

# TELE script

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- Code to automatically produce 4 lens telescopes with given magnification
- used in FFADA program
- rewritten from FORTRAN to Python
- based on calculations for 3 thin lenses  $\rightarrow$  requires:
  - first drift length (e.g.  $L^*$ )
  - last drift length (little to no impact on result when kept short)
  - first quadrupole (roughly defined by  $L^*$  and maximum gradient)
- $\Rightarrow$  ideal for FFS design

## 4 Lens System

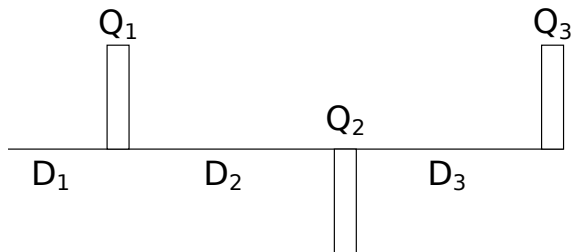
$$M_{tot} = D_4 \cdot Q_4 \cdot D_3 \cdot Q_3 \cdot D_2 \cdot Q_2 \cdot D_1 \cdot Q_1 \cdot D^*$$

$L^*$  is given, first guess for  $Q_1$  is defined by  $L^*$  and max. gradient,  $D_4$  chosen freely (result depends only weakly on  $D_4$ ),  $M_{tot}$  defined by magnification

$$\Rightarrow D_4^{-1} M_{tot} D^{*-1} Q_1^{-1} = Q_4 \cdot D_3 \cdot Q_3 \cdot D_2 \cdot Q_2 \cdot D_1 = M_3 \text{ lens}$$

→ reduced 4 lens system to 3 lens system

## 3 thin lenses



$$Q_3 \cdot D_3 \cdot Q_2 \cdot D_2 \cdot Q_1 \cdot D_1 = M_3 \text{ lens in } x \text{ and } y \quad (1)$$

→ 8 nonlinear equations to solve (numerically expensive) with many unphysical solutions (e.g. negative drifts)

→ using iterative method by Y-C Chao (1992) instead

# Iterative methode

Step 1:

$$Q_2 \cdot D_2 = M^1 \quad (2)$$

$$\Rightarrow \begin{bmatrix} 1 & L_2 \\ K_2 & 1 + K_2 L_2 \end{bmatrix} = M^1$$

$$\Rightarrow L_2 = M_{1,2}^1 \quad K_2 = M_{2,1}^1$$

$$\Rightarrow \begin{bmatrix} 1 & M_{1,2}^1 \\ M_{2,1}^1 & 1 + M_{1,2}^1 M_{2,1}^1 \end{bmatrix} = M^1 \quad (3)$$

Step 2:

$$M^1 = Q_2 \cdot D_2 = D_3^{-1} M^2 Q_1^{-1} \quad (4)$$

Using Eq. 3 we get expressions for  $L_3, K_1, L_2, K_2$  as functions of matrix  $M^2$

Step 3:

$$M^2 = D_3 \cdot Q_2 \cdot D_2 \cdot Q_1 = Q_3^{-1} M^3 D_1^{-1} \quad (5)$$

similar to Step 2 just with larger equations

*"The algebra involved in this step is too massive to be reproduced here."*

Y-C Chao

## REFERENCE

1. U. Napoly, Thin lens telescopes for final focus systems, CERN/LEP-TH/89-69, CERN Note 102.

## APPENDIX A EXPLICIT FORMS OF X, Y, AND Z IN EQ. (3.18)

By careful manipulation of Eq. (1.2), taking advantage of the simplified forms for the sum and difference of its  $x$ -part and  $y$ -part, one arrives at two independent and relatively simple equations for  $L_1$  and  $K_3$  as follows:

$$\begin{aligned} [g^2 - 2(g-1)g]K_3L_1 + (g-1)B\bar{K}_3 + (g-1)C\bar{L}_1 + g(g-1)^2 &= 0, \\ [(g-1)g^2 - g^2] \bar{K}_3L_1 - (g-1)gB\bar{K}_3 & \quad (A.1) \\ -[g-1]gC\bar{L}_1 + [g-1]C\bar{B} - g^2(g-1) &= 0 \end{aligned}$$

where

$$\begin{aligned} \bar{K}_3 &= gK_3 - \varepsilon, & \bar{L}_1 &= gL_1 - \lambda \\ \bar{B} &= (g\bar{B} - B), & \bar{C} &= (g\bar{C} - C) \\ \bar{I} &= \frac{M_{11} + M_{12}}{2}, & \bar{e} &= \frac{M_{21} - M_{22}}{2} \\ \bar{J} &= \frac{M_{11} + M_{12}}{2}, & \bar{h} &= \frac{M_{21} - M_{22}}{2} \\ \bar{r} &= \frac{M_{21} + M_{22}}{2}, & \bar{z} &= \frac{M_{11} - M_{12}}{2} \end{aligned}$$

Elimination of say,  $K_3$  in Eq. (A.1) thus leads to the following equation:

$$A_1L_1^2 + B_1L_1 + C_1 = 0, \quad (A.2)$$

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where

$$\begin{aligned} A_1 &= (g-1)(g-a)(g+a)C, \\ B_1 &= -(2g^2 - 2g - g^2)B\bar{C} - g(g^2 - 2g^2 - 2g^2g^2 + g^2 + g^2g^2 + g^2), \\ C_1 &= (g-1)B(\bar{B}C + g^2 - g^2 - g^2). \end{aligned}$$

The above expression is really more symmetric in the matrix elements if one uses the explicit forms of  $g$  and  $\varepsilon$ :

$$\begin{aligned} A_1 &= \hat{C}(M_{21}M_{11})(M_{21} + M_{22} - 2), \\ B_1 &= \frac{-\hat{B}\hat{C}(M_{21}^2 + 5M_{21}M_{22} - 4M_{21} + M_{22}^2 - 4M_{22})}{4} \\ &\quad - \frac{(2M_{11} - 2M_{12})}{18} (M_{21}^2 - 8M_{21}M_{22} + 7M_{22}M_{21} \\ &\quad - 4M_{21}^2 + 7M_{21}M_{22} + M_{22}^2 - 4M_{22}^2), \\ C_1 &= \frac{-B(M_{21} + M_{22} - 2)(2M_{21}M_{21}^2 - M_{21}^2 - 2M_{21}^2M_{22} + M_{22}^2 - 4BC)}{3} \end{aligned}$$

Finally  $A$ ,  $r$ , and  $\varepsilon$  in equation Eq. (3.15) are given by

$$X = 2Ae, \quad Y = -B, \quad \text{and} \quad Z = B^2 - 4A_1C_1. \quad (A.3)$$

The complexity of Eqs. (A.2) and (A.3) does not pose any problem in terms of coding into a FORTRAN program and maintaining high degrees of accuracy and efficiency.

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Eq. (3.18) into equations obtained at earlier stages of the iteration with fewer elements:

$$K_3 = -\frac{-2 + M_{e22} + M_{y22} - M_{e21}L_1 - M_{y21}L_1}{-M_{e12} + M_{y12} + M_{e11}L_1 - M_{y11}L_1},$$

$$K_1 = \frac{K_2 D}{D}, \quad K_3 = \frac{K_2 D}{D},$$

$$L_2 = \frac{L_2 D}{D}, \quad L_3 = \frac{L_3 D}{D}, \quad (3.19)$$

where

$$K_{1D} = -M_{e21} - M_{y21} + M_{e11}K_3 - M_{y11}K_3,$$

$$L_{2D} = -(M_{y12} - M_{y11}L_1)(M_{e22} - M_{e12}K_3 - (M_{e21} - M_{e11}K_3)L_1) + (M_{e12} - M_{e11}L_1)(M_{y22} + M_{y12}K_3 - (M_{y21} + M_{y11}K_3)L_1),$$

$$K_{2D} = (M_{y21} + M_{y11}K_3)(M_{e22} - M_{e12}K_3 - (M_{e21} - M_{e11}K_3)L_1) + (M_{e21} - M_{e11}K_3)(M_{y22} + M_{y12}K_3 - (M_{y21} + M_{y11}K_3)L_1),$$

$$L_{3D} = -M_{e12} + M_{y12} + M_{e11}L_1 - M_{y11}L_1,$$

$$D = -M_{e30} + M_{y30} + M_{e10}K_3 + M_{y10}K_3 + M_{e21}L_1 - M_{y21}L_1 - M_{e11}K_3L_1 - M_{y11}K_3L_1.$$



- no simple criterion to ensure physical solutions
- no proof the results are always real numbers
- explicit solution  $\rightarrow$  fast numerical calculation

# Finding physical solutions

- physical solution (i.e. positive drift lengths) not guaranteed → introduction of *Figure Of Merit*

$$FOM = \frac{1}{\sum_i L_i \cdot \sum_j K_j}$$

- maximizing FOM = best balance between overall length and integrated Quadrupole strength (chromaticity)
- TELE increases/decreases length of first quadrupole (without changing gradient) till a local maximum of the FOM is found
- physical solution still not guaranteed but more likely
- optimum solution also not guaranteed due to search for local maximum

- O. Napoly, B. Dunham, 'FFADA, Computer Design of Final Focus Systems for Linear Colliders', EPAC94, London, England, June 1994, p. 698
- Y-C Chao, J. Irwin, 'Solution of a Three-Thin-Lens System', SLAC-PUB-5834 (1992)
- B. Zotter, 'Design Considerations for a Chromatically Corrected Final Focus System for TeV Colliders', CLIC-Note-64 (1988)
- O. Napoly, 'Thin Lens Telescopes for Final Focus Systems', CLIC Note 102 (1989)