6.43
Inner length	(mm)	250.00
Groove thickness	(mm)	0.80
Magnetic surface	(m <sup>2</sup> )	0.28197
Center radius	(mm)	18.91

A measurement is an average over 250 mm

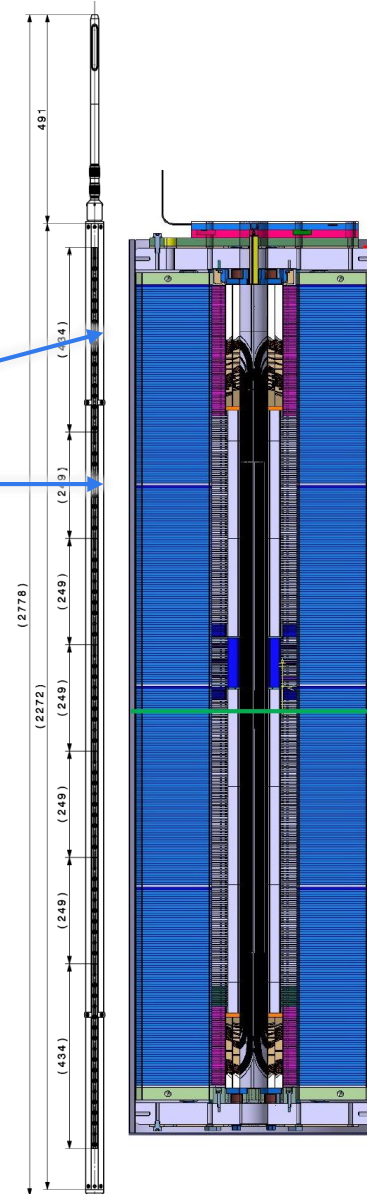


# Measurement system 1.9 K

- Flexible software Framework for Magnetic Measurements (FFMM)
- Fast Digital Integrators (FDI)
- Motor + encoder + slip-ring unit (MRU)
- Vertical rotating shaft in liquid He

Number of turns	-	36	36
Inner width	mm	10.3	10.3
Inner length	mm	431.5	246.5
Groove thickness	mm	0.57	0.57
Magnetic surface	m <sup>2</sup>	0.17	0.10
Center radius	mm	21.5	21.5

A measurement is an average over 250 mm



# MM test strategy

## 1) At ambient temperature

- Collared coil (CC) at  $\pm 20$  A
- Cold mass (CM) at  $\pm 20$  A

## 2) At cryogenic temperature

- CM with the following powering cycles
  - Stair-step cycle preceded by a quench
  - Machine cycle preceded by a quench
  - Ramp-rate study
- Additional tests
  - Variable minimum current at 1.9 K and 4.5 K on MBHSP101
  - Long plateau (10 h) at nominal on MBHSP102

## 3) At ambient temperature

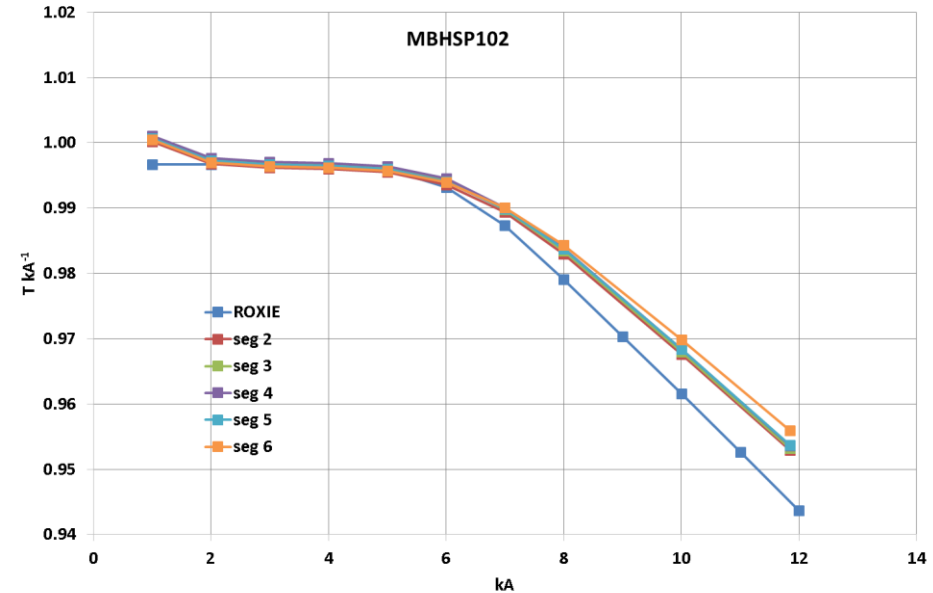
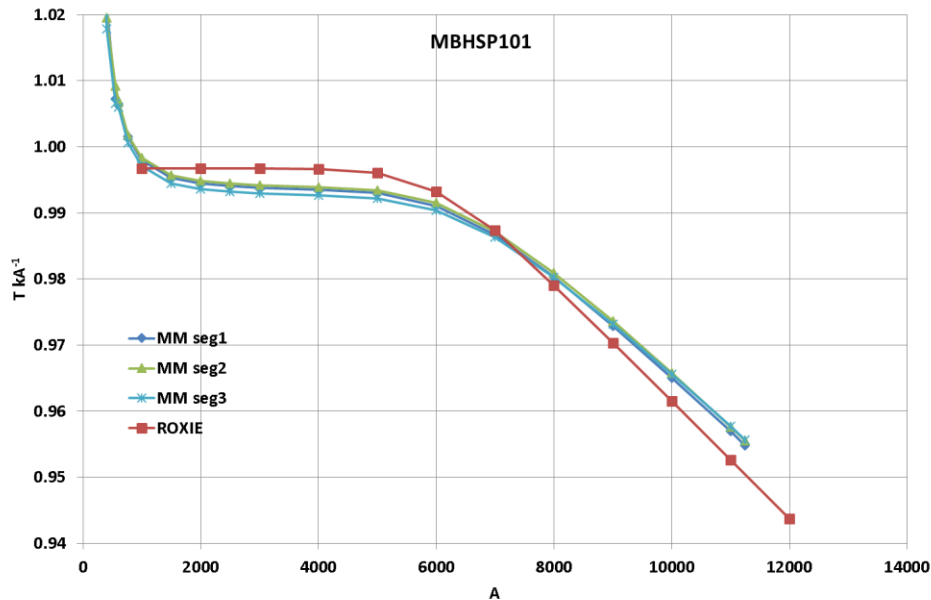
- CM at  $\pm 20$  A

# Tested magnets

## 2-m models with single aperture

- MBHSP101
  - CC and CM at 300 K
  - CM at 1.9 K
  - CM at 300 K
- MBHSP102
  - CC and CM at 300 K
  - CM at 1.9 K
  - CM at 300 K
- MBHSP103
  - CC and CM at 300 K

# Transfer function



- Measurements and 2-D ROXIE model in agreement for geometric TF
  - -30 units on MBHSP101 probably due to shaft calibration
  - Perfect agreement on MBSP102
- Saturation overestimated by the model
  - +55 units measured on both magnet models



# Transfer function

Possible sources of error:

## Iron properties

Using data from LHC production the discrepancy decrease by 20 units (from ~70 to ~50 units)

## Packing factor of the yoke laminations

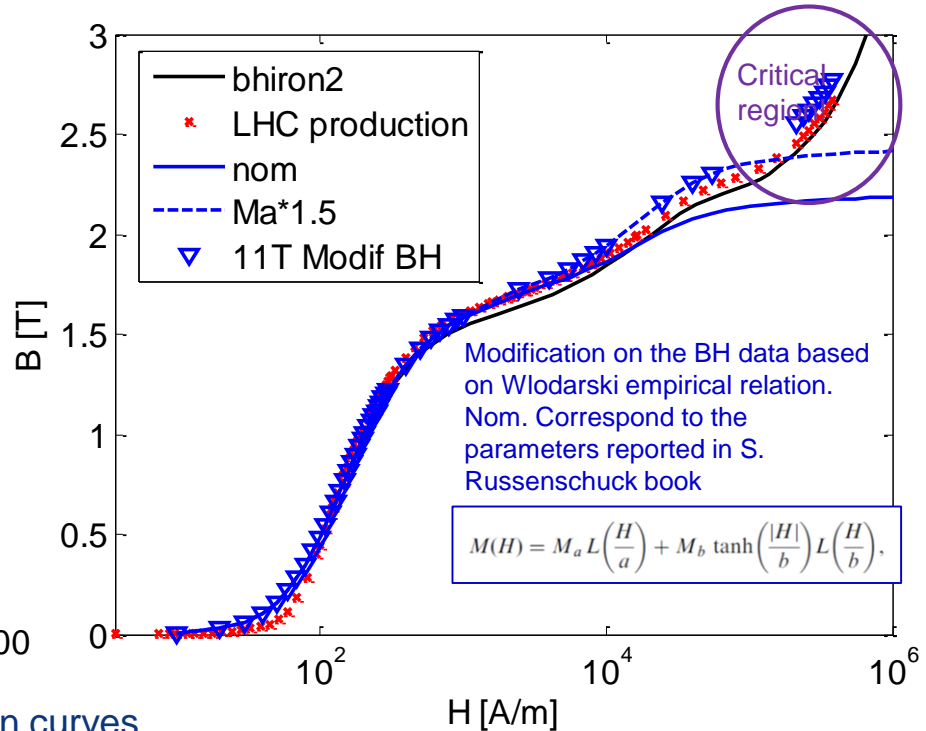
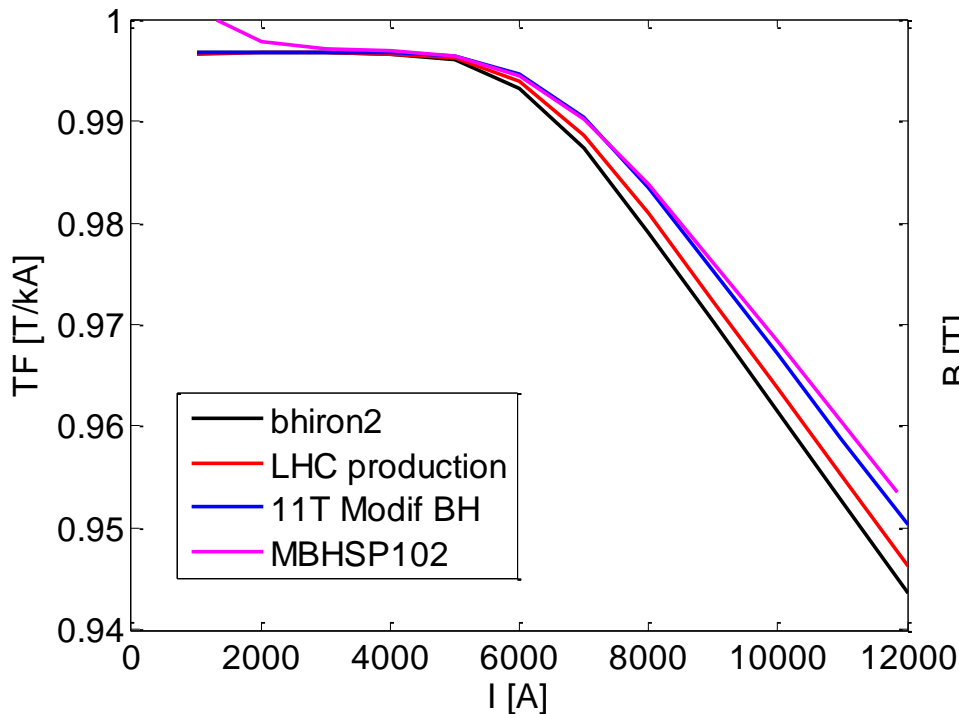
Its effect is up to ~15 units

## Geometric

Rather big displacements needed to explain 50 units (350  $\mu\text{m}$  smaller coil gives ~15 units)

# Transfer function

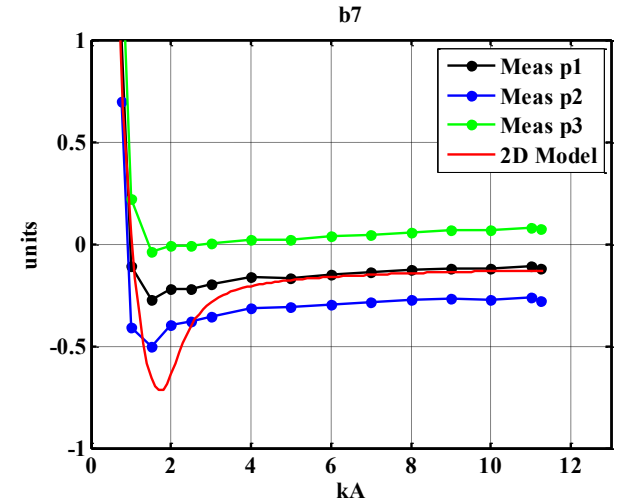
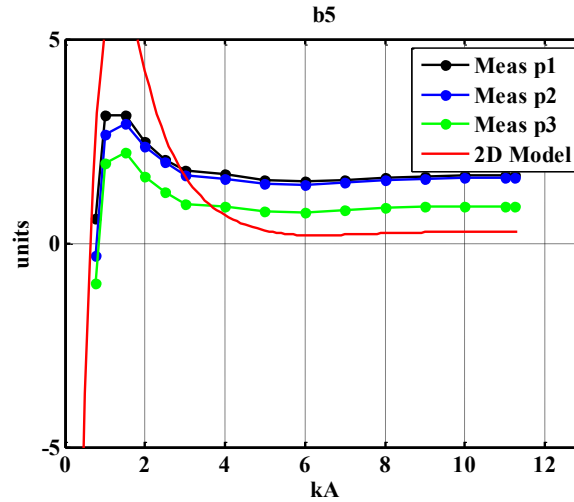
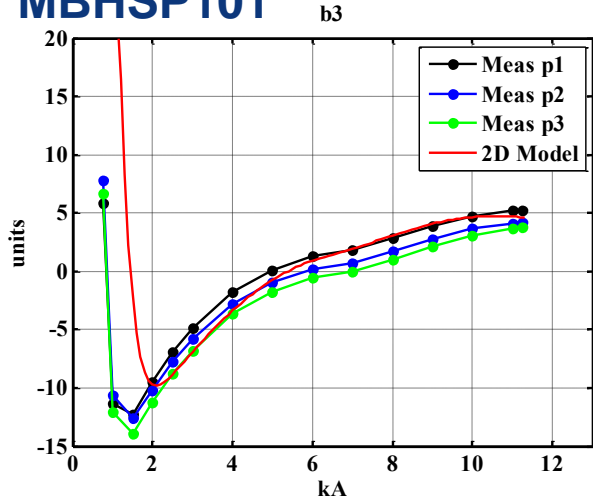
- The main source of error is the magnetic properties of the iron:
  - Discrepancy ~ **80 units** using ROXIE bhdata2
  - Discrepancy ~ **55 units** using LHC production data
  - Discrepancy ~ **15 units** using a modified bh data based on [1]



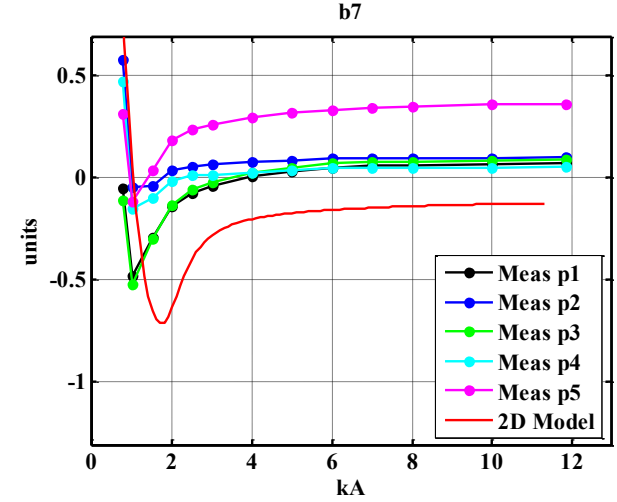
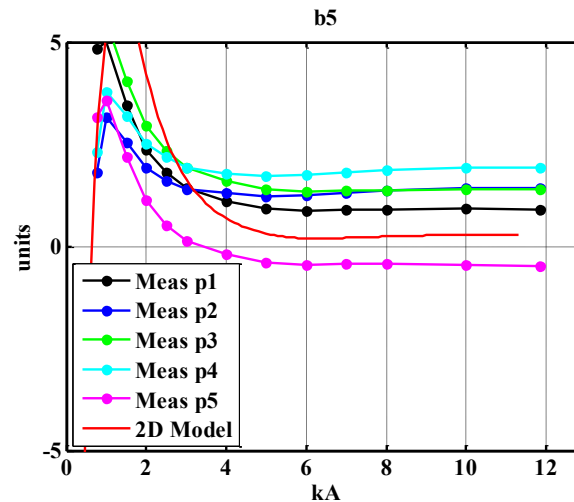
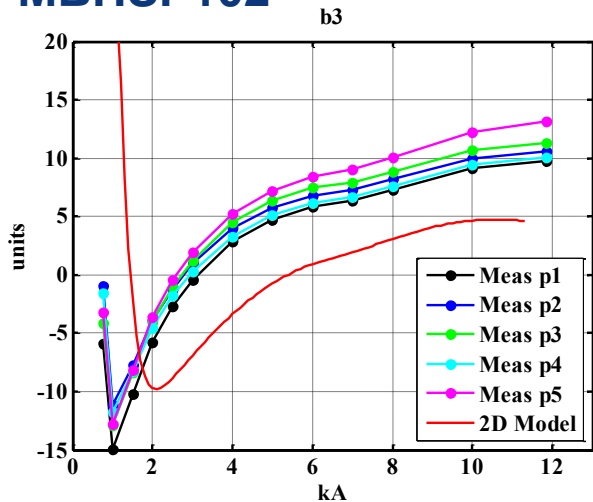
[1] Z. Wlodarki. Analytical description of magnetization curves

# Allowed multipoles

## MBHSP101



## MBHSP102



# Geometric multipoles

## MBHSP101

random block displacements of 60  $\mu\text{m}$

	pos 1		pos 2		pos 3				tolerances	
TF (T kA <sup>-1</sup> )	0.9930		0.9934		0.9922		6.23 units		-	
n	bn	an	bn	an	bn	an	$\sigma$ bn	$\sigma$ an	$\sigma$ bn	$\sigma$ an
2	0.86	5.47	-0.59	5.11	-2.14	4.66	1.50	0.41	1.70	1.82
3	6.35	-1.21	5.25	-0.78	4.60	-1.75	0.88	0.49	1.08	1.18
4	0.30	1.72	-0.51	0.99	-0.19	-0.26	0.41	1.00	0.62	0.67
5	1.49	0.01	1.43	0.43	0.72	0.48	0.43	0.26	0.35	0.39
6	0.01	0.49	-0.15	0.70	0.04	0.49	0.10	0.12	0.17	0.20
7	-0.06	-0.19	-0.22	-0.07	0.13	0.11	0.18	0.15	0.10	0.10
8	-0.01	0.10	-0.02	0.01	0.03	-0.01	0.03	0.06	0.06	0.05
9	0.89	-0.20	0.85	-0.32	0.80	-0.33	0.04	0.07	0.03	0.02
10	0.00	0.00	-0.01	0.00	-0.02	0.01	0.01	0.00	0.01	0.01
11	0.37	-0.06	0.37	-0.12	0.39	-0.14	0.01	0.05	0.01	0.01

Reference radius 17 mm

# Cold/warm correlation

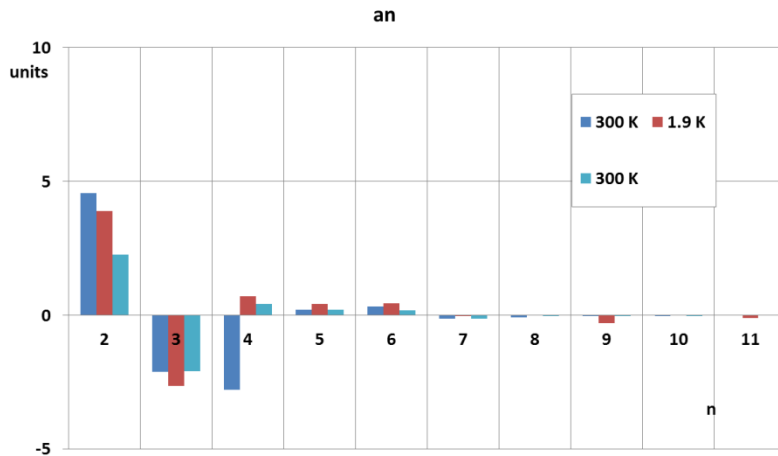
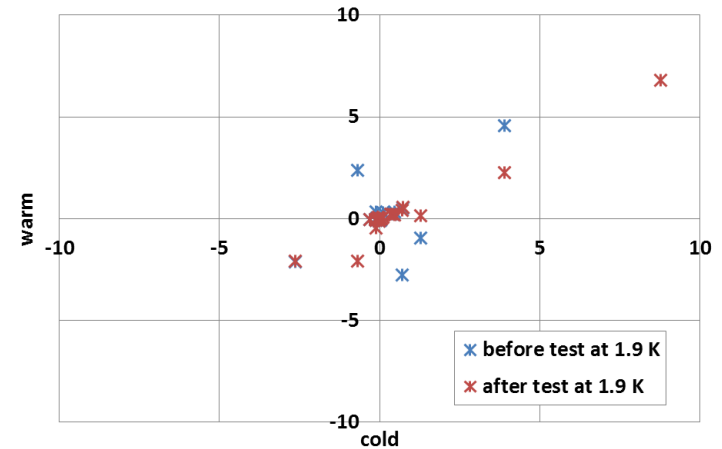
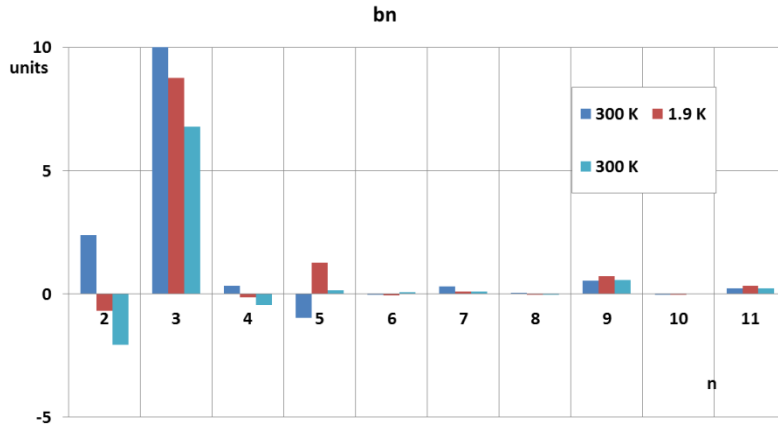
## MBHSP101 half magnet

	half magnet			half magnet			half magnet	
Temp.	300 K before cold tests			1.9 K			300 K after cold tests	
TF	0.735			0.747			0.736	
n	bn	an		bn	an		bn	an
2	2.38	4.57		-0.68	3.89		-2.07	2.28
3	10.56	-2.12		8.77	-2.63		6.80	-2.08
4	0.33	-2.78		-0.12	0.70		-0.44	0.43
5	-0.96	0.22		1.28	0.43		0.15	0.22
6	-0.03	0.33		-0.05	0.46		0.07	0.18
7	0.30	-0.12		0.10	-0.01		0.09	-0.12
8	0.05	-0.08		-0.02	0.02		-0.01	-0.01
9	0.55	-0.02		0.72	-0.30		0.57	-0.03
10	0.00	0.00		-0.01	0.01		0.01	-0.02
11	0.23	0.02		0.33	-0.09		0.24	0.02

Reference radius 17 mm

# Cold/warm correlation

## MBHSP101 half magnet



- Changes on multipoles before/after test at cold
- Better cold/warm correlation with measurements at warm **after** cold tests

Reference radius 17 mm

# Geometric multipoles

## MBHSP102 central field

	300 K before tests at 1.9 K		1.9 K at 5 kA on three central segments						300 K after tests at 1.9 K	
	1.2 m		0.250 m		0.250 m		0.250 m		1.2 m	
n	bn	an	bn	an	bn	an	bn	an	bn	an
2	0.33	6.76	1.75	2.73	1.22	3.56	0.69	3.67	0.21	7.51
3	9.50	-0.84	11.32	-1.78	11.82	-1.38	10.75	0.25	10.05	-1.12
4	0.24	1.28	0.54	0.19	0.32	-0.33	-0.29	-0.20	0.23	1.50
5	1.56	-0.02	1.17	-0.59	1.39	0.20	1.65	0.58	1.42	0.01
6	0.00	0.03	-0.01	0.13	0.19	-0.42	0.09	-0.24	0.01	0.05
7	0.16	-0.02	0.16	-0.22	0.10	-0.07	0.12	-0.06	0.18	-0.01
8	0.08	0.03	0.03	-0.04	0.05	-0.09	0.03	0.05	0.05	0.03
9	0.83	0.00	0.63	-0.13	0.64	0.02	0.62	0.22	0.83	-0.02
10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
11	0.40	0.02	0.22	-0.04	0.19	0.05	0.17	0.16	0.40	0.02
12	-0.06	0.01	-0.03	0.06	-0.06	0.04	-0.07	0.02	-0.01	0.01
13	-0.10	0.00	-0.11	-0.01	-0.11	0.00	-0.11	0.00	-0.09	0.00
14	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.00
15	-0.02	0.00	-0.02	0.00	-0.02	0.00	-0.02	-0.01	-0.02	0.00

Reference radius 17 mm

# Geometric multipoles

## MBHSP102 integral field

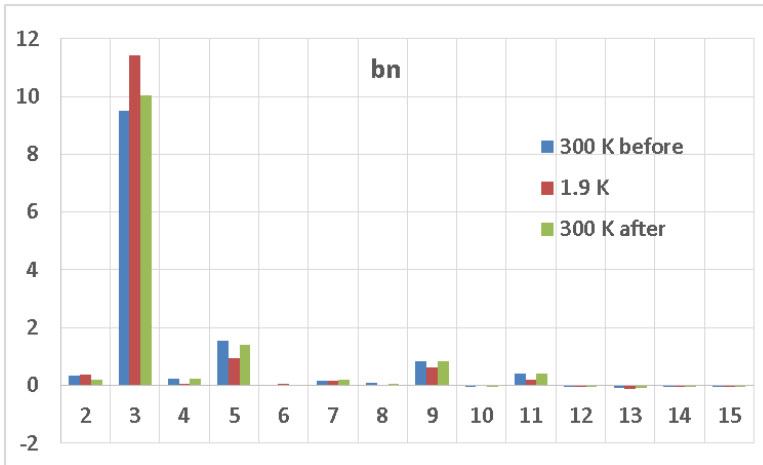
n	300 K before tests at 1.9 K		1.9 K		300 K after tests at 1.9 K	
	bn	an	bn	an	bn	an
2	0.41	3.23	0.51	2.33	0.83	4.15
3	14.20	-1.81	14.54	-1.02	14.26	-1.80
4	0.39	0.75	0.03	0.69	0.34	1.11
5	3.13	0.50	1.69	0.33	3.36	0.39
6	-0.06	-0.03	0.06	-0.07	-0.09	0.06
7	0.07	0.06	0.22	0.06	0.02	0.10
8	0.07	0.00	0.02	0.00	0.07	-0.02
9	0.70	0.00	0.63	0.05	0.71	-0.02
10	-0.01	-0.01	0.00	0.00	0.01	0.01
11	0.35	0.05	0.22	0.07	0.34	0.05
12	-0.06	0.00	-0.02	0.01	-0.02	0.00
13	-0.09	0.00	-0.11	0.00	-0.09	0.00
14	0.00	0.01	0.00	0.00	0.00	0.01
15	-0.02	0.00	-0.02	0.00	-0.02	0.00

Reference radius 17 mm

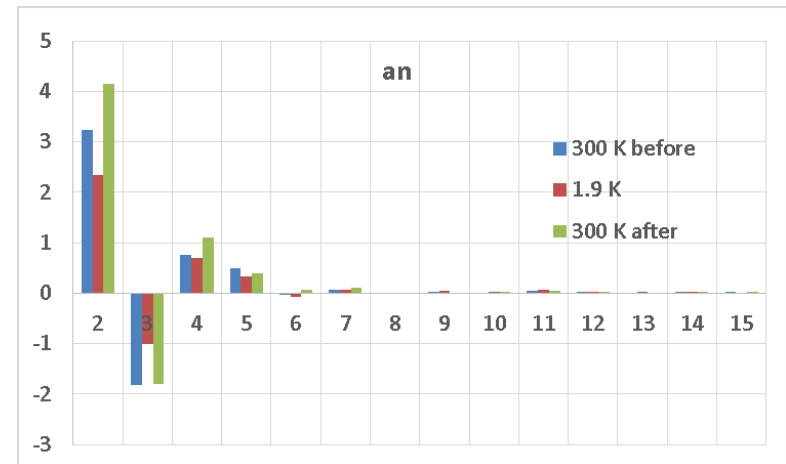
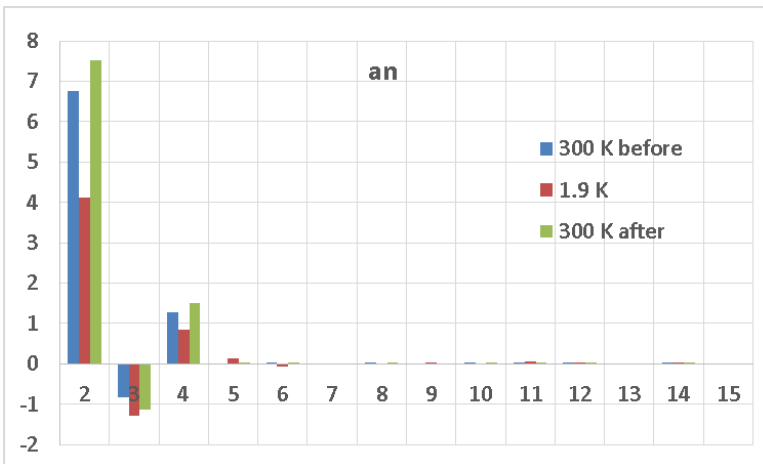
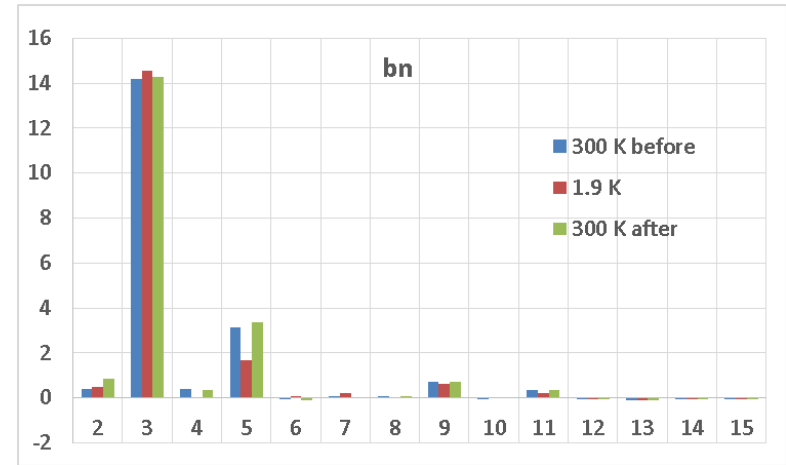


# Cold/warm correlation MBHSP102

## Central field



## Integral field



- No changes on multipoles before/after test at 1.9 K

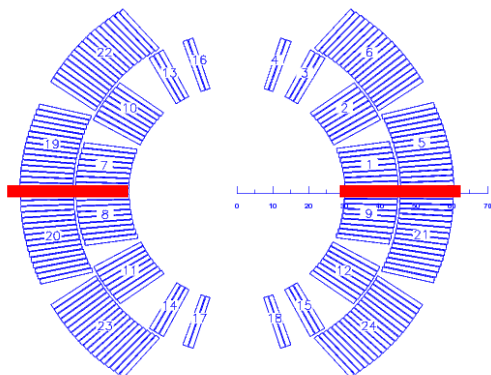
# Inverse Analysis

MBHSP101* (mid plane 125 um off)		After collaring	After shell welding	1.9K 5 kA	1.9K $I_{nom}$
b3			7.00	5.25	5.25
b5			0.14	1.43	1.43
b7			0.18	-0.22	-0.22
b9			0.76	0.85	0.85

MBHSP102 (mid plane OK)		After collaring	After shell welding	1.9K 5 kA	1.9K $I_{nom}$
b3		1.71	9.50	11.82	11.82
b5		2.24	1.56	1.39	1.39
b7		0.11	0.16	0.10	0.10
b9		0.88	0.83	0.64	0.64

\*  $I_{nom}$  11.25 instead of 11.85

- Shift on  $b_3$  of 6.5 units between the first and second model.
- The main difference among them is the mid-plane shim:
  - MBHSP101 : 250  $\mu\text{m}$  excess (0.125  $\mu\text{m}$  per coil)
  - MBHSP102 : nominal
- ROXIE-ANSYS interface to evaluate the impact of the actual coil geometry on the harmonics.

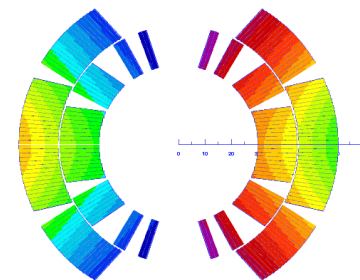
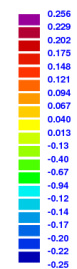


ANSYS  
displacements

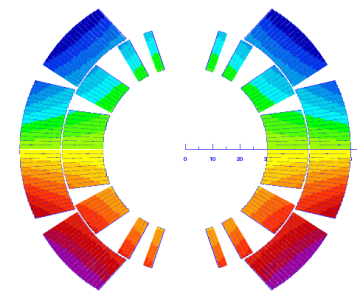
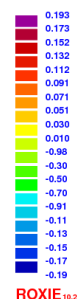
Apply displacement  
in ROXIE strands

Study impact of the  
displacements on  
field quality in ROXIE

ANSYS x-disp (mm)



ANSYS y-disp (mm)



# MBHSP101

- reasonable for b3
- Still a discrepancy on b5

<b>MBHSP101*</b> <b>(mid plane 125 um off)</b>		<b>After collaring</b>	<b>After shell welding</b>	<b>1.9K 5 kA</b>	<b>1.9K I<sub>nom</sub></b>
<b>b3</b>			7.00	5.25	5.25
<b>b5</b>			0.14	1.43	1.43
<b>b7</b>			0.18	-0.22	-0.22
<b>b9</b>			0.76	0.85	0.85

\* Inom 11.25 instead of 11.85

	<b>ROXIE</b>		<b>ROXIE + ANSYS</b>		<b>ROXIE</b>		<b>ROXIE + ANSYS</b>	
<b>Midplane 125 um off</b>	<b>After collaring</b>	<b>After shell welding</b>	<b>After collaring</b>	<b>After shell welding</b>	<b>1.9 K 5 kA</b>	<b>1.9 K Inom</b>	<b>1.9K 5 kA</b>	<b>1.9K I<sub>nom</sub></b>
<b>b3</b>	-5.58	2.57			2.55	1.79		5.04
<b>b5</b>	-1.41	-1.45			-1.49	-1.25		-0.78
<b>b7</b>	-0.64	-0.50			-0.52	-0.55		-0.21
<b>b9</b>	1.00	0.42			0.82	0.87		0.81

# MBHSP102

- reasonable for b3
- Still a discrepancy on b5

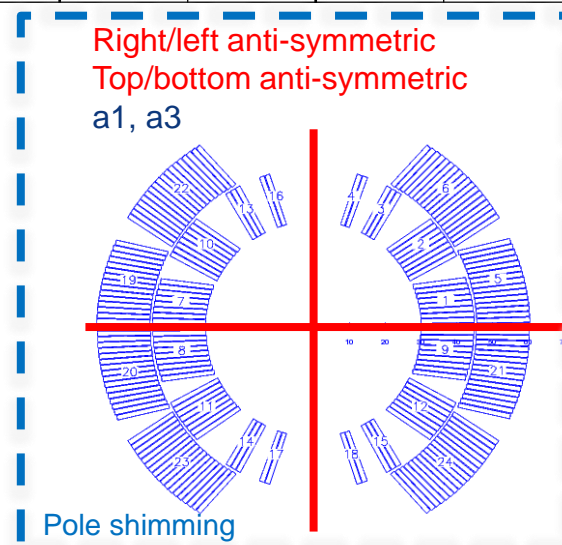
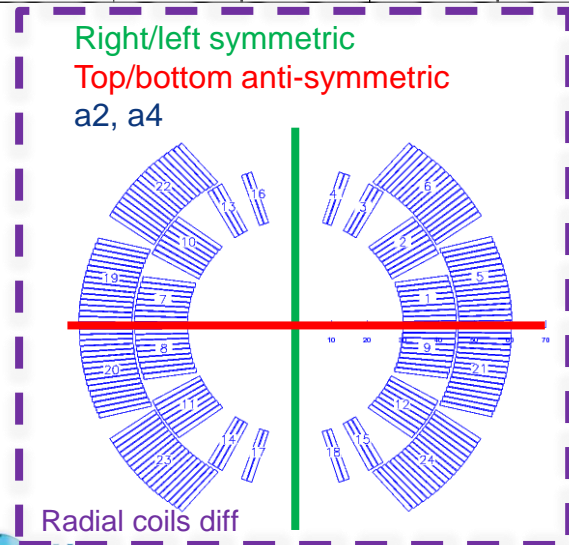
<b>MBHSP102 (mid plane OK)</b>	RT	After collaring	After shell welding	1.9K 5 kA	1.9K I <sub>nom</sub>
b3		1.71	9.50	11.82	11.82
b5		2.24	1.56	1.39	1.39
b7		0.11	0.16	0.10	0.10
b9		0.88	0.83	0.64	0.64

	ROXIE		ROXIE + ANSYS		ROXIE		ROXIE + ANSYS	
<b>Midplane OK</b>	After collaring	After shell welding	After collaring	After shell welding	1.9 K 5 kA	1.9 K I <sub>nom</sub>	1.9K 5 kA	1.9K I <sub>nom</sub>
b3	-0.40	6.76			6.77	6.22		12.70
b5	0.49	0.08			0.06	0.38		-0.05
b7	-0.12	-0.09			-0.10	-0.10		0.04
b9	1.11	0.89			0.91	0.96		0.84

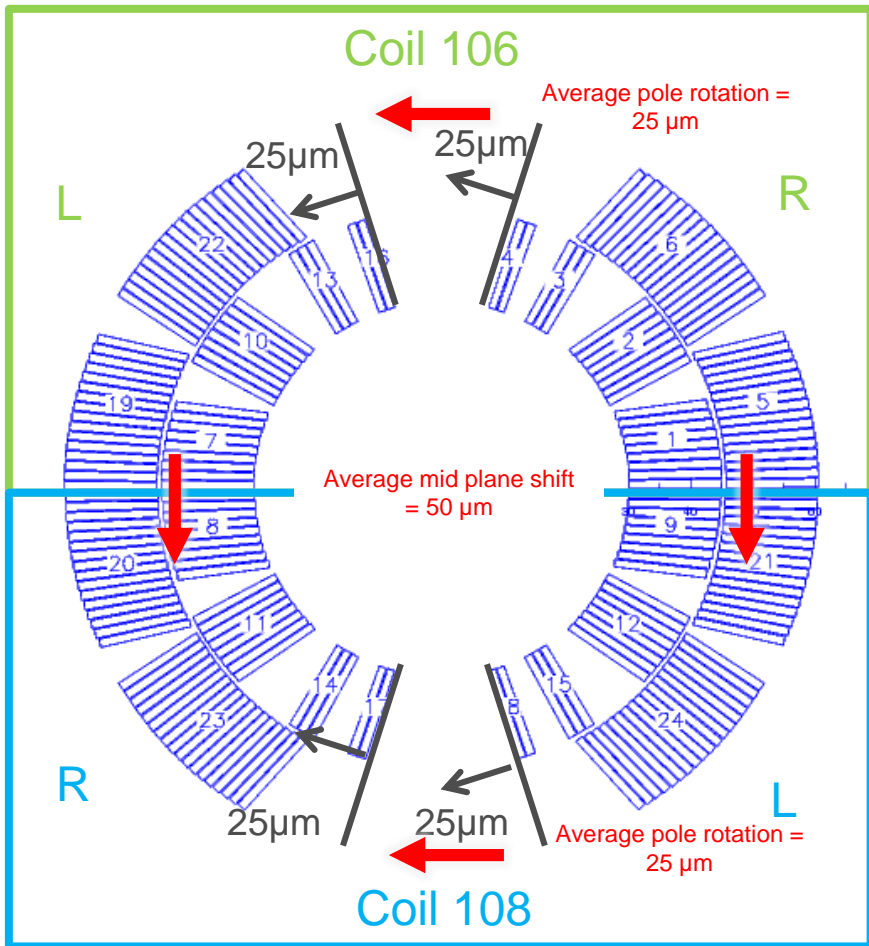
# MBHSP102 non-allowed

- For the non-allowed, only  $a_2$  is not within the boundaries set by the manufacturing tolerances.
- It can be easily explained by the differences in coil outer radial insulation

n	300 K at 20 A		300 K at 20 A		1.9 K at 5 kA						Manufacturing tolerance	
	Collared coil		Cold mass		seg3		seg4		seg5			
n	bn	an	bn	an	bn	an	bn	an	bn	an	bn	an
2	0.00	8.72	0.33	6.76	1.75	2.73	1.22	3.56	0.69	3.67	1.93	2.87
3	1.71	-0.93	9.50	-0.84	11.32	-1.78	11.82	-1.38	10.75	0.25	1.24	1.66
4	0.21	1.66	0.24	1.28	0.54	0.19	0.32	-0.33	-0.29	-0.2	0.6	1
5	2.24	-0.01	1.56	-0.02	1.17	-0.59	1.39	0.2	1.65	0.58	0.31	0.64



# MBHSP102 Coil Geometry

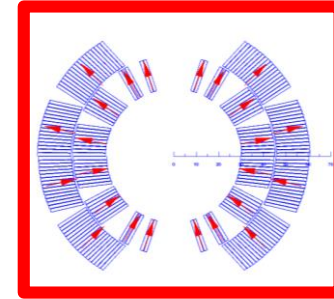


Pole shimming	SS-316	Kapton
Nominal	0.125	3x0.125
106 right	0.1	3x0.125
106 left	0.15	3x0.125
108 right	0.15	3x0.125
108 left	0.1	3x0.125

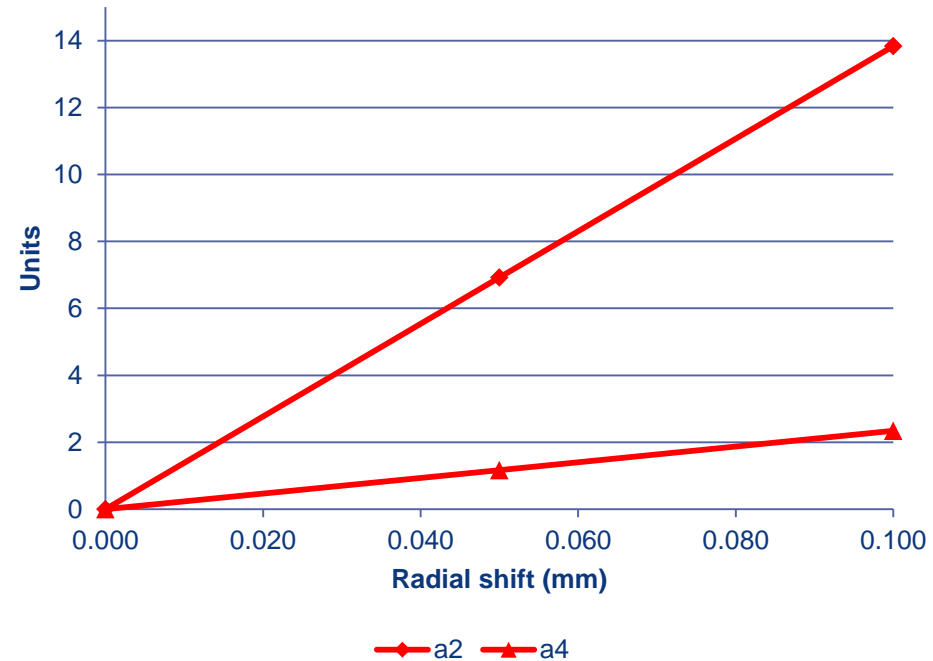
Radial Insulation	S2-Wrap	Kapton
Nominal	0.2	0.5
106 inner	0.0	0.5
106 outer	0.0	0.5
108 inner	0.1	0.5
108 outer	0.1	0.5

# MBHSP102 a2, a4

A radial shift of 50  $\mu\text{m}$  explain a2 and a4, which is reasonable considering that coil 106 has 100  $\mu\text{m}$  less of radial insulation



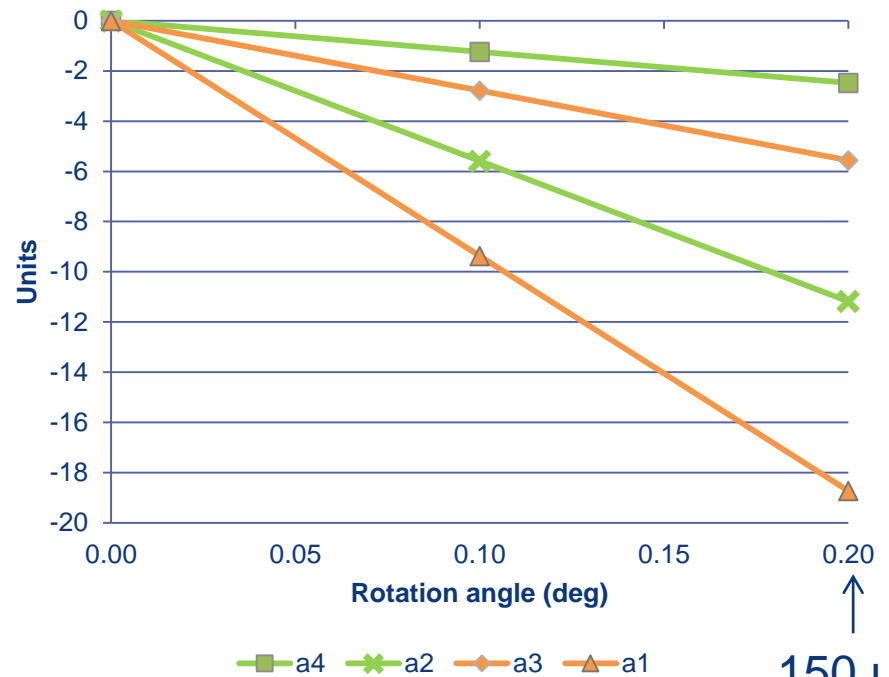
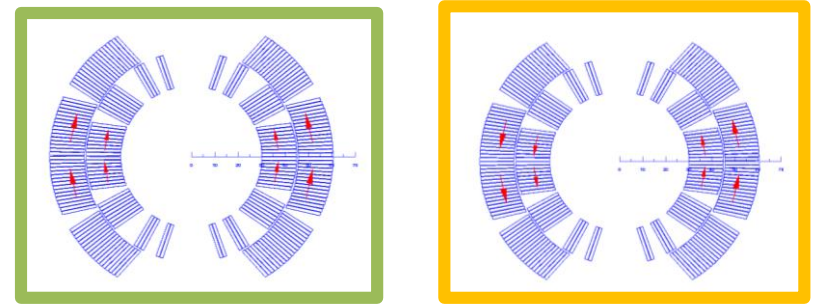
CC	R22		ROXIE	
	0.795		0.798	
	bn	an	bn	an
2	0.00	8.72	0.00	0.00
3	1.71	-0.93	-0.40	0.00
4	0.21	1.66	0.00	0.00
5	2.24	-0.01	0.49	0.00



# MBHSP102 a3, a5

- To explain a3/a5 we need anti-symmetry in both axis
- 20  $\mu\text{m}$  of rotation on the mid-plane is enough to justify a<sub>3</sub>,
- But from mechanical measurements it seems that the mid-plane is shifted (i.e. a<sub>2</sub> a<sub>4</sub>) and not rotated. 70  $\mu\text{m}$  of rotation in the mid-plane explains the measured a2 and a4 (which can be also explain with the differences in coil radial shimming).

CC	R22		ROXIE	
	0.795		0.798	
	n	bn	bn	an
2	0.00	8.72	0.00	0.00
3	1.71	-0.93	-0.40	0.00
4	0.21	1.66	0.00	0.00
5	2.24	-0.01	0.49	0.00



150  $\mu\text{m}$



# Ramp-rate dependence

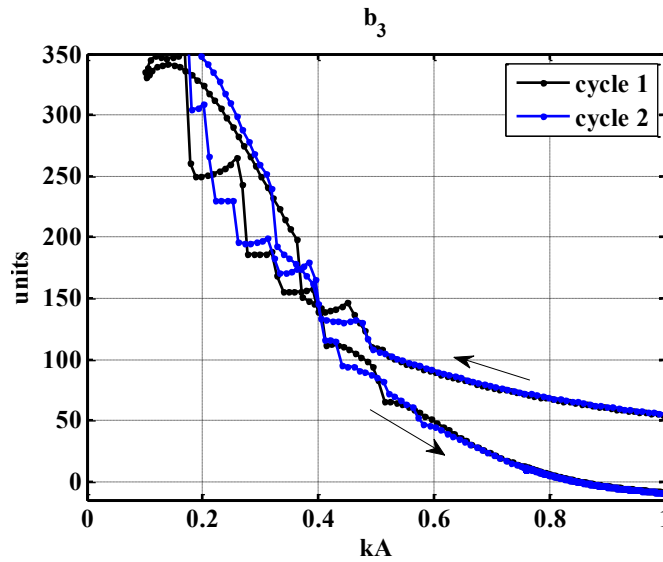
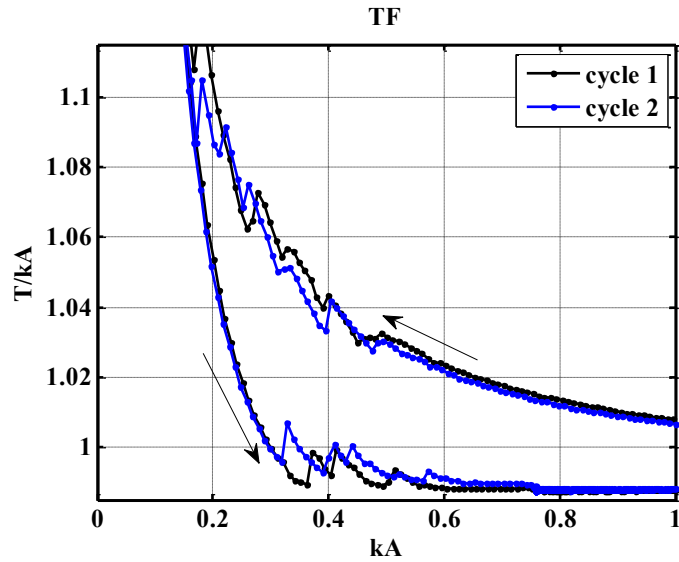
MBHSP101										
A s <sup>-1</sup>	0	10	20	40	80	0	10	20	40	80
	$\Delta b_n$ at 5 kA (units)					$\Delta a_n$ at 5 kA (units)				
2	0.00	0.10	0.05	-0.03	-0.20	0.00	-0.05	-0.11	-0.12	-0.13
3	0.00	0.03	0.05	0.06	0.16	0.00	0.02	-0.04	-0.15	-0.30
4	0.00	0.02	0.05	0.09	0.21	0.00	0.01	0.02	0.04	0.10
5	0.00	-0.04	-0.05	-0.10	-0.17	0.00	0.00	0.00	-0.01	-0.01
6	0.00	0.00	0.00	0.05	0.10	0.00	0.01	0.02	0.02	0.01
7	0.00	0.02	0.00	0.01	0.00	0.00	-0.03	-0.01	-0.03	-0.01
8	0.00	0.03	0.03	0.04	0.05	0.00	0.01	0.00	0.02	0.01
9	0.00	0.00	0.00	0.01	0.01	0.00	0.00	0.01	0.01	0.04

MBHSP102										
A s <sup>-1</sup>	0		20	50	100	0		20	50	100
	$\Delta b_n$ at 5 kA (units)					$\Delta a_n$ at 5 kA (units)				
2	0.00		-0.02	-0.14	-0.12	0.00		-0.26	-0.62	-0.84
3	0.00		0.16	0.32	0.54	0.00		-0.04	0.04	0.12
4	0.00		0.02	0.04	0.08	0.00		-0.16	-0.28	-0.38
5	0.00		-0.14	-0.08	0.02	0.00		-0.06	-0.02	-0.02
6	0.00		0.00	0.02	0.06	0.00		0.02	-0.02	-0.06
7	0.00		0.02	0.02	0.04	0.00		0.00	0.00	0.00
8	0.00		0.00	0.02	0.08	0.00		0.00	-0.02	0.00
9	0.00		0.02	0.00	-0.02	0.00		0.00	0.02	0.02

- Small effects on both magnets

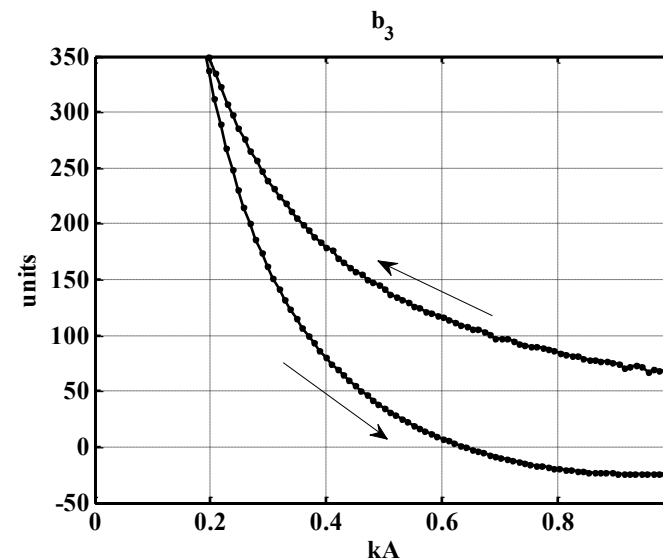
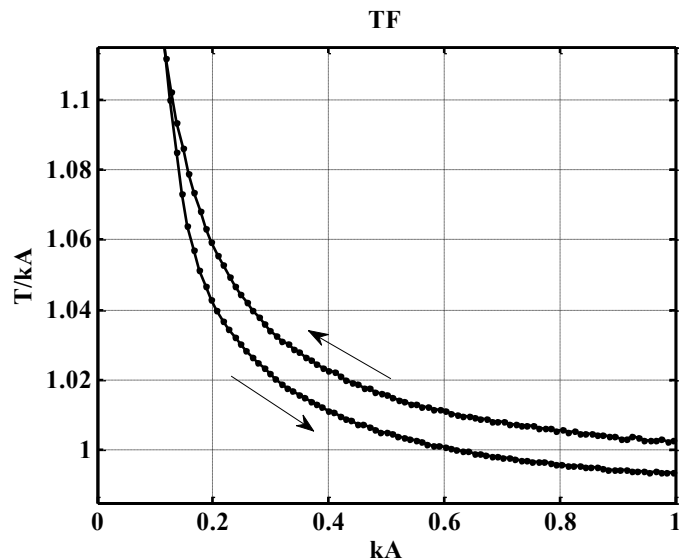
Reference radius 17 mm

# Noise at low current MBHSP101



At 1.9 K

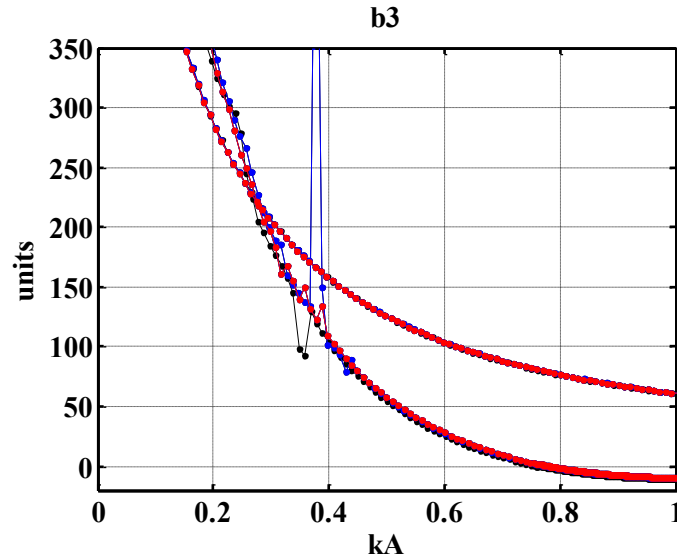
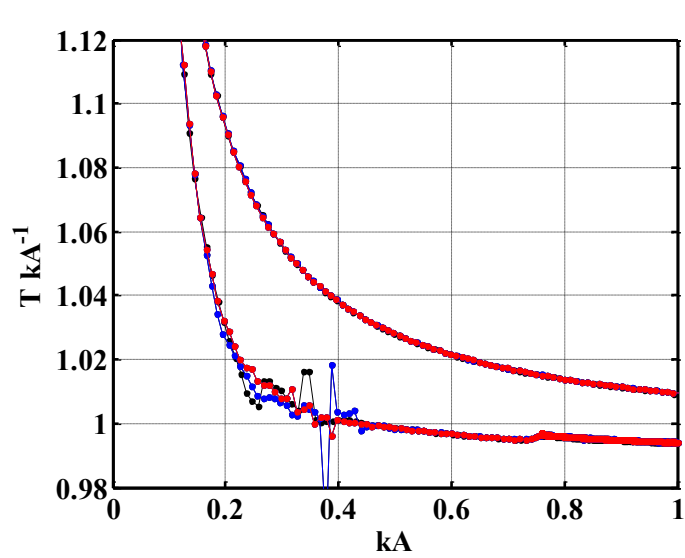
- Noise up to 600 A
- Visible on TF and multipoles



At 4.5 K

- No noise at low current
- Noise of smaller amplitude at higher current

# Noise at low current MBHSP102

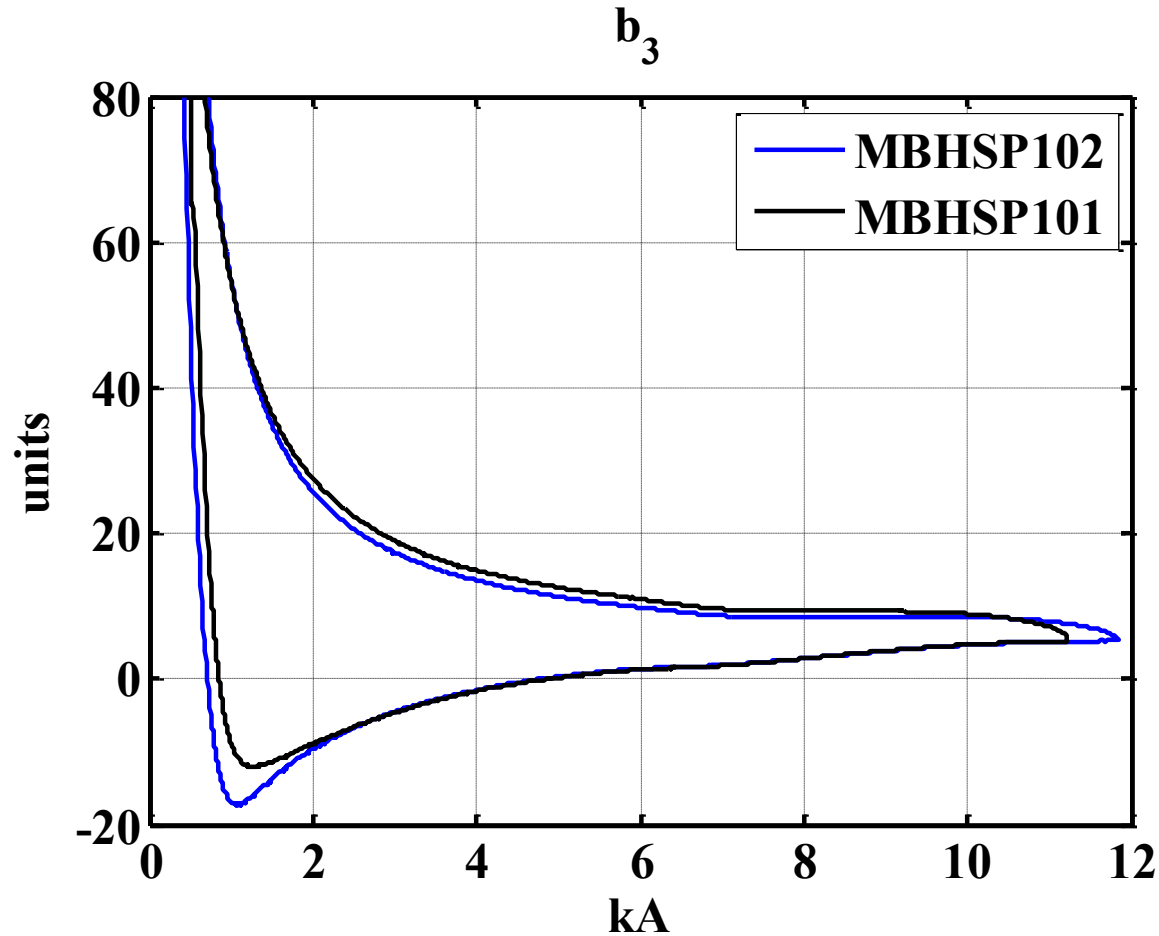


At 1.9 K

- Noise up to 500 A
- Visible on TF and multipoles

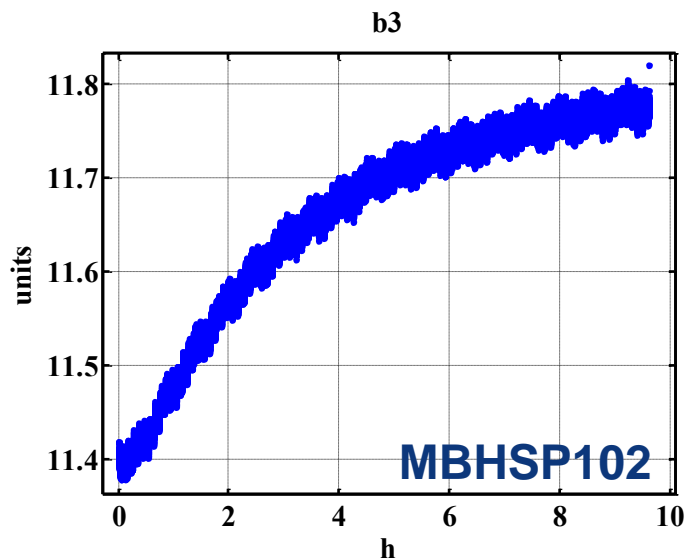
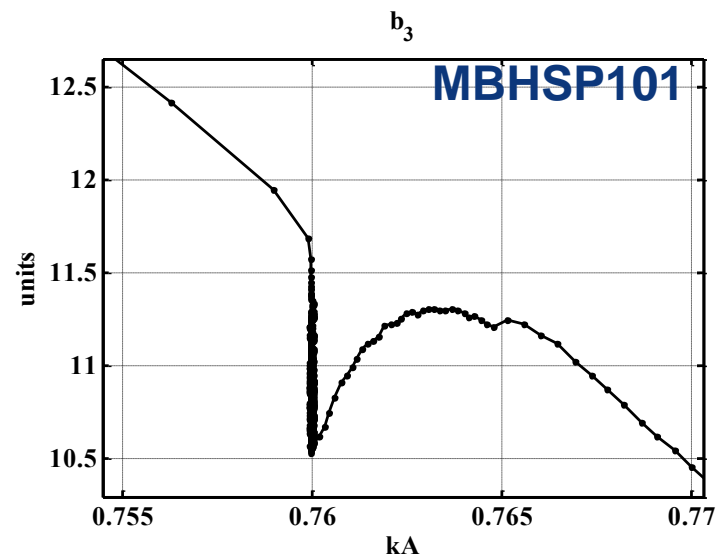
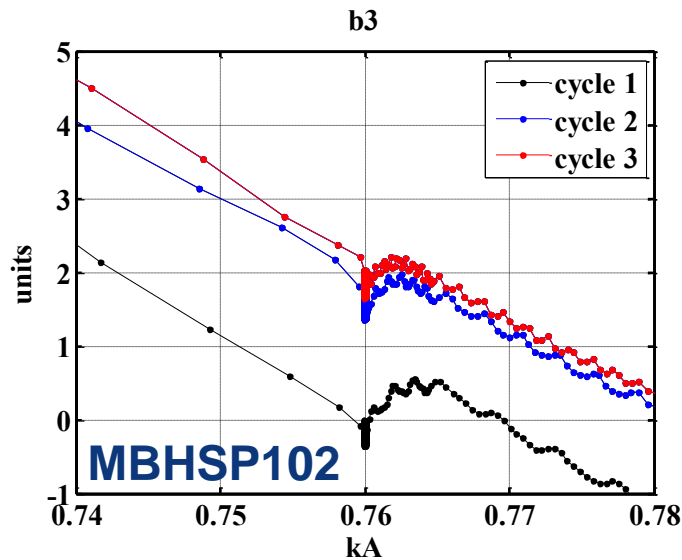
No tests at 4.5 K

# Persistent currents



- Differences on measured  $b_3$  magnetization cycle

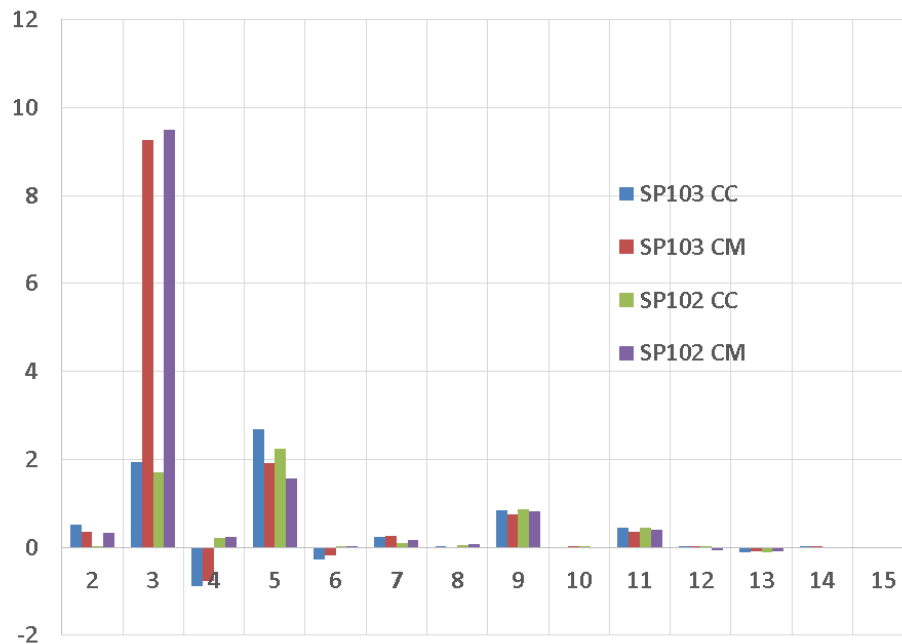
# Other measurements



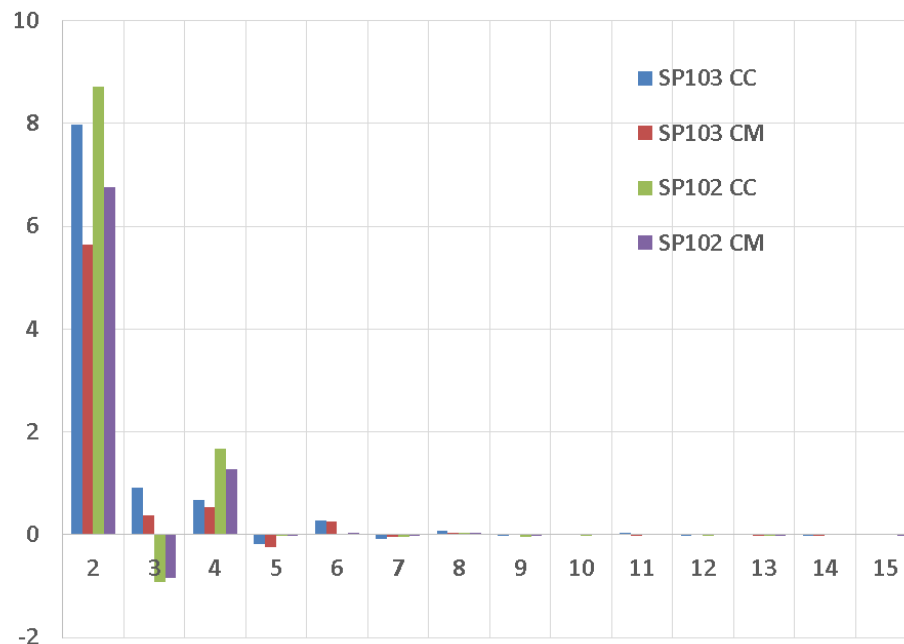
- Settling of  $b_3$  after 3 cycles
- Decay at injection of 1.2 units observed on SP101
- Decay of 0.4 units on  $b_3$  during a 10-h long plateau at nominal current

# MBHSP103

bn



an



- Results of measurements at 300 K on MBHSP103 are very similar to those on MBHSP102

# Conclusions

3 short models tested (2 warm and cold, and 1 warm)

## Transfer function

- Geometric in agreement with the model
- Saturation overestimated by the model

## Multipoles

- Geometric in general agreement with the model
- Discrepancies on persistent current effects

## Ramp-rate dependency

- Relatively small effects

## Cold/Warm correlation

- Change before/after cold tests on MBHSP101
- Better correlation on MBHSP102