

## 1. Background and objective

Coil assembly using multiple conductors with different  $I_c$

High  $I_c$  conductor at high normal magnetic field ( $I_c$  grading) can reduce whole ac loss in coil assembly

Low  $I_c$  conductor is relatively cheap compared with high  $I_c$  conductor

Complicated ac loss density distribution

Ac loss characteristics in coil assemblies are complexity related to distribution of magnetic field seen by conductors

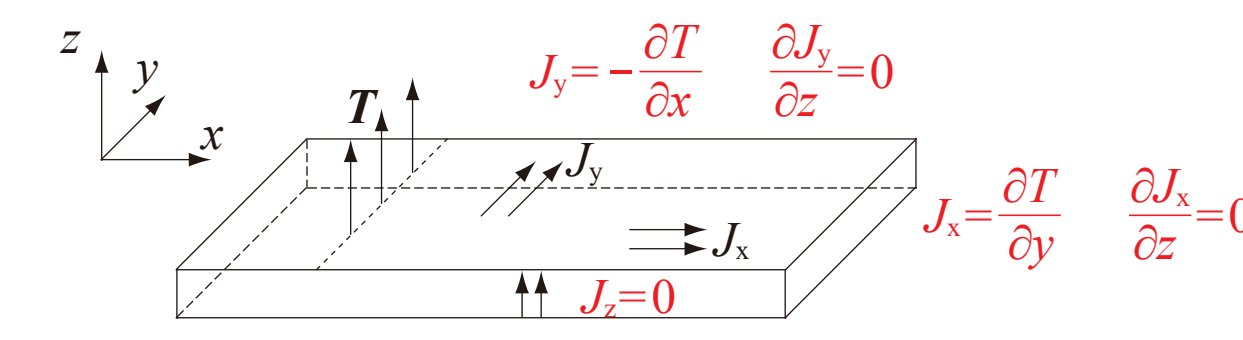
- Conducting cross-sectional electromagnetic field analyses for coil assemblies
- Revealing how coil geometries and conductors affect ac loss density distribution

## 2. Analysis method and analyzed coils

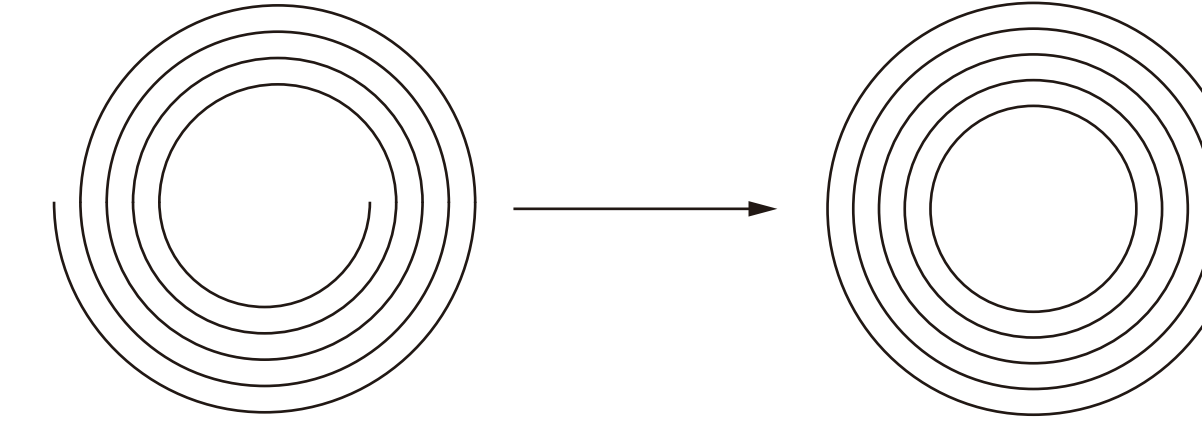
Equation to be solved in cross-sectional model

$$-\frac{\partial}{\partial y} \frac{1}{\sigma} \frac{\partial T}{\partial y} \mathbf{n} + \frac{\partial}{\partial t} \left( \sum \int \mathbf{B}_{s-f} \cdot \mathbf{n} \frac{\partial T'}{\partial y'} \mathbf{n}' t_s dy' \right) = 0.$$

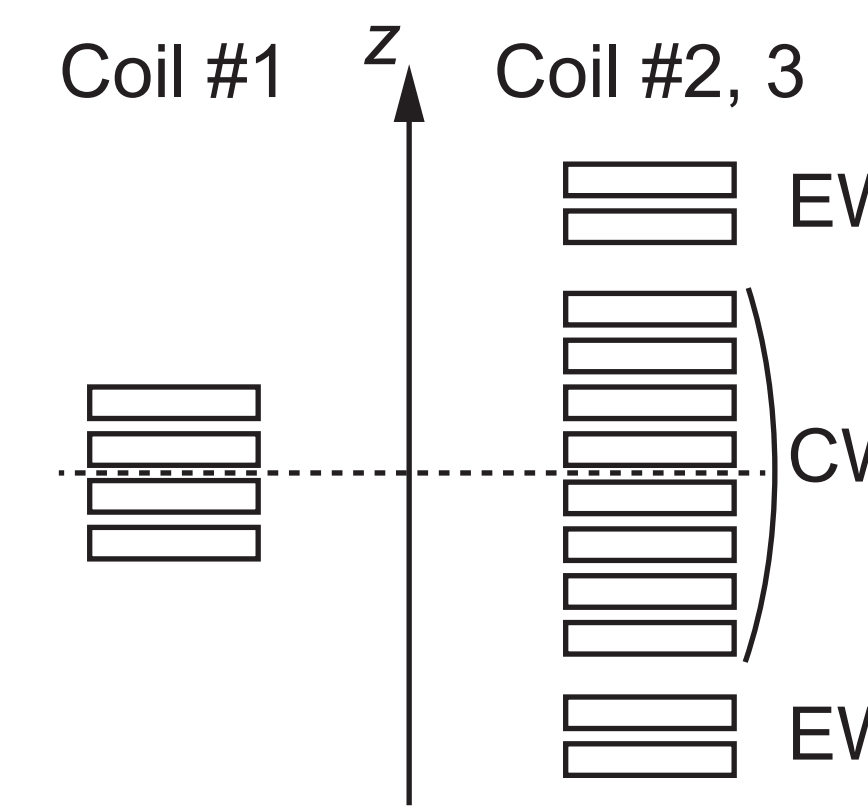
Thin strip approximation



Axisymmetric approximation



Specifications of analyzed coil assemblies			
Coil no.	#1	#2	#3
Number of PCs	4	12 (8 in CW / 4 EWs)	12
Conductor used	#1	#1 (EW) #2 (CW)	#3 (EW) #2 (CW)
Inner / outer radius	30 mm / 36.5 mm		
Overall height	20 mm	64 mm	64 mm
Gap between PCs in EW / CW	1 mm		
Gap between EW and CW	N/A	2 mm	2 mm
Number of turns / PC	20 / PC		
Separation between turns	0.225 mm		
Total conductor length	16.7 m	50.0 m	50.0 m



## 3. Field dependence of $J_c$ & $n$ of conductors

Specifications of conductors

Conductor no.	#1	#2	#3
Manufacturer	SuperPower	SuperPower	SuNAM
Lot no.	SCS4050-AP M3-774-1	SCS4050-AP M4-134-3	HCN04200 14111401
Width	4.0 mm	4.0 mm	4.0 mm
Tape thickness	0.1 mm	0.1 mm	0.1 mm
superconducting layer thickness	1.0 $\mu$ m	1.0 $\mu$ m	1.3 $\mu$ m

Formulation of  $J_c(B, \phi)$  &  $n(B, \phi)$

$$x(B, \phi) = (x_{ab}^m + x_c^m)^{1/m},$$

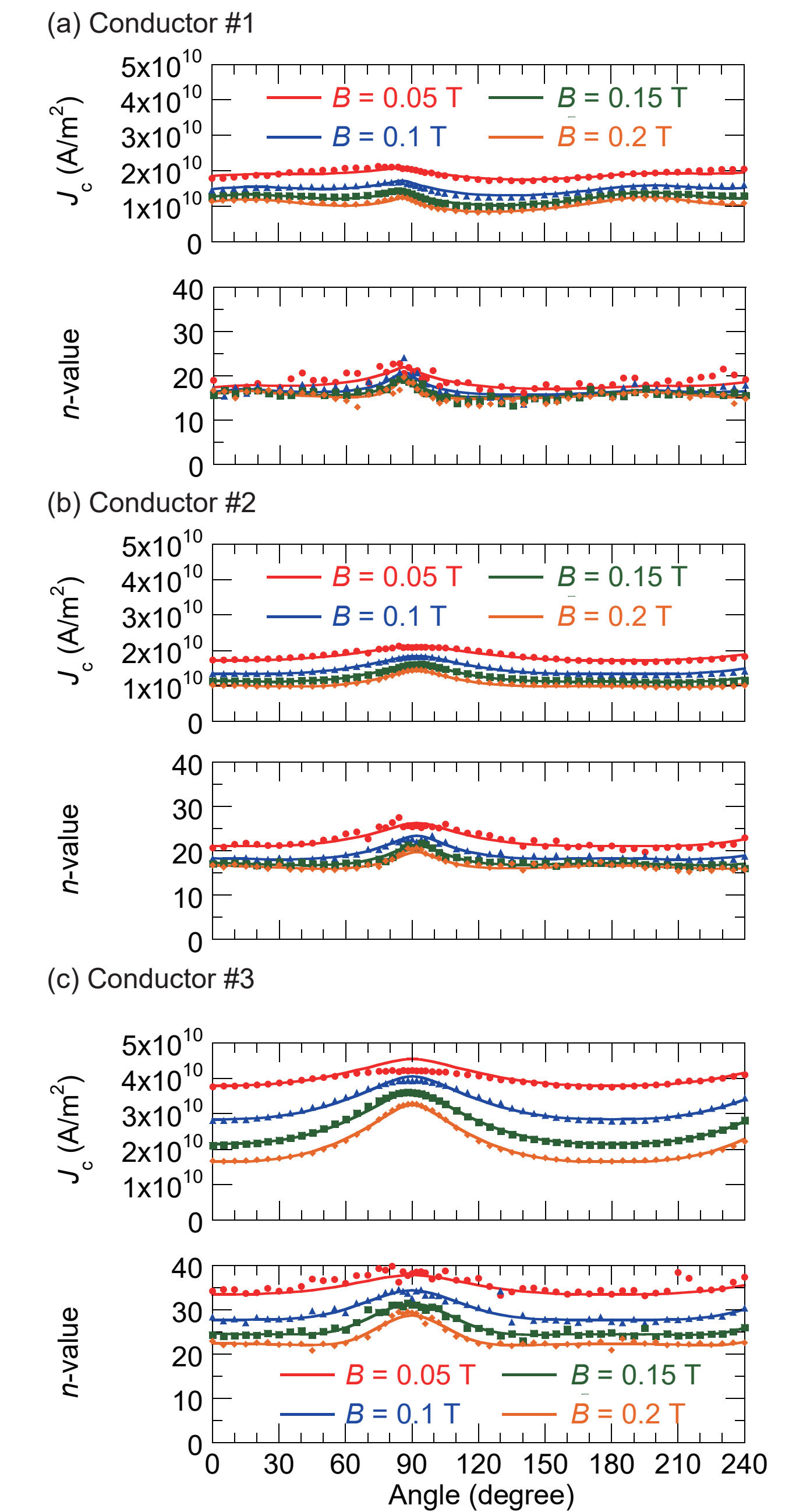
$$x_{ab,c}(B, \phi) = x_{0ab,c} / (1 + B f_{ab,c}(\phi)) B_{0ab,c}^{f_{ab,c}}.$$

$x$  means  $J_c$  or  $n$ , and the subscription  $ab,c$  means  $ab$  or  $c$

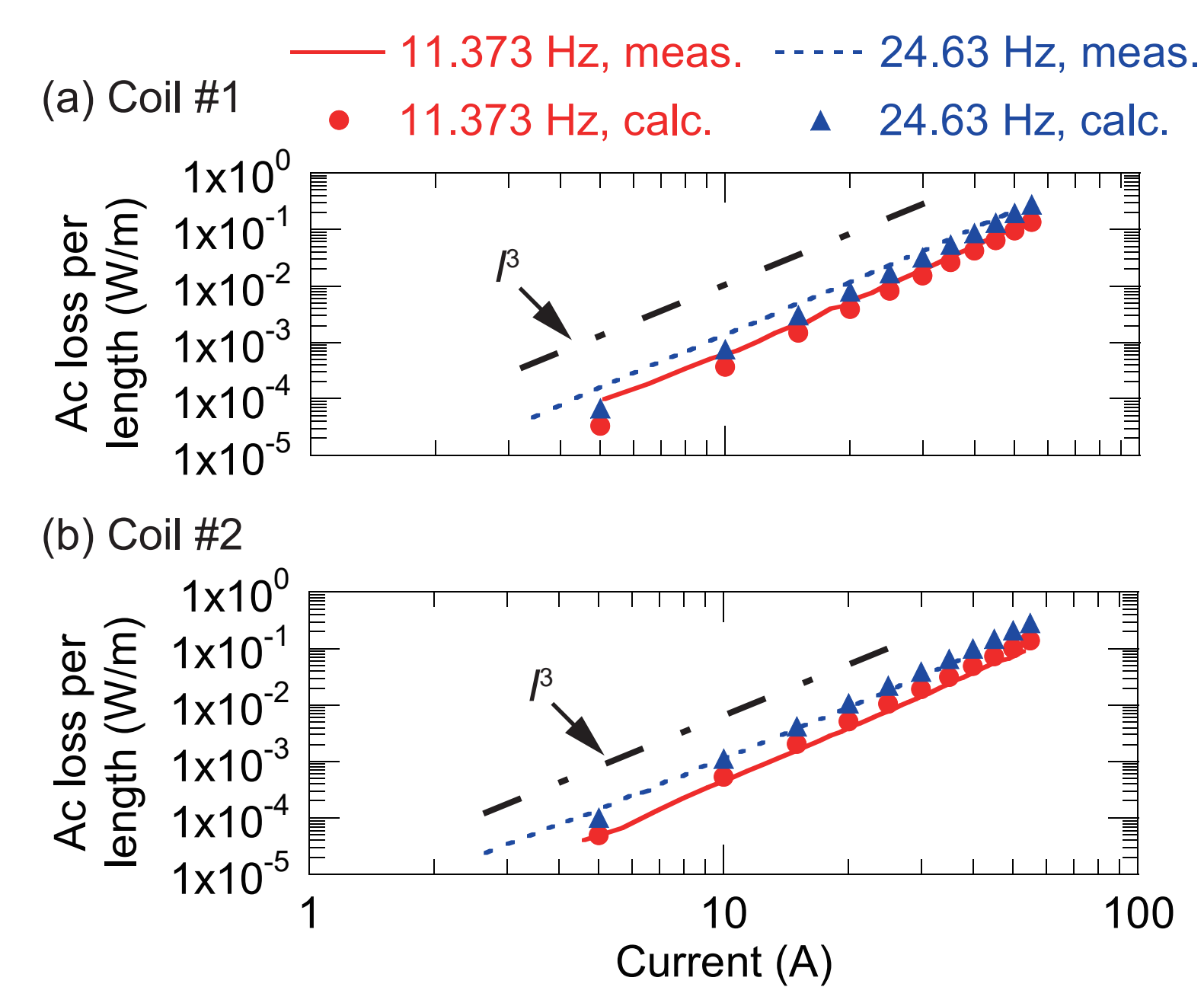
$$f_{ab}(\phi) = \sqrt{u_{ab}^2 \cos^2(\phi - \delta_{ab}) + \sin^2(\phi - \delta_{ab})},$$

$$f_c(\phi) = \begin{cases} \sqrt{\cos^2(\phi - \delta_c) + u_c^2 \sin^2(\phi - \delta_c)} & (-90^\circ + \delta_c \leq \phi \leq 90^\circ + \delta_c) \\ \sqrt{v^2 \cos^2(\phi - \delta_c) + u_c^2 \sin^2(\phi - \delta_c)} & (\text{otherwise}) \end{cases}$$

$\phi = 0$  is the direction of normal vector of wide face of conductor

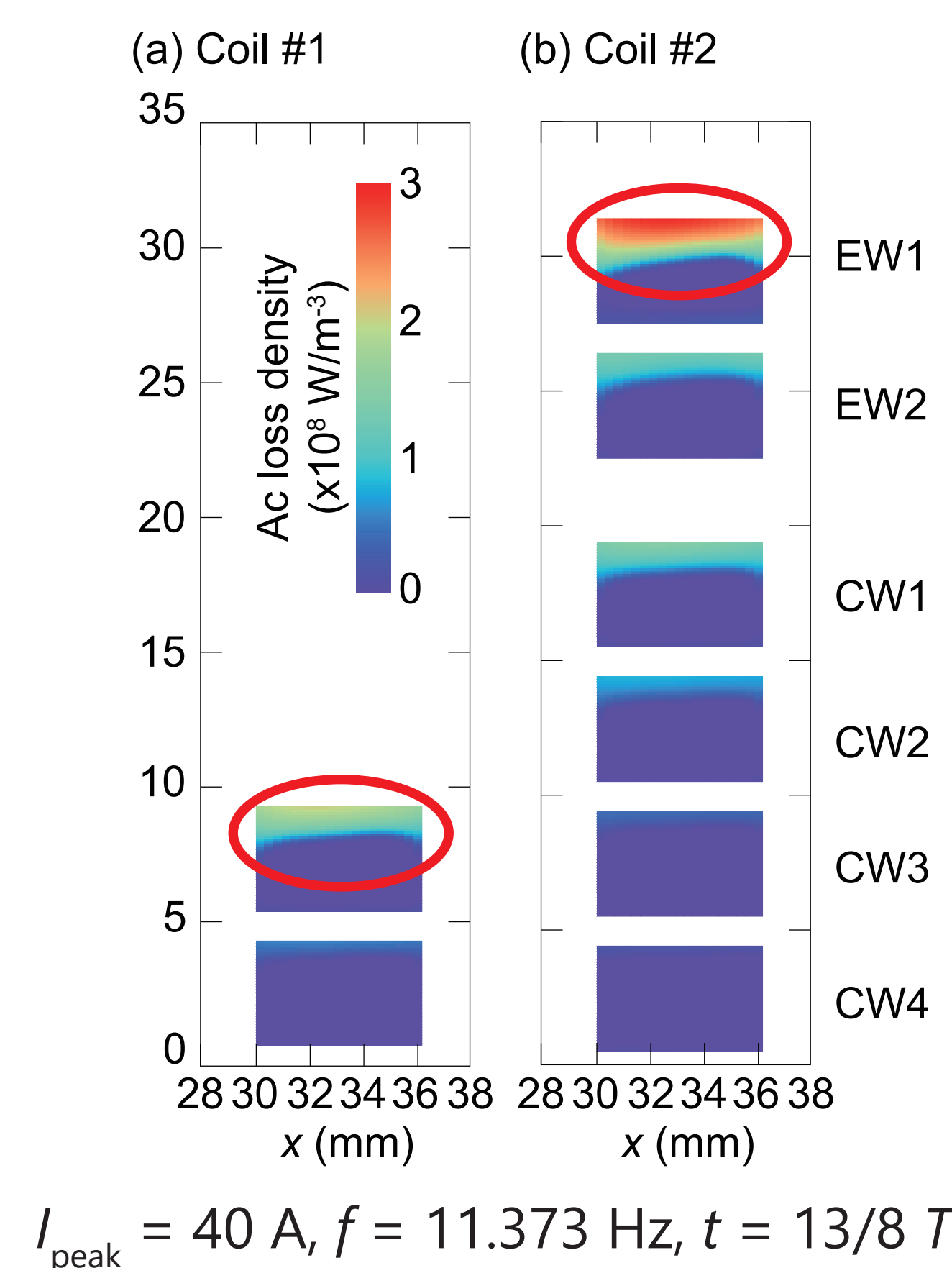


## 4. Meas. & Calc. results – coil #1 vs. #2



Calculated ac losses when  $I_{peak} = 40$  A,  $f = 11.373$  Hz

Coil no.	#1	#2
J/cycle	$6.18 \times 10^{-2}$	$2.14 \times 10^{-1}$
J/m/cycle	$3.71 \times 10^{-3}$	$4.28 \times 10^{-3}$



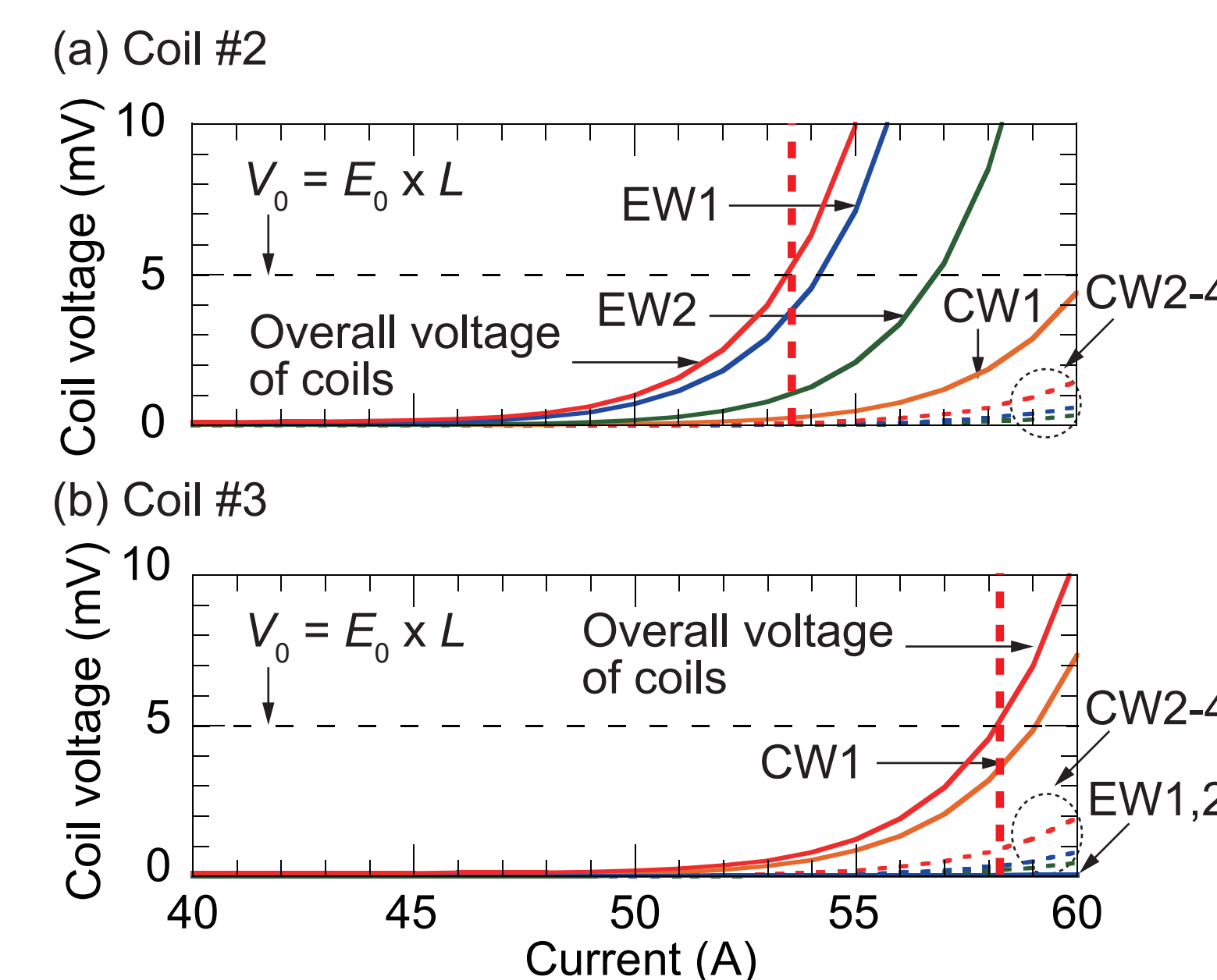
Meas. and calc. results were in good agreement

- Concentrated ac loss density in the outermost coil
- Large magnetic field lead to large ac loss density

## 5. Effect of $I_c$ grading (coil #2 vs. #3) – coil $I_c$

Coil $I_c$	
Coil #2	53.4 A
Coil #3	58.2 A

Only 9% increase

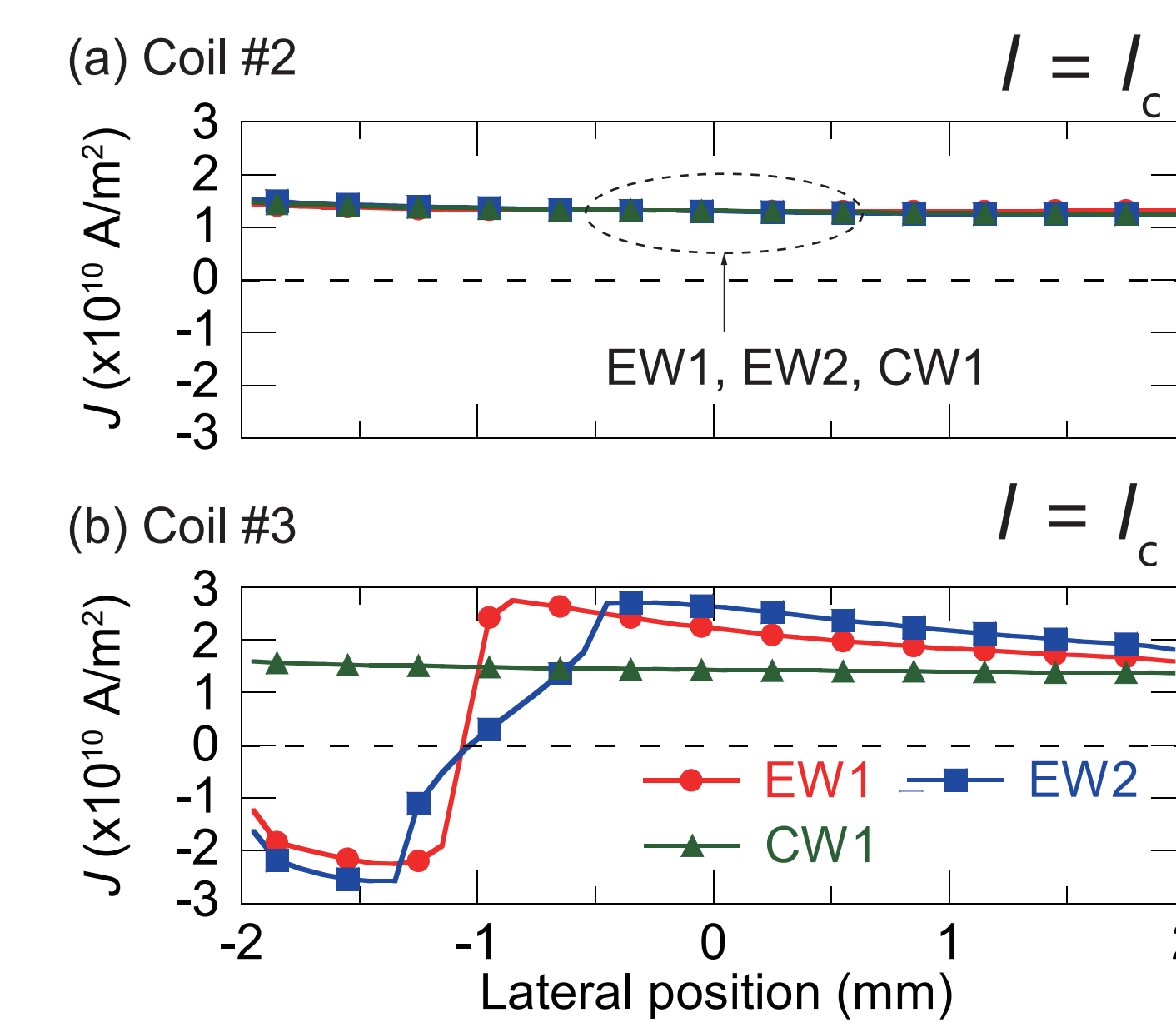


No contributions of EW1,2 in coil #3 to overall voltage

Increase of voltage in CW1 in coil #3

Twice higher  $I_c$  conductor in EW resulted in only 9% increase in coil  $I_c$ .

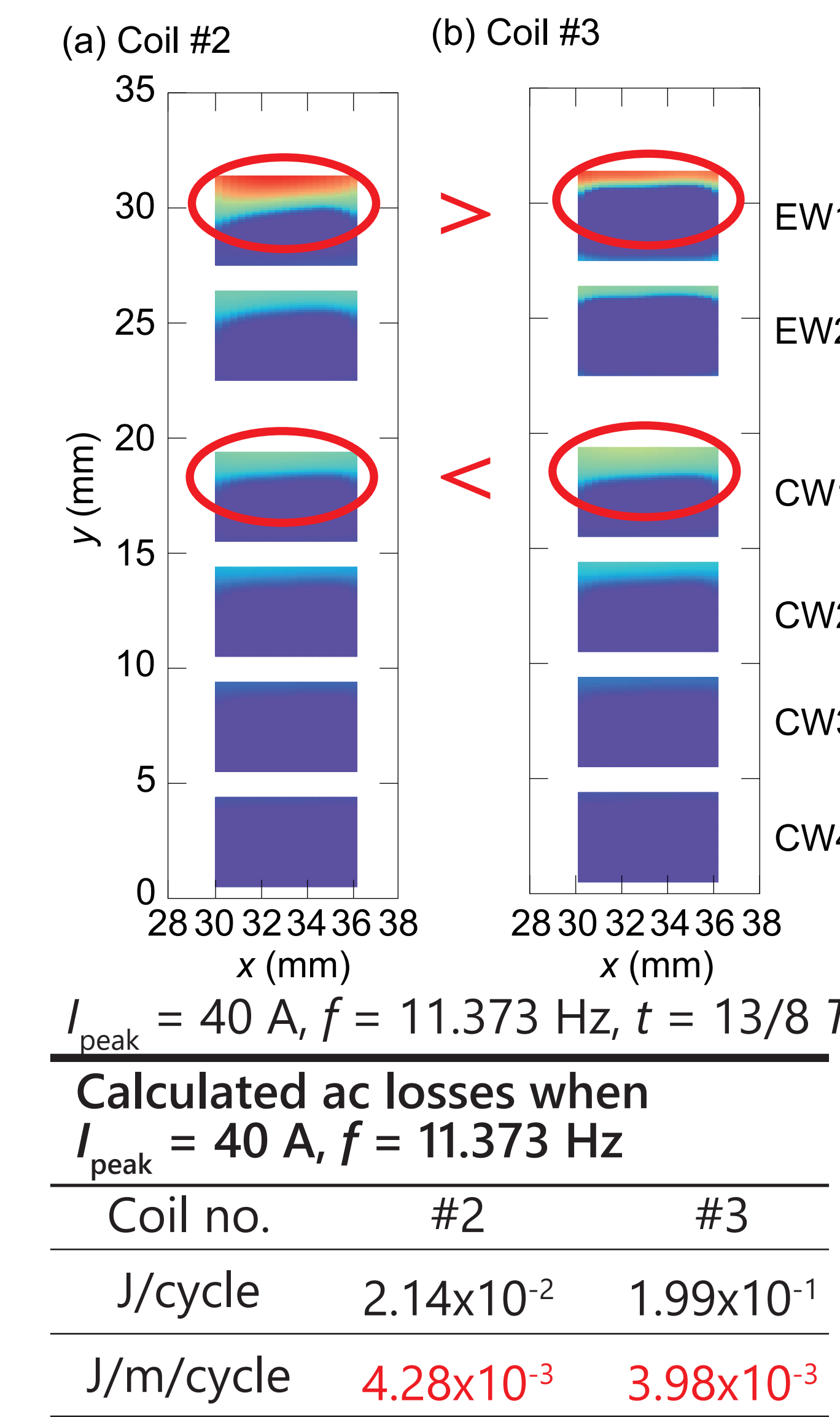
Why?



Strong non-uniformity of  $J$  distribution in EW in coil #3

Increase in the magnetic field at CW1 in coil #3

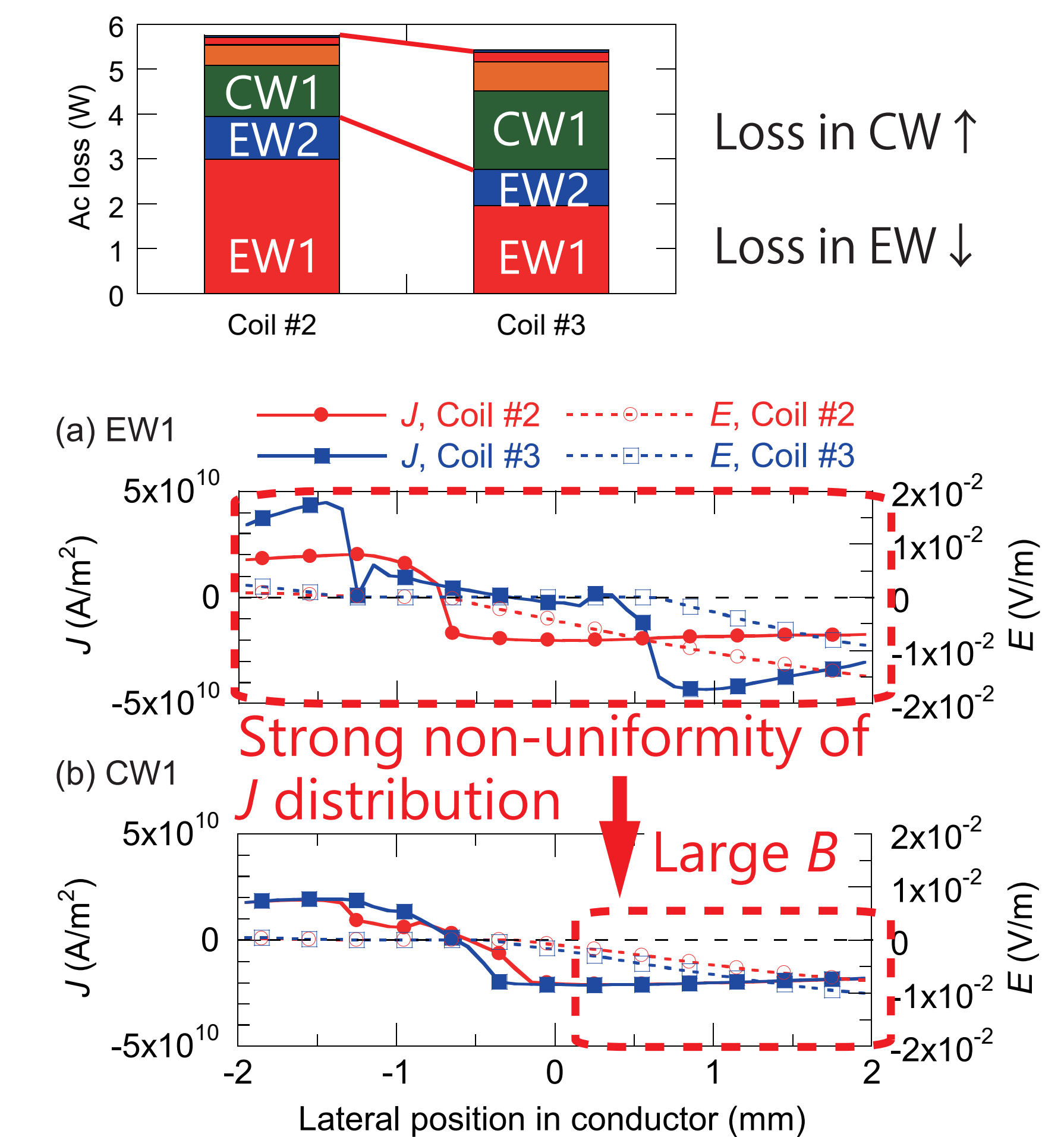
## 6. Effect of $I_c$ grading (coil #2 vs. #3) – ac loss



Calculated ac losses when  $I_{peak} = 40$  A,  $f = 11.373$  Hz

Coil no.	#2	#3
J/cycle	$2.14 \times 10^{-2}$	$1.99 \times 10^{-1}$
J/m/cycle	$4.28 \times 10^{-3}$	$3.98 \times 10^{-3}$

Decrease in ac loss, but small effect



High  $J_c$  in EW results in strong magnetic interaction between coils, and it deteriorate effect of  $I_c$  grading

## Acknowledgement

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