

# Optics Measurement Techniques for Transfer Line & Beam Instrumentation

*CAS for Beam Injection, Extraction and Transfer Line  
Erice, 16<sup>th</sup> and 17<sup>th</sup> of March 2017*

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## **Acknowledgement:**

- To the organizers for the invitation to this presentation
- To P. Kowina, R. Singh (GSI) and M. Schuh (KIT) for very valuable discussion
- To numerous further colleagues for versatile & enlightening discussions and providing material

## Diagnostics is the 'sensory organs' for the beam.

### Different demands lead to different installations:

- Quick, non-destructive measurements leading to a single number or simple plots  
Used as a check for online information. Reliable technologies have to be used  
*Example:* Current measurement by transformers
- Complex instruments for severe malfunctions, accelerator commissioning & development  
The instrumentation might be destructive and complex  
*Example:* Emittance determination

### General usage of beam instrumentation:

- Monitoring of beam parameters for operation, beam alignment & accelerator development
- Instruments for automatic, active beam control  
*Example: Synchrotron:* Closed orbit feedback using position measurement by BPMs  
*Slow extraction:* Control of extraction strength to stabilize beam  $I_{beam}(t)$  at target

### Non-destructive ('non-intercepting') methods are preferred:

- The beam is not influenced  $\Rightarrow$  the **same** beam can be measured at several locations
- The instrument is not destroyed

# Outline of the Lecture



## The ordering of the subjects is oriented by the beam quantities:

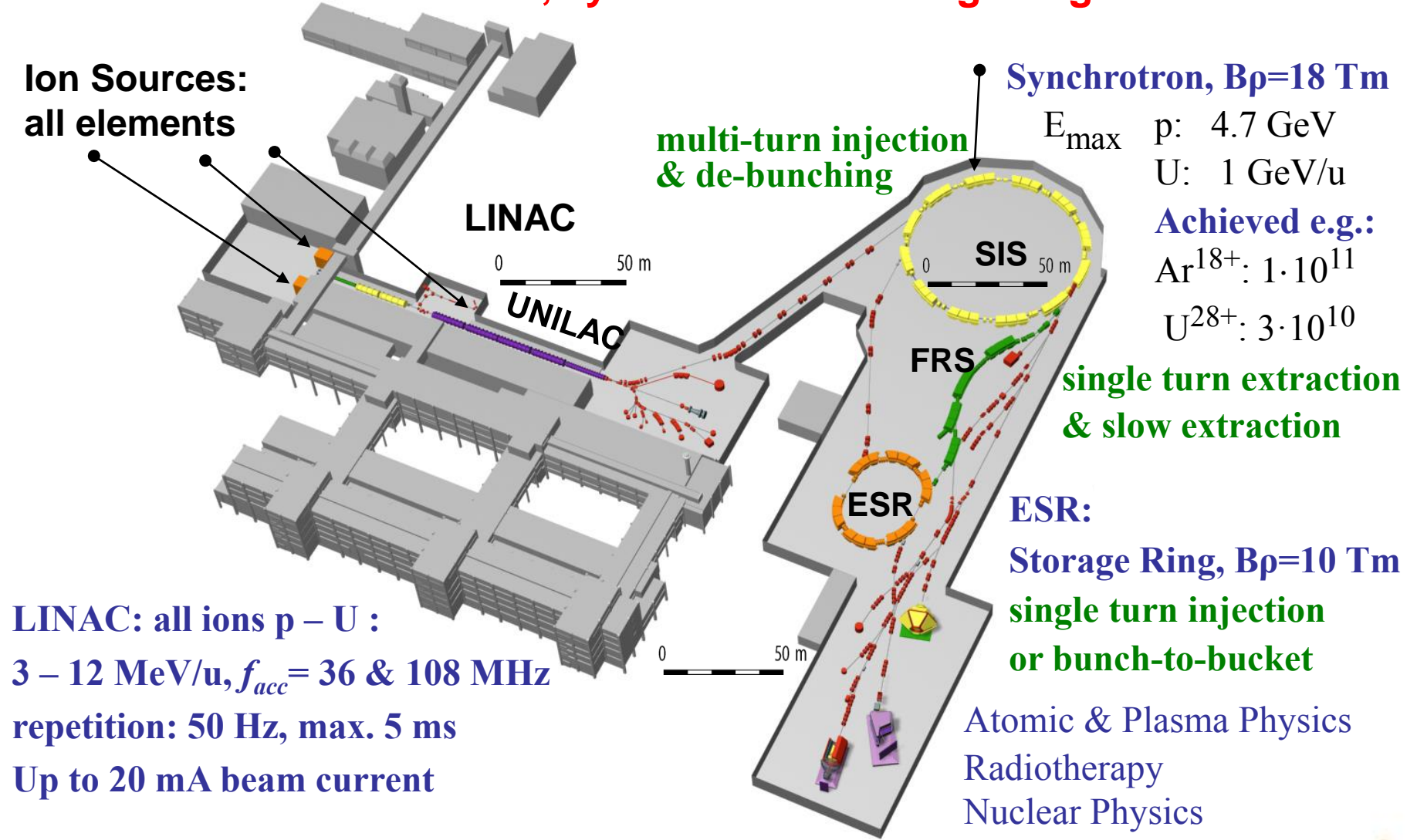
- **Current measurement:** Transformers, Faraday cups, particle detectors
  - **Beam loss detection:** Secondary particle detection for optimization and protection
  - **Profile measurement:** Various methods depending on the beam properties
  - **Transverse emittance measure:** Destructive devices, linear transformations
  - **Pick-ups for bunched beams:** Principle of rf pick-ups & relevant beam measurements
  - **Measurement of longitudinal parameters:** time structure of bunches, beam energy spread energies, longitudinal emittance
- } 1<sup>st</sup> lecture  
} 2<sup>nd</sup> lecture  
} 3<sup>rd</sup> lecture

## Some instruments must be different for:

- Transfer lines with single pass ↔ synchrotrons with multi-pass
- Electrons are (nearly) always relativistic ↔ protons are at the beginning non-relativistic

**Remark:** Most example for GSI **only** because the author is familiar with this facility!

## The GSI linear accelerator, synchrotron & storage ring for ions



**LINAC: all ions p – U :**  
 $3 - 12\text{ MeV/u}$ ,  $f_{\text{acc}} = 36 \text{ \& } 108\text{ MHz}$   
 repetition: 50 Hz, max. 5 ms  
 Up to 20 mA beam current

The beam current and its time structure the basic quantity of the beam.

- It is the first check of the accelerator functionality
- It has to be determined in an absolute manner
- Important for transmission measurement and to prevent for beam losses.

**Different devices are used:**

- **Transformers:** Measurement of the beam's **magnetic field**

They are non-destructive. No dependence on beam energy

They have lower detection threshold.

- **Faraday cups:** Measurement of the beam's **electrical charges**

- **Particle detectors:** Measurement of the particle's **energy loss** in matter

**Remark:** Typical beam instruments are mounted outside of rf cavities to prevent for electro-magnetic interference from the high field; only inside cyclotrons some instruments.

# Magnetic field of the beam and the ideal Transformer

➤ Beam current of  $N_{part}$  charges with velocity  $\beta$

$$I_{beam} = qe \cdot \frac{N_{part}}{t} = qe \cdot \beta c \cdot \frac{N_{part}}{l}$$

➤ cylindrical symmetry

→ only azimuthal component

$$\vec{B} = \mu_0 \frac{I_{beam}}{2\pi r} \cdot \vec{e}_\varphi$$

Example:  $I = 1\mu\text{A}$ ,  $r = 10\text{cm} \Rightarrow B_{beam} = 2\text{pT}$ , earth  $B_{earth} = 50\mu\text{T}$

**Idea: Beam as primary winding and sense by sec. winding.**

⇒ Loaded current transformer

$$I_1/I_2 = N_2/N_1 \Rightarrow I_{sec} = 1/N \cdot I_{beam}$$

➤ Inductance of a torus of  $\mu_r$

$$L = \frac{\mu_0 \mu_r}{2\pi} \cdot l N^2 \cdot \ln \frac{r_{out}}{r_{in}}$$

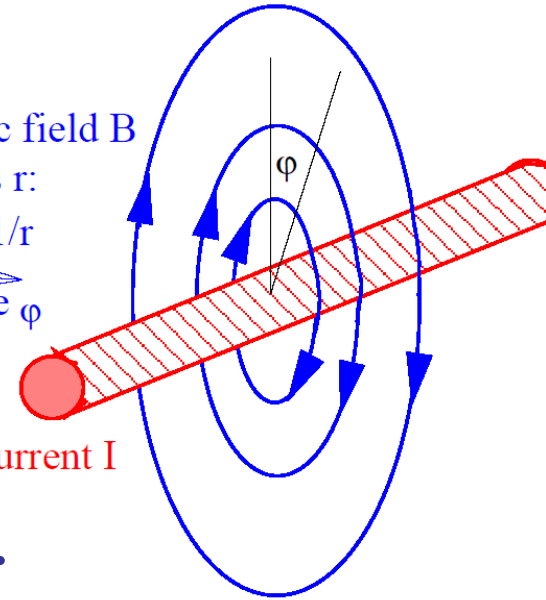
➤ Goal of torus: Large inductance  $L$  and guiding of field lines.

Definition:  $U = L \cdot dI/dt$

magnetic field B at radius r:

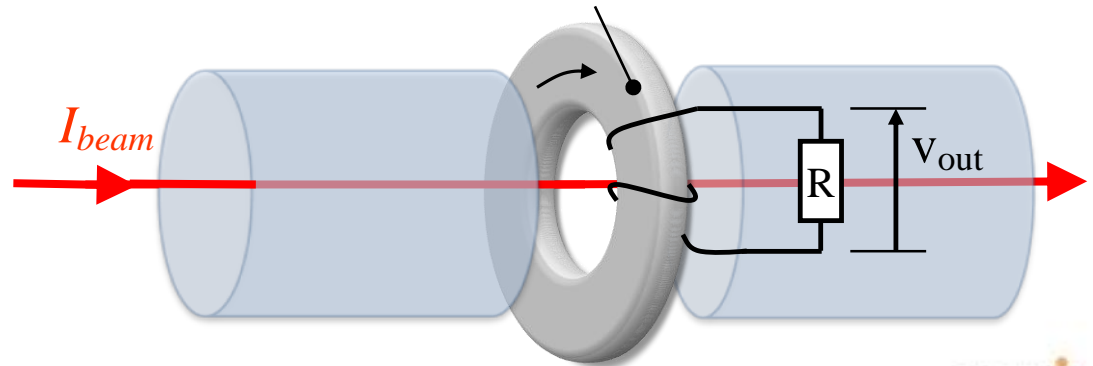
$$B \sim 1/r$$

$$\vec{B} \parallel \vec{e}_\varphi$$



beam current I

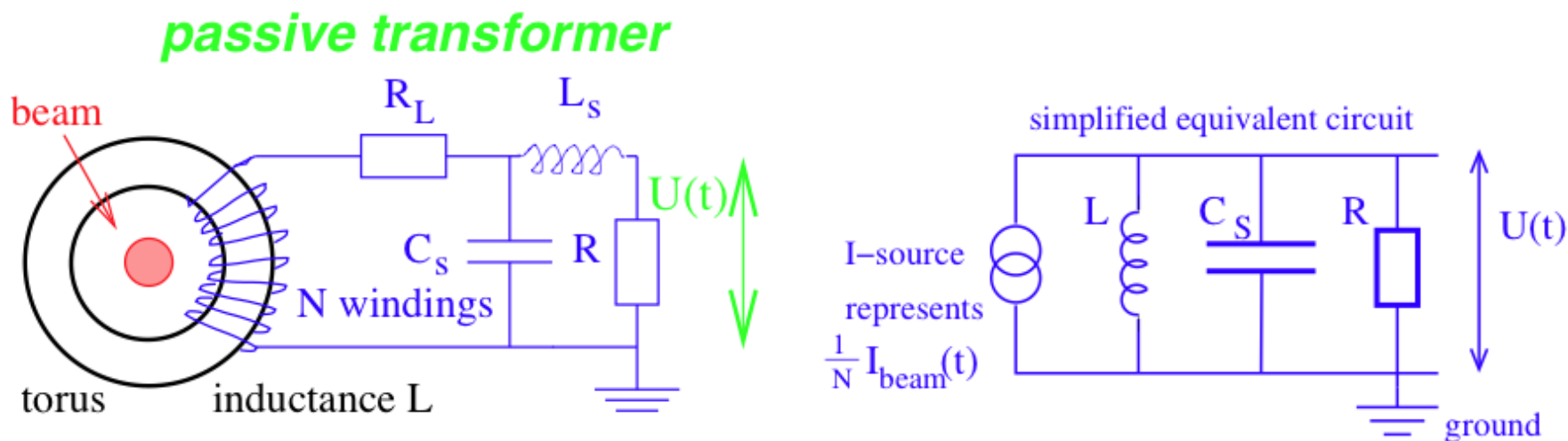
Torus to guide the magnetic field



# Passive Transformer (or Fast Current Transformer FCT)



Simplified electrical circuit of a passively loaded transformer:



A voltage is measured:  $U = R \cdot I_{sec} = R / N \cdot I_{beam} \equiv S \cdot I_{beam}$

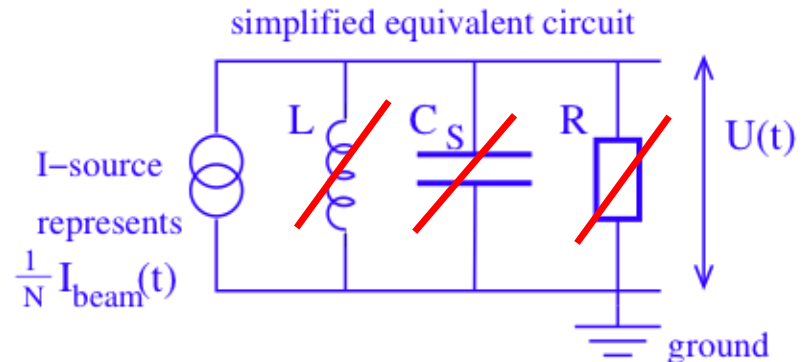
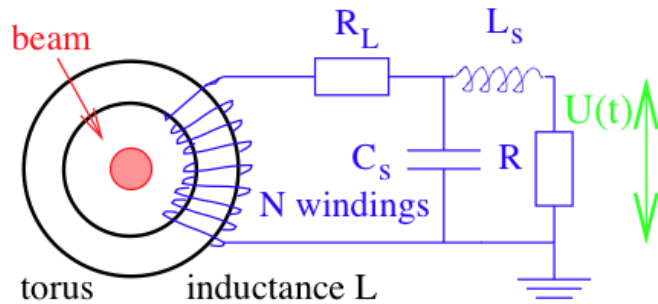
with **S sensitivity** [V/A], equivalent to transfer function or transfer impedance **Z**

Equivalent circuit for analysis of sensitivity and bandwidth

(disregarding the loss resistivity  $R_L$ )

# Bandwidth of a Passive Transformer

## Analysis of a simplified electrical circuit of a passively loaded transformer: *passive transformer*



For this parallel shunt:

$$\frac{1}{Z} = \frac{1}{i\omega L} + \frac{1}{R} + i\omega C_S \Leftrightarrow Z = \frac{i\omega L}{1 + i\omega L/R - \omega L/R \cdot \omega R C_S}$$

➤ **Low frequency**  $\omega \ll R/L$  :  $Z \rightarrow i\omega L$

i.e. no dc-transformation

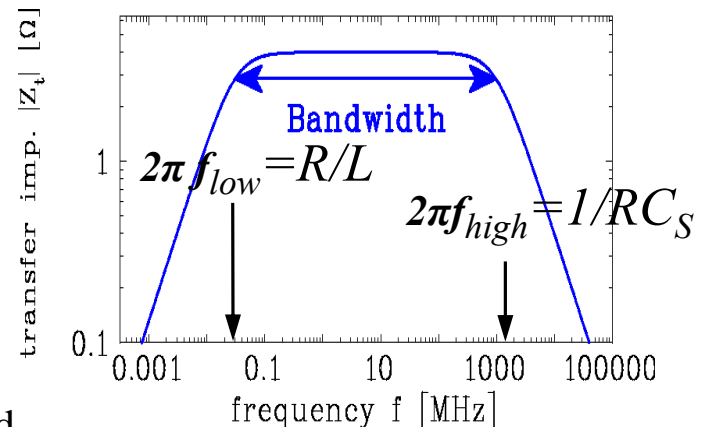
➤ **High frequency**  $\omega \gg 1/RC_S$  :  $Z \rightarrow 1/i\omega C_S$

i.e. current flow through  $C_S$

➤ **Working region**  $R/L < \omega < 1/RC_S$  :  $Z \simeq R$

i.e. voltage drop at R and sensitivity  $S=R/N$ .

No oscillations due to over-damping by low  $R = 50 \Omega$  to ground.





# Response of the Passive Transformer: Rise and Droop Time



## Time domain description:

Droop time:  $\tau_{droop} = 1/(2\pi f_{low}) = L/R$

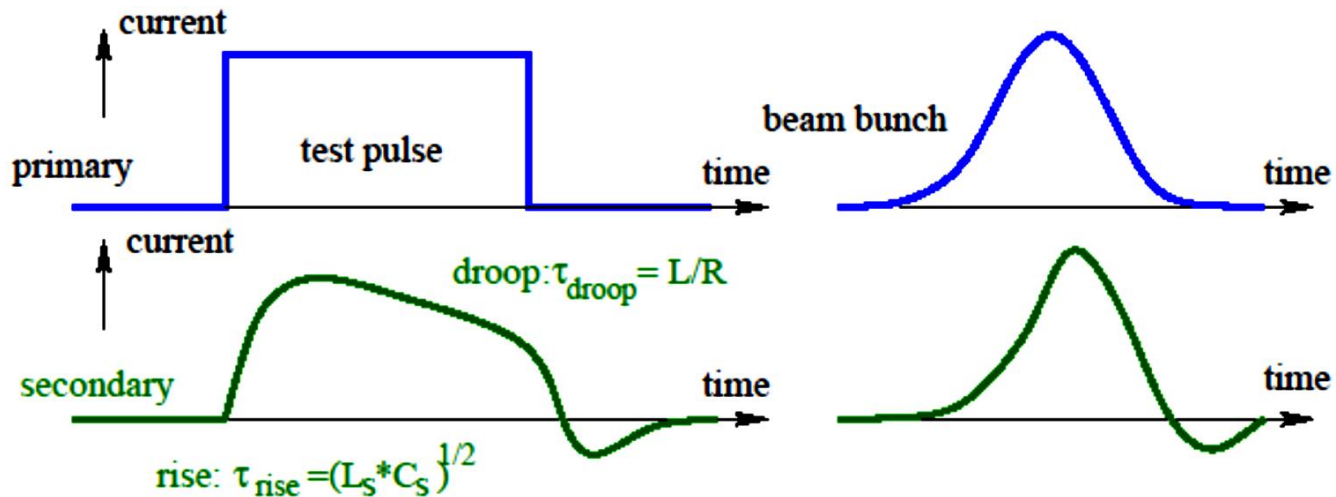
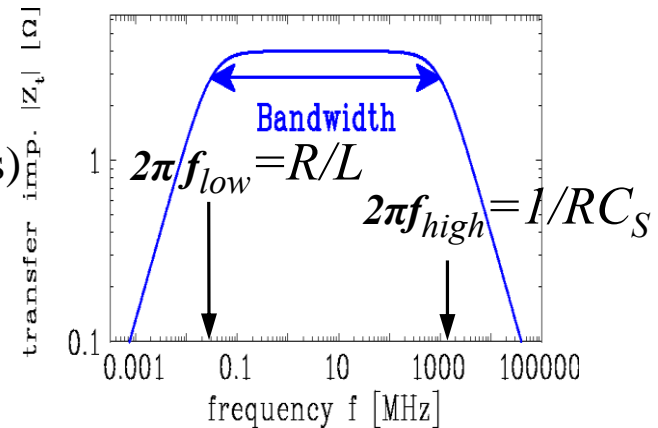
Rise time:  $\tau_{rise} = 1/(2\pi f_{high}) = 1/RC_S$  (ideal without cables)

Rise time:  $\tau_{rise} = 1/(2\pi f_{high}) = \sqrt{L_S C_S}$  (with cables)

$R_L$ : loss resistivity,  $R$ : for measuring.

For the working region the voltage output is

$$U(t) = \frac{R}{N} \cdot e^{-t/\tau_{droop}} \cdot I_{beam}$$



## Example for passive Transformer

For bunch beams e.g. transfer between synchrotrons  
typical bandwidth of  $2 \text{ kHz} < f < 1 \text{ GHz}$   
 $\Leftrightarrow 1 \text{ ns} < t \approx 1/f < 200 \text{ } \mu\text{s}$  is well suited

*Example GSI type:*

Inner / outer radius	70 / 90 mm
Torus thickness	16 mm
Torus material	$(\text{CoFe})_{70\%}(\text{MoSiB})_{30\%}$
Permeability	$\mu_r \approx 10^5$ for $f < 100\text{kHz}$ $\mu_r \propto 1/f$ above
Windings	10
Sensitivity	4 V/A for $R = 50 \text{ } \Omega$
Droop time $\tau_{\text{droop}} = L/R$	0.2 ms
Rise time $\tau_{\text{rise}} = \sqrt{L_S C_S}$	1 ns
Bandwidth	2 kHz ... 300 MHz

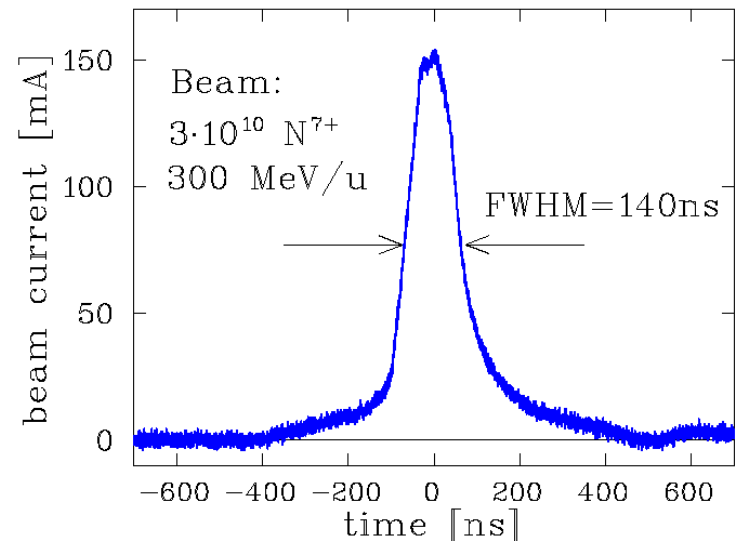
Numerous application e.g.:

- Transmission optimization
- Bunch shape measurement
- Input for synchronization of ‘beam phase’

From  
Company Bergoz



Fast extraction from GSI synchrotron:



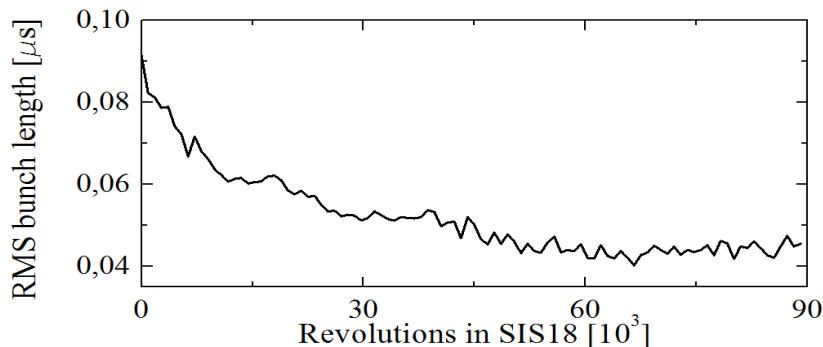
# Example for passive Transformer

For bunch beams e.g. during accel. in a synchrotron  
 typical bandwidth of  $2 \text{ kHz} < f < 1 \text{ GHz}$

$\Leftrightarrow 1 \text{ ns} < t \approx 1/f < 200 \text{ } \mu\text{s}$  is well suited

*Example GSI type:*

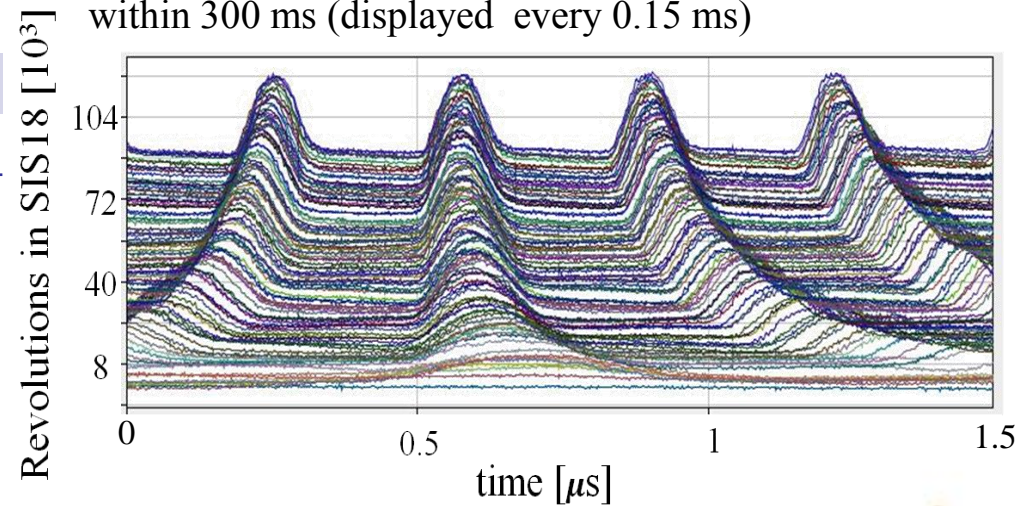
Inner / outer radius	70 / 90 mm
Torus thickness	16 mm
Torus material	(CoFe) <sub>70%</sub> (MoSiB) <sub>30%</sub>
Permeability	$\mu_r \approx 10^5$ for $f < 100\text{kHz}$ $\mu_r \propto 1/f$ above
Windings	10
Sensitivity	4 V/A for $R = 50 \text{ } \Omega$
Drop time $\tau_{\text{droop}} = L/R$	0.2 ms
Rise time $\tau_{\text{rise}} = \sqrt{L_S C_S}$	1 ns
Bandwidth	2 kHz ... 300 MHz



From  
 Company Bergoz



*Example: U<sup>73+</sup> from 11 MeV/u ( $\beta = 15 \%$ ) to 350 MeV/u within 300 ms (displayed every 0.15 ms)*

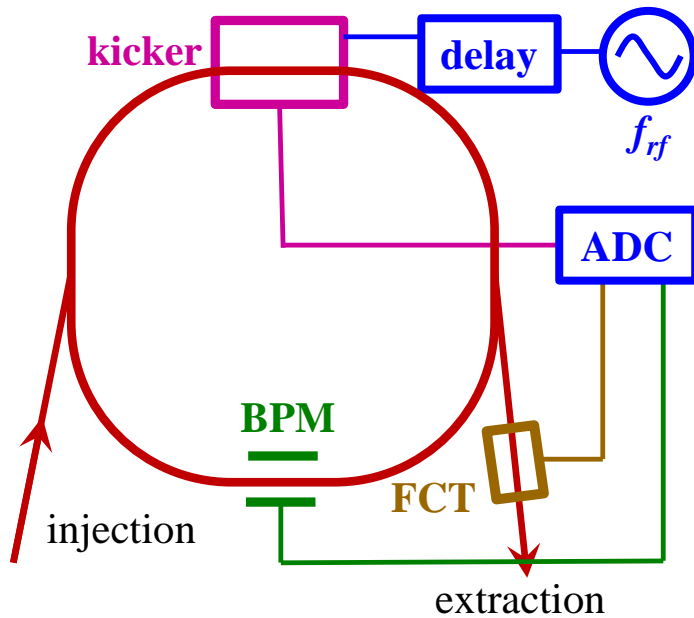


# Control of extraction Kicker for 'fast' Extraction

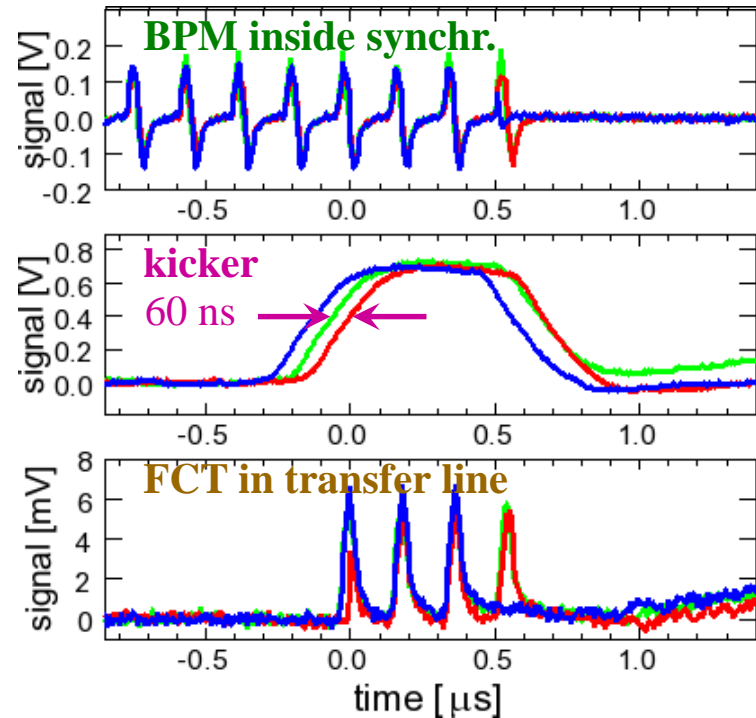


## Control of kicker timing by FCT measurement in transfer line

- **Correct timing:**
  - all bunches are extracted
- **Too late (here  $\Delta t = 60 \text{ ns} \approx 120^\circ @ f_{rf}$ ):**
  - first bunch is only partly extracted
- **Too early (here  $\Delta t = -60 \text{ ns} \approx -120^\circ @ f_{rf}$ ):**
  - last bunch is not extracted



Example:  $C^{6+}$  at 600 MeV/u,  $f_{rf}=5.46 \text{ MHz}$ ,  $h = 4$



# Longitudinal Bunch Diagnostics inside Synchrotron using FCT



- Acceleration and bunch 'gymnastics' are performed **inside** synchrotrons
- Bunch shaping for fast, single turn extraction

Measurement within synchrotron because bunch shape is constant during transport in most cases

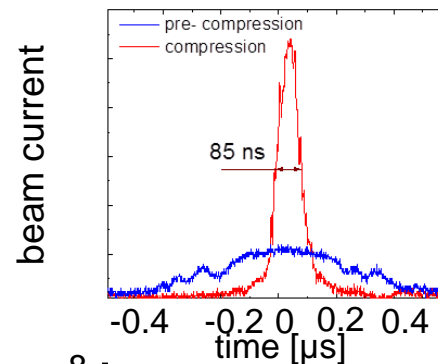
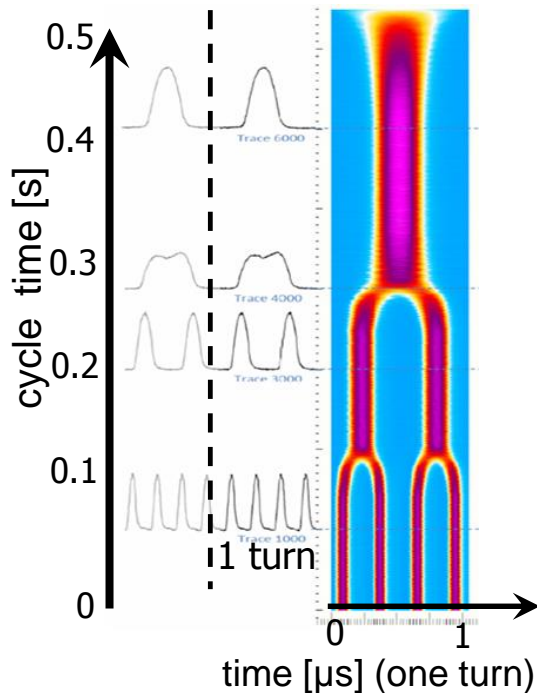
*Example:* Transfer line  $L=100\text{m}$ ,  $\beta=1$ ,  $\frac{\Delta p}{p} = 2 \cdot 10^{-3} \rightarrow \Delta t = \frac{\Delta p}{p} \cdot t_{drift} = \frac{\Delta p}{p} \cdot \frac{L}{\beta c} = 0.7 \text{ ns} \ll \sigma_{bunch}$

*Example:* Bunch merging at upper flattop using 2 cavities at GSI synchrotron

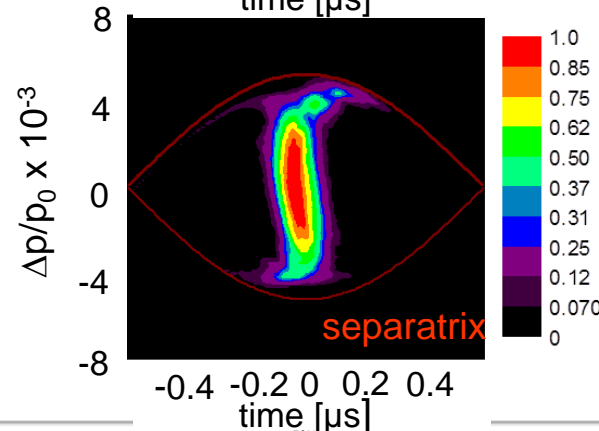
Beam:  $10^9 \text{ U}^{73+}$  at 600 MeV/u, FCT

*Example:* Bunch shape for 'bunch compression' prior to extr.

Beam:  $\text{U}^{73+}$  at 300 MeV/u at GSI synchrotron



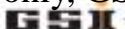
After acceleration  
before & after  
bunch compression



Tomographic  
reconstruction of  
longitudinal  
phase space  
depicted for  
min. bunch width

Courtesy H. Klingbeil, U. Hartel, et al. GSI

Courtesy O. Chroniy, GSI

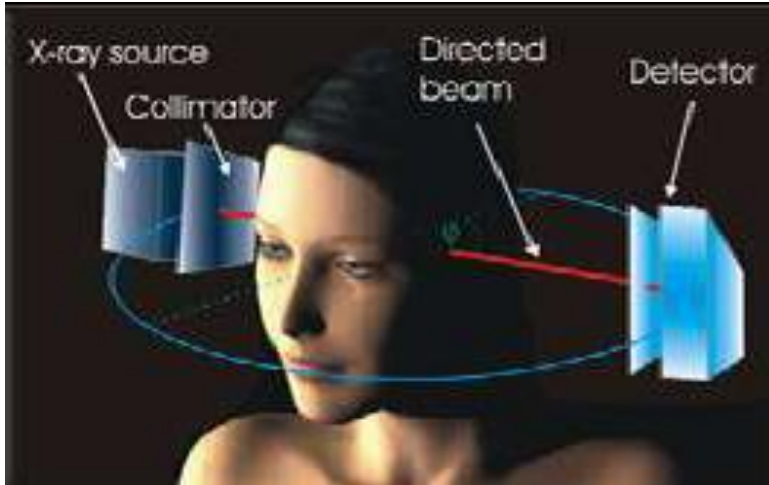


# Longitudinal Emittance using tomographic Reconstruction

Tomography is medical image method

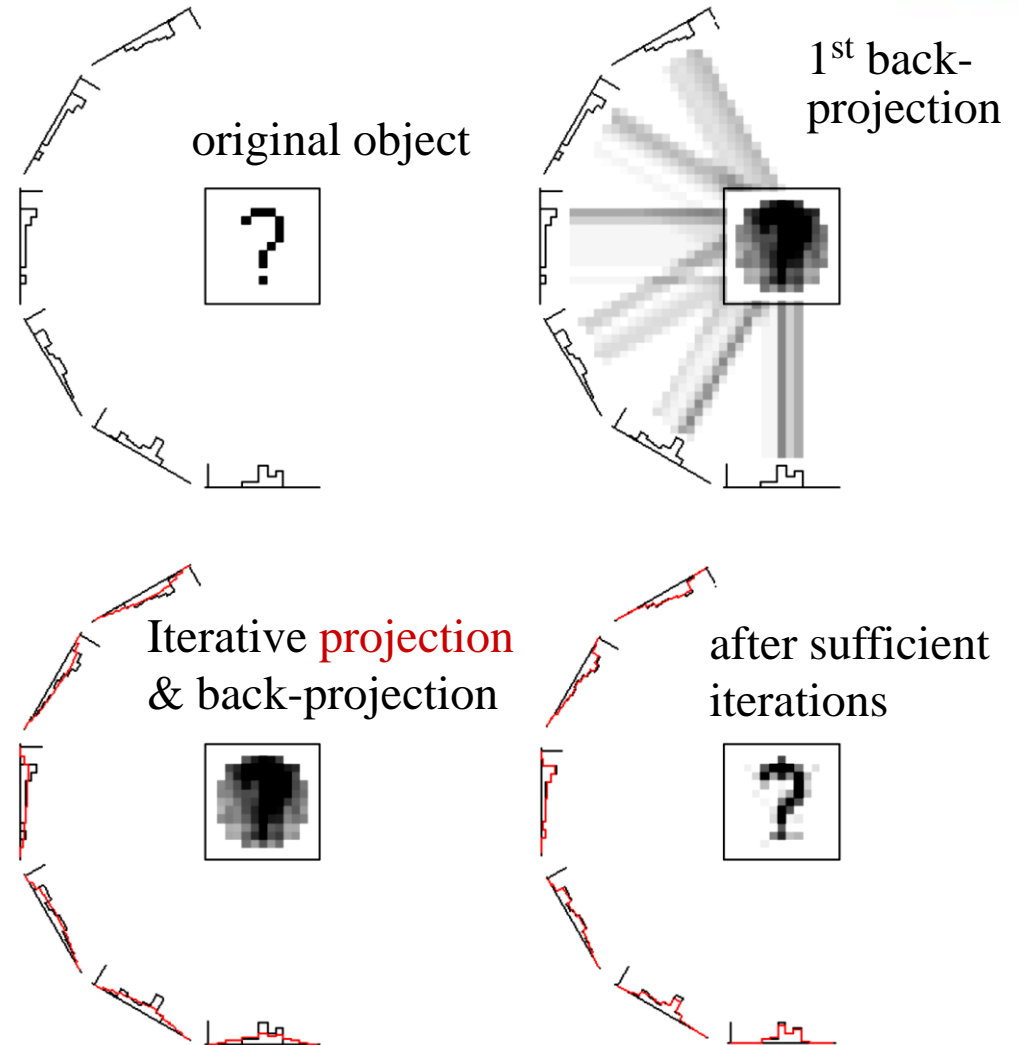
Tomography:

2-dim reconstruction of sufficient 1-dim projections



Algebraic back projection:

Iterative process by redistributing the 2-dim image and considering the differences to the previous iteration step.



# Longitudinal Emittance using tomographic Reconstruction

Tomography is medical image method

Tomography:

2-dim reconstruction of sufficient 1-dim projections

Application at accelerators:

Longitudinal emittance evolution in synchrotrons.

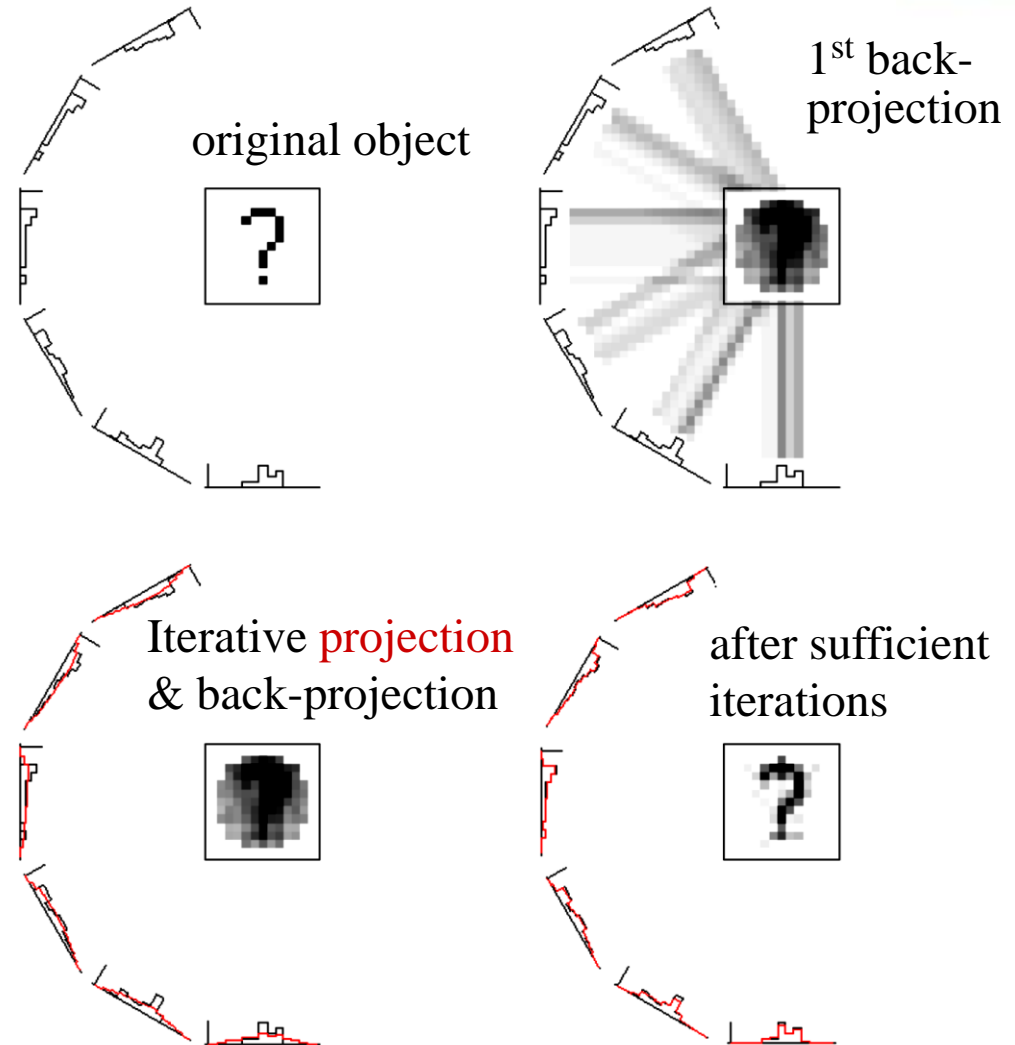
Bunch observation:

Each revolution, the bunch shape changes a bit due to synchrotron oscillations.

Fulfilled condition:  $f_{synch} \ll f_{ref}$ .

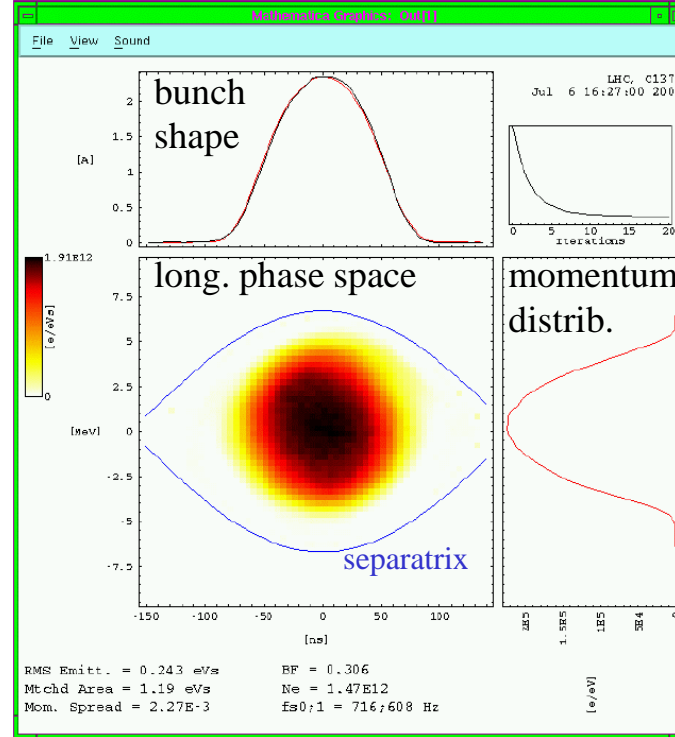
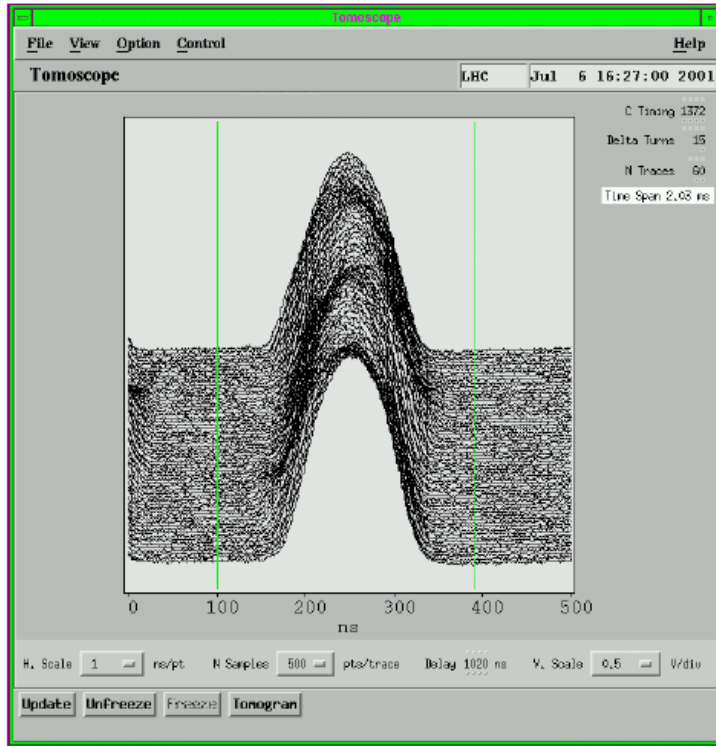
Algebraic back projection:

Iterative process by redistributing the 2-dim image and considering the differences to the previous iteration step.

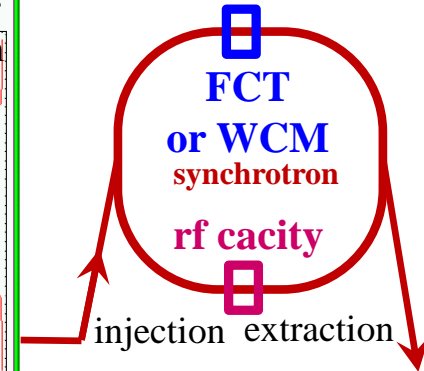


# Results of tomographic Reconstruction at a Synchrotron I

Bunches from 500 turns at the CERN PS and the phase space for the first time slice, measured with a wall current monitor:



Courtesy S. Hancock,  
J.L. Sanchez Alvarez:  
<http://cern.ch/tomography>



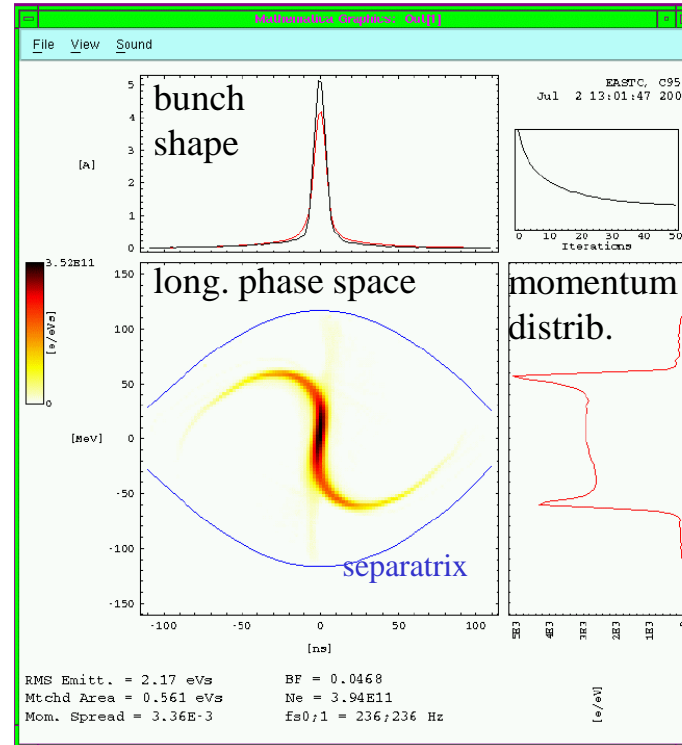
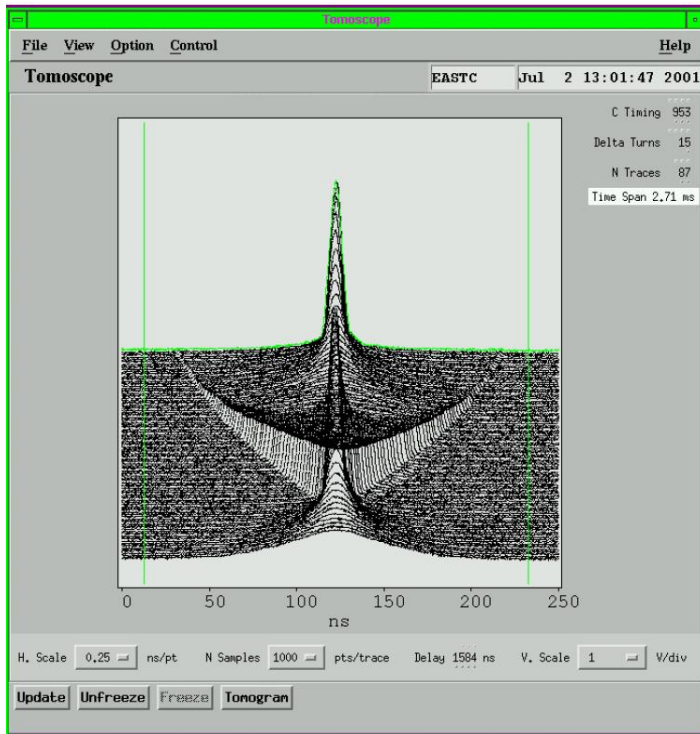
**Typical bucket filling. Important knowledge for bunch 'gymnastics'.**



# Results of tomographic Reconstruction at a Synchrotron II

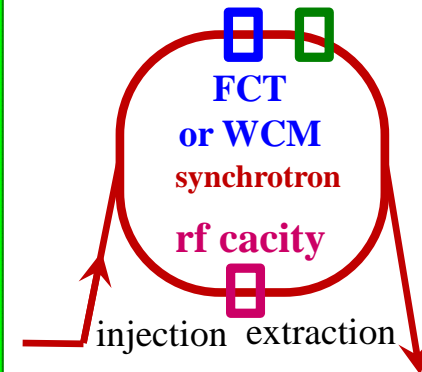


Bunches from 500 turns at the CERN PS and the phase space for the first time slice, measured with a wall current monitor:



Courtesy S. Hancock,  
J.L. Sanchez Alvarez:  
<http://cern.ch/tomography>

kicker control by beam



**Mismatched bunch shown oscillations and filamentation due to ‘bunch-rotation’.**

**Application:** Bunch rotation for short bunch extraction for experiments, alignment of kicker timing

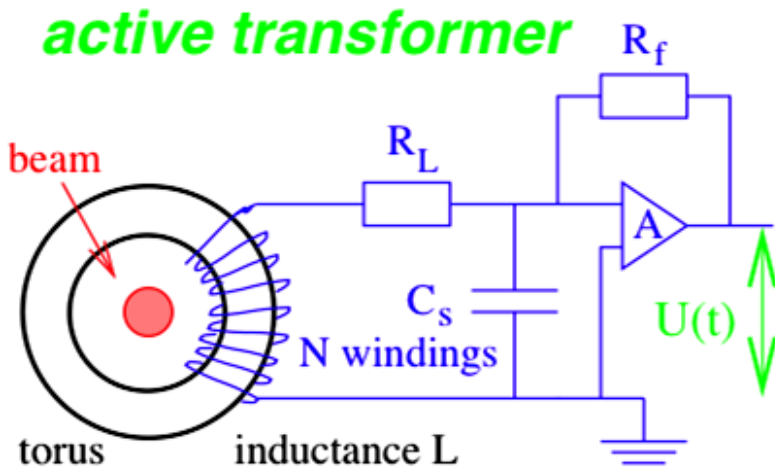
**Remark:** For typical proton synch with  $E > 1$  GeV.: negligible change of bunch shape in transfer line  
 $\Rightarrow$  measurement often done using synchrotron diagnostics.

# 'Active' Transformer with longer Droop Time

## Active Transformer or Alternating Current Transformer ACCT:

uses a trans-impedance amplifier (I/U converter) to  $R \approx 0 \Omega$  load impedance i.e. a current sink  
 + compensation feedback  
 $\Rightarrow$  longer droop time  $\tau_{droop}$

Application: measurement of longer  $t > 10 \mu\text{s}$  e.g. at pulsed LINACs



The input resistor is for an op-amp:  $R_f/A \ll R_L$

$$\Rightarrow \tau_{droop} = L/(R_f/A + R_L) \approx L/R_L$$

Droop time constant can be up to 1 s!

The feedback resistor is also used for range switching.

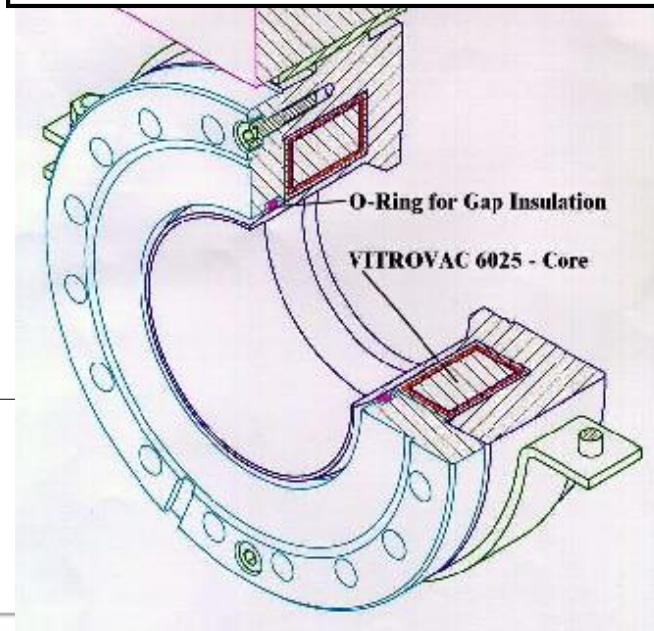
An additional active feedback loop is used to compensate the droop.

# 'Active' Transformer Realization

Active transformer for the measurement of long  $t > 10 \mu\text{s}$  pulses e.g. at pulsed LINACs



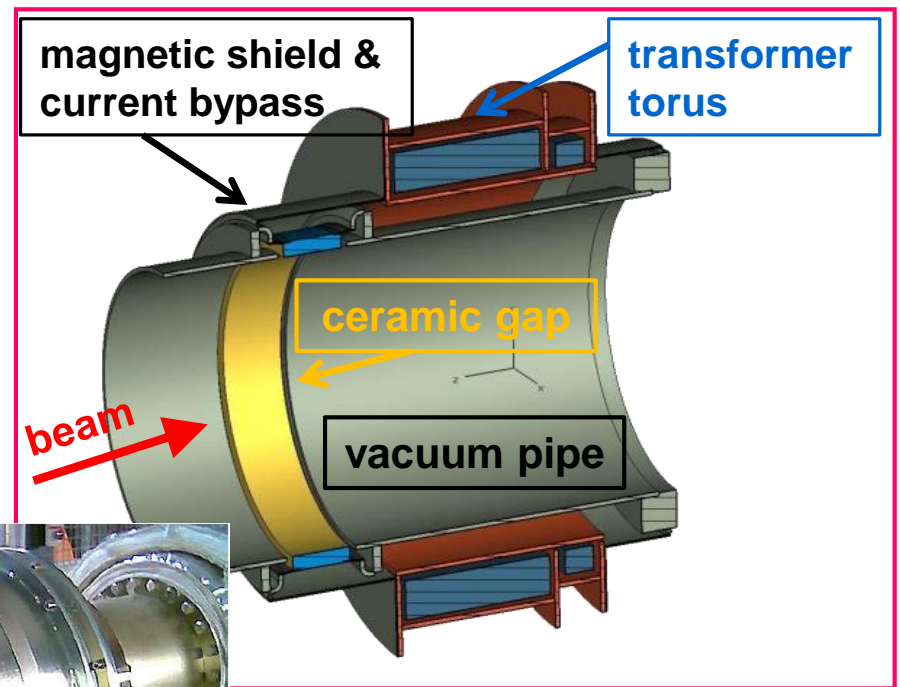
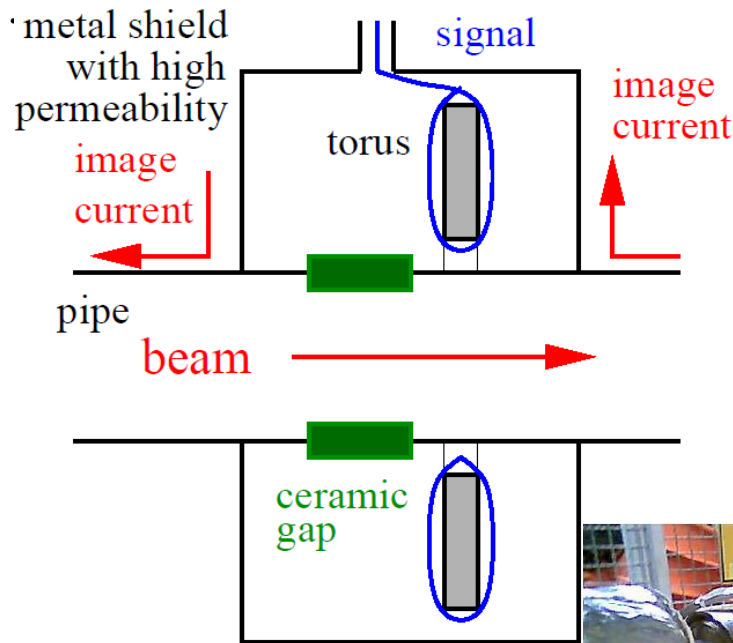
<b>Torus inner radius</b>	$r_i=30 \text{ mm}$
<b>Torus outer radius</b>	$r_o=45 \text{ mm}$
<b>Core thickness</b>	$l=25 \text{ mm}$
<b>Core material</b>	<b>Vitrovac 6025</b> $(\text{CoFe})_{70\%}(\text{MoSiB})_{30\%}$
<b>Core permeability</b>	$\mu_r=10^5$
<b>Number of windings</b>	2x10 crossed
<b>Max. sensitivity</b>	$10^6 \text{ V/A}$
<b>Beam current range</b>	10 $\mu\text{A}$ to 100 mA
<b>Bandwidth</b>	1 MHz
<b>Droop</b>	0.5 % for 5 ms
<b>rms resolution</b>	0.2 $\mu\text{A}$ for full bw



# Shielding of a Transformer

## Task of the shield:

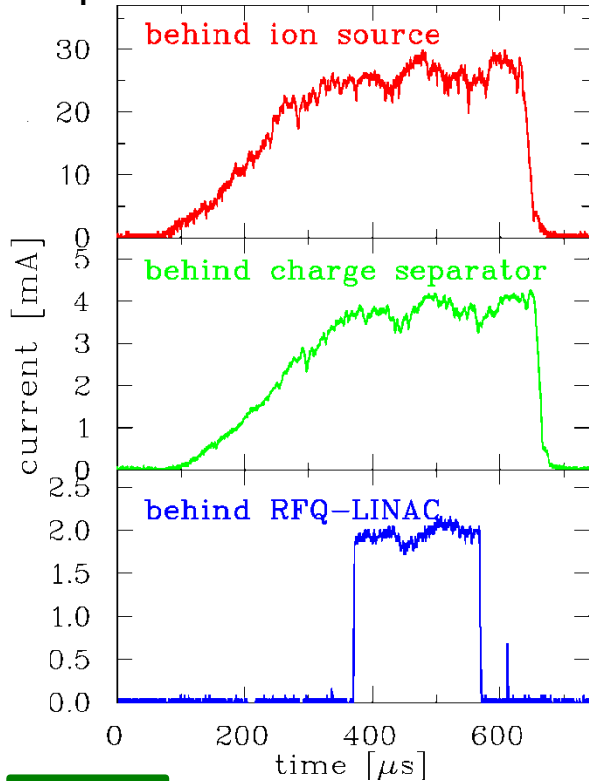
- The image current of the walls have to be bypassed by a gap and a metal housing.
- This housing uses  $\mu$ -metal and acts as a shield of external B-field  
(remember:  $I_{beam} = 1 \mu\text{A}$ ,  $r = 10 \text{ cm} \Rightarrow B_{beam} = 2\text{pT}$ , earth field  $B_{earth} = 50 \mu\text{T}$ )



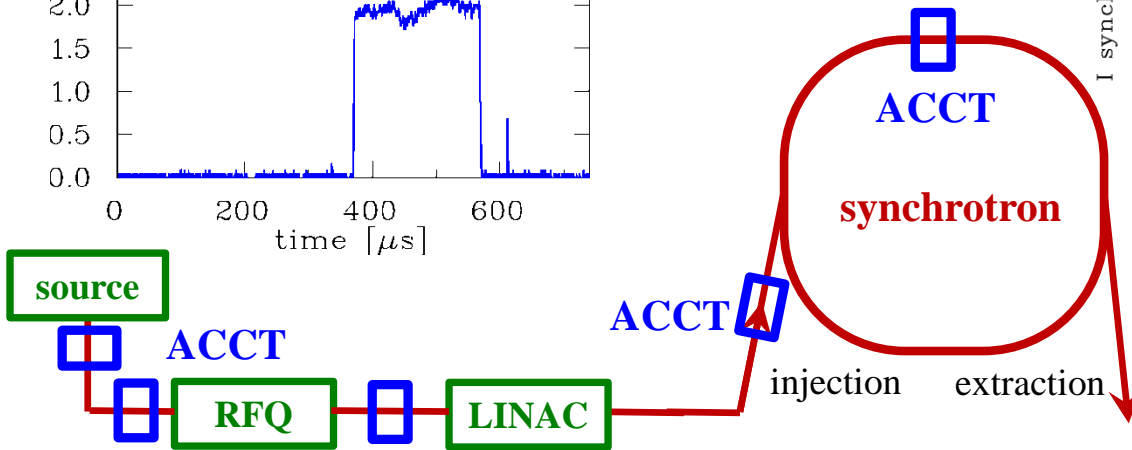
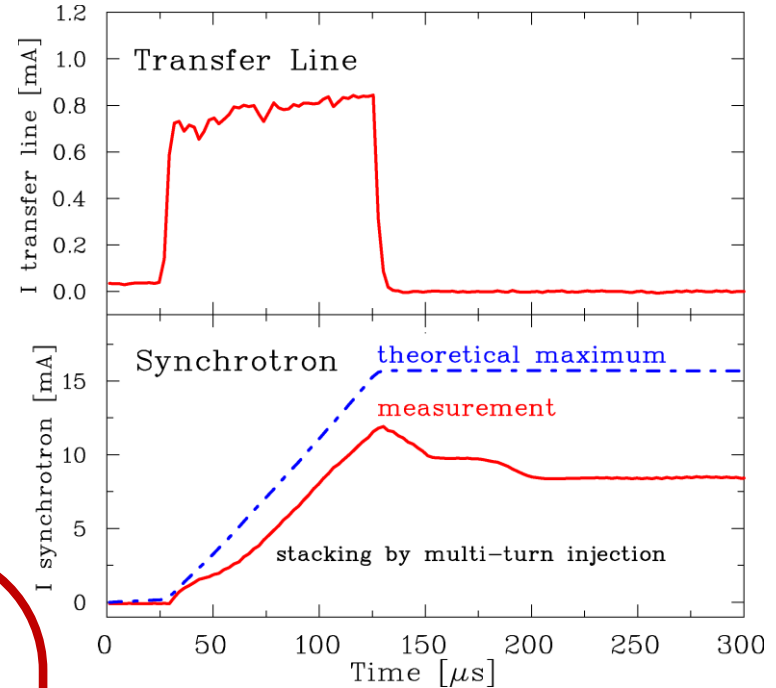
# 'Active' Transformer Measurement

Active transformer for the measurement of long  $t > 10 \mu\text{s}$  pulses e.g. at pulsed LINACs

**Example:** Transmission and macro-pulse shape for  $\text{Ni}^{2+}$  beam at GSI LINAC



**Example:** Multi-turn injection of a  $\text{Ni}^{26+}$  beam into GSI Synchrotron, 5  $\mu\text{s}$  per turn

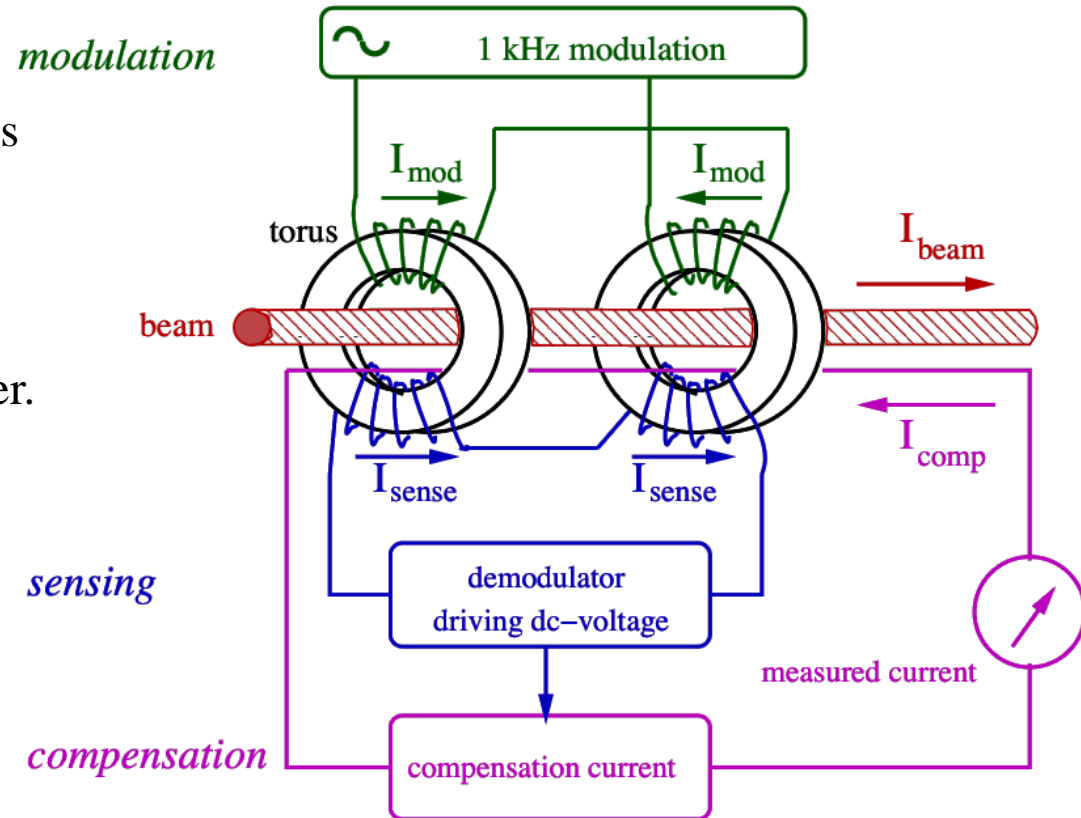


→ Transformer are frequently used for operation.

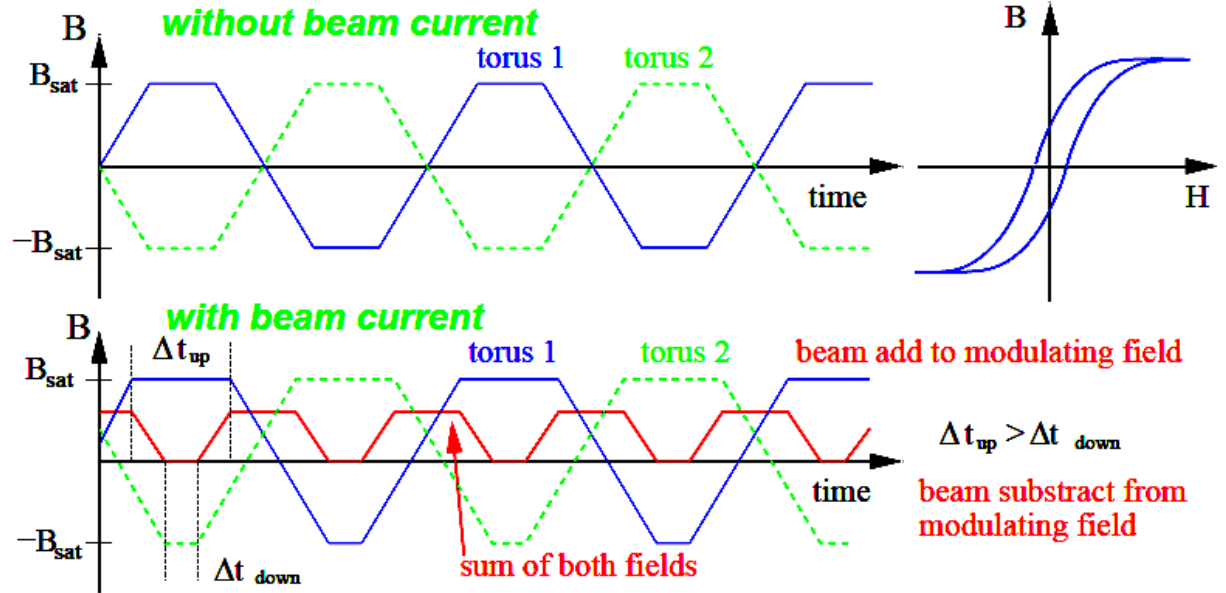
# The dc Transformer

How to measure the DC current? The current transformer discussed sees only B-flux *changes*. The DC Current Transformer (DCCT) → look at the magnetic saturation of two torii.

- **Modulation** of the primary windings forces both torii into saturation twice per cycle
- **Sense windings** measure the modulation signal and cancel each other.
- But with the  $I_{beam}$ , the saturation is shifted and  $I_{sense}$  is not zero
- **Compensation current** adjustable until  $I_{sense}$  is zero once again



# The dc Transformer



➤ **Modulation without beam:**

typically about 1 kHz to saturation → **no net flux**

➤ **Modulation with beam:**

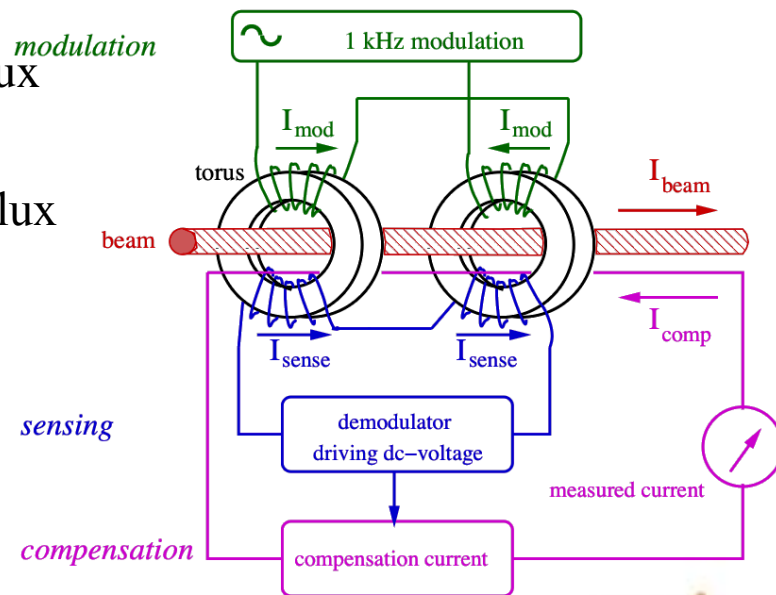
saturation is reached at different times, → net flux

➤ **Net flux:** double frequency than modulation

➤ **Feedback:** Current fed to compensation winding

for larger sensitivity

➤ **Two magnetic cores:** Must be very similar.

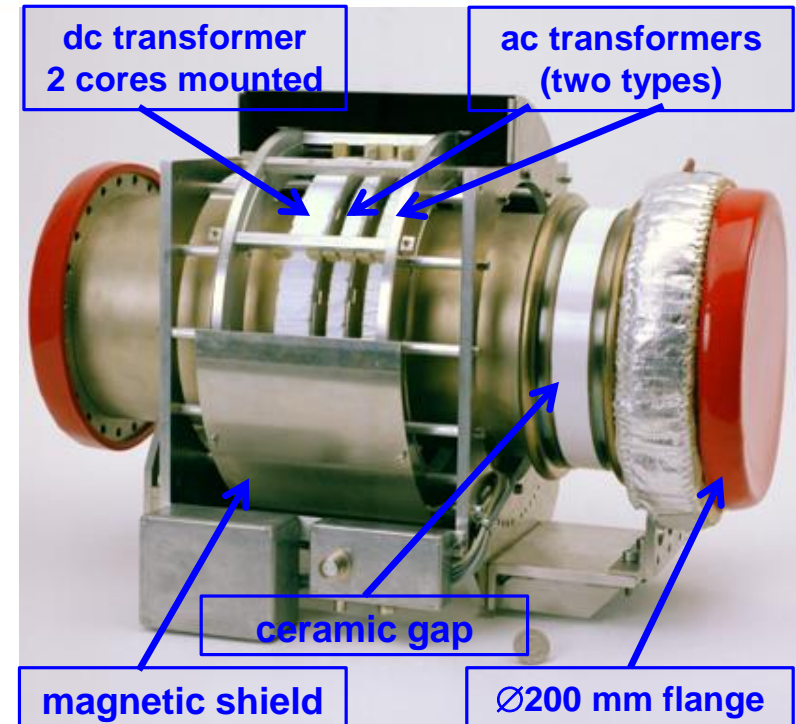
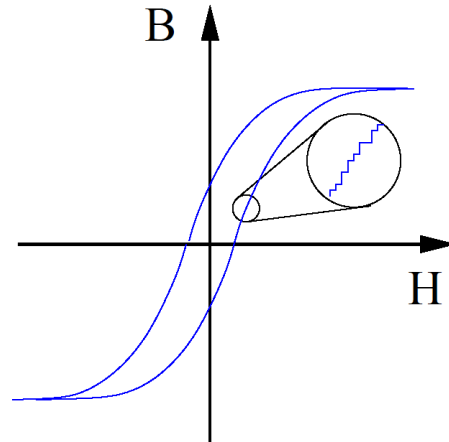


# The dc Transformer Realization

## Example: The DCCT at GSI synchrotron

<b>Torus radii</b>	$r_i = 135 \text{ mm}$ $r_o = 145 \text{ mm}$
<b>Torus thickness</b>	$d = 10 \text{ mm}$
<b>Torus permeability</b>	$\mu_r = 10^5$
<b>Saturation inductance</b>	$B_{\text{sat}} = 0.6 \text{ T}$
<b>Number of windings</b>	16 for modulation & sensing 12 for feedback
<b>Resolution</b>	$I_{\text{beam}}^{\text{min}} = 2 \mu\text{A}$
<b>Bandwidth</b>	$\Delta f = \text{dc} \dots 20 \text{ kHz}$
<b>Rise time constant</b>	$\tau_{\text{rise}} = 10 \mu\text{s}$
<b>Temperature coefficient</b>	$1.5 \mu\text{A}/^\circ\text{C}$

Resolution limit  
of  $\approx 1 \mu\text{A}$  caused by  
Barkhausen noise due  
to changes of Weiss domains





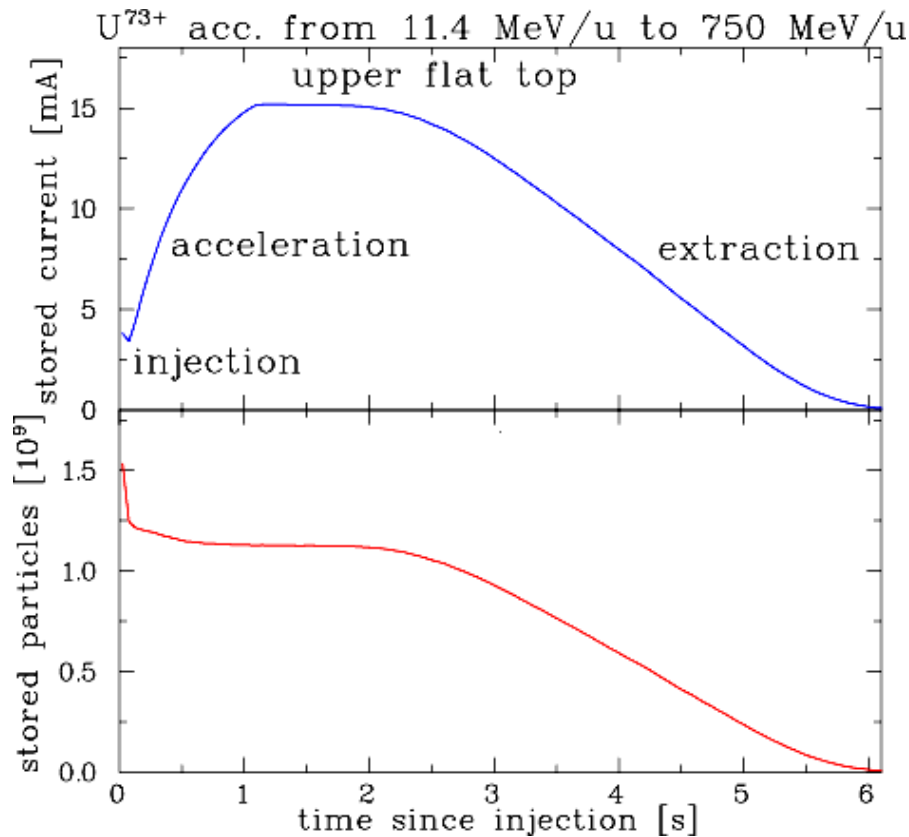
# Measurement with a dc Transformer



## Application for dc transformer:

⇒ Observation of beam behavior with typ. 20  $\mu\text{s}$  time resolution → **the** basic operation tool.

Example: The DCCT at GSI synchrotron:



**Important parameter:**

**Detection threshold:  $\approx 1 \mu\text{A}$**

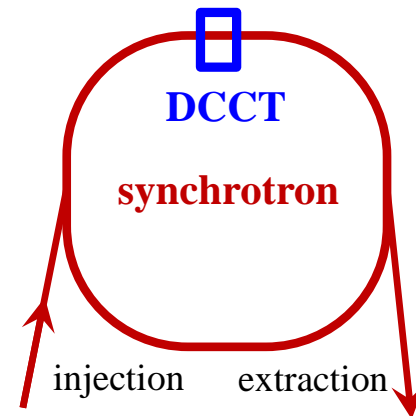
(= resolution)

Bandwidth:  $\Delta f = \text{dc to } 20 \text{ kHz}$

Rise-time:  $t_{\text{rise}} = 20 \mu\text{s}$

Temperature drift:  $1.5 \mu\text{A}/^\circ\text{C}$

⇒ compensation required.



The beam current is the basic quantity of the beam.

- It is the first check of the accelerator functionality
- It has to be determined in an absolute manner
- Important for transmission measurement and to prevent beam losses.

**Different devices are used:**

- **Transformers:** Measurement of the beam's **magnetic field**

They are non-destructive. No dependence on beam energy

They have lower detection threshold.

- **Faraday cups:** Measurement of the beam's **electrical charges**

They are destructive. For low energies only

Low currents can be determined.

- **Particle detectors:** Measurement of the particle's **energy loss** in matter

# Energy Loss of Ions in Copper

Bethe Bloch formula:  
(simplest formulation)

$$-\frac{dE}{dx} = 4\pi N_A r_e m_e c^2 \cdot \frac{Z_t}{A_t} \rho_t \cdot \frac{Z_p^2}{\beta^2} \left( \ln \frac{2m_e c^2 \gamma^2 \beta^2}{I} - \beta^2 \right)$$

## Semi-classical approach:

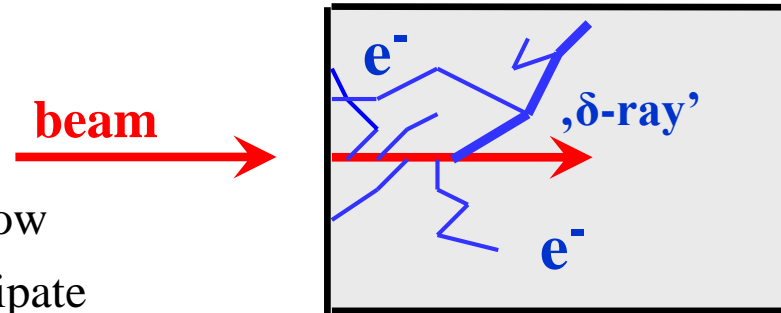
- Projectiles of mass  $M$  collide with free electrons of mass  $m$
- If  $M \gg m$  then the relative energy transfer is low  
⇒ many collisions required many electrons participate

proportional to electron density  $n_e = \frac{Z_t}{A_t} \rho_t$

⇒ low straggling for the heavy projectile i.e. ‘straight trajectory’

- If projectile velocity  $\beta \approx 1$  low relative energy change of projectile ( $\gamma$  is Lorentz factor)
- $I$  is mean ionization potential including kinematic corrections  $I \approx Z_t \cdot 10 \text{ eV}$  for most metals
- Strong dependence on projectile charge  $Z_p$

Constants:  $N_A$  Avogadro number,  $r_e$  classical  $e^-$  radius,  $m_e$  electron mass,  $c$  velocity of light



# Energy Loss of Ions in Copper

Bethe Bloch formula: 
$$-\frac{dE}{dx} = 4\pi N_A r_e m_e c^2 \cdot \frac{Z_t}{A_t} \rho_t \cdot \frac{Z_p^2}{\beta^2} \left( \ln \frac{2m_e c^2 \gamma^2 \beta^2}{I} - \beta^2 \right)$$

Range: 
$$R = \int_0^{E_{\max}} \left( \frac{dE}{dx} \right)^{-1} dE$$

with approx. scaling  $R \propto E_{\max}^{1.75}$

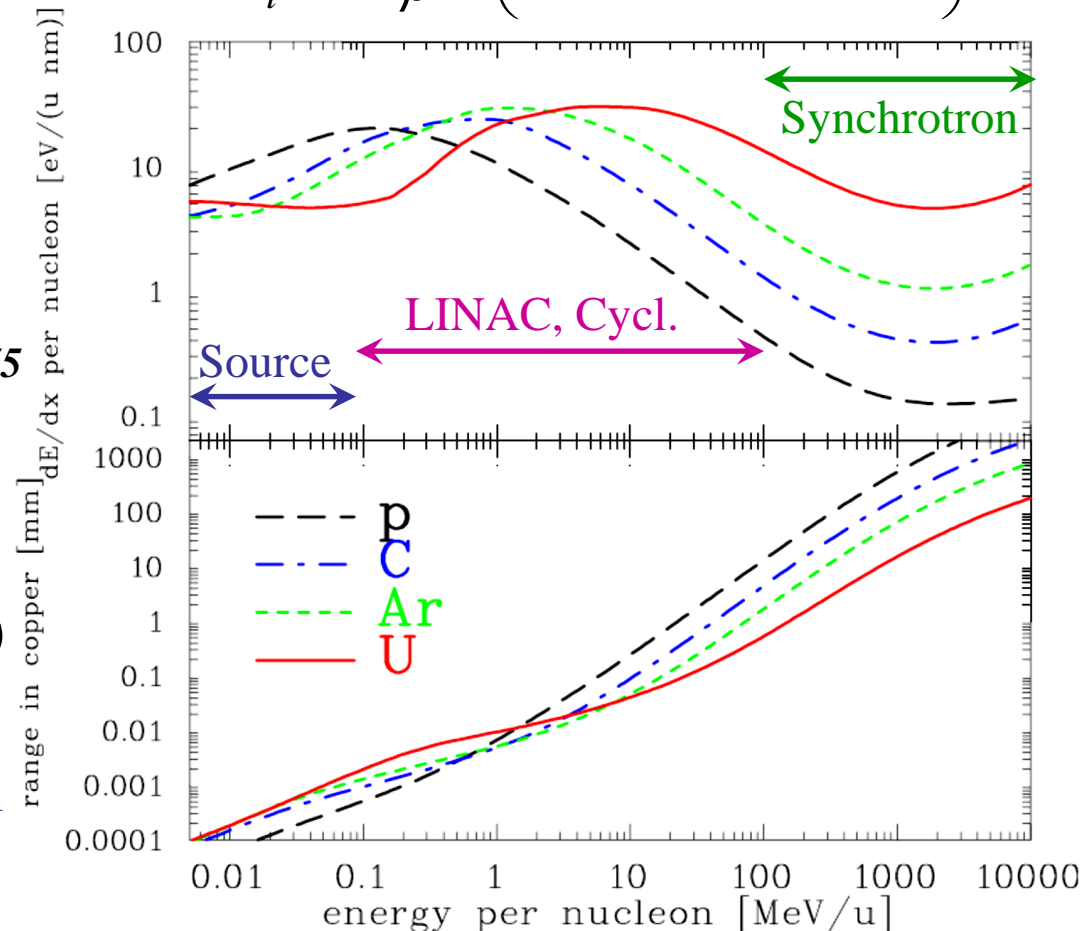
Numerical calculation

with semi-empirical model e.g. SRIM

Main modification  $Z_p \rightarrow Z_p^{\text{eff}}(E_{\text{kin}})$

⇒ Cups only for

$E_{\text{kin}} < 100 \text{ MeV/u}$  due to  $R < 10 \text{ mm}$



# Secondary Electron Emission caused by Ion Impact

Energy loss of ions in metals close to a surface:

Closed collision with large energy transfer:  $\rightarrow$  fast  $e^-$  with  $E_{kin} > 100$  eV

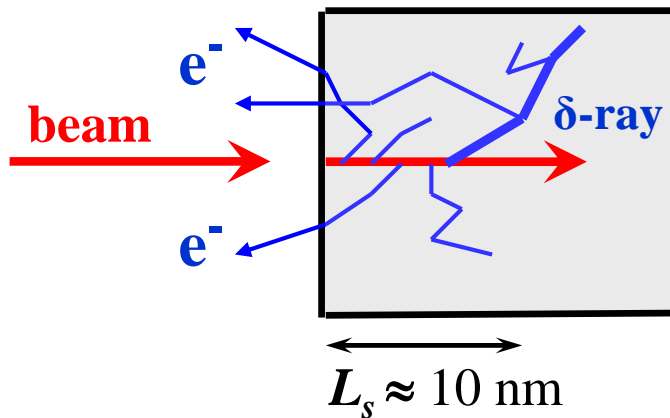
Distant collision with low energy transfer  $\rightarrow$  slow  $e^-$  with  $E_{kin} \leq 10$  eV

$\rightarrow$  'diffusion' & scattering with other  $e^-$ : scattering length  $L_s \approx 1 - 10$  nm

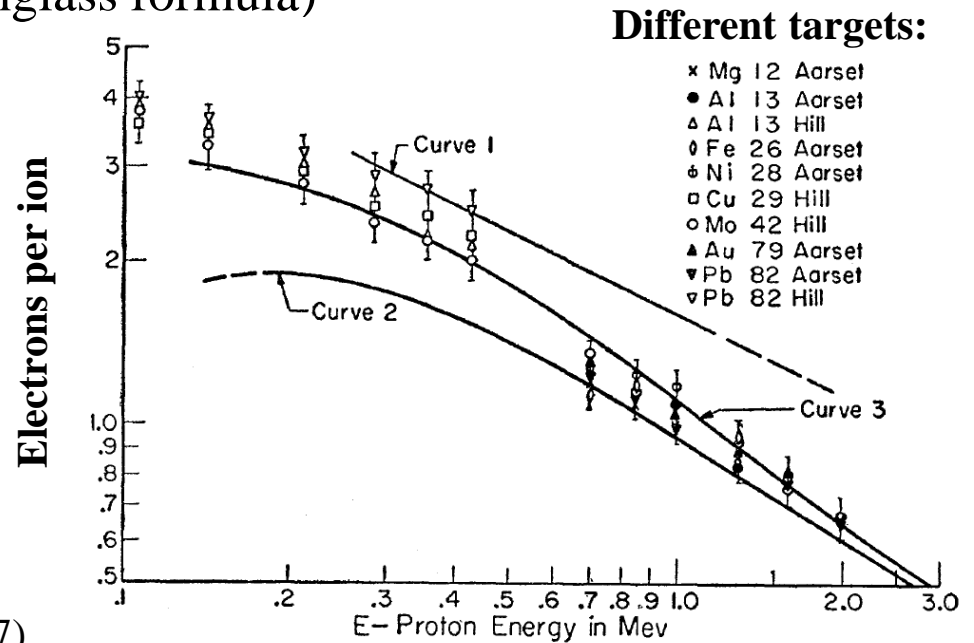
$\rightarrow$  at surface  $\approx 90\%$  probability for escape

Secondary **electron yield** and energy distribution comparable for all metals!

$$\Rightarrow Y = const. * dE/dx \quad (\text{Sternglass formula})$$



From E.J. Sternglass, Phys. Rev. 108, 1 (1957)



# Secondary Electron Emission caused by Ion Impact

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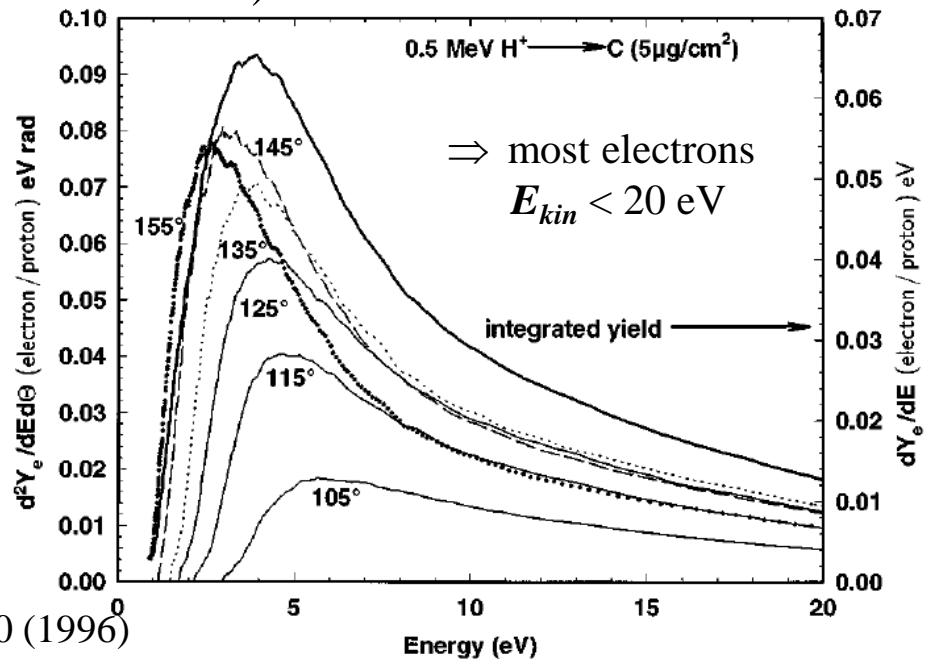
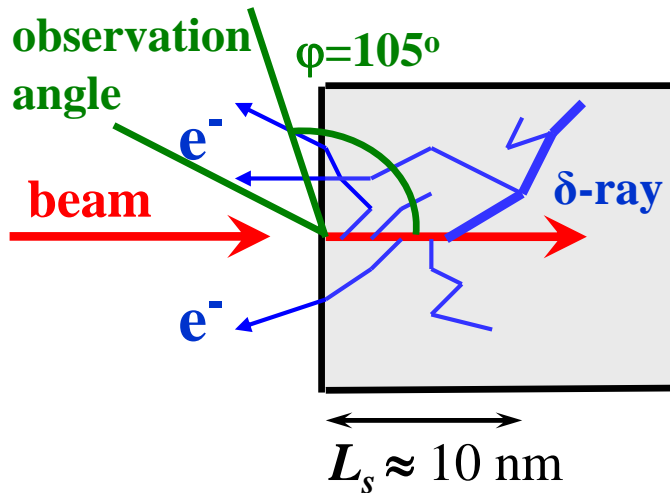
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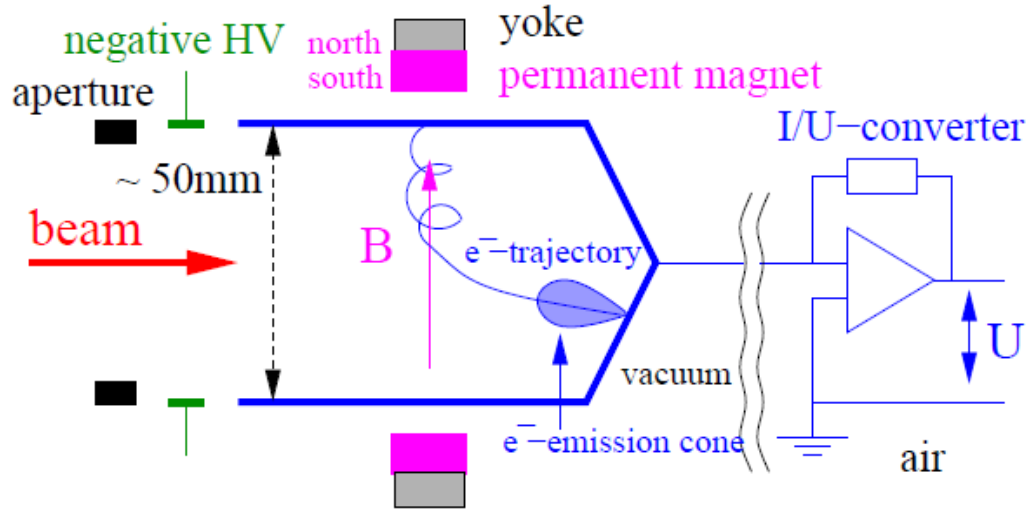


From C.G. Drexler, R.D. DuBois, Phys. Rev. A 53, 1630 (1996)

# Faraday Cups for Beam Charge Measurement



The beam particles are collected inside a metal cup  
⇒ The beam's charge are recorded as a function of time.



The cup is moved in the beam pass → destructive device

**Currents down to 10 pA with bandwidth of 1 kHz!**

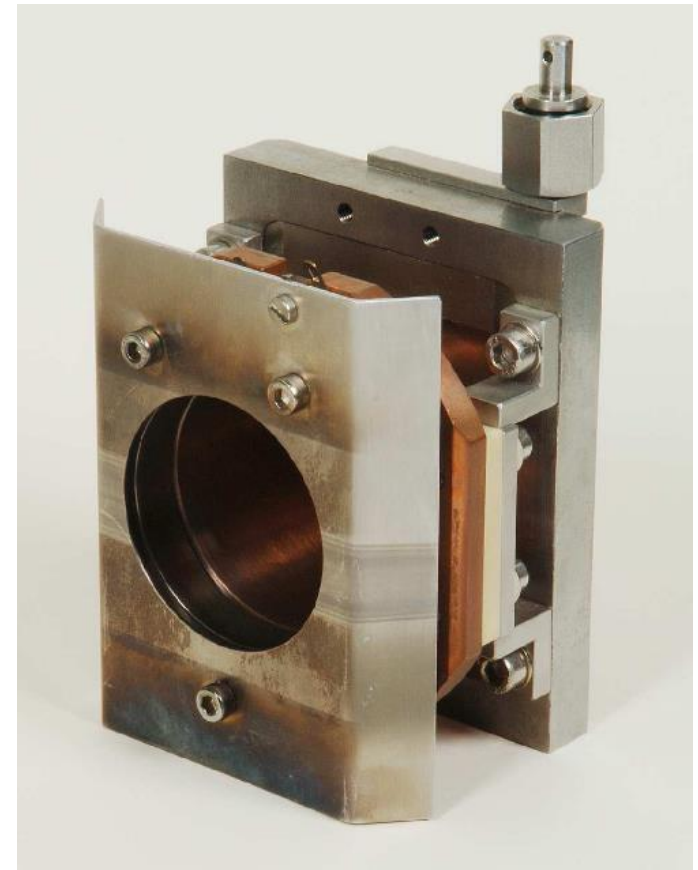
## Magnetic field:

To prevent for secondary electrons leaving the cup

*and/or*

## Electric field:

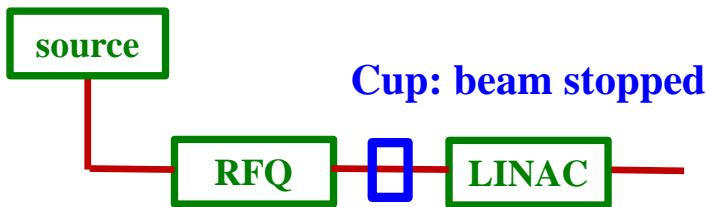
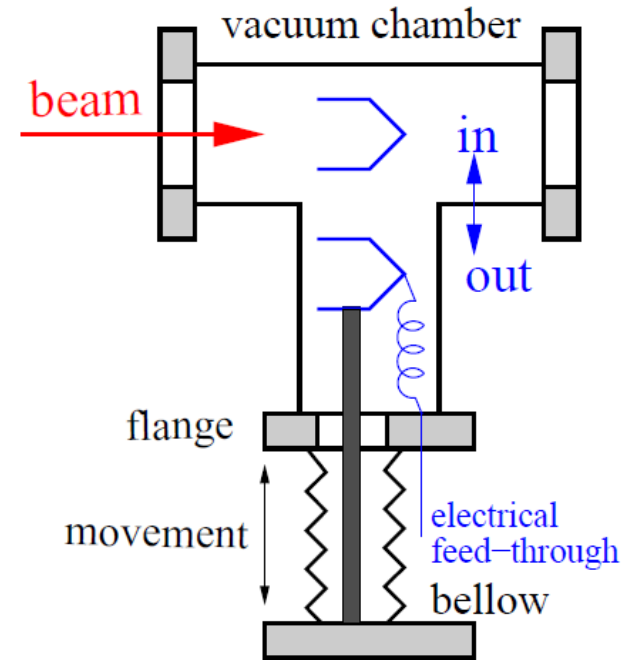
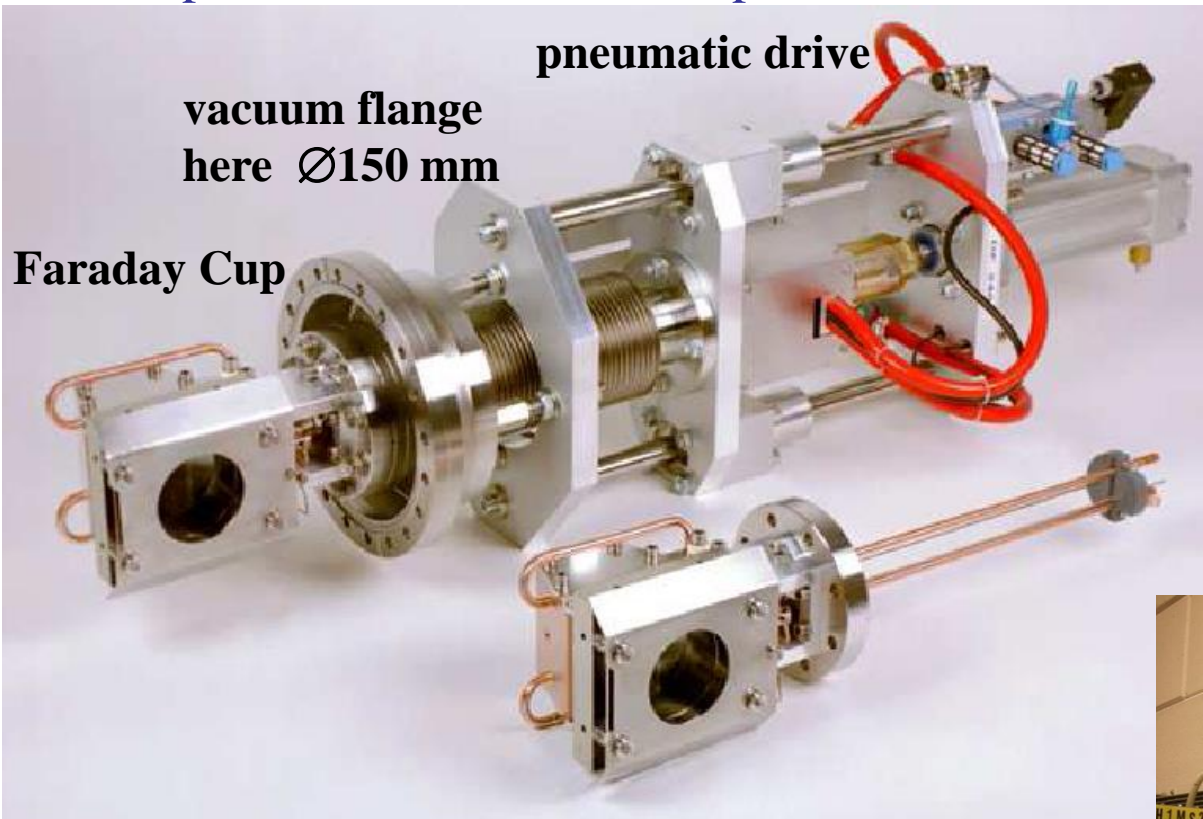
Potential barrier at the cup entrance.



# Realization of a Faraday Cup at GSI LINAC



The Cup is moved into the beam pass.

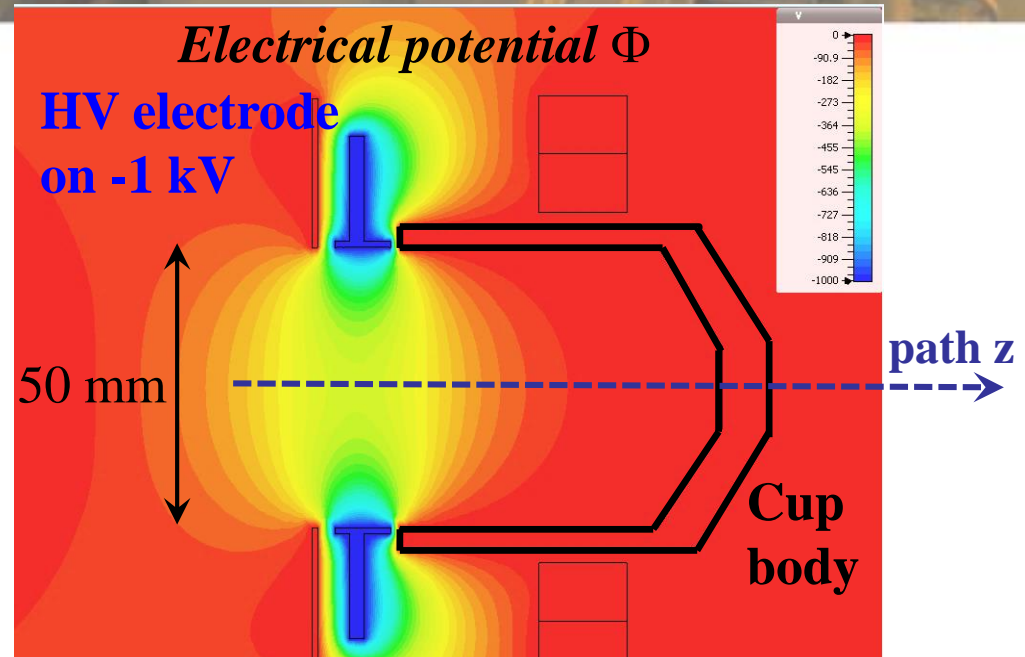
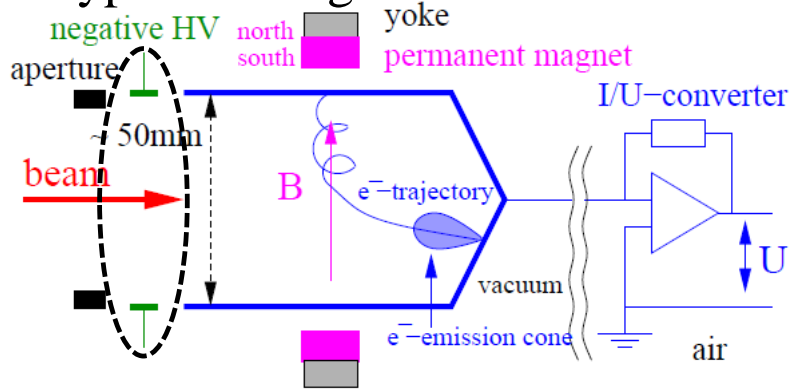




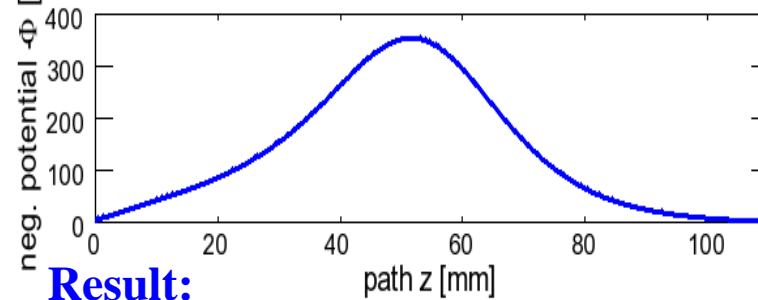
# Secondary Electron Suppression: Electric Field

A ring shaped electrode is used at the entrance of Faraday Cup:

Typical voltage 100 to 1000 V



potential on central axis for -1 kV@electrode



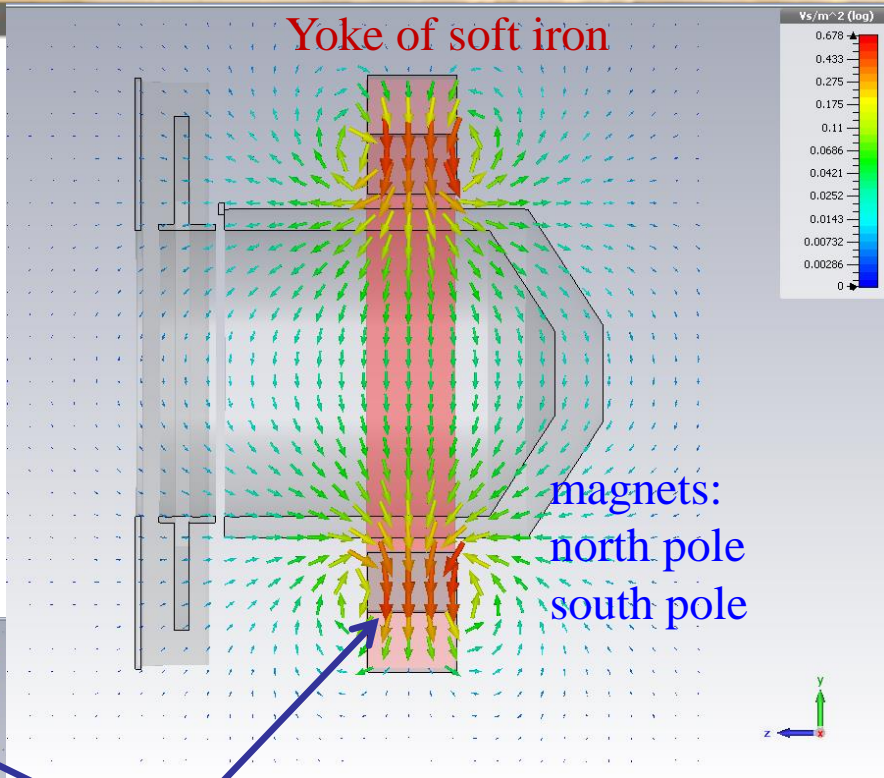
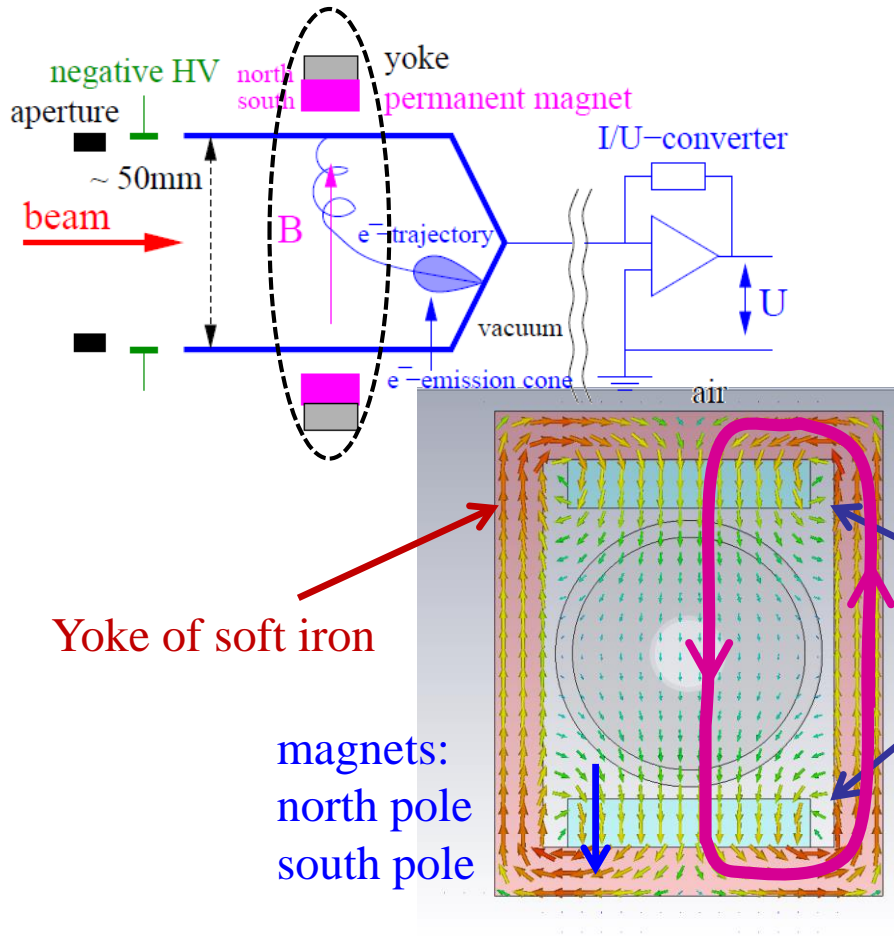
**Result:**

here: potential at center  $\approx 35\%$  of applied voltage

Courtesy of J. Latzko, GSI

# Secondary Electron Suppression: Magnetic Field

Co-Sm permanent magnets within the yoke and the calculated magnetic field lines.  
 The central field strength is  $B \approx 0.1$  T.



Courtesy of J. Latzko, GSI

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- Important for transmission measurement and to prevent for beam losses.

**Different devices are used:**

- **Transformers:** Measurement of the beam's **magnetic field**

They are non-destructive. No dependence on beam energy

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They are destructive. For low energies only

Low currents can be determined.

- **Particle detectors:** Measurement of the particle's **energy loss** in matter

Examples are scintillators, ionization chambers, secondary e<sup>-</sup> emission monitors

Used for low currents at high energies e.g. for slow extraction from a synchrotron.

# Low Current Measurement for slow Extraction

Slow extraction from synchrotron: lower current compared to LINAC, but higher energies and larger range  $R \gg 1$  cm.

Extracted current  $I_{beam} = qe \frac{N_{part}}{t}$  :

- Slow extraction: e.g.  $N_{part} = 10^{12}$  protons per  $t = 10$  s = 1.6  $\mu$ A i.e. below DCCT threshold
- Fast extraction: e.g.  $N_{part} = 10^{12}$  protons per  $t = 100$  ns = 1.6 A

## Detector types:

- **Particle counting:**

max:  $r \approx 10^6$  1/s

- **Energy loss in gas (IC):**

min:  $I_{sec} \approx 1$  pA

max:  $I_{sec} \approx 1$   $\mu$ A

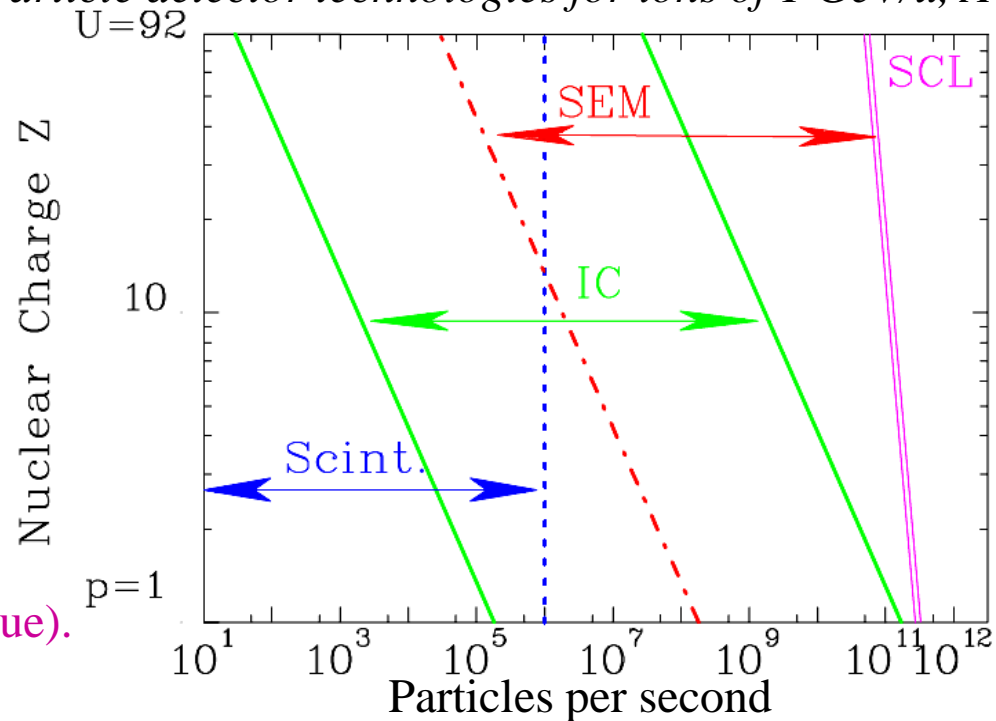
- **Sec. e<sup>-</sup> emission:**

min:  $I_{sec} \approx 1$  pA

- **Max. synch. filling:**

Space Charge Limit (SCL, typ. value).

Particle detector technologies for ions of 1 GeV/u,  $A = 1$  cm<sup>2</sup>:



# Example of Scintillator Counter

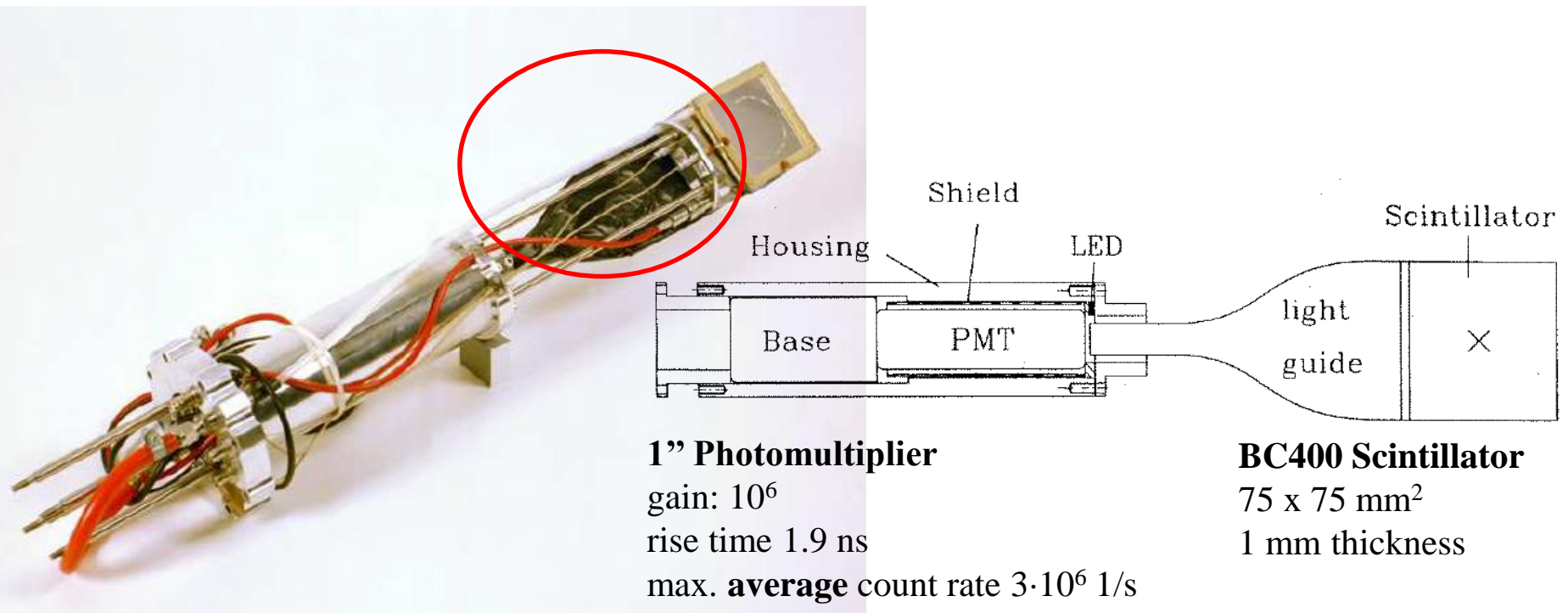
Example: Plastic Scintillator i.e. organic fluorescence molecules in a plastic matrix

Here: BC 400 (emission  $\lambda_{max} = 420 \text{ nm}$ , pulse width  $\approx 3 \text{ ns}$  + cable dispersion, size )

**Advantage:** any mechanical form, cheap, blue wave length, fast decay time

**Disadvantage:** not radiation hard

Particle counting: Photomultiplier  $\rightarrow$  discriminator  $\rightarrow$  scalar  $\rightarrow$  computer



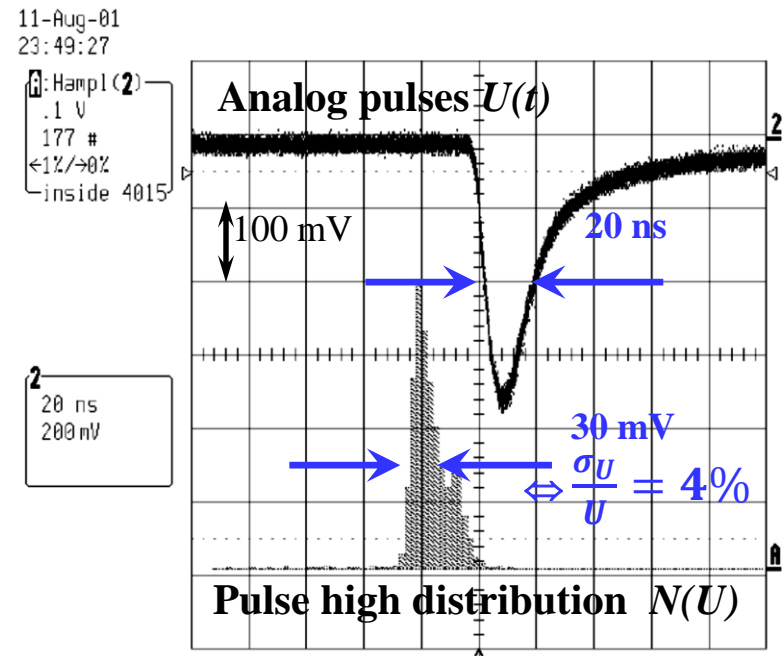
# Properties of a good Scintillator



## Properties of a good scintillator:

- Light output linear to energy loss
- Fast decay time → high rate
- No self-absorption
- Wave length of fluorescence  
 $350 \text{ nm} < \lambda < 500 \text{ nm}$
- Index of refractivity  $n \approx 1.5$   
→ light-guide
- Radiation hardness  
e.g. Ce-activated inorganic  
are much more radiation hard.

Analog pulses from a plastic sc. with a low current 300 MeV/u Kr beam.



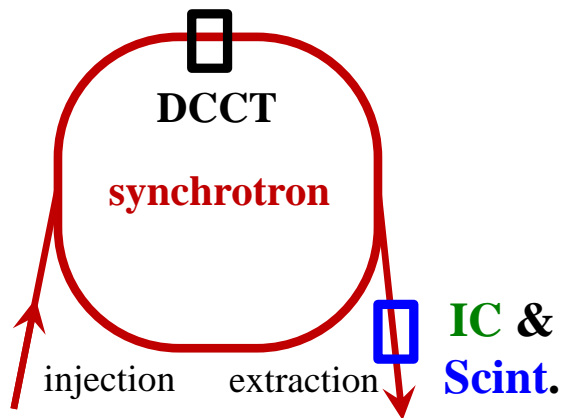
The scaling is 20 ns/div and 100 mV/div.

# Monitoring of Slow Extraction

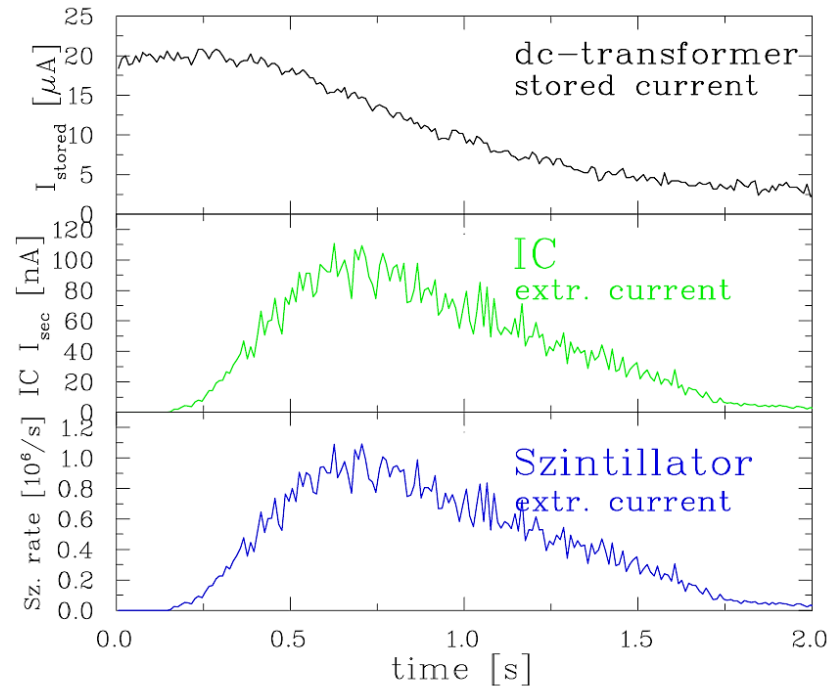
Slow extraction from a synchrotron delivers countable currents.

## Usage for:

- Optimization of extraction efficiency
- If possible transmission active control
- Alignment of coarse time dependent  $I_{beam}(t)$
- Determination & optimization of fine  $I_{beam}(t)$
- Calibration of different detectors

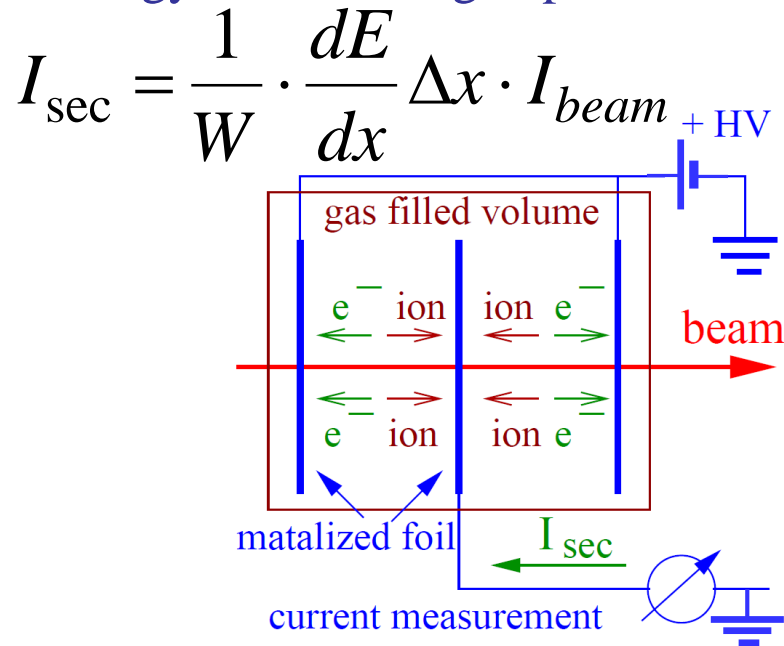


*Example:* Comparison for different detector types: dc-transformer DCCT inside synchrotron., ionization chamber and scintillator for 250 MeV/u Pb<sup>67+</sup> beam with 10<sup>6</sup> particles.

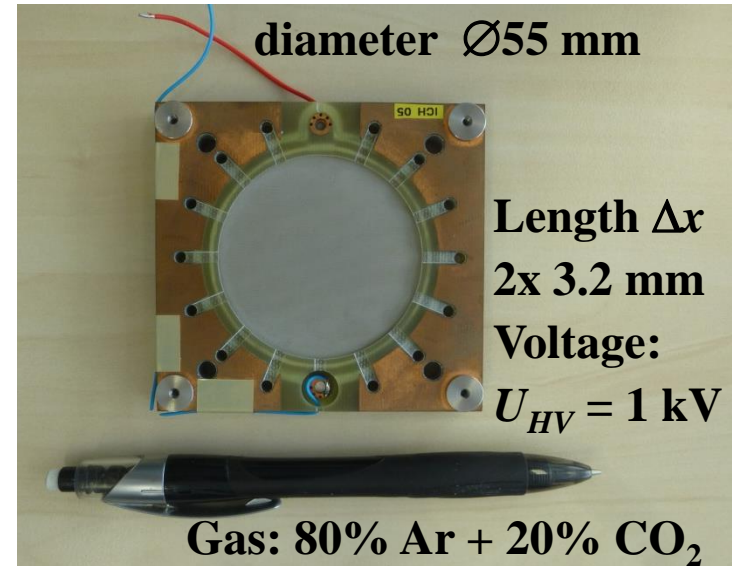


# Ionization Chamber (IC): Electron Ion Pairs

Energy loss of charged particles in gases → electron-ion pairs → low current meas.



*Example: GSI type:*



## *W-value*

is the average energy for one  $e^-$ -ion pair:

Gas	Ionization Pot.	W-value
He	24.5 eV	42.7 eV
N <sub>2</sub>	15.5 eV	36.4 eV
O <sub>2</sub>	12.5 eV	32.2 eV
Ar	15.7 eV	26.3 eV
CO <sub>2</sub>	13.7 eV	33.0 eV

## GSI realization:

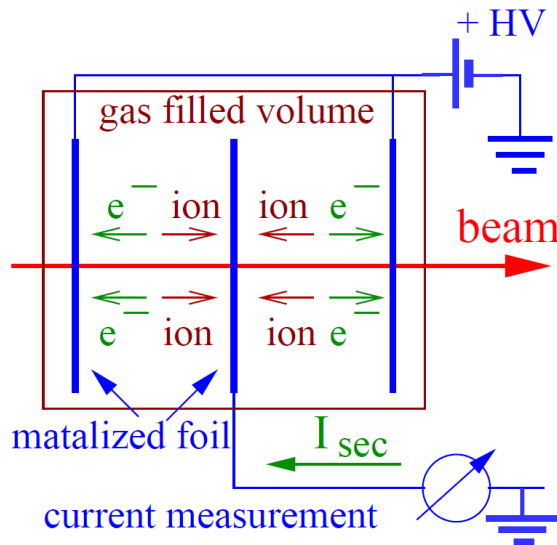
- Energy calculation  $dE/dx$  with SRIM or LISE
- Current measurement via current-to-frequency converter IFC



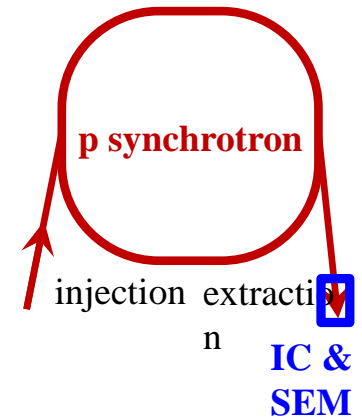
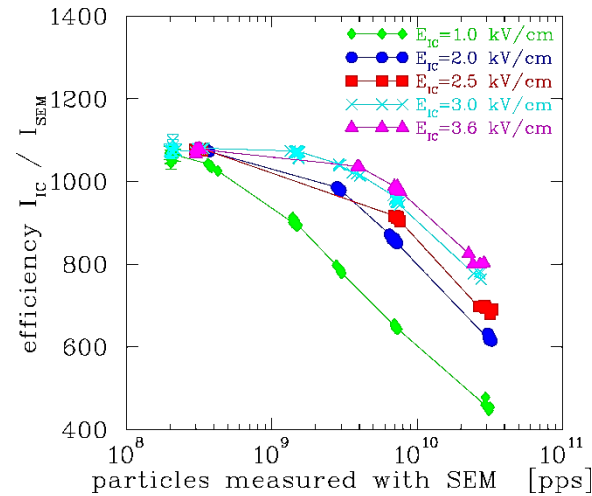
# Lower and upper Limit of IC Current

**Lower limit** of a IC is given by the most sensitive current measurement:

typically min.  $I_{sec} \approx 10$  pA with 1 ms time resolution  $\Leftrightarrow$  bandwidth 0.3 kHz (note  $U_{noise} \propto \sqrt{\Delta f}$ )



Example: GSI slow extraction of 2 s, 300 MeV/u  $Ne^{10+}$



**Upper limit** of a IC is related to the recombination of gas ions e.g.  $Ar^+ + e^- \rightarrow Ar$

- The density of  $Ar^+$  and is  $n_{Ar} \propto I_{beam}$  and of  $e^-$   $n_e \propto I_{beam}$
- Recombination:  $Ar^+ + e^- \rightarrow Ar$  leads to loss of sec. charges  $I_{REC} \propto \alpha \cdot n_{Ar} \cdot n_e \propto I_{beam}^2$
- Drift time  $Ar$ :  $t_{drift} \propto E_{IC} \approx 50\mu s$  &  $e^-$ :  $t_{drift} \propto E_{IC} \approx 0.1\mu s$ ; rate coefficient  $\alpha = 10^{-9} \text{ cm}^3/\text{s}$
- Effect remarkable for secondary current  $I_{sec} > 1 \mu A$  or dose rate of  $D_{IC} > 30 \text{ Gy/s}$

e.g. max  $I_{beam}$  for 1 GeV/u,  $t_{ex}=1$  s,  $\varnothing$  0.5 cm:  $p \rightarrow 10^{11}$  1/s,  $Ne \rightarrow 10^9$  1/s,  $U \rightarrow 10^7$  1/s

# Secondary Electron Monitor (SEM): Electrons from Surface

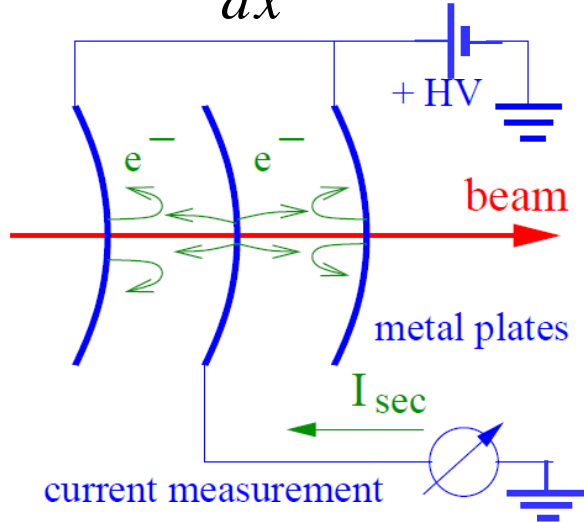


For higher intensities SEMs are used.

Due to the energy loss, secondary  $e^-$  are emitted from a metal surface.

The amount of secondary  $e^-$  is proportional to the energy loss

$$I_{\text{sec}} = Y \cdot \frac{dE}{dx} \cdot I_{\text{beam}}$$



Example: GSI SEM type:

Material	Pure Al ( $\approx 99.5\%$ )
# of electrode	3
Active surface	80 x 80 mm <sup>2</sup>
Distance between electrodes	5 mm
Applied voltage	+ 100 V

**Advantage for Al:** good mechanical properties.

**Disadvantage:** Surface effect!

e.g. decrease of yield  $Y$  due to radiation

$\Rightarrow$  calibration versus IC required to reach 5%.

It is a *surface* effect:

$\rightarrow$  Sensitive to cleaning procedure

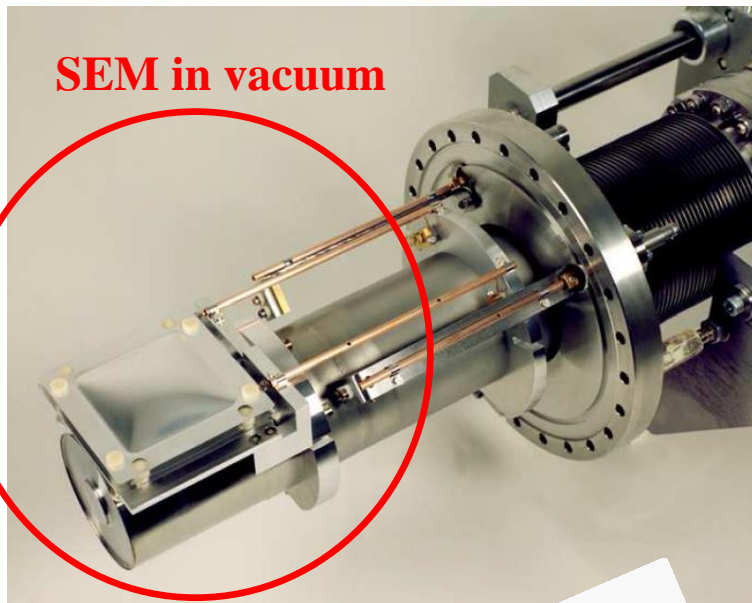
$\rightarrow$  Possible surface modification by radiation

Sometimes they are installed permanently in front of an experiment.

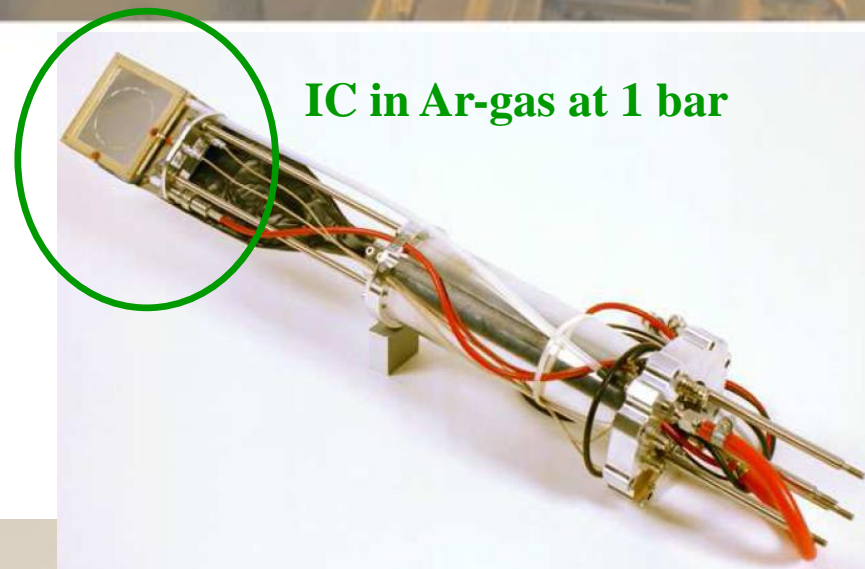
# GSI Installation for SEM, IC and Scintillator



SEM in vacuum



IC in Ar-gas at 1 bar



beam

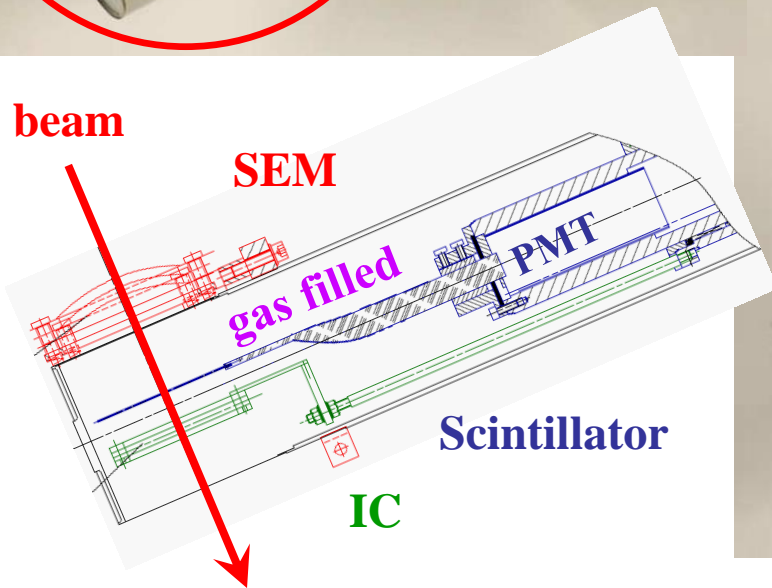
SEM

gas filled

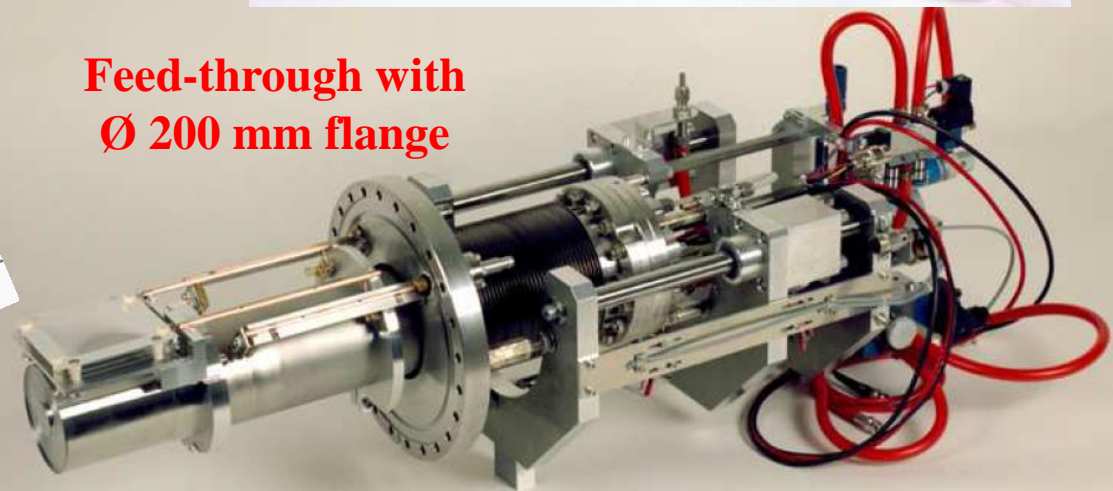
PMT

Scintillator

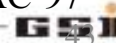
IC



Feed-through with  
Ø 200 mm flange



P. Forck et al., DIPAC'97



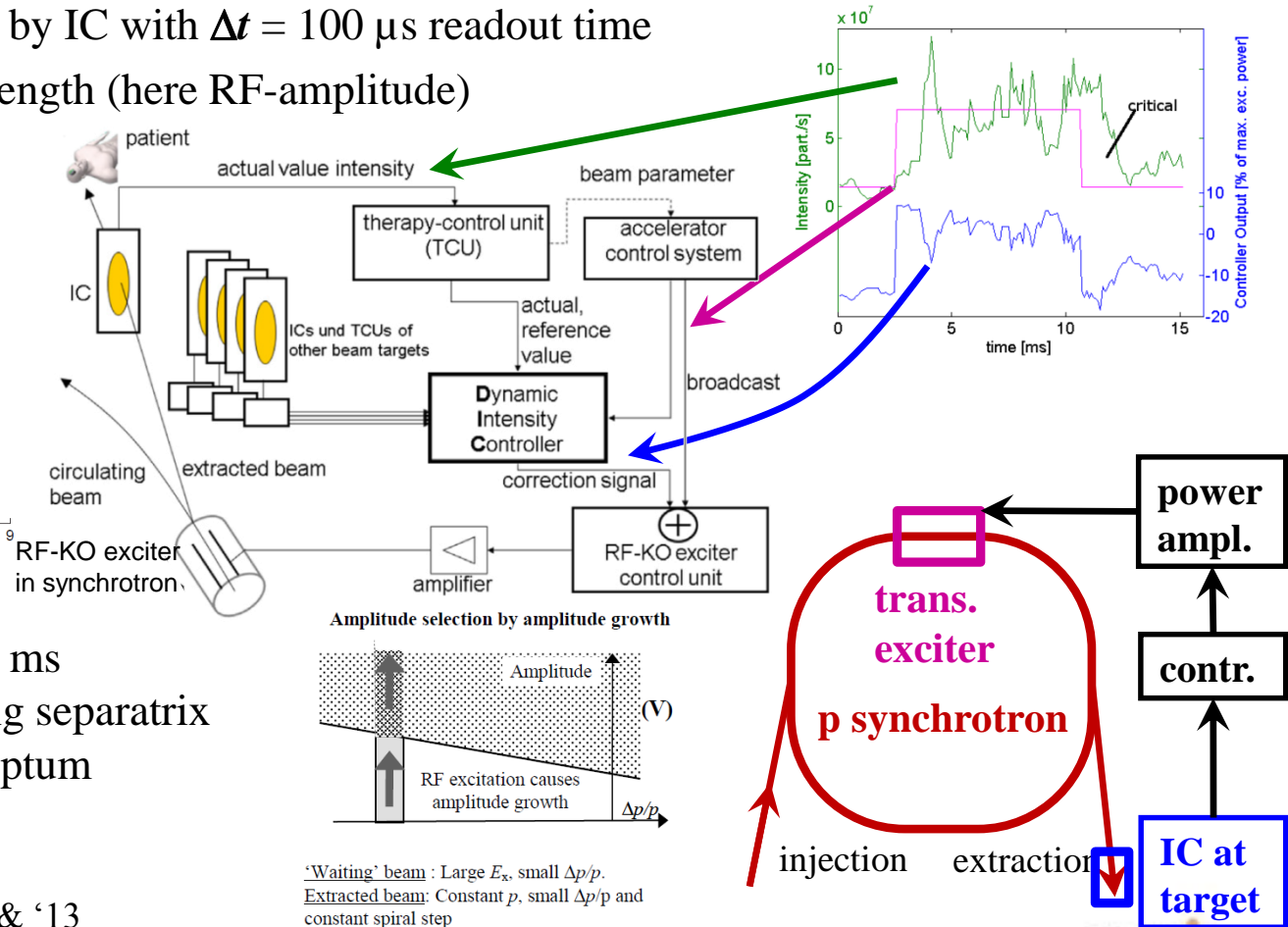
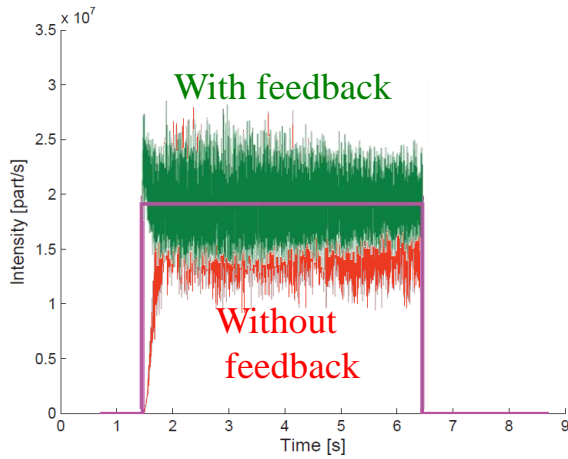
# Current Control for slow Extraction using the Signal from IC



Slow extraction: A constant beam delivery  $I_{beam}(t)$  at experiment is desired  
 → feedback: **Input** IC monitor for the *extracted* beam on target, **Output**: extraction strength in synchr.

**Example** from medical facility HIT:  $C^{6+}$  at 250 MeV/u

- Beam current measurement by IC with  $\Delta t = 100 \mu s$  readout time
- Regulation of extraction strength (here RF-amplitude)



Regulation achievements:  $\approx 10$  ms limited by latency from crossing separatrix until reach the electro-static septum

Courtesy C. Schömers (HIT) et al., NIM A 795, 92 (2015) and IPAC'11 & '13

'Waiting' beam : Large  $E_x$ , small  $\Delta p/p$ .  
 Extracted beam: Constant  $p$ , small  $\Delta p/p$  and constant spiral step

# Summary for Current Measurement



## Current is the basic quantity for accelerators!

### **Transformer:** → measurement of the beam's magnetic field

- magnetic field is guided by a high  $\mu$  toroid
- types: passive (large bandwidth,  $I_{min} \approx 30 \mu\text{A}$ , BW = 10 kHz ... 500 MHz ),  
active (low droop,  $I_{min} \approx 0.3 \mu\text{A}$ , BW = 10 Hz .... 1 MHz )  
dc (two toroids + modulation,  $I_{min} \approx 1 \mu\text{A}$ , BW = dc ... 20 kHz )
- non-destructive, used for all beams

### **Faraday cup:** → measurement of beam's charge

- low threshold by I/U-converter:  $I_{beam} > 10 \text{ pA}$
- totally destructive, used for low energy beams

### **Scintillator,** → measurement of the particle's energy loss

### **IC, SEM:**

- particle counting (Scintillator)
- secondary current: **IC** from gas ionization or **SEM** sec.  $e^-$  emission surface
- no lower threshold due to single particle counting
- partly destructive, used for high energy beams

When energetic beam particles penetrates matter, secondary particles are emitted:

this can be  $e^-$ ,  $\gamma$ , protons, neutrons, excited nuclei, fragmented nuclei...

⇒ Spontaneous radiation and permanent activation is produced.

⇒ Large variety of Beam Loss Monitors (**BLM**) depending on the application.

**Protection:** Sensitive devices e.g. super-conducting magnets to prevent quenching  
(energy absorption by electronic stopping)

→ **interlock signal for fast beam abortion.**

**Beam diagnostics:** Alignment of the beam to prevent for activation

→ **optimal transmission to the target.**

- Several devices are used, depending on particle rate and required time resolution
- Some applications for usage

# Basic Idea of Beam Loss Monitors



## Basic idea for Beam Loss Monitors BLM:

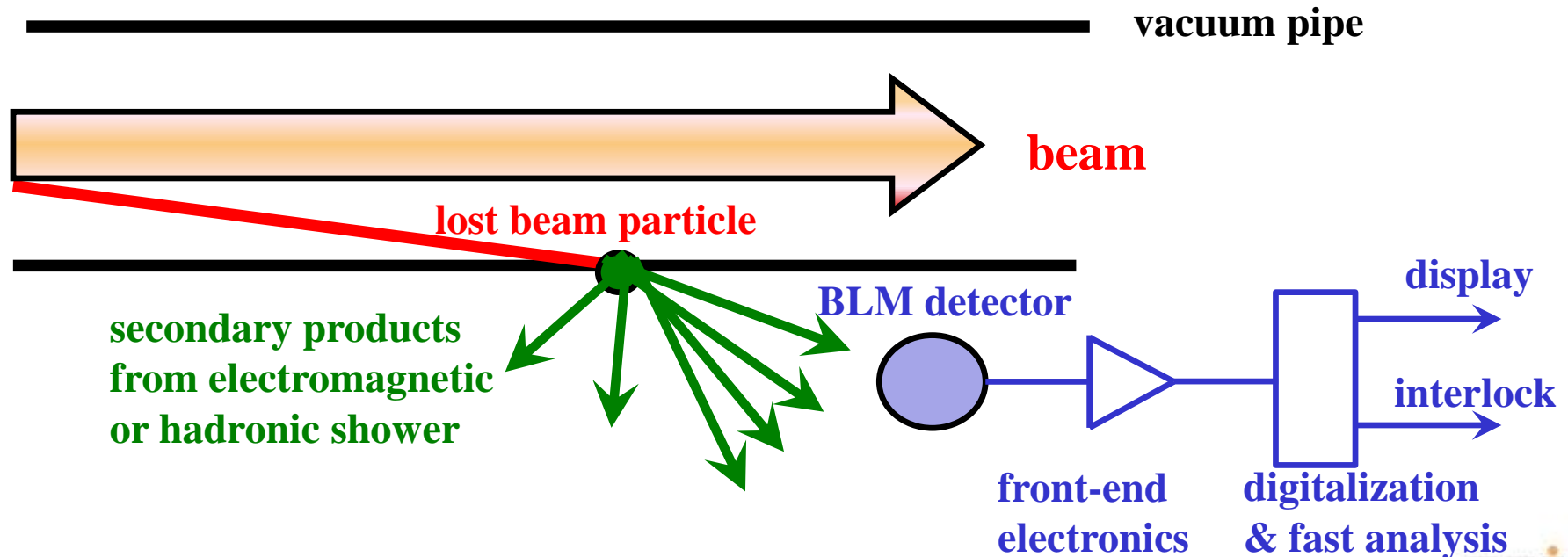
A loss beam particle must collide with the vacuum chamber or other insertions

⇒ Interaction leads to some shower particle:

$e^-$ ,  $\gamma$ , protons, neutrons, excited nuclei, fragmented nuclei

→ detection of these secondaries by an appropriate detector outside of beam pipe

→ relative cheap detector installed at many locations



## Processes for interaction of electrons

For  $E_{kin} > 100$  MeV:

Bremsstrahlungs-photon dominated

$\Rightarrow \gamma \rightarrow e^+ + e^-$  or  $\mu^\pm, \pi^\pm$  ....

$\rightarrow$  electro-magnetic showers

$\Rightarrow$  excitation of

nuclear giant resonances  $E_{res} \approx 6$  MeV

via  $(\gamma, n)$ ,  $(\gamma, p)$  or  $(\gamma, np)$

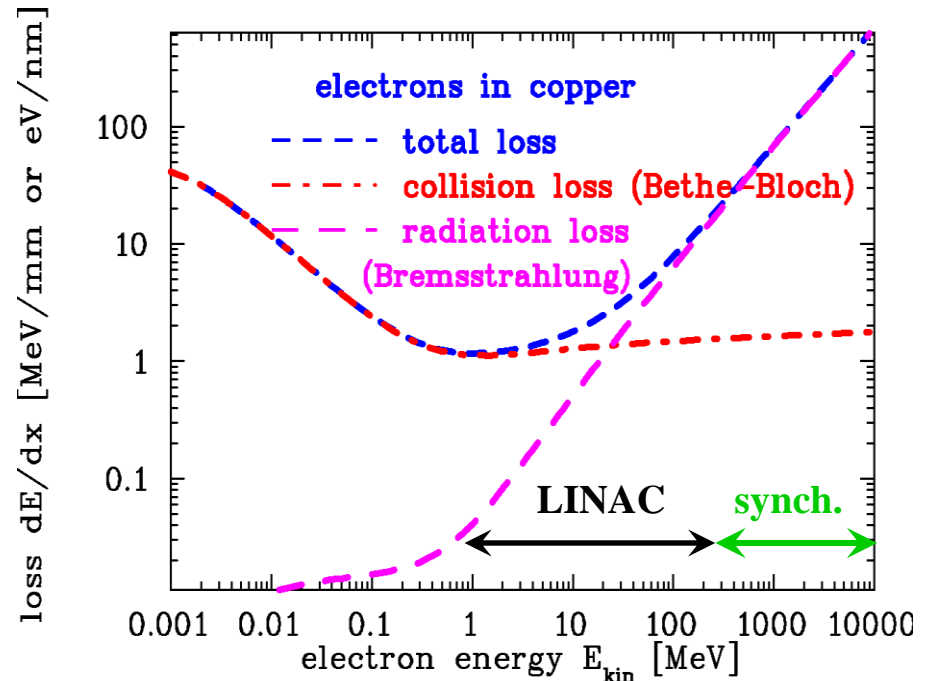
$\rightarrow$  fast neutrons emitted

$\rightarrow$  neutrons: Long ranges in matter due to lack of ele.-mag. interaction.

For  $E_{kin} < 10$  MeV:

$\Rightarrow$  only electronic stopping

(x-rays, slow  $e^-$ ).

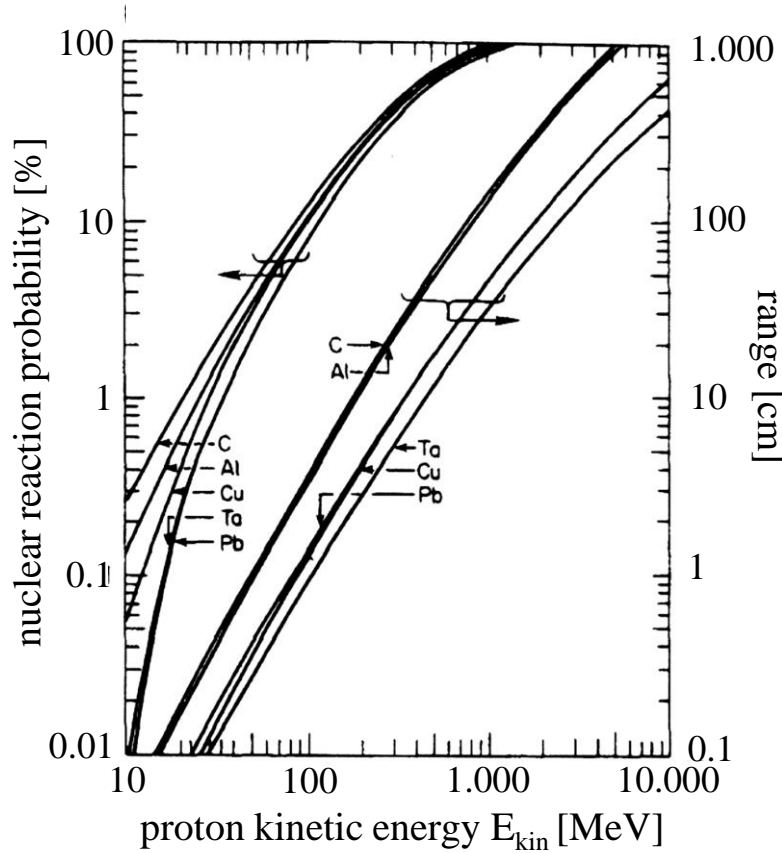




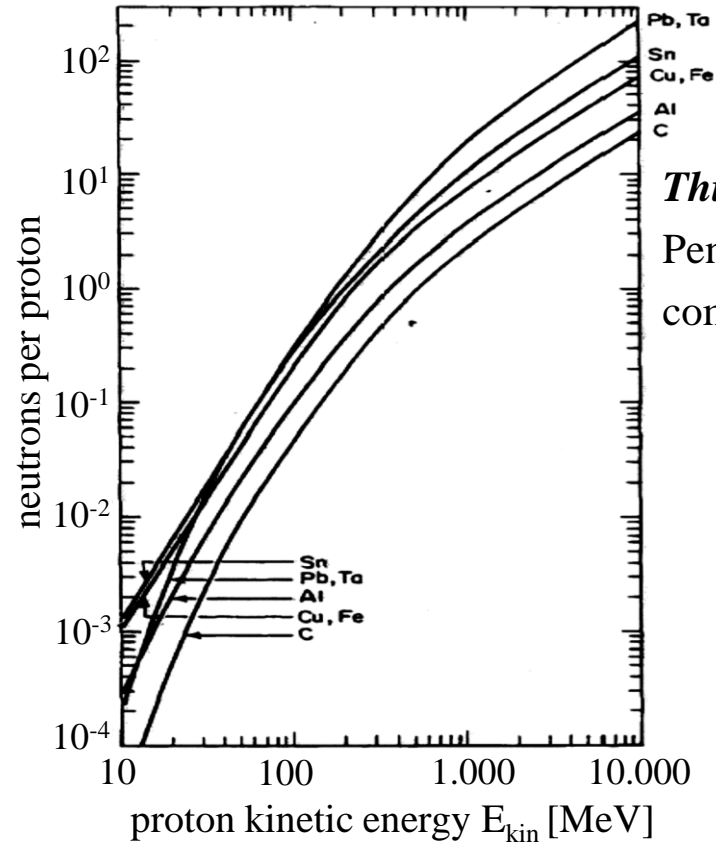
# Secondary Particle Production for Proton Beams



Nuclear reaction probability:



Neutron yield per proton:



⇒ High rate of neutron with broad energy & angular distribution

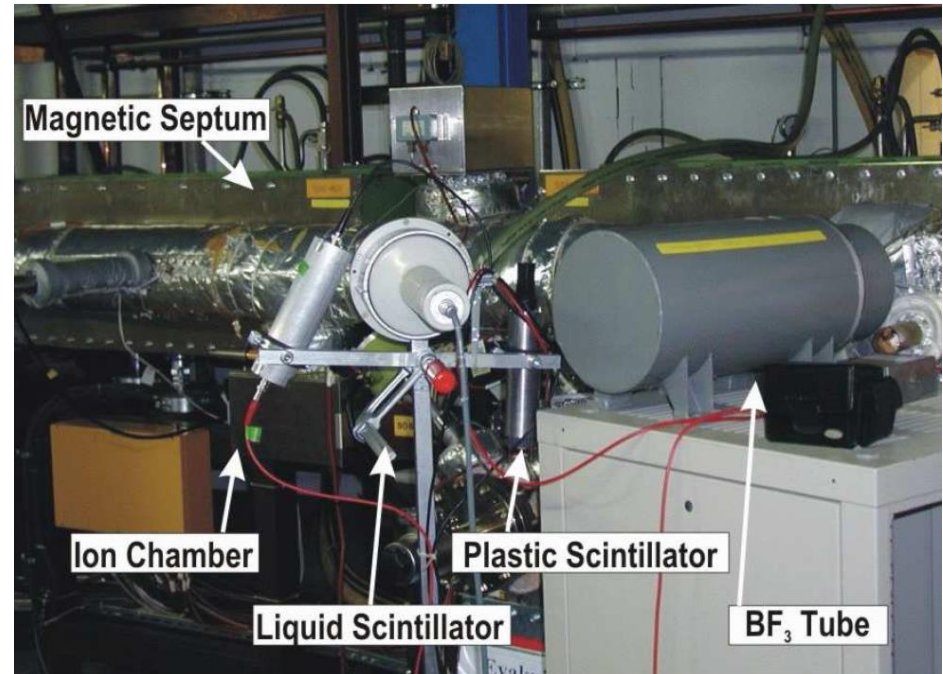
⇒ Role of thumb for protons: Sufficient count rate for beam loss monitoring only for  $E_{kin} \geq 100$  MeV

Courtesy R.H. Thomas, in Handbook on Acc. Phys. & Eng. (ed. A.W. Chao, et al.)



## Outline:

- Physical process from beam-wall interaction
- **Different types of Beam Loss Monitors**  
     **different methods for various beam parameters**
- Machine protection using BLMs
- Summary



# Scintillators as Beam Loss Monitors

## Plastics or liquids are used:

- detection of **charged particles**  
by electronic stopping
- detection of **neutrons**  
by elastic collisions n on p in plastics  
and fast p electronic stopping.

## Scintillator + photo-multiplier:

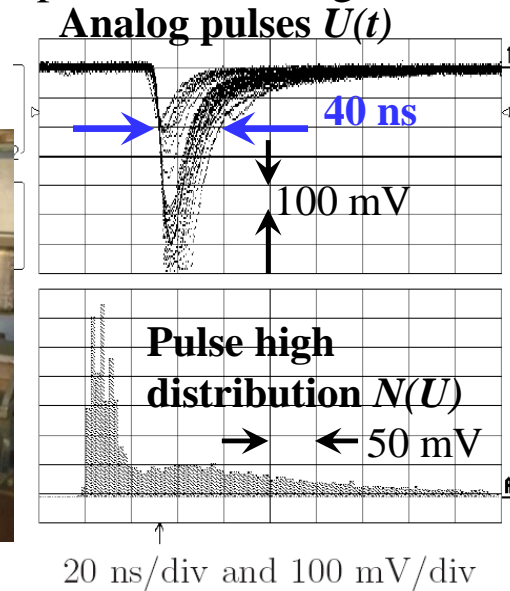
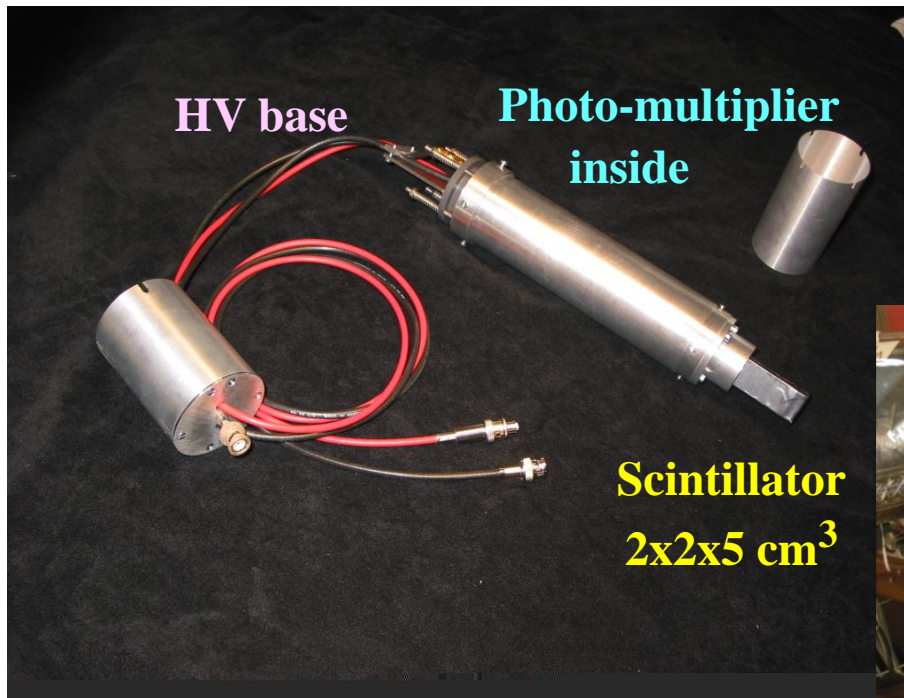
counting (large PMT amplification)  
or analog voltage ADC (low PMT amplification)

Radiation hardness:

plastics 1 Mrad =  $10^4$  Gy

liquid 10 Mrad =  $10^5$  Gy

*Example:* Analog pulses of plastic scintillator:  
⇒ broad energy spectrum  
due to many particle species and energies.



20 ns/div and 100 mV/div

# PIN-Diode (Solid State Detector) as BLM

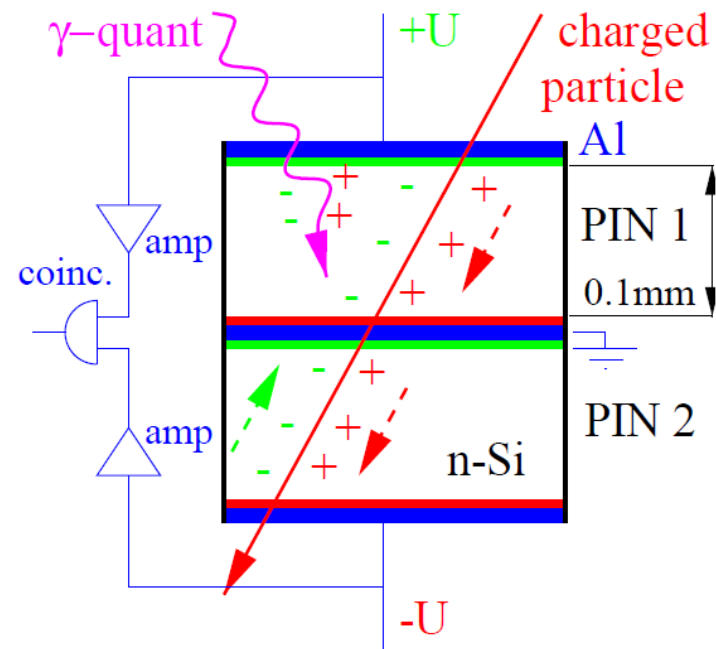
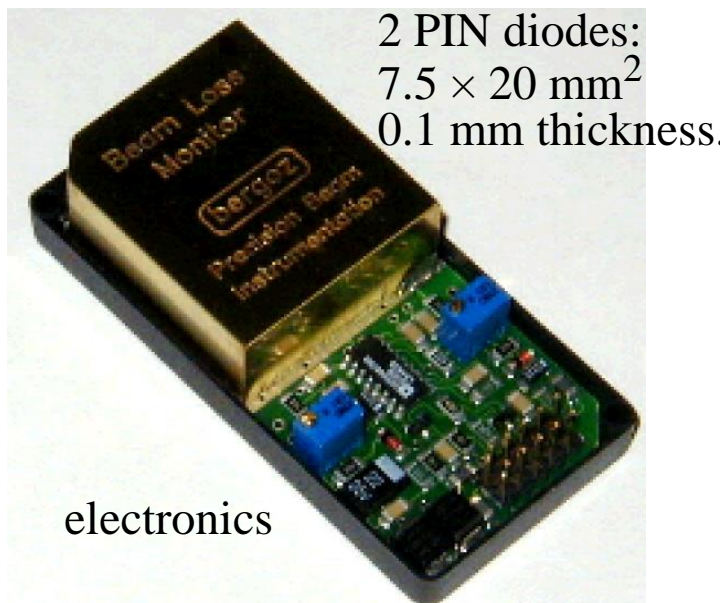


Solid-state detector: Detection of charged particles.

## Working principle

- About  $10^4$  e<sup>-</sup>-hole pairs are created by a Minimum Ionizing Particle (MIP).
- A coincidence of the two PIN reduces the background due to low energy photons.
- A counting module is used with threshold value comparator for alarming.

→ **small and cheap detector.**



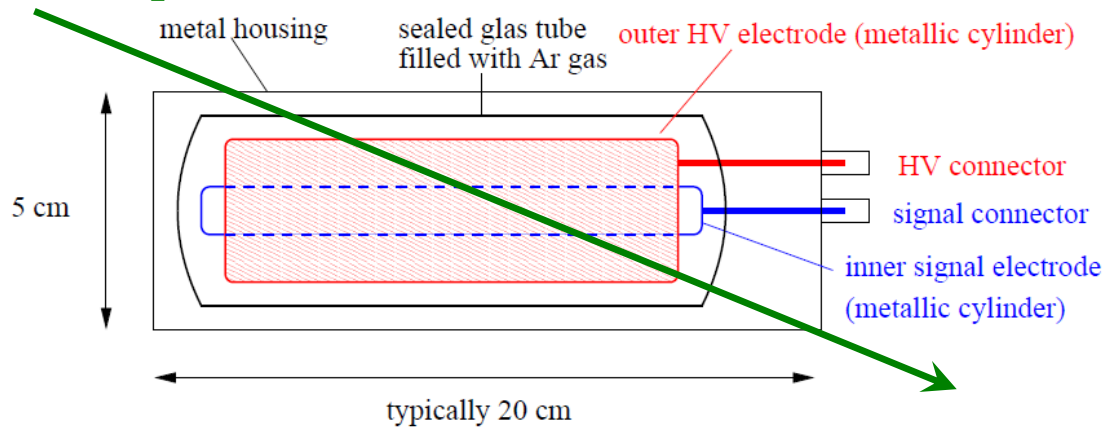
# Excuse: Ionization Chamber (IC)

Energy loss of charged particles in gases → electron-ion pairs → current measurement

$$I_{\text{sec}} \propto \frac{1}{W} \cdot \frac{dE}{dx} \Delta x$$

$W$  is average energy for one  $e^-$ -ion pair:

**shower particle**



Gas	Ionization Pot. [eV]	W-Value [eV]
Ar	15.7	26.4
N <sub>2</sub>	15.5	34.8
O <sub>2</sub>	12.5	30.8
Air		33.8

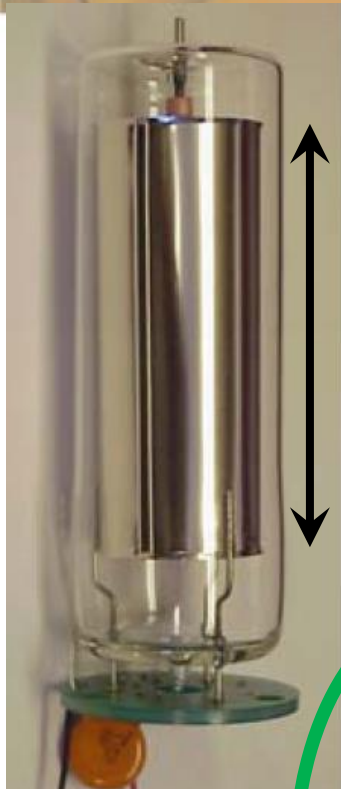
## Sealed tube Filled with Ar or N<sub>2</sub> gas:

- Creation of Ar<sup>+</sup>-e<sup>-</sup> pairs, average energy  $W=32$  eV/pair
- measurement of this current
- Slow time response due to 100 μs drift time of Ar<sup>+</sup>.

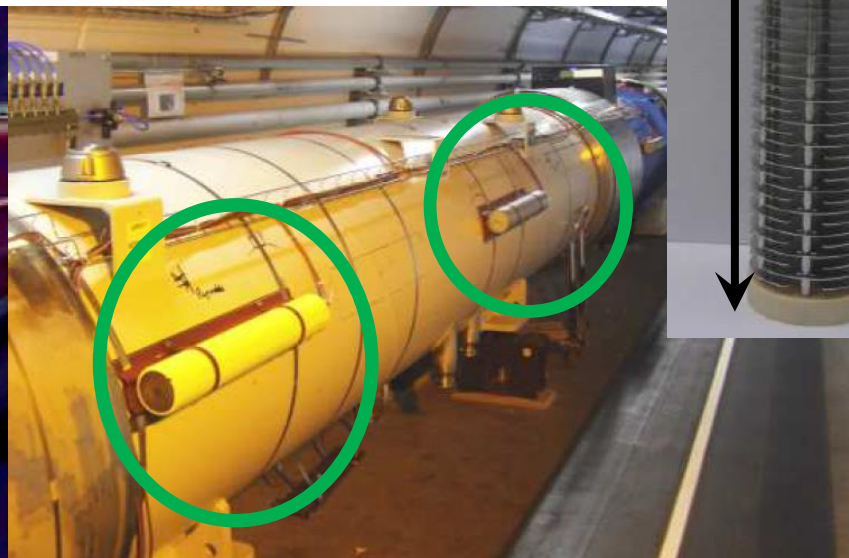
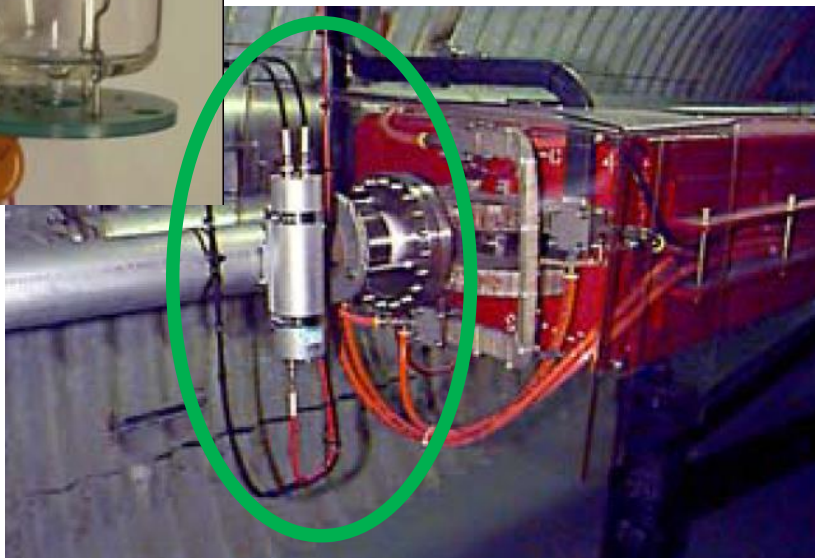
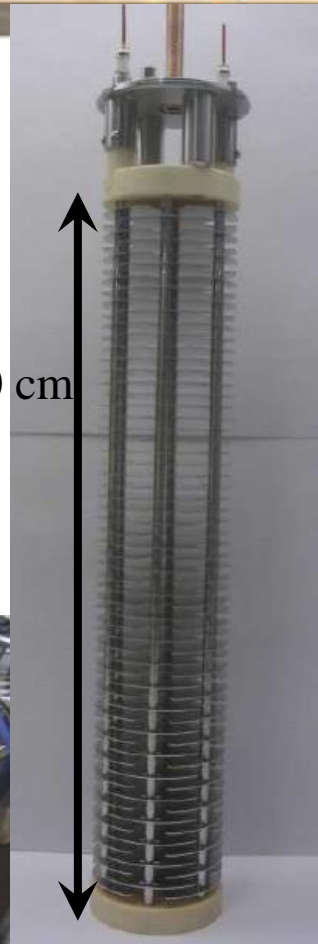
**Per definition: direct measurement of dose.**



# Ionization Chamber as BLM: TEVATRON and CERN Type



TEVATRON, RHIC type	size	CERN type
15cm, $\varnothing$ 6 cm		50 cm, $\varnothing$ 9 cm
Ar at 1.1 bar	<b>gas</b>	N <sub>2</sub> at 1.1 bar
three	<b># of electrodes</b>	61
1000 V	<b>voltage</b>	1500 V
3 $\mu$ s	<b>reaction time</b>	0.3 $\mu$ s
15 cm	<b># at the synchr.</b>	$\approx$ 4000 at LHC
	<b>aver. distance</b>	1 BLM each $\approx$ 6 m



# Secondary Electron Monitor as BLM

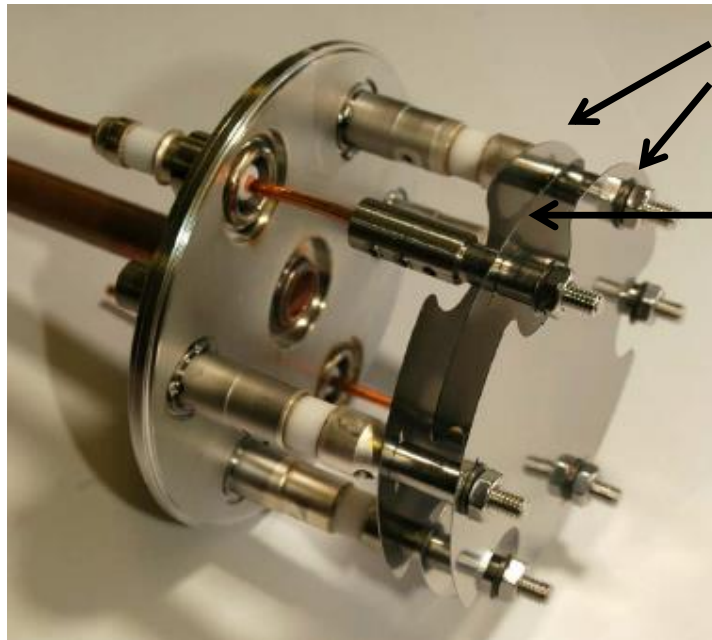


Ionizing radiation liberates secondary electrons from a surface.

Working principle:

- Three plates mounted in a vacuum vessel (passively NEG pumped)
- Outer electrodes: biased by  $U \approx +1$  kV
- Inner electrode: connected for current measurement (here current-frequency converter)

→ **small and cheap detector, very insensitive.**



HV electrodes

Electrode for  
measured  
current

Detector with intrinsic amplification:  
Secondary electron multiplier  
i.e. a ‘photo-multiplier without  
photo-cathode’

# Comparison of different Types of BLMs



Different detectors are sensitive to various physical processes  
very different count rate, but basically proportional to each other

⇒ **Linear behavior for all detectors**

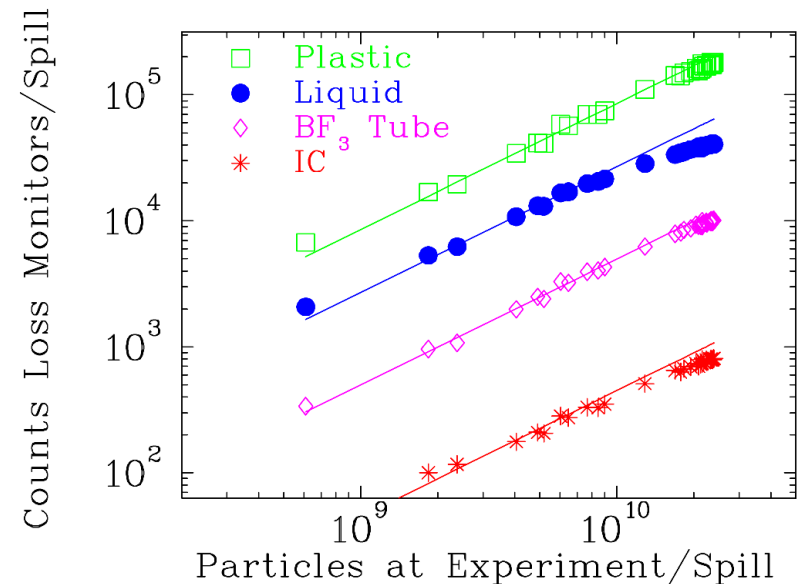
but quite different count rate:

$$r_{\text{IC}} < r_{\text{BF}_3} < r_{\text{liquid}} < r_{\text{plastic}}$$

Choice of the detector type:

- IC:
  - measurement of absolute dose
  - low signal, sometimes slow
- PIN-diode, scintillator or diamond detector:
  - fast due to particle counting
  - might need calibration

*Example:* Beam loss for 800 MeV/u O<sup>8+</sup>  
determined different BLMs at GSI-synchr.:



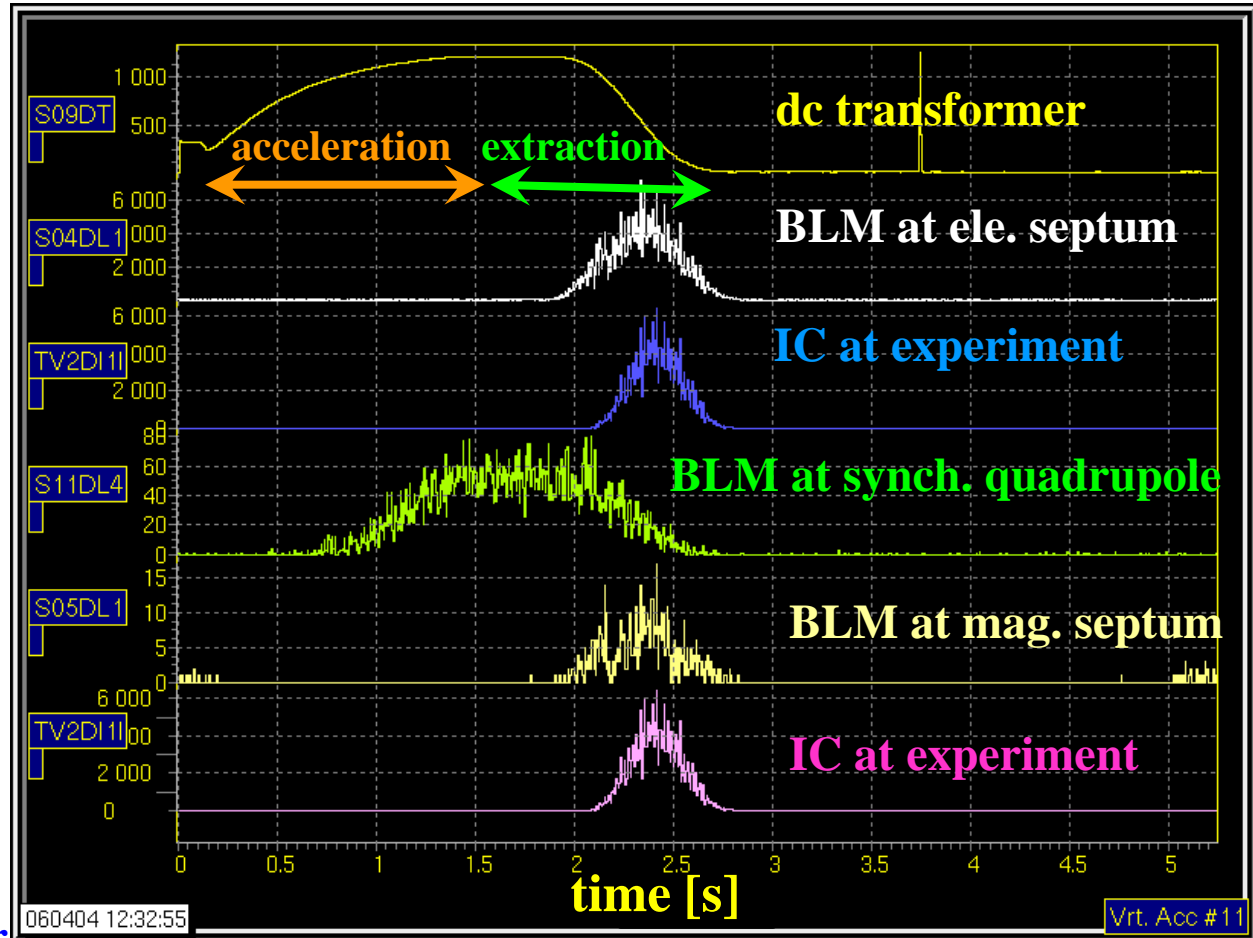
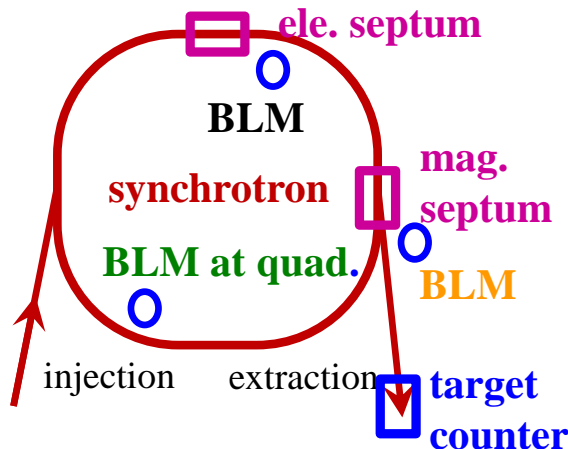


# Application of BLMs for slow Extraction: Time Dependence

BLM are cheap and can be installed at several locations and determine local loss:

Example at SIS synchr. using quadrupole variation for slow extraction:

- Losses during acceleration
  - Losses at ele. septum
  - Momentum dependent extraction current  
⇒ change of extraction angle  
⇔ time-dependent losses at mag. septum
- ⇒ used for optimization of time-dep. extraction angle

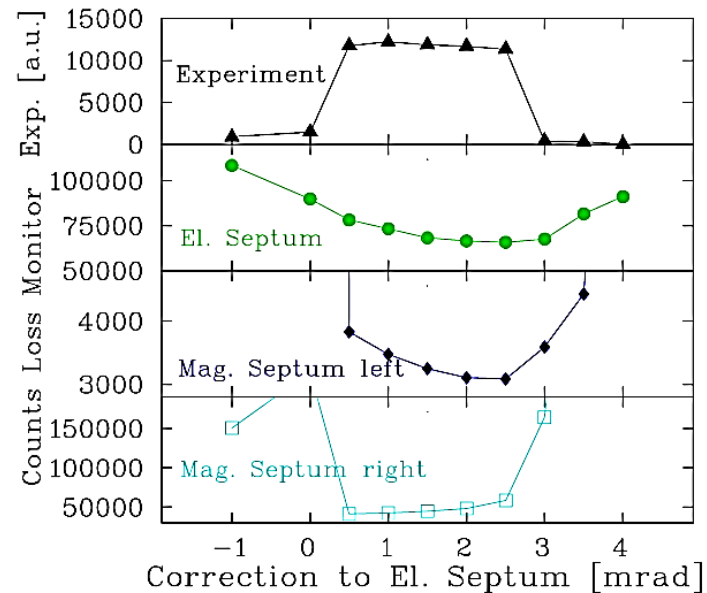
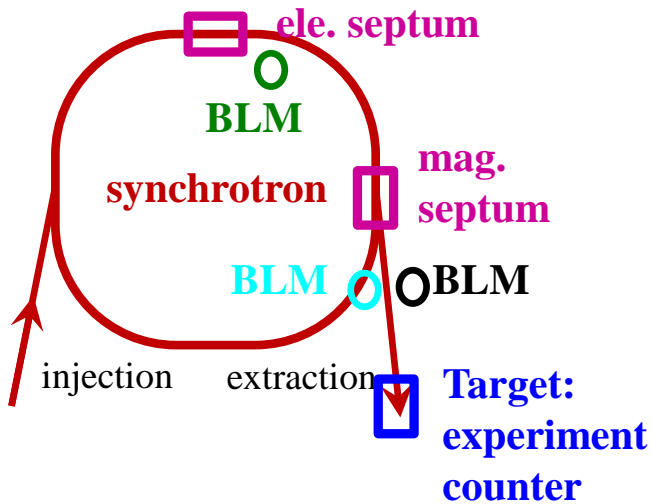
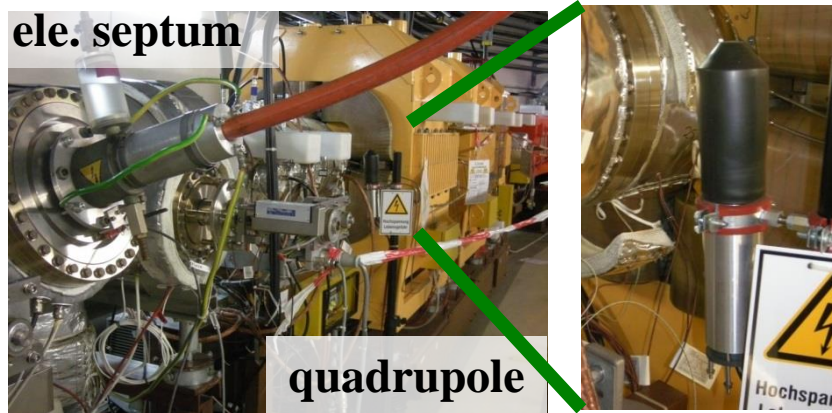


# Application of BLMs for slow Extraction: Transfer Line Alignment



**Example:** Counts per spill from scintillators

at different location for optimization of extraction efficiency and transmission to target:



## Advantage:

- very sensitive device for optimization
- cheap monitors mounted at many locations outside the vacuum pipe

Losses lead to permanent activation  $\Rightarrow$  maintenance is hampered  
and to material heating (vacuum pipe, super-cond. magnet etc.)  $\Rightarrow$  destruction.

## Types of losses:

- **Irregular** or fast losses by malfunction of devices (magnets, cavities etc.)  
→ BLM as online control of the accelerator functionality and **interlock generation**.
- **Regular** or slow losses e.g. at collimator, by lifetime inside synchrotron or slow extraction  
→ BLM used for alignment

## Demands for BLM:

- **High sensitivity** to detect behavior of beam halo e.g. at collimator
- **Large dynamic range:**
  - low signal during normal operation, but large signal in case of malfunction
  - detectable without changing the full-scale-range  
e.g. scintillators from  $10^2$  1/s up to  $10^7$  1/s in counting mode.

Monitoring of loss rate in control room *and* as interlock signal for beam abortion.

## Measurement of the lost fraction of the beam:

- detection of secondary products
- sensitive particle detectors are used outside the vacuum
- cheap installations used at many locations

**Used as interlock in all high current machines for protection.**

**Additionally used for sensitive ‘loss studies’.**

**Depending on the application different types are used:**

### Frequently used:

- **Scintillators:** very sensitive, fast response, largest dynamics, not radiation hard
- **PIN diode:** insensitive, fast response, not radiation hard, cheap
- **IC:** medium sensitive, slow response, radiation hard, cheap, **absolute measurement of dose**
- **SEM:** very in-sensitive, i.e. suited for high radiation area, fast radiation hard, cheap

Further types are used: electron multiplier,  $\text{BF}_3$  neutron counter, cable-based IC, optical fibers....

**Thank you for your attention!**