

History and Lessons from Existing and Studied High Energy Hadron Machines

FCC-hh: Beam Dump Concepts Session

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Northern Illinois University

Historical Perspective

- The Tevatron
- The Superconducting Super Collider (SSC)
- The Large Hadron Collider (LHC)
- The Very Large Hadron Collider study (VLHC)
- The Future Circular Collider study (FCC)



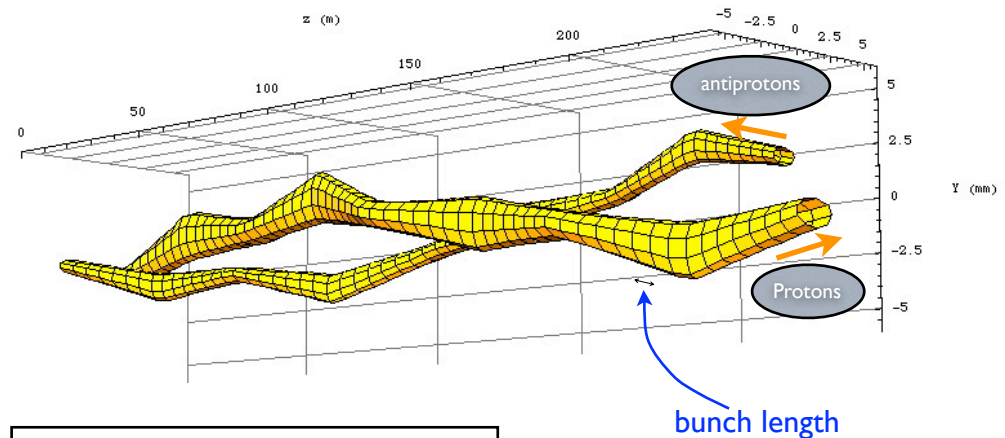
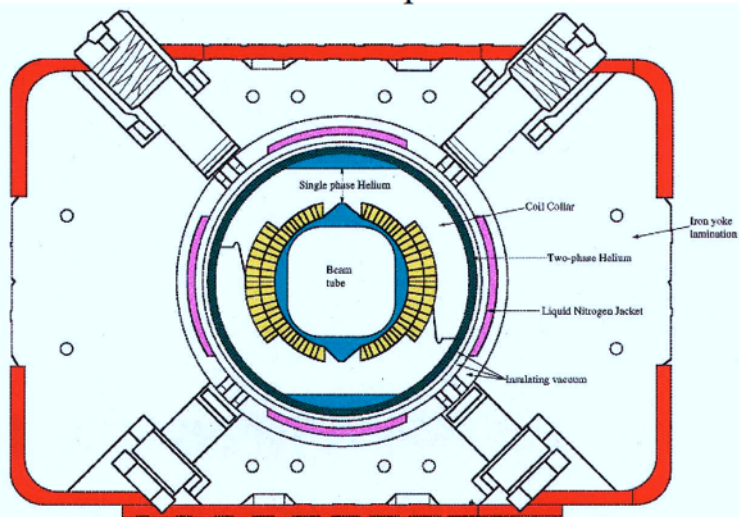
The Tevatron

- 1st superconducting synchrotron
- 4.4 T magnets; 4°K
- collide protons w/ antiprotons
- common beam pipe



X (mm)

Tevatron Dipole



Helical orbits through 4 standard arc cells of the Tevatron



Tevatron Abort System

- Prior to Tevatron, the original “Main Ring” at Fermilab existed in the same tunnel
 - 400 GeV beam, $\sim 3 \times 10^{13}$ p, 10 s cycle
 - corresponds to ~ 2 MJ beam energy
- Tevatron originally ran as fixed target synchrotron, with 800 GeV beam
 - $\sim 2 \times 10^{13}$ p, 30 - 120 s cycles; 2.6 MJ
- When reconfigured for colliding beams, the beam abort system was changed to an “internal abort”; re-use the “C0” straight section for a possible new interaction region
 - 980 GeV, $\sim 1 \times 10^{13}$ p \rightarrow ~ 1.5 MJ
 - less for antiprotons (eventually, up to ~ 0.75 MJ)



The Energy Doubler (a.k.a., Tevatron)

-191-

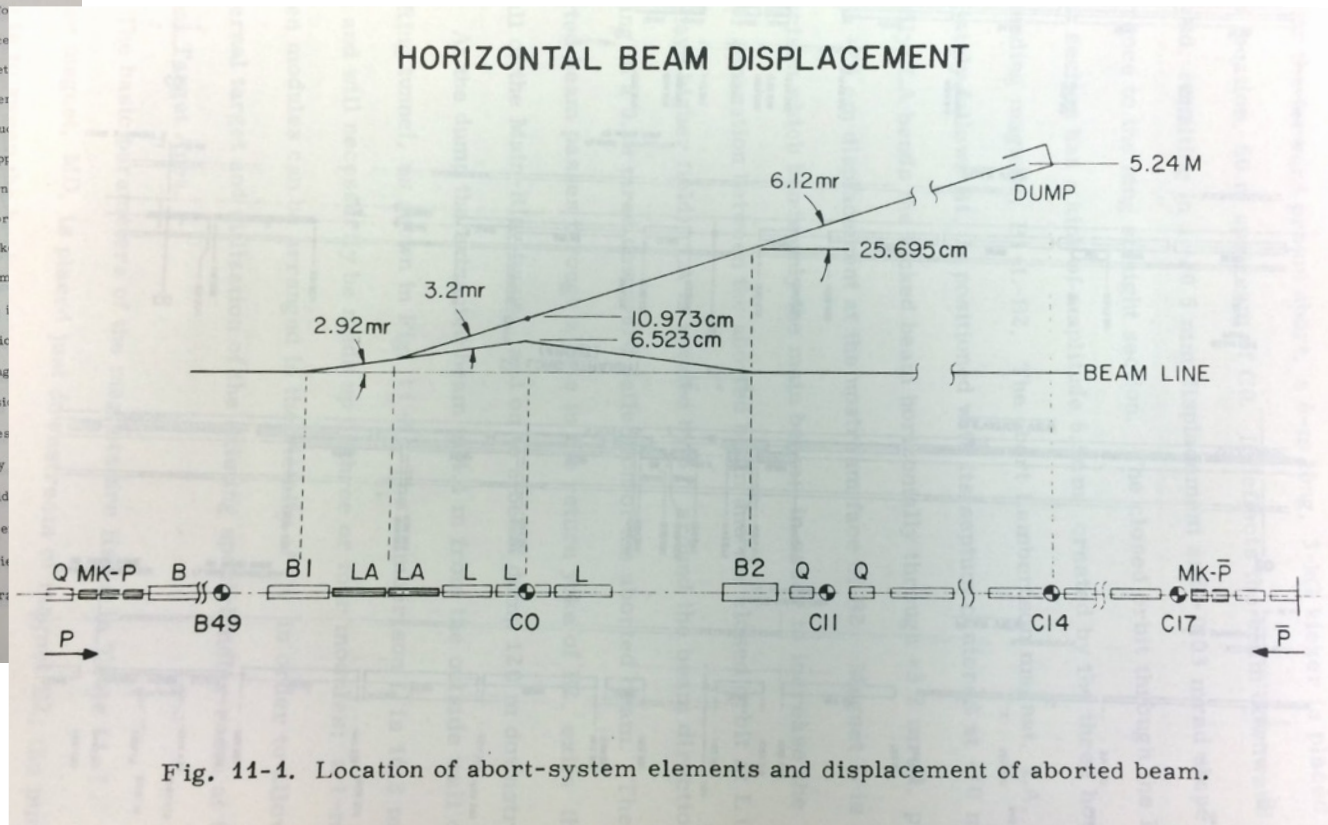
11. BEAM-ABORT SYSTEM

11.1 Requirements and General Design

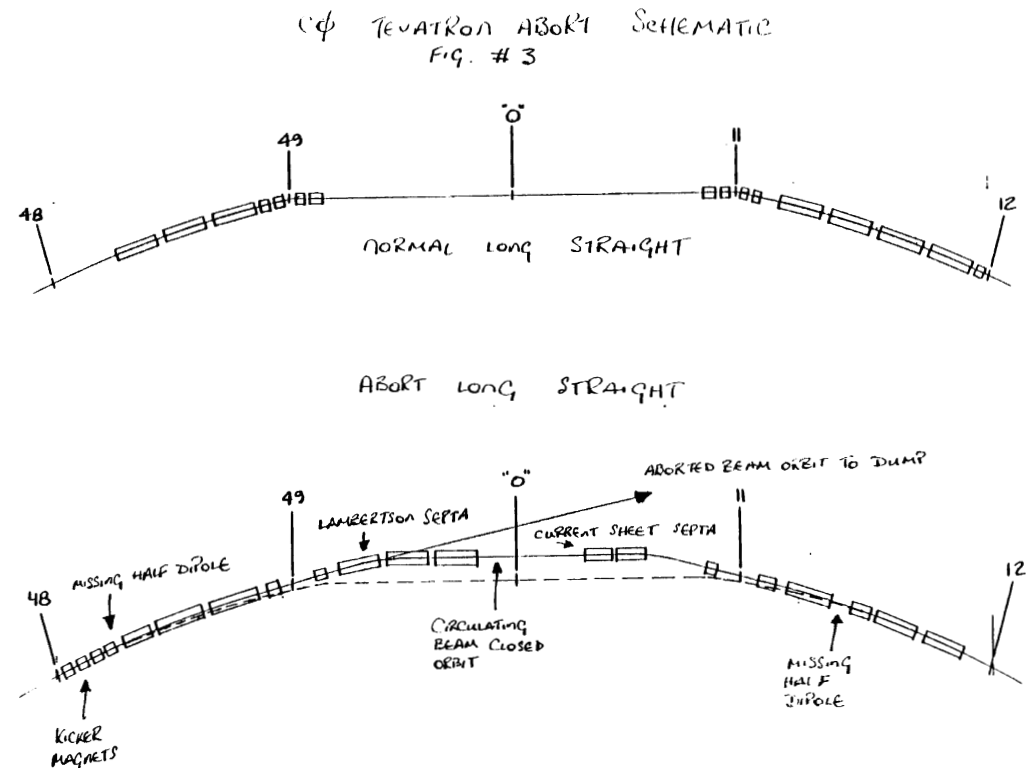
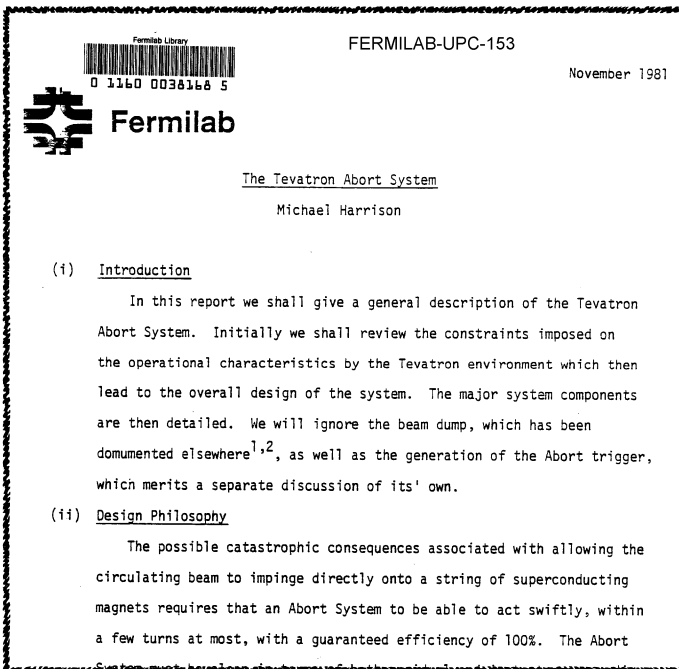
Detailed studies have shown that if even a tiny fraction of the 2×10^{13} protons circulating in the ring interact in the nearby solid material, for example, in the vacuum-chamber wall or injection or extraction device then a disruptive quench of one or more of the superconducting magnet will likely result. It is therefore imperative that a beam-abort system exist that can anticipate the imminent occurrence of such quench-induced losses and cleanly dispose of the beam before they are allowed to happen.

Clearly the most effective strategy is one of prompt single-turn extraction to an external beam dump. The basic elements of the abort system will therefore consist of a fast-rise full-aperture kick followed by a Lambertson septum magnet and a magnetic beam channel to an external beam dump. The elements of the abort system are meshed with elements of a straight-section bump (discussed in Section 10.2) used for radiation protection of the downstream superconducting magnets. The effect of beam lost on the magnetic septum and collimators inside the magnets is reduced in this way. Estimates indicate that a few times as many protons can be lost on the septum. Then the extraction inefficiency of the abort system should be less than 1%. For operation in the $\bar{p}\bar{p}$ collider an abort for the backward moving \bar{p} 's is also required. Since the number of \bar{p} 's is less than 1×10^{11} , a considerably larger inefficiency can be tolerated; a fast kick into the face of a dump block placed several meters from the closed orbit will suffice.

Energy Doubler Design Report, 1979



Tevatron Fixed Target Abort Layout



Aborted beam moves through field-free region of the Lambertson septum.
Warm bending magnets incorporated, on the same bus as SC magnets.



Tevatron *Fixed Target* Beam Dump

- Designed for 3.2 MJ over 21 μ s
- 10-20 yr lifetime

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IEEE Transactions on Nuclear Science, Vol. NS-28, No. 3, June 1981

A HIGH INTENSITY BEAM DUMP FOR THE TEVATRON BEAM ABORT SYSTEM

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Introduction

The beam abort system proposed¹ for the Fermilab Tevatron Accelerator will extract the proton beam from the ring in a single turn ($\sim 20\mu$ s) and direct it to an external beam dump. It is the function of the beam dump to absorb the unwanted beam and limit the escaping radiation to levels that are acceptable to the surrounding populace and apparatus. In addition, it is clearly desirable that it be maintenance free and have a lifetime equal to that of the accelerator, 10-20 years. A beam dump that is expected to meet these requirements has been designed and constructed. We describe below the detailed design of the dump, including considerations leading to the choice of materials.

Tevatron ring to avoid quenches induced by transient radiation from the dump during beam aborts; $s_{min} = 55m$. The cost of civil construction for the dump argues for keeping s close to s_{min} ; the incremental cost was estimated at $10K\$/m_{min}$.

Choice of Material for Dump Core

The reliability of the dump depends critically on the integrity of the material which makes up the upstream five hadronic absorption lengths (λ_a) of the core. Operating experience both at CERN and Fermilab has clearly demonstrated the capability of 400 GeV proton beams of similar size and intensity to fracture leading to the choice of materials.

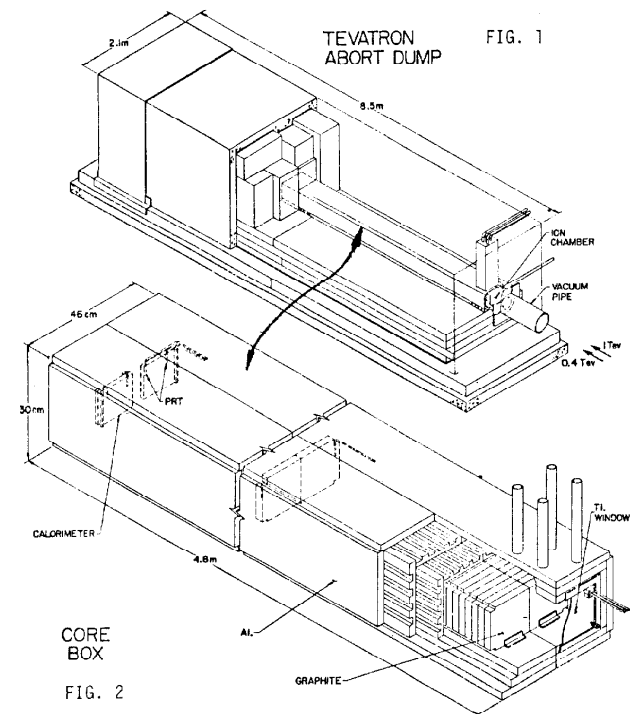


FIG. 2



Tevatron Collider Abort System

- After being reconfigured for colliding beams, the beam abort system was soon changed to an “internal abort”; desire was to re-use the “C0” straight section for a possible new interaction region
 - 980 GeV, $\sim 1 \times 10^{13}$ p \longrightarrow ~ 1.5 MJ
 - for antiprotons, eventually, up to ~ 0.75 MJ



Tevatron Internal Abort

Proceedings of the 1988 Summer Study on HEP in the 1990's, Snowmass, CO, June 6-Jul 15,

-1-

INTERNAL BEAM ABORT SYSTEM FOR THE TEVATRON UPGRADE

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INTRODUCTION

In this note we shall examine the of an internal beam dump system for running in the pbar-p collider mode that the beam energy can be as high as 1.8 TeV. The motivation behind this report is the fact that the present proton abort system is a single-turn fast-extraction system, which progressively more difficult to perform as the beam energy is raised without lengthening the straight section. We examine three designs (Fig. 1). The first is a system of two beam dumps at each end of the straight section, the second dump is an absorber for the secondary particles.

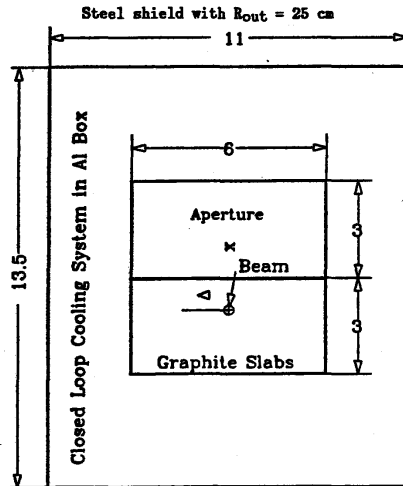


Figure 6 Core of the internal beam abort dump, Scheme 1(B). All dimensions are in cm.

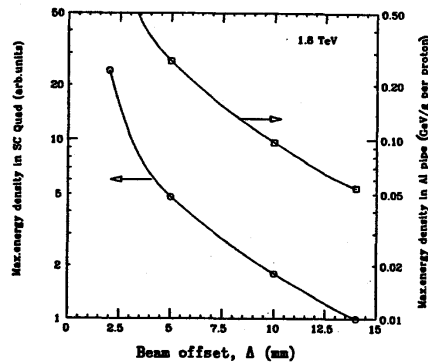


Figure 7 Maximum energy deposition density in the first downstream quadrupole superconducting coils and in the aluminum beam pipe inside the internal abort dump versus beam displacement in the dump.

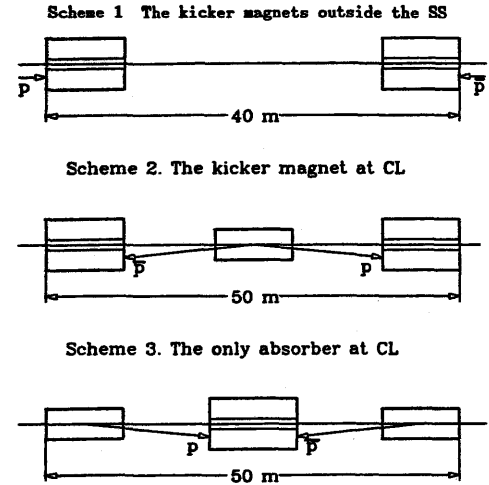


Figure 1 Three examined designs for the Tevatron internal beam dump system.

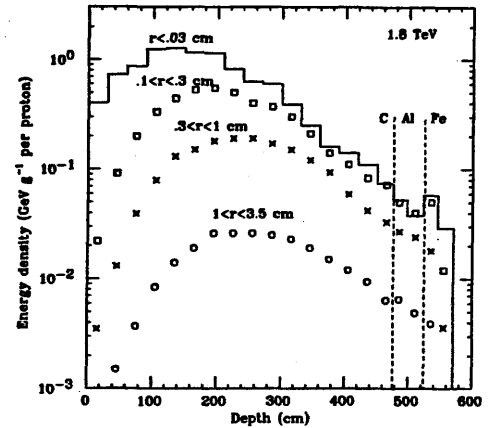
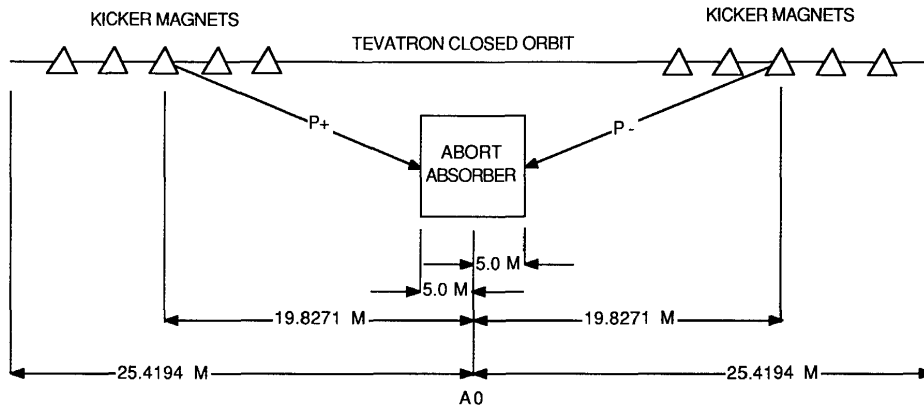


Figure 3 Longitudinal distributions of energy deposition density in the various radial bins of the core of the internal beam dump at the 1.8 TeV proton abort with a beam spot of 0.48×0.34 mm (R+V) rms.

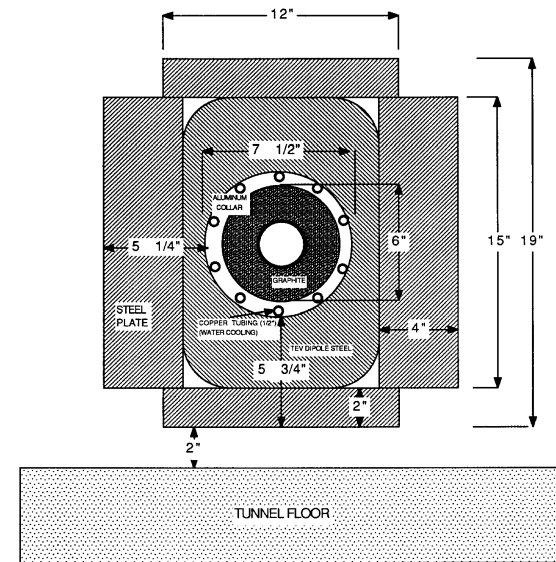


Tevatron Collider Abort System



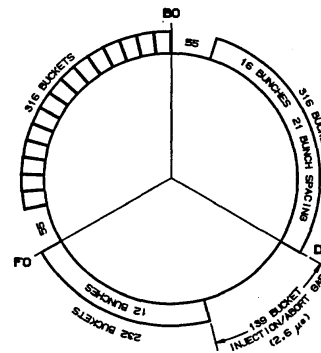
FLANGE TO FLANGE LENGTH OF EACH MAGNET IS 2.2369 METERS

FIGURE 1. TEVATRON UPGRADE ABORT LAYOUT



LENGTH OF RECTANGULAR STEEL SHELL IS 3 METERS
 LENGTH OF DIPOLE STEEL IS 4.5 M
 VACUUM TUBE IS 2.5" OD X 0.060" WT

FIGURE 9. CROSS SECTION OF THE GRAPHITE PORTION OF THE ABSORBER



ALTERNATE 44 BUNCH INJECTION PATTERN

C. Crawford, 1989



The SSC Beam Abort System

With 20 TeV per beam, and 1.3×10^{14} p per beam, yields stored beam energy of 400 MJ

On the Design of Beam Absorbers for the SSC

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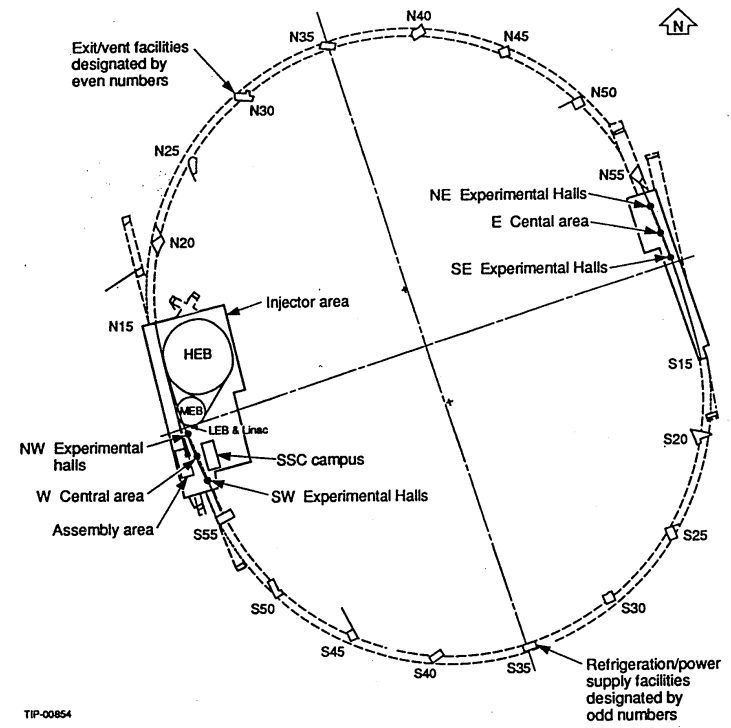
Abstract

The 20 TeV beam absorbers for the Superconducting Super Collider (SSC) present a formidable design challenge. Protons from the SSC will have: 20 times the energy, be 20 times harder to bend, and be distributed with a natural transvers-size $\sqrt{20}$ times smaller than from all previous accelerators. This paper concentrates on the thermo-physical demands made on a beam backstop in terminating 20 TeV protons. In particular radiation-shielding, logic, control, and beam diagnostic requirements will not be discussed[1]. We will report on Monte Carlo simulations, made using the MARS10 code of N. Mokhov[2], which provides a basis for evaluating beam spreading and painting scenarios. The merits of various standard painting schemes are then discussed. Finally, we

the field-free region of a string of Lambertson-style septum magnets, down a separate ~2 km long channel and into a multi-layer beam backstop. The central backstop-core will consist of graphite 10 m in extent and 2 m in diameter. Surrounding the graphite will be additional radiation-shielding and monitoring devices. Graphite will be used for the core-region both to diminish the long-term production of residual radioactivity and to maximize design-robustness (by longitudinally spreading the shower energy-deposition).

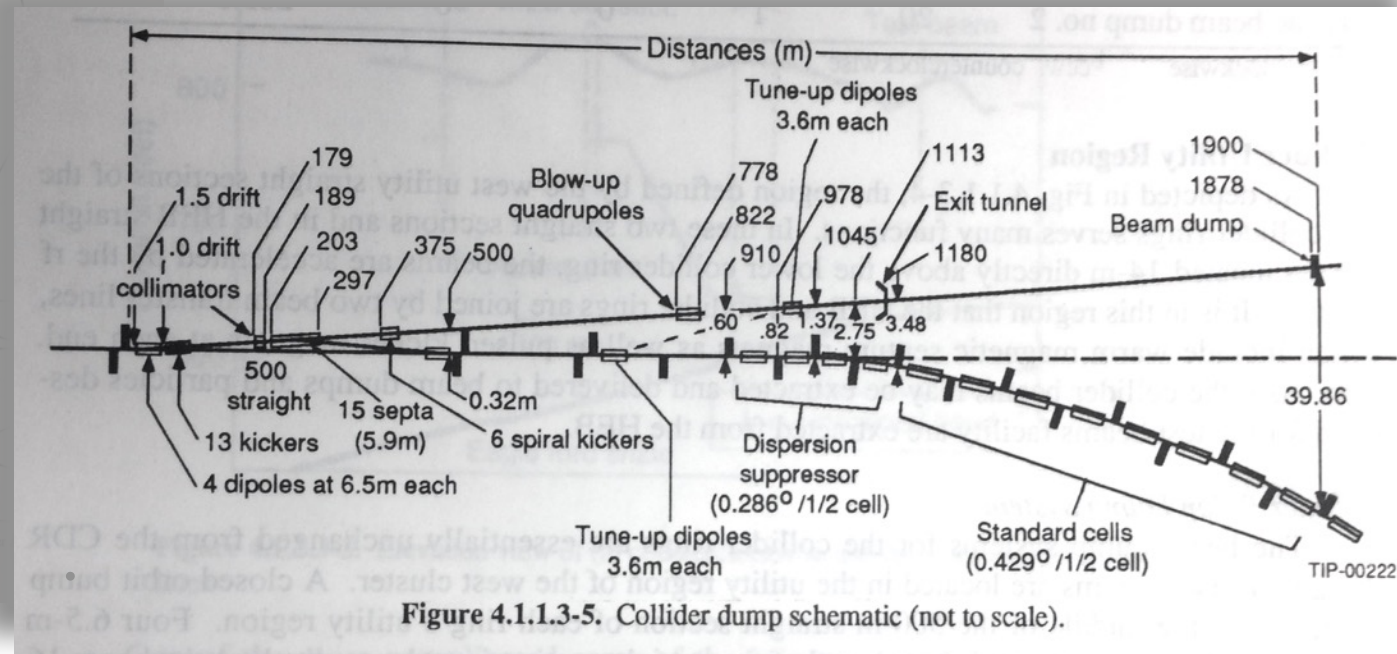
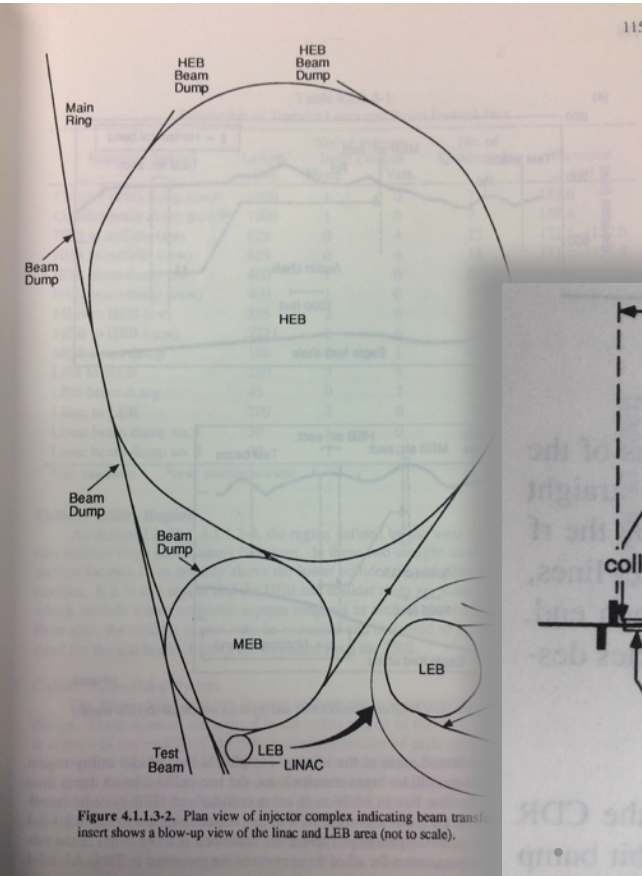
2. METHODOLOGY

The high-energy cascade showers resulting from 20 TeV protons are simulated using the MARS series of computer code of N. Mokhov[2]. The current version, MARS12, uses



The SSC Beam Abort System

Layout based much on Tevatron design

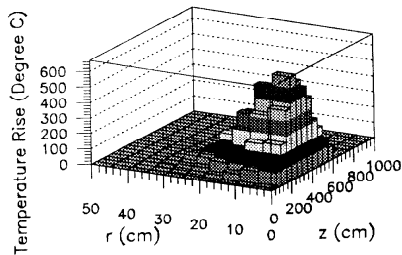


The SSC Beam Abort System

In addition to beam dump design development, the need was foreseen to spread out the beam via a sweeping or “raster” system

3. RESULTS

For the core of the beam backstop, it is desirable to choose a material with a high cracking/melting temperature and low density (to spread the shower longitudinally as much as possible); for these reasons, graphite is a natural choice. Carbon's low atomic number, also helps to reduce the amount of long-term induced radioactivity due to spallation fragments. A reference plot of $\Delta T(r,z)$, the radially-symmetric temperature distribution, due to a round-Gaussian ($\sigma=10\text{cm}$) beam profile incident along the axis of a graphite core, is shown in Figure 2, for 1.3×10^{14} protons ($=10^{33}$ luminosity).



Original “blow-up lens” system was enhanced with a spiral kicker system

“Raster Scan” painting system, using two frequencies (H/V) was chosen in the end

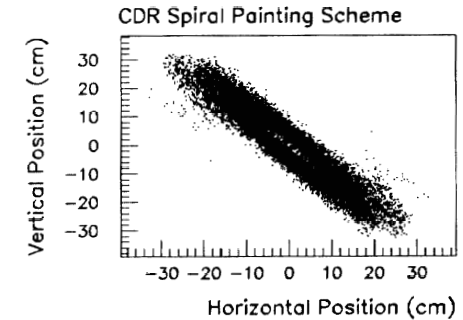


Fig. 5. CDR spiral painting with phase slippage.

A raster-pattern (shown in Figure 6) can be created via a combination of fast and slow kickers. Such a painting scheme with less needed fast-kicker strength and vastly reduced sensitivity to phase errors, is expected to be more reliable than the CDR spiral plan; however, there is some beam pile up near the outer edges of the raster pattern.

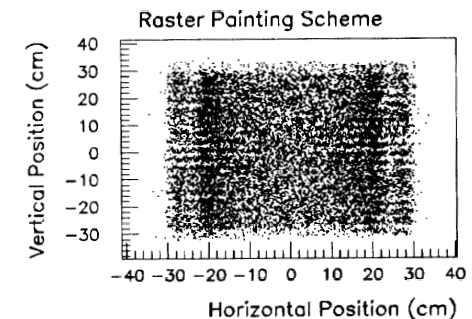


Fig. 6. Beam profile for raster painting scheme.

Hydrodynamic Calculations

- Early hydrodynamic computations of beam interacting with matter (beam pipes, magnets, tunnel walls!!, ...) began in the early 1990s with the SSC

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Hydrodynamic Calculations of 20-TeV Beam Interactions with the SSC Beam Dump

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Abstract

The 300 μ s, 400 MJ SSC proton beam must be contained when extracted to the external beam dump. The current design for the SSC beam dump can tolerate the heat load produced if the beam is deflected into a raster scan over the face of the dump. If the high frequency deflecting magnet were to fail, the beam would scan a single strip across the dump face resulting in

correctly modeled energy deposition. We chose the MARS¹ energy deposition code and both the Eulerian MESA² and Lagrangian SPHINX³ hydrodynamics codes.

ILCOMPUTER CODES

A. MESA

MESA is a two- and three-dimensional Eulerian hydrodynamics code². While originally developed for simulating

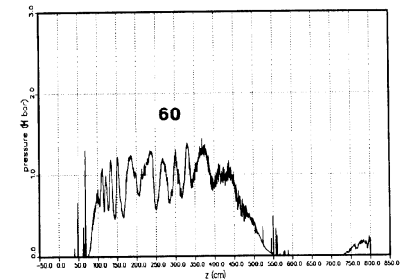


Figure 3 Axial Pressure from 2D MESA at nominal fluence

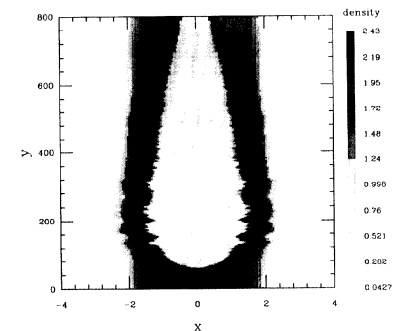


Figure 4 Density from 2D SPHINX at high fluence

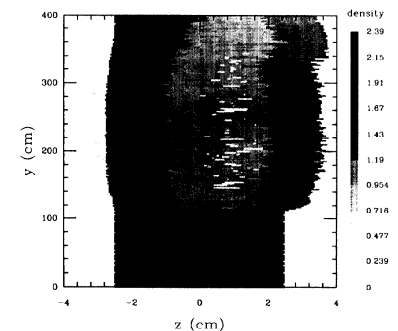


Figure 5 Density from 3D SPHINX at high fluence

12

PAC 1993

Reliability Issues — Abort Pre-Fire

- By 1990s the Tevatron had a good operational record, and a *history* of abort module pre-fires. Worried about this quite a lot at SSC

PAC 93

Dealing With Abort Kicker Prefire in the Superconducting Super Collider

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Abstract

The Superconducting Super Collider uses a single-turn extraction abort system to divert the circulating beam to a massive graphite absorber at normal termination of the operating cycle or in case of any of a number of predefined fault modes. The Collider rings must be designed to be tolerant to abort extraction kicker prefires and misfires because of the large circulating beam energy. We have studied the consequences of beam loss in the accelerator due to such prefires and misfires in terms of material heating and radiation generation using full scale machine simulations and Monte-Carlo energy deposition calculations. Some results from these calculations as well as possible protective measures for minimizing the damaging effects of kicker prefire and misfire are discussed in this paper.

I. INTRODUCTION

The Superconducting Super Collider beam[1,2] contains approximately 420 MJ of circulating beam energy

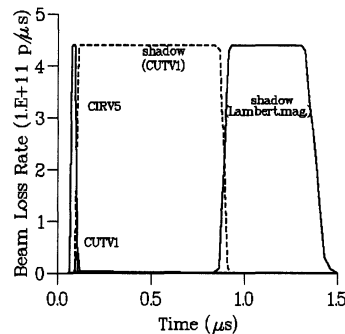


Figure 2. Beam Loss During the 3 μ s Kicker Rise Time

developed the notion of an “anti-kicker”

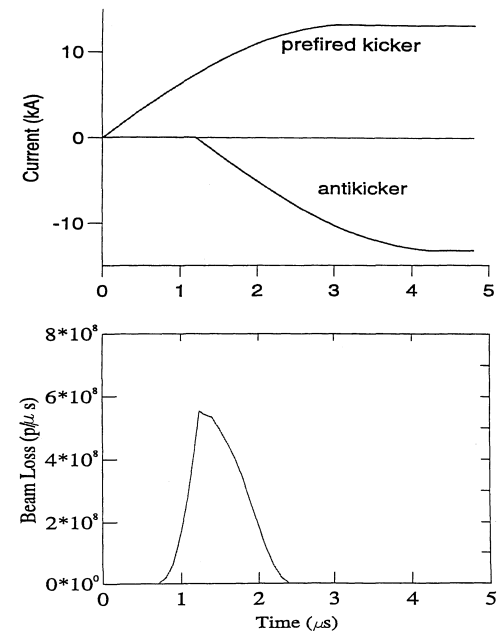


Fig. 7. Beam loss vs time for 1.2 μ s antikicker delay.



The LHC Abort System

- As this system has actually been constructed(!), many more details exist for the LHC than were developed and executed for the SSC hardware

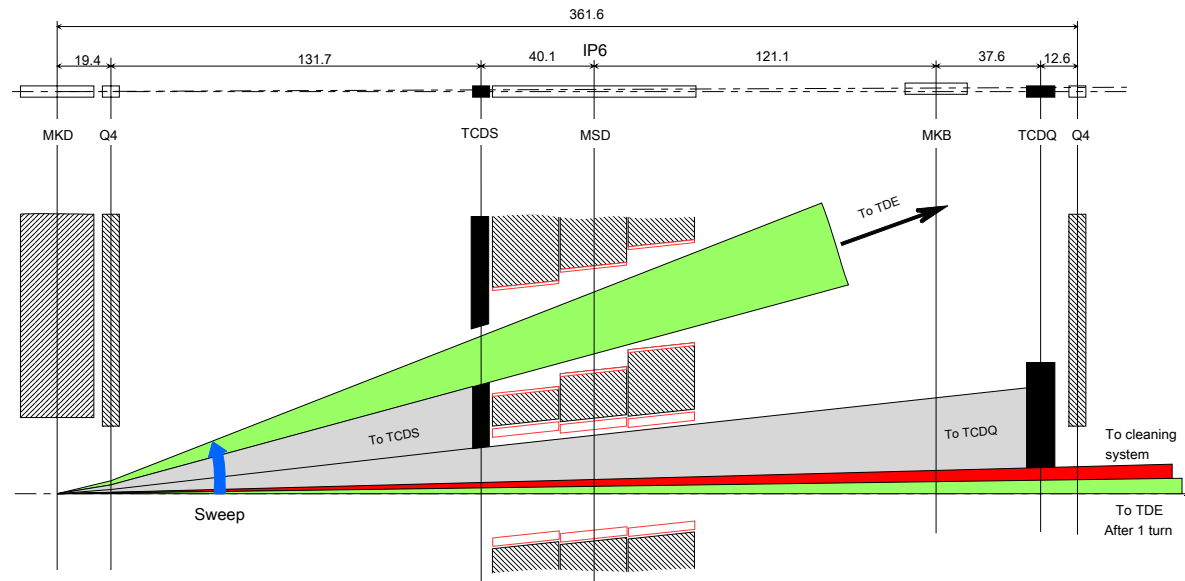
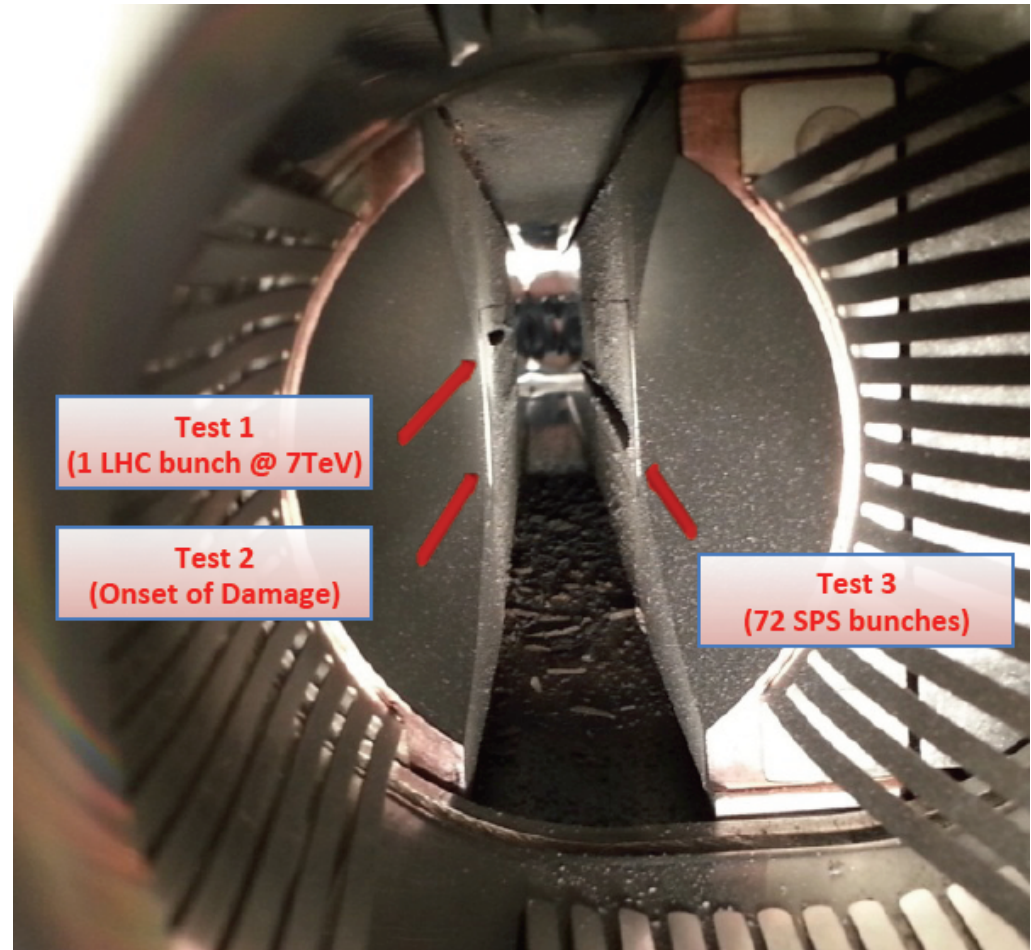


Figure 17.11: Schematic and functional layout of TCDS and TCDQ diluter systems.

Machine Protection

Many tests were performed on the LHC system components, and undoubtedly much operational experience now exists that can be used to predict performance of future FCC systems

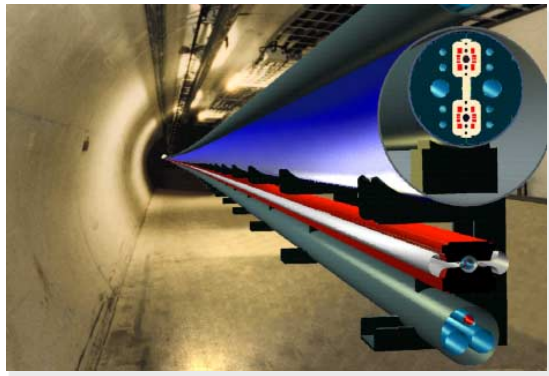
Will leave this to my CERN colleagues to discuss...



The VLHC Beam Abort Design

Design Study for a Staged Very Large Hadron Collider

Report by the collaborators of
 The VLHC Design Study Group:
 Brookhaven National Laboratory
 Fermi National Accelerator Laboratory
 Laboratory of Nuclear Studies, Cornell University
 Lawrence Berkeley National Laboratory
 Stanford Linear Accelerator Center



Design studies for a *Really* Large Hadron Collider began in mid-1990s

Culminated in the VLHC (Very Large!) report of 2001

Extracted Beam Lines and Absorbers for a 50x50 TeV Hadron Collider

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ABSTRACT

An extracted beam line has been designed for the 50 TeV or 50 TeV proton beams of the low-field version of RLHC. In order to kick the beams out of the machine in one turn, two beam absorbers have been considered: a graphite-core absorber and an atmospheric pressure air-core absorber. Using the MARS3 code, the necessary absorber dimensions and beam sizes have been determined. In the case of the graphite core, it is shown that the only feasible way to make the beams big enough is to sweep the beams around the face of the absorbers during the 1.8 ms spill time. This is not needed for the air-core absorber, but an extra 8 Km of tunnel is needed.

1. INTRODUCTION

As currently designed, the low-field version of the RLHC [1] has 1.12E15 protons circulating at 50 TeV in each beam, i.e., 9 GJ per beam. That is enough energy to cause severe damage to the machine and environment. The beams have sizes (σ) of typically 0.07 mm in the arcs and 0.14 mm at the center of a utility straight section (assuming a normalized emittance of 1 a mm-mrad). Obviously, if such a beam goes astray, it will melt a hole through a magnet and do further damage outside the machine [2]. The requirements for the reliability of a one-turn extraction mechanism are orders-of-magnitude greater than for the Tevatron, where a misfired extraction kicker magnet only causes a quench of the machine.

It turns out to be quite straight forward to kick the beams out of the machine towards absorbers. A scaled-up

Like the Tevatron [4] and the SSC [5], the LHC design uses fast kicker magnets to switch the circulating beams into the other aperture of Lambertson magnets. Unlike the Tevatron and the SSC, the circulating beams go through the field-free holes in the Lambertson magnets, and the extracted beams are bent upward in the Lambertson magnets so as to clear the first quadrupoles in the downstream half of the straight section (see Fig. 1). The total length of the

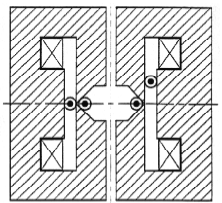


Figure 1: The LHC dual-bore Lambertson magnet.

straight section is 526 m. We have taken the length of the RLHC straight section to be 2000 m [6]. To scale the LHC straight section to the RLHC, we simply multiplied all the magnet spacings by the factor 2000/526. This leads to a layout for the RLHC straight section shown in Fig. 2. The

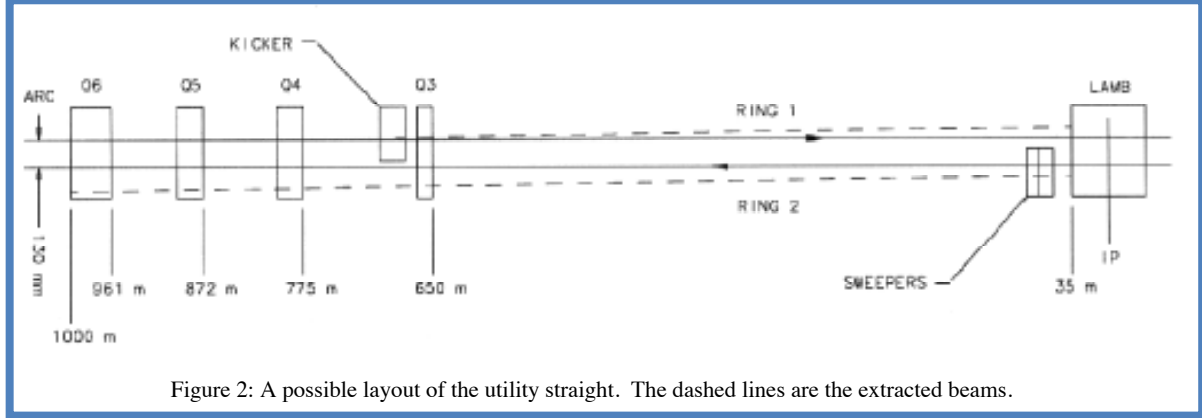


Figure 2: A possible layout of the utility straight. The dashed lines are the extracted beams.

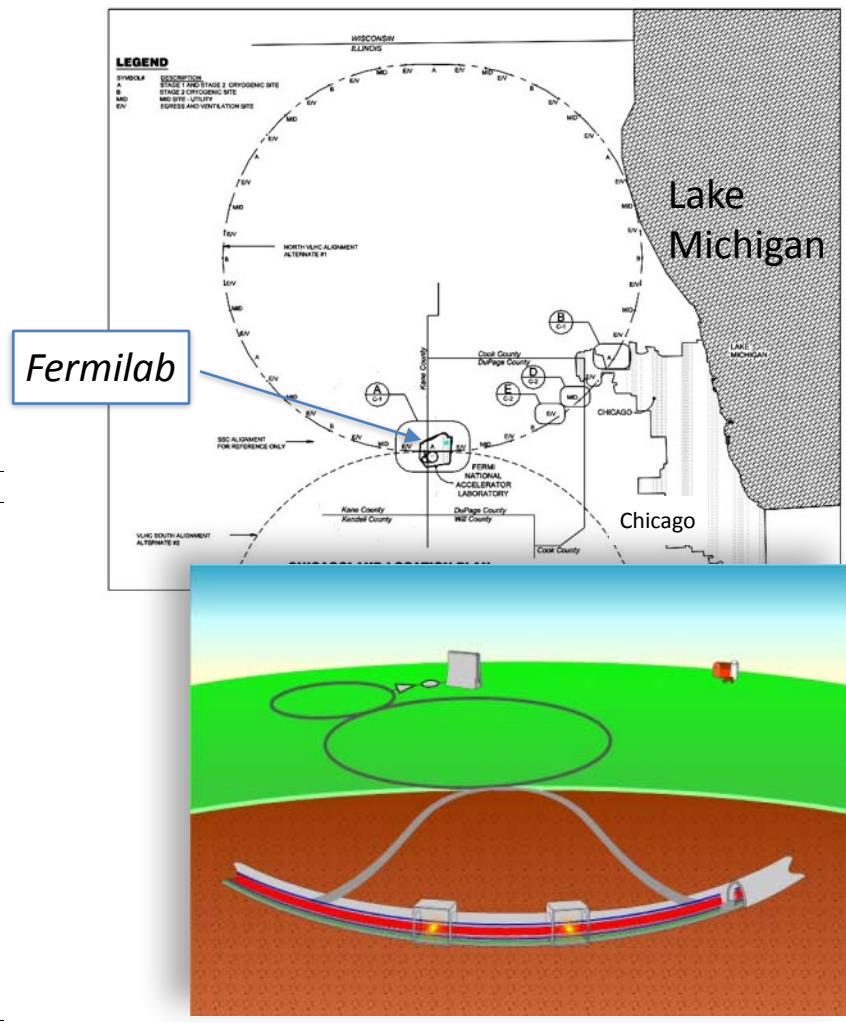


VLHC Parameters

- Stage 1: 20 TeV; 3.0 GJ
- Stage 2: 240 TeV; 3.9 GJ

Table 1.1. The high-level parameters of both stages of the VLHC.

	Stage 1	Stage 2
Total Circumference (km)	233	233
Center-of-Mass Energy (TeV)	40	175
Number of interaction regions	2	2
Peak luminosity (cm ⁻² s ⁻¹)	1 × 10 ³⁴	2.0 × 10 ³⁴
Luminosity lifetime (hrs)	24	8
Injection energy (TeV)	0.9	10.0
Dipole field at collision energy (T)	2	9.8
Average arc bend radius (km)	35.0	35.0
Initial number of protons per bunch	2.6 × 10 ¹⁰	7.5 × 10 ⁹
Bunch spacing (ns)	18.8	18.8
β* at collision (m)	0.3	0.71
Free space in the interaction region (m)	± 20	± 30
Inelastic cross section (mb)	100	130
Interactions per bunch crossing at L _{peak}	21	54
Synchrotron radiation power per meter (W/m/beam)	0.03	4.7
Average power use (MW) for collider ring	25	100
Total installed power (MW) for collider ring	35	250



The VLHC Beam Abort Design

- A new concept developed during the VLHC investigation:
 - a “graphite shadow”
 - sacrificial device

Proceedings of the 2001 Particle Accelerator Conference, Chicago

BEAM-INDUCED ENERGY DEPOSITION ISSUES IN THE VERY LARGE HADRON COLLIDER*

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Abstract

Energy deposition issues are extremely important in the Very Large Hadron Collider (VLHC) with huge energy stored in its 20 TeV (Stage-1) and 87.5 TeV (Stage-2) beams. The status of the VLHC design on these topics, and possible solutions of the problems are discussed. Protective measures are determined based on the operational and accidental beam loss limits for the prompt radiation dose at the surface, residual radiation dose, ground water activation, accelerator components radiation damage and quench stability. The beam abort and beam collimation systems are designed to protect accelerator from accidental and operational beam losses. IR region quadrupoles from irradiation

On a large scale, muon fluxes around the machine can drive the complex layout and other related issues. Many other radiation issues, such as radiation damage to electronics and other sensitive equipment in the tunnel, radiation streaming to the surface through access and ventilation shafts, unsynchronized beam abort etc., are or will be attacked. Here we consider just a few most important issues.

1.2 Superconducting Magnets

The warm-iron design of the transmission line magnet of the Stage-1 [1] is less sensitive to radiation-induced quenches than ordinary magnets. To determine tolerable

2 BEAM ABORT SYSTEM

It turns out to be quite straight forward to kick the beams out of the machine towards absorbers (Fig. 3). Like the Tevatron, SSC and LHC, a single-turn extraction is used to switch the circulating beam from the field-free hole to the field gap of the Lambertson magnets, which extract the beam from the machine. Separation of the circulating and extracted beams is 25 mm at the entrance to the Lambertson magnets. Special large-aperture warm quadrupoles are used upstream of the Lambertsons so that no aperture restriction and quench problem exist. To protect the Lambertson septa and some other critical components from accidental destruction by the beam, resulting from a kicker timing error, it was proposed to put a graphite shadow right in front of these components [5]. The shadow piece, a few cm across and 4-m long at 20 TeV, is an inert device with an aperture the same as that of the adjacent component which it protecting.

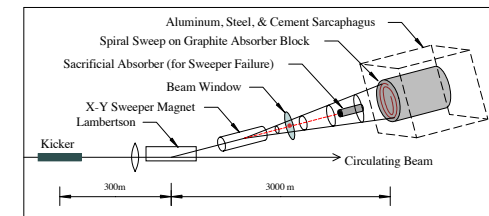


Figure 3: Schematic layout of beam abort channel.

For TeV beams, the natural choice for the absorber is



The VLHC Beam Abort Design

5.3.2.3 Beam Sweeping System

A spiral beam sweeping scheme similar to the SSC and LHC is used to spread energy across the absorber core. The magnets are described in Sec 5.3.2.2 and a vertical sweeper, 90° out of phase, both oscillate with decay frequency should increase as the radius of the spiral decreases in order to rise constant. Since this is electrically difficult, a suitable compromise is to keep the temperature below 1500 °C. If the beam sigma was 0.5 mm, the frequency of these sweepers would be 9.7 kHz.

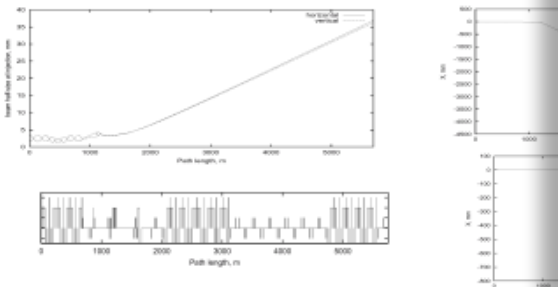


Figure 5.56. Beam sweeping system optics. Left: 3-sigma beam half-size (at 20 TeV is 4.5x smaller), and beam line layout. Right: beam displacement extraction straight section and maximum sweeping kick in the hole

The requirements for the reliability of a one-turn extraction mechanism are comparable to the SSC [90] and LHC [91]. The extraction kicker is broken into 10 independent modules, with any 7 out of 10 sufficient for a safe abort. Solid-state pulsers (as opposed to Thyratrons) will be used to minimize accidental prefires. Three Musketeer logic (“All-for-one, and one-for-all!”) guarantees that any single module firing will automatically trigger the rest of the modules.

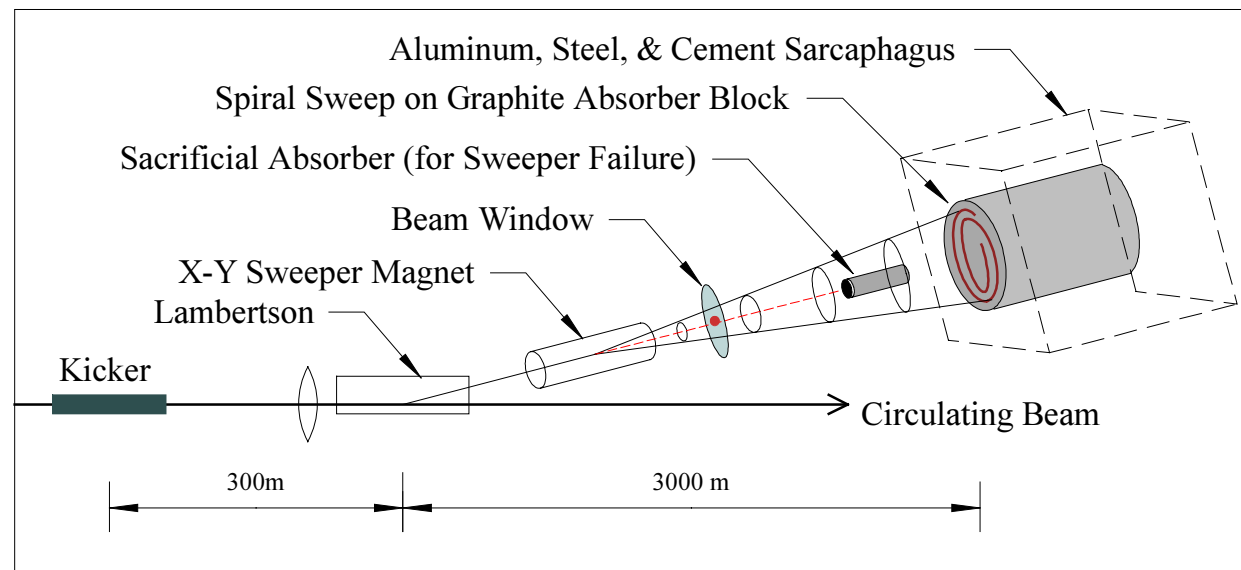


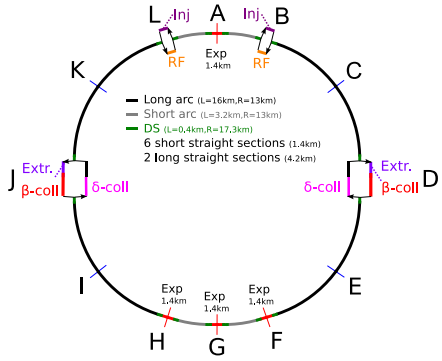
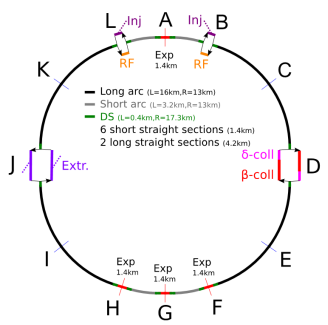
Figure 5.55. Schematic layout of beam abort channel including kickers, Lambertson septa, extraction beam sweeping, beam window, sacrificial rod, and graphite beam absorber. Under normal circumstances the extracted beam is swept in a spiral pattern to spread the energy across the graphite dump. If the sweeper magnet fails, the beam travels straight ahead into a sacrificial graphite rod, which takes the damage and must be replaced.



FCC Beam Abort — 8.4 GJ beams

Alternative Baseline Option

- Betatron and energy collimation are lumped together
- Potentially improved collimation efficiency
- Betatron collimation system followed by energy collimation in each beam
- How much separation is required?
- Both beams are extracted in the same insertion
- Have to figure out best configuration



FCC is looking at alternate layouts for collimation (betatron, momentum) and extraction systems

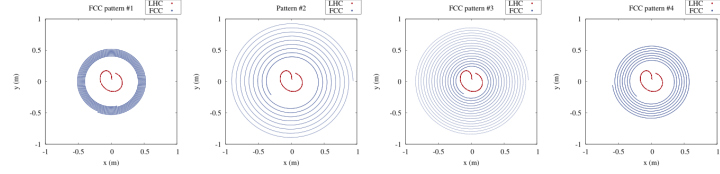


A. Lechner, FCC dump meeting, 20th Jan. 2016

Overview of multi-spiral dilution patterns (from F. Burkart)

MKB frequency modulation	Frequency	B · dl ³	Distance between neighbouring bunches	Distance between neighbouring branches	
#1 ^b	No	32.8 kHz	34 Tm	2.00–2.64 mm	1.6 cm
#2	No	32.8 kHz	56 Tm	1.87–4.70 mm	6.5 cm
#3 ^c	No	50.9 kHz	53 Tm	1.83–6.95 mm	4.0 cm
#4 ^c	Yes	20–43 kHz	39 Tm	1.90 mm	3.7 cm

^a) For a dump line length of 2.5 km. ^b) See F. Burkart, FCC Dump Meeting, 02/07/2015. ^c) See F. Burkart, FCC Dump Meeting 02/12/2015.



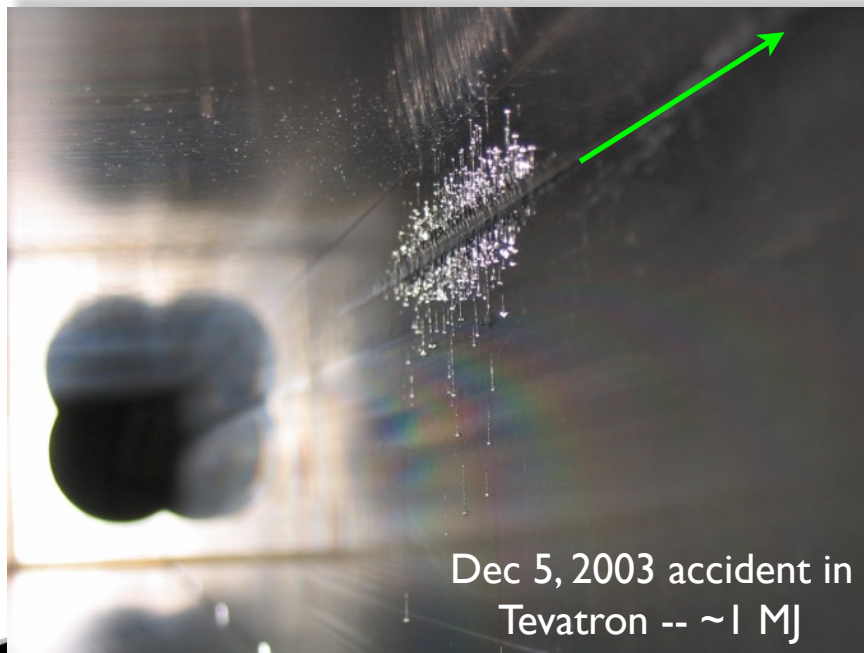
- Some remarks:
 - Pattern **do not yet account for realistic filling schemes** including gaps → this will still increase the total sweep path length by several 10%
 - Only studied regular sweeps as shown above, but **did not yet assess the consequences of failure scenarios** for the different pattern/kicker parameters

Spiral dilution patterns appear to produce acceptable local energy density for FCC conditions; under study (see talks later this session)



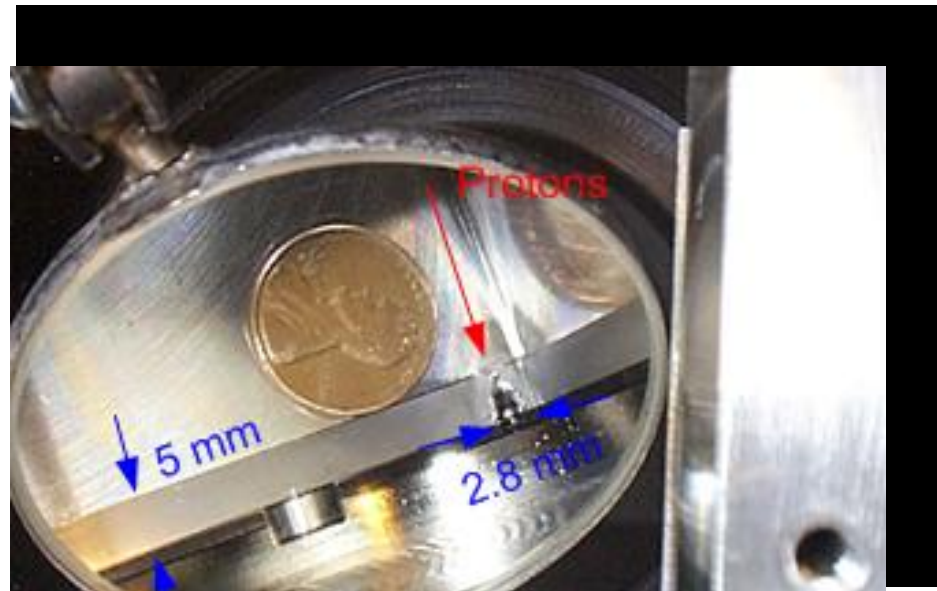
Tevatron Beam Incident of 5 Dec 2003

- The abort system fired, but not before the beam was moved to the edge of the collimator by a decaying power supply to a corrector magnet



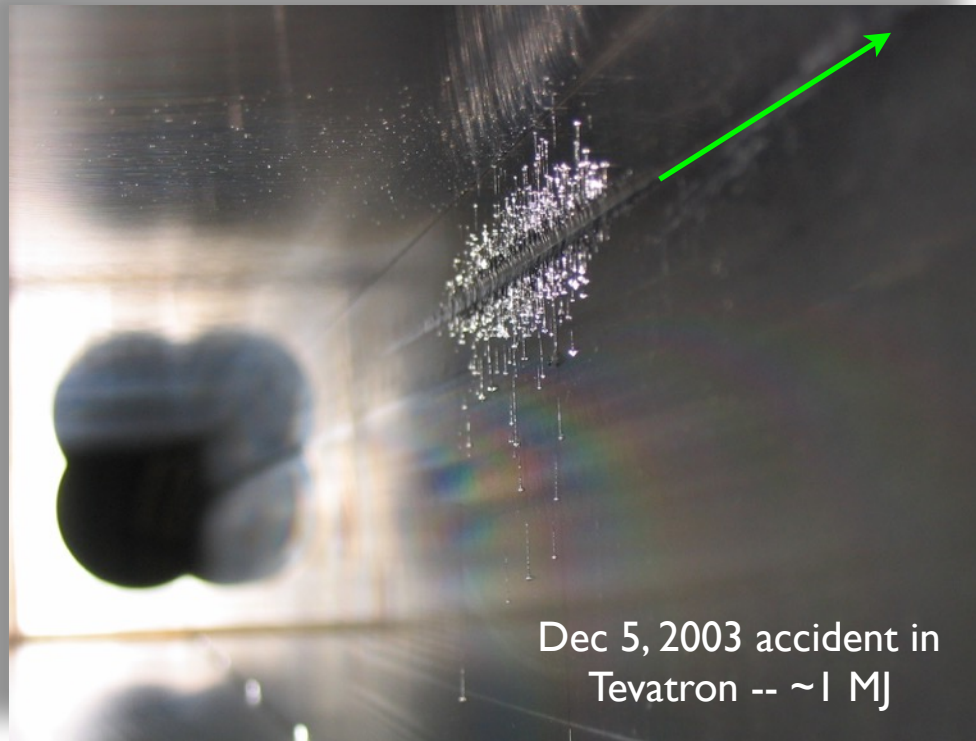
E03 1.5m collimator

~1 MJ beam stored energy, 0.98 TeV



D49 target

Note: this beam loss corresponds to
 10^{-4} of total **FCC** beam energy!



Comments on FCC Beam Abort

- New, much higher level of beam energy
- SC magnet fields go up; NC fields have not
- thus, when incorporating NC magnets need much more space to create required angular deflections
- Possible to incorporate similar concepts into FCC design, but really in need of a new concept...
 - incorporating rad-hard HTS magnets ??



SSC Documents (full texts available on INSPIRE)

1. [Beam Loss and Radiation Effects in the SSC Lattice Elements](#)
I.S. Baishev, A.I. Drozhdin, N.V. Mokhov ([Serpukhov, IHEP](#)). Jul 28, 1990. 92 pp.
2. [Hydrodynamic calculations of 20-TeV beam interactions with the SSC beam dump](#)
D.C. Wilson, C.A. Wingate, John C. Goldstein, R.P. Godwin (Los Alamos), N.V. Mokhov (SSCL). 1993. 3 pp.
Published in Conf.Proc. C930517 (1993) 3090-3092
3. [2-TeV HEB Beam Abort at the SSCL](#), [R. Schailey](#), [J. Bull](#), [T. Clayton](#), [P. Kocur](#), [N.V. Mokhov \(SSCL\)](#). May 1993. 3 pp., Published in **Conf.Proc. C930517 (1993) 1369-1371**, SSCL-PREPRINT-419, C93-05-17
4. [Dealing with Abort Kicker Prefire in the Superconducting Super Collider](#)
[A.I. Drozhdin](#), [I.S. Baishev](#), [N.V. Mokhov](#), [B. Parker](#), [R.D. Richardson](#), [J. Zhou \(SSCL\)](#). May 1993. 3 pp.
Published in **Conf.Proc. C930517 (1993) 3772-3774**, SSCL-PREPRINT-329, C93-05-17
5. [Consequences of Kicker Failure during HEB to Collider Injection and Possible Mitigation](#)
[R. Soundranayagam](#), [A.I. Drozhdin](#), [N.V. Mokhov](#), [B. Parker](#), [R. Schailey](#), [F. Wang \(SSCL\)](#). May 1993. 3 pp.
Published in **Conf.Proc. C930517 (1993) 1360-1362**, SSCL-PREPRINT-358, C93-05-17
6. [Beam Loss Monitor System for the SSC](#), [R.G. Johnson](#), [N.V. Mokhov \(SSCL\)](#). Oct 1993. 10 pp.
Published in In ***Santa Fe 1993, Beam instrumentation* 191-200**. SSCL-PREPRINT-523, C93-10-20
7. [Accidental Beam Loss in Superconducting Accelerators: Simulations, Consequences of Accidents and Protective Measures](#), [A. Drozhdin](#), [N. Mokhov](#), [B. Parker \(SSCL\)](#). Feb 1994. 31 pp.
Published in **Submitted to: Nucl.Instrum.Meth.** , SSCL-PREPRINT-556



VLHC Documents (full texts available on INSPIRE)

1. [Beam-induced energy deposition issues in the Very Large Hadron Collider](#)
N.V. Mokhov, A.I. Drozhdin, G.W. Foster (Fermilab). Jun 2001. 3 pp.
Published in [Conf.Proc. C0106181 \(2001\) 3171-3173](#), FERMILAB-CONF-01-135, PAC-2001-RPAH137
2. [Design Study for a Staged Very Large Hadron Collider](#)
[VLHC Design Study Group](#) Collaboration ([Giorgio Ambrosio et al.](#)). Jun 2001. 271 pp.
SLAC-R-591, SLAC-R-0591, SLAC-591, SLAC-0591, FERMILAB-TM-2149

see also: <http://lss.fnal.gov/archive/other/ssc/>

*Thank you to Nikolai Mokhov
for input and for the list of
SSC/VLHC documents!*

