



Hi-Lumi LHC Twin Aperture Orbit Correctors 0.5 m Model Magnet Development & Cold Test

Presented by G. De Rijk

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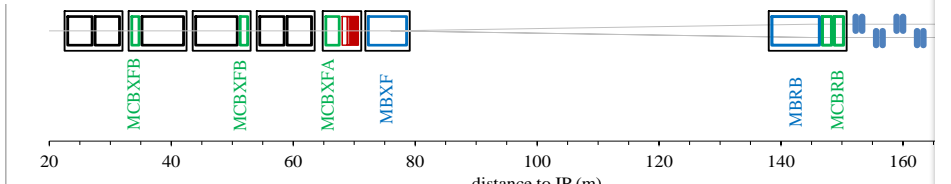
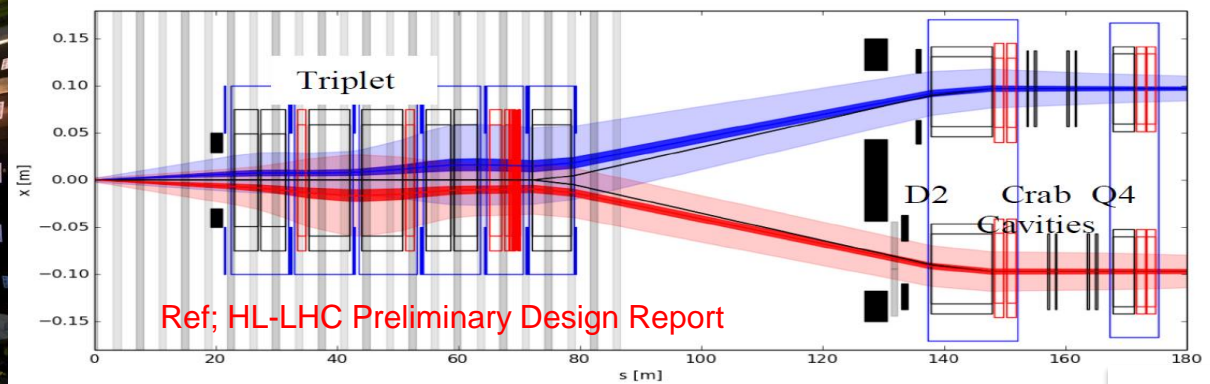
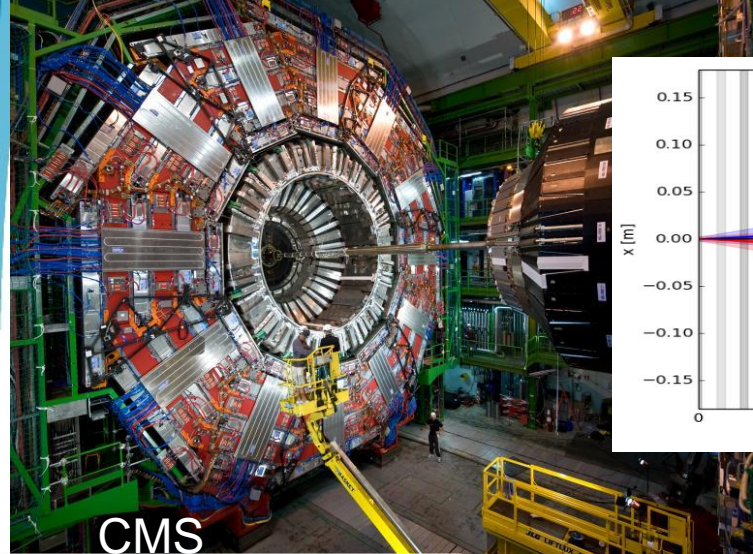
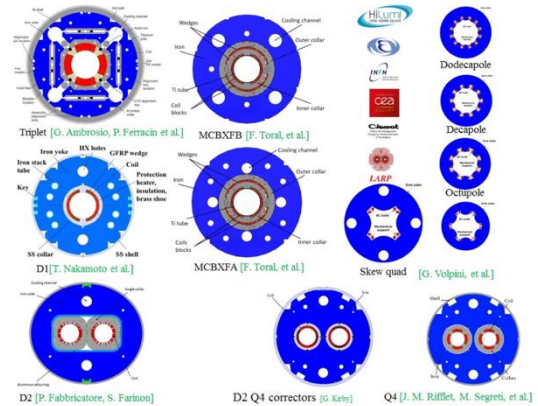
Talk Over View

- What is “High Luminosity LHC”
- Orbit Corrector Function & Environment
- CCT aperture development :
- Winding tests
- Coil development
- Cold test
- Planning
- Conclusions

What is "High Luminosity LHC"



Goal of Hi-Lumi LHC
increase Luminosity
by factor ~ 10
In CMS and ATLAS
Installation Due
2024 - 2026



Upgrade Magnet Set

Specification and choice of CCT

Specification

- 2 aperture H,V dipole corrector
- $\int B=5Tm$, $B= 2.8 T$, $L_{mag}=1.8m$
- $I_{max} = 600A$

Ribbon $\cos\Theta$ vs CCT

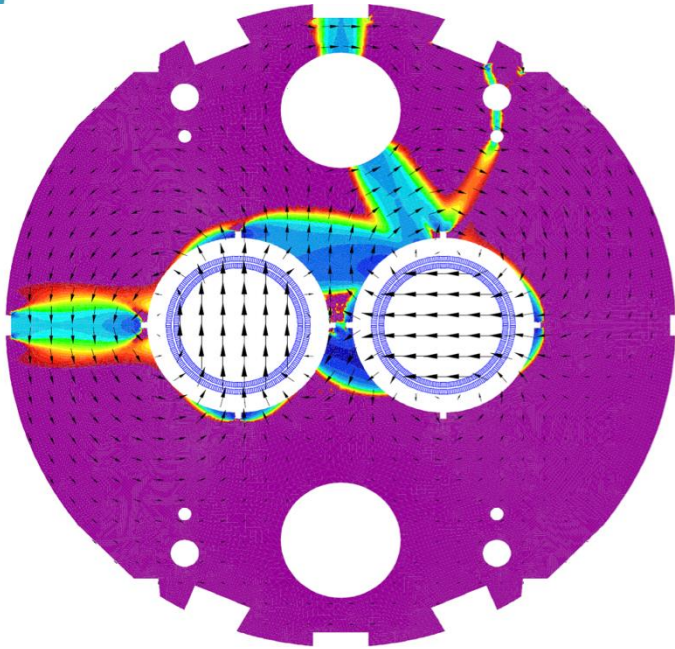
Ribbon $\cos\Theta$

- Field quality limited due to collars using up yoke space between the apertures
- Ribbon glue is rad hard limited
- Ribbon conductor suffers from electrical shorts during production and ongoing degradation during operation, probably due to radiation damage.

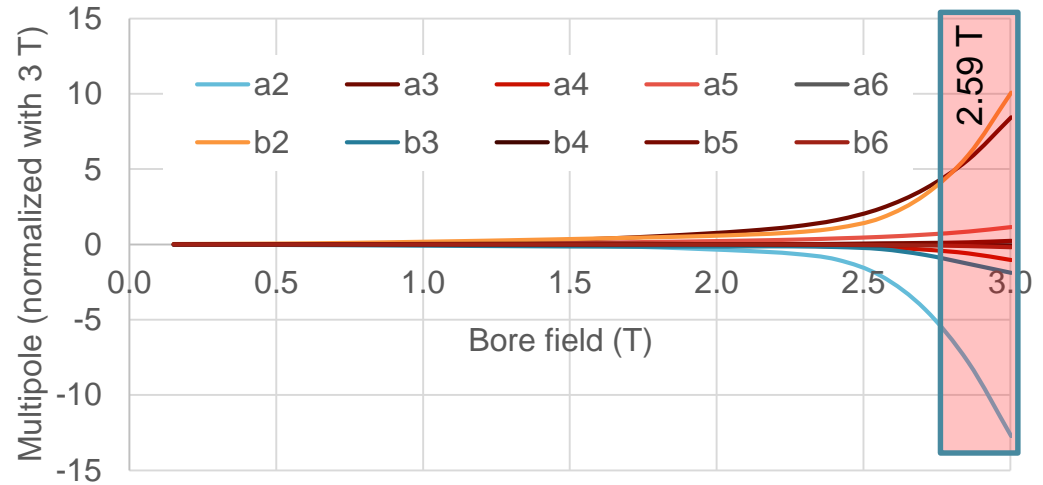
CCT:

- Radiation hard “full metal jacket” design
- Low cost
- Fast to produce.
- Very good field quality
- Little tooling

Magnetic Field Optimization



Case, Radial hybrid pole keys, aperture 2, both powered



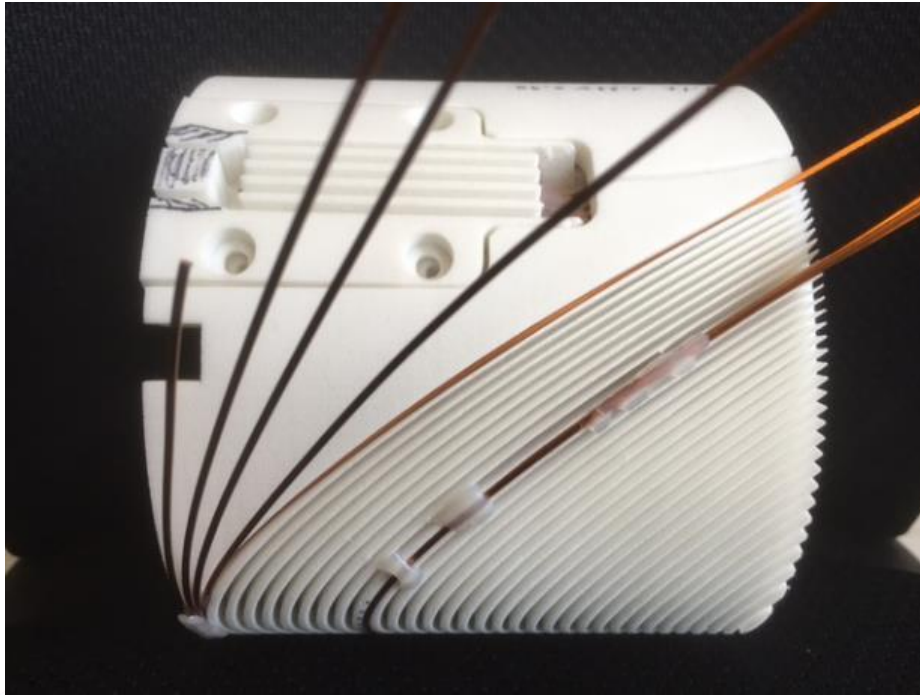
More complicated than one plot,

Example of one configuration Presenting harmonic solution due to high field in the adjacent aperture

To achieve 5 Tm field integral with less than 10 units we first determine the maximum field in one aperture that will not pollute the field quality in the adjacent aperture.

1st winding test with the rectangular wire

!!!! Rectangular wire failed !!!
Impossible to wind in channel



The enamel rectangular wire rotated as we tried to wind and finally was impossible to wind into the slot!

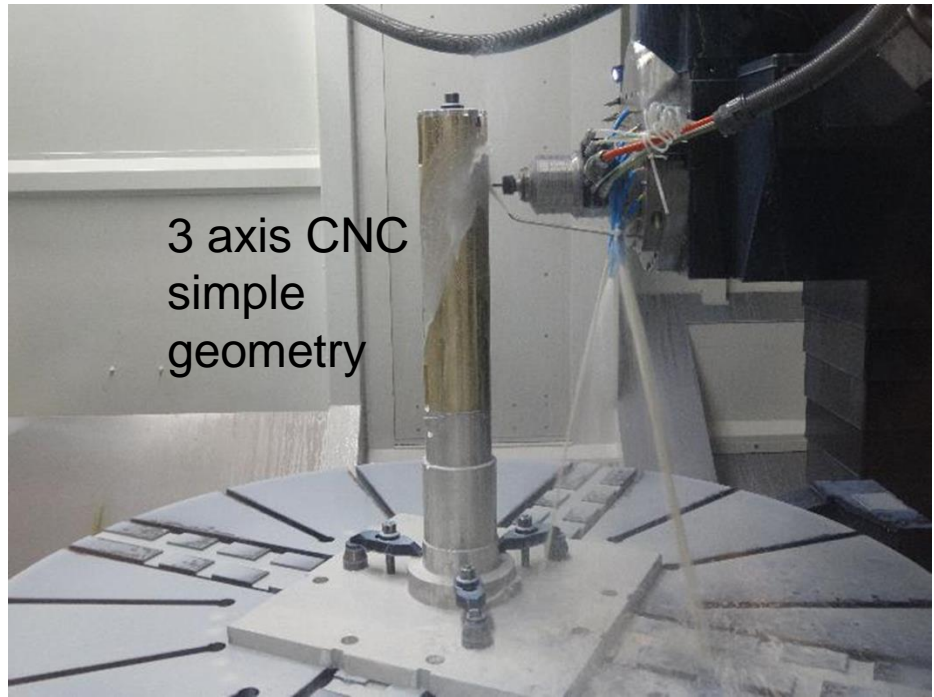




Cutting tests 0.1mm to 0.4mm wall thickness select 0.35mm min value.



1mm dia x 7 mm high speed tool.

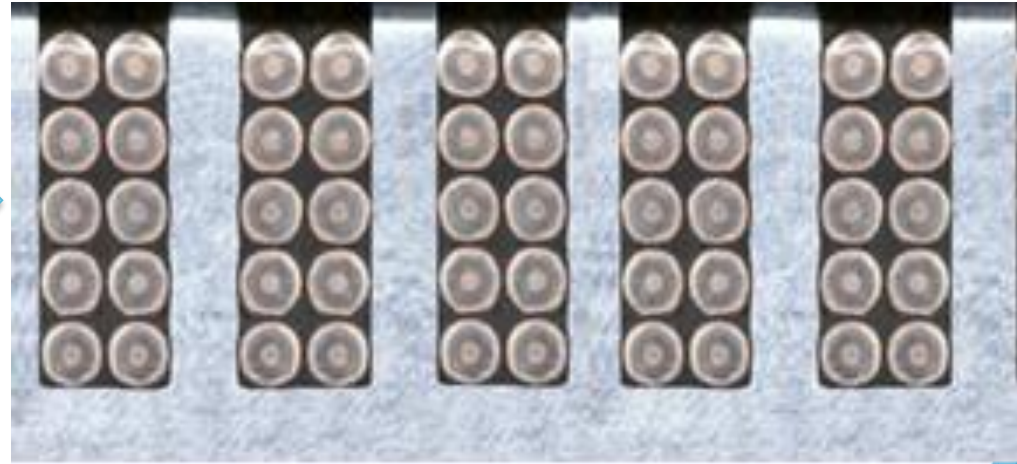
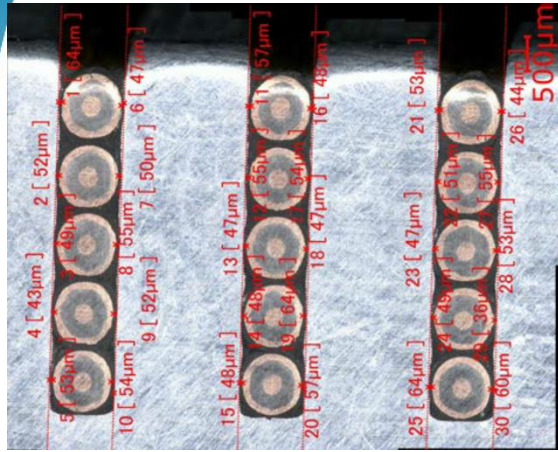


3 axis CNC
simple
geometry

Machining the short 0.5m model CCT formers
Multi pass cuts.

- With 1 mm slot the tool breaks often
- Many passes needed

Machined former development



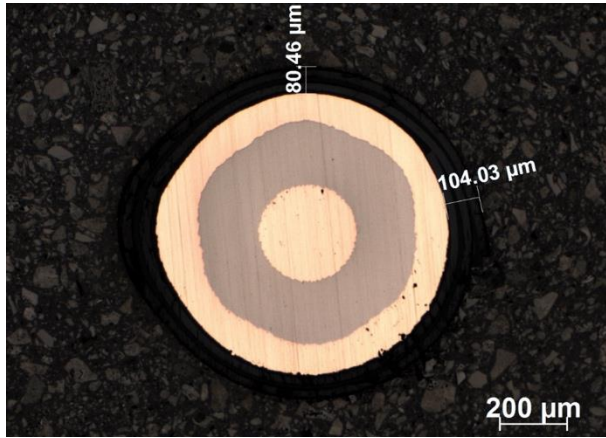
The 1mm wide x 5mm deep channel **could not be machined** over the 128 m long 0.5m former!

Moving to a 2 mm wide slot, the cutting tool is much stronger!

The machining time / cost to machine the channel is reduced!

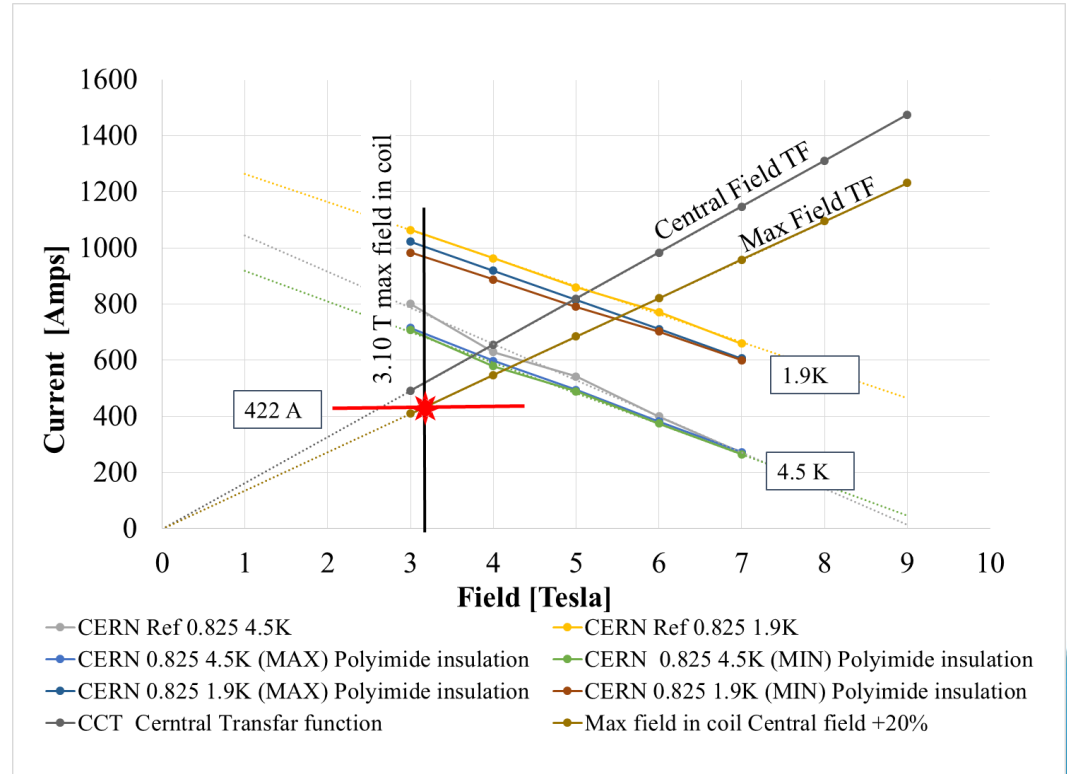
The double slot width reduces machining time (cost) but doubles the number of joints

Wire Performance with polyimide insulation

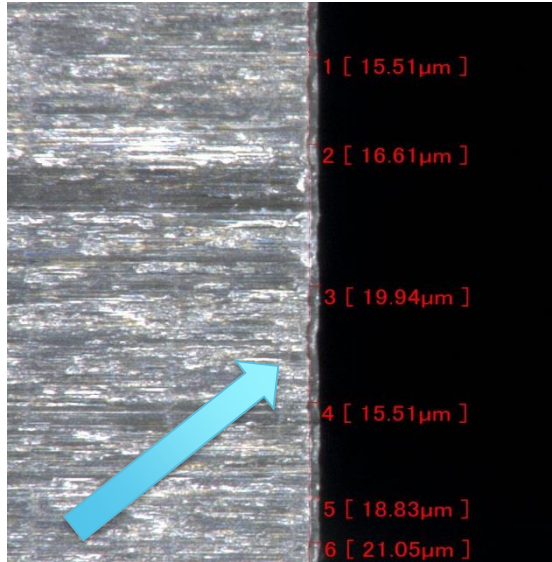


Insulation curing temperature 420 C for 30 sec degraded the wire I_c by 10%.

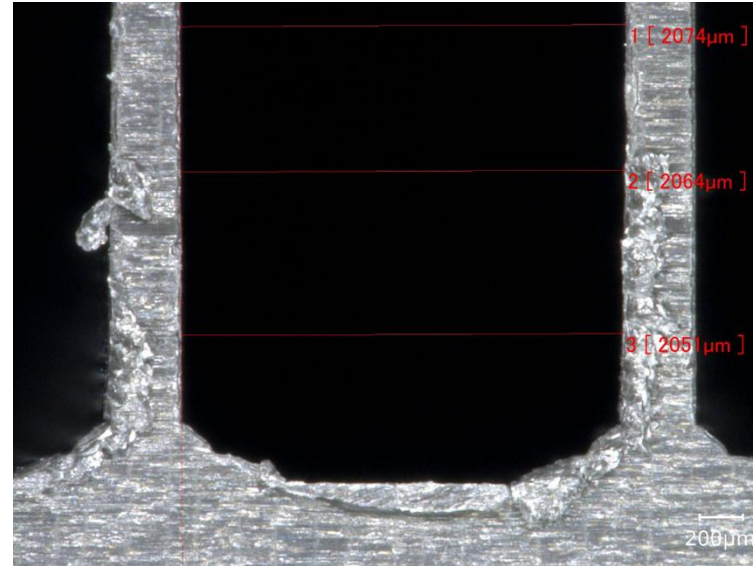
Magnet margin is still high at 55 % SS



CNC machined slot width 2.10 mm wide.
Anodization 0.040 mm layer thickness
Anodization surface build up 0.020mm
final slot width 2.06 mm



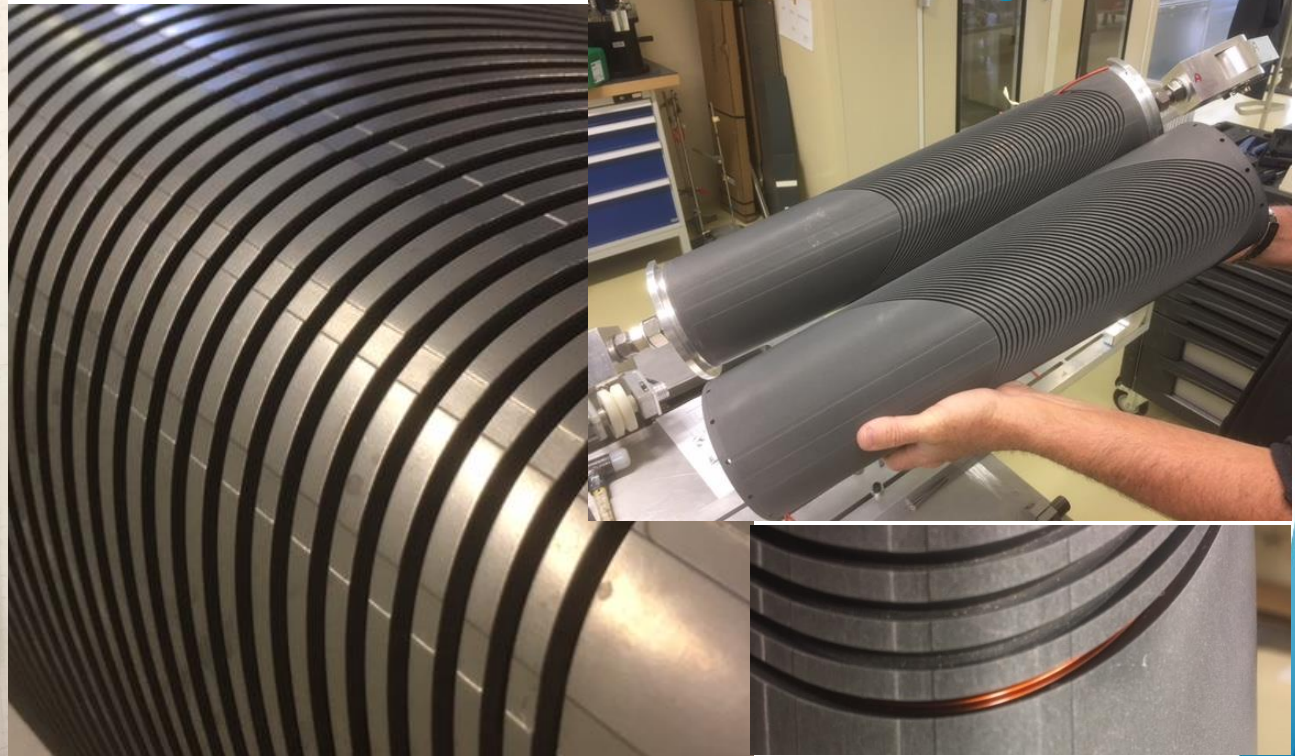
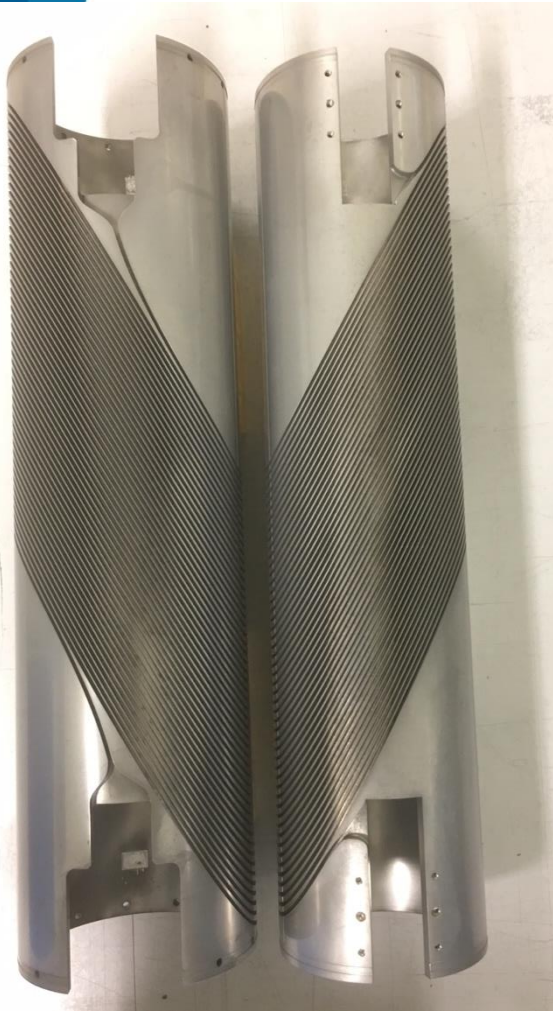
Anodized coating 0.02mm



The anodized coating give a hard surface protection that bonds well to the resin & provides some electrical insulation

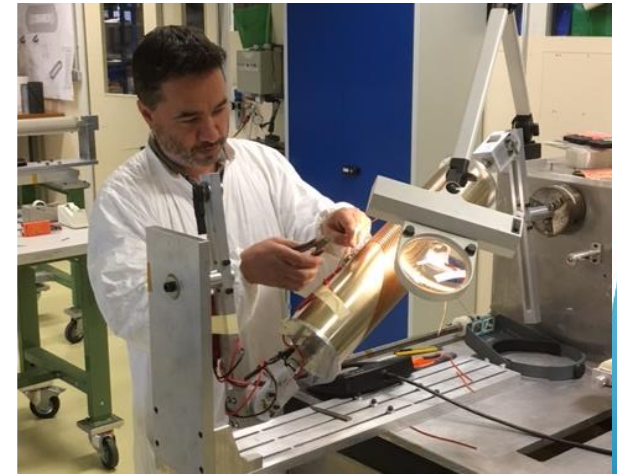
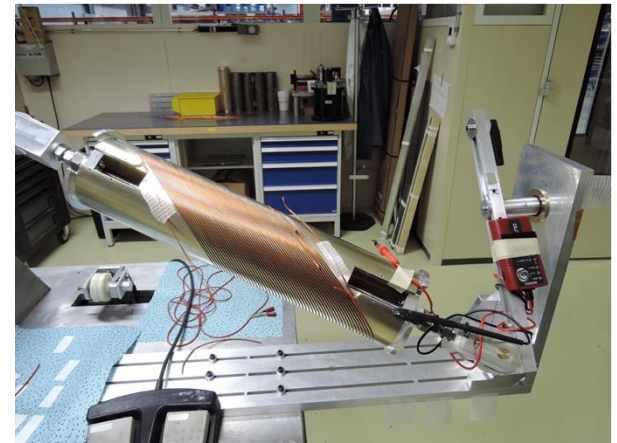
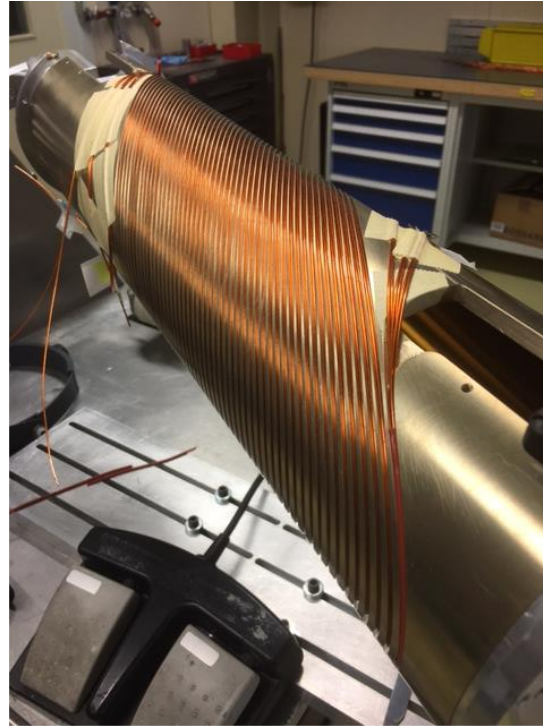
Al formers 6082-T6 for the final magnets

Polishing test to de-burr? and then Hard Anodization (Micro-Machining)



Example of polishing to remove burrs

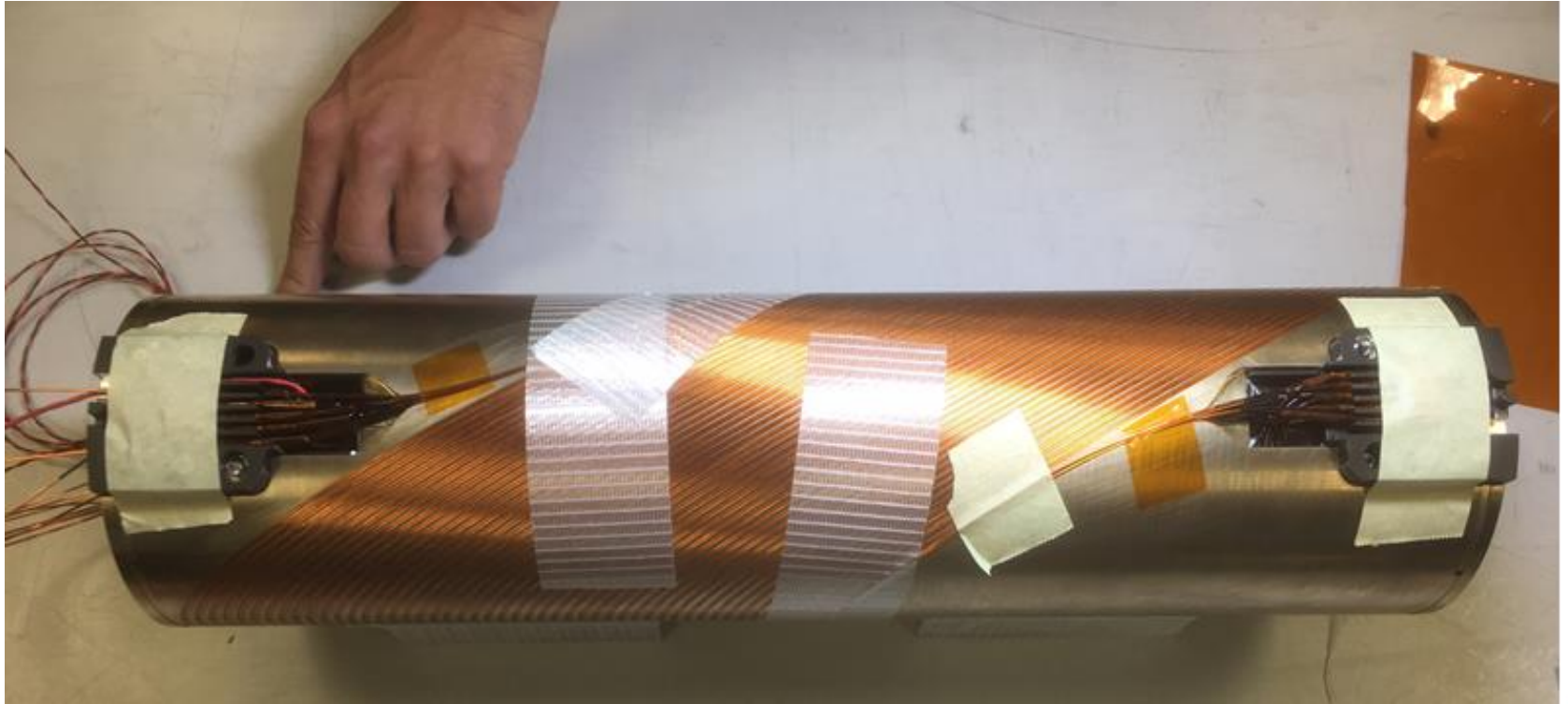
Coil Winding first model



First single aperture model still with Al-bronze formers

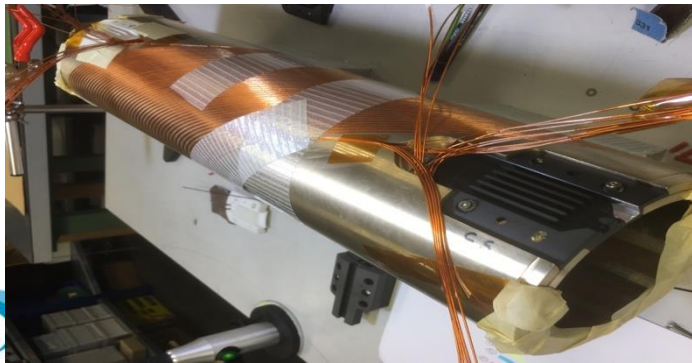
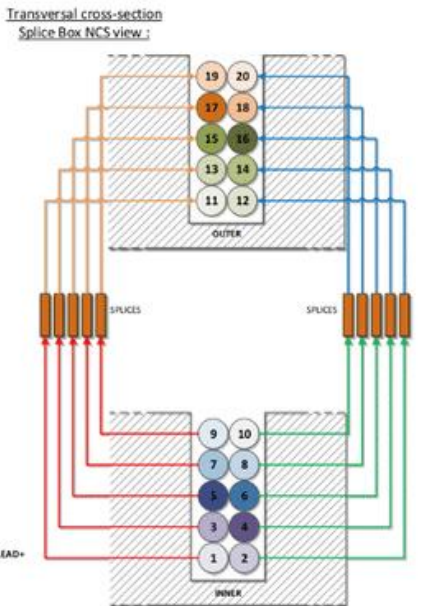
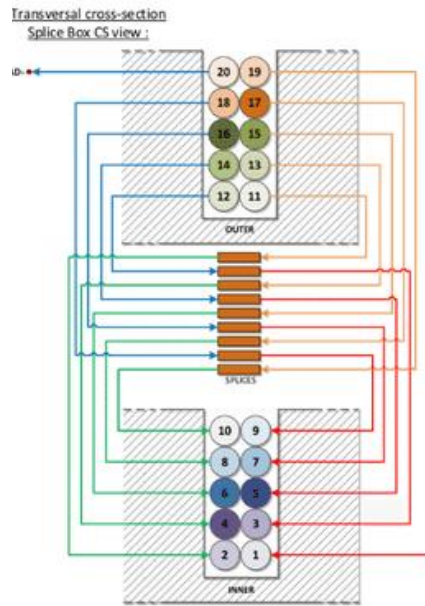
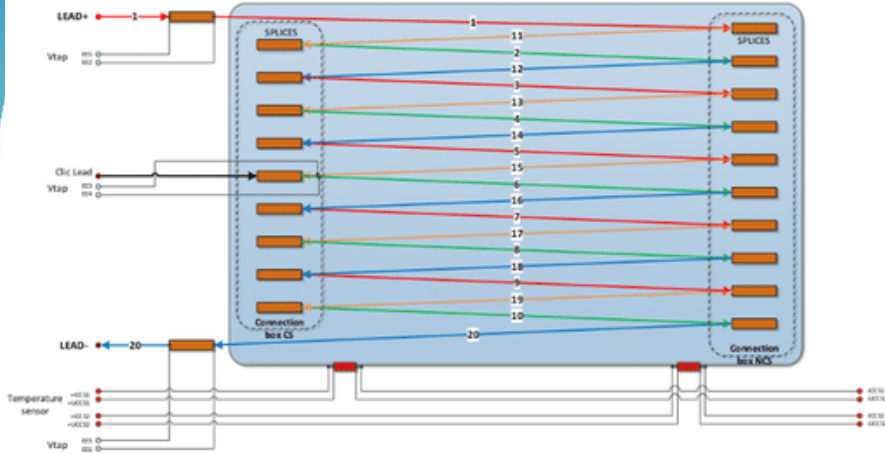
Two wires are wound at the same time, with low tension.
This is repeated until we have the full 2 wide by 5 high coil.

Joints at both end in the magnet former



The joints have to be on the former to cope with thermal contraction effects

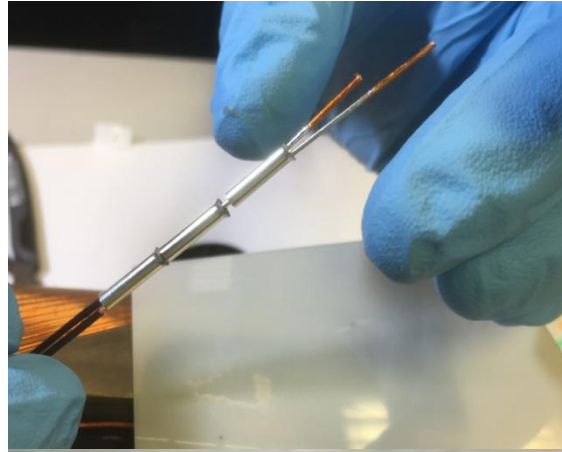
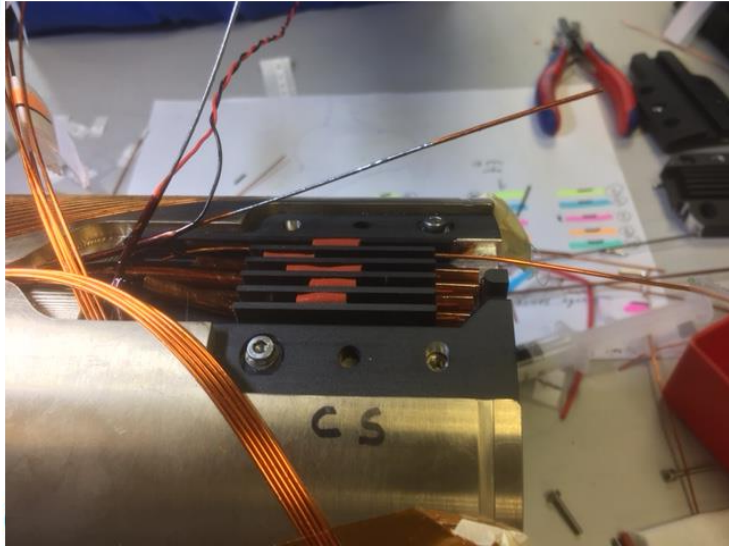
Wiring Diagram



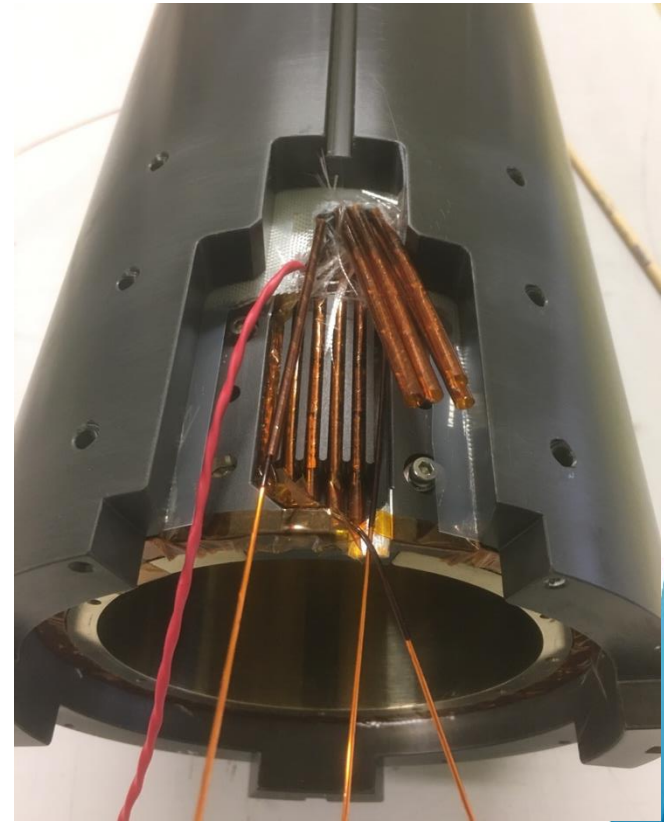
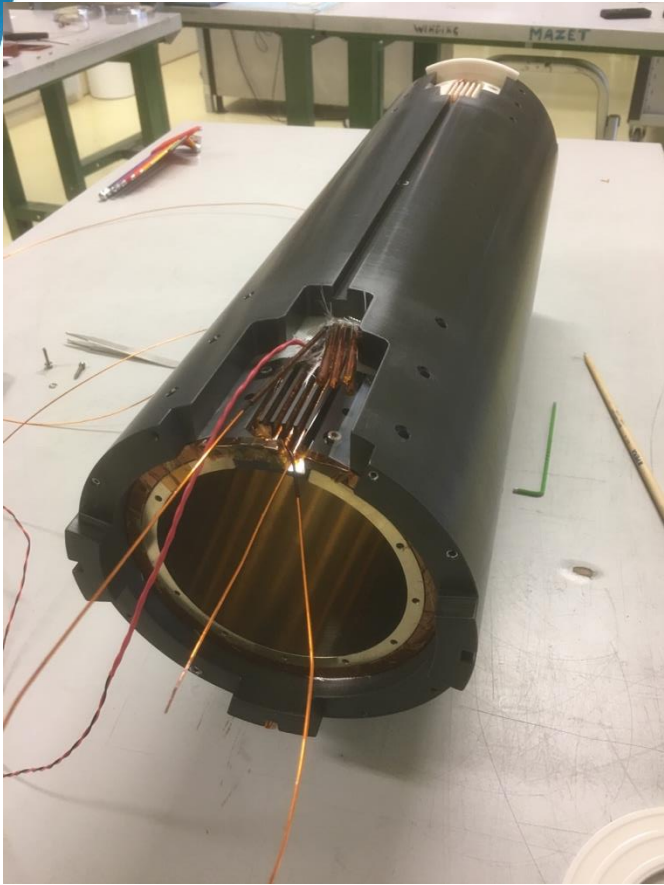
Jointing

Jointing system:

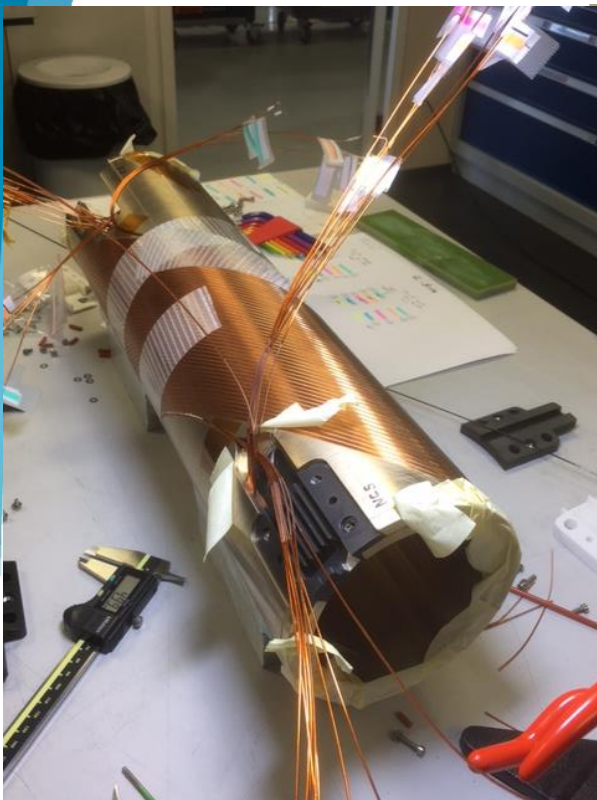
- 1) Tinned wires,
- 2) Copper tubes
- 3) Crimp for mechanical support
- 4) Solder
- 5) Insulation



Joint box



Coils impregnated inside the magnet outer support tube

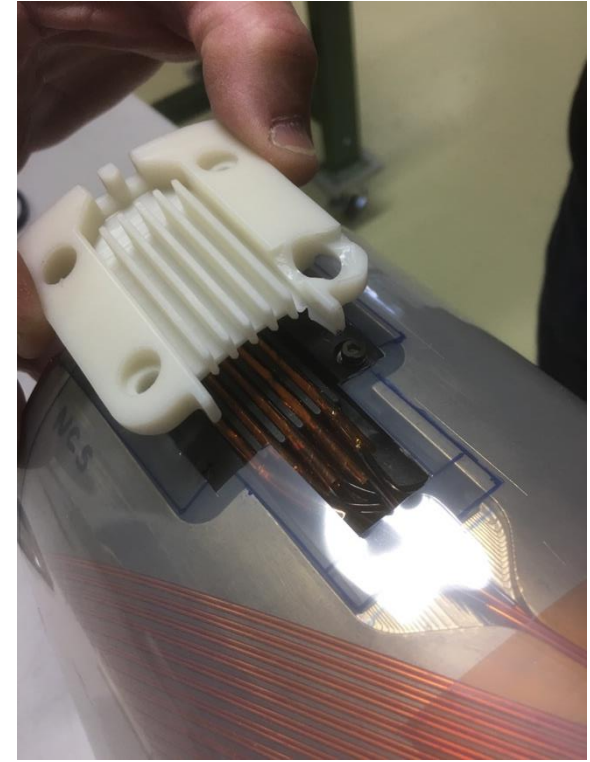


Vacuum / pressure Impregnation seal



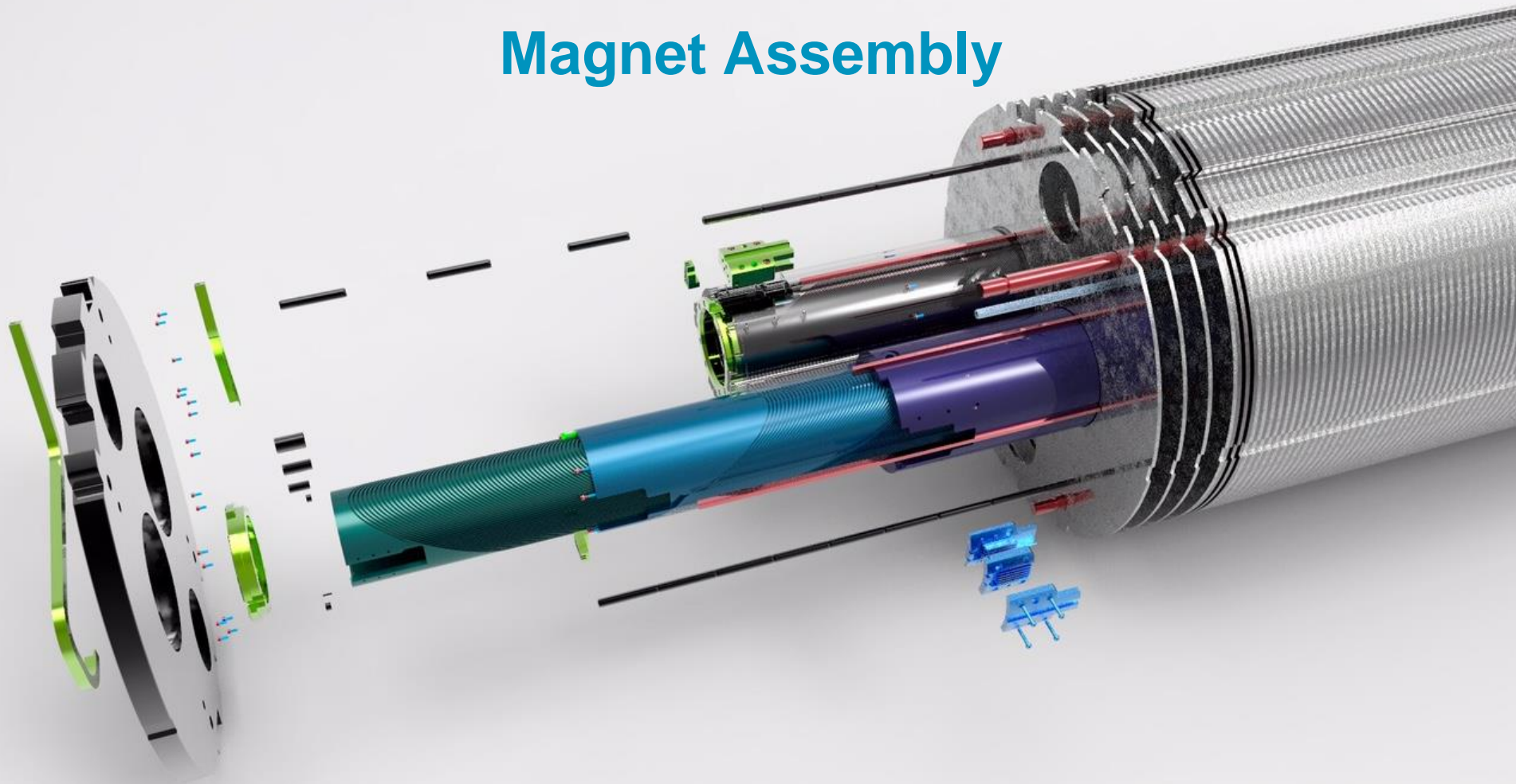
Seal mechanical support

Insulation between the two layers



Two layers of insulation Polyimide or Mylar with min 4 mm
brake down distance from ground or the other former

Magnet Assembly



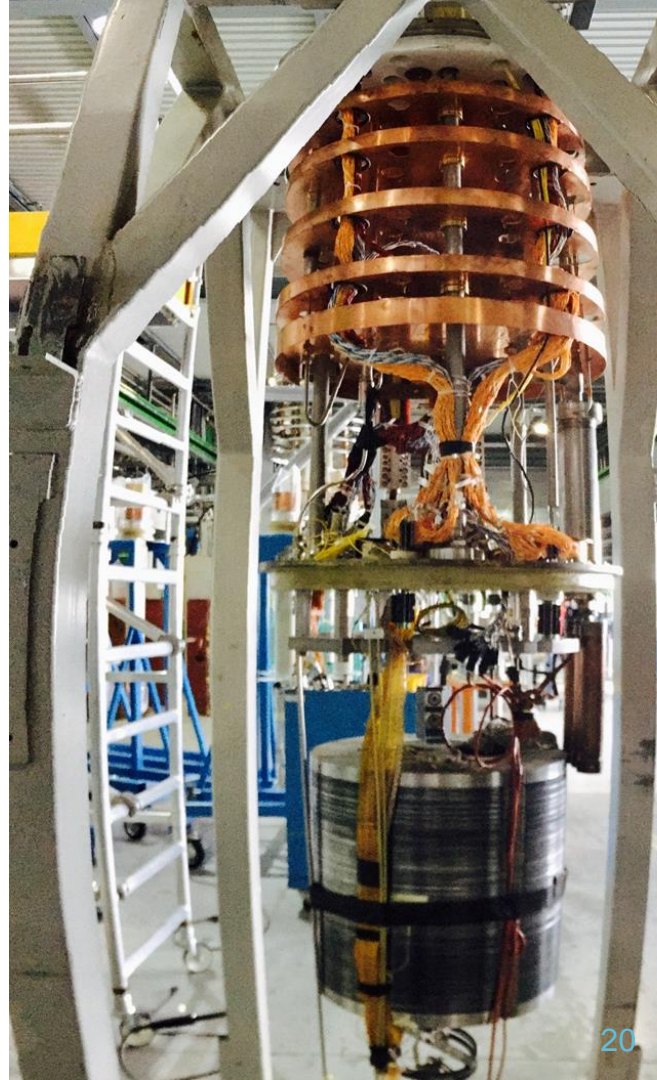
First model Magnet Test

First test of 0.5 m model, single aperture Al-Bronze former

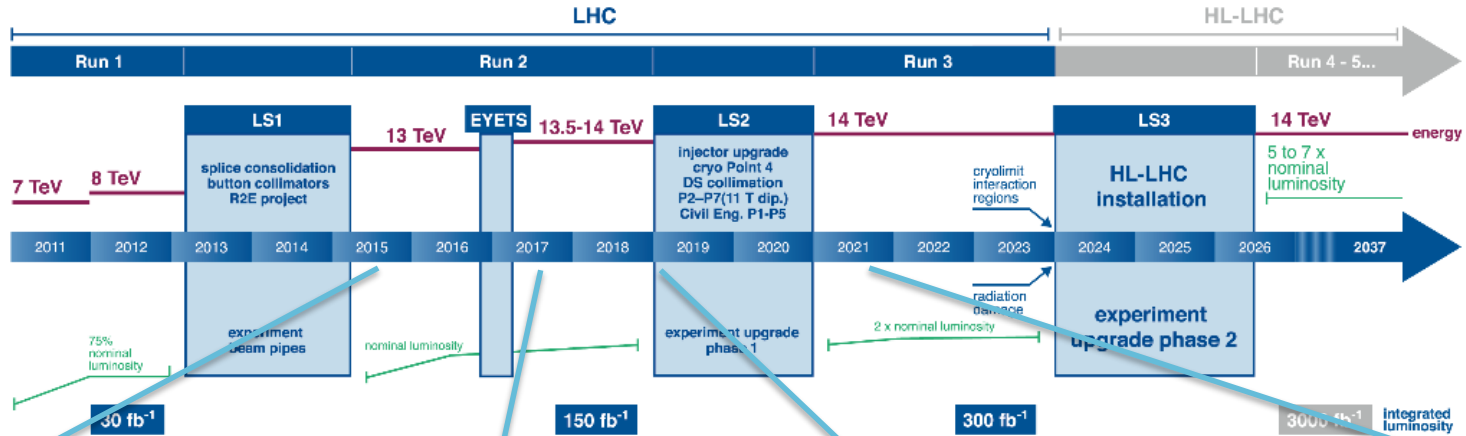
- Tested to 1.9K
- RRR of wire measured at 253, high!
- No quench up to 422 A nominal
- One quench at 438 A (short model hot spot 63K, voltage to Ground 320V, for 2.2m magnet this would then be 193 K and 330 V)
- Then No quench up to 460 A ultimate design value
- Thermal cycle no quench.
- Nominal ramp rate 4.2 A/s.
- Max tested ramp rate with no quench 40 A/s

Joint resistances: Average 5.7 nOhm's
120 +/- 20 n Ω over one aperture.

Energy distribution during quench : with 0.7 Ω dump:
Coil 13%, Dump 59%, aluminium support tube and formers 28%

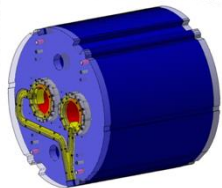


LHC / HL-LHC Plan

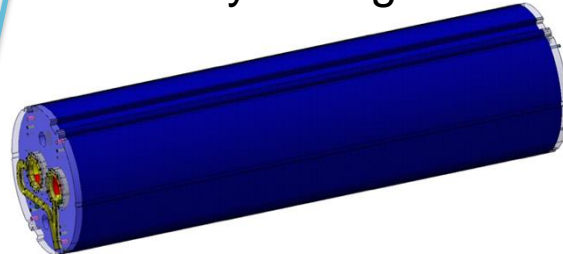


LHC/ HL-LHC Plan (last update 22.02.2016)

0.5m model tested
Summer 2017



Full size prototype
Assembly during 2018



18 - 20 off twin aperture
magnets production in industry
delivery ~ 2020



Closing Comments and Conclusions

- CERN is developing a CCT 3 Tesla orbit corrector for use Hi-Lumi LHC
- This old idea from the 1960's has many positive points:
 - Simple design / Potentially low-cost, No significant tooling.
 - Field errors appear to be insensitive to small mechanical errors.
 - Radiation hard design, "Full metal jacket around impregnated conductor".
- Short 0.5 metre Proof of concept model test successfully completed .
- 2.2 m prototype test planned for winter 2017 / 2018 Full Field quality will be measured in this test .
- Series production ~ 18 to 20 – twin aperture magnets Should start in 2019

***Thank you for your
attention***

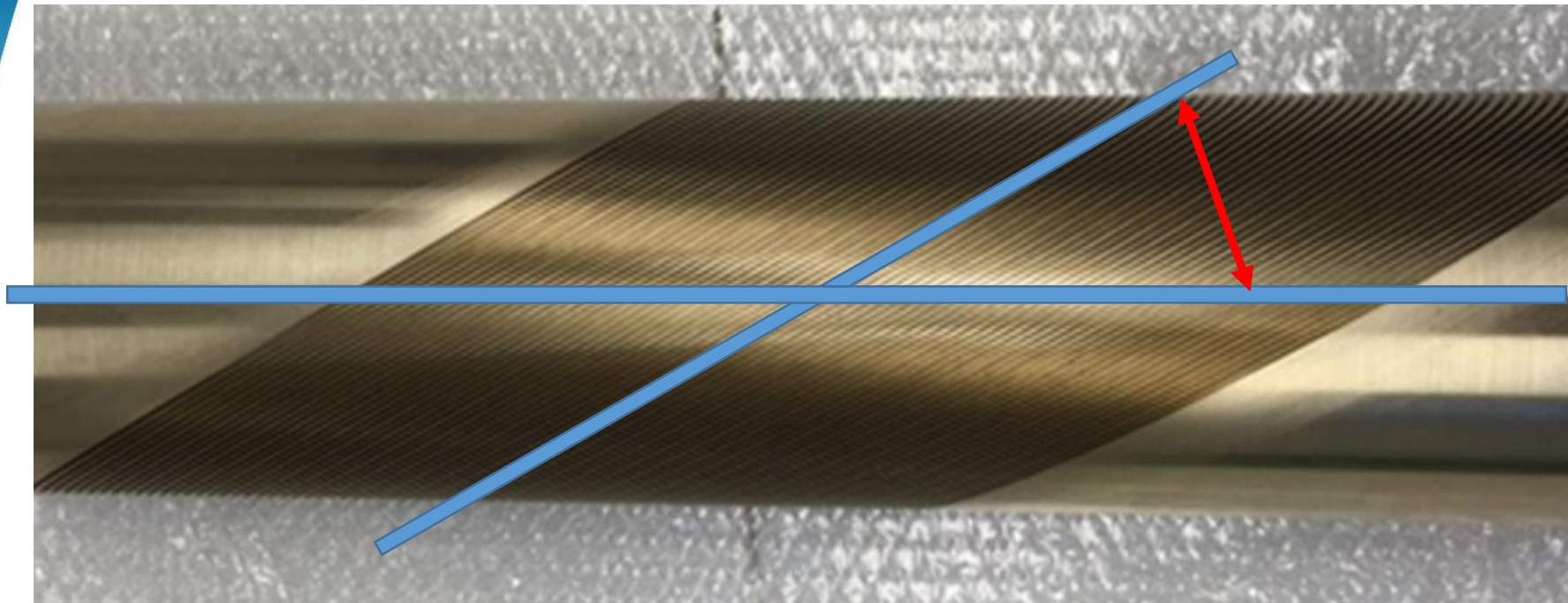




Extras

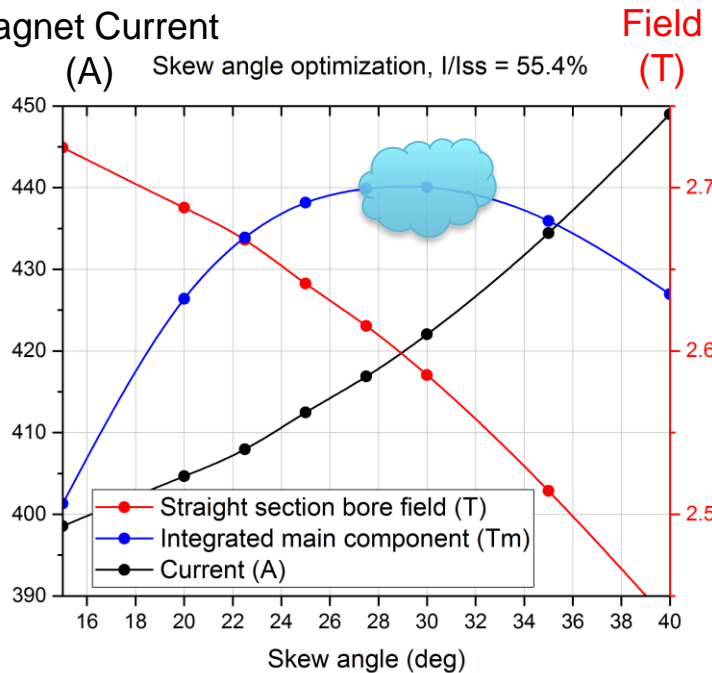




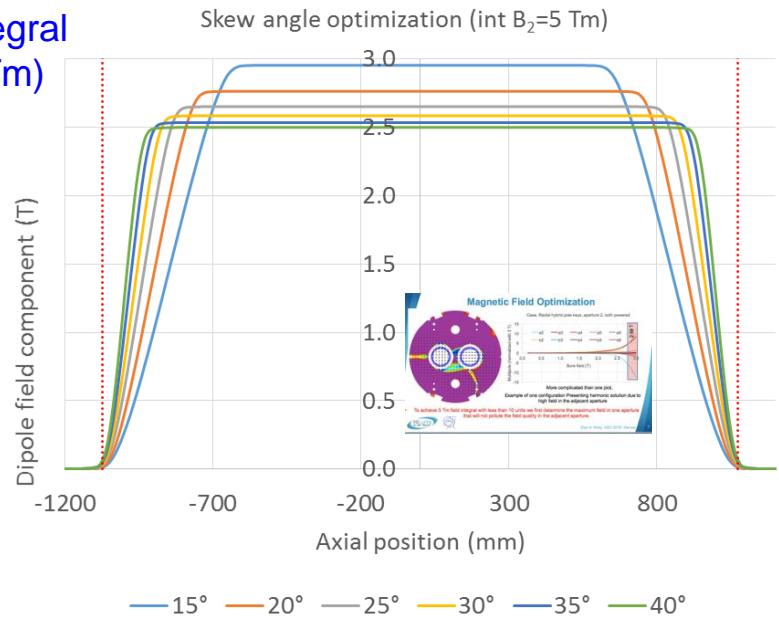


Definition of CCT skew angle

Magnet Current



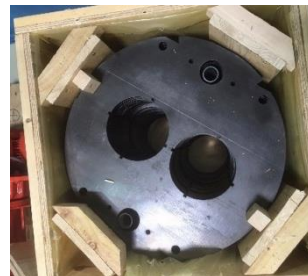
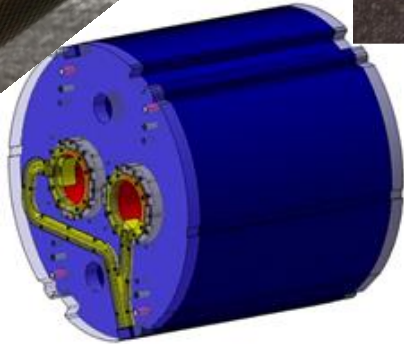
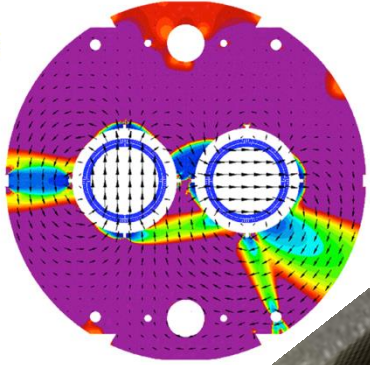
Field Integral (Tm)



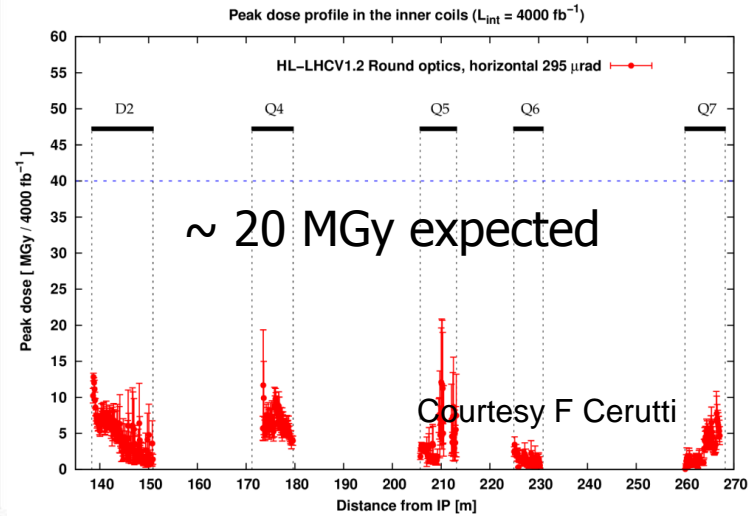
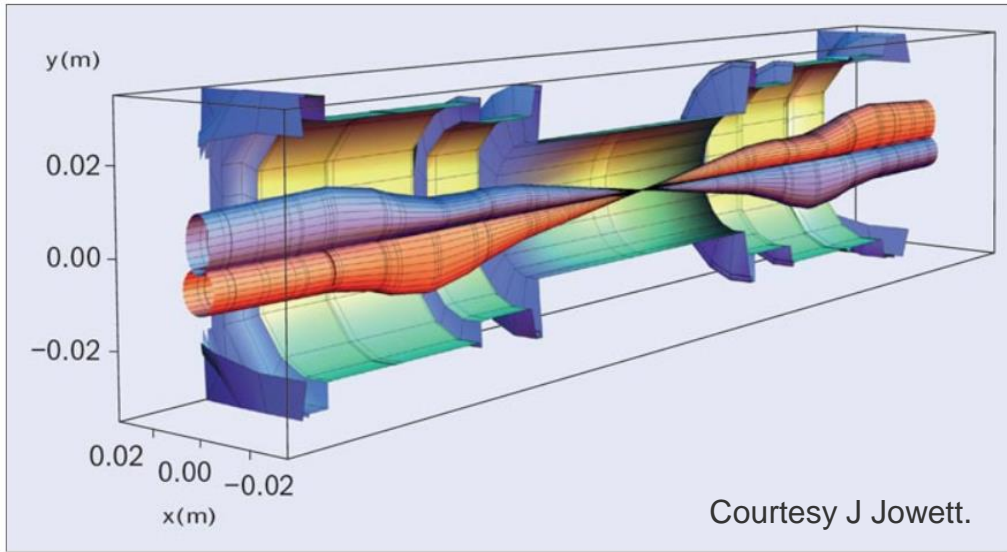
CCT skew angle optimisation

Due to the cross talk the max aperture field is set to $\sim 2.7 \text{ T}$
 For a fixe d 5 Tm integral & magnet length $\sim 2\text{m}$ the optimum skew angle is 30 deg.
 Lower skew angles give more field less conductor but have longer ends!

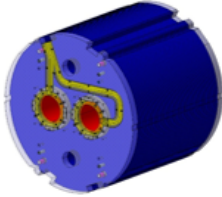
Components for the 0.5m model



Orbit Corrector Function & Environment



The two counter rotating HL-LHC beams are brought to full energy, then the sets of orbit correctors quickly (within 100 sec) maneuver the two beams into collision.

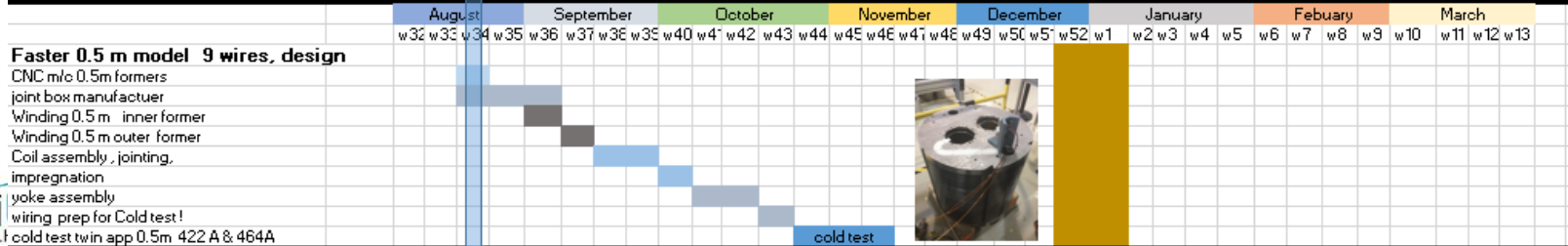
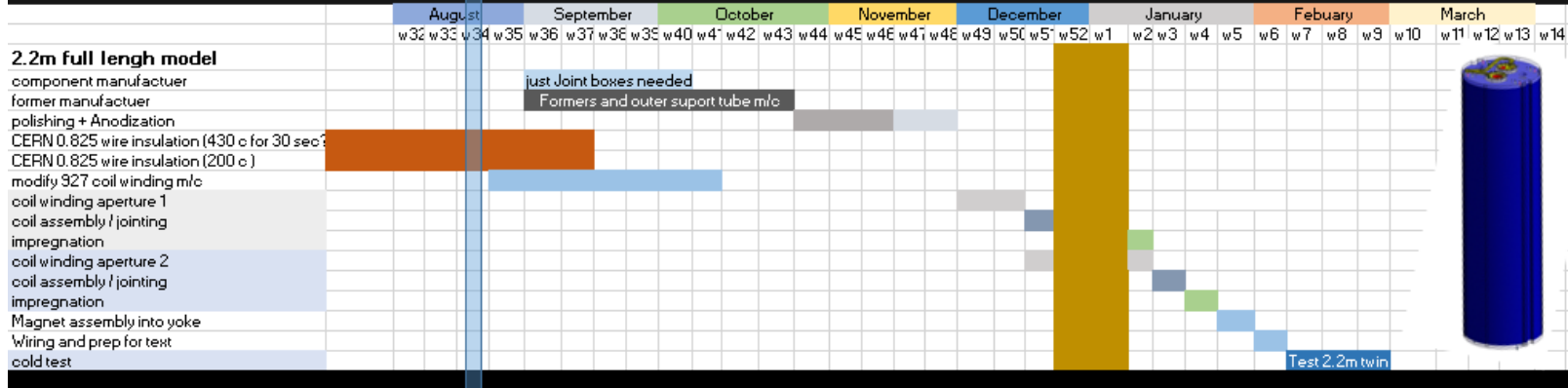
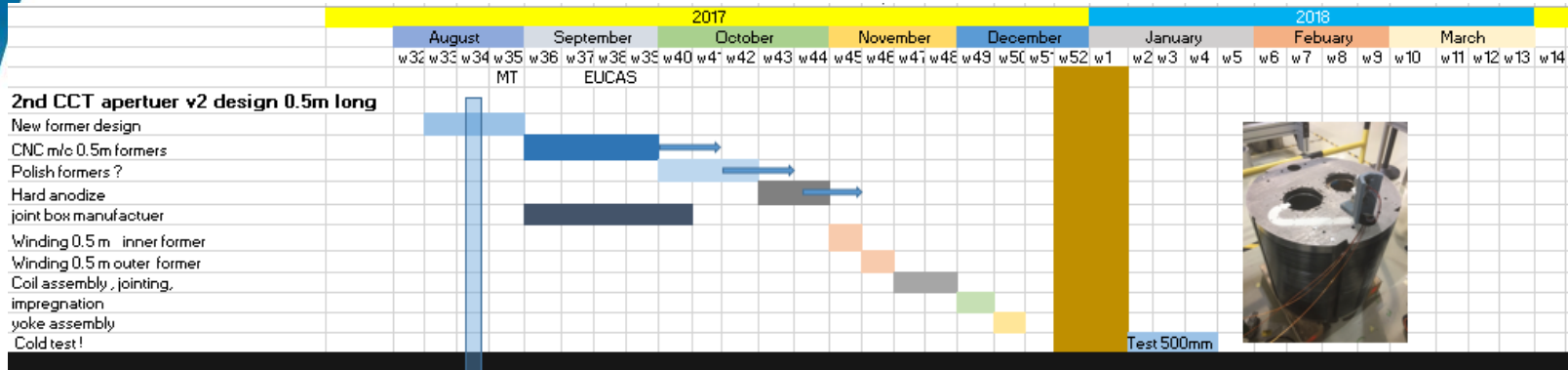


Manufacturing follow-up F	
0.5	
ITEM Number	ST0772446
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Nomenclature	LHCMCBYY0035
Date	03.05.2016
Q4 CORRECTOR ASSEMBLY v3	CDD folder
Extracted by	L. Gentini

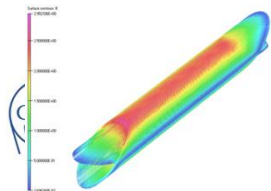
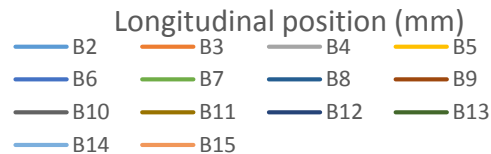
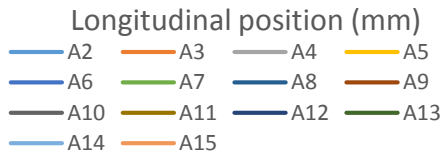
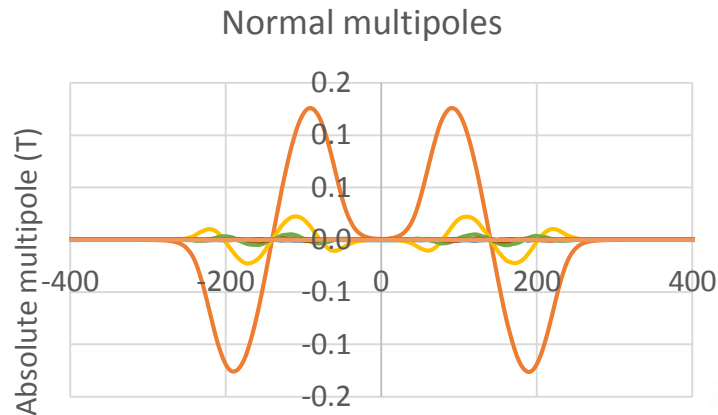
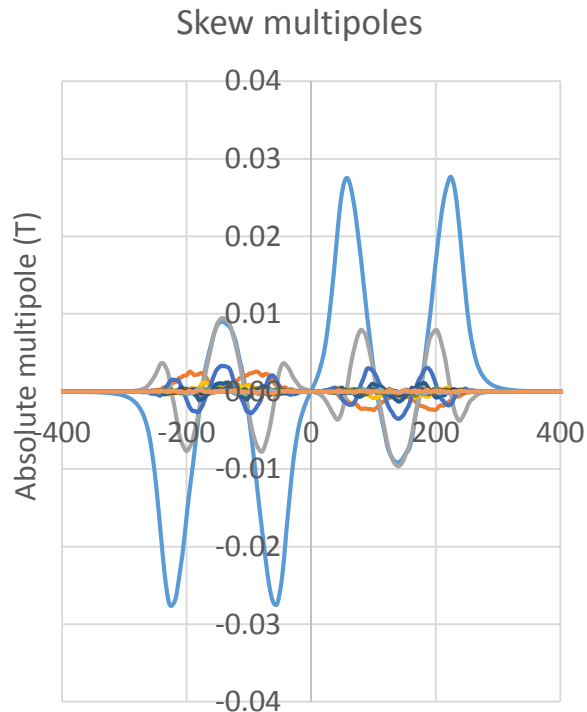
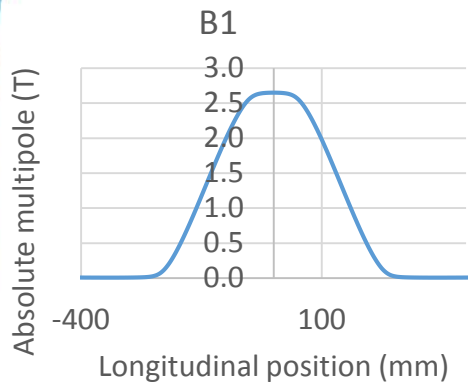
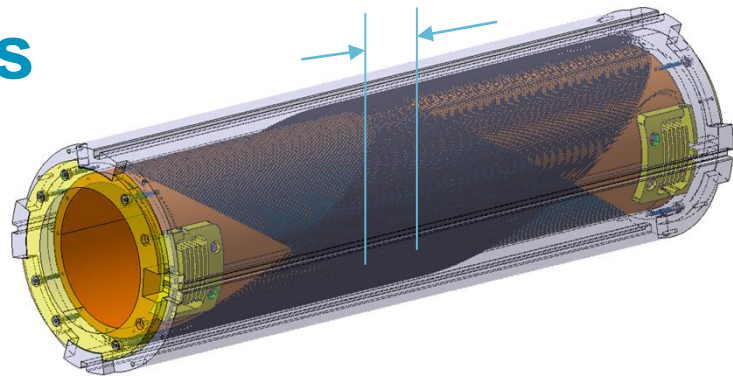
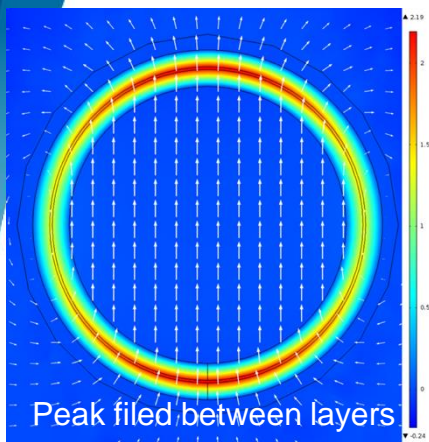
Design responsible	Drawing status	Manufacturing / order res...
L. Gentini	(blank)	(blank)
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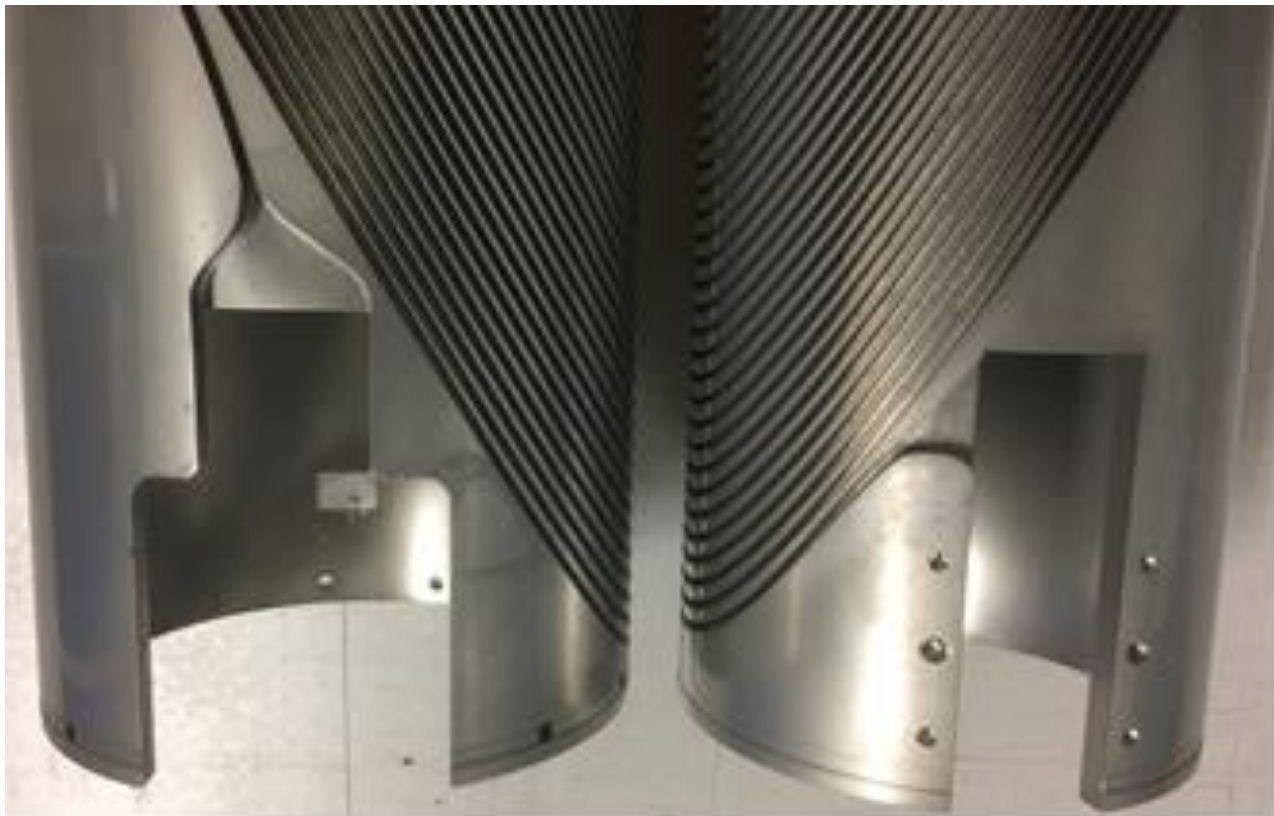
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								Design responsible	Drawn status	Design No	Manufacturing order responsible	M		
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LHCMCBYY	ST0739488	FIX INSULATING END PLATE	2	CERN Design	Epoxy GF EP GC 308 (G-II)					L. Gentini				
LHCMCBYY	ST0747071	WIRE EXIT BOX	2	CERN Design	Epoxy GF EP GC 308 (G-II)					L. Gentini				
LHCMCBYY	ST0737413	500 mm KEY	4	CERN Design	EN 14307 (St. Steel 304L)					L. Gentini				
LHCMCBYY	ST0763312	Q4 CORRECTOR YOKE V2	84	CERN Design	ARMCO® (Fe 99,99%)					L. Gentini				
LHCMCBYY	ST0765324	Q4 FIX EXTREMITY FLANGE V2	1	CERN Design	EN 14306 (St. Steel 304L)					L. Gentini				
LHCMCBYY	ST0772764	Q4 FREE EXTREMITY FLANGE V2	1	CERN Design	EN 14306 (St. Steel 304L)					L. Gentini				
LHCMCBYY	ST0772447	MAGNET COIL ASSEMBLY v3	2	CERN Design						L. Gentini				
LHCMCBYY	ST0772448	INNER COIL v3	2	CERN Design	Copper					L. Gentini				
LHCMCBYY	ST0772487	OUTER COIL v3	2	CERN Design	Copper					L. Gentini				
LHCMCBYY	ST0776711	INSULATING FREE END PLATE	2	CERN Design	Epoxy GF EP GC 308 (G-II)					L. Gentini				
LHCMCBYY	ST0776540	CONNECTION BOX 2	4	CERN Design	Epoxy GF EP GC 308 (G-II)					L. Gentini				
LHCMCBYY	ST0776578	YOKE ROD V2	4	CERN Design	EN 14307 (St. Steel 304L)					L. Gentini				
LHCMCBYY	ST0772446	V3 Q4 CORRECTOR ASSEMBLY								L. Gentini				
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LHCMCBYY	ST0769172	INSULATING WIRE LINE 2 V2	1	CERN Design	Epoxy GF EP GC 308 (G-II)					L. Gentini				
LHCMCBYY	ST0769174	INSULATING WIRE COVER 1 V2	1	CERN Design	Epoxy GF EP GC 308 (G-II)					L. Gentini				
LHCMCBYY	ST0779927	HYBRID YOKING KEY - OUTER PART	4	CERN Design	ARMCO® (Fe 99,99%)					L. Gentini				
LHCMCBYY	ST0779653	HYBRID YOKING KEY - INNER PART	4	CERN Design	EN 14306 (St. Steel 304L)					L. Gentini				
LHCMCBYY	ST0779921	HYBRID YOKING KEY ASSEMBLY	4	CERN Design						L. Gentini				
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	ISO 4762_M4x12-A4	HEX SKT HD CAP SCREW_M4X12	16	Normalized	St. Steel A4	47.62.71.155.7								
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Low number of drawings / components ~ 20 leading to low cost of manufacture!

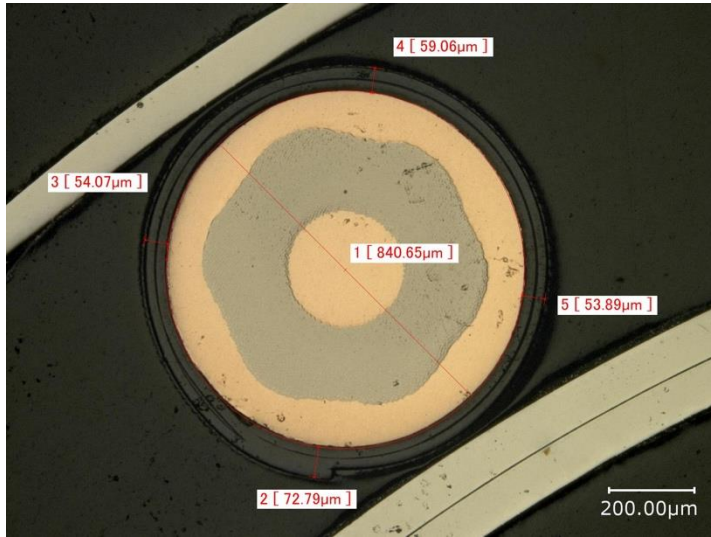


CCT Field profiles



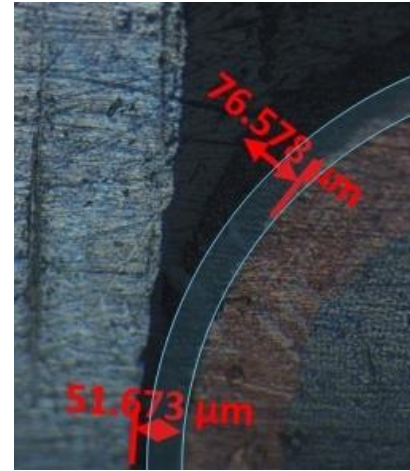


Base line insulation



Polyimide 48 % overlapped wrapped
4mm wide tape,

Insulation tested at > 9 kV (very good)



Glass sleeve compressed thickness ~ 0.052 mm

Polyimide tape provides electrical insulation
Glass sleeve impregnated with radiation hard resin provides mechanical support.