

# Real-time functional diagnostics of superconducting magnets using acoustic techniques

M. Marchevsky

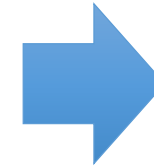
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## ■ Operational

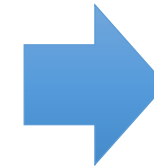
- Quench detection and localization
- Conductor instabilities
- Thermal monitoring
- Mechanical integrity monitoring



- Safety
- Cost reduction

## ■ General and predictive

- Understanding training and memory effects
- Finding design limitations
- Benchmarking of electro-mechanical models



- Improving magnet performance

## Acoustic diagnostics



- ✓ Fast: sound propagation velocity is several km/s
- ✓ Not intrusive: sensors are at the outer surfaces
- ✓ Immunity to magnetic fields
- ✓ inexpensive, portable and adaptable to various magnet configurations

## Singular events

### Mechanical

- Cracking / fracture of epoxy, de-laminations
- Sudden mechanical motion of conductor or structural part

### Electromagnetic -> Mechanical

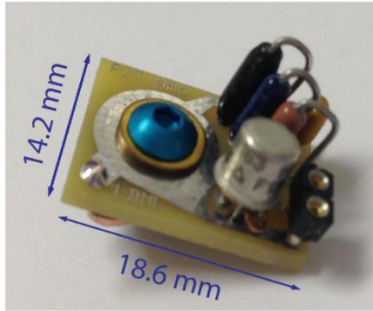
- Flux jump, as current re-distribution in the cable leads to the local variation of the electromagnetic force

## Continuous perturbations

- Vibrations of coils, shell and support structures)
- Background noise (helium boiling, pumps, etc.)

- **Quench development** leads to a local thermal expansion and change in the local stress at sub-millisecond time scale, which *may* lead to acoustic emission. However, magnets that are conductor-limited are near-quiet acoustically at quench.

- “Acoustic emission from NbTi superconductors during flux jump”, G. Pasztor and C. Schmidt, Cryogenics 19, 608 (1979).
- “Sources of acoustic emission in superconducting magnets”, O. Tsukamoto and Y. Iwasa, J. Appl. Phys. 54, 997 (1983).



- In-house developed amplified cryogenic sensors
- Built-in GaAs MOSFET amplifiers have 300-1.9 K operational range
- Bandwidth up to ~300 kHz



**Continuous streaming  
at 1 MHz, 4 ch**  
Precise axial  
localization and time-  
frequency analysis



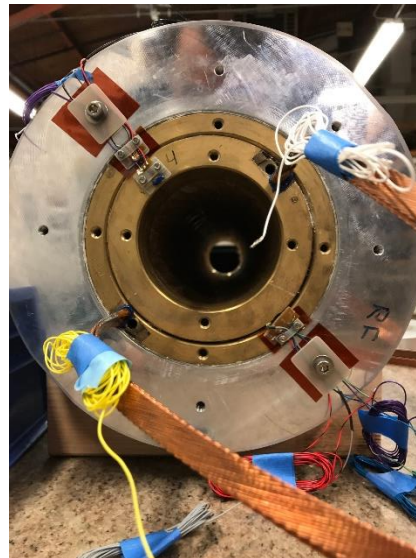
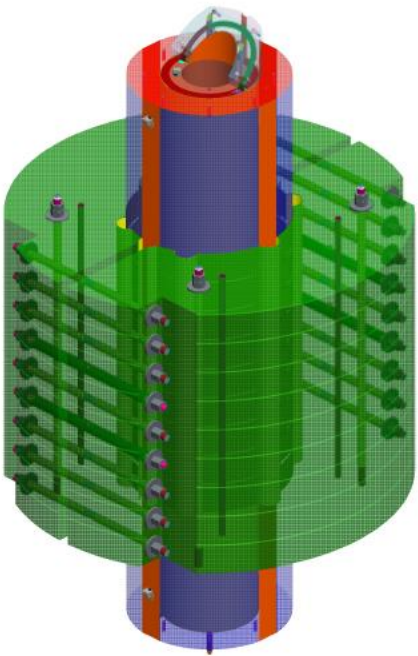
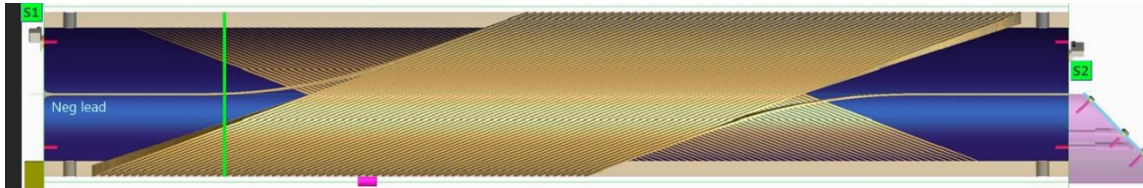
**Continuous streaming at  
40 kHz, 32 ch**



**Triggered  
acquisition at 1 MHz,  
16 ch**  
Axial / angular quench  
localization

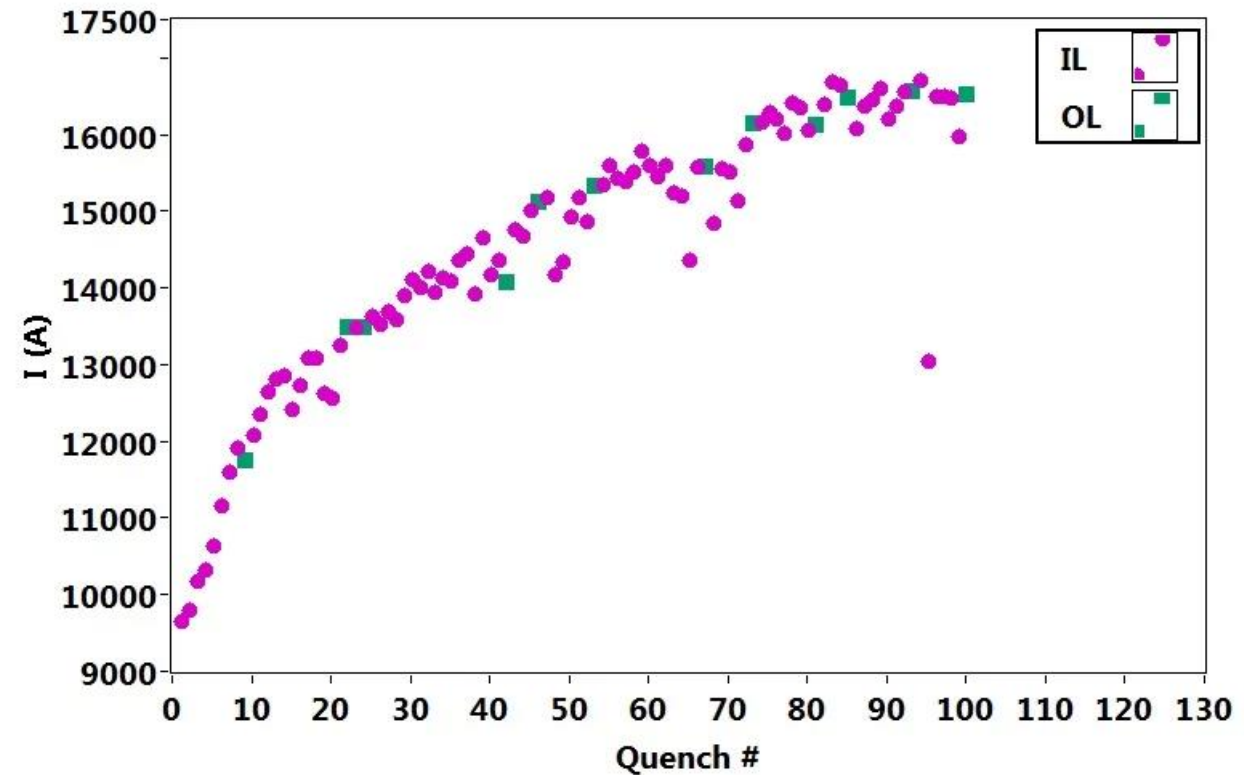


**Continuous or  
triggered acquisition  
0.5 – 10 MHz, 8 ch.**  
“Active” mechanical  
integrity monitoring



- Highest quench current: 16731 A
- Bore dipole field: 9.14 T
- Field at the conductor: 10.32 T
- “Short sample” limit: 19.3 kA (4.5 K)

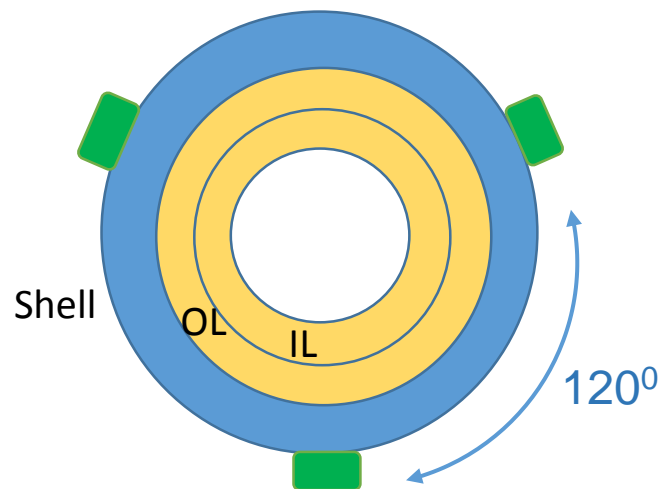
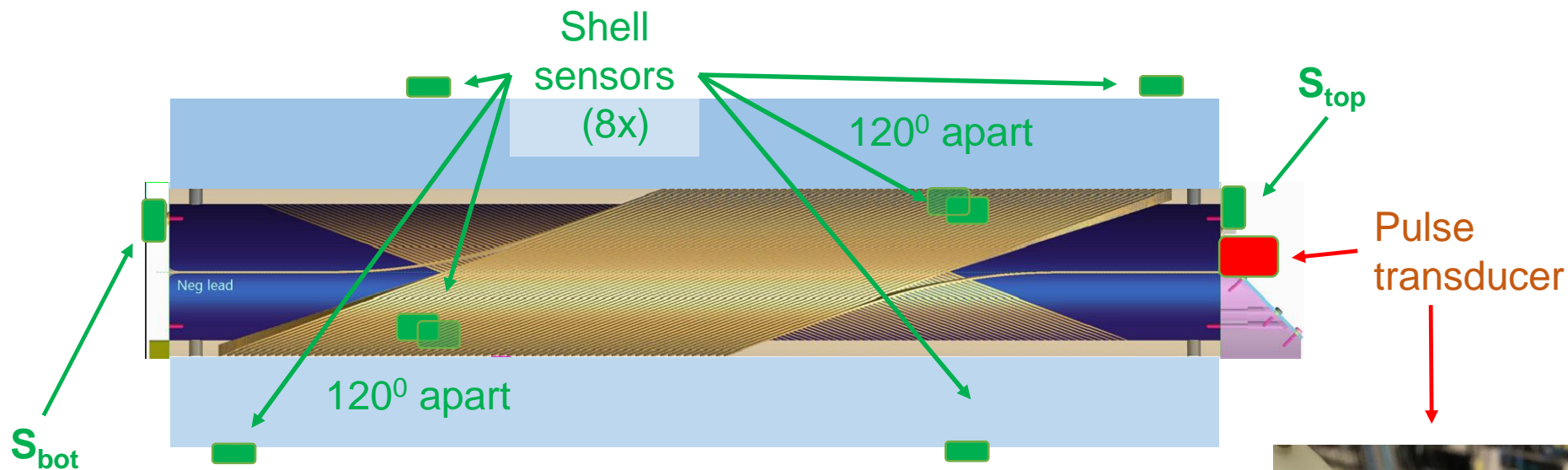
Training plot



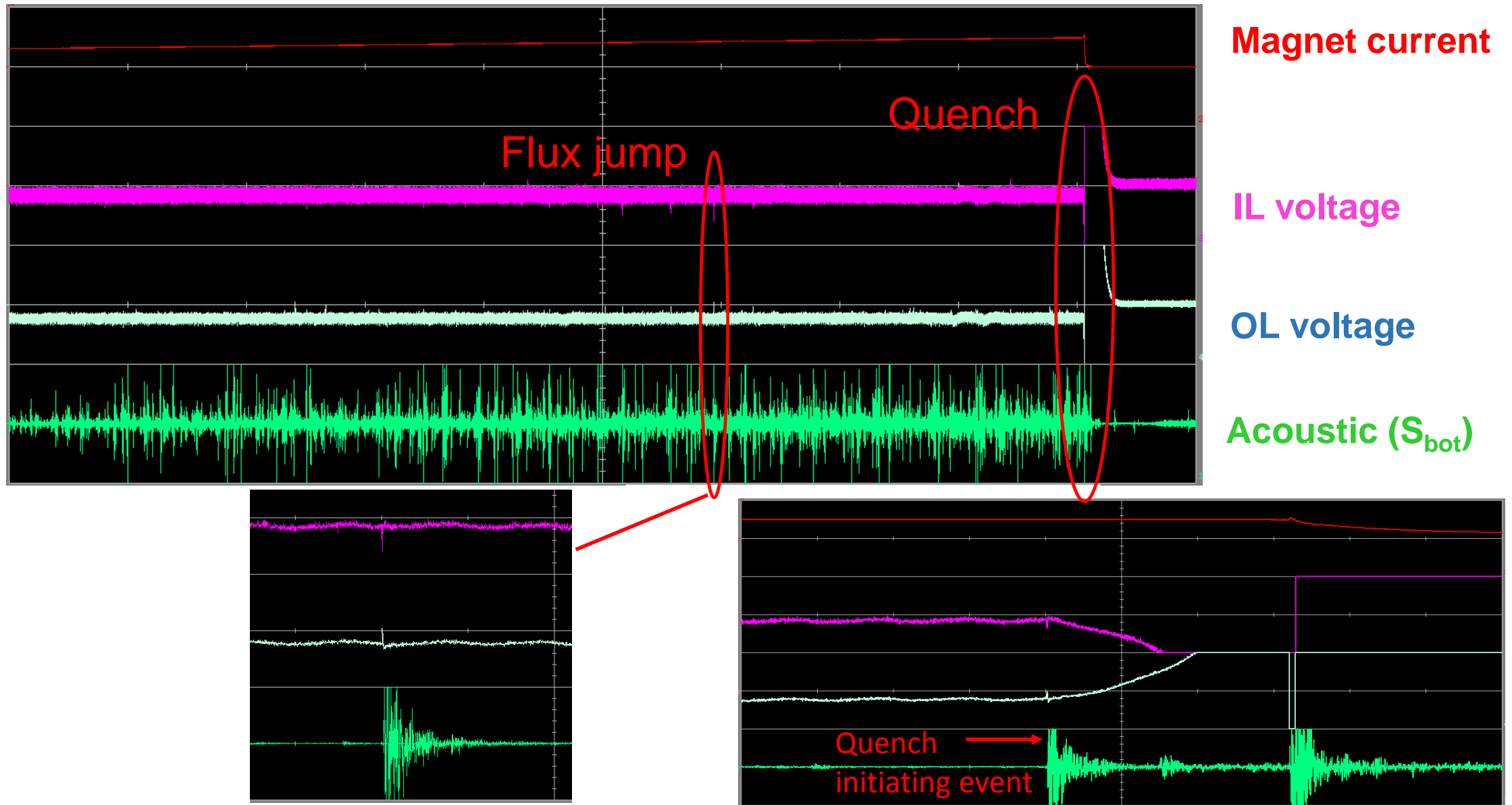
**D. Arbelaez : Mon-Af-Or7, CCT4 design and test results**

**L. Brower : Tue-Af-Po2.10, CCT magnet modeling**

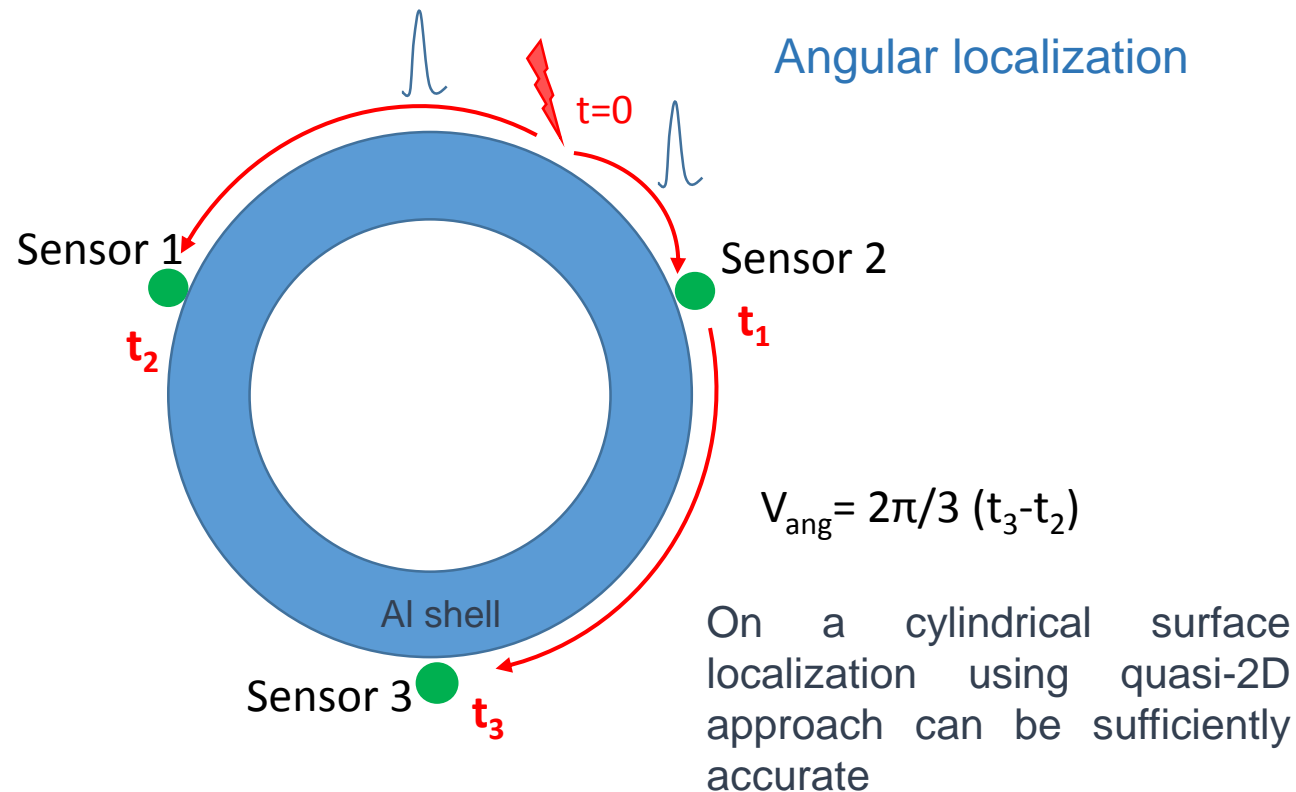
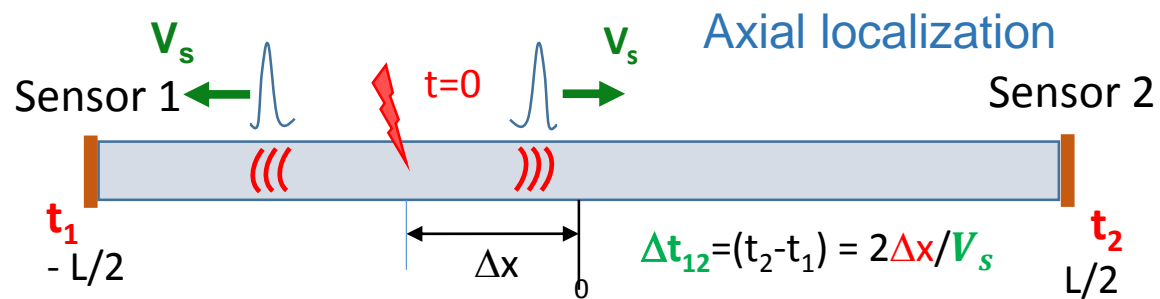




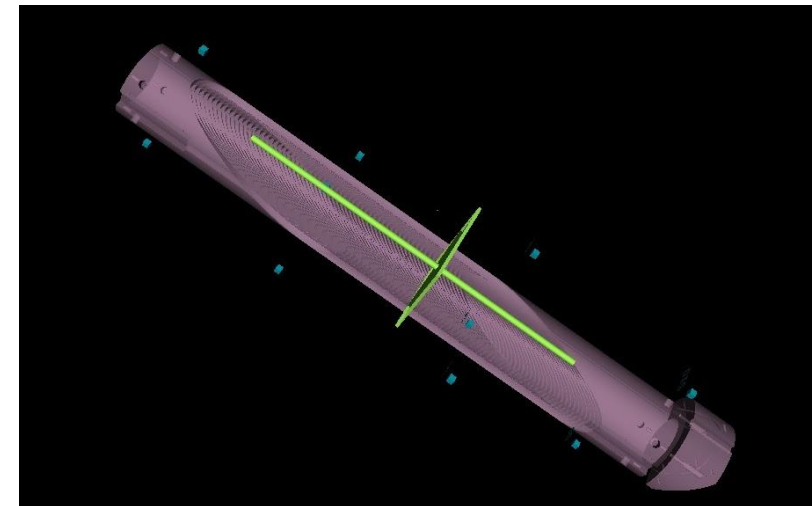
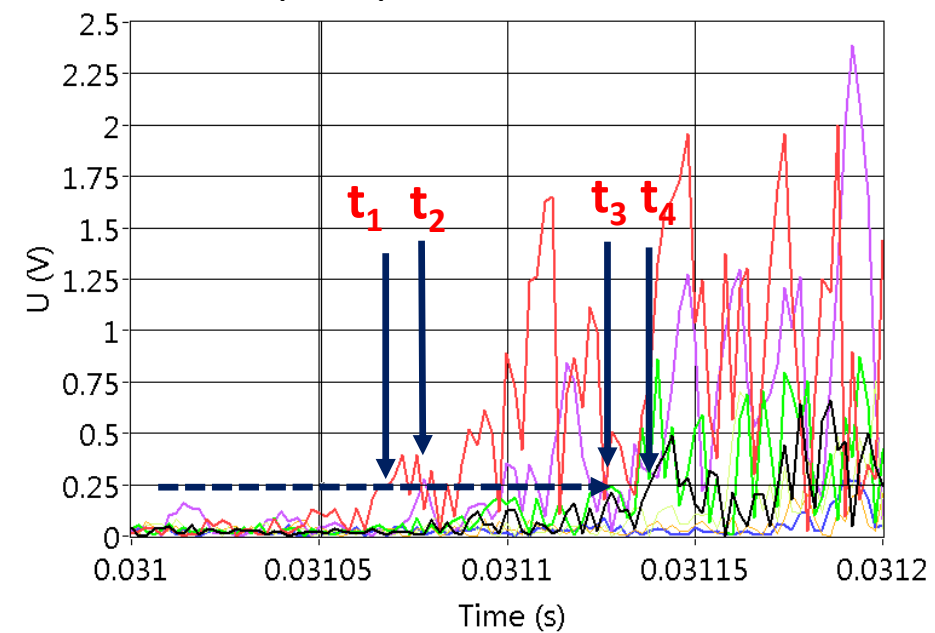
# First quench in the CCT4



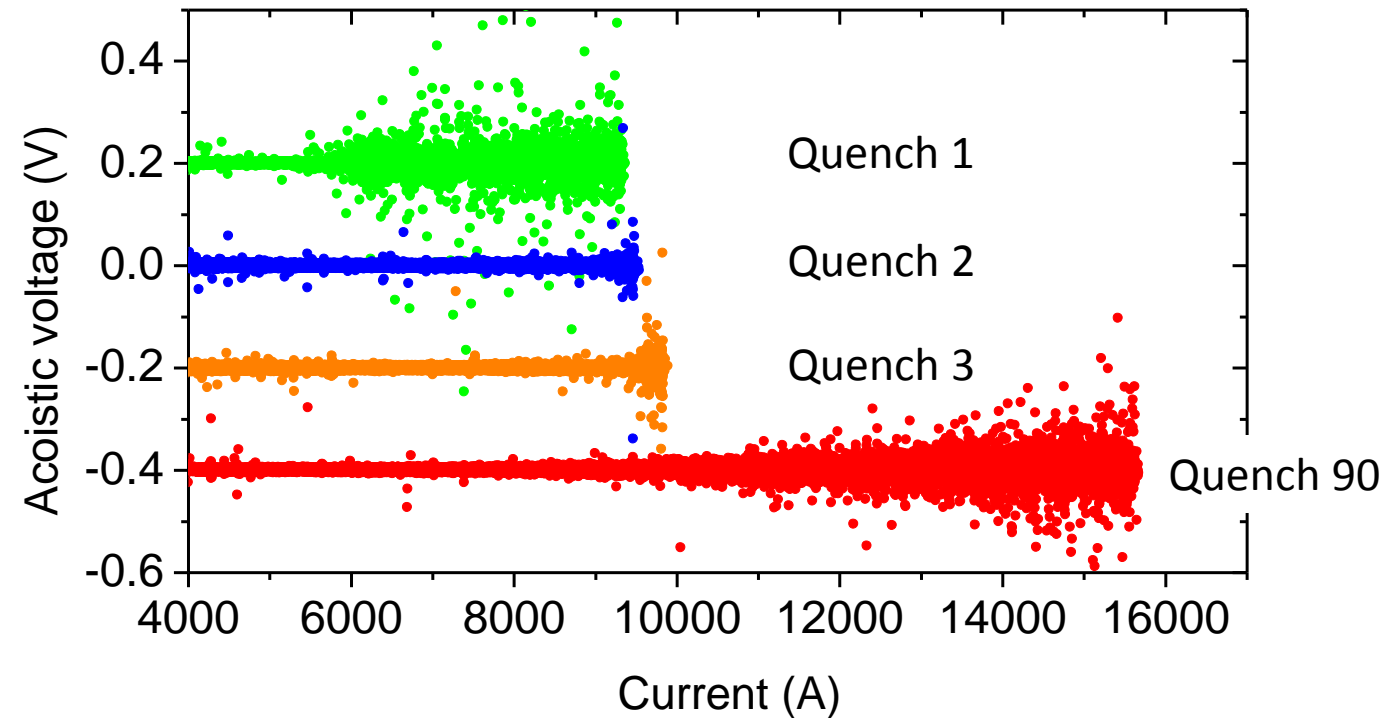
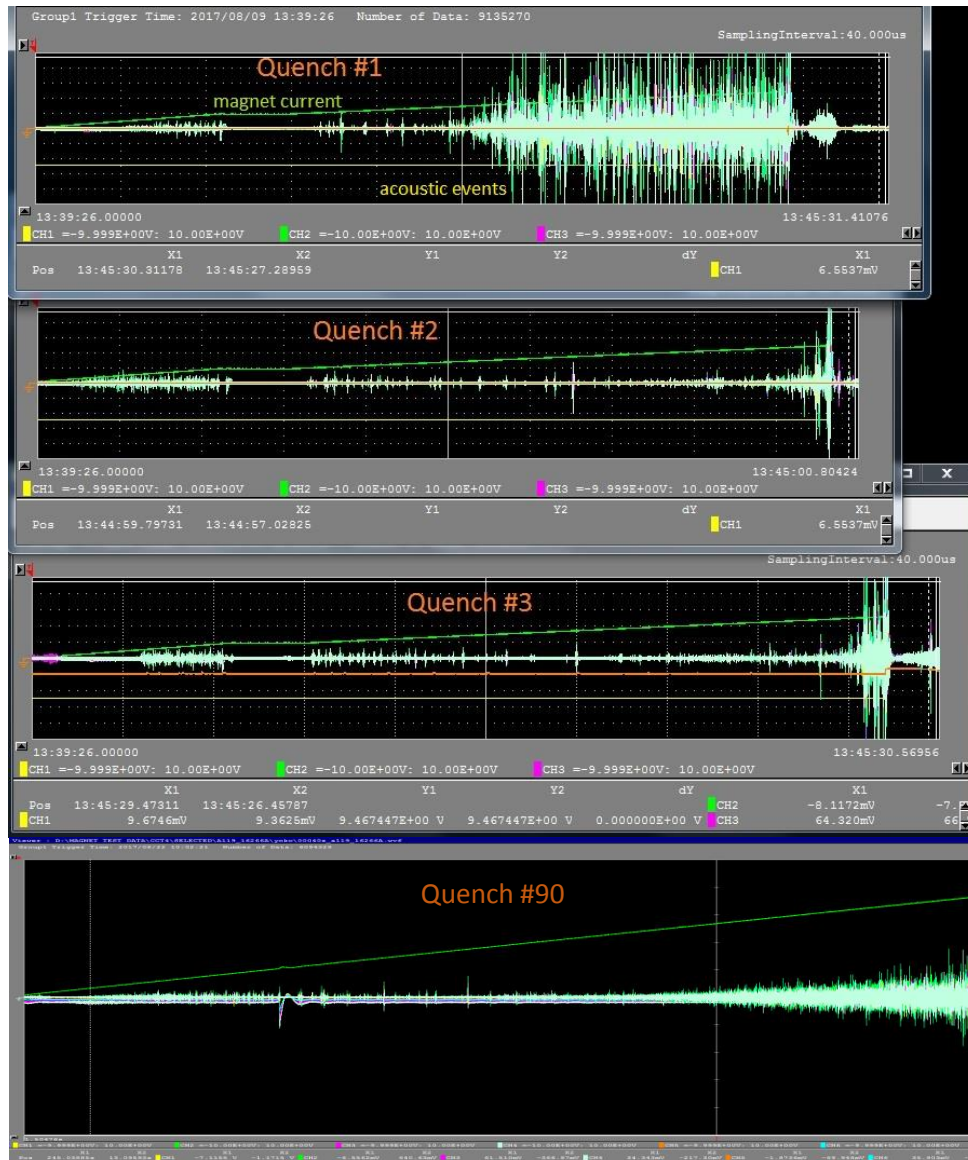
# Axial and azimuthal quench localization



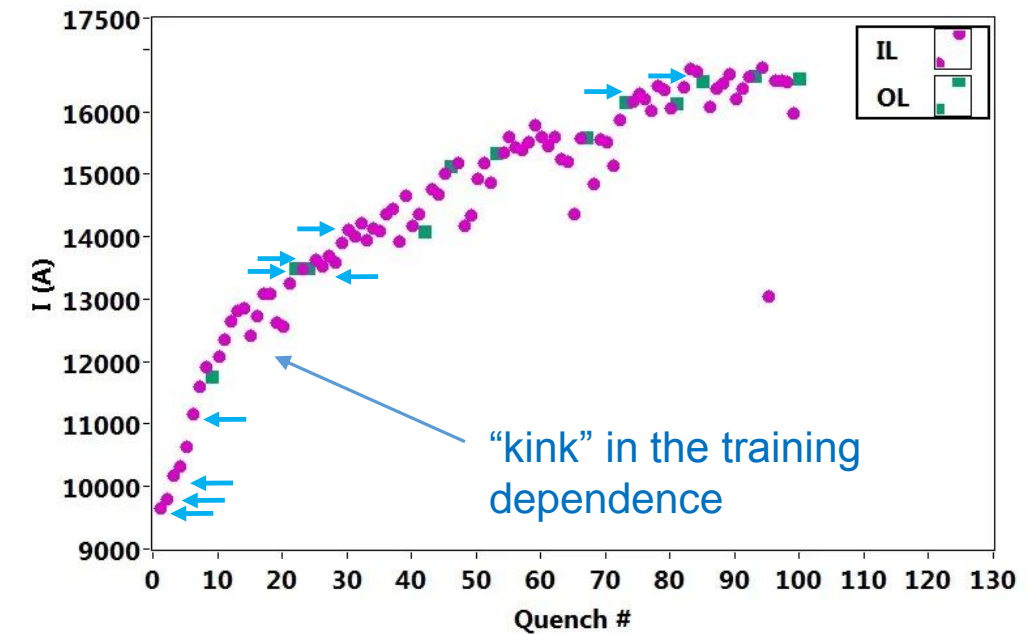
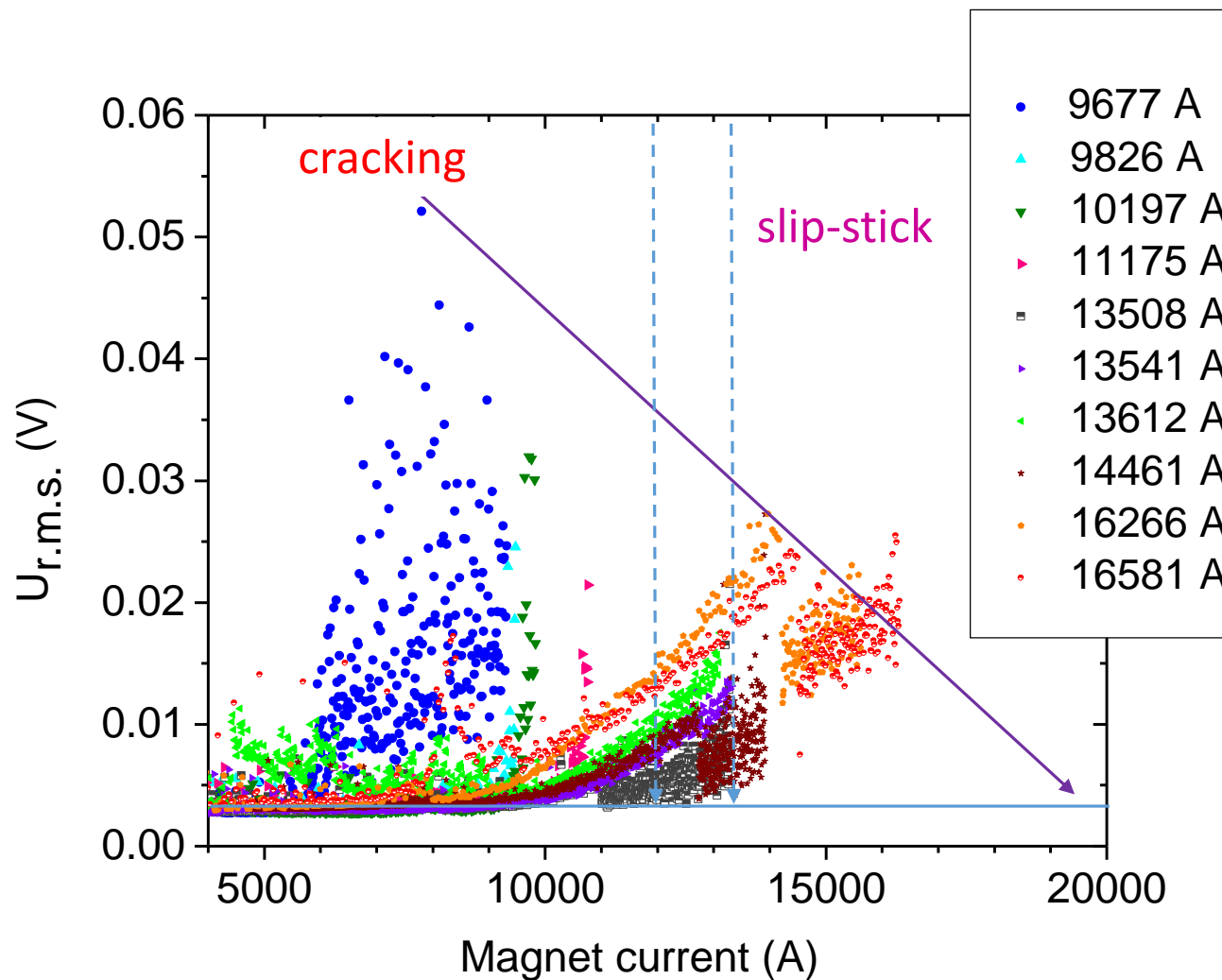
Example: quench #4 at 10350 A



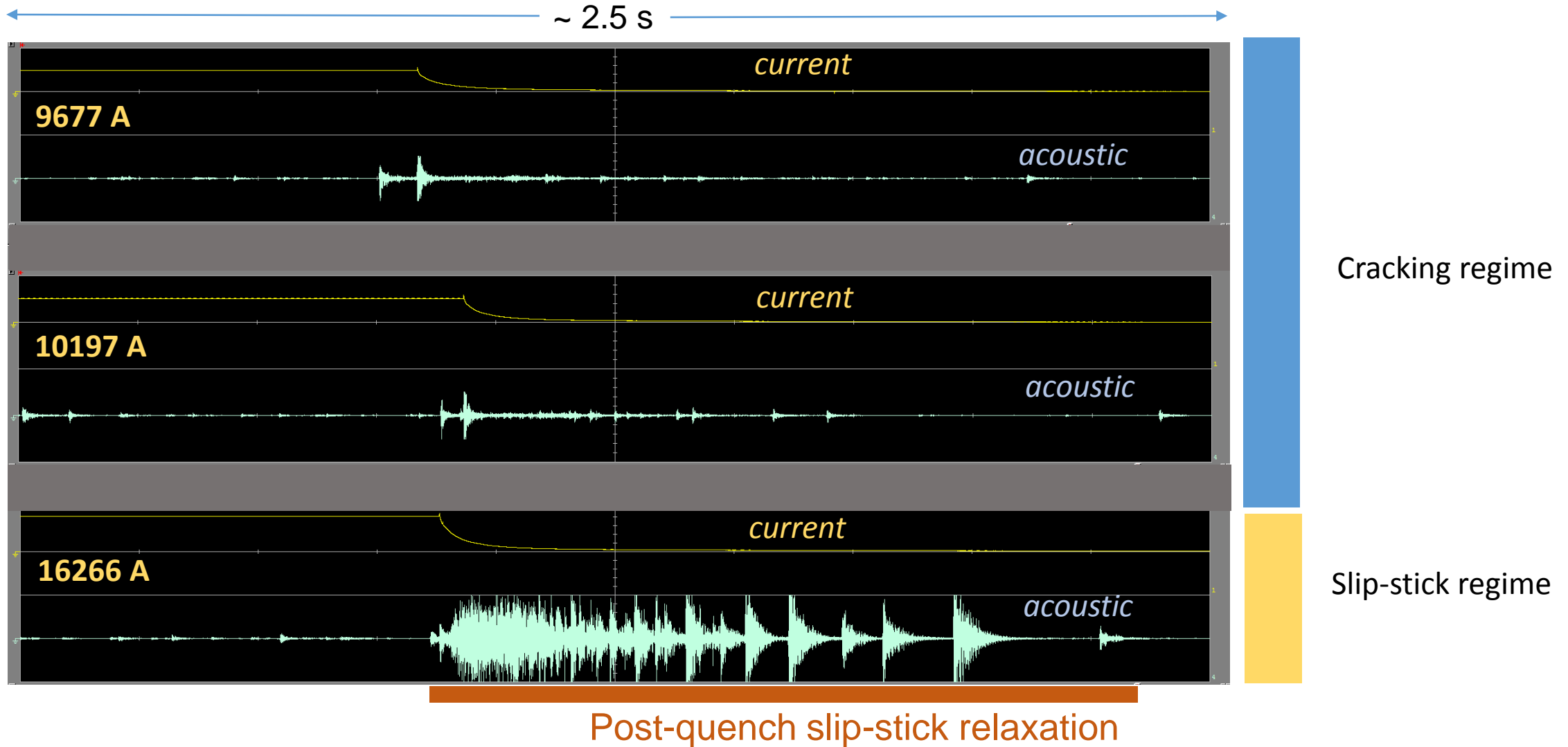




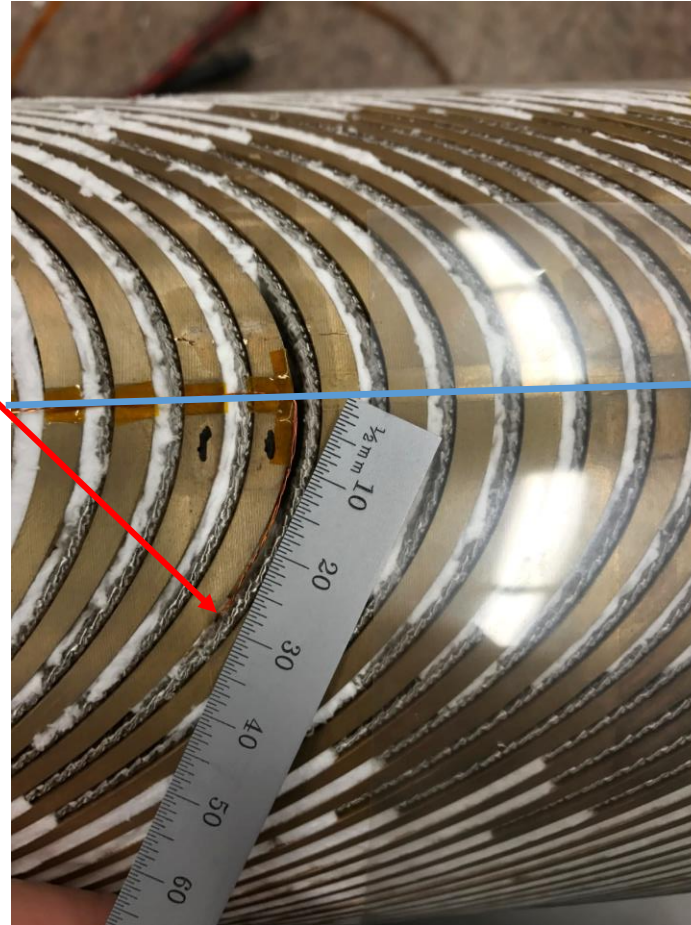
- CCT4 magnet shows mechanical memory in the initial quenches (Kaiser effect)
- However, as training progressed, noise grows in amplitude towards the quench, erasing the memory effect.



Similar behavior was earlier seen in a different kind of high-field  $Nb_3Sn$  dipole; see [M. Marchevsky, et al., Cryogenics 69, 50 \(2015\), DOI: 10.1016/j.cryogenics.2015.03.005](#)



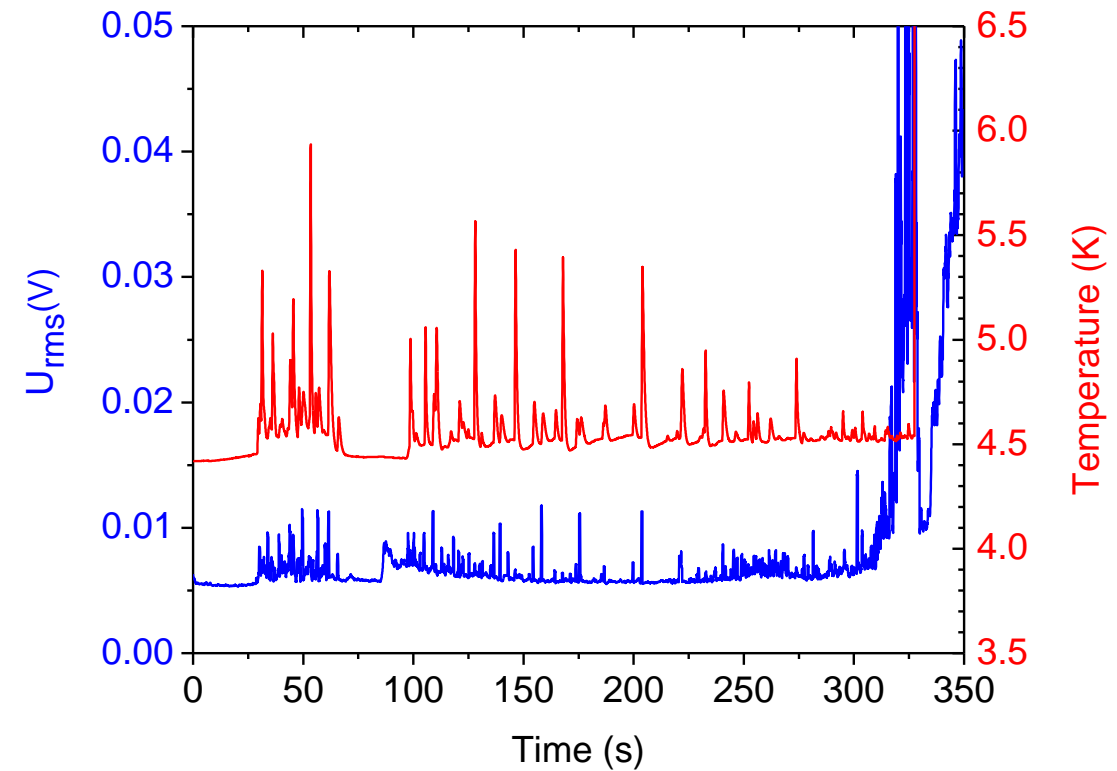
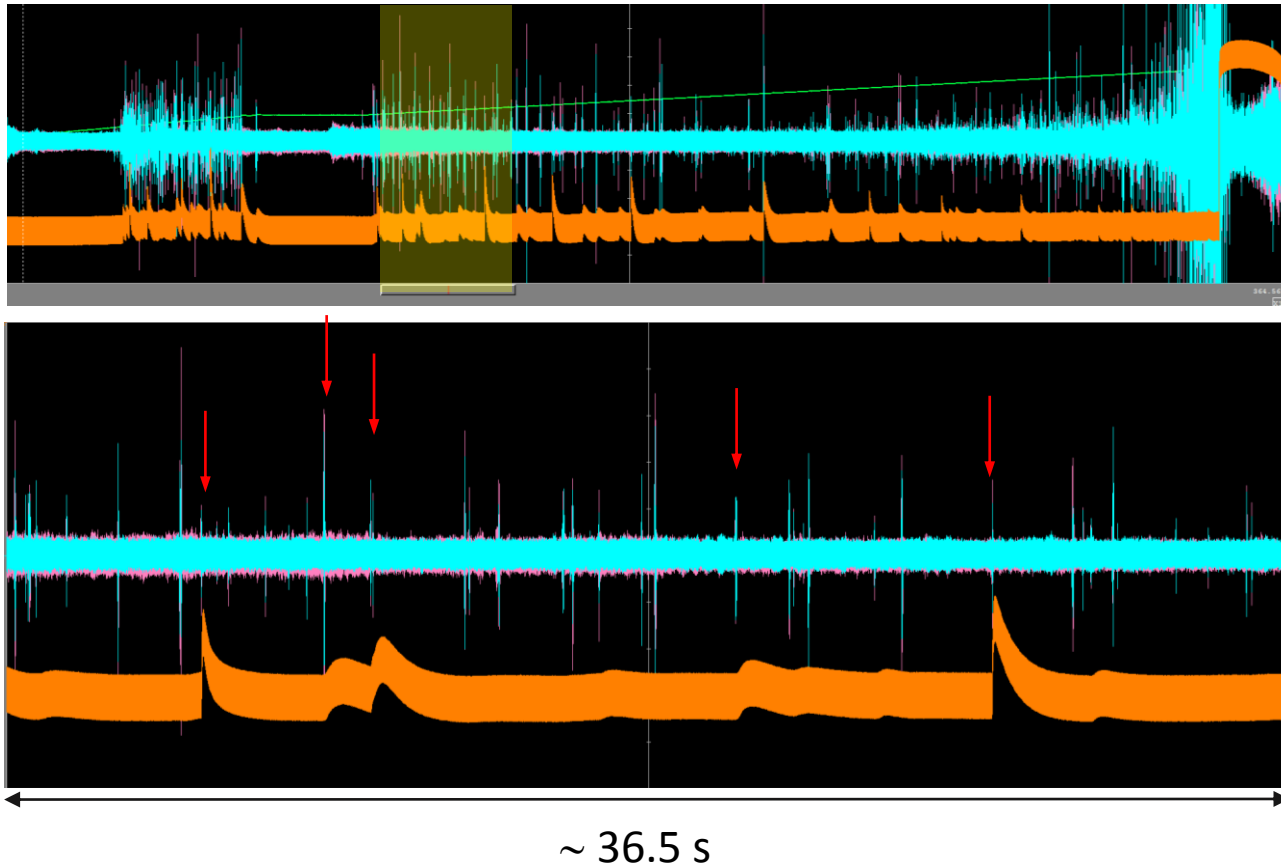
A thermometer of  $\sim 1 \text{ mm}^2$  size was installed directly in the cable groove, in the magnet outer layer, prior to impregnation



Pole location

Thermometer was powered by  $10 \mu\text{A}$  bias current and monitored simultaneously with acoustic signal and coil voltages during ramps.

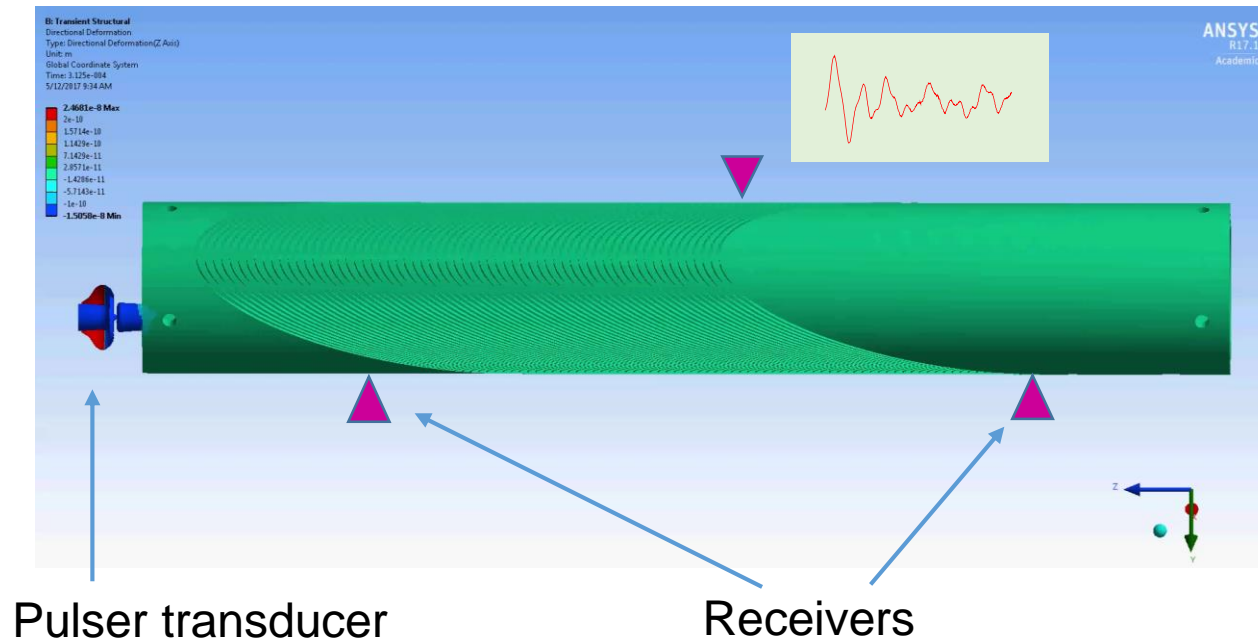




- Temperature spikes as high as 1 K are observed in the “cracking” regime. All of them are time-correlated with the acoustic events, and few also correlate with voltage spikes on the coils
- A minor ( $< 20$  mK) gradual temperature rise, or none at all is seen in the “slip-stick” regime prior to quenching

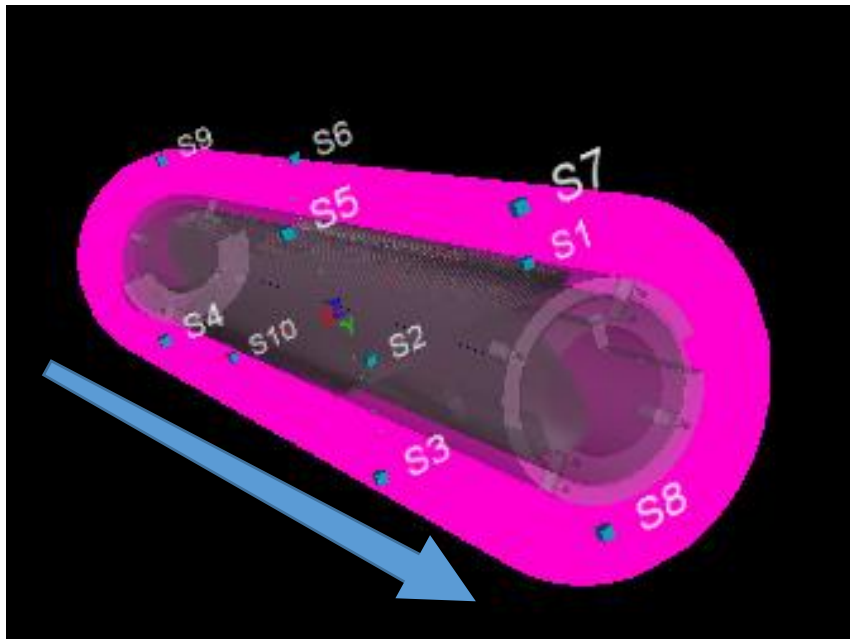


ANSYS simulation of transient deformation in the CCT mandrel upon pulsing a piezo-transducer

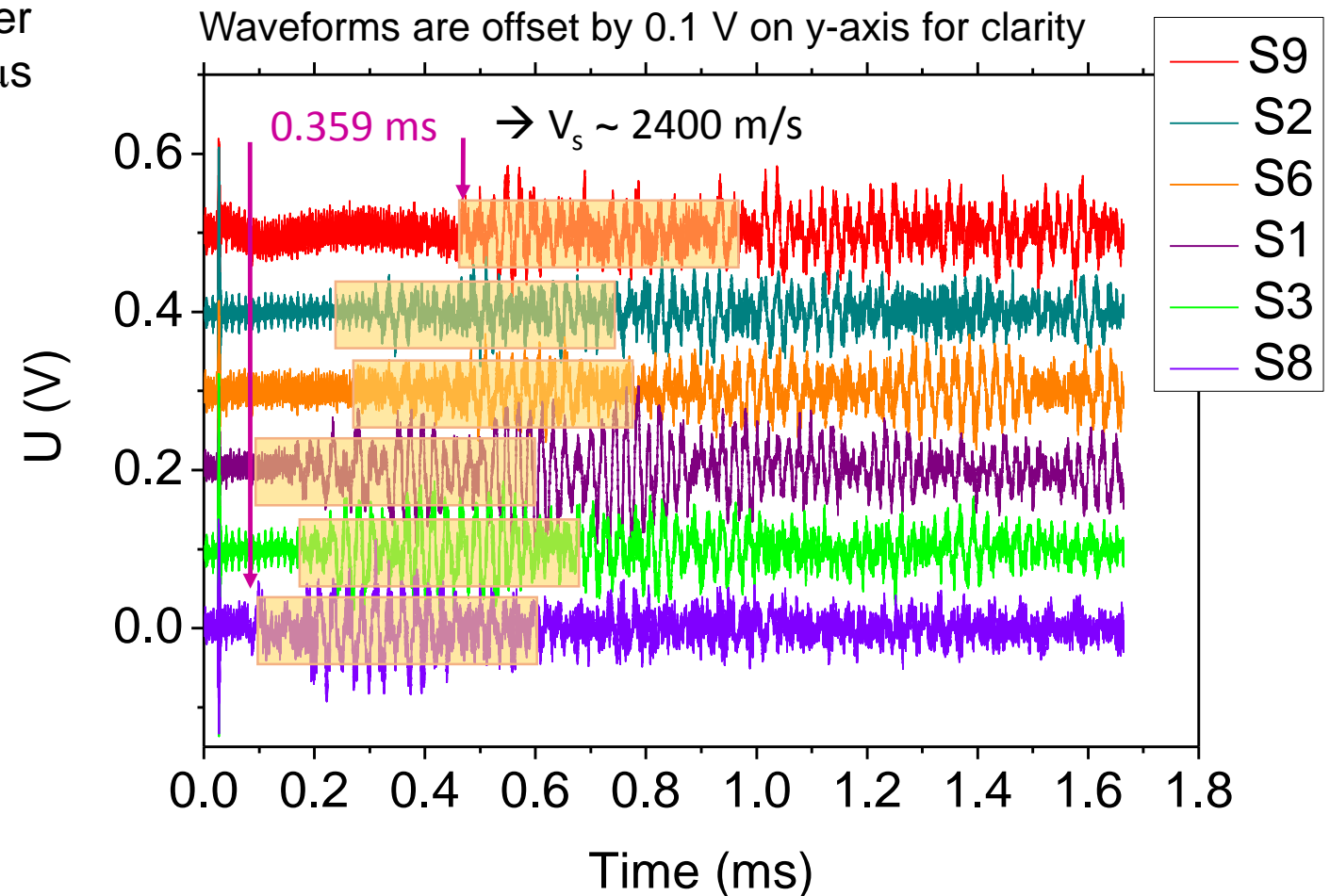


- Coil is pulsed using a piezo-transducer, and resulting perturbation is recorded by sensors distributed along the magnet
- The ring-down deformation  $x(t)$  at any location is **uniquely defined** by the magnet geometry, Young's moduli of the materials, and their mutual **interfaces**
- Acoustic wave reverberates multiple times thus allowing to **detect structural perturbation** anywhere in the magnet
- Technique is **non-invasive**, and be adapted to existing magnet systems

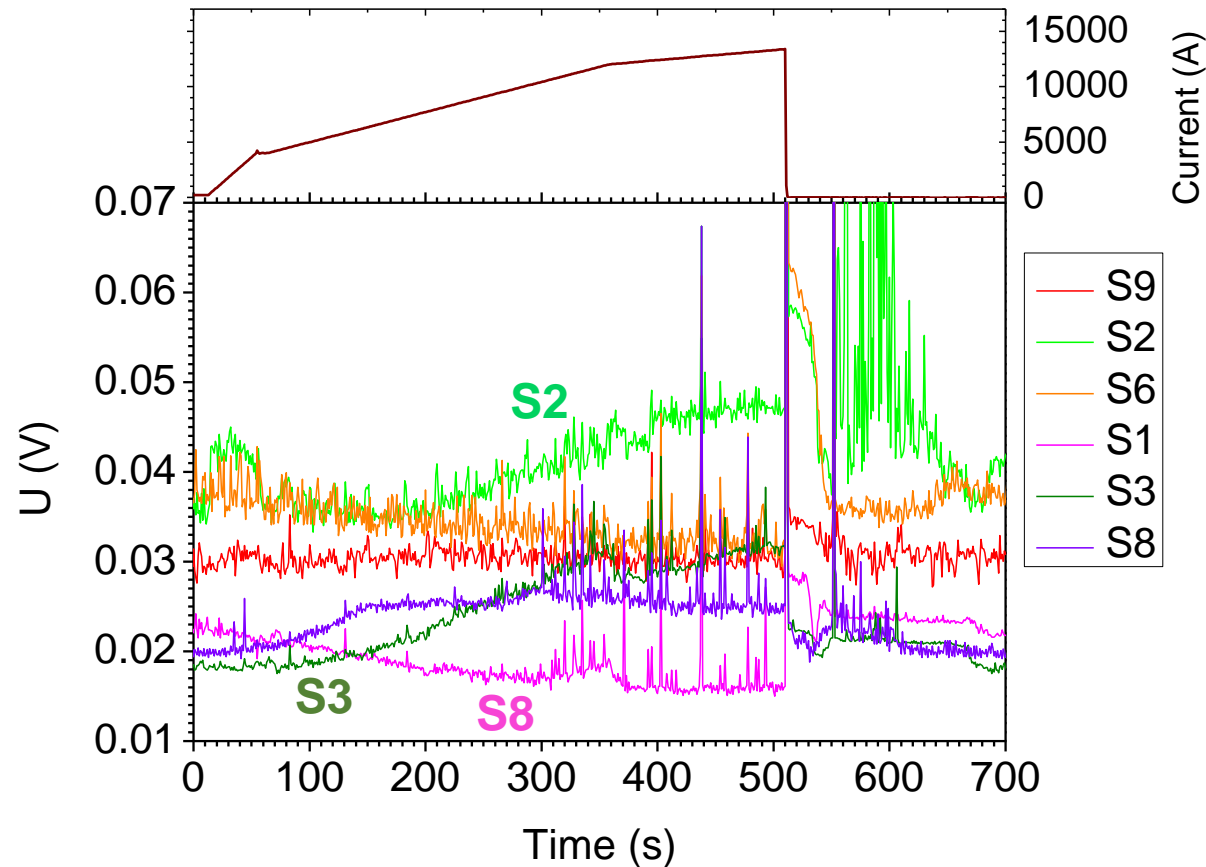
Transducer is mounted on the inner layer mandrel; powered with a 100 V / 14  $\mu$ s rectangular pulse at 1-10 Hz repetition rate



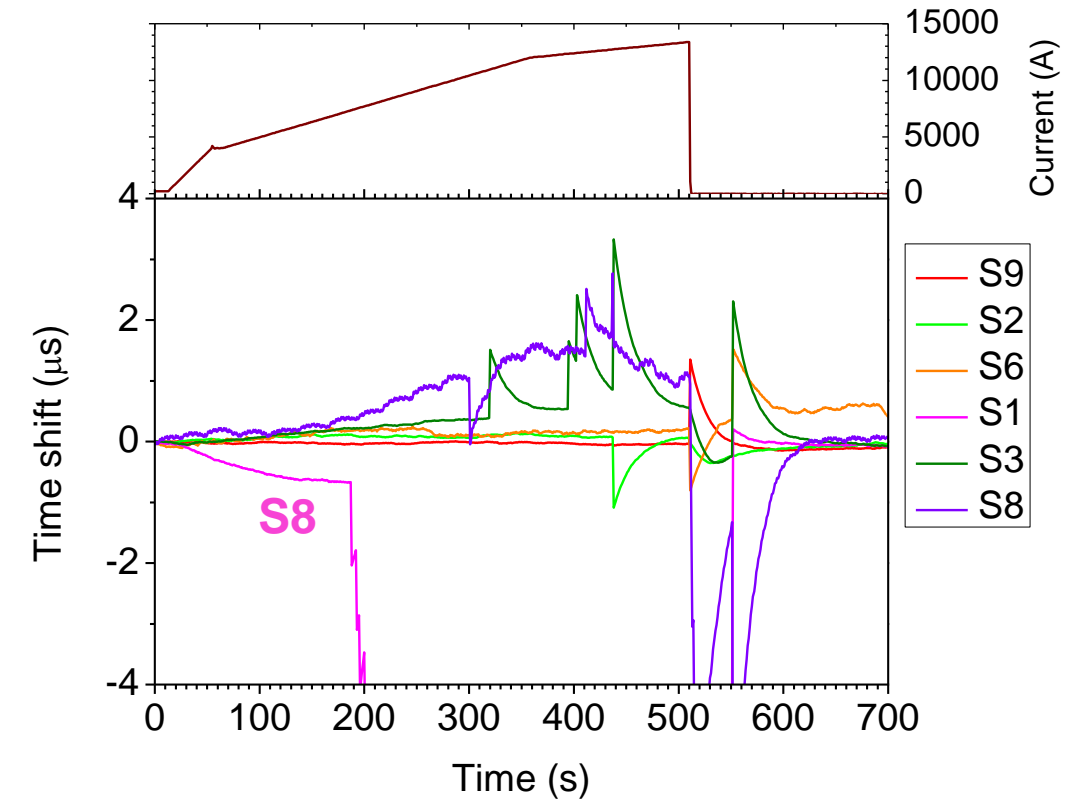
Pulse wave propagation:  
S9  $\rightarrow$  S2 S4 S6  $\rightarrow$  S3 S2 S7  $\rightarrow$  S8



0.5 ms window is set individually for each waveform. and then periodically monitored with each pulse



Time shift is found by cross-correlating the initial “reference” waveforms with the consecutive ones. Same principle was used in [M. Marchevsky and S.A. Gourlay, Appl. Phys. Lett. 110, 2017 doi:10.1063/1.4973466](#)



- As magnet deforms under stress, sensors S2 and S3 are seeing an improving mechanical contact between shell and inner / outer layers, while S1 is seeing a loss of mechanical contact.

- Localization of quenches using acoustic sensor array is a solid diagnostic tool for studying mechanically-initiated quenches
- Acoustic emission diagnostics can provide a unique insight towards understanding magnet training
- Two distinctly different slopes of CCT4 training curve can be tentatively identified as ones dominated by epoxy cracking and slip-stick motion respectively
- Active acoustic approach allows for a real-time monitoring of magnet mechanical integrity and rigidity of its interfaces

*Work in progress on analyzing high-frequency acoustic data, and developing algorithms for events sorting according to their associated disturbance spectra and deposited energy.*