

Electro-mechanical measurements of mechanical lap joint of HTS STARS conductors

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Outline

Joint-winding of HTS helical coils is a challenging option for LHD-type helical fusion reactor FFHR-d1. The coil is wound by joining HTS STARS (stacked tapes assembled in rigid structure) conductor segments with mechanical joints.

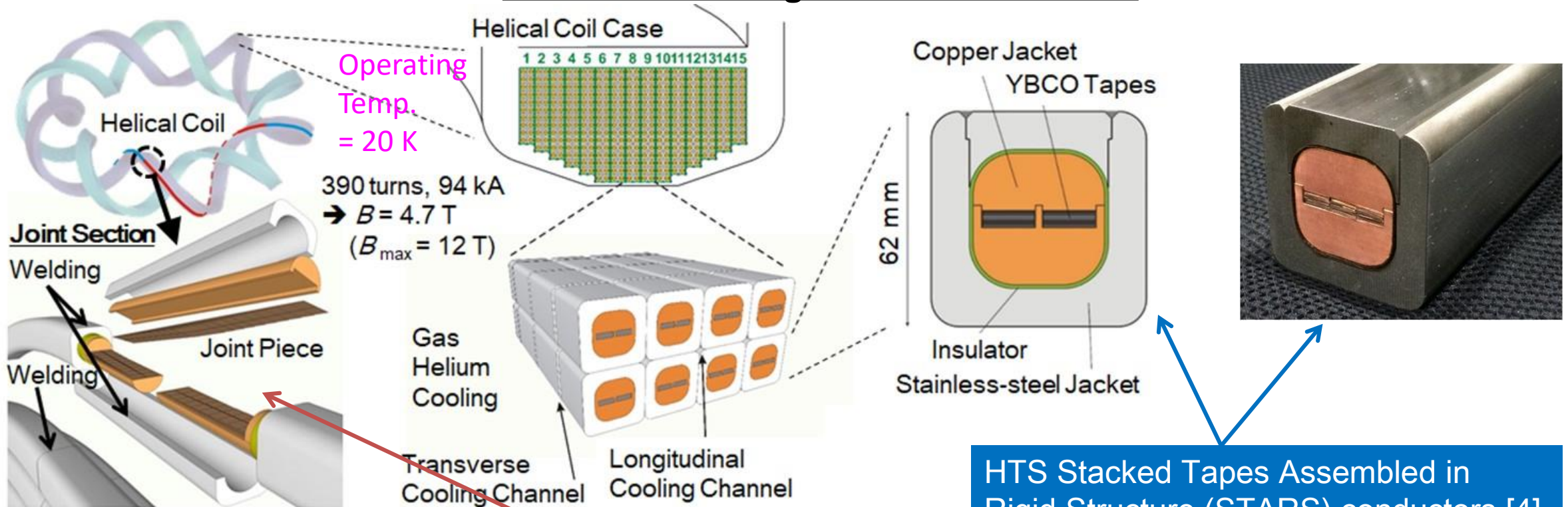
We plan to do electro-mechanical measurements of mechanical lap joint of middle-scaled HTS STARS conductor (~ 10 kA) using FBI test facility at KIT. This presentation introduces design, fabrication and pre-measurements of the joint at Tohoku Univ.

Outline of this presentation

1. Introduction
2. Design and method
3. Fabrication and measurement
4. Summary

1. Introduction

1-1. Joint-winding of HTS helical coils



Design of a helical coil of FFHR-d1 [1][2]
(Joint-winding [3] as challenging option)

→ solve technical issue:
difficulty of fabrication of helical coils

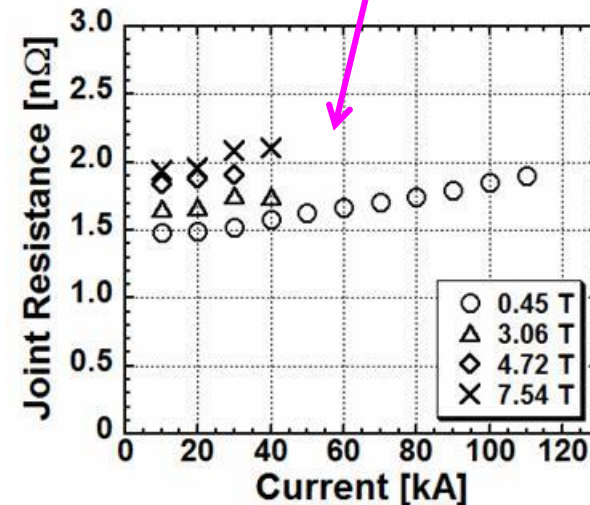
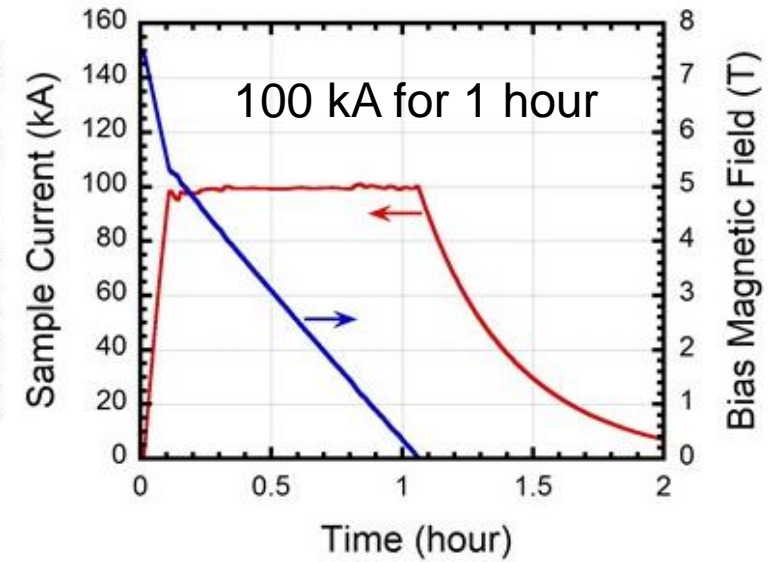
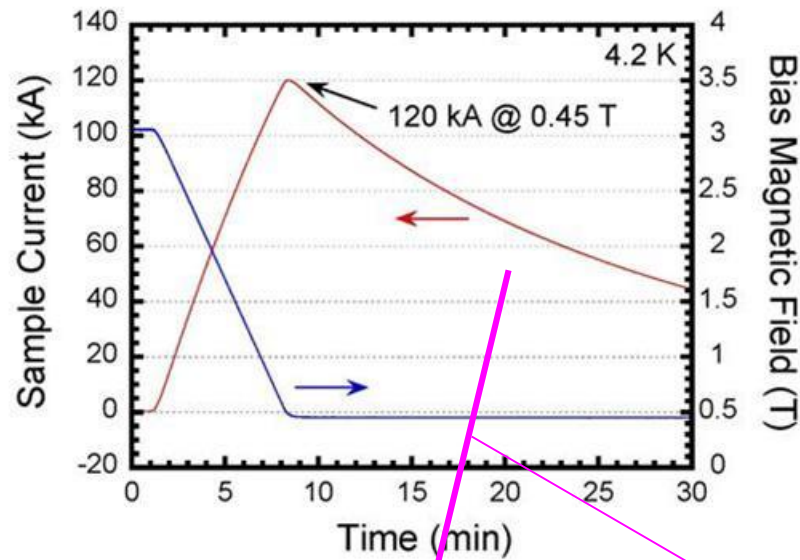
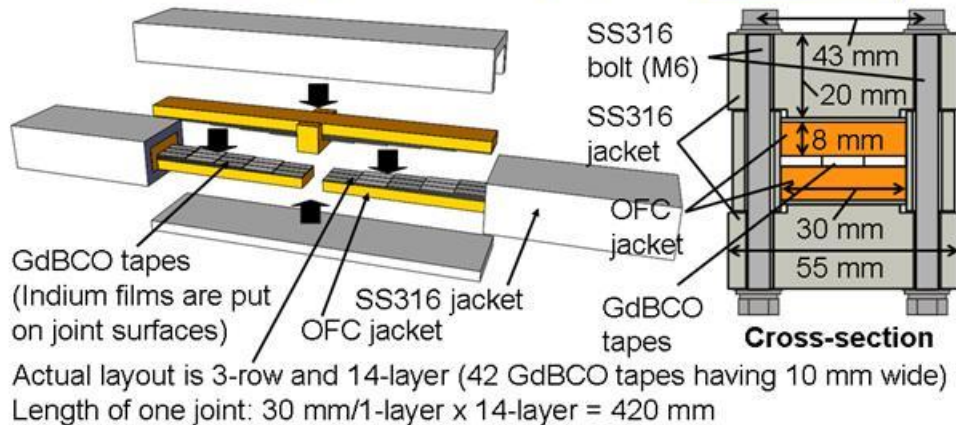
Bridge-type mechanical lap joint [5]

- The joint has a stepwise structure for face-to-face connection of REBCO surfaces
- REBCO tapes are joined by mechanical contact and just pressed together (indium foils are inserted between joint surfaces).
- Stainless steel jacket is welded to ensure tensile strength.

- [1] A. Sagara et al., Fusion Eng. Des., 89, 2014, 2114-.
- [2] A. Sagara et al., Nucl. Fusion, 57, 2017, 086046.
- [3] N. Yanagi et al., Fusion Sci. Technol., 60, 2011, 648-652.
- [4] N. Yanagi, S. Ito et al., Nucl. Fusion, 55, 2014, 053021.
- [5] S. Ito et al., Plasma Fusion Res., 9, 2014, 4602305.

1. Introduction

1-2. Test of a prototype STARS conductor joint



Joint resistance is evaluated by decay time constant

1.8 nΩ
at 100 kA

~10 pΩm²
(~100 nΩcm²)

Sufficiently small from a viewpoint of electric power to run a cryoplant

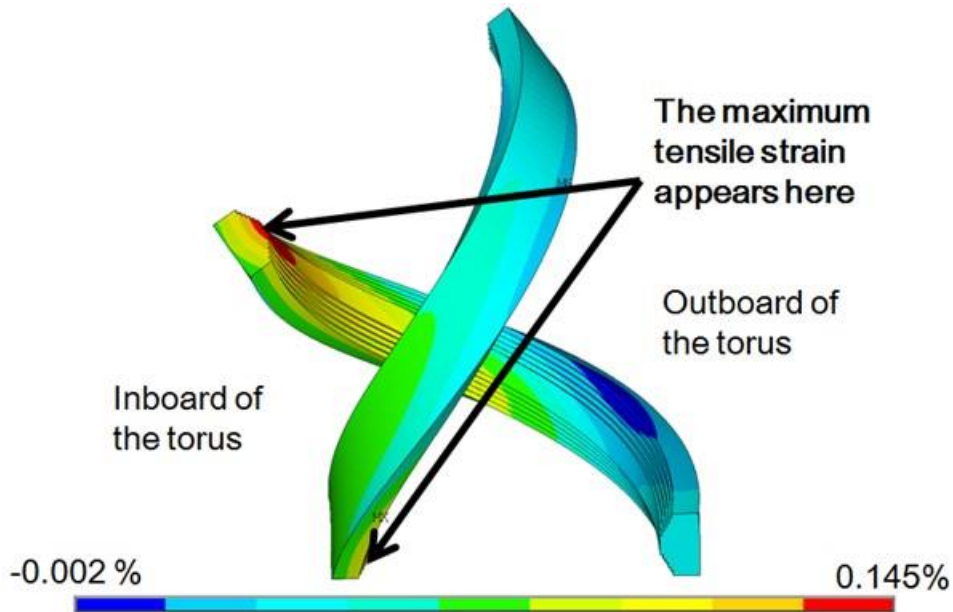
[4] N. Yanagi, S. Ito et al., Nucl. Fusion, 55, 2014, 053021.

[5] S. Ito et al., Plasma Fusion Res., 9, 2014, 4602305.

Prototype STARS conductor joint [4, 5]

1. Introduction

1-3. Electro-mechanical property of mechanical lap joint of REBCO tapes

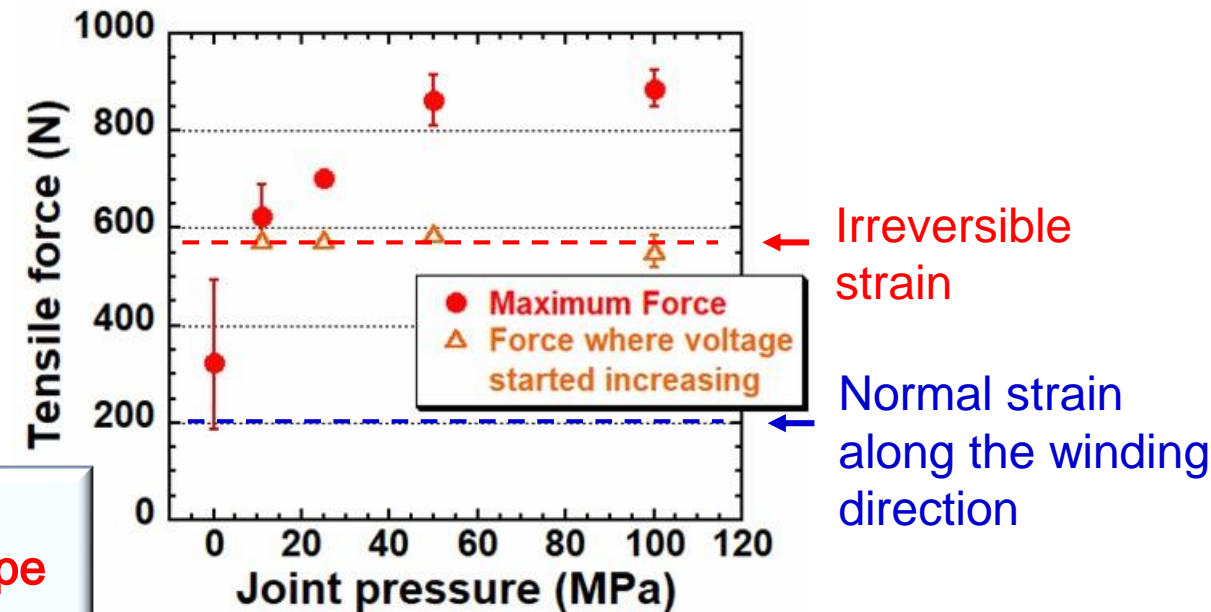
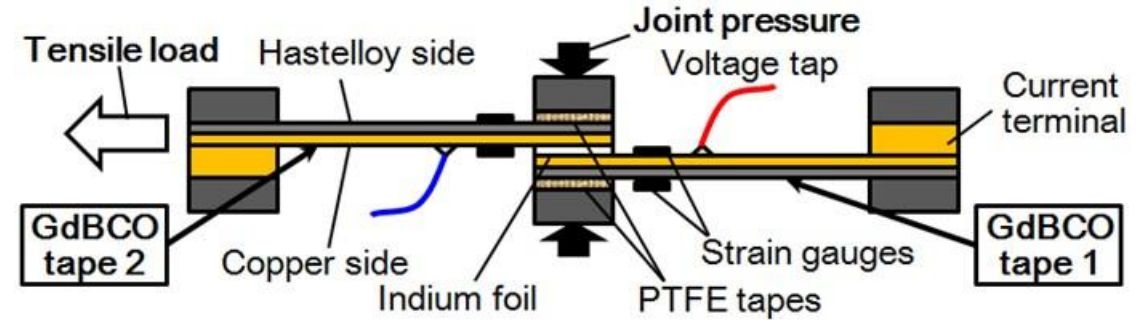


Normal strain distribution along the winding direction of the helical coils (Numerical analysis) in FFHR-d1 [6]

• Normal strain along the winding direction:

– Maximum strain: 0.145% < Irreversible strain of REBCO tape

Irreversible strain { Fujikura's REBCO tape: 0.43%-0.53% [7]
Superpower's REBCO tape: 0.6% [8]



Tensile test of mechanical lap joint of REBCO tapes at 77 K [6]

Strength of joint is sufficiently large
(From a viewpoint of normal strain along the winding direction)

[6] S. Ito et al., IEEE TAS, 25(3) (2015), 4201205.

[7] M. Sugano et. al., Supercond. Sci. Technol. 25(5), 2012, 054014.

[8] H. Song, et. al., IEEE TAS, 23(3) 2013, 4600806.

1. Introduction

1-4. Research issue and objective

We successfully achieved...

- 1.8 n Ω (~ 10 p Ω m²) at 100 kA using prototype STARS conductor joint.
- Sufficient strength at 77 K using mechanical lap joint of REBCO tapes.

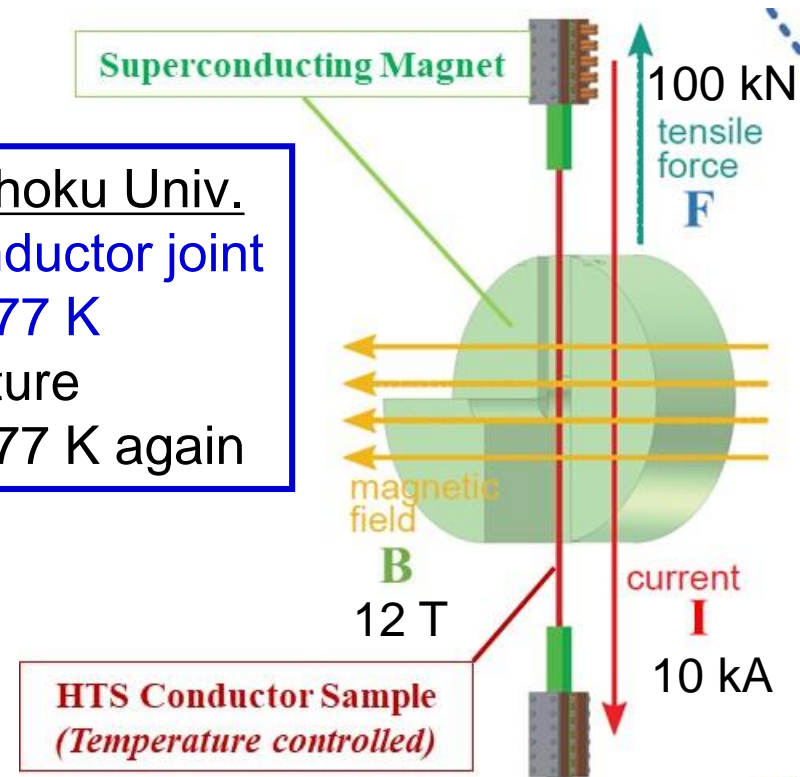
→ Can we achieve sufficient strength for STARS conductor joint at lower temperature?

Sample preparation and pre-measurement at Tohoku Univ.

- Design and fabricate a 10 kA class STARS conductor joint
- Measure critical current and joint resistance at 77 K
- Apply a tensile force of 10 kN at room temperature
- Measure critical current and joint resistance at 77 K again

Measurement at KIT

- Critical current and joint resistance at 4.2 K and different fields
- Joint resistance at 4.2 K and 12 T for various sample elongations



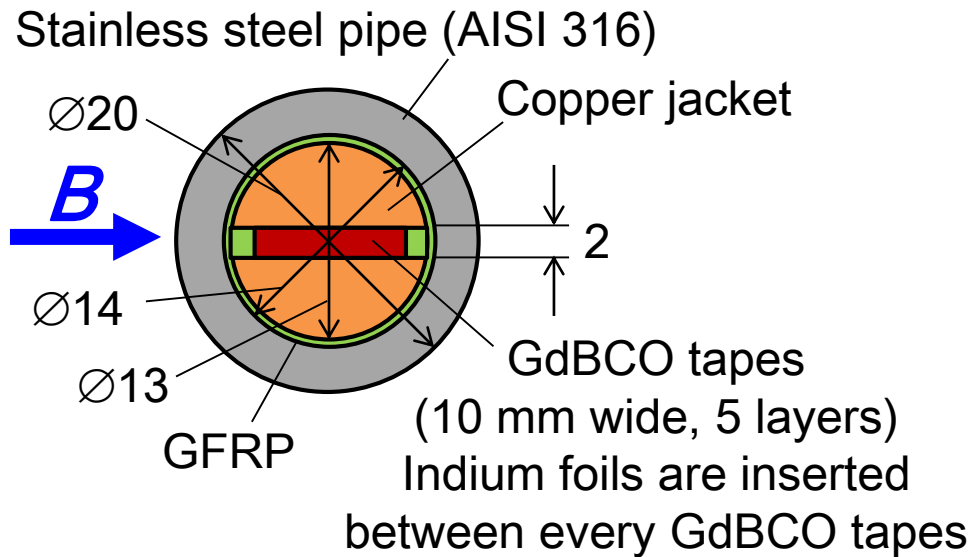
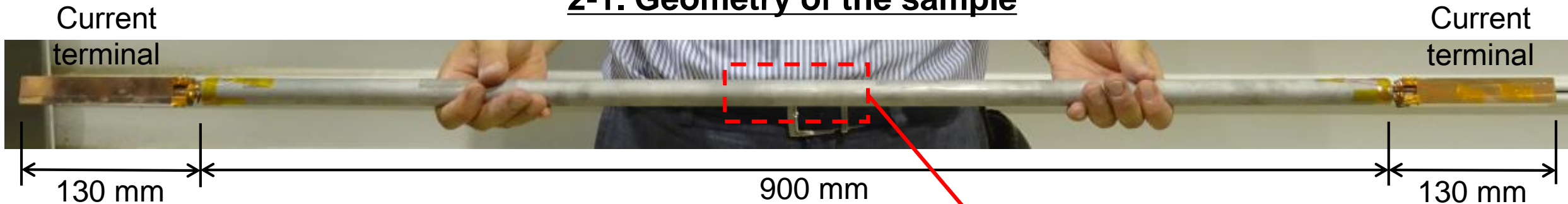
FBI test facility at KIT

Courtesy of C. Barth, Ph.D. Thesis 2013

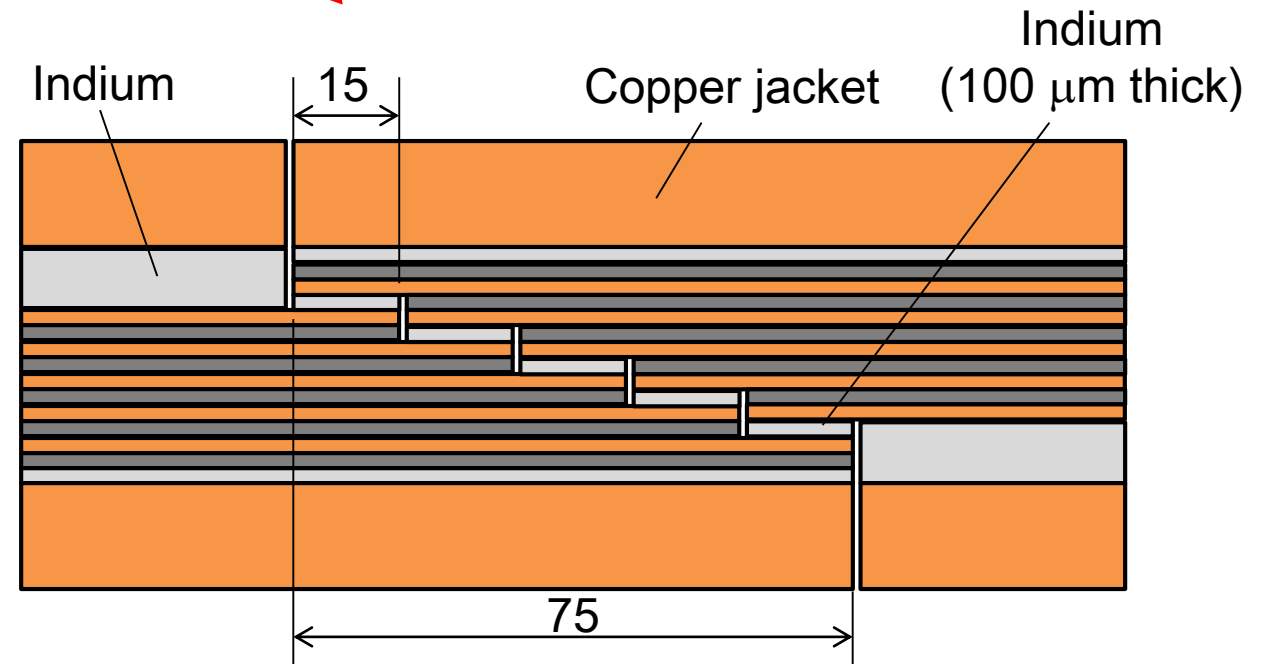
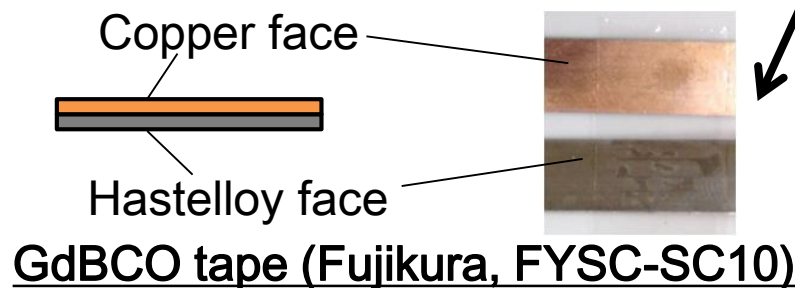
(<http://digbib.ubka.uni-karlsruhe.de/volltexte/1000035747>)

2. Design and method

2-1. Geometry of the sample



Cross section of the conductor



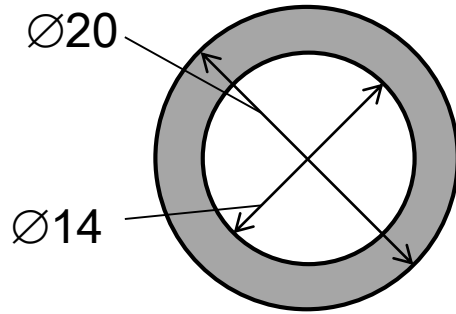
Schematic illustration of the joint section
(mechanical lap joints with indium foils inserted
between joint surfaces)

2. Design and method

2-2. Mechanical properties

Applied tensile force

- 10 kN at room temperature (Tohoku Univ.)
- 100 kN at 4.2 K (KIT)



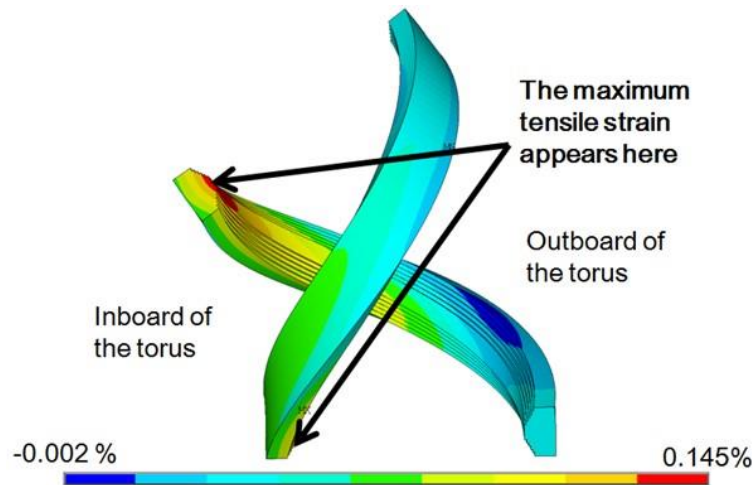
- Rough estimation of strain considering only the stainless steel jacket
- Cross sectional area: 160 mm²
- Young's modulus: 195 GPa (293 K), 208 GPa (4.2 K)
- Yield stress: 240 MPa (293 K), 550 MPa (4.2 K)

10 kN at room temp. (Tohoku Univ.)

- Tensile stress = $(10 \times 10^3) / (160 \times 10^{-6}) = 6.24 \times 10^7 = 62.4 \text{ MPa}$
- Tensile strain = $(6.24 \times 10^7) / (195 \times 10^9) = 3.20 \times 10^{-4} = 0.032\%$
< Normal strain along the winding direction
< Irreversible strain of REBCO tape

100 kN at 4.2 K (KIT)

- Tensile stress = $(100 \times 10^3) / (160 \times 10^{-6}) = 6.24 \times 10^8 = 624 \text{ MPa}$
- Tensile strain = $(6.24 \times 10^7) / (208 \times 10^9) = 3.00 \times 10^{-3} = 0.3\%$
> Normal strain along the winding direction
< Irreversible strain of REBCO tape

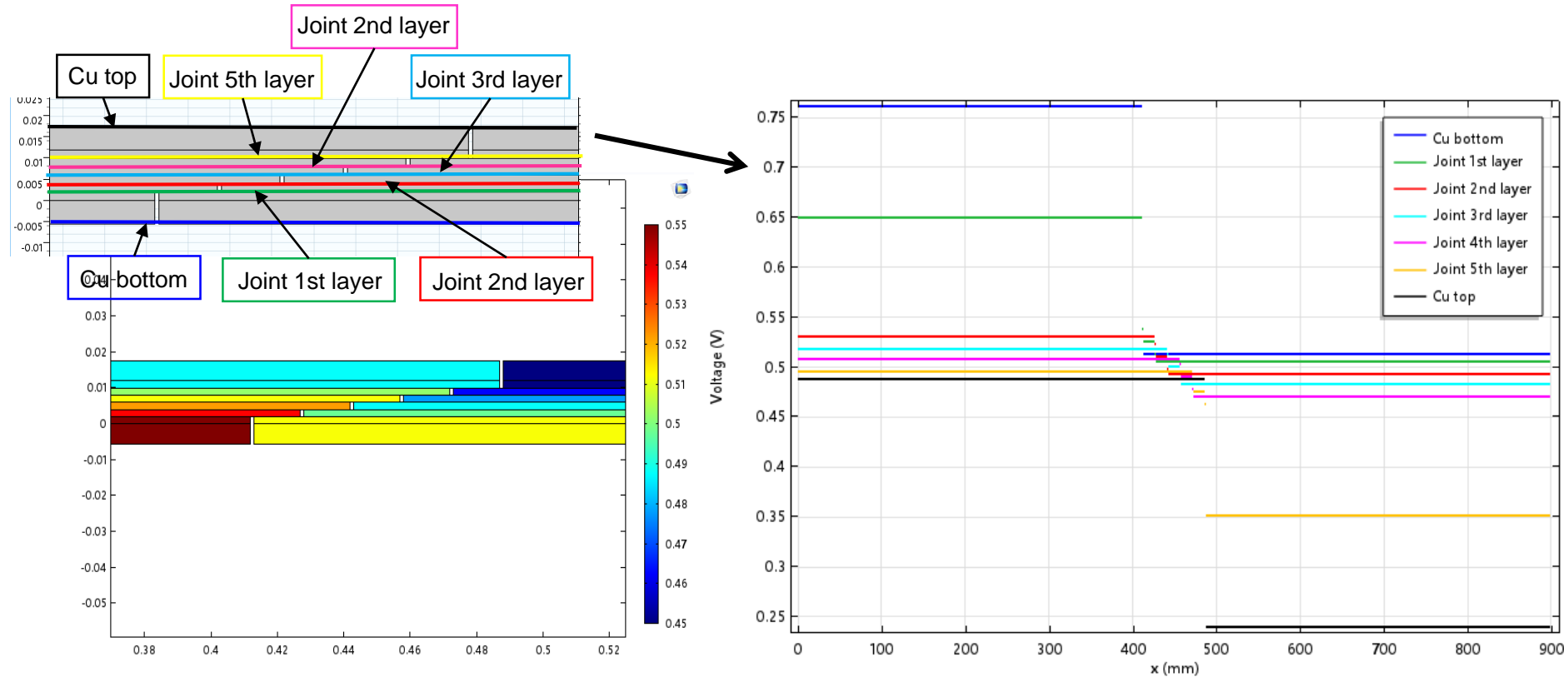


Irreversible strain of Fujikura's REBCO tape: 0.43%-0.53%

2. Design and method

2-3. Problem of voltage measurement

- If there is no interface resistance, potential distribution of every GdBCO tape layers and copper jackets are the same, but with interface resistance, they are different.
- Voltage drop of each joint section (each layer) can not be evaluated by taps attached on copper jacket according to numerical analysis taking inter-layer resistance.



Potential distribution in the joint section

Joint resistivity for mechanical lap joint with indium: $10 \text{ p}\Omega\text{m}^2$ for every layers

Interface resistivity between GdBCO layers: $1 \text{ }\mu\Omega\text{m}^2$ for every layers

2. Design and method

2-4. Experimental procedure

1) Joint resistance and I_c measurements for each GdBCO tape.

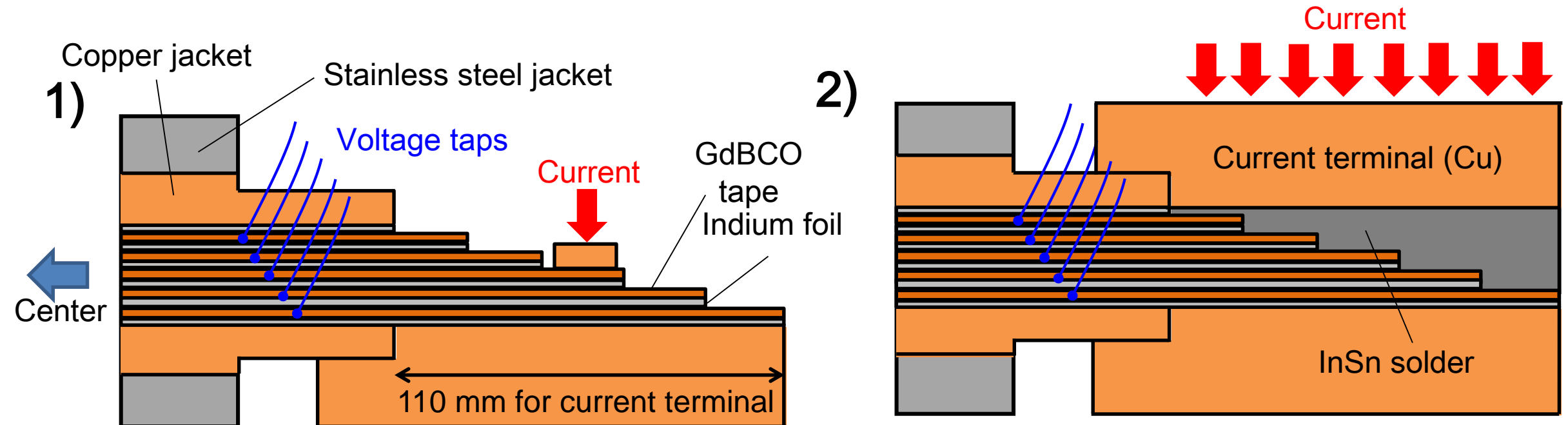
Current is applied to each GdBCO tape one by one before fixing current terminal (copper block).
The data is used as joint resistance and I_c at 77 K, self field.

2) Evaluation of current distribution

After fixing the current terminal, current is applied from the current terminal. We've already known each joint resistance by 1), so we can evaluate current flowing each GdBCO tape by voltage measurement.

3) Pre-tensile test at room temp.

Applying tensile force upto 10 kN at room temp. Then repeat 2).



3. Fabrication and measurement

3-1. Preparation of mechanical lap joint of each layer

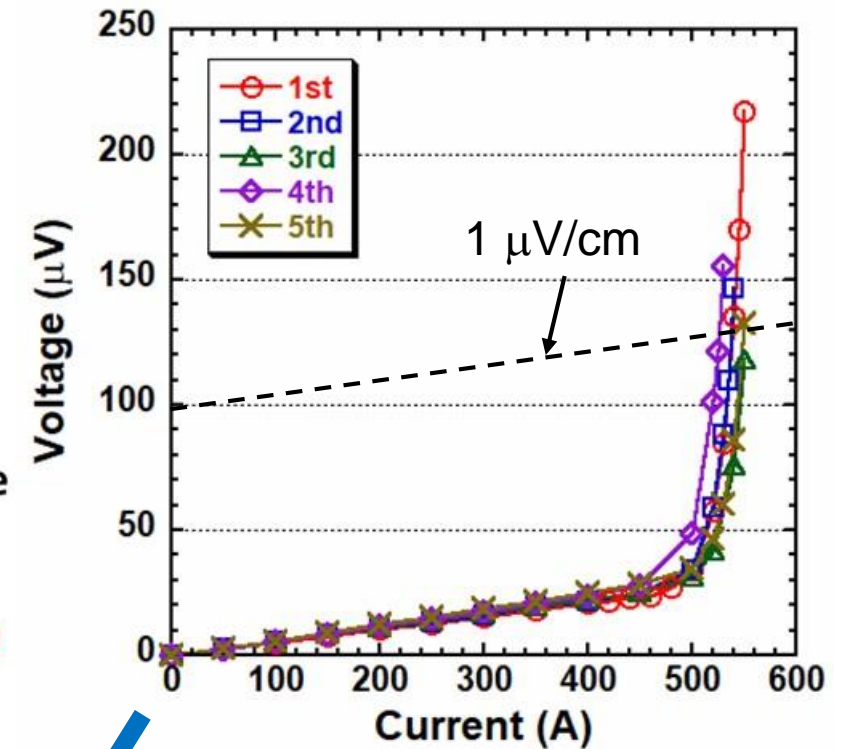
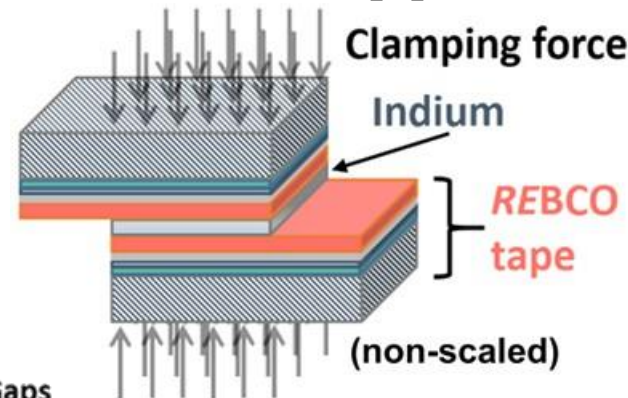
• REBCO tape

Copper stabilized GdBCO tape (Fujikura, FYSC-SC10)

- Thickness: $\sim 190\text{ }\mu\text{m}$
Cu ($100\text{ }\mu\text{m}$) / Sn ($2\text{--}4\text{ }\mu\text{m}$) / Ag ($8.2\text{ }\mu\text{m}$) / GdBCO ($1.8\text{ }\mu\text{m}$) / Buffer ($\sim 0.5\text{ }\mu\text{m}$) / Hastelloy ($75\text{ }\mu\text{m}$)
- Width: 10 mm

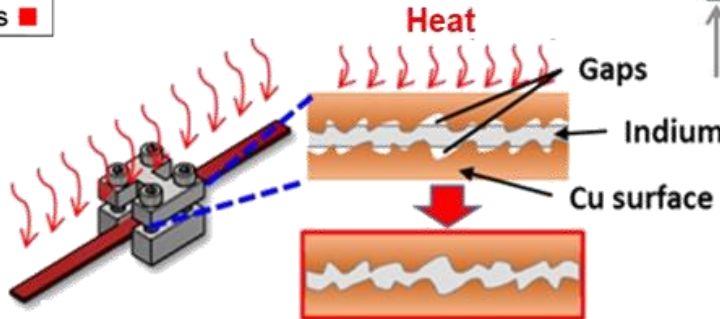
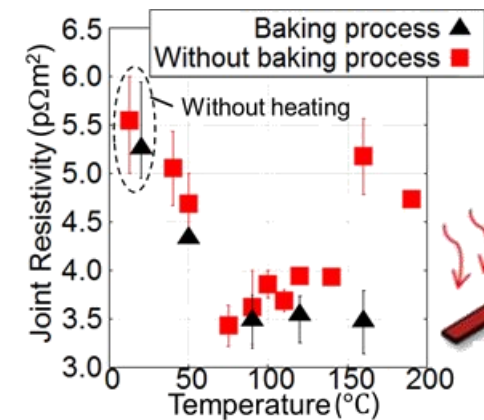
• Mechanical lap joint with low-temperature heat treatment [1]

- Joint area: 10 mm (width) \times 15 mm (length)
- Inserted indium foil: $100\text{ }\mu\text{m}$ thick
- Joint pressure: 100 MPa
- Heating treatment: $90\text{ }^{\circ}\text{C}$ for 30 min



***I-V* curve for each layer**

1st layer: $I_C = 540\text{ A}$, $R = 52\text{ n}\Omega$, $RS = 7.8\text{ p}\Omega\text{m}^2$ ($78\text{ n}\Omega\text{cm}^2$)
 2nd layer: $I_C = 535\text{ A}$, $R = 54\text{ n}\Omega$, $RS = 8.1\text{ p}\Omega\text{m}^2$ ($81\text{ n}\Omega\text{cm}^2$)
 3rd layer: $I_C = 550\text{ A}$, $R = 56\text{ n}\Omega$, $RS = 8.4\text{ p}\Omega\text{m}^2$ ($84\text{ n}\Omega\text{cm}^2$)
 4th layer: $I_C = 525\text{ A}$, $R = 58\text{ n}\Omega$, $RS = 8.7\text{ p}\Omega\text{m}^2$ ($87\text{ n}\Omega\text{cm}^2$)
 5th layer: $I_C = 550\text{ A}$, $R = 62\text{ n}\Omega$, $RS = 9.3\text{ p}\Omega\text{m}^2$ ($93\text{ n}\Omega\text{cm}^2$)



3. Fabrication and measurement

3-2. Assembling the joint sample

Joint



Putting GdBCO tapes jointed by mechanical lap joint with indium foils on the copper jacket.
100- μm -thick Indium foils are inserted between GdBCO tapes.
Voltage taps made of 50- μm -thick copper foil are set between GdBCO tapes.



Fixing the GdBCO tapes, the indium foils and the copper jacket by pressing them.

➔ Failed: Difficult to press them accurately...

The sample was rotated and can not be fixed by the pressing...

Terminal copper block was not soldered at this time
(Boundary region between the jacket and the terminal connected by bolts to protect GdBCO tapes for the current terminal)

3. Fabrication and measurement

3-2. Assembling the joint sample



Wrapping the copper jacket with prepreg sheets of GFRP.
Inserting the sample into the stainless steel jacket.

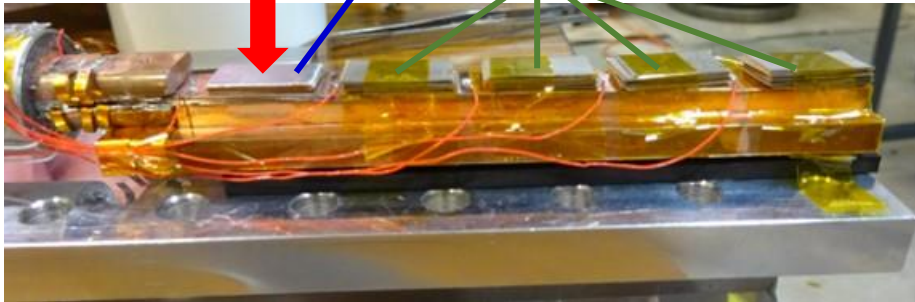


Curing GFRP at 100 °C for 5 hours

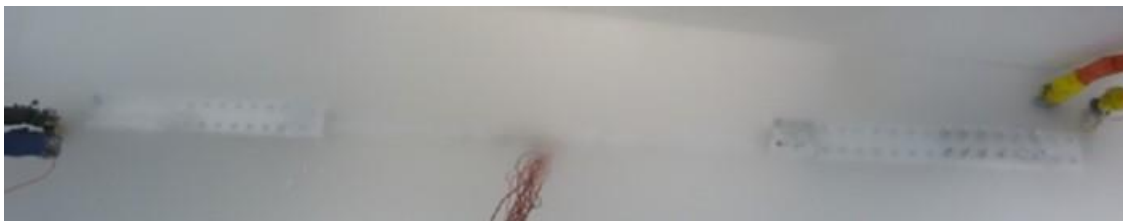
Applying current
only to this layer

Copper plate

Spacers (insulated)



Setting the terminal to apply current to only one layer

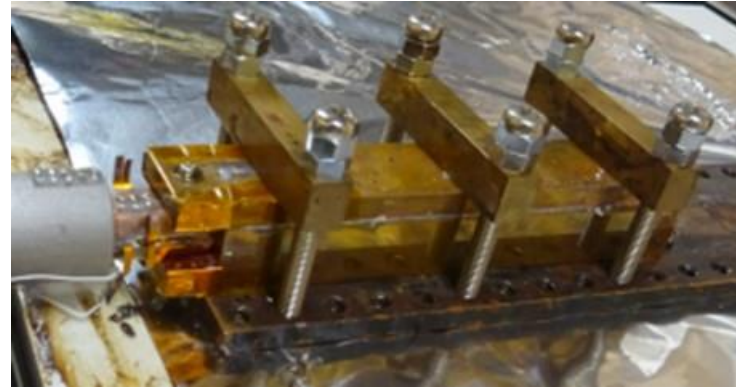


Connector to DC
current supply

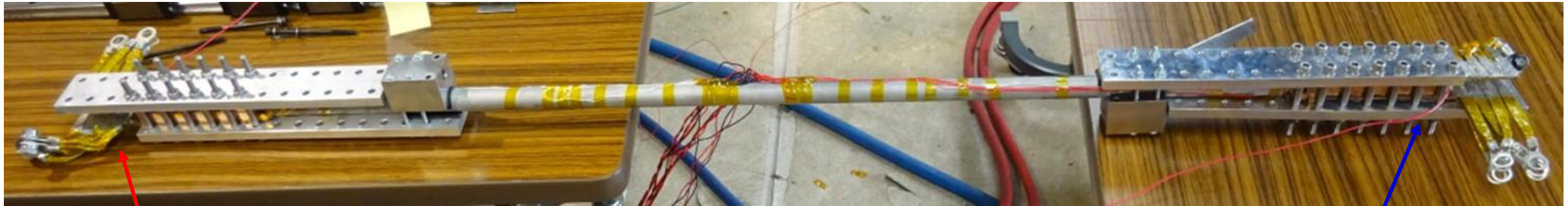
Measuring the voltage signals in liquid nitrogen.
Repeat the measurement changing layers where
current is applied.
(5th → 4th → 3rd → 2nd → 1st layers)

3. Fabrication and measurement

3-2. Assembling the joint sample



Soldering (InSn solder) the GdBCO tapes with the copper block at the terminal



Fixing the connectors to DC current supply to the current terminal.
Measuring the voltage signals in liquid nitrogen.

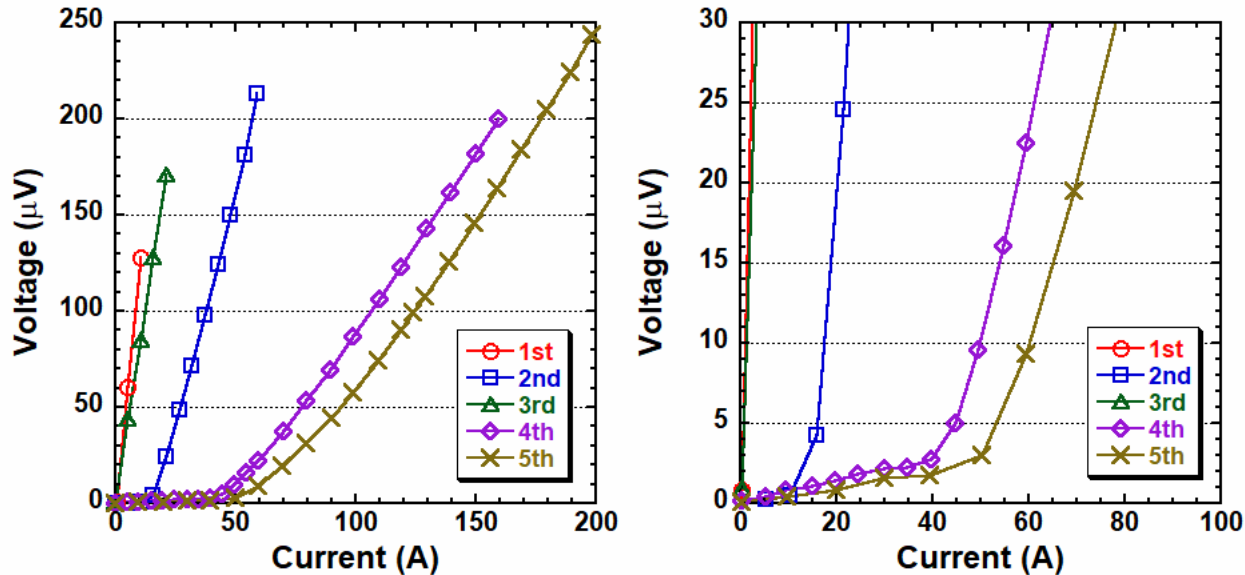


Connector to DC
current supply

Voltage tap to measure voltage whole region of the sample
including terminal resistance

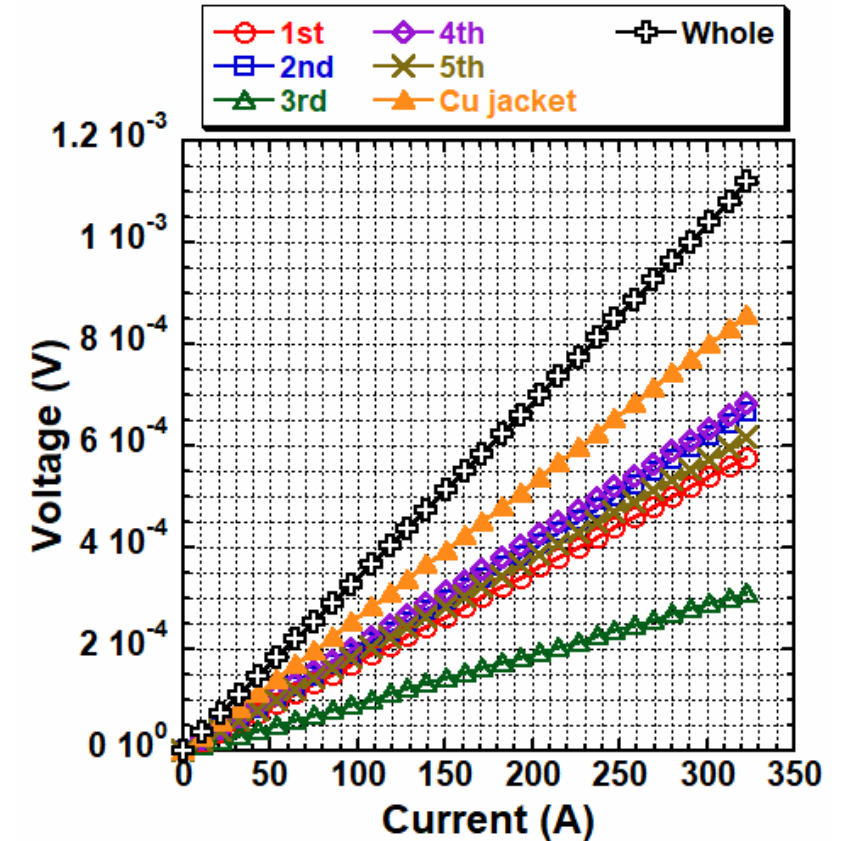
3. Fabrication and measurement

3-3. Voltage measurement



I-V curve for each layer before fixing the current terminal

Critical current for every layers were degraded.
Joint resistance was kept to be its original value for
2nd, 4th and 5th layers.



I-V curve after fixing the current terminal

Voltage drop measured by taps attached on the copper jacket showed meaningless data
I-V curve shows further degradation of critical current (= 0 A for all layers)

The GdBCO tapes were not fixed to the copper jacket. Pressing process was failed.

➔ The GdBCO tapes could be bent locally during both the pressing process and the setting for measurement.

4. Summary

Background of this study

- Joint-winding of HTS coils is the challenging option for design of FFHR-d1.
- Prototype STARS Conductor joint achieved 120 kA and 1.8 nΩ at 4.2 K
- The joint of REBCO tapes had sufficient strength at 77 K.



Objective of this study

- To show sufficient strength for STARS conductor joint at lower temperature, we plan to do electro-mechanical measurement of 10-kA-class STARS conductor joint at FBI test facility.
- For the measurement, the joint sample was tried to be prepared at Tohoku Univ.

Present situation

- A method to measure voltage of the joint sample was proposed.
- The joint sample was fabricated and tested at 77 K, but failed at fabrication process.
 - ➔ Try to fix problems of the fabrication process and continue to advance the project.