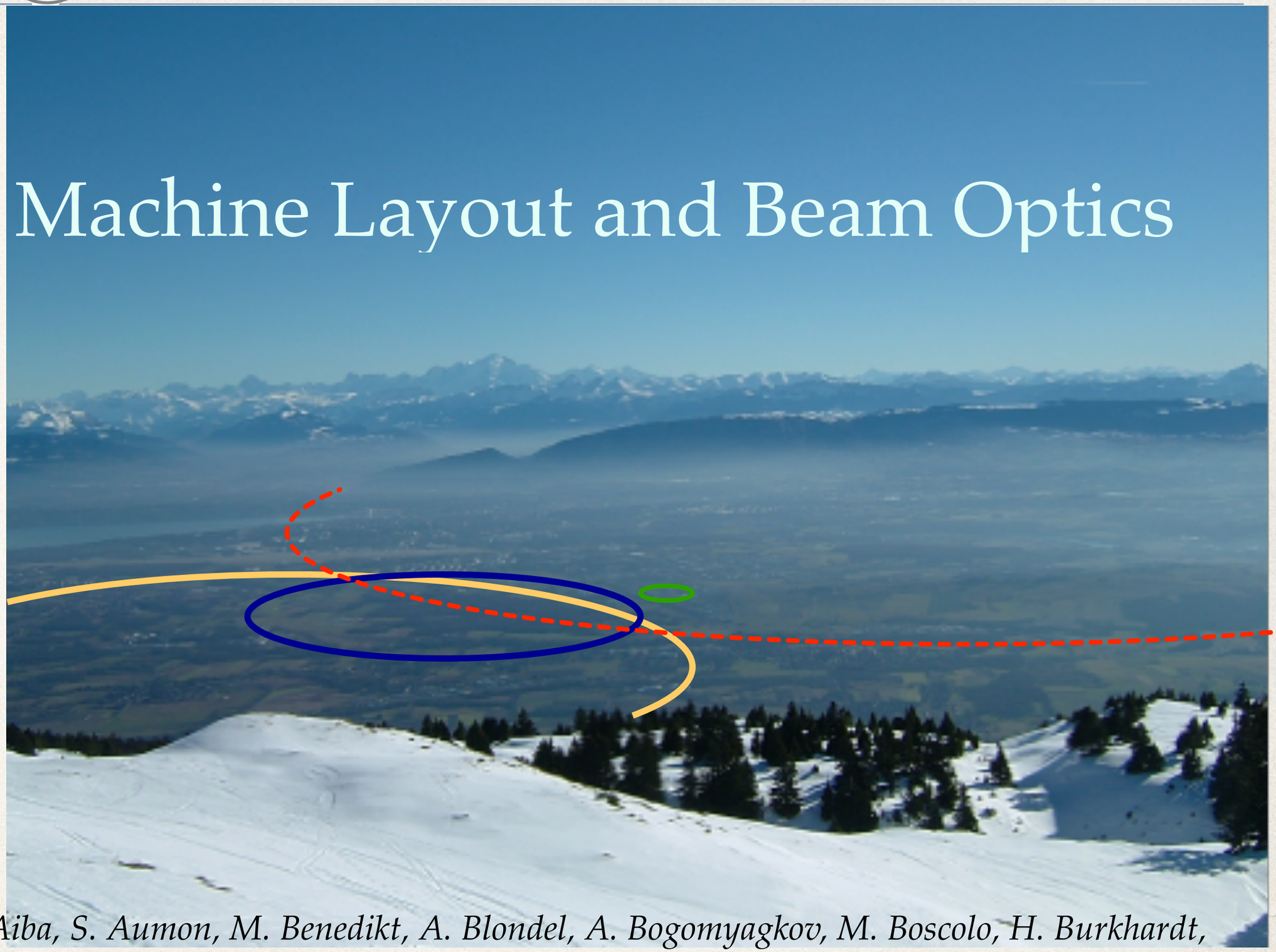
FCC-ee Machine Layout and Beam Optics



FCC Week 2016

11 Apr. 2016

Rome

K. Oide (KEK)

Contributed by M. Aiba, S. Aumon, M. Benedikt, A. Blondel, A. Bogomyagkov, M. Boscolo, H. Burkhardt, Y. Cai, A. Doblehammer, B. Haerer, B. Holzer, J. Jowett, I. Koop, M. Koratzinos, E. Levitchev, L. Medrano, K. Ohmi, Y. Papaphilippou, P. Piminov, D. Shatilov, S. Sinyatkin, M. Sullivan, D. Zhou, F. Zimmermann.

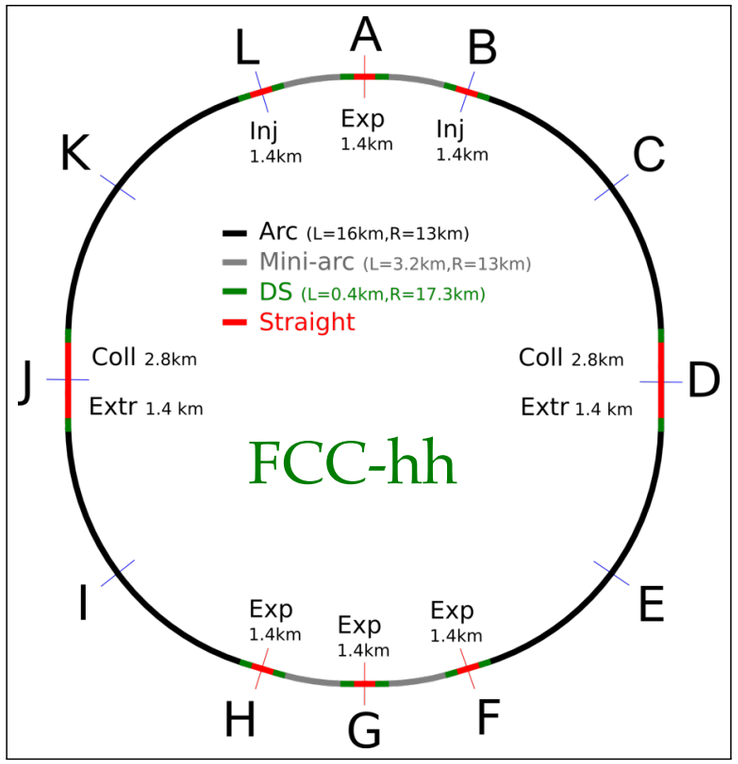
Design constraints & assumptions

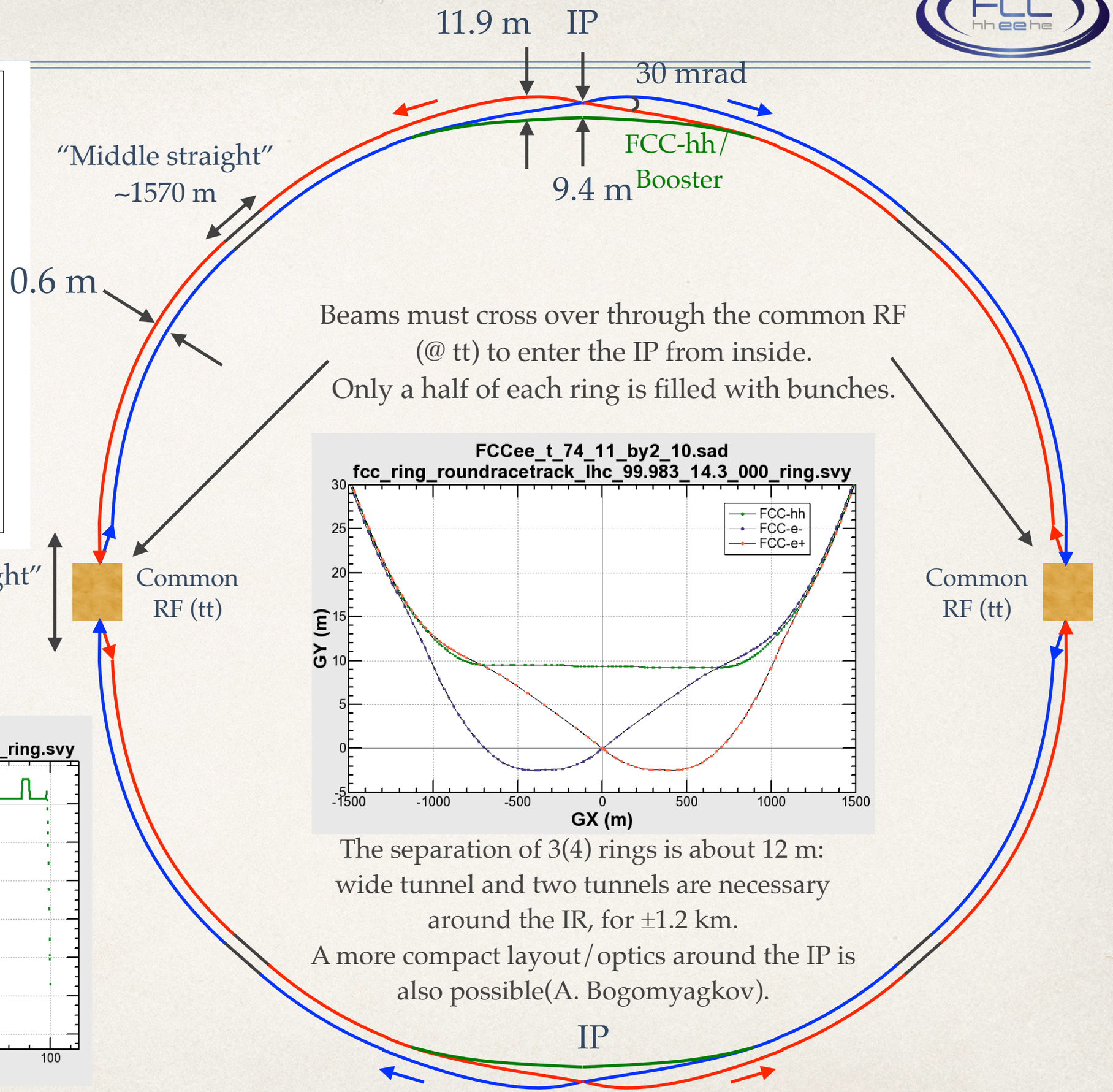
- C = 100 km, fits to the FCC-hh tunnel as much as possible.
- 2 IPs / ring.
- 30 mrad crossing angle at the IP with crab waist.
- Common lattice for all energies.
- $\varepsilon_x \leqq 1.3$ nm @ 175 GeV.
- ±2% momentum acceptance at 175 GeV.
- Vertical emittance less than 1 pm at 175 GeV.
- $\beta_{x,y}^* = (1\text{ m}, 2\text{ mm})$ at 175 GeV, (0.5 m, 1 mm) at 45.6 GeV.
- Suppress the synchrotron radiation to the IP below 100 keV, up to 500 m upstream (as suggested by H. Burkhardt).
- “tapering” to cure the sawtooth at high energy.

Parameters

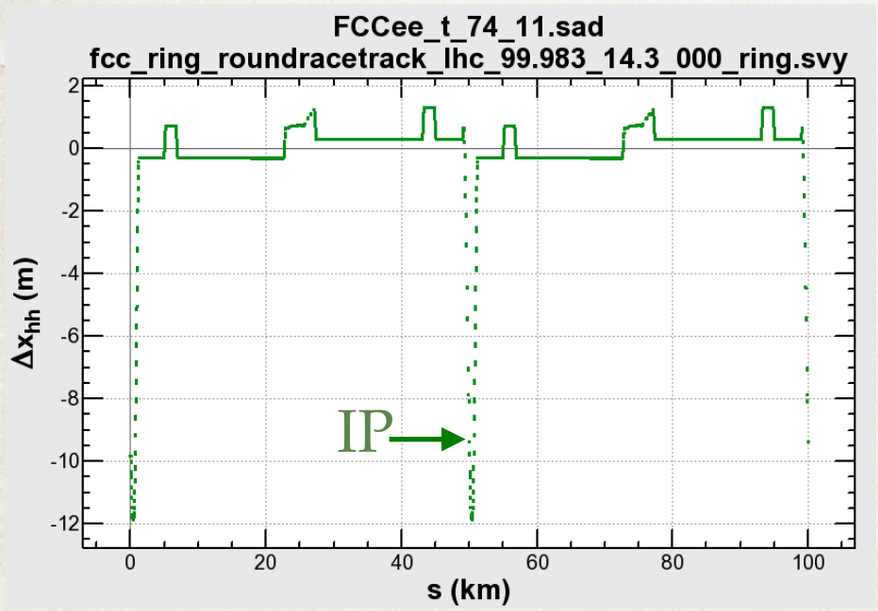
Circumference [km]	99983.76	
Number of IPs / ring	2	
Crossing angle at IP [mrad]	30	
Solenoid with compensation at IP	±2 T × 1 m	
ℓ^* [m] (asymmetric version)	2.2 / 2.9	
Critical energy of photons to IP	< 100 keV @ 175 GeV, up to 510 m upstream	
IR Optics	asymmetric	
Local chromaticity correction	Y	
Crab sexts	integrated with LCCS	
Arc cell	FODO, 90°/90°	
Arc sextuple families	292 (paired)	
mom. comp. [10^{-5}]	0.70	
Tunes (x/y)	387.08 / 387.14	
Ebeam [GeV]	**45.6**	**175**
SR energy loss per turn [GeV]	0.0346	7.47
Current / beam [mA]	1450	6.6
$P_{SR,tot}$ [MW]	100.3	98.6
ε_x [nm]	0.86	1.26
β^*_x [m]	0.5 (1)	1 (0.5)
β^*_y [mm]	1 (2)	2 (1)
RF frequency [MHz]	400	
$\sigma_{\delta,SR}$ [%]	0.038	0.141
$\sigma_{z,SR}$ [mm]	2.8 @ V_c = 78 MV	2.4 @ V_c = 9.04 GV
Synchrotron tune	-0.0158 @ V_c = 78 MV	-0.0657 @ V_c = 9.04 GV

Layout of FCC-ee



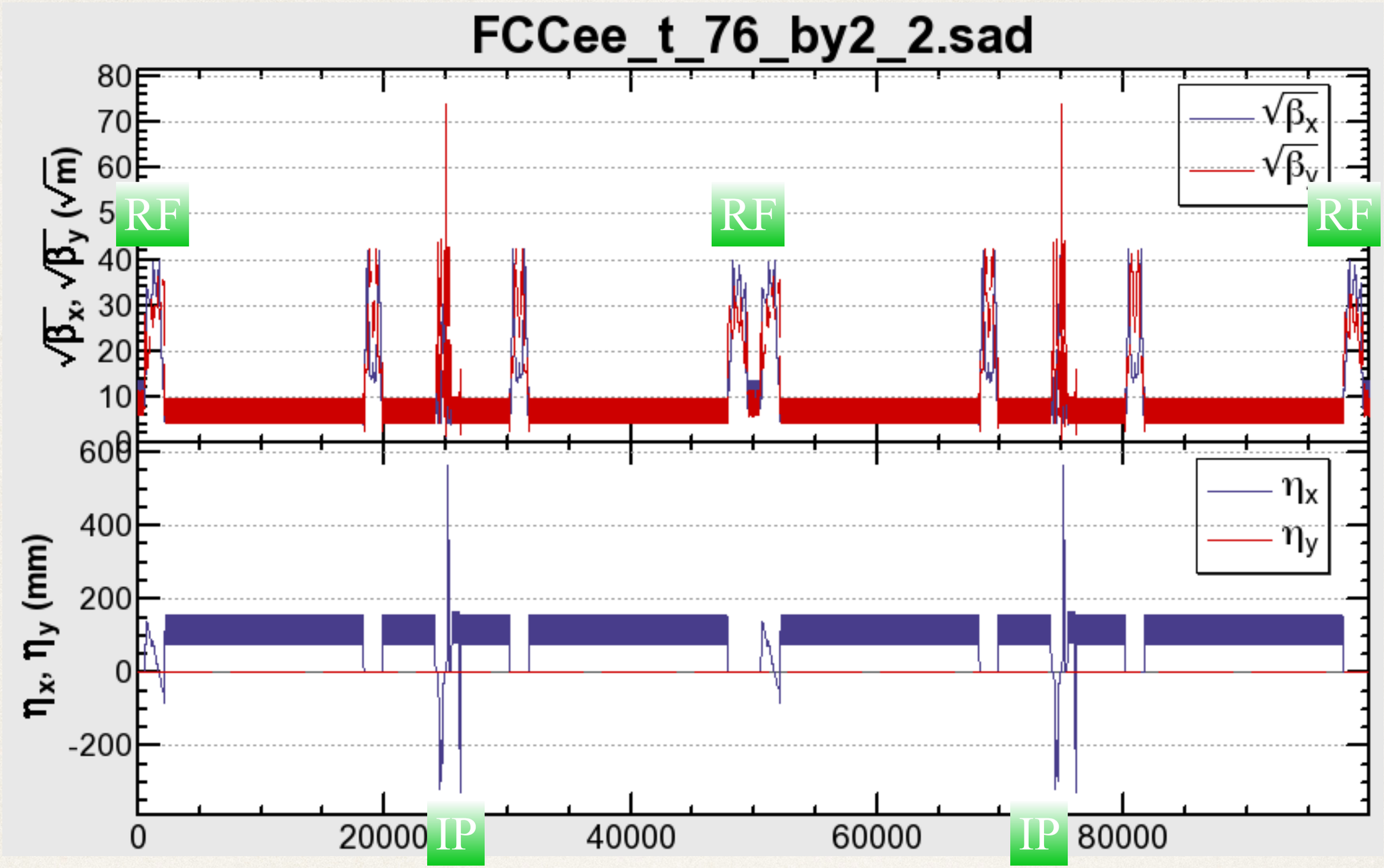


The separation of 3(4) rings is about 12 m:
wide tunnel and two tunnels are necessary
around the IR, for ±1.2 km.
A more compact layout/optics around the IP is
also possible(A. Bogomyagkov).



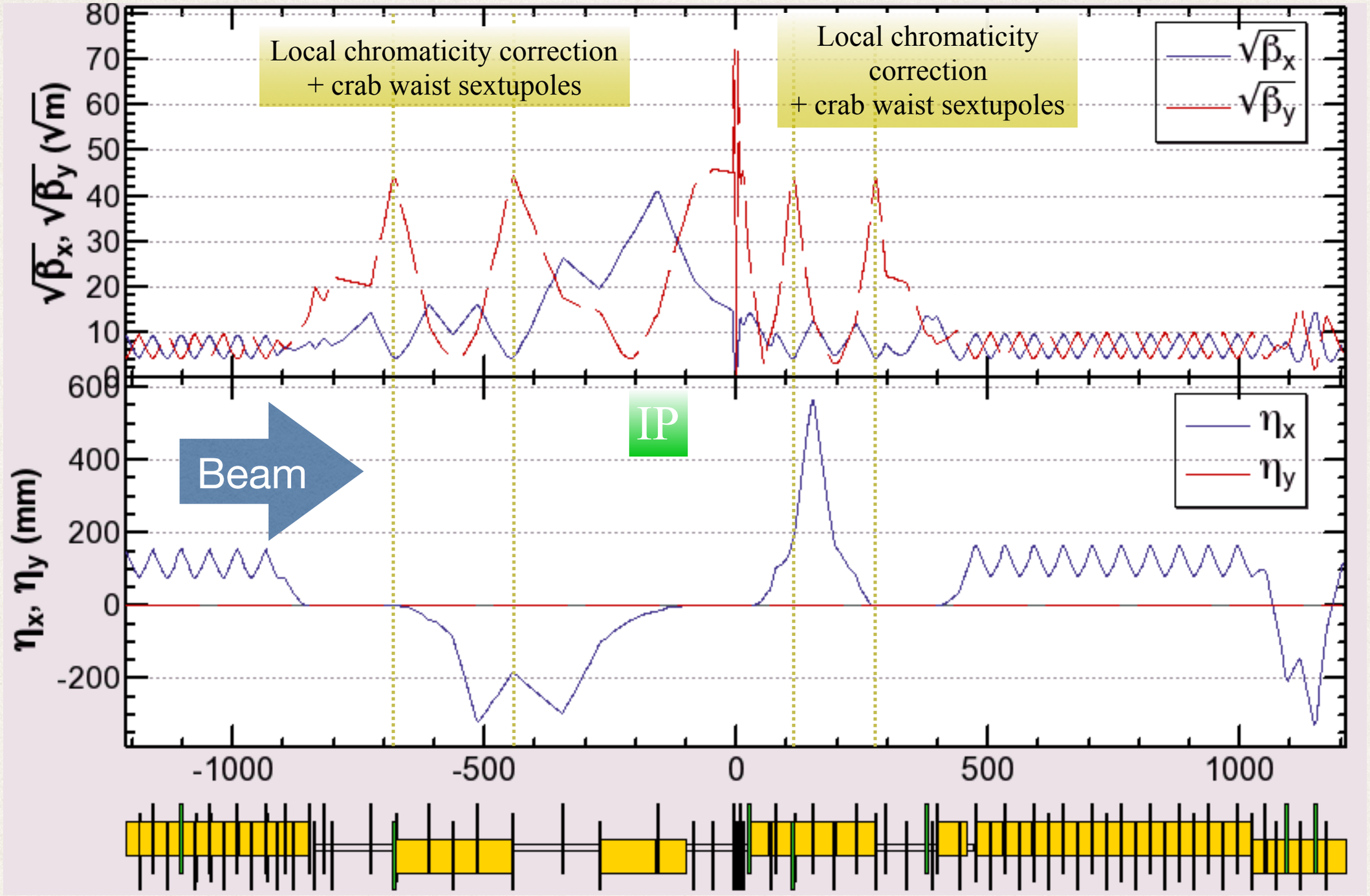
Relative distance to FCC-hh

Ring Optics



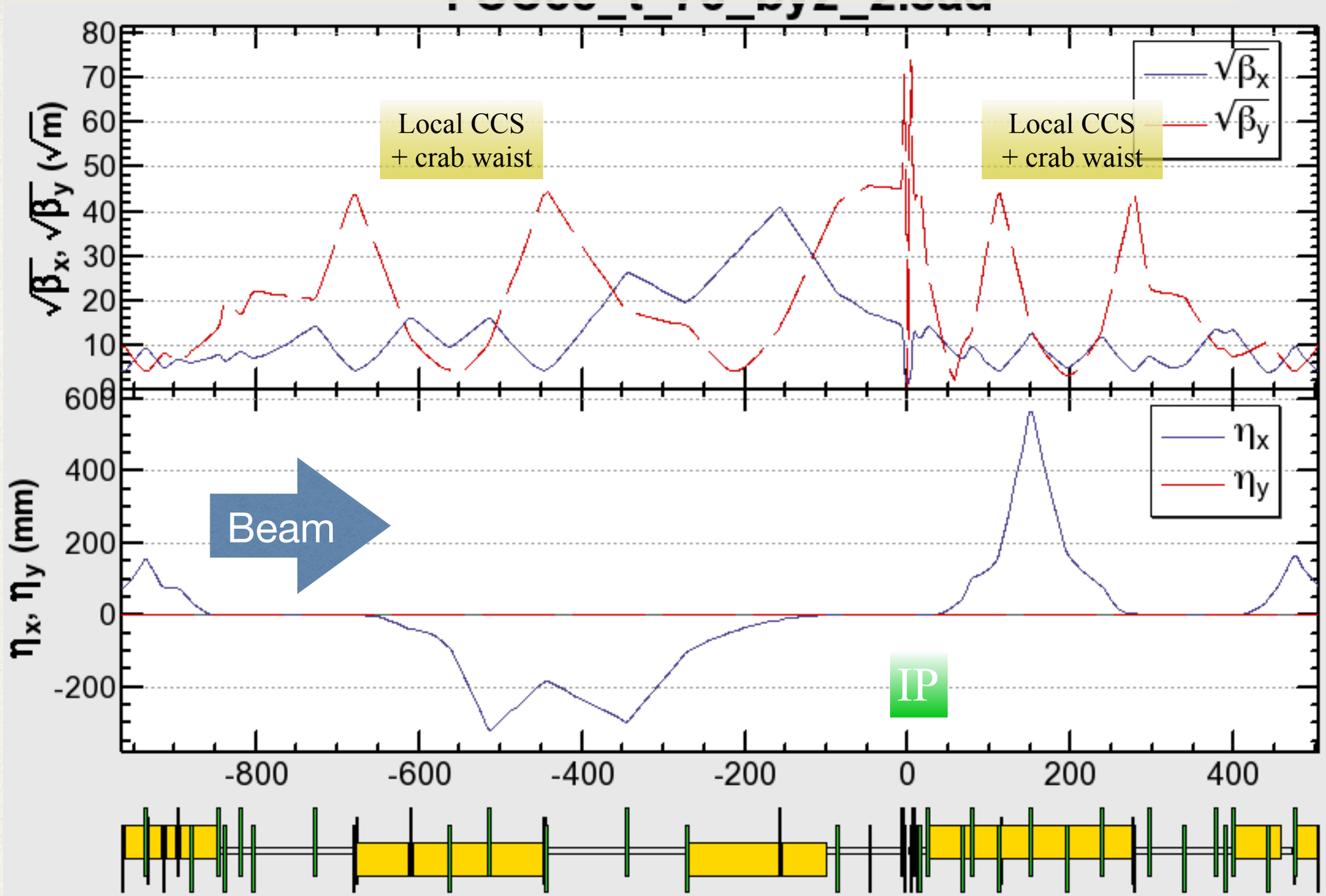
- Above are the optics for tt, $\beta^*_{x/y}$ = 1 m / 2 mm.
- 2 IP/ring.
- The optics for straight sections except for the IR are tentative, customizable for infection/ extraction/collimation, etc.

Interaction Region



- The optics in the interaction region are asymmetric.
- The synchrotron radiation from the upstream dipoles are suppressed below 100 keV up to 450 m from the IP.
- The crab sextuples are integrated in the local chromaticity correction in the vertical plane.

Synchrotron radiation toward the IP @ 175 GeV

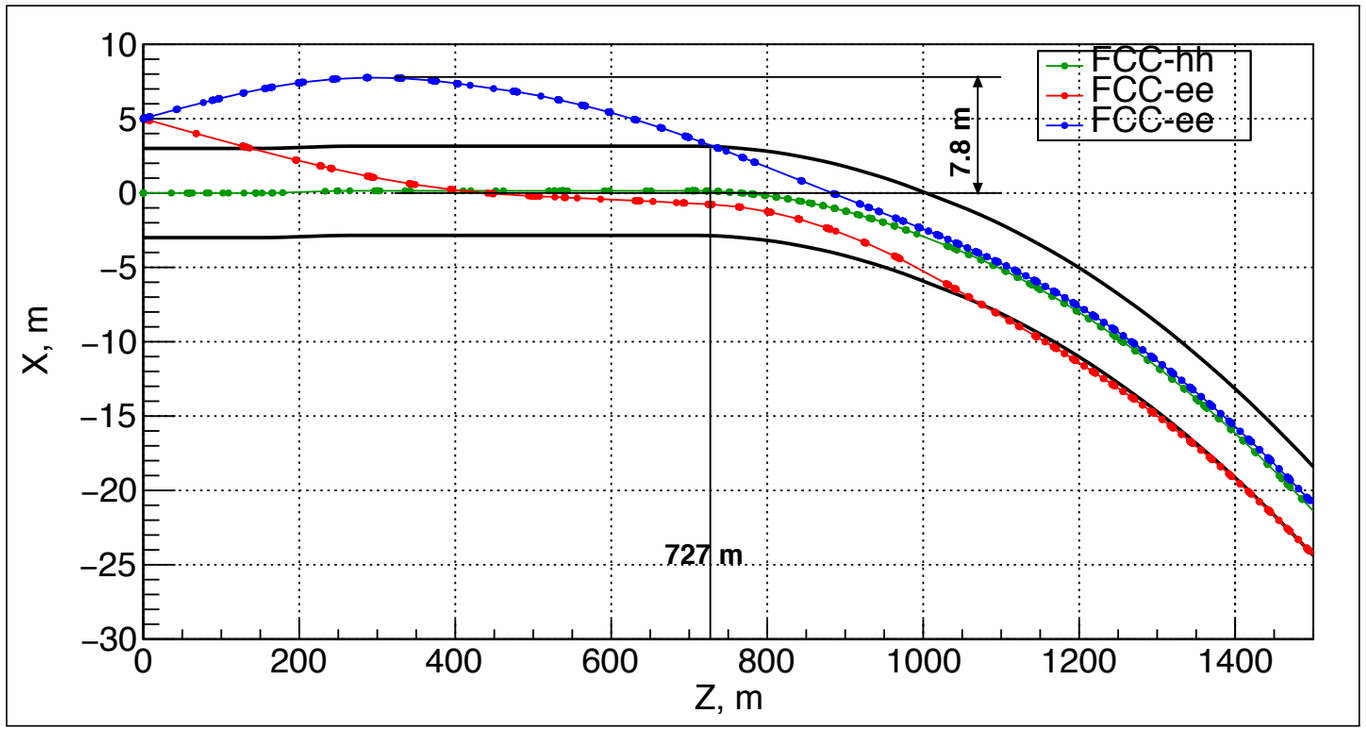


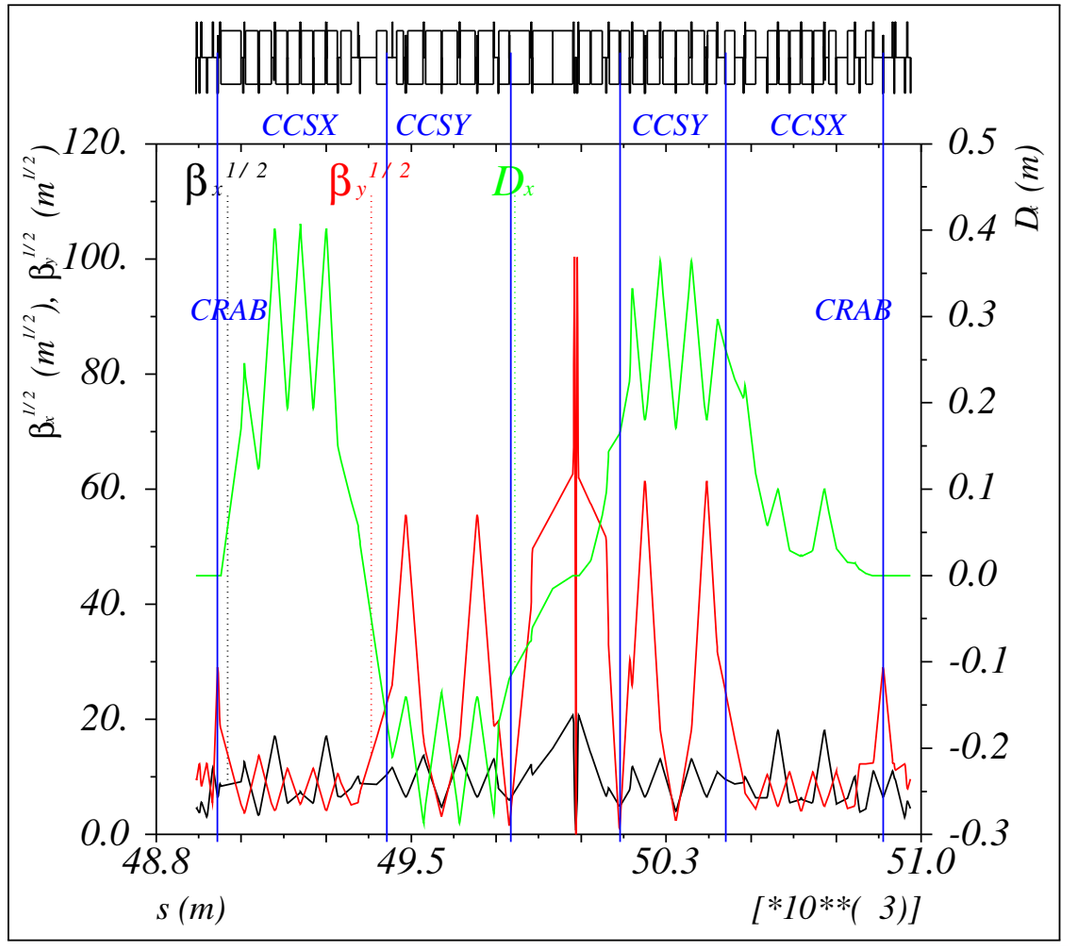
u_c (keV)	1062	930	204	449	292	9.1	100	100	691	1472	296	533
P_{SR} (kW)	16.6	15.3	1.7	5.4	2.3	0.003	0.67	0.34	11.2	38.7	1.9	6.9

$u_c < 100$ keV up to 510 m from the IP.

More compact IR (A. Bogomyagkov)

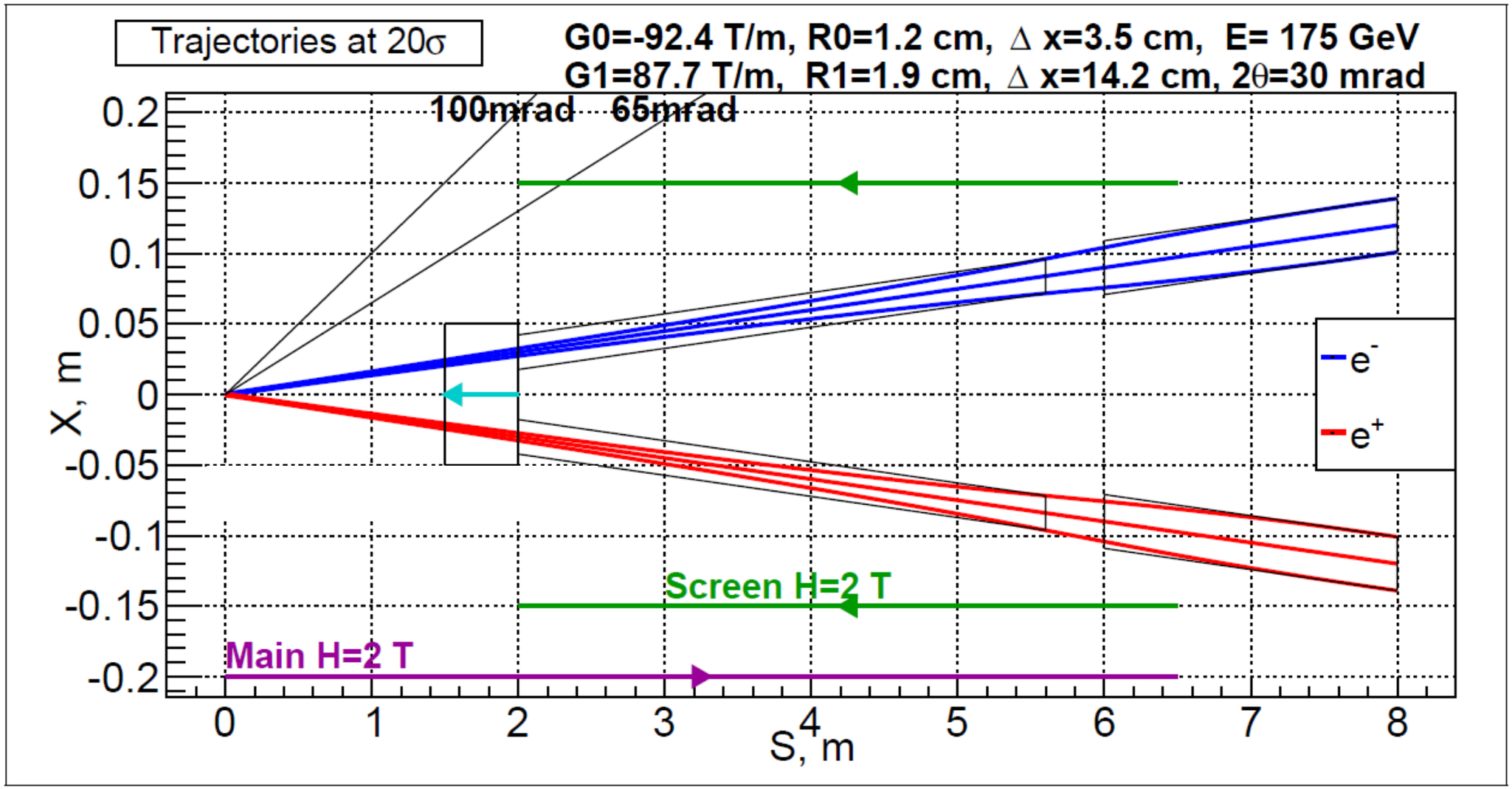
Interaction Region layout 30 mrad





- A more compact layout / optics (AB Lattice) has been developed by A, Bogomyagkov.
- The deviation from FCC-hh is reduced to 5 m (9.5 m), the maximum excursion 7.8 m (11.9 m), the wide tunnel region ±730 m (1,200 m).
- Local chromaticity correction for both X and Y can be installed.
- A stronger dipoles are necessary for upstream of the IP (100 keV up to ~200 m, 200 keV up to ~300 m).

Solenoid compensation / shielding at the IR

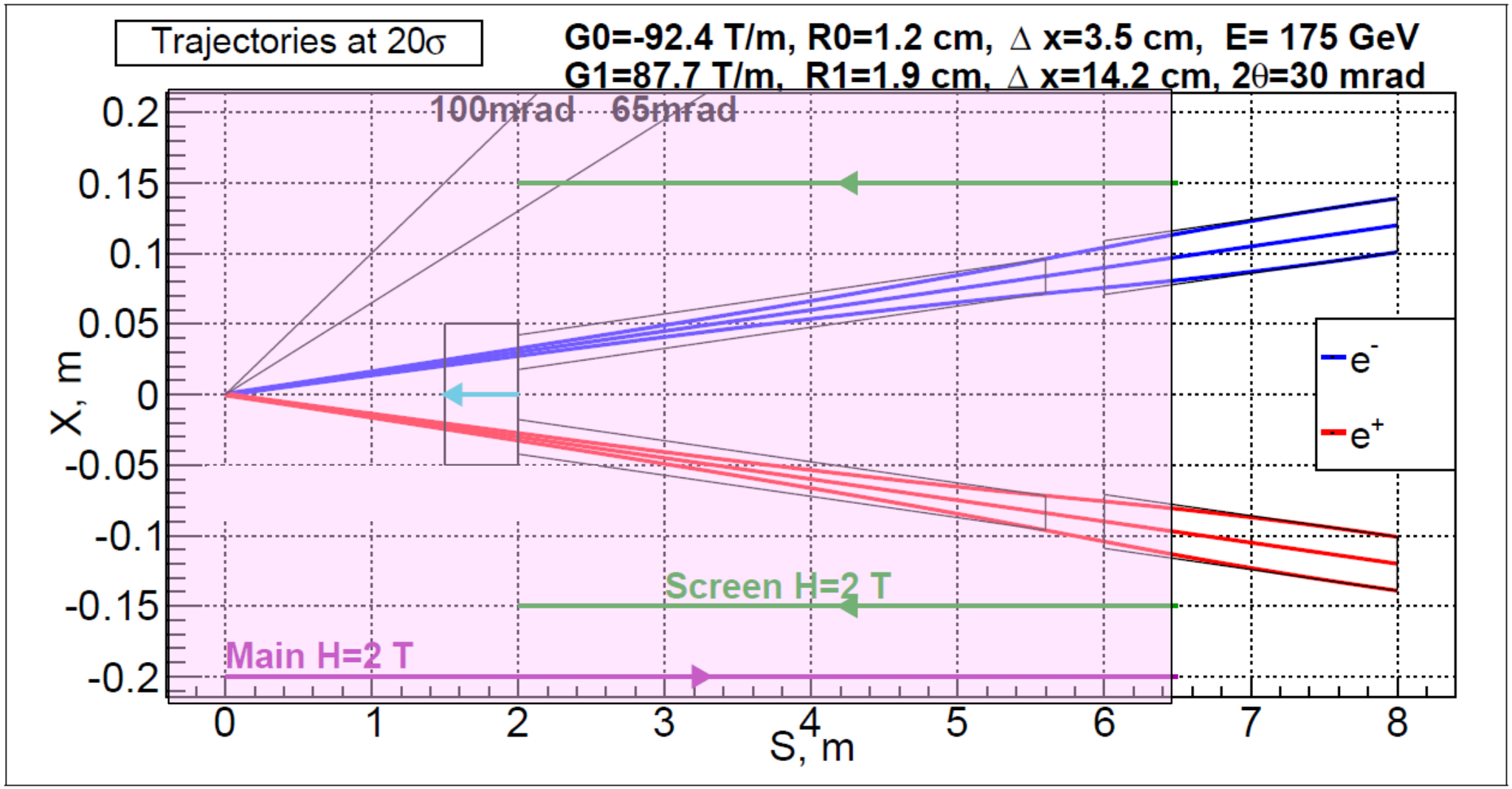


Favoured design at the moment. (it is not clear that a luminometer can fit inside the compensating solenoid)

- The effect of the solenoids are locally compensated within ±2 m around the IP.
- The final quads are shielded.

M. Koratzinos

Solenoid compensation / shielding at the IR



Main detector solenoid

Favoured design at the moment. (it is not clear that a luminometer can fit inside the compensating solenoid)

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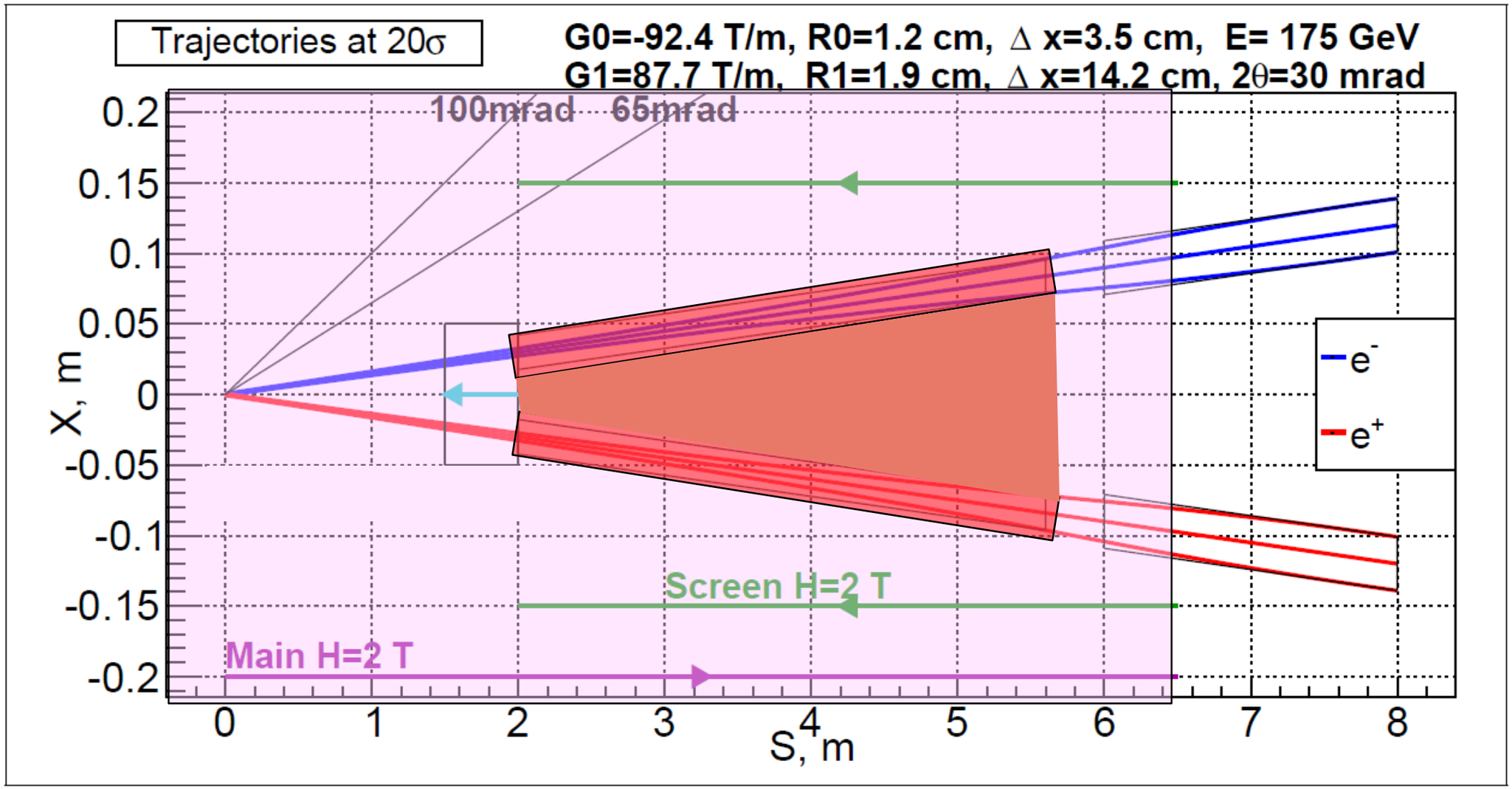

Final quads

Main detector solenoid

Favoured design at the moment. (it is not clear that a luminometer can fit inside the compensating solenoid)

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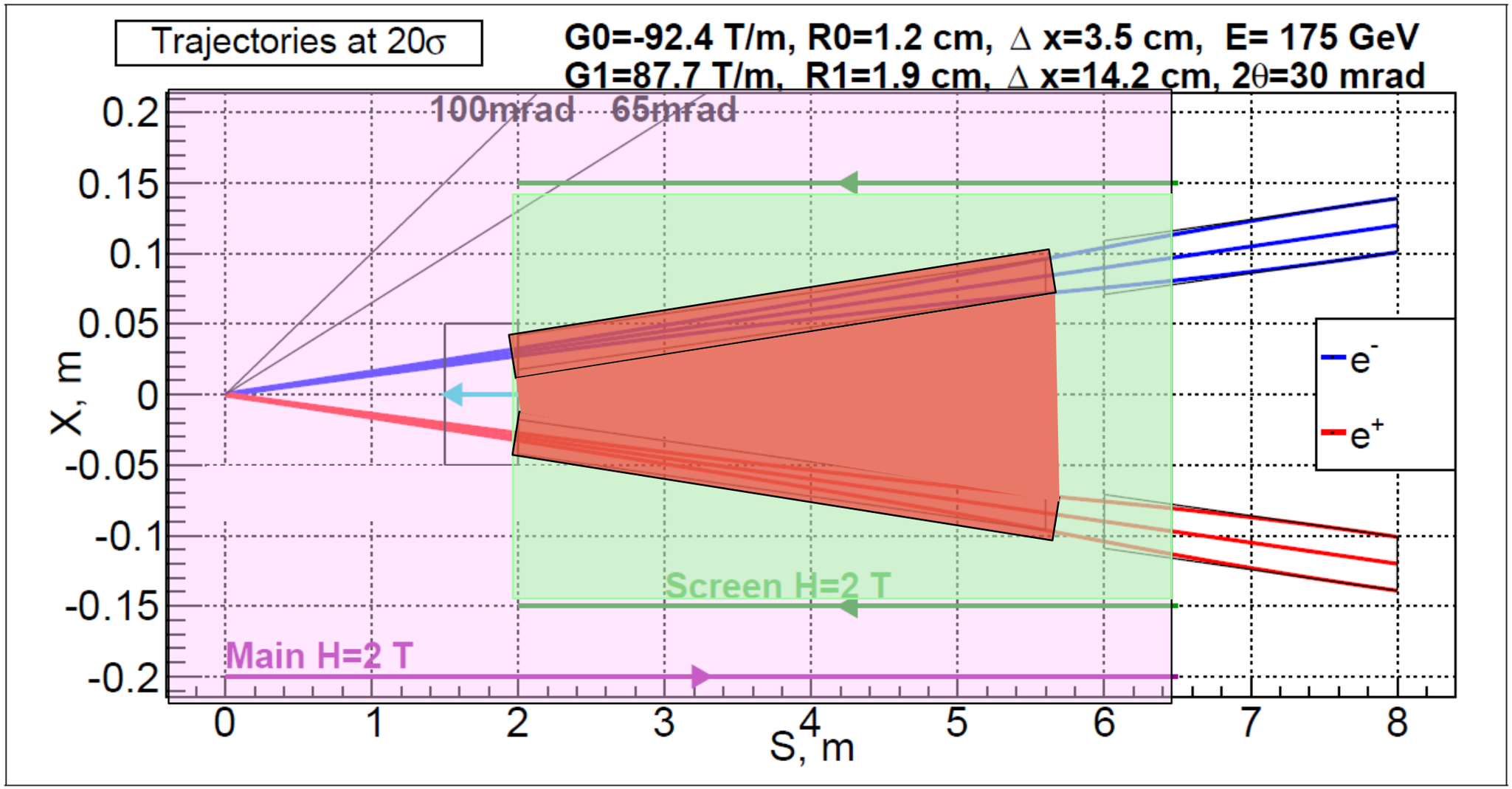
- The final quads are shielded.

M. Koratzinos

Solenoid compensation / shielding at the IR



Final quads

Main detector solenoid

Quad screening solenoid

Favoured design at the moment. (it is not clear that a luminometer can fit inside the compensating solenoid)

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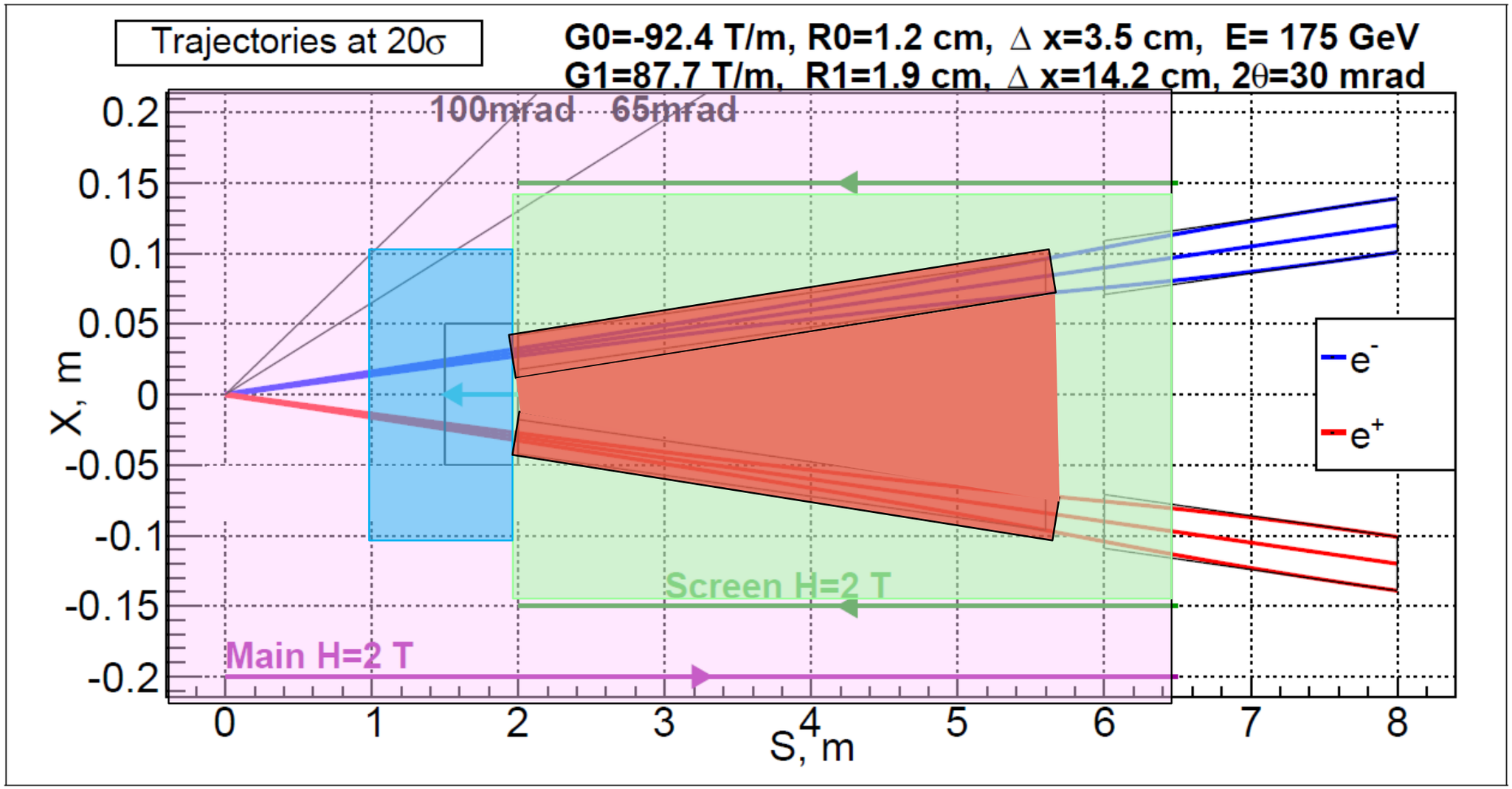
- The final quads are shielded.

M. Koratzinos

Solenoid compensation / shielding at the IR



Final quads

Main detector solenoid

Quad screening solenoid

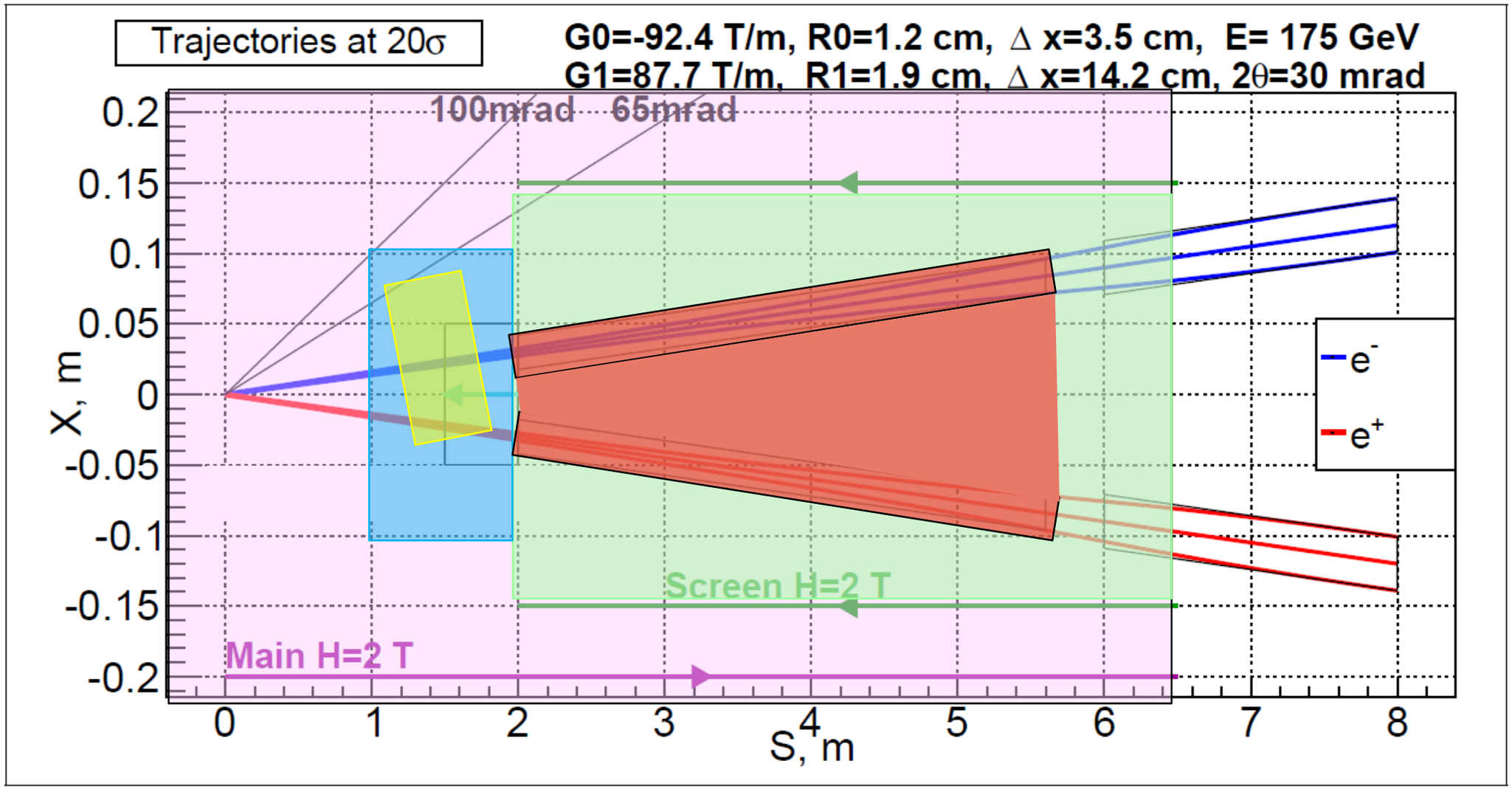
Compensating solenoid, -4T

Favoured design at the moment. (it is not clear that a luminometer can fit inside the compensating solenoid)

- The effect of the solenoids are locally compensated within ±2 m around the IP.
- The final quads are shielded.

M. Koratzinos

Solenoid compensation / shielding at the IR



Final quads

Main detector solenoid

Quad screening solenoid

Compensating solenoid, -4T

Luminosity counter?

Favoured design at the moment. (it is not clear that a luminometer can fit inside the compensating solenoid)

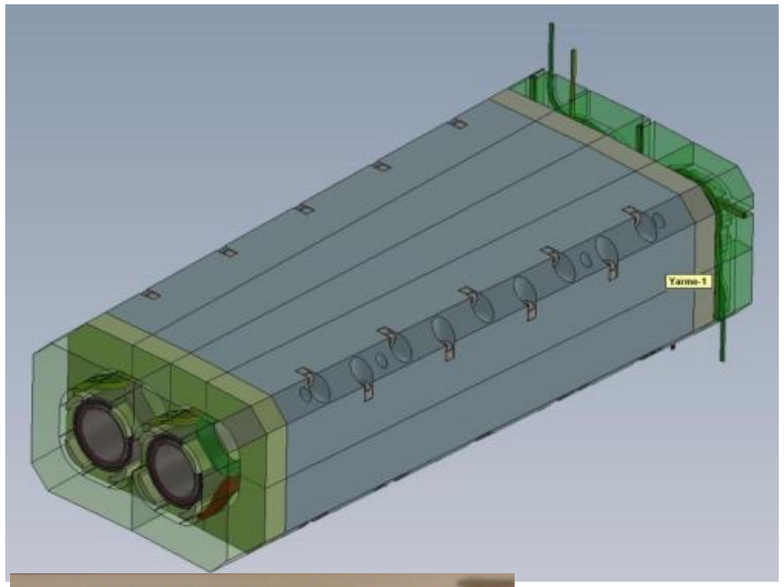
- The effect of the solenoids are locally compensated within ±2 m around the IP.
- The final quads are shielded.

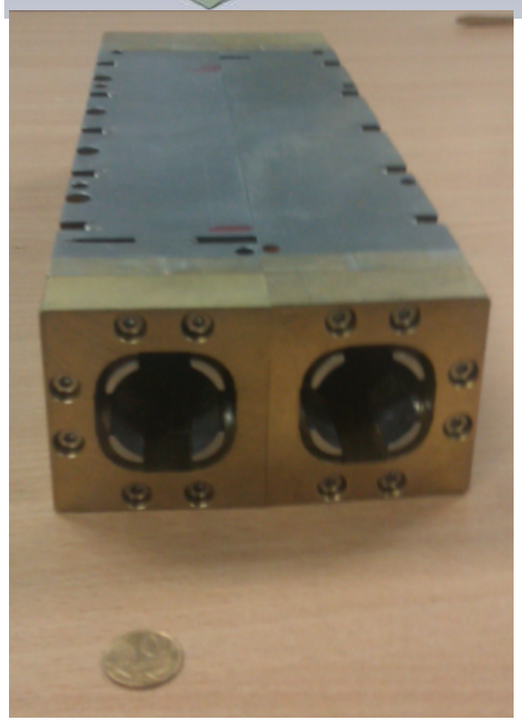
M. Koratzinos

SC final focus quadrupole at BINP

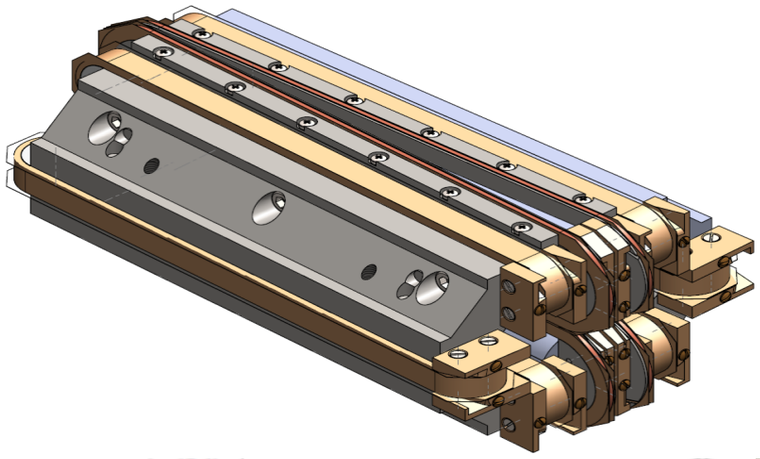
Main contributors are Ivan Okunev and Pavel Vobly

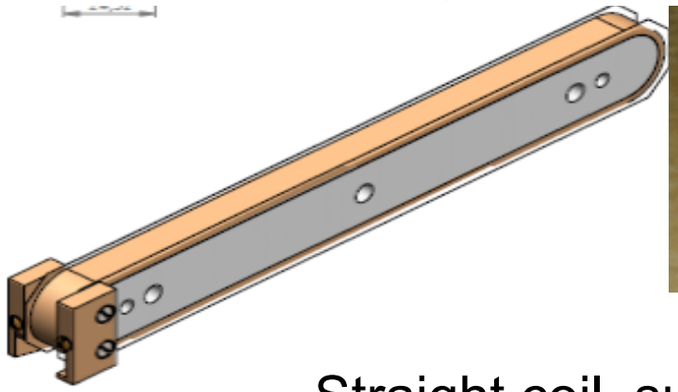
Two versions of the FF twin-aperture iron yoke quad prototype with 2 cm aperture and 100 T/m gradient are in production.

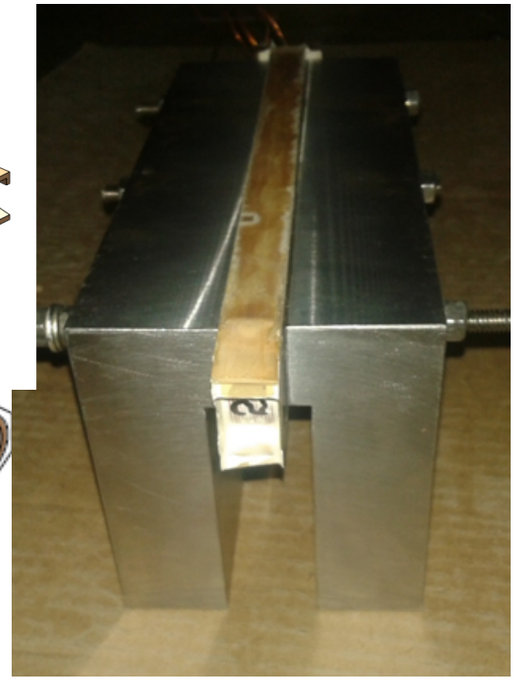




Saddle-shaped coils, complicated in production, the first coil failed. New winding device is in development.







Straight coil, successfully wound and tested (650 A instead of the nominal 400 A)

SC final focus quadrupole at BINP

Main contributors are Ivan Okunev and Pavel Vobly

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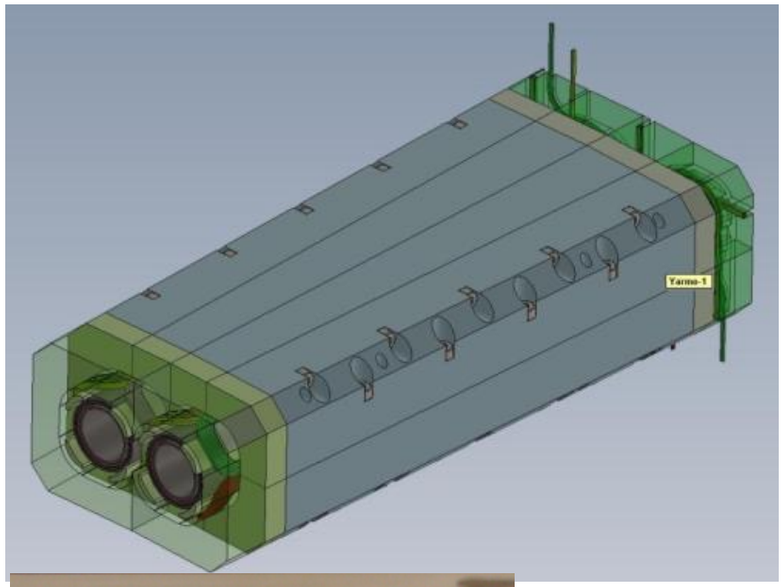

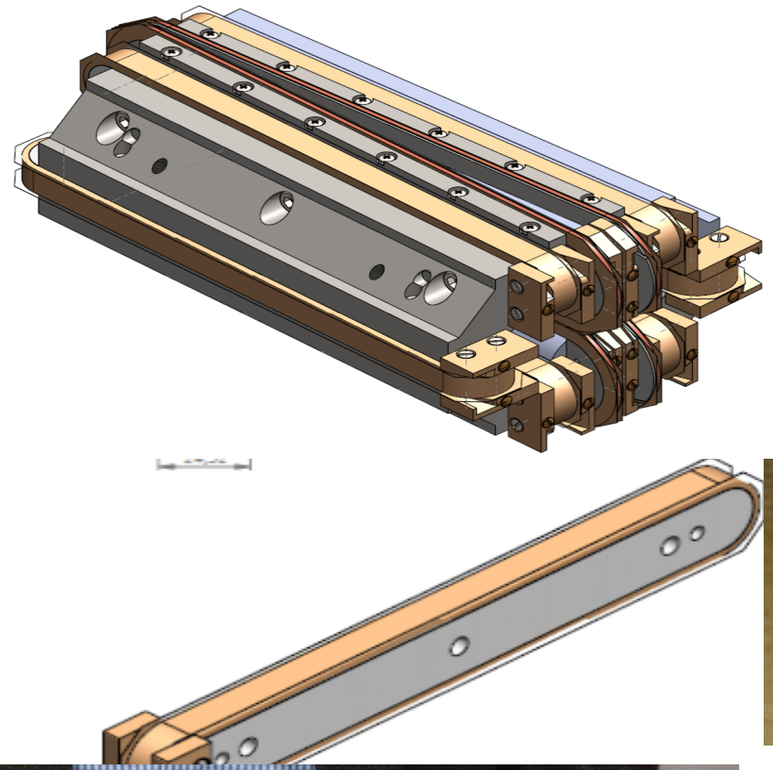

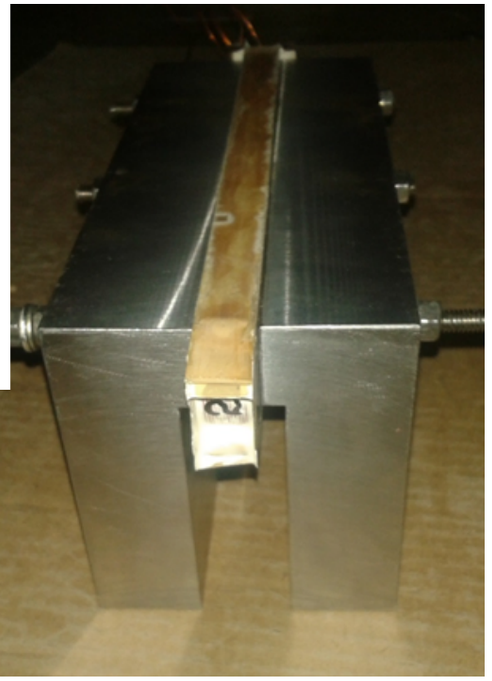

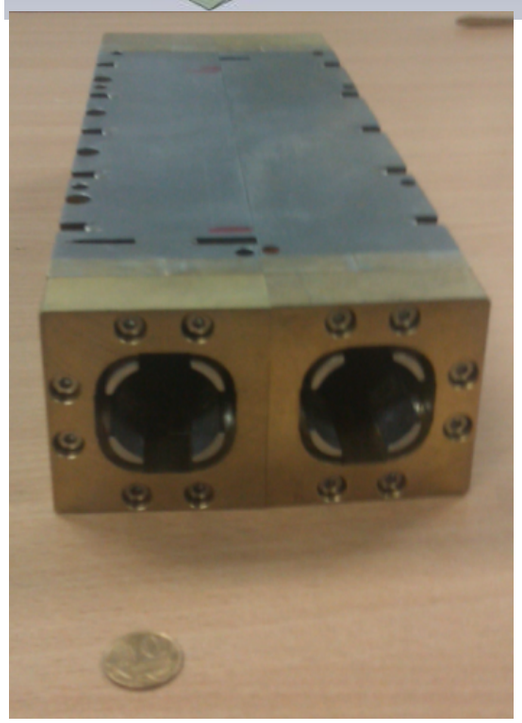

Saddle-shaped coils
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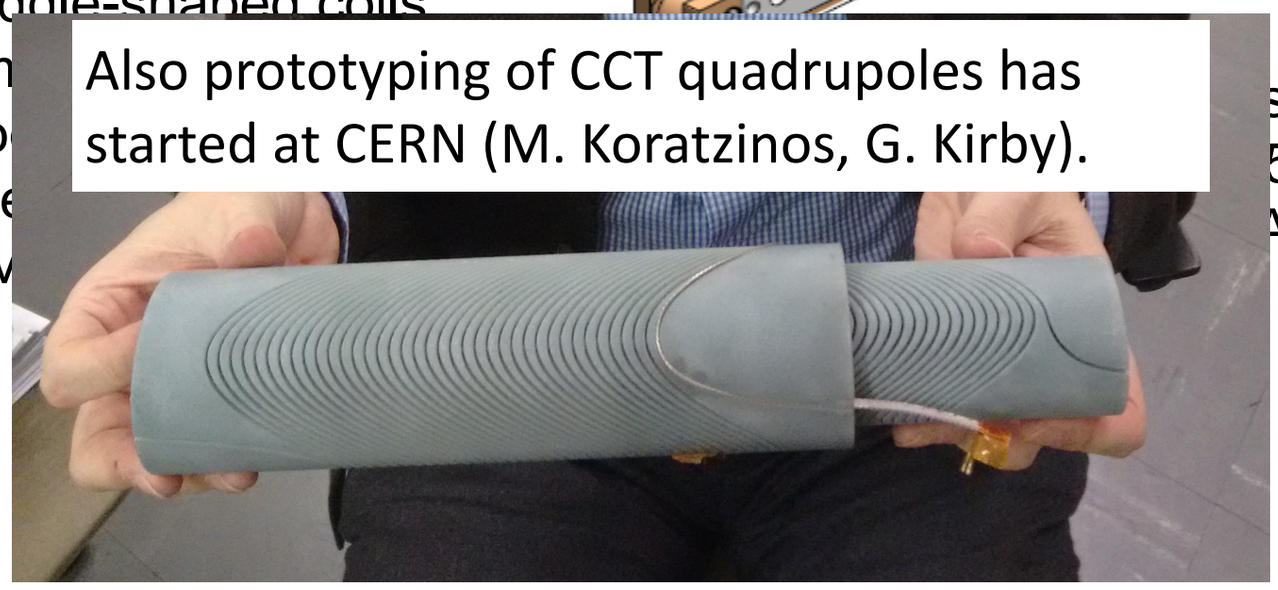
successfully wound
50 A instead of the
A)

Also prototyping of CCT quadrupoles has started at CERN (M. Koratzinos, G. Kirby).



Another QD0 prototype

A new version of QD0 was developed at BINP recently and a single-aperture prototype was manufactured.

Main parameters:

Max.gradient 100 T/m

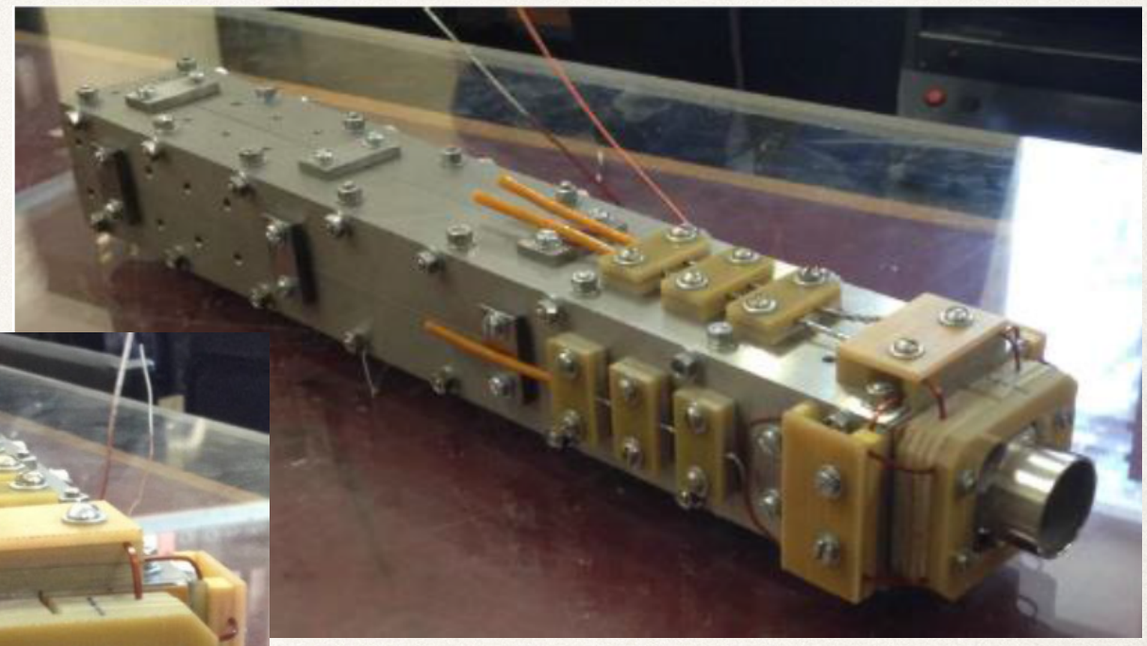
Max.current 1100 A

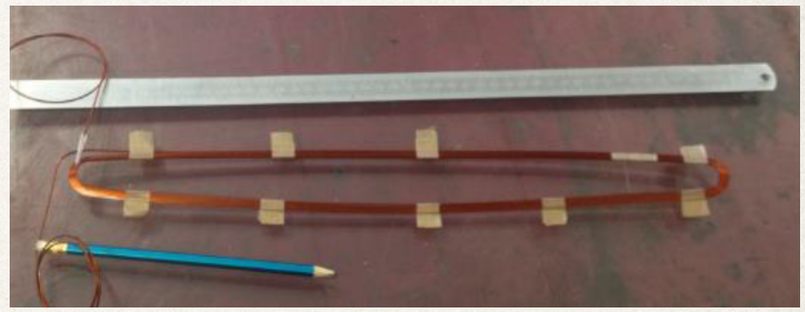
Length 40 cm

Aperture 2 cm

NbTi 1.8 x 1.4 mm^2

Saddle-type coils

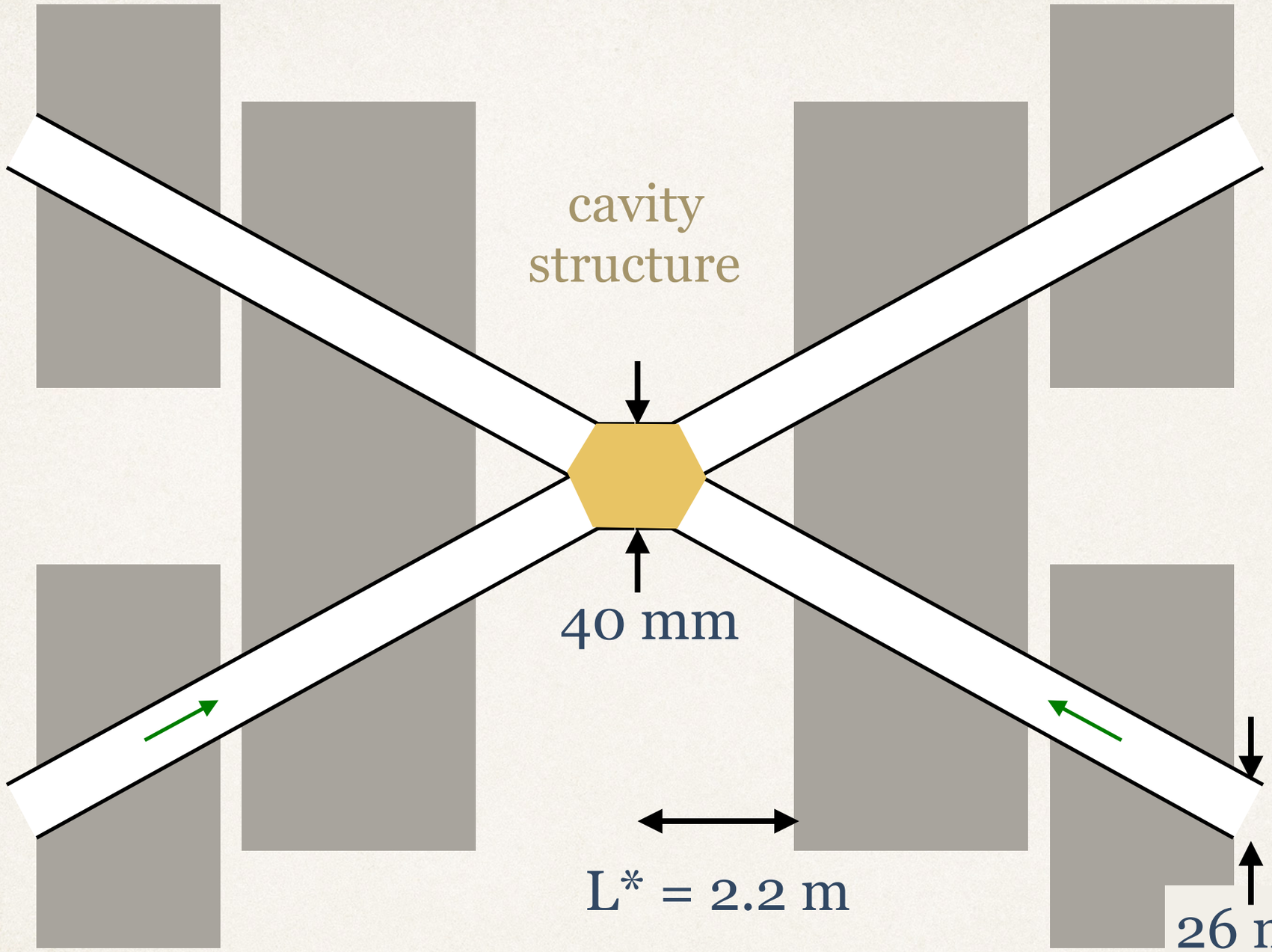




During the first cryo-test (01.02.16) the current of 1060 A was achieved after 3 quenches.

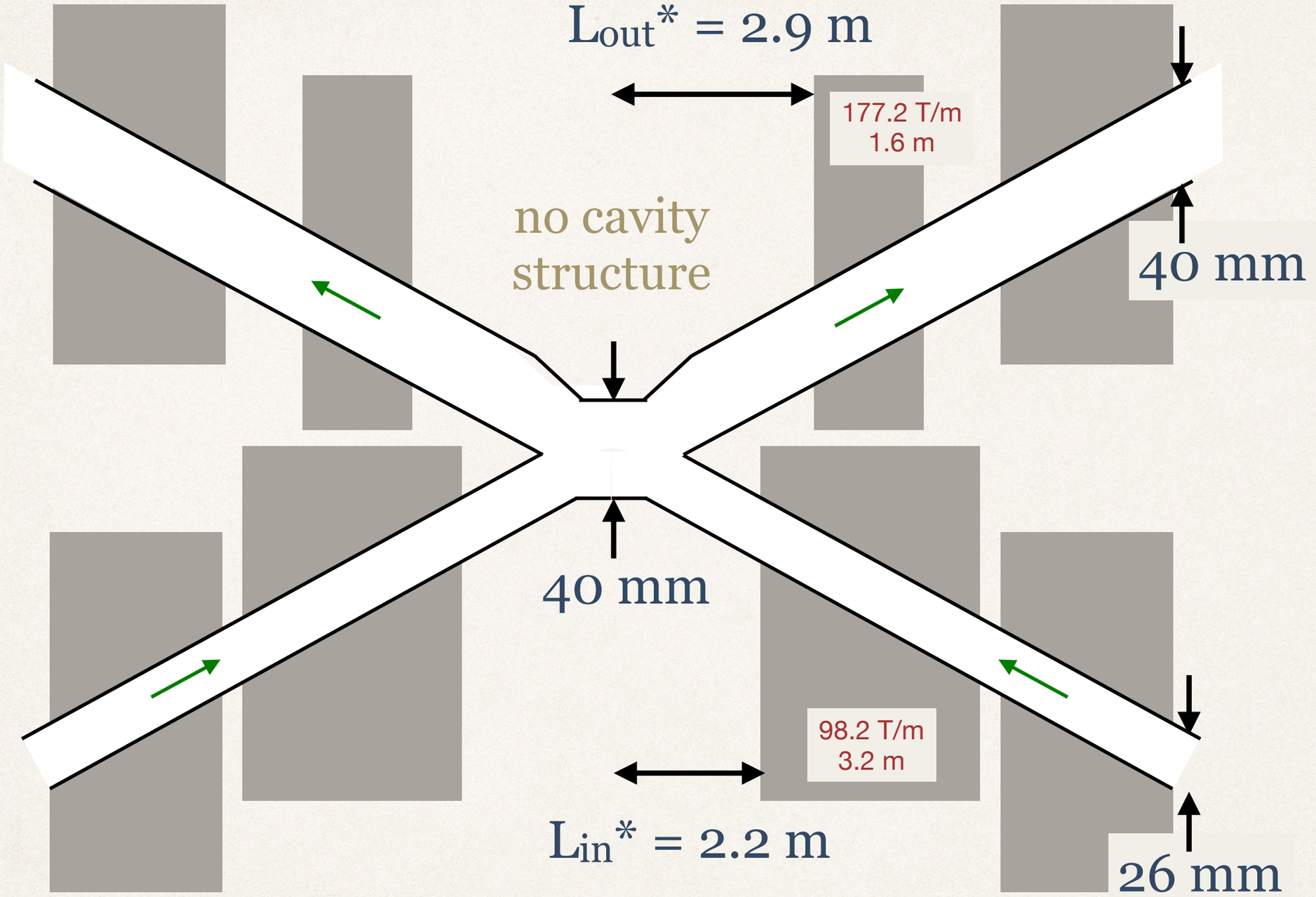
A. Bogomyagkov, E. Levechev

HOM trapping by the cavity structure at IP



- HOM is trapped in the IP beam pipe, if all beam pipes are narrower than the IP, which needs to be larger that 40 mm (M. Sullivan).
- Heating, esp. at Z.
- Leak of HOM to the detector, through the thin Be beam pipe at the IP.

Asymmetric L*: larger outgoing beam pipe & thinner final quads

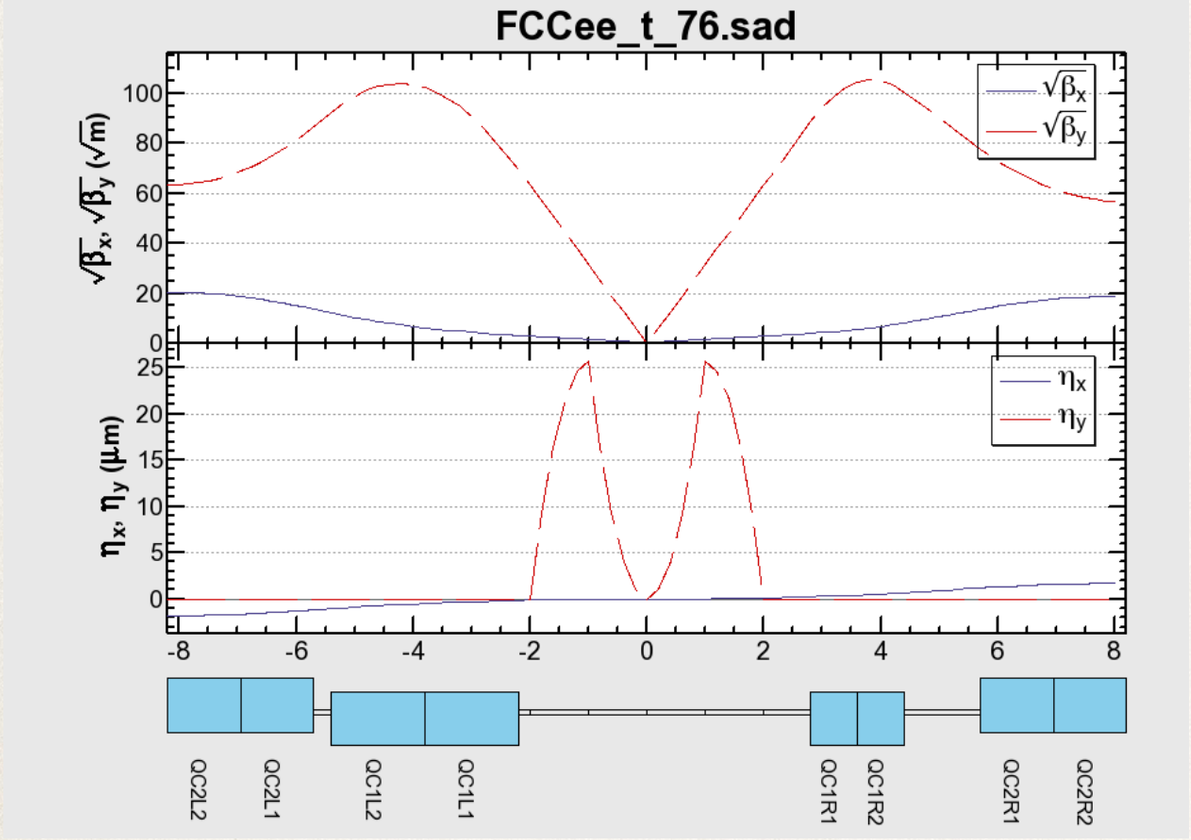


- The HOM can escape to the outside through the outgoing beam pipe, which has a diameter not smaller than IP.
- The outgoing final quad becomes thinner and stronger (E. Levichev, S. Sinyatkin).

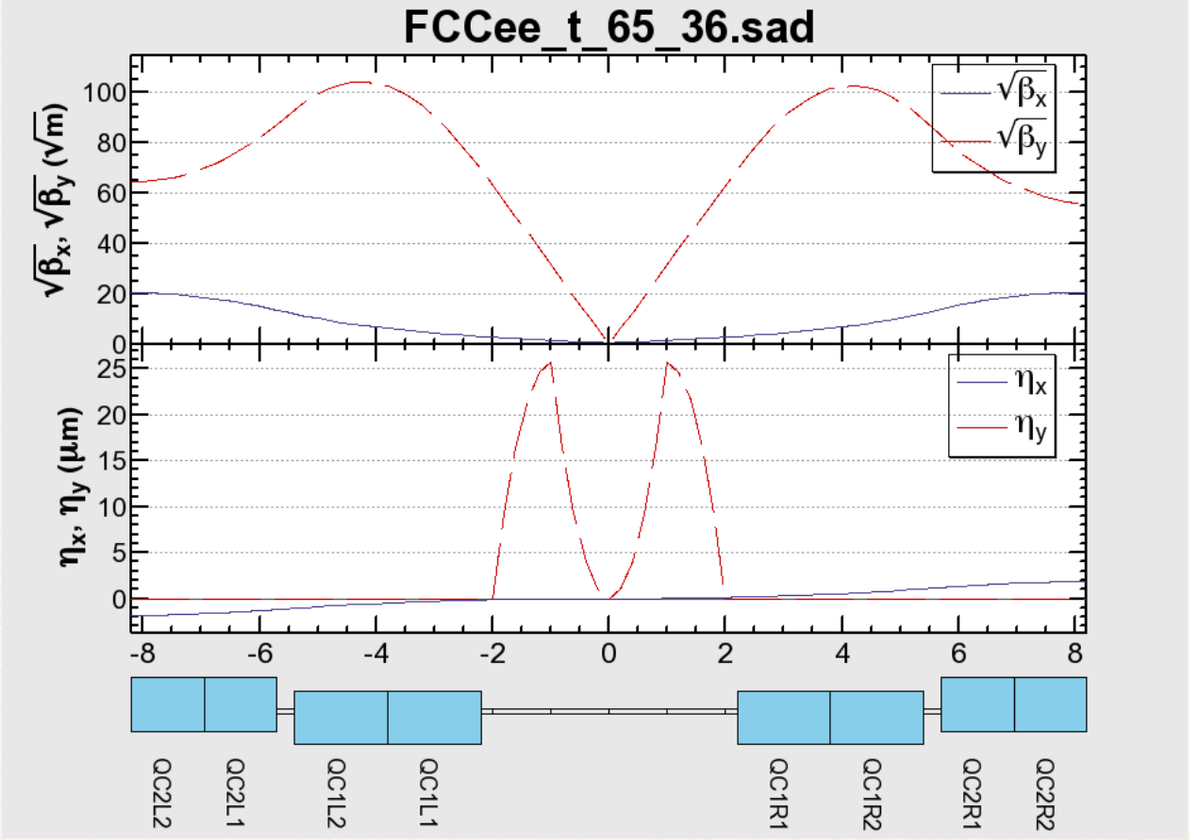
Optics at the IP

175 GeV, $\beta^*_{x,y}$ = (0.5 m, 1 mm)

Asymmetric L*

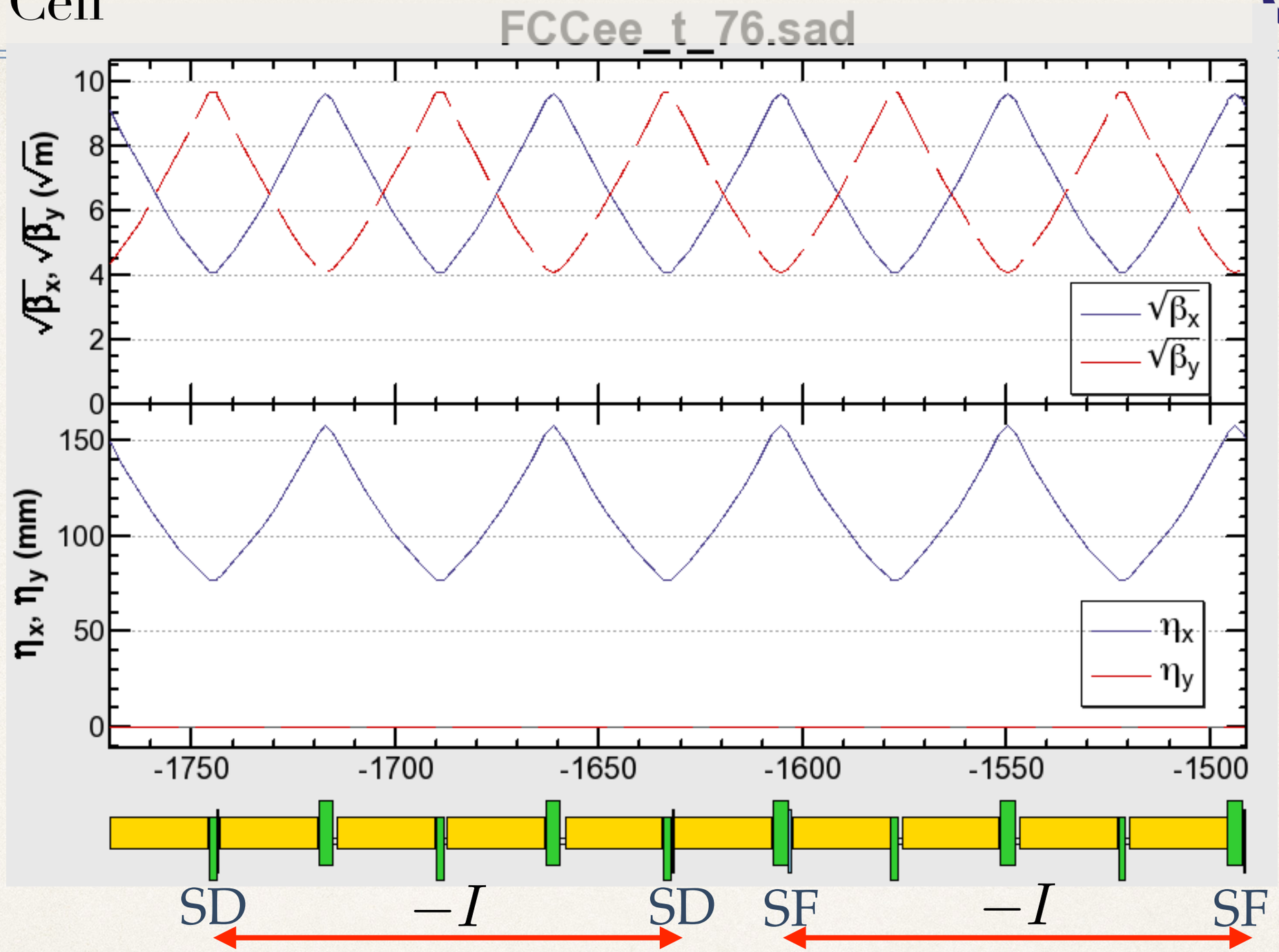


Symmetric L*



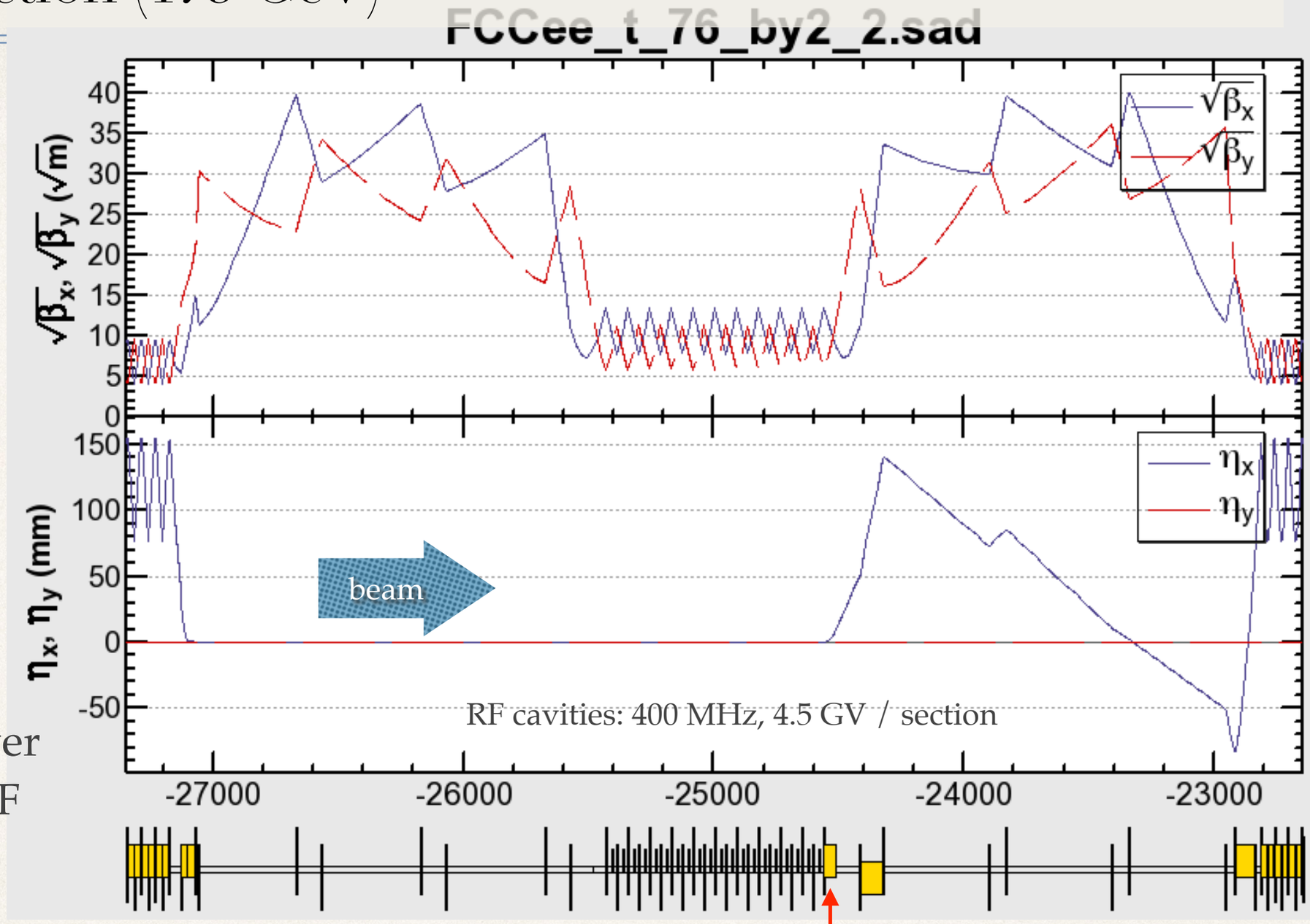
- Even with the asymmetric L*, the optics, so as the chromaticity, look similar.
- The solenoid compensation is unchanged: locally compensated up to 2.2 m from the IP.
- Longer L* downstream may give a space for a luminometer.

The Arc Cell



- Basically a 90/90 degree FODO cell.
- The quadrupoles QF/QD are 3.5 m/1.8 m long, respectively, to reduce the synchrotron radiation. They also depends on the design of quads and the beam pipe (A. Milanese, F. Zimmermann).
- All sextupoles are paired with -*I* transformation.
- 292 sextupole pairs per half ring.

The RF section (175 GeV)



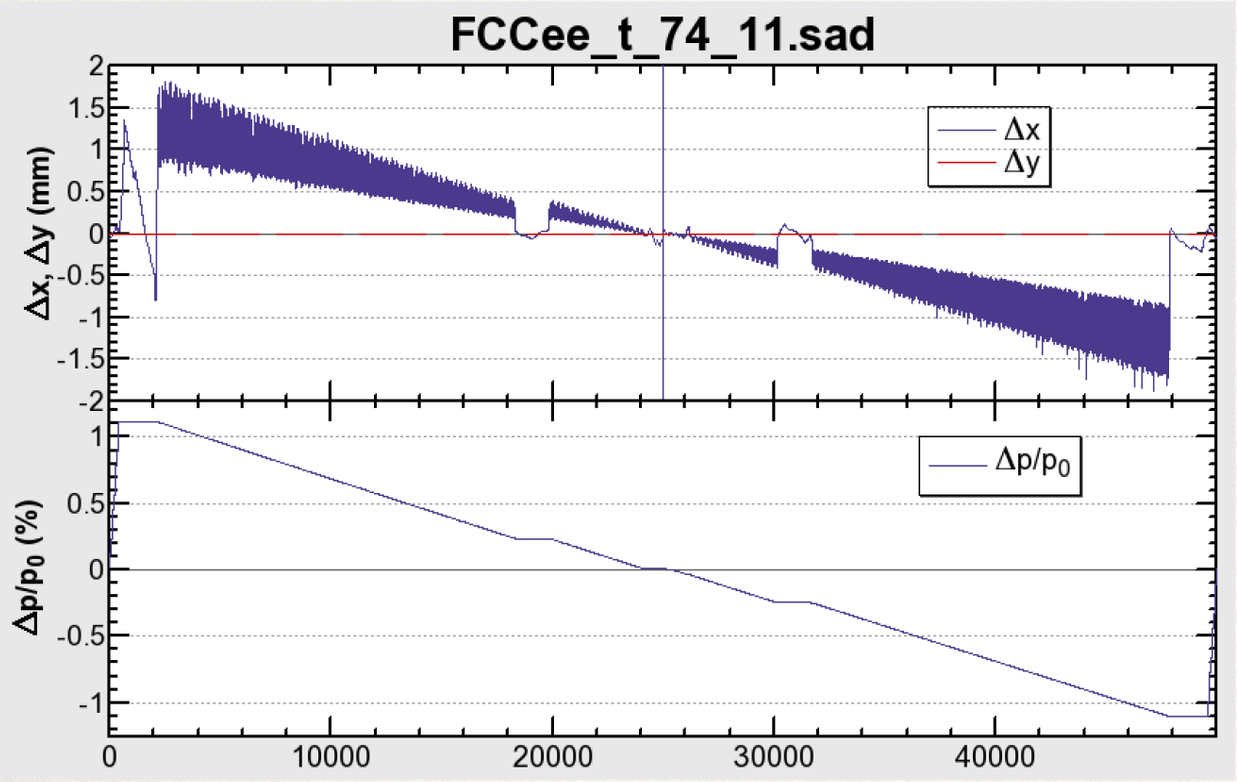
Beams cross over through the RF section.

An electrostatic separator, combined with a dipole magnet

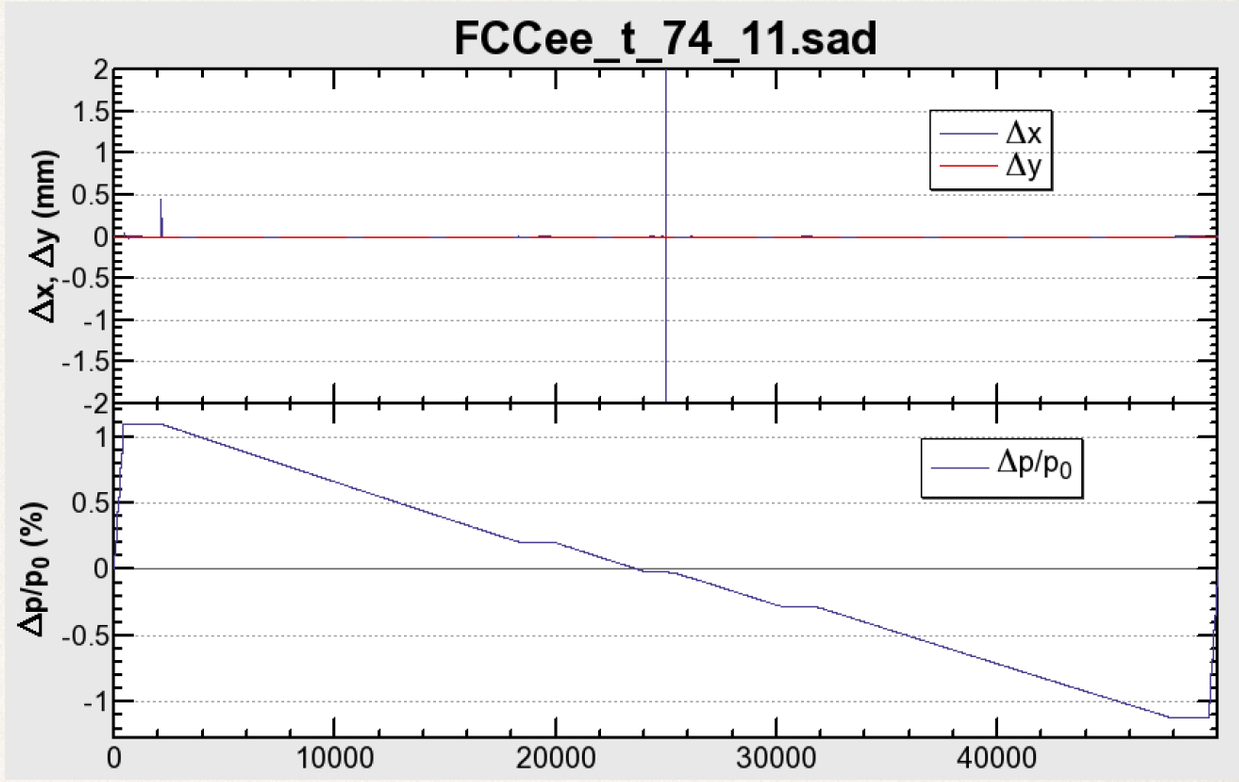
- The usage of the straights on the both sides of the RF is to be determined.
- If the nominal strengths of quads are symmetrical in the common section, it matches to the optics of both beam.
- This section is compatible with the RF staging scenario. For lower energy, the common RF and cross over will not be necessary.

The Sawtooth & Tapering (175 GeV)

No Taper



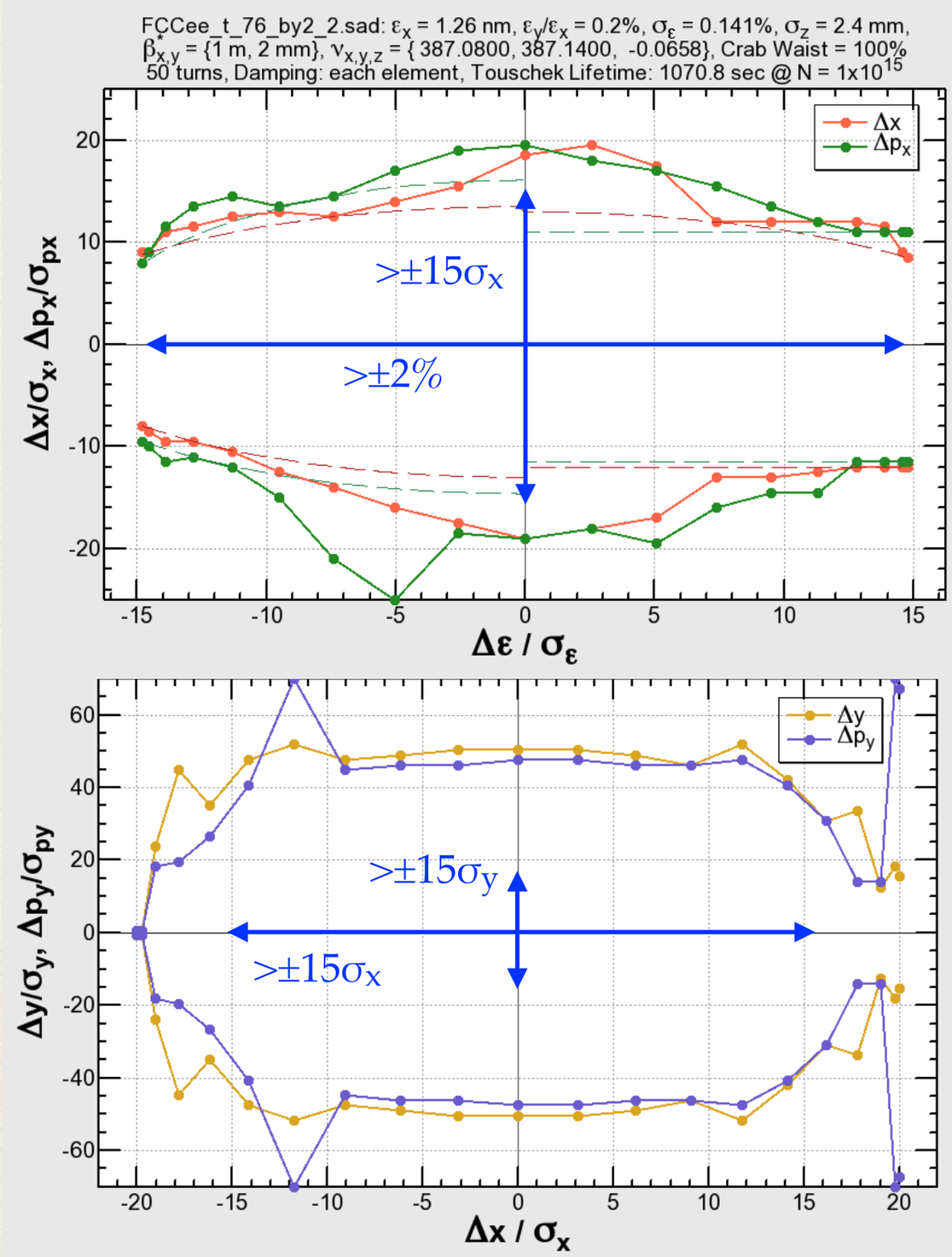
Tapered



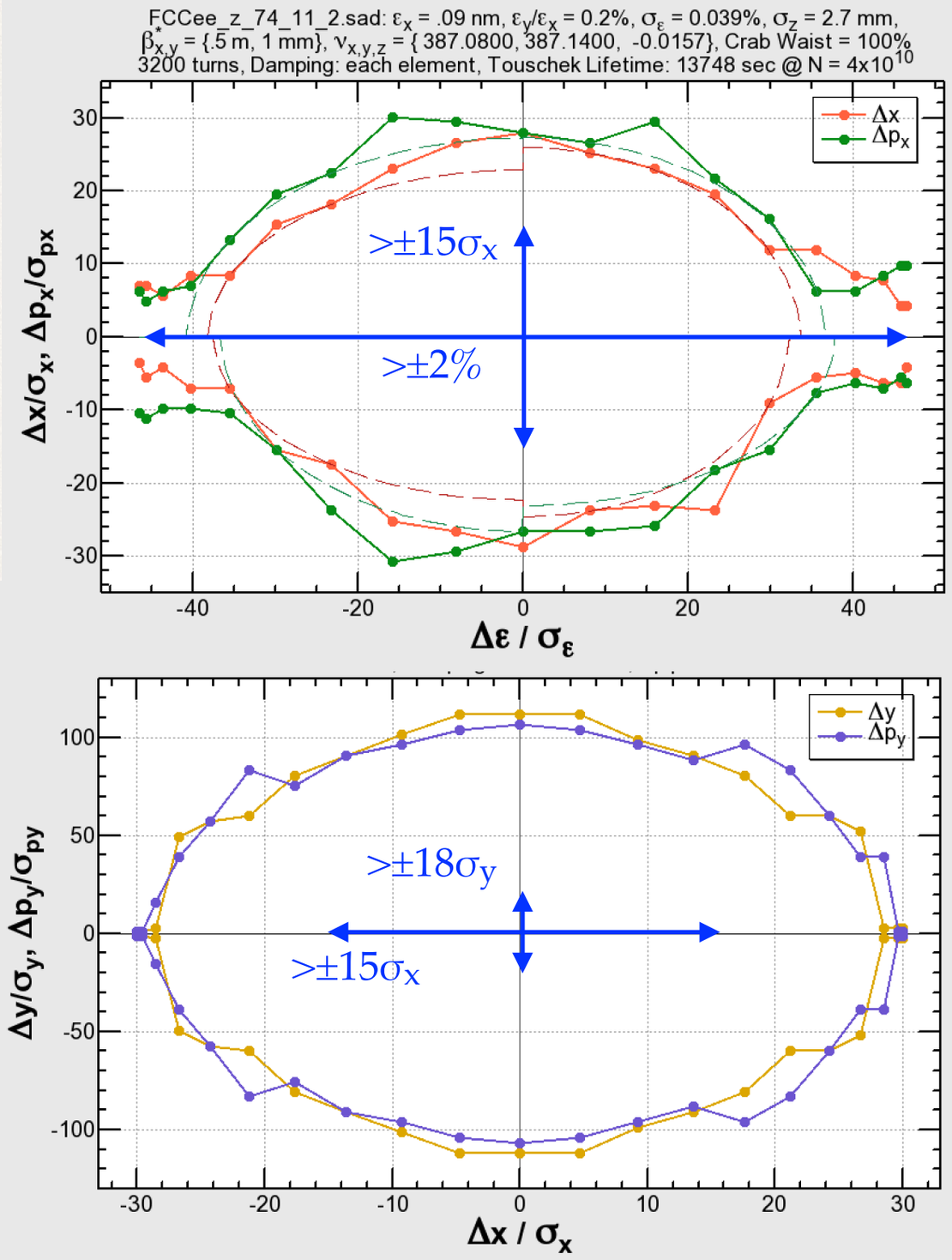
- The change of the orbit due to energy loss along the arc causes serious deformation on the optics, causing the loss of the dynamic aperture.
- Everything can be cured almost completely by “tapering”, i.e. scaling the strengths of all magnets along the local energy of the beam: this is one of the best merits of a double-ring collider (F. Zimmermann).

Dynamic Aperture satisfies the requirements.

175 GeV, $\beta^*_{x,y}$ = (1 m, 2 mm)



45.6 GeV, $\beta^*_{x,y}$ = (0.5 m, 1 mm)



Requirements assuming the same horizontal emittance as the collider and 1% coupling from the booster:

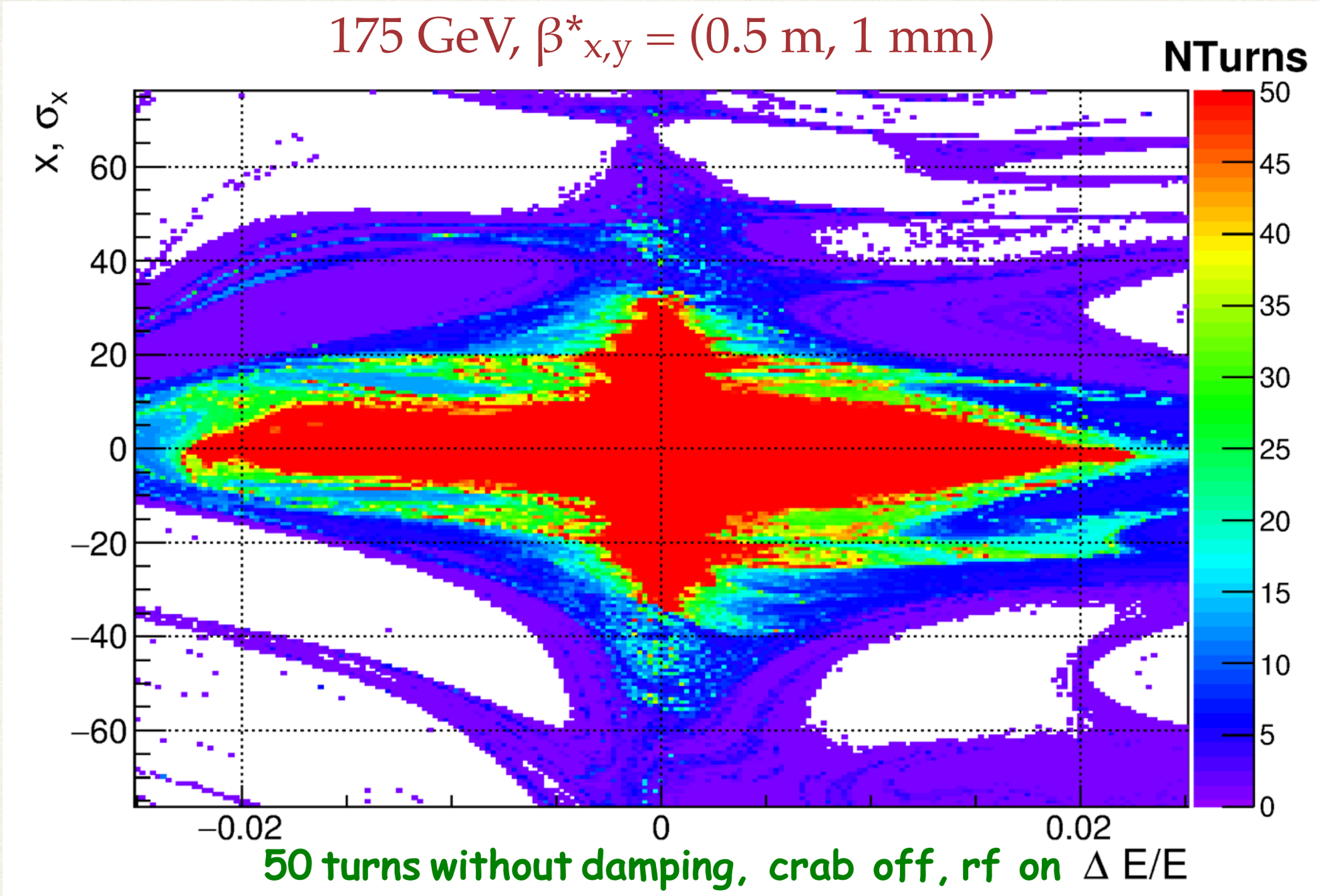
$\Delta p/p > \pm 2\%$, $\Delta x > 15\sigma_x$, $\Delta y > 15\sigma_y$ @ 175 GeV, $\Delta p/p > \pm 2\%$, $\Delta x > 15\sigma_x$, $\Delta y > 18\sigma_y$ @ 45.6 GeV (See M. Aiba's talk).

Effects included in the dynamic aperture survey

Effects	included?	significance for DA in FCC-ee @ 175 GeV
synchrotron motion	yes	**essential**
radiation damping (turn by turn)	yes	**essential** aperture↑
radiation damping (each element, esp. quads)	yes (no fluctuation yet)	**essential** aperture↓
“tapering”	yes	**essential**
crab waist	yes	yes, aperture↓
solenoids	yes	minimal, if locally compensated
Maxwellian fringe field	yes	small
kinematical terms	yes	small
beam-beam	yes (weak-strong)	yes, esp. on lifetime (D. Zhou)
errors/misalignments	not yet	**essential**, correction schemes must be developed

Dynamic Aperture for the AB Lattice

175 GeV, $\beta^*_{x,y}$ = (0.5 m, 1 mm)

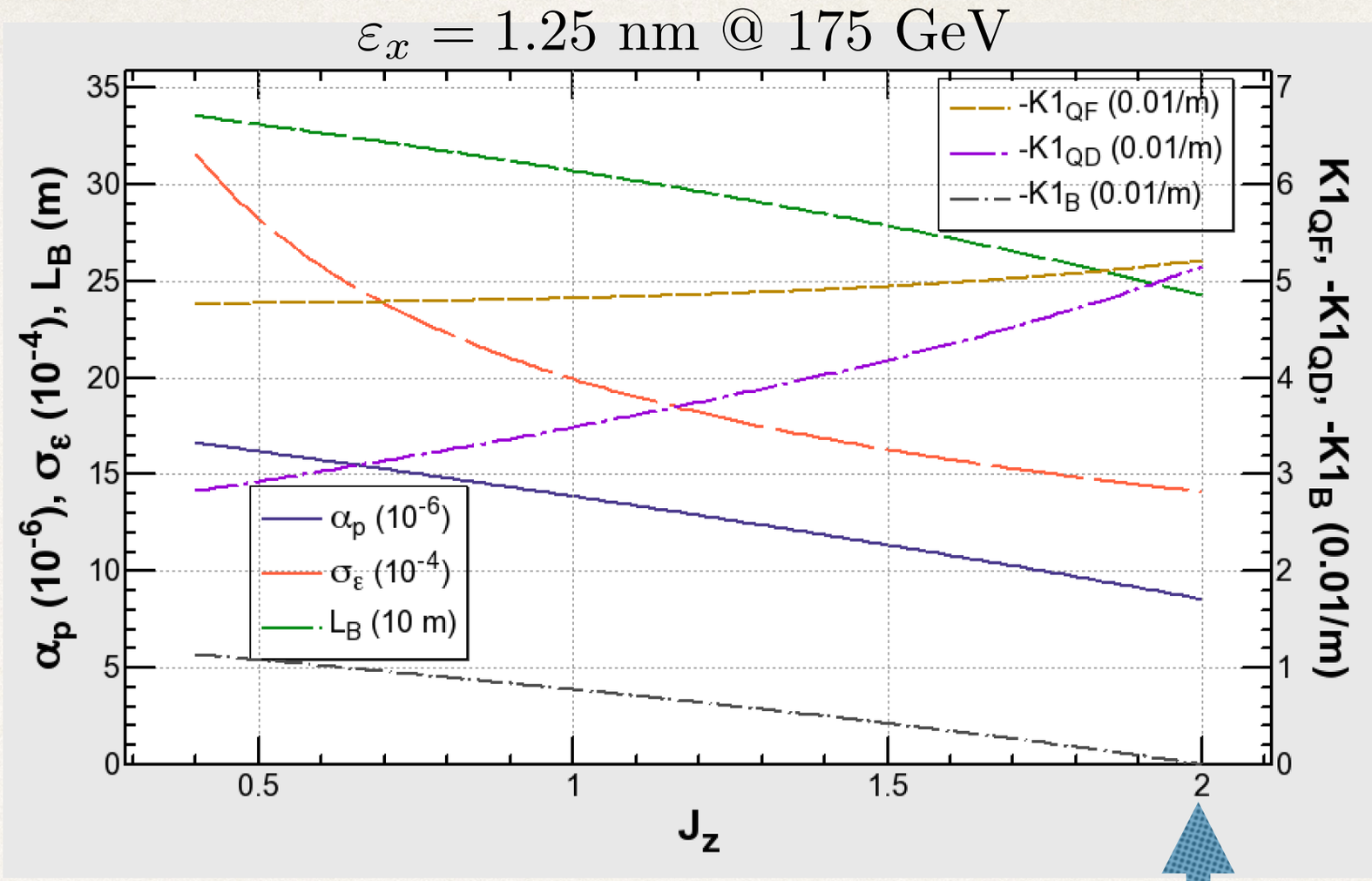


ε_x=1.4 nm·rad, 0.2% coupling, τ_x=44 turns, ν_s=0.0807, Urf=11 GV

The dynamic aperture for the AB lattice is under optimization, and looks promising so far.

P. Piminov, A. Bogomyagkov

A possibility of combined function dipole in the arc



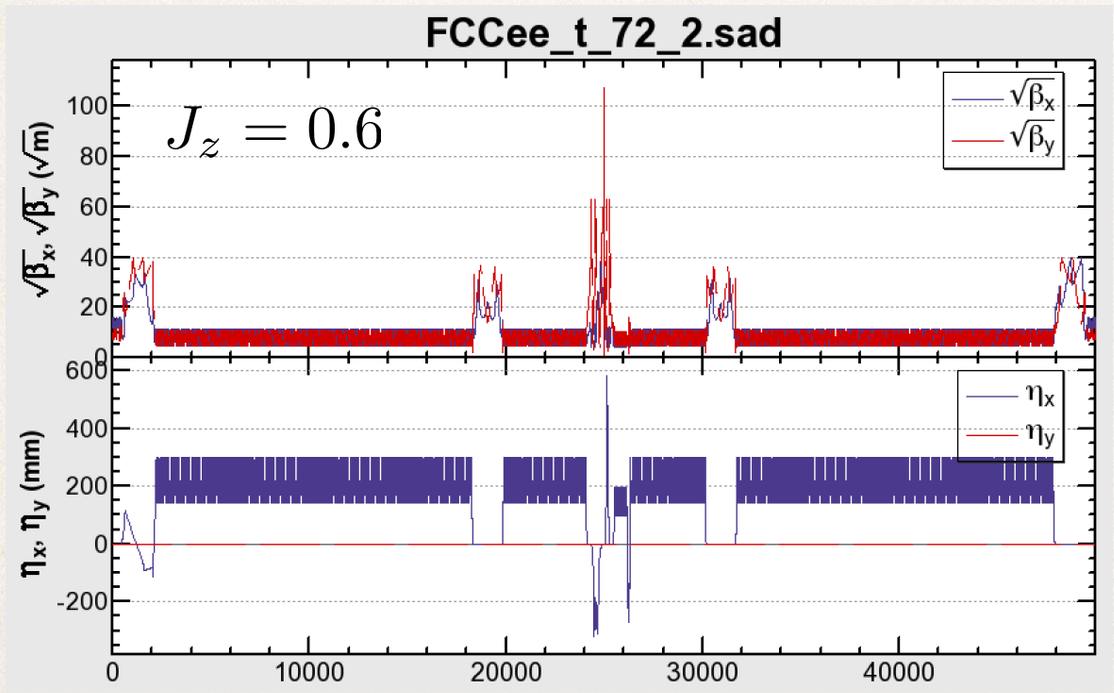
A negative field gradient in the main dipole of the unit cell provides:

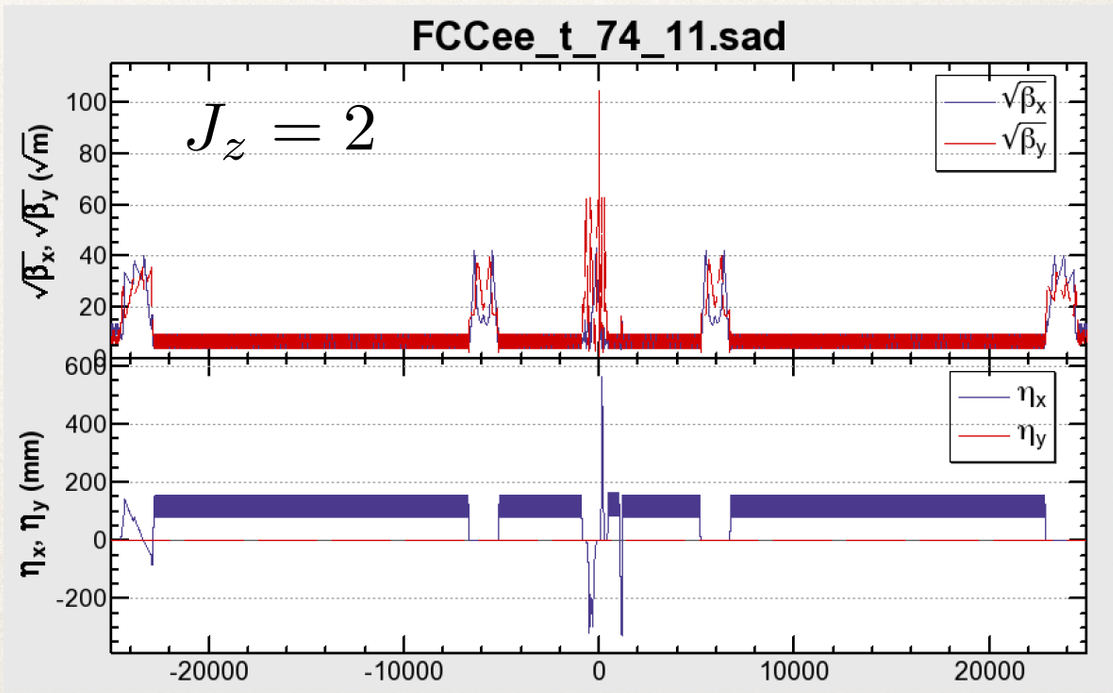
- longer cell length for a given emittance / better packing factor
- larger momentum compaction (longer bunch length for a same RF voltage)
- larger energy spread
- larger dispersion
- weaker sextupoles

Suggested by E. Levechev

An example of combined function: $J_z = 0.6$ @ 175 GeV

Jz	0.6	2
# of FODO cells	**1062**	1442
Length of dipole (m)	33.9	23.1
H dispersion at SF (cm)	**29.6**	16.3
1 turn energy loss (GV)	**7.09**	7.74
momentum spread (%)	0.24	0.14
momentum compaction (10^{-6})	**12.8**	7.2
bunch length (mm)	5.0	2.4
RF voltage (GV)	9.6	9.4
synchrotron tune	-0.10	-0.068

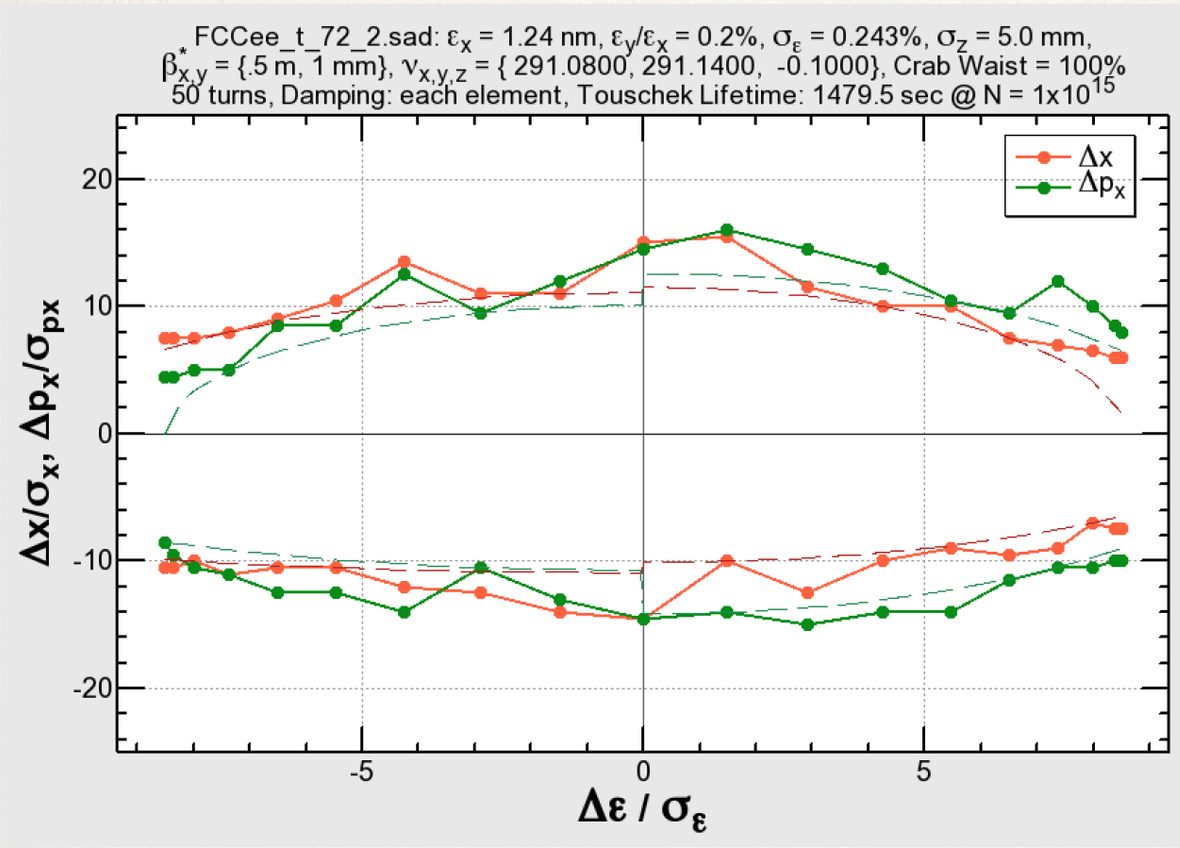




Dynamic aperture of combined function lattice.

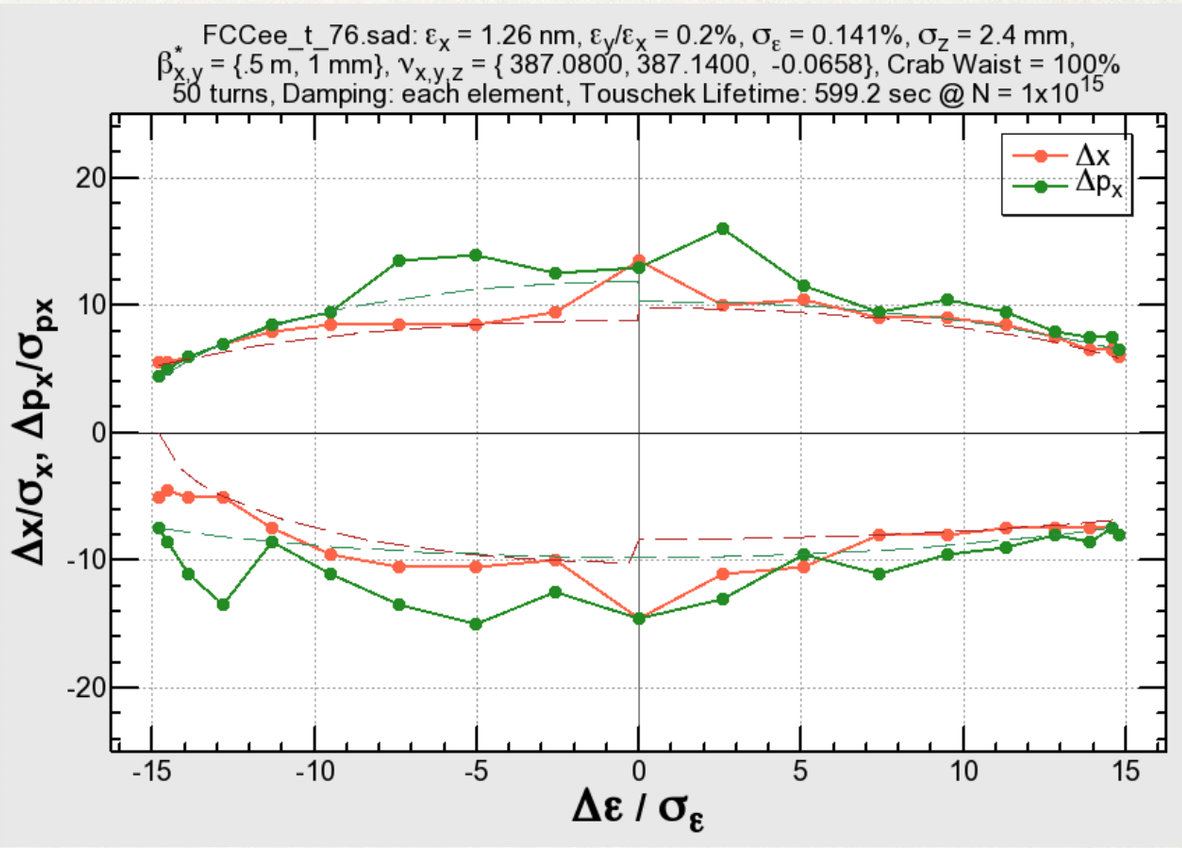
175 GeV, $\beta^*_{x,y}$ = (0.5 m, 1 mm)

Combined function dipole



±2%

Flat dipole



±2%

- The dynamic aperture is comparable to the flat-dipole lattice.
- Looking for beam-beam simulation and hardware solution of the dipole.

Some related talks during this workshop

RF system parameters for Z, W, H and tt	O. Brunner	Tue. 8:30
Beam dynamics: RF requirements for the FCC-hh and FCC-ee options	E. Shaposhnikova	Tue. 8:50
Beam-beam simulations of FCC-ee with Lifetrac	D. Shatilov	Wed. 8:30
Beam-beam simulations and ecloud in e+ ring	K. Ohmi	Wed. 8:50
Interplay of the beam-beam effect and the lattice nonlinearity	D. Zhou	Wed. 9:10
A new beam-beam effect in collisions with crossing angle	V. Telnov	Wed. 9:30
Challenges for FCC-ee MDI	M. Boscolo	Wed. 8:30
Synchrotron radiation background	H. Burkhardt	Wed. 8:50
FCC-ee Interaction Region Layout	M. Sullivan	Wed. 9:10
Backgrounds in the FCC-ee detector and consequences for the trigger and DAQ	E. Perez	Wed. 9:30
FCC-ee warm magnets design	A. Milanese	Wed. 14:10
FCC-ee IR optics solutions	A. Bogomyagkov	Wed. 15:30
Arc optics, global Q' correction and emittance variation	B. Harer	Wed. 15:50
Lattice for a Higgs factory	Y. Cai	Wed. 16:40
Tolerance studies and coupling correction for FCC-ee	S. Aumon	Thu. 10:30
Dynamic aperture	L. Medrano	Thu. 10:50
FCC-ee injector complex incl. Booster	Y. Papaphilippou	Thu. 11:10
Preliminary inector linac design	S. Polozov	Thu. 13:50
Design of the booster ring optics	O. Etisken	Thu. 14:05
Top-up injection schemes	M. Aiba	The. 14:35

… and more …

Some related posters during this workshop

Beam dump for the FCC-ee collider	A. Apyan	Wed. 17:30
Superconducting Cavity Design for FCC-ee	S. Zadeh	Wed. 17:30
Superconducting sputtered Nb3Sn films for SRF applications	K. Ilyina	Wed. 17:30
Tapering options for the FCC-ee collider	A. Doblhammer	Wed. 17:30

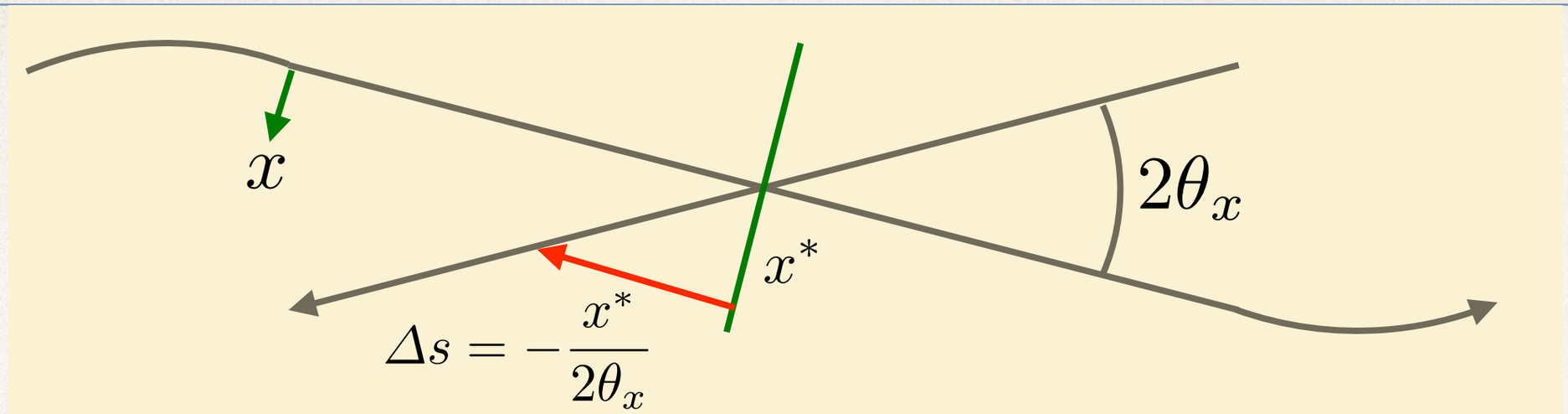
… and more …

Summary

- **Optics for FCC-ee are presented, considering:**
  - 2 IPs/ring, with 30 mrad crossing angle.
  - Local chromaticity correction with crab waist.
  - Suppression of synchrotron radiation in the IR below 100 keV up to 510 m from the IP.
  - Solenoid at IP & its compensation.
  - Possible asymmetric L* for wider outgoing beam pipe at the IP.
  - Element-by-element synchrotron radiation.
  - Tapering of all magnets according to the local beam energy to suppress sawtooth.
  - Common RF sections with cross-over of two beams (at least at tt).
  - Optimization of dynamic aperture with hundreds of sextuple families .
  - Geometrical fitting to the FCC-hh tunnel.
  - Combined function dipole in the arc will bring a number of merits, if realized.
- **Resulting dynamic aperture almost satisfies the requirements.**
- Things need further investigation:
  - Field quality, more realistic profile of magnetic field.
  - Tolerances / tuning scheme for machine errors, misalignments.
  - and more…

Backups

Crab waist sextuple within CCS



The crab waist scheme shifts the vertical waist of a beam by

$$\Delta s = -\frac{x^*}{2\theta_x} \ . \tag{1}$$

Thus the associated transformation is

$$y^* \to y^* - p_y^* \Delta s = y^* + \frac{p_y^* x^*}{2\theta_x} \ , \tag{2}$$

which is performed by a Hamiltonian at the IP:

$$H^* = \frac{x^* p_y^{*2}}{4\theta_x} \ . \tag{3}$$

If there are the phase relations between the IP and the sextupoles:

$$\Delta\psi_x = 2\pi \ \text{ and } \ \Delta\psi_y = 2.5\pi, \tag{4}$$

then the variables at the IP (x^*, p_y^*) are expressed in those at the sext (x, y):

$$x^* = \sqrt{\frac{\beta_x^*}{\beta_x}} x, \quad p_y^* = \frac{y}{\sqrt{\beta_y^* \beta_y}} \ . \tag{5}$$

Thus the Hamitonian at the IP is equivalent to a Hamiltonian at the sext:

$$H = \frac{x y^2}{4\theta_x \beta_y^* \beta_y} \sqrt{\frac{\beta_x^*}{\beta_x}} \ , \tag{6}$$

which can be approximated by a Hamiltonian of a sextupole:

$$H_s = \frac{k_2}{6} \left(x^3 - 3xy^2 \right) \ , \tag{7}$$

with

$$k_2 = -\frac{1}{2\theta_x \beta_y^* \beta_y} \sqrt{\frac{\beta_x^*}{\beta_x}} \ . \tag{8}$$

Chromogeometric aberration of CCS

Consider the transfer matrix between sexts of YCCS with momentum dependence:

$$m_y = \begin{pmatrix} -1+8\delta^2 & -2\delta\ell(-4-4\sqrt{2}+(6+5\sqrt{2})\delta) \\ \delta/\ell(-4-4\sqrt{2}+(14+9\sqrt{2})\delta) & -1+8\delta^2 \end{pmatrix} + O(\delta^3)\ , \tag{1}$$

and similar for m_x. Then the emittance increment due to the sextupole kick is calculated as:

$$\begin{aligned} R\delta^2 \quad &\equiv \quad \frac{\Delta\varepsilon_y}{\varepsilon_y} = \frac{256\delta^2}{\beta_x\beta_y^2\eta_x^2\ell^2}(2\sqrt{2}\beta_y+\ell\xi_y)^2 && (2)\\ &\times \quad \Big((6-4\sqrt{2})\beta_y^2\varepsilon_x\ell^2 + ((9-6\sqrt{2})\beta_y^2-2\ell^2)\beta_x\beta_y\varepsilon_y && (3)\\ &\quad + ((2\sqrt{2}-1)\beta_y^2+(14+8\sqrt{2})\ell^2)\beta_x^2\varepsilon_x\Big)\ , && (4)\end{aligned}$$

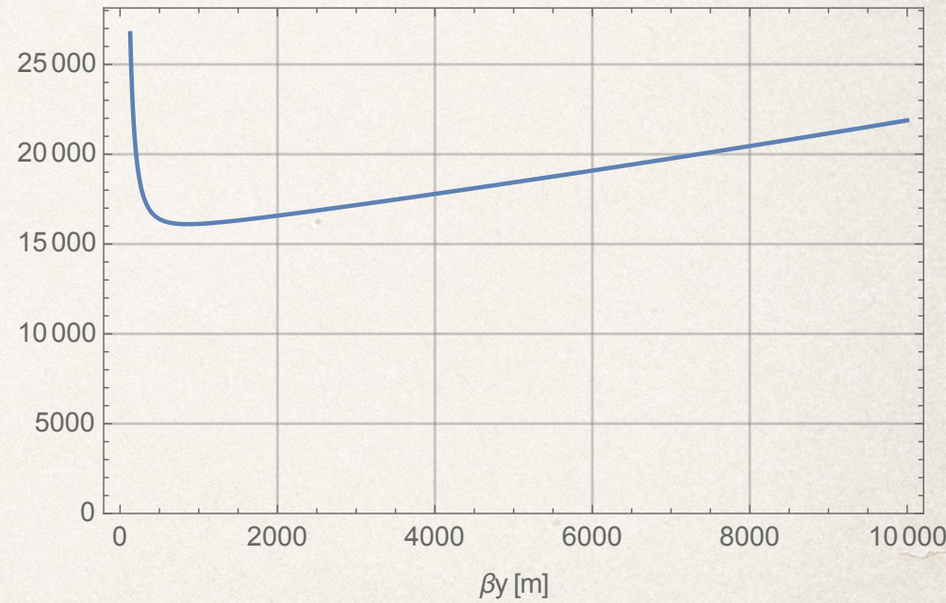
where β_x, β_y,and η_x are the values at the sextupole, ℓ the separation of quads, and we have assumed

$$-k_2\beta_y\eta_x = \xi_y + 2\sqrt{2}\beta_y/\ell\ . \tag{5}$$

If we plug in the numbers:

$$\beta_x = 15\text{ m},\ \varepsilon_x = 1.2\text{ nm},\ \varepsilon_y = 2.4\text{ pm},\ \eta_x = 0.16\text{ m},\ \ell = 58\text{ m},\ \xi_y = 3,500\ , \tag{6}$$

we get the following graph.



Although the optimum is at around $\beta_y = 600$ m, the increment is small up to $\beta_y \lesssim 8,000$ m.

- Above are just tentative optics.
- Usage of these sections is to be determined.

A rough estimation of radiation by arc quads

- The radiation power:

$$P \propto \gamma^2 B^2 \ell$$

- Ratio of powers by dipoles and quadrupoles per unit cell:
  - dipole:

$$P_d \propto \gamma^2 \left(\frac{B\ell_{\rm cell}}{B\rho}\right)^2 \left(\frac{B\rho}{\ell_{\rm cell}}\right)^2 \ell_{\rm cell} \propto \gamma^4 \frac{\theta^2}{\ell_{\rm cell}}$$

  - quadrupole:

$$P_q \propto \frac{\gamma^2}{2} \left(\frac{B'\Delta x \ell_q}{B\rho}\right)^2 \left(\frac{B\rho}{\ell_q}\right)^2 \ell_q \propto \frac{\gamma^4}{2} \frac{k_1^2 \Delta x^2}{\ell_q}$$

  - ratio:

$$\frac{P_q}{P_d} = \frac{(k_1 \ell_{\rm cell})^2}{2} \frac{\beta_{xq}}{\ell_{\rm cell}} \frac{n^2 \varepsilon_x}{\theta^2 \ell_q}, \qquad \Delta x^2 = n^2 \beta_{xq} \varepsilon_x$$

- In the case of a 90° cell, $k_1 \ell_{\rm cell} = 2\sqrt{2}, \beta_{xq}/\ell_{\rm cell} = 1 + \frac{1}{\sqrt{2}}$, then:

$$\frac{P_q}{P_d} = (4 + 2\sqrt{2}) \frac{n^2 \varepsilon_x}{\theta^2 \ell_q}$$

- or a particle with an amplitude of $n\sigma_x$ will receive an energy loss per every turn:

$$\frac{\Delta p_1}{p_0} = \frac{P_q}{P_d} \times \frac{U_0}{E} = (4 + 2\sqrt{2}) \frac{n^2 \varepsilon_x}{\theta^2 \ell_q} \alpha_\varepsilon \qquad (\alpha_\varepsilon\text{: long. damping per turn})$$

- which causes a synchrotron motion with a momentum amplitude $\pm \Delta p/p_0$:

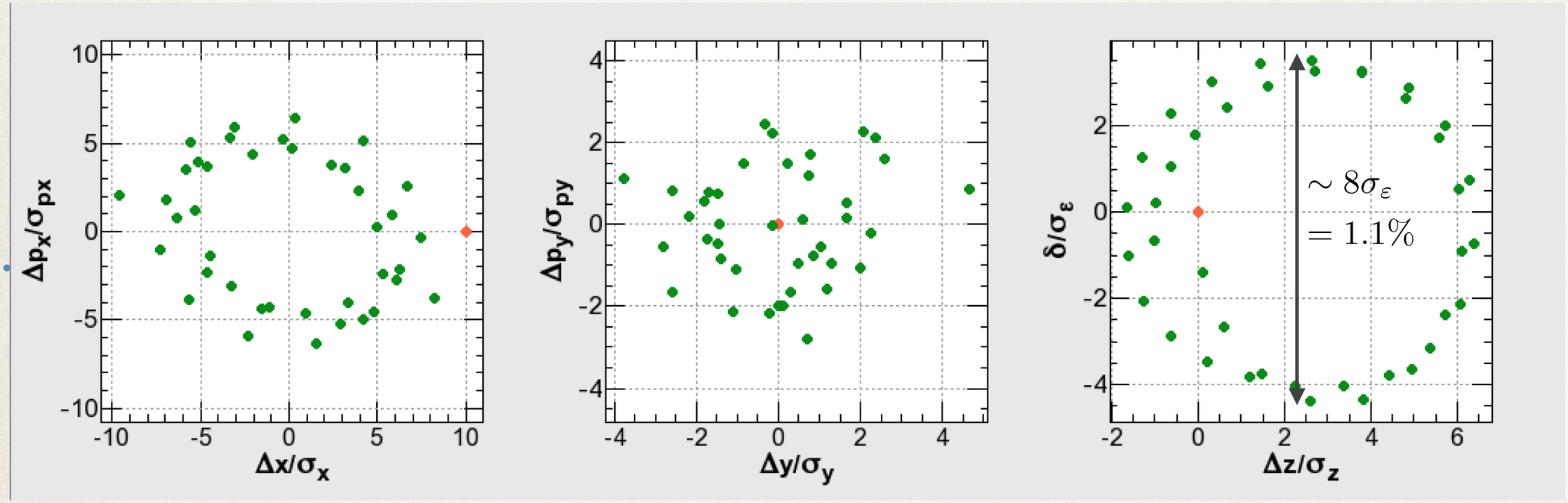
$$\frac{\Delta p}{p_0} = \frac{1}{2\pi\nu_s} \frac{\Delta p_1}{p_0} = \left(2 + \sqrt{2}\right) \frac{n^2 \varepsilon_x}{\pi \theta^2 \ell_q} \frac{\alpha_\varepsilon}{\nu_s}$$

A rough estimation of radiation by arc quads (cont'd)

$$\varepsilon_x = 2 \text{ nm}, \theta = 2\pi/1240, \alpha_\varepsilon/\nu_s = 0.41 \quad \text{gives}$$

$$\frac{\Delta p}{p_0} = 0.58\% \left(\frac{n}{10}\right)^2 \left(\frac{0.6 \text{ m}}{\ell_q}\right)$$

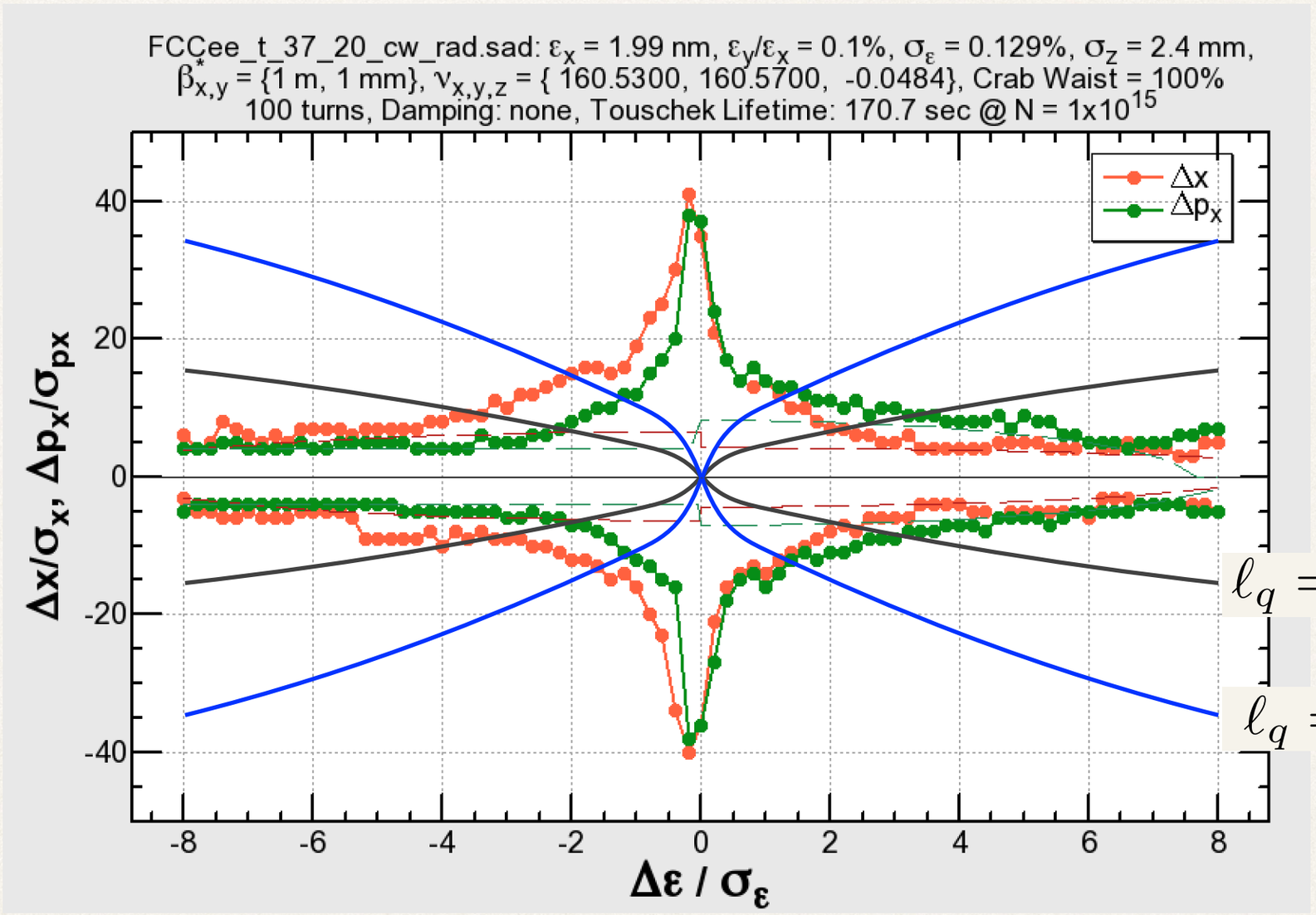
- If we plug-in the number for FCC-ee-tt:



* only damping, no fluctuation, is taken into account in simulations in these slides.

Cf. Barbarin, F ; Iselin, F Christoph ; Jowett, John M, 4th European Particle Accelerator Conference, London, UK, 27 Jun - 1 Jul 1994, pp.193-195

The effect on the dynamic aperture



$\ell_q = 0.6$ m

$\ell_q = 3$ m

$\Delta x/\sigma_x$