

M_{ain} Q_{uadrupoles}

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FCC 2015 targets

	G (T/m)	B_{peak} (T)	Bore (mm)	Length (units x m)
MQ FCC	420	12	50	800 x 6.5
MQ LHC	223	6.5	56	392 x 3.2

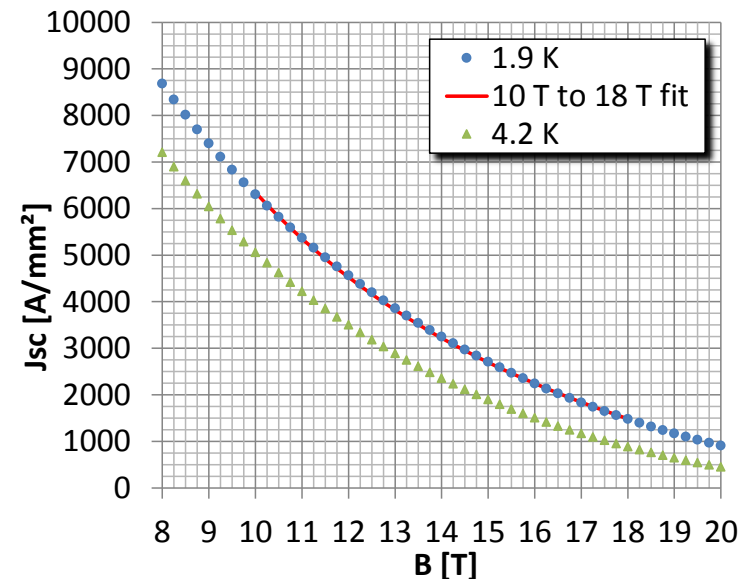
Number of apertures	(-)	2	2
Inter-aperture spacing	(mm)	250	194
Operating temperature	(K)	1.9	1.9
Margin along the loadline	(%)	20	20
Yoke OD max	(mm)	800	

SC density / cable features

- Specifications close to EuroCirCol project (16 T Nb₃Sn dipole)

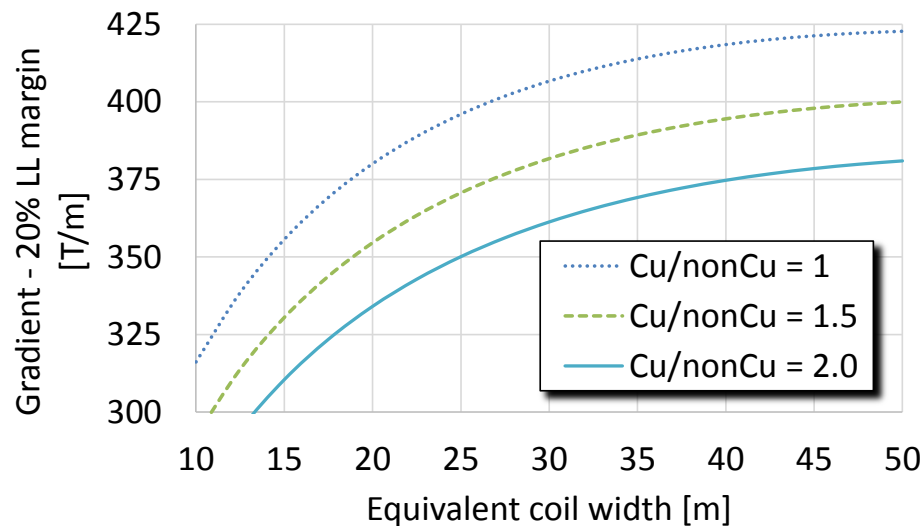
- Cable specifications
 - Strand diameter max: 1.1 mm
 - Number of strands max: 40
 - Cu/non-Cu ratio min: 1/1
- SC current density
 - 1500 A/mm² @ 16 T and 4.2 K
 - 2250 A/mm² @ 16 T and 1.9 K
 - Hyperbolic fit for scaling law

$$J_{sc}(B) = a \left(\frac{b}{B} - 1 \right) \text{ with } a = 4600 \text{ A/mm}^2, b = 23.8 \text{ T}$$



Equivalent coil width vs gradient

- What the scaling law* provides:
 - no gain in [T/m] beyond 45 mm eq. coil width
 - protection drives the design: Cu/nonCu vs amount of conductor
 - at first glance, can go beyond 380 T/m



*Todesco et al, Semi-analytical approaches to magnet design, Wamsdo 2013

Rossi L., Todesco E. Electromagnetic design of superconducting quadrupoles, PRSTAB, 2006

2 Nb₃Sn layers – version 1

- Protection $T_{\text{hotspot}} < 350 \text{ K}$ @ 105% of I_{nominal}
- Triggering time (15 ms) + QH delay (25 ms)
 - Cu/nonCu = 2.2
 - $I_n = 24100 \text{ A}$
 - $G = 364 \text{ T/m}$
 - $J_{\text{overall}} = 716 \text{ A/mm}^2$
 - Bare cable width = 15.75 mm

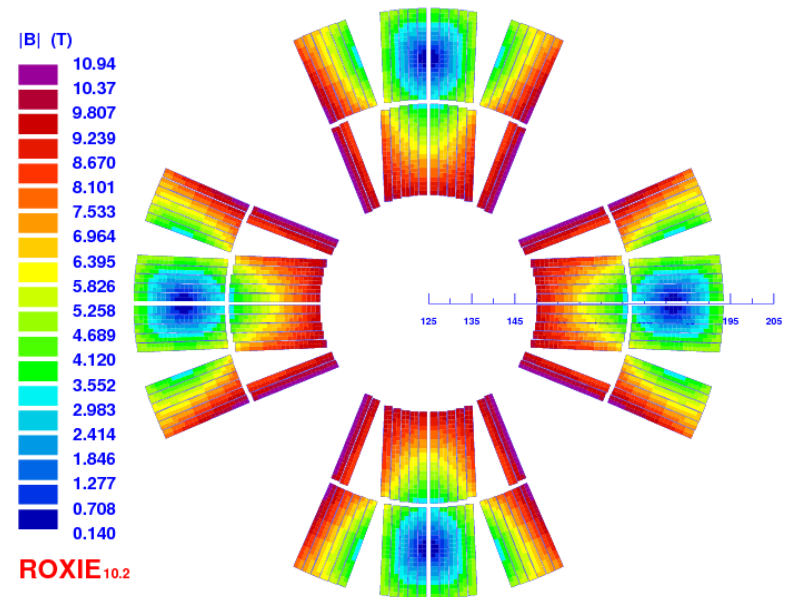
-> 2 layer designs lead to high Cu/nonCu ratio for protection



[based on Mikko Karppinen's design]

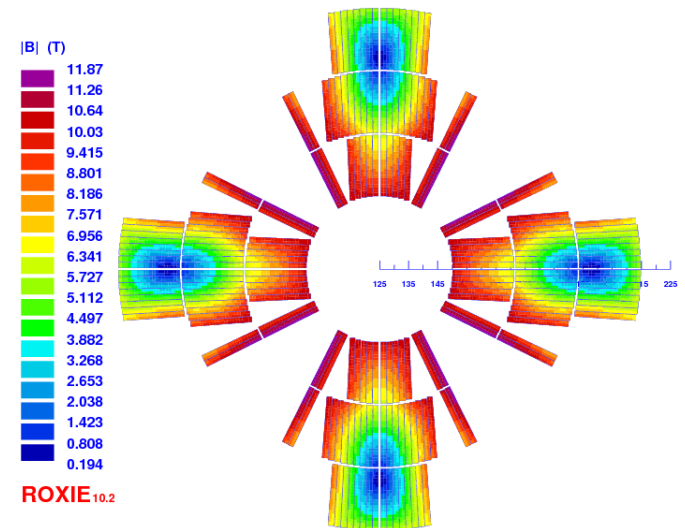
2 Nb₃Sn layers – version 2

- Protection $T_{\text{hotspot}} < 350 \text{ K @ } 105\% \text{ of } I_{\text{nominal}}$
- Triggering time (15 ms) + QH delay (25 ms)
 - Cu/nonCu = 1.8
 - $I_n = 29900 \text{ A}$
 - $G = 390 \text{ T/m}$
 - $J_{\text{overall}} = 680 \text{ A/mm}^2$
 - Bare cable width:
 - 21.0 mm (Fresca2-like cable)



3 Nb₃Sn layers – version 3

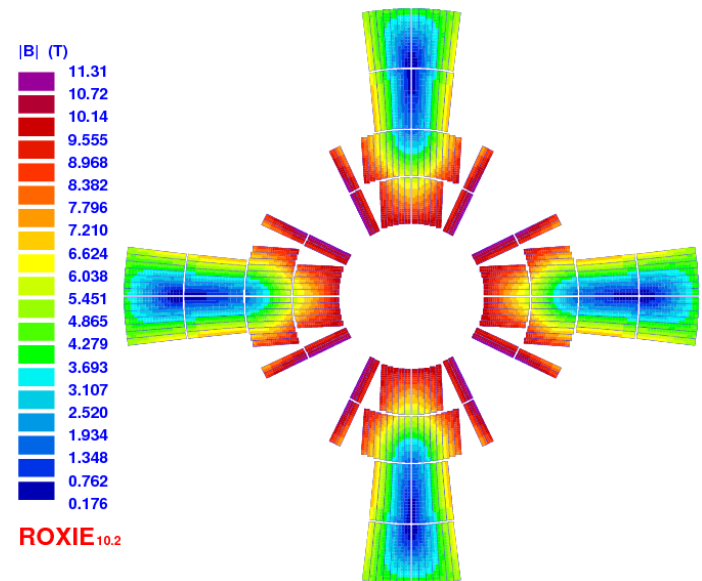
- Protection $T_{\text{hotspot}} < 350 \text{ K @ } 105\% \text{ of } I_{\text{nominal}}$
- Triggering time (15 ms) + QH delay (25 ms)
 - Cu/nonCu = 1.55
 - $I_n = 27260 \text{ A}$
 - $G = 413 \text{ T/m}$
 - $J_{\text{overall}} = 610 \text{ A/mm}^2$
 - Bare cable width:
 - 21.0 mm (Fresca2-like cable)



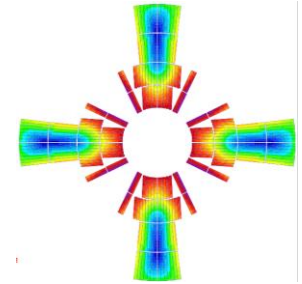
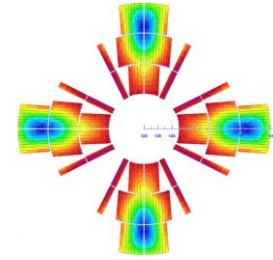
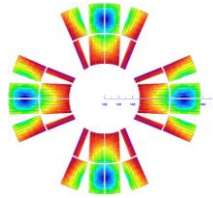
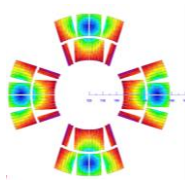
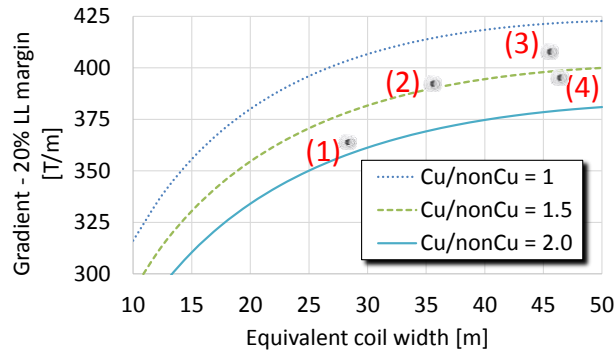
[Ezio Todesco's design]

2 Nb₃Sn layers + 2 Nb-Ti layers – v4

- Protection $T_{\text{hotspot}} < 350 \text{ K}$ @ 105% of I_{nominal}
- Triggering time (15 ms) + QH delay (25 ms)
 - $\text{Cu/nonCu} = 1.95_{\text{Nb}_3\text{Sn}} - 1.05_{\text{Nb-Ti}}$
 - $I_n = 21200 \text{ A}$
 - $G = 392 \text{ T/m}$
 - $J_{\text{copper}} = 630_{\text{Nb}_3\text{Sn}} - 450_{\text{Nb-Ti}} \text{ A/mm}^2$
 - Bare cable width:
 - $15.75_{\text{Nb}_3\text{Sn}} - 20.2_{\text{Nb-Ti}} \text{ mm}$



Summary design options



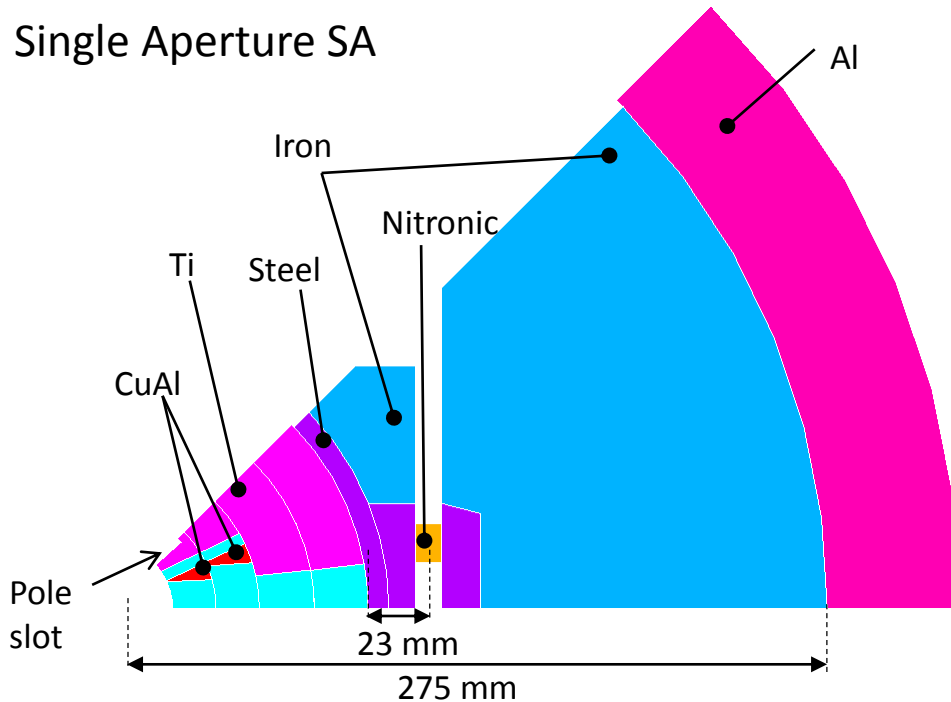
	Units	v1 Nb ₃ Sn	v2 Nb ₃ Sn	v3 Nb ₃ Sn	v4 Nb ₃ Sn	Nb-Ti
Gnom	T/m	365	390	413	392	
Inom	A	24100	29900	27260	21200	
Bpeak	T	10.07	10.94	11.87	11.31	
Ind. diff (2 ap)	mH/m	1.77	1.87	4.08	5.26	
Stored energy (2 ap)	kJ/m	617	843	1533	1216	
Φ x nb strands	mm x adim	1.0 x 30	1.0 x 40	1.0 x 40	1.0 x 30	1.065 x 38
Cu/nonCu		2.2	1.8	1.55	1.95	1.05
Est. length	m	7.4	6.9	6.5	6.9	
Est. quantity of cond.	tons	330	435	590	330	+ 318



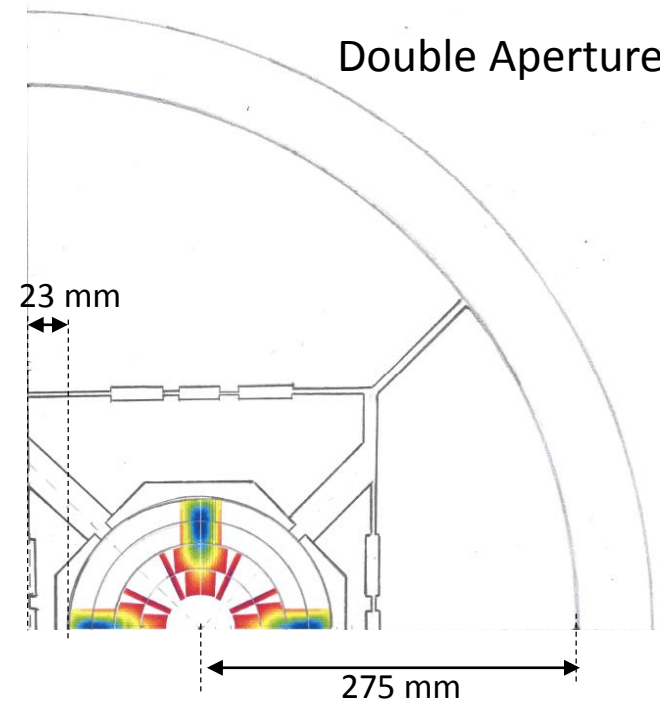
1 m shorter quad -> 1% more filling factor for dipoles -> 1 % more margin on dipoles -> ~300-500 tons saved on dipoles

Single aperture model – v4 (1/4)

Single Aperture SA



Double Aperture DA



- SA yoke radius = 275 mm

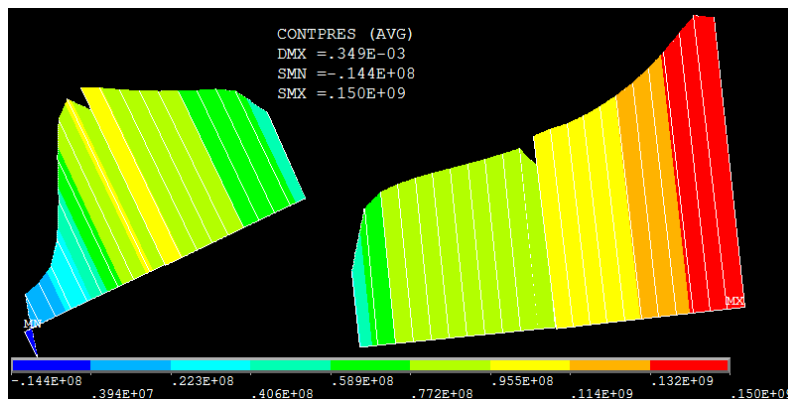
- distance between aperture center and shell in the DA configuration

- SA distance outer coil to middle of the key = 23 mm

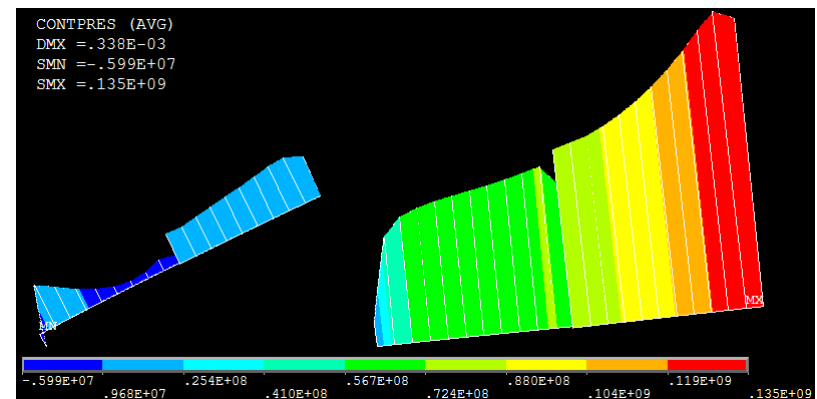
- distance between outer coil and center of the DA configuration

- Mechanical properties similar for Nb₃Sn and Nb-Ti coils
- Key: 400 μm extra size
- Shell: 51 mm
- Contact coil-pole at 105 % of $I_{\text{nominal}} = 21200 \text{ A}$ (22260 A)

Cool-down



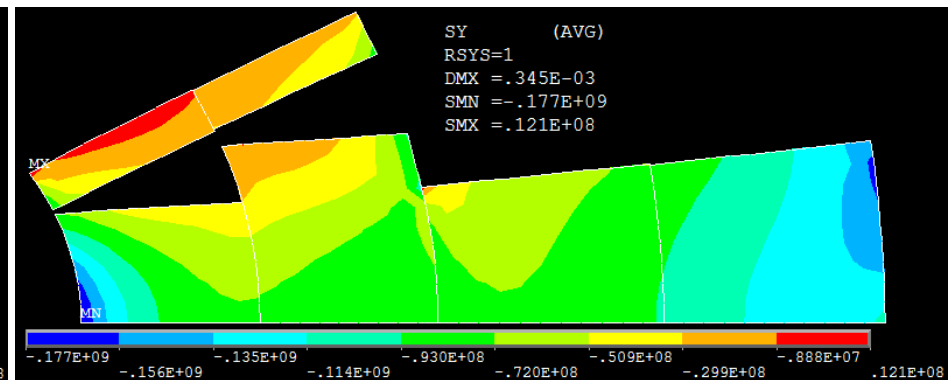
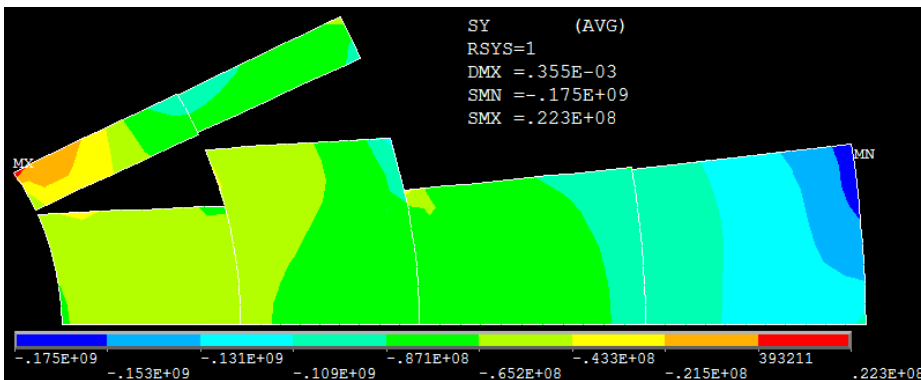
Powering at 105 %



- Azimuthal stress in the coil: 180 MPa
 - ~70 MPa at warm. (not shown)
- Radial stress in the coil: 110 MPa at cold (not shown)

Azimuthal stress: cool-down

Azimuthal stress: powering at 105 %

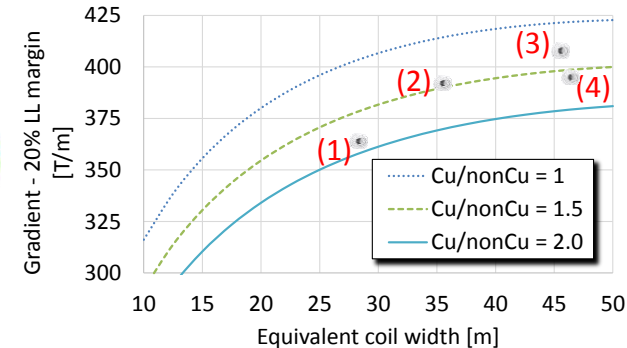
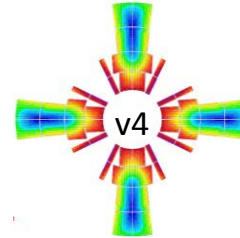
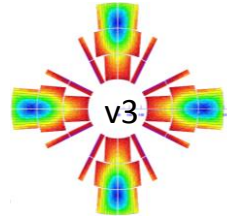
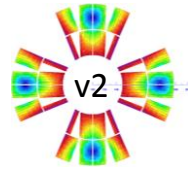
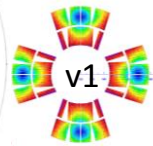
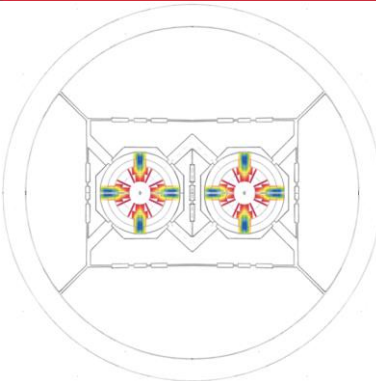


Single aperture model – v4 (4/4)

Von mises [MPa]	Material	Key insertion	Cool-down	Powering 105%
Pole	Ti6Al4V	184	324	278
Collar	316LN	131	355	378
Pad	Iron	42	205	203
Yoke	Iron	74	188	190
Key support	316LN	193	635	641
Key	Nitronic40®	404	1280	1300
Shell	AL 7075	124	251	260

- Peak stress values in the key corners can be reduced

Conclusion



- Quadrupole magnets with gradients from 365 to 415 T/m
- Quantity of conductor between 300 to 600 tons of Nb₃Sn (~5% of dipoles)
- Preliminary single aperture mechanics promising (double ap. tbc)
- Double aperture central part: shims or bladder&key?
- Magnet end windability (15.75 mm or 21 mm cable) →
- Development phase ideas:
 - Starting with v1 and v2 which are somehow the cores of v4 and v3
 - Then, if needed, go for v4 or v3 which are more complex design

