



**High
Luminosity
LHC**

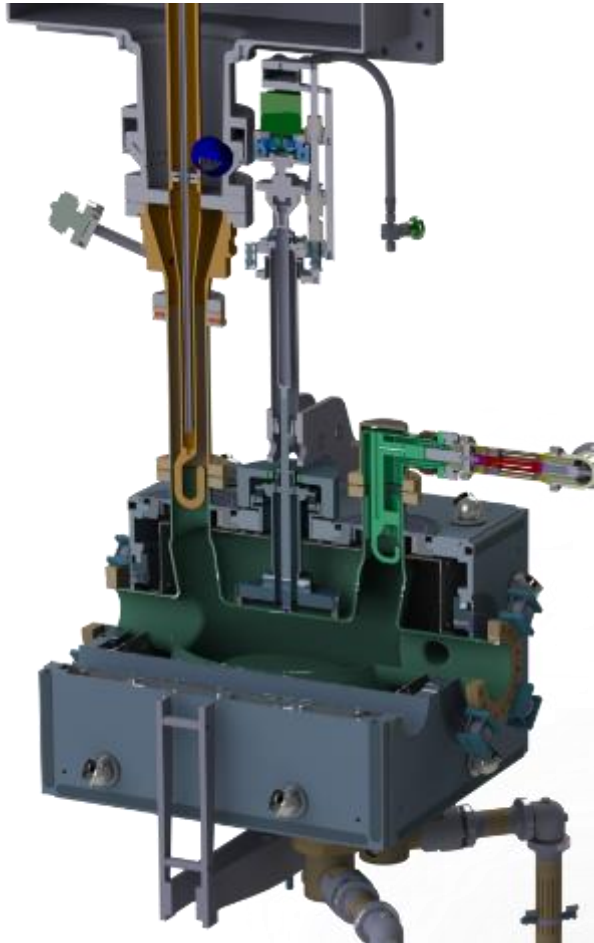
CRAB cavities Cryomodule review Tuner

((CERN) **Kurt Artoos**, Rama Calaga, Ofelia Capatina, Teddy Capelli, Federico Carra, L. Dassa, Norbert Kuder,
Raphael Leuxe,
P. Minginette
Colleagues USLARP , STFC

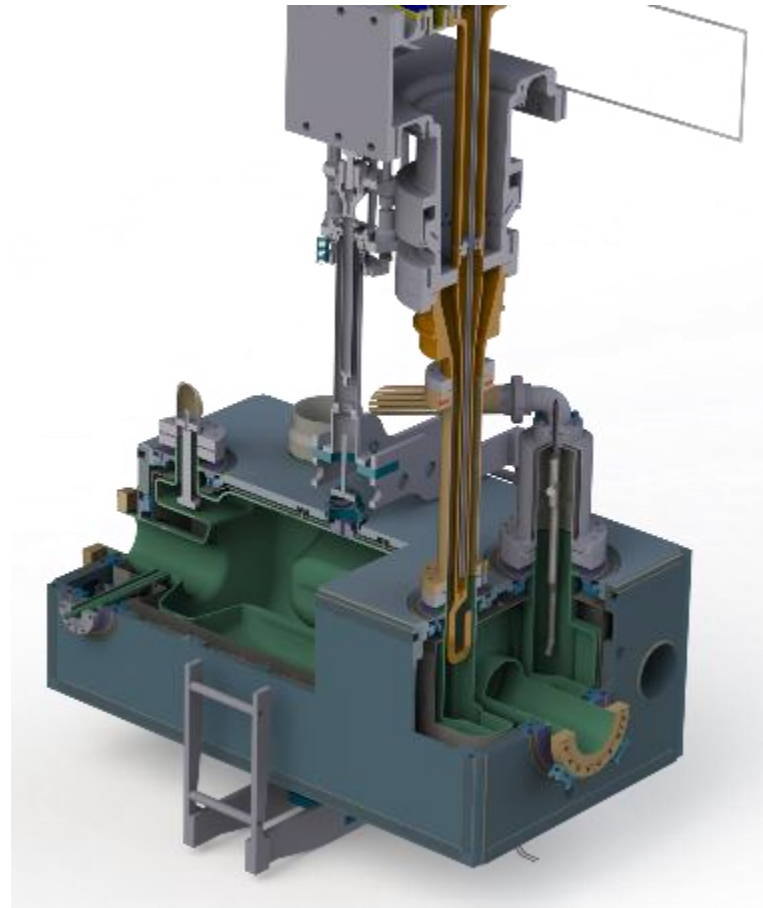
Contents

- Tuning principle
- DQW and RFD Tuning forces, stress and range
- DQW pre tuning
- Tuning frame
- Status SM18 tuner
- Studies SPS tuner

Symmetric actuation on cavity through tuner frame and concentric tubes.
Motorization outside cryostat
Centre of the actuation is floating



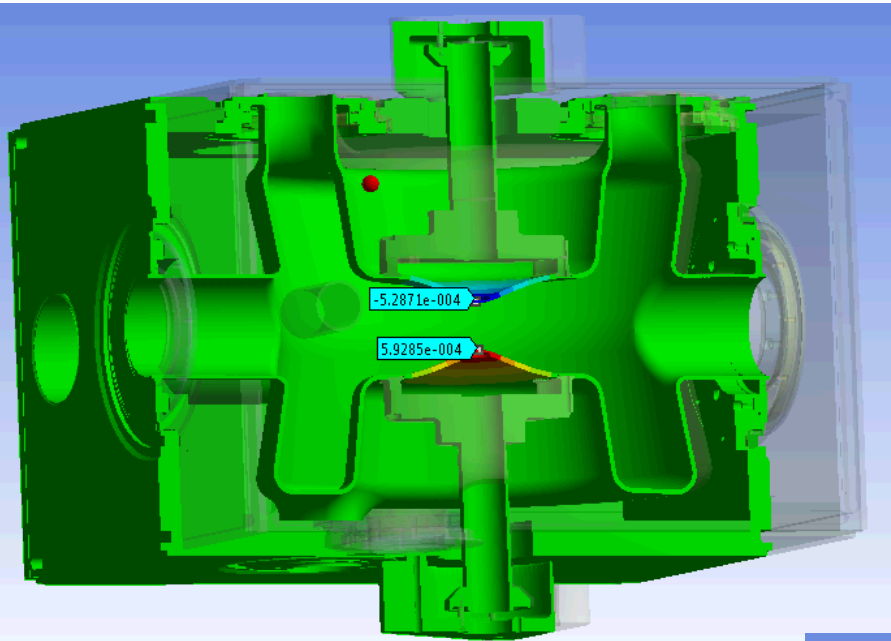
DQW : 186 kHz/mm *
S. Vérdu Andrés , B. Xiao



RFD : 345 kHz/mm *
H. Park

* Measured as tuner stroke or Δ distance between 2 plates

DQW



Cavity (RT , no PCB) with He vessel +
pretuning device
Input force 2.5 kN

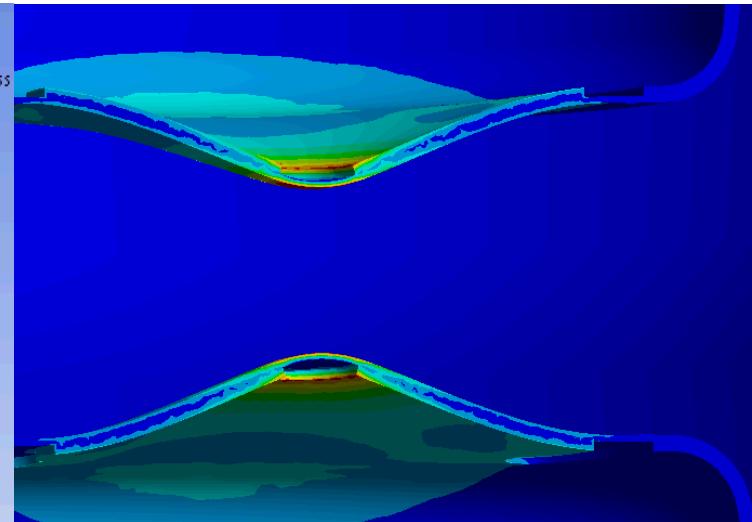
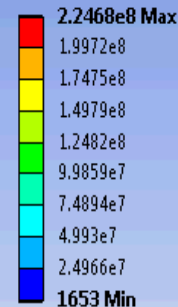
Displacement z **0.53/0.6 mm**
Maximum eq. Stress **225 MPa**
Corresponds to about **0.21 MHz (0.42 MHz
pp) ***

**For 400 MPa/1.2= 333 MPa -> 0.31 MHz
(0.62 MHz) range (linear), 3.7 kN, ±1.6 mm**

Force/tuner stroke **2.2 kN/mm**
199 MPa/mm

At RT for 50 MPa , 0.25 mm maximum
tuner stroke for 0.5 kN

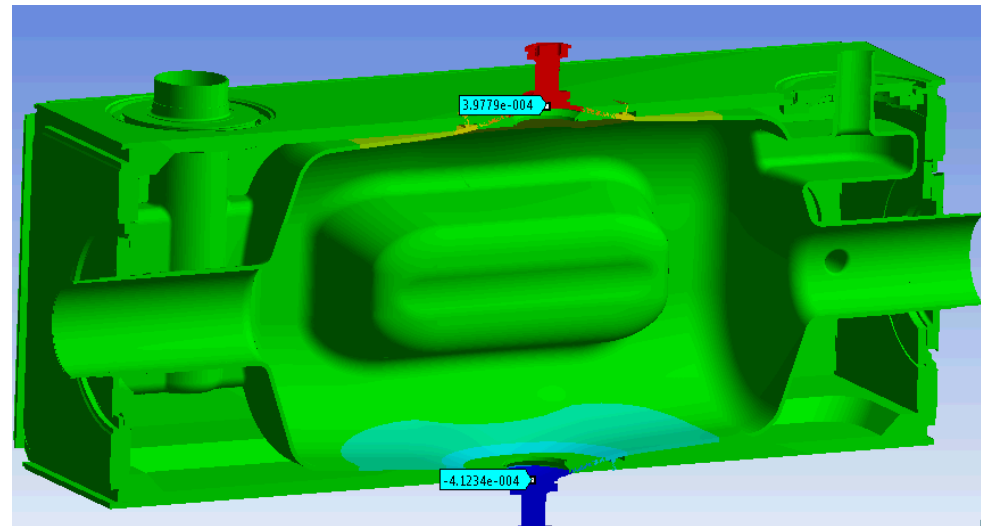
B: Static Structural
Equivalent Stress 4
Type: Equivalent (von-Mises) Stress
Unit: Pa
Time: 1
5/5/2015 21:37



RFD

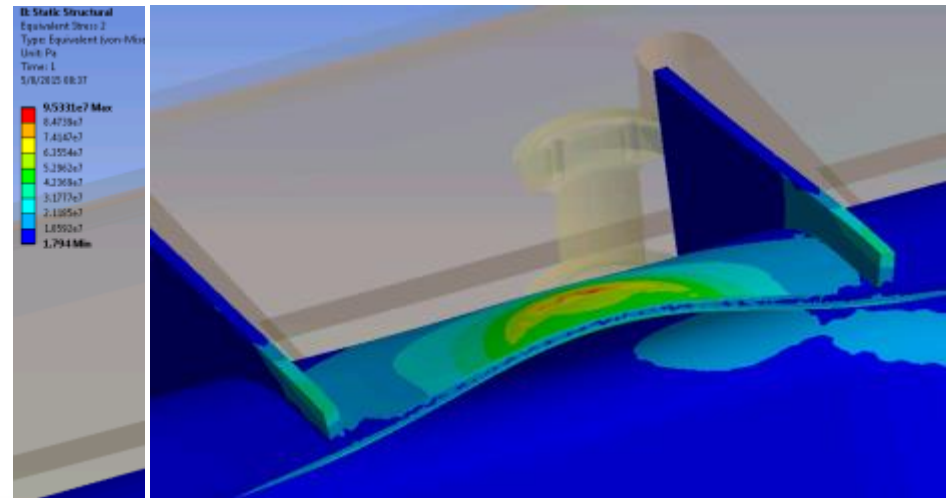
Cavity (RT , no PCB) with He vessel
Input force 2 kN

Displacement z 0.4/0.41 mm
Maximum eq. Stress **95 MPa**
Corresponds to about **0.280 MHz (0.560 MHz pp)**
For $400 \text{ MPa}/1.2 = 333 \text{ MPa} \rightarrow 0.980 \text{ MHz}$
(1.96 MHz) range (linear), 7 kN, $\pm 2.8 \text{ mm}$

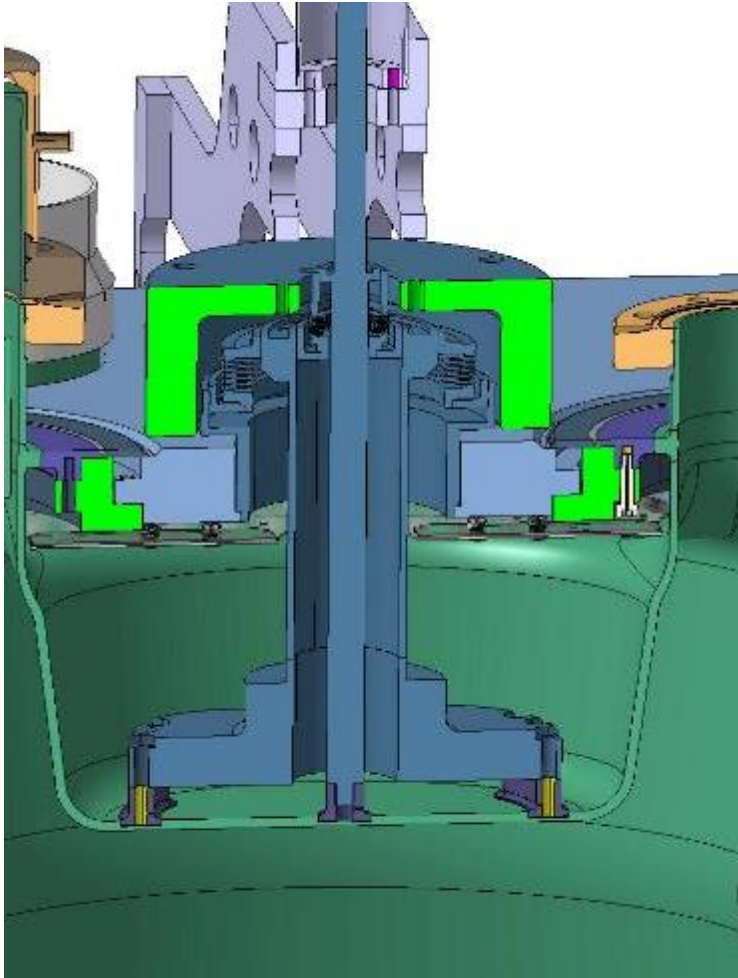


Force/tuner stroke **2.5 kN/mm**
115 MPa/mm

At RT for 50 MPa , 0.42 mm max tuner stroke for 1 kN



Pre tuning DQW



At warm

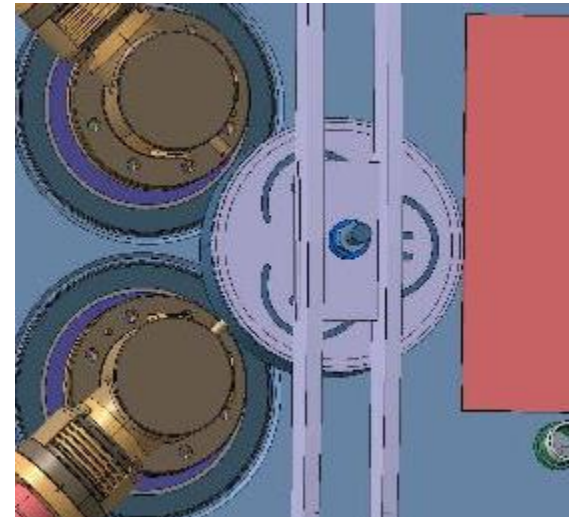
Bellows are outside of the helium vessel

3 M6 screws (pull) and studs (push)

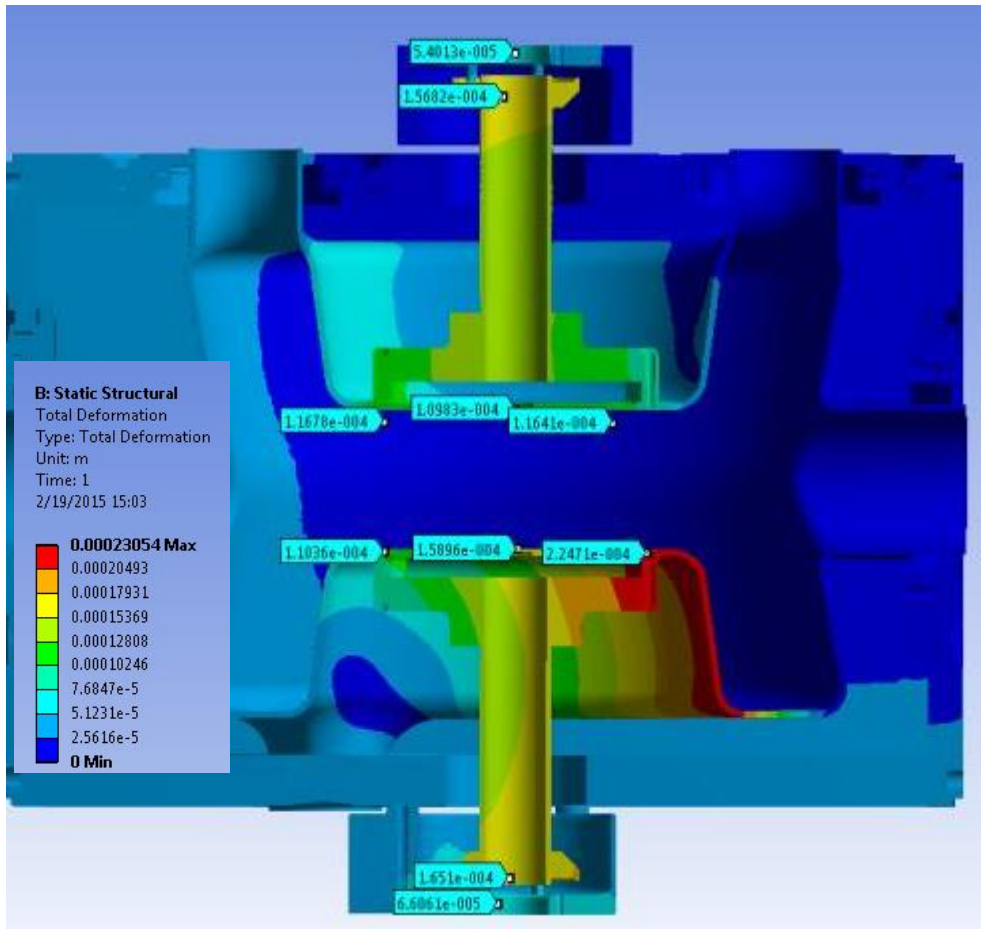
Pitch 1 mm

Bellows (Ti) will be probably edge welded

Sensitivity 0.8023 MHz/mm (distance between plates) (Binping Xiao)

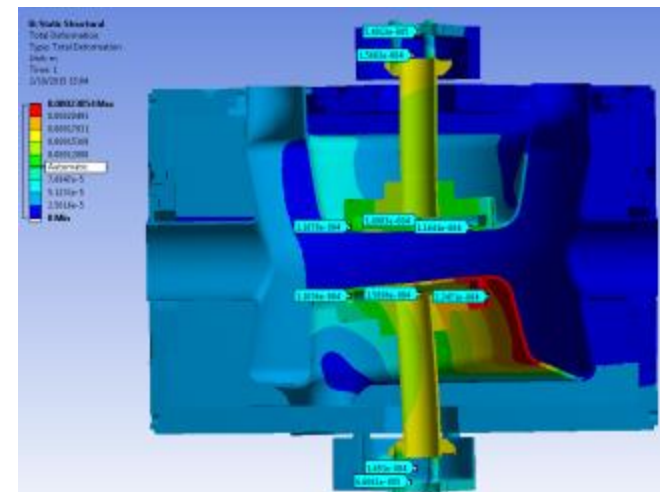


Deformation

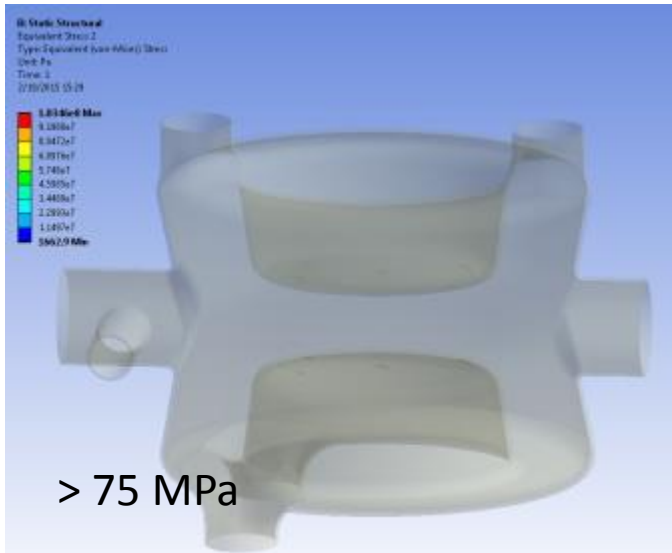
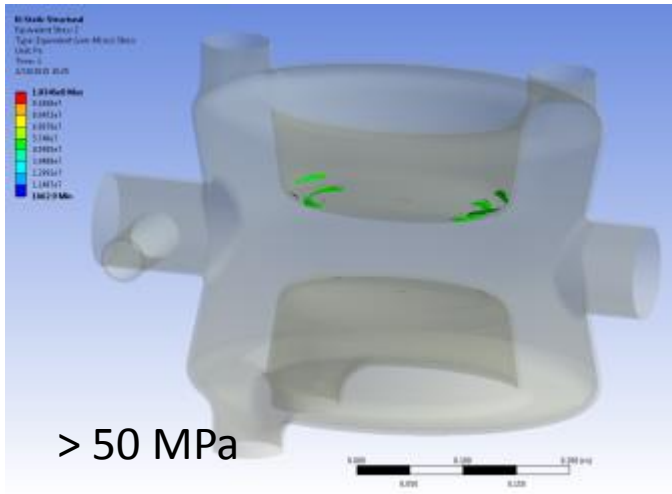


Top : 0.21 mm screw motion
 -> 0.11 mm plate deformation
 Bottom: 0.23 mm screw
 -> 0.16 mm centre plate def.

Force: about 3 kN /screw M6x1
 σ_i screw = 178 MPa (0.3 friction)
 Flexibility gives the resolution



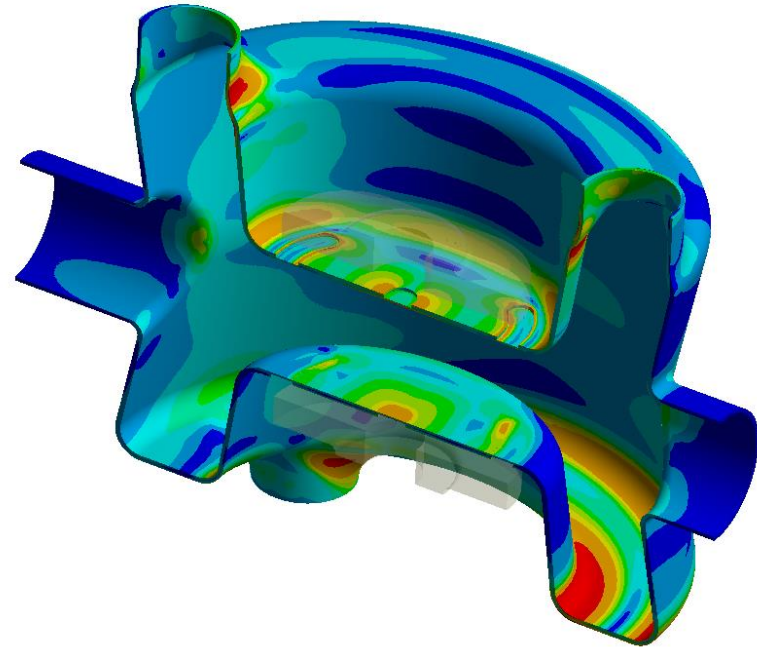
Pretuning stress



Pre-tuning 0.2 mm (distance plates) + pressure

B: Submodel
Stress Cavity
Type: Stress Intensity
Unit: MPa
Time: 4
06/05/2015 09:02

130.21 Max
75
50
42.868
35.736
28.603
21.471
14.339
7.2069
0.074691 Min



Ref. L. Dassa For the helium vessel as pressure vessel this would be a limit (needs some thinking)

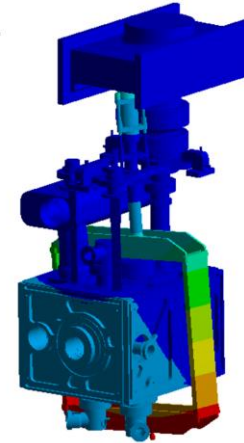
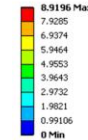
0.16 MHz (0.32 MHz) for 0.8 MHz/mm

Design tuning frame

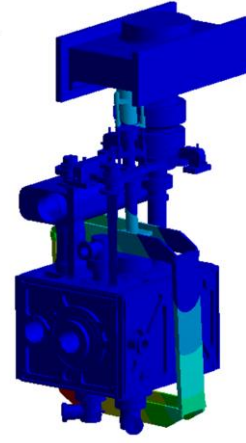
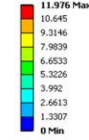
Modal analysis of the support structure indicated presence of low vibration modes of the titanium tuning frame

A first improvement was made to divide the mass by 2

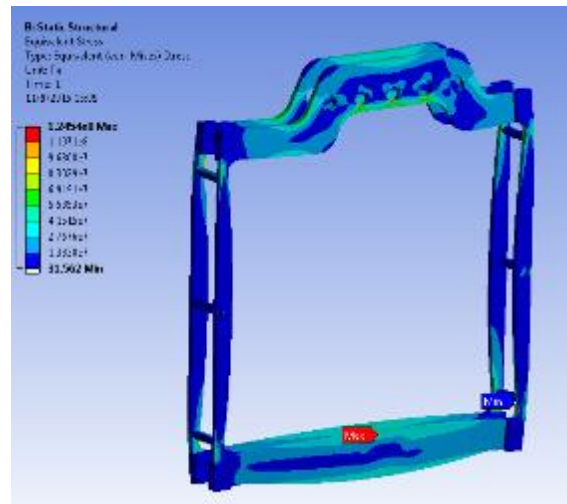
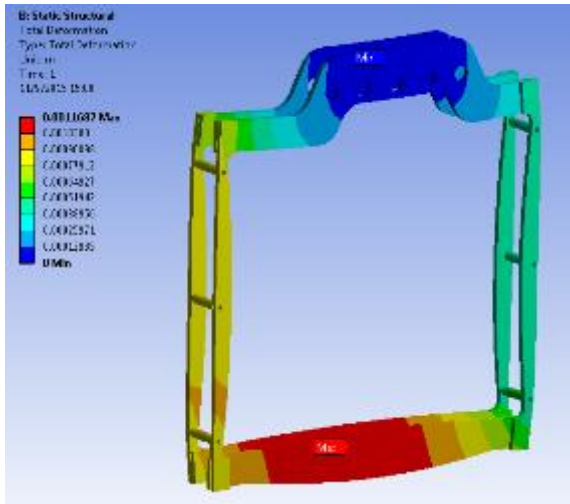
C-Modal
Total Deformation
Type: Total Deformation
Frequency: 8.8509 Hz
Unit: mm
01/09/2015 13:48



C-Modal
Total Deformation 2
Type: Total Deformation
Frequency: 9.8713 Hz
Unit: mm
01/09/2015 13:49



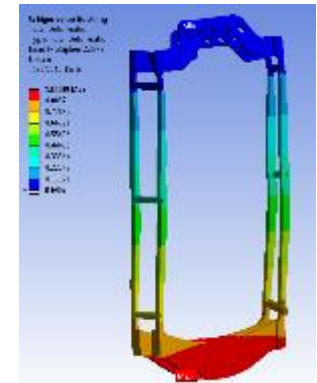
Calculations T. Jones



7 kN load

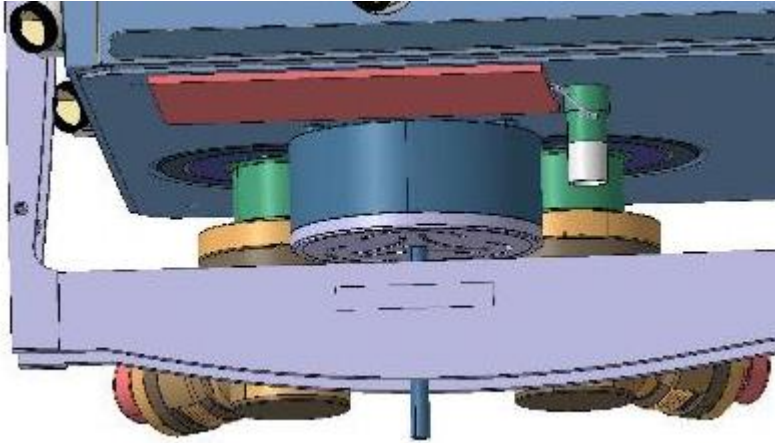
Some optimisation still to be done
Flexibility of the frame could be used
to increase the tuning resolution

Buckling analysis
Multiplier 4.2



Calculations N. Kuder

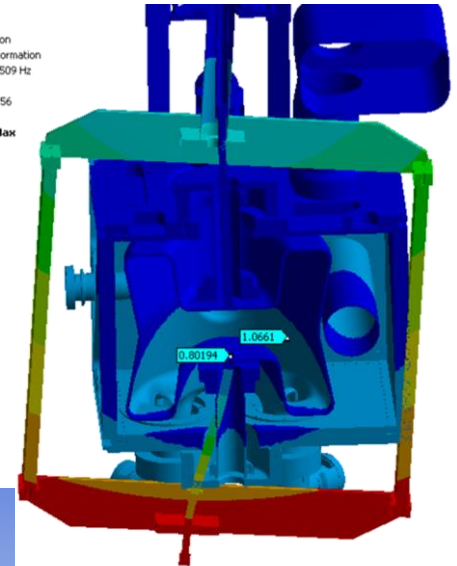
Flexural guide



1 mm thick Titanium
Gr. 5 Plate (or CuBe)

C: Modal
Total Deformation
Type: Total Deformation
Frequency: 8.8509 Hz
Unit: mm
01/09/2015 13:56

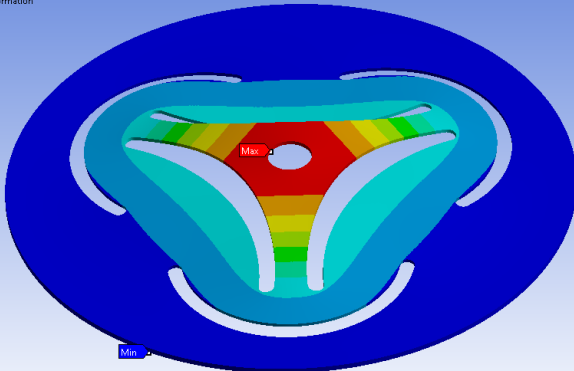
8.9196 Max
7.9285
6.9374
5.9464
4.9553
3.9643
2.9732
1.9821
0.99106
0 Min



Calculations T. Jones

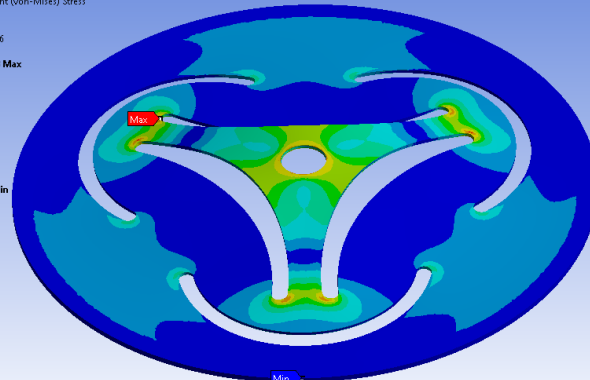
B: Static Structural
Total Deformation
Type: Total Deformation
Unit: m
Time: 1
11/9/2015 15:52

0.003 Max
0.0026667
0.0023334
0.002
0.0016667
0.0013334
0.001
0.0006668
0.0003334
0 Min



B: Static Structural
Equivalent Stress
Type: Equivalent (von-Mises) Stress
Unit: Pa
Time: 1
11/9/2015 15:56

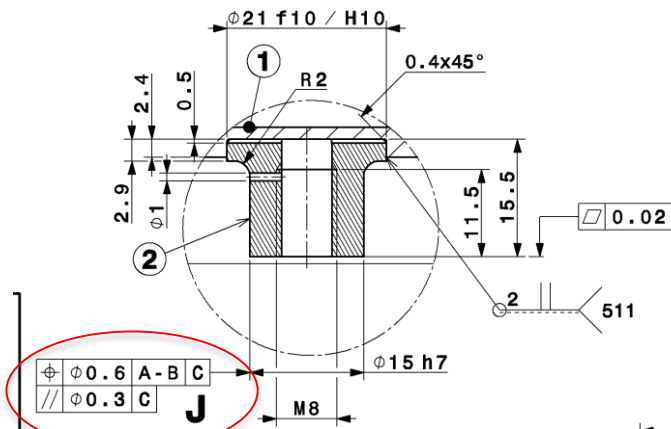
3.2705e8 Max
2.8071e8
2.5437e8
2.1803e8
1.8169e8
1.4536e8
1.0902e8
7.2578e7
3.634e7
1326.4 Min



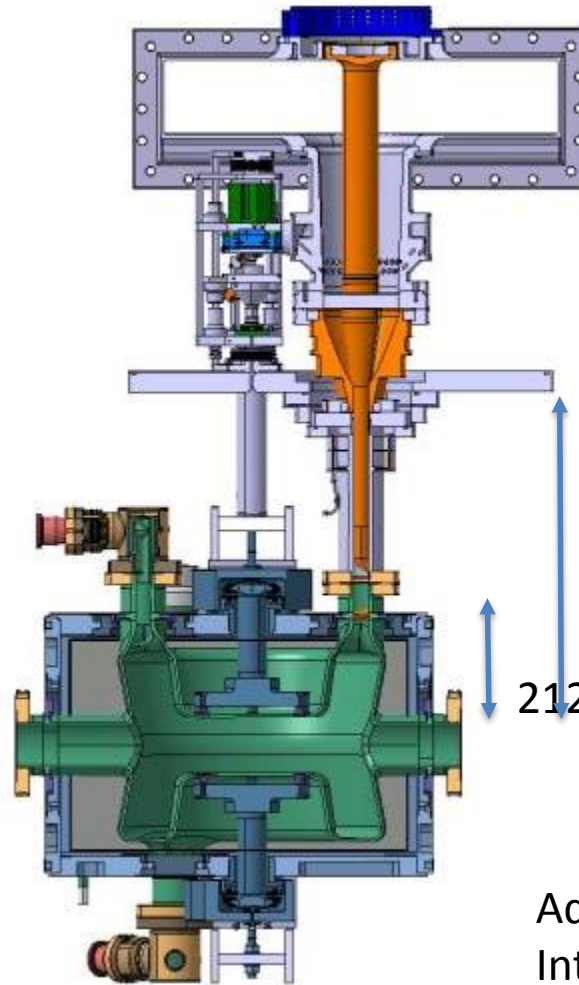
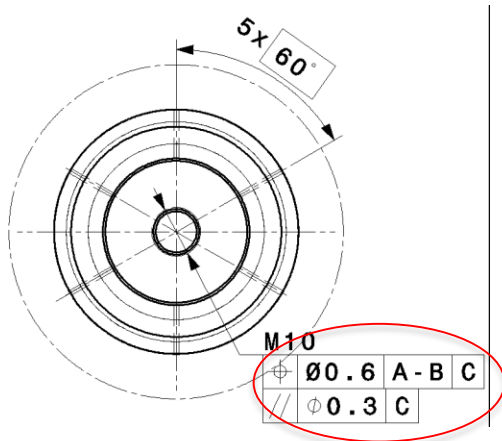
3 mm displacement
Axial stiffness 22 N/mm
Lateral stiffness $17 \cdot 10^6$ N/m
Torsional stiffness 0.1 mrad/Nm

See talk T. Jones for results modal behaviour

Tolerances tuner axis



= 1.49°



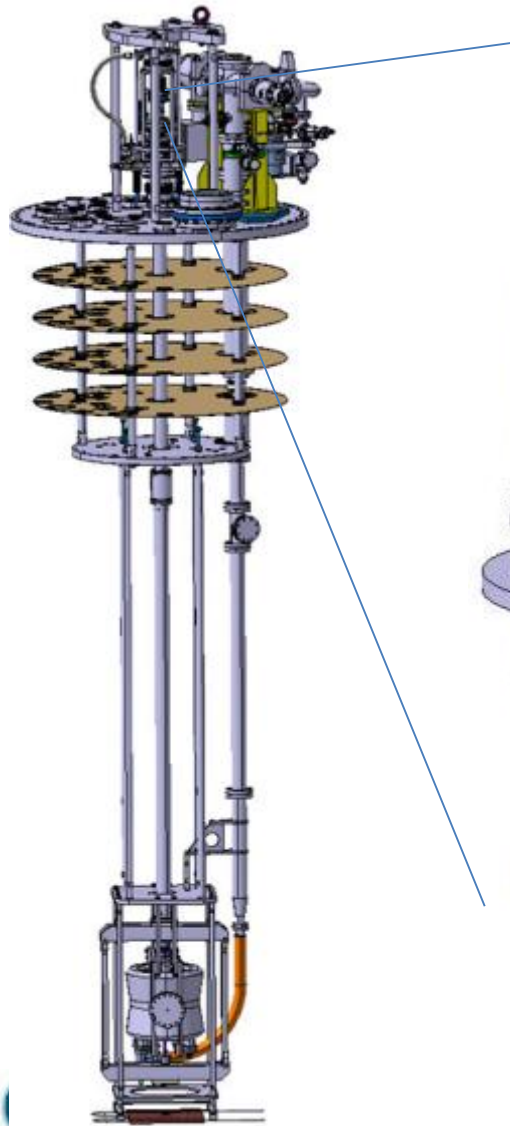
545 mm → 14 mm

212 mm → 5.5 mm

Adjustments to be foreseen
Introduce hinges (flexural)

Status SM18 p.o.p. tuner

Design: P. Minginette



**Motor 1.3 Nm Bipolar Nema 23
(1.8 deg/step)**

HD HFUS-20-100-2SO

Ratio i : 0.01 ,
repeat. peak Torque 82 Nm, average
torque 49 Nm

Accuracy < 1 arcmin, precision < 0.1
arcmin

Fa Dyn 7.7 kN, $\eta \approx 0.80$ (grease, 20 °C)

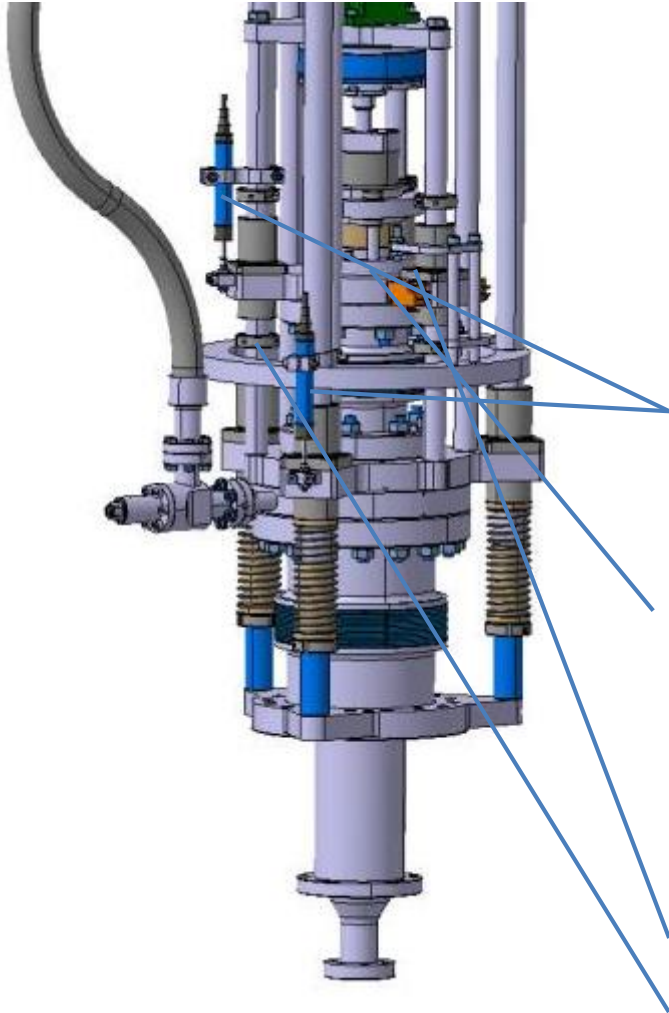
Roller screw Rollvis RV 12 x 1
 $\eta = 0.79$, static load capacity 17 kN

$$M = \rho i F / 2000 \pi \eta = 0.01 \text{ Nm} \quad F = 4 \text{ kN}, \rho = 1$$

Detend torque 0.017 Nm, self locking

Instrumentation

Design: P. Minginette



Precision linear motor:

1 step = $1.8^\circ \times 0.01 \rightarrow 0.1 \mu\text{m}$ ($p=1 \text{ mm}$)

Precision HD 0.1 arcmin or $0.0017^\circ \rightarrow 10 \text{ nm}$

Altered by friction in guides

DQW $\sim 20\text{-}2 \text{ Hz}$

RFD $\sim 35\text{-}3.5 \text{ Hz}$

Instrumentation:

Potentiometer Megatron RC13-25 M

25 mm range , 1 k Ω , resolution $\sim 10 \mu\text{m}$



Load cell Kistler

4576A55C1 class 0.1

DQW (2.2 kN/mm) $\rightarrow 1.5 \mu\text{m}$ precision

RFD (2.5 kN/mm) $\rightarrow 1.3 \mu\text{m}$ precision

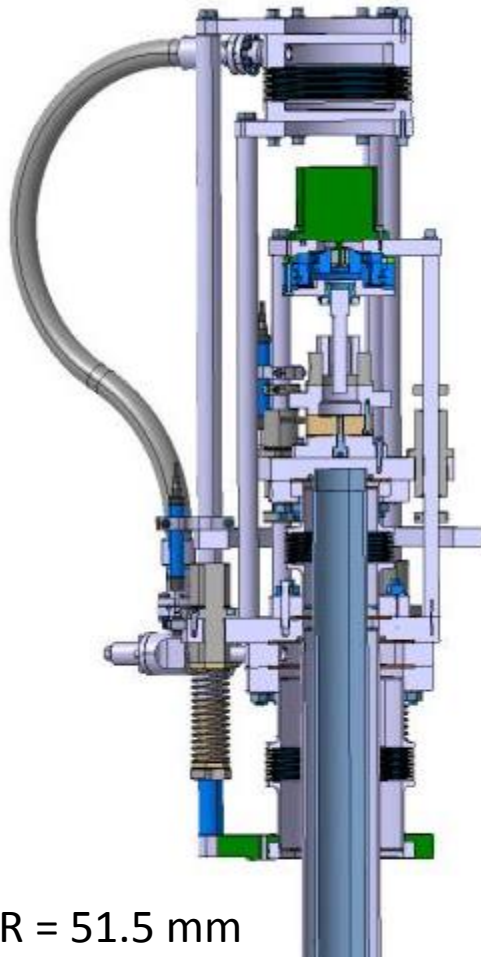
limit switches

Mechanical stops



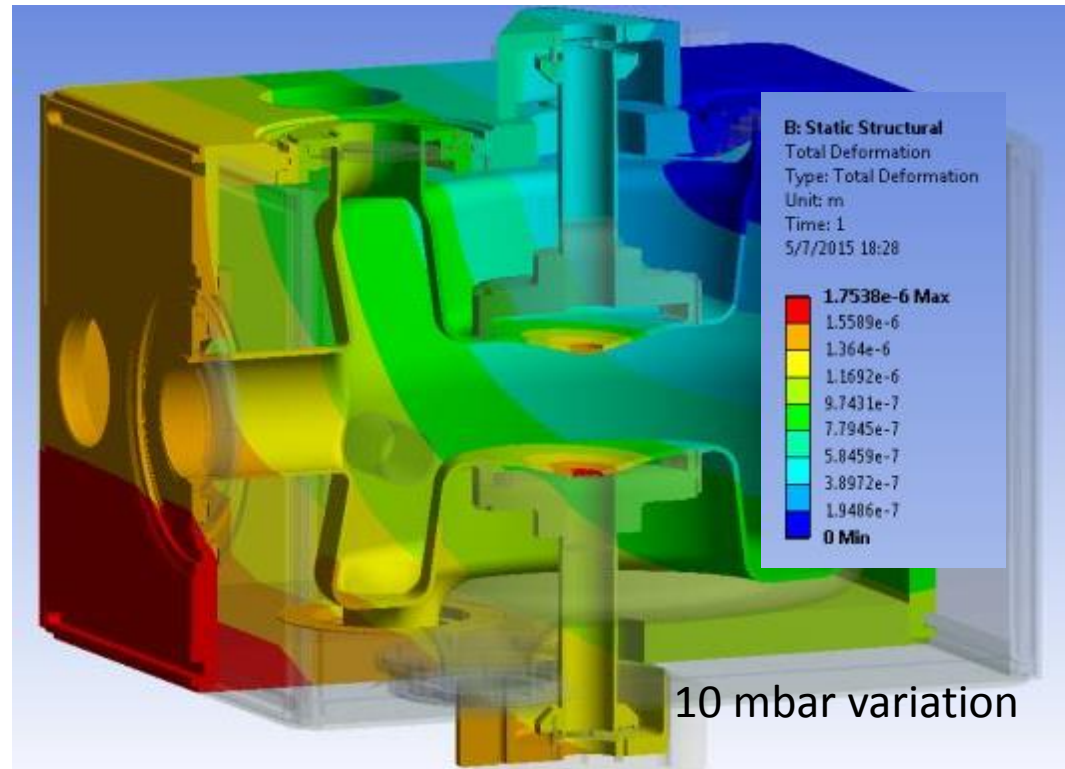
Pressure compensation

1 atm = 101.325 kPa , Force = 844 N (on 2 tuning tubes)
Day variations 3 mbar 2.5 N
Week variations 10 mbar 8.3 N



R = 51.5 mm

Surface 0.0083 m²



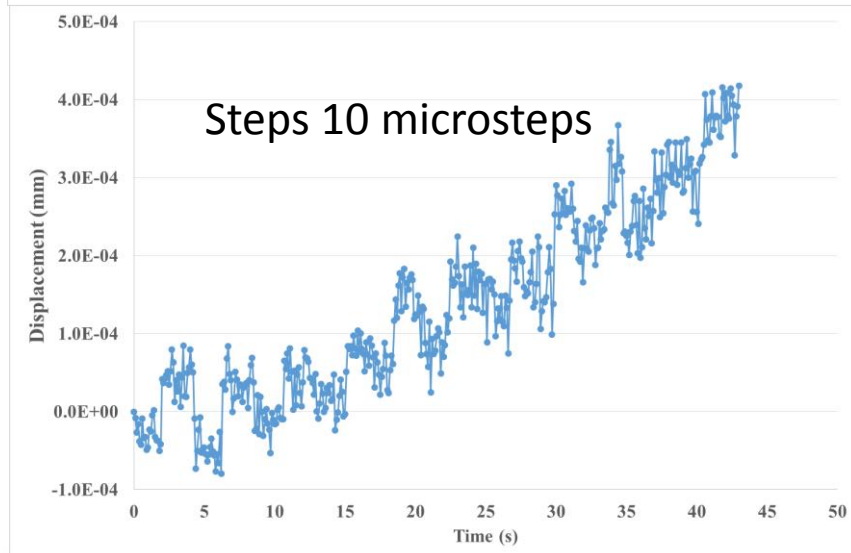
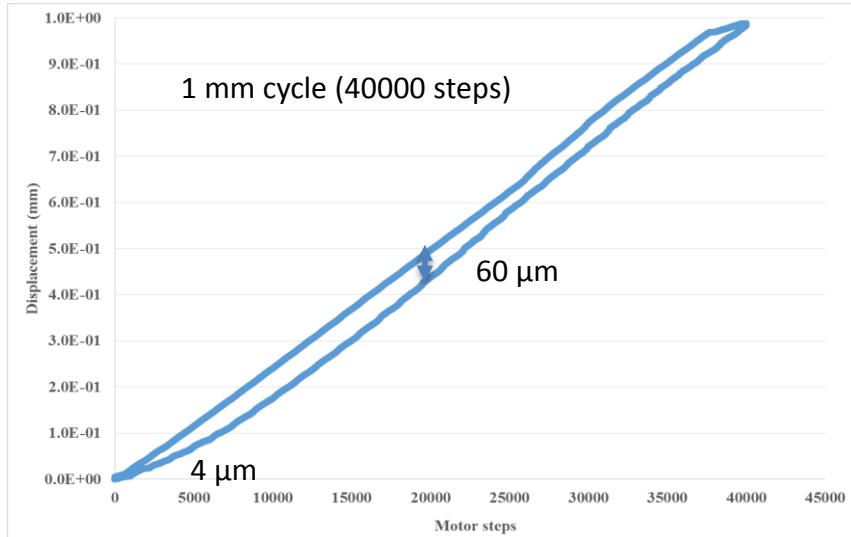
1 atm = 0.19 mm on each plate

Load compensating springs : 3 x 5 N/mm

Status p.o.p. tuner test

Linear motor protoype tested without load

- Fully assembled and tested with 400 microsteps (with LVDT)



LVDT not adapted
Sensor noise
Friction in sensor
Drift (thermal ?)

Estimate:
Precision $\sim 0.5 \mu\text{m}$
 $\sim 100 \text{ Hz DQW}$,
 175 Hz RFD

Measurement E. Gallay

Next steps p.o.p. tuner test

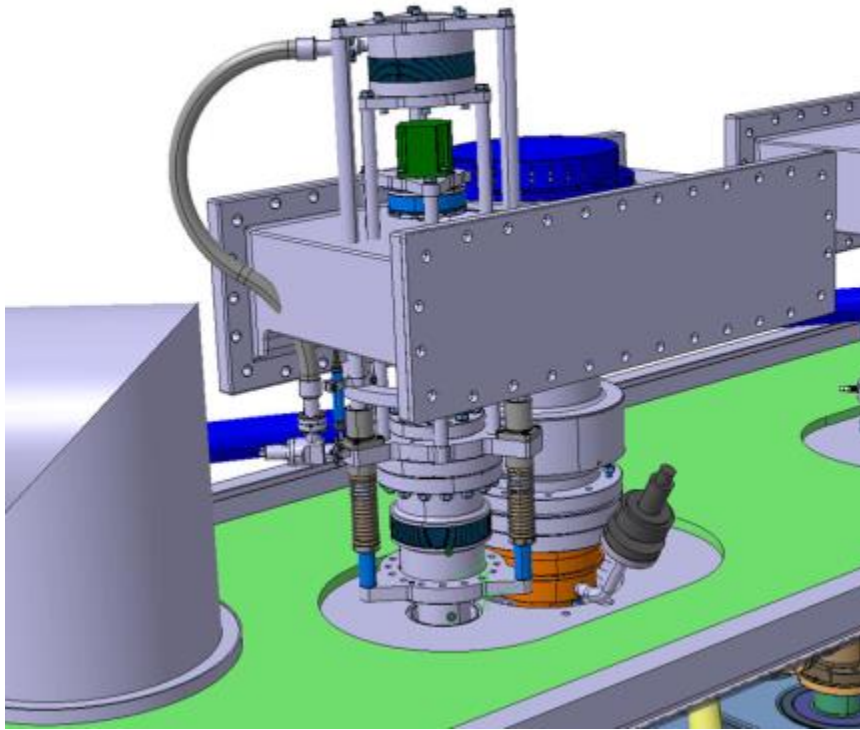


Test on p.o.p. DQW in SM18 at 2 K

- Measure directly frequency resolution + precision
- Test pressure compensation
- Status: several parts available, in preparation

Action : Build a test bench for prototype motor testing
+ fatigue cycles + qualification radiation resistance

- Integrate a spring to represent the load from cavity
- Integrate an optical linear encoder without frictional guides and nm resolution
- Test in temperature stable room



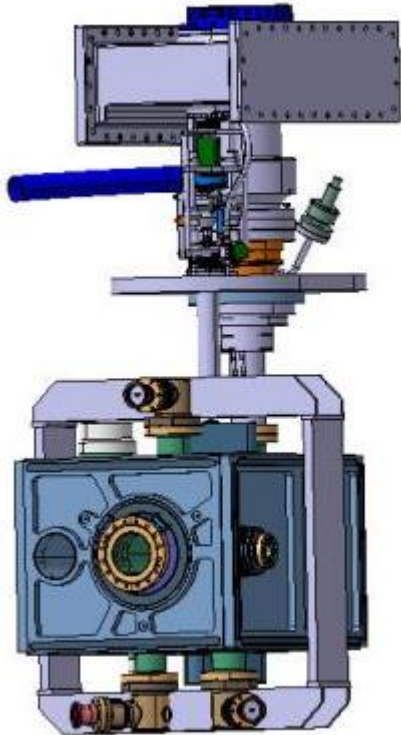
Drawbacks first design:

Size ...

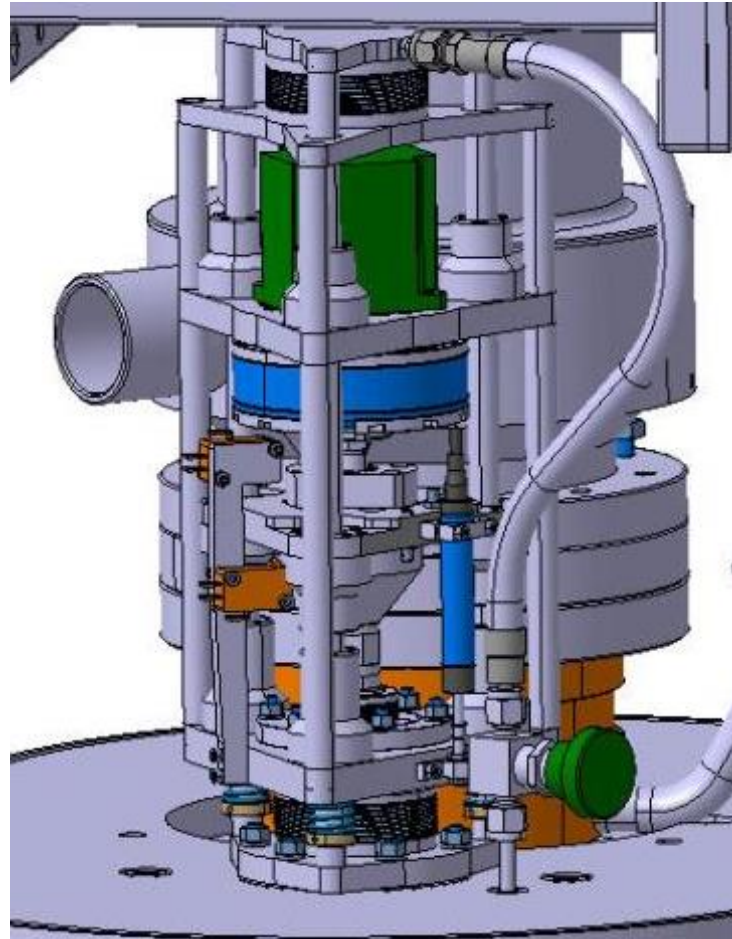
Mass \sim 10 kg

Motorisation can not be replaced
without opening cryostat (maintainability)

Status design for SPS test (v1)



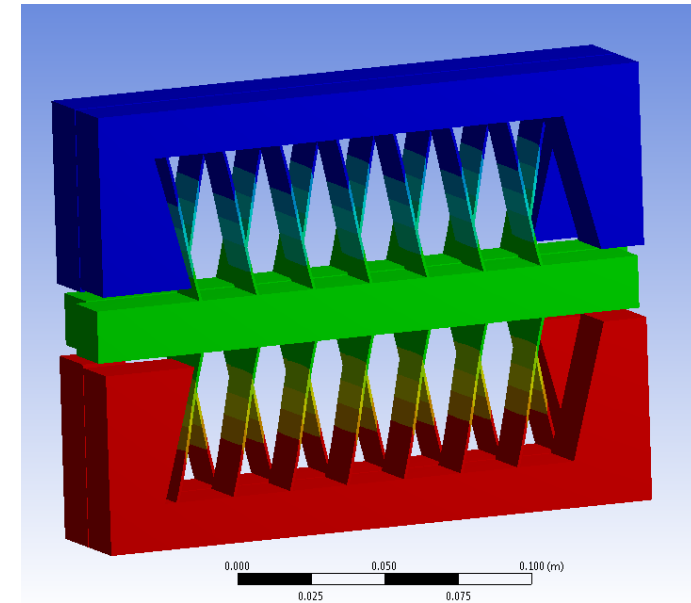
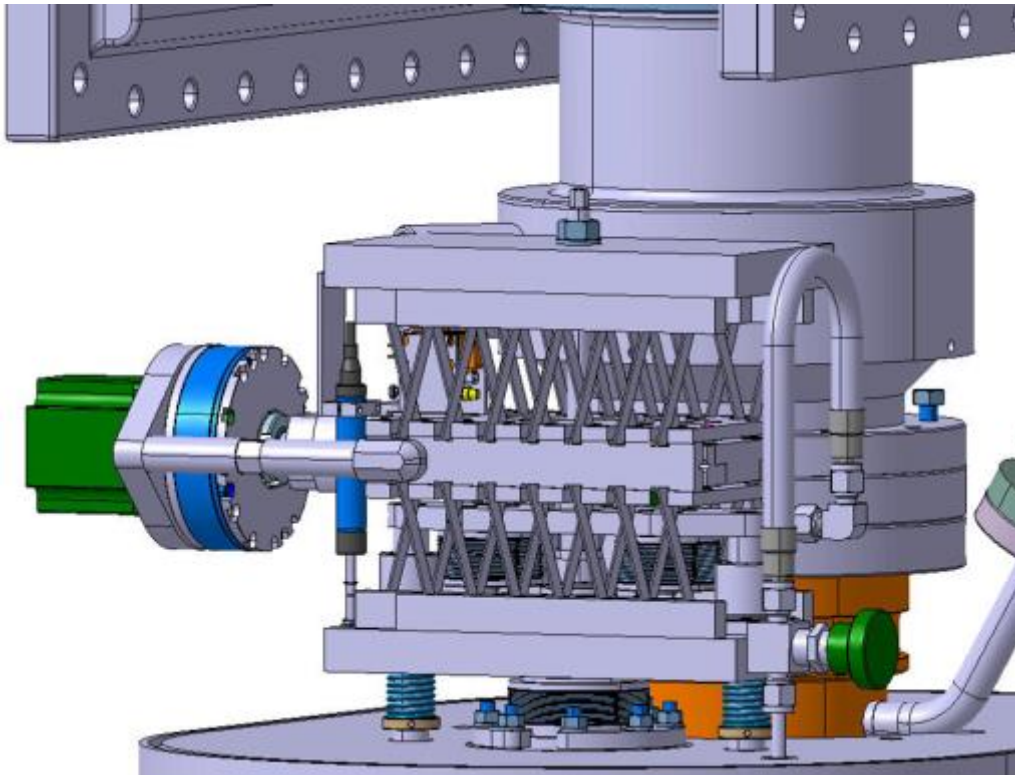
Design: P. Minginette



Size ok
Smaller mass
Can be
dismounted
from cryostat



Status design for SPS test (v2)



- Only concept so far
- Compact
- 10 to 20 times better resolution
- Centre of actuation is materialised
- Dismountable

Design: **P. Minginette**

Conclusions

- Calculations for DQW and RFD show the tuning ranges available that are smaller than the error on p.o.p.
- A first prototype of the tuner motorisation has been built, tests with p.o.p. DQW in preparation
- Options for the SPS tuner are under study, taking care of integration, resolution, pressure and load compensation and instrumentation
- To be included in study: radiation, thermal optimisation
- Test program to be prepared

- Thank you



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