



Improved anchoring of SSS with vacuum barrier to avoid displacement

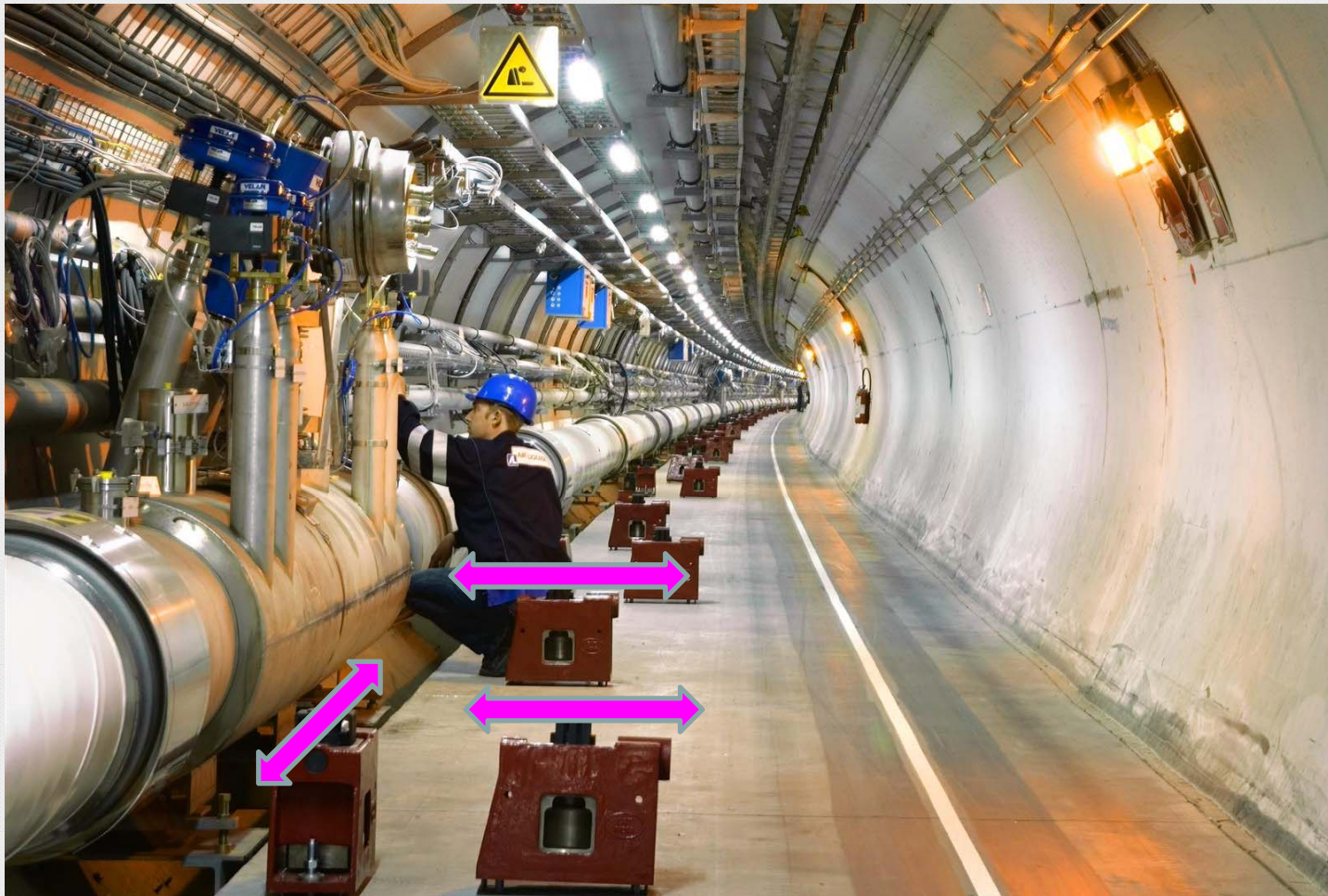
Ofelia Capatina (speaker), Katy Foraz (coordinates all the activities),
Antonio Foreste, Vittorio Parma, Thierry Renaglia, Jean-Pierre Quesnel

- Introduction
- Initial requirements and actual SSS supporting
- Updated requirements and improved supporting design
- Planning and costs
- Next weak point?
- Conclusion

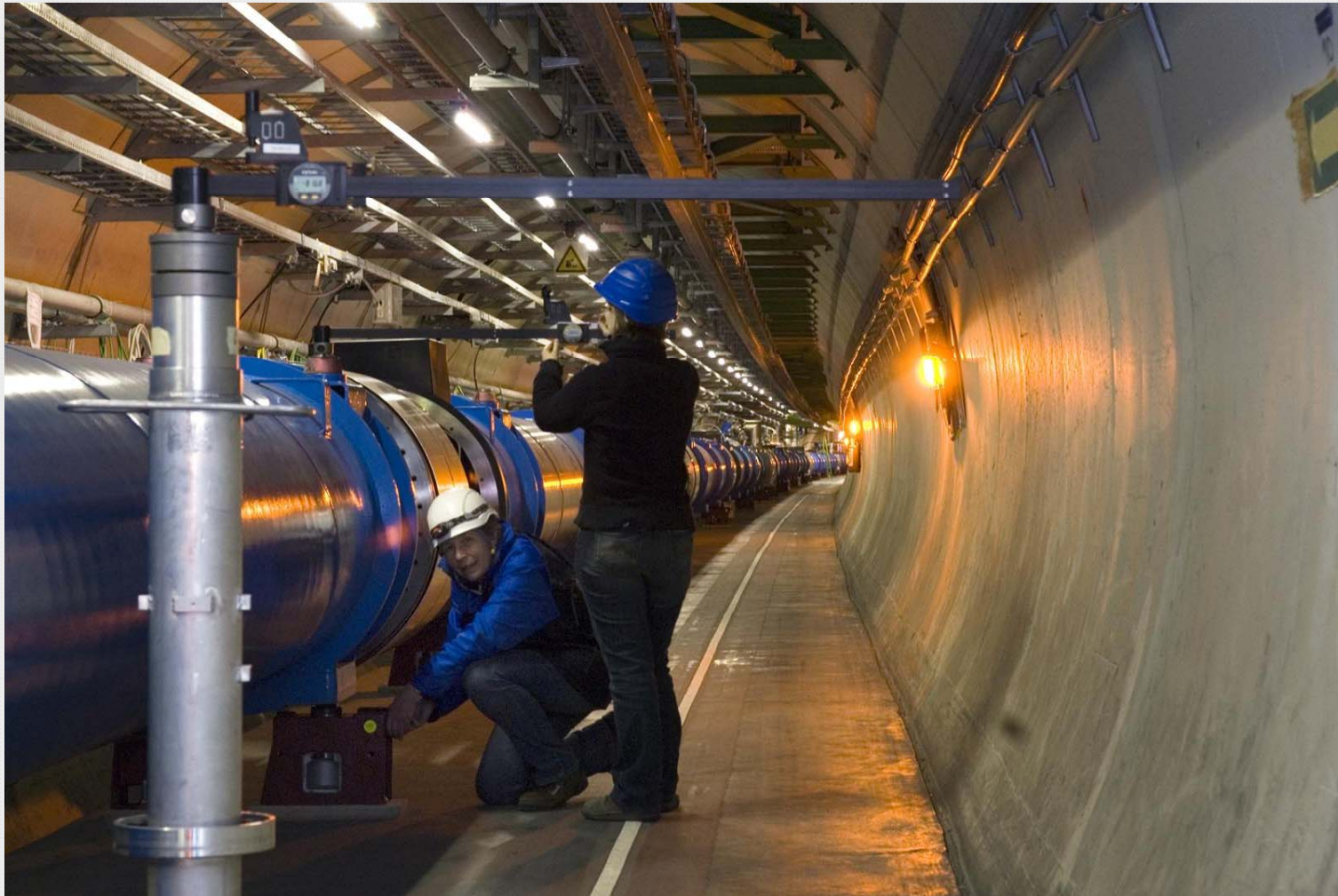
- Incident on 19th of September 2008 => failure of some supports of SSS in sector 3-4 due to longitudinal loads



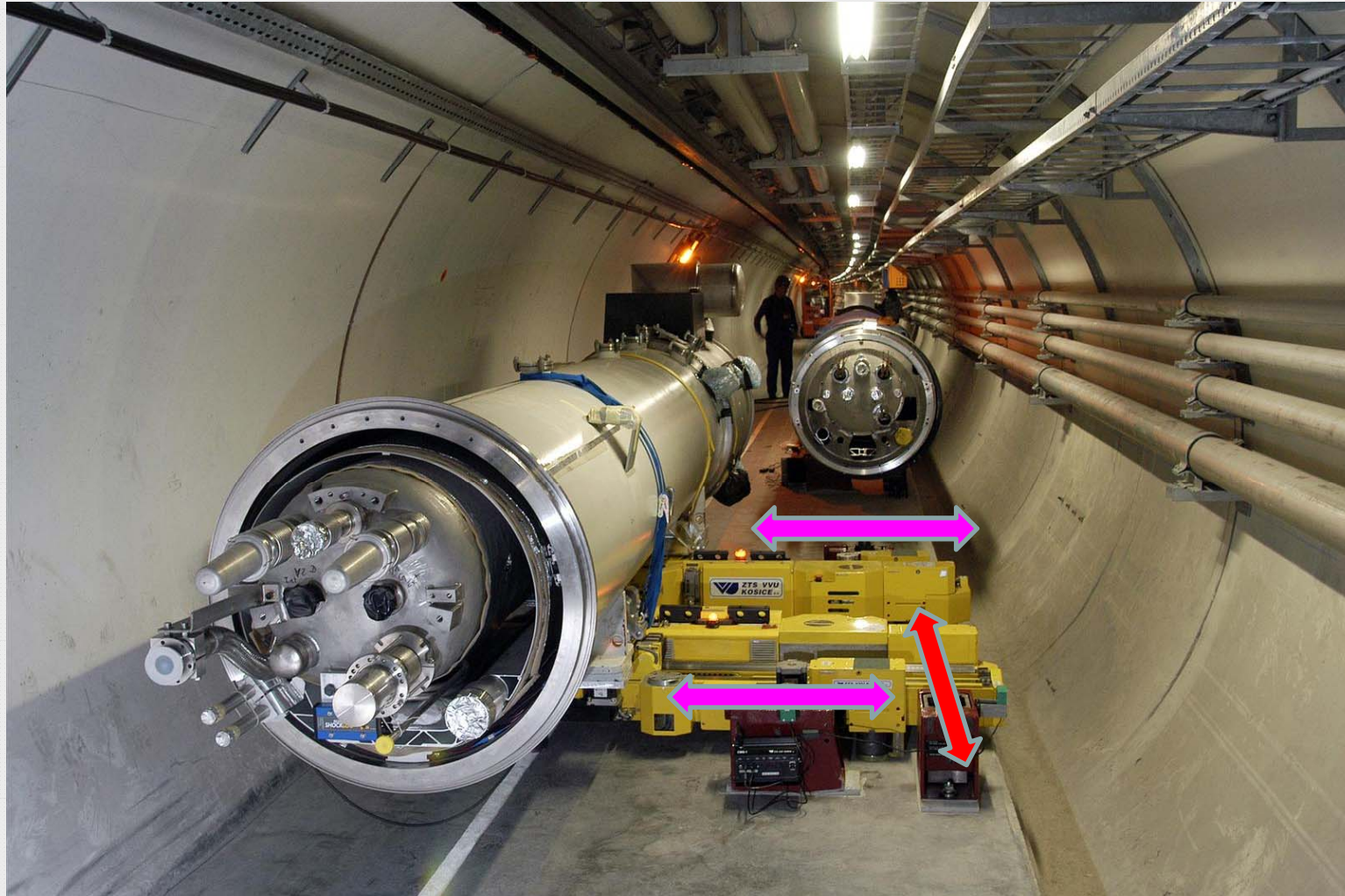
- Each SSS is installed on 1 jacks for longitudinal alignment + 2 for transversal alignment; The 3 jacks are used for vertical alignment





- Alignment done by geometers after installation



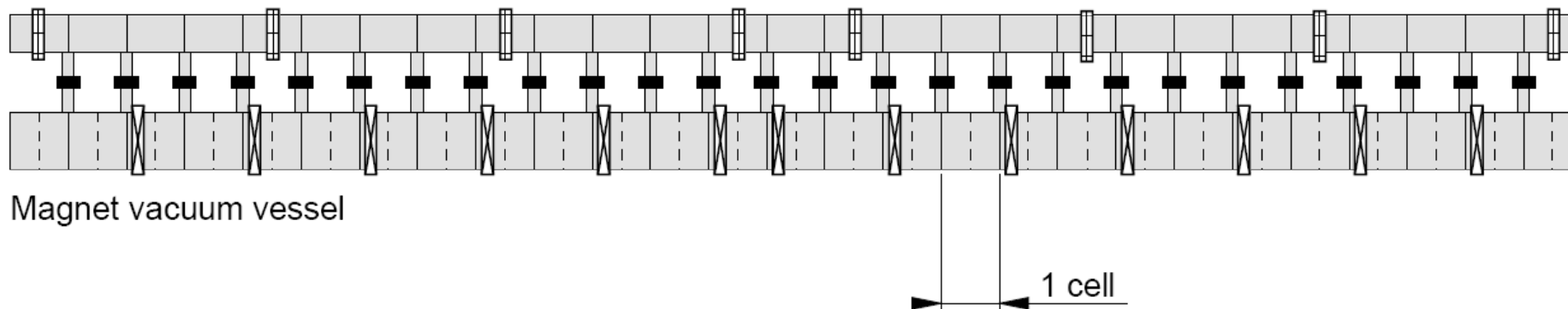
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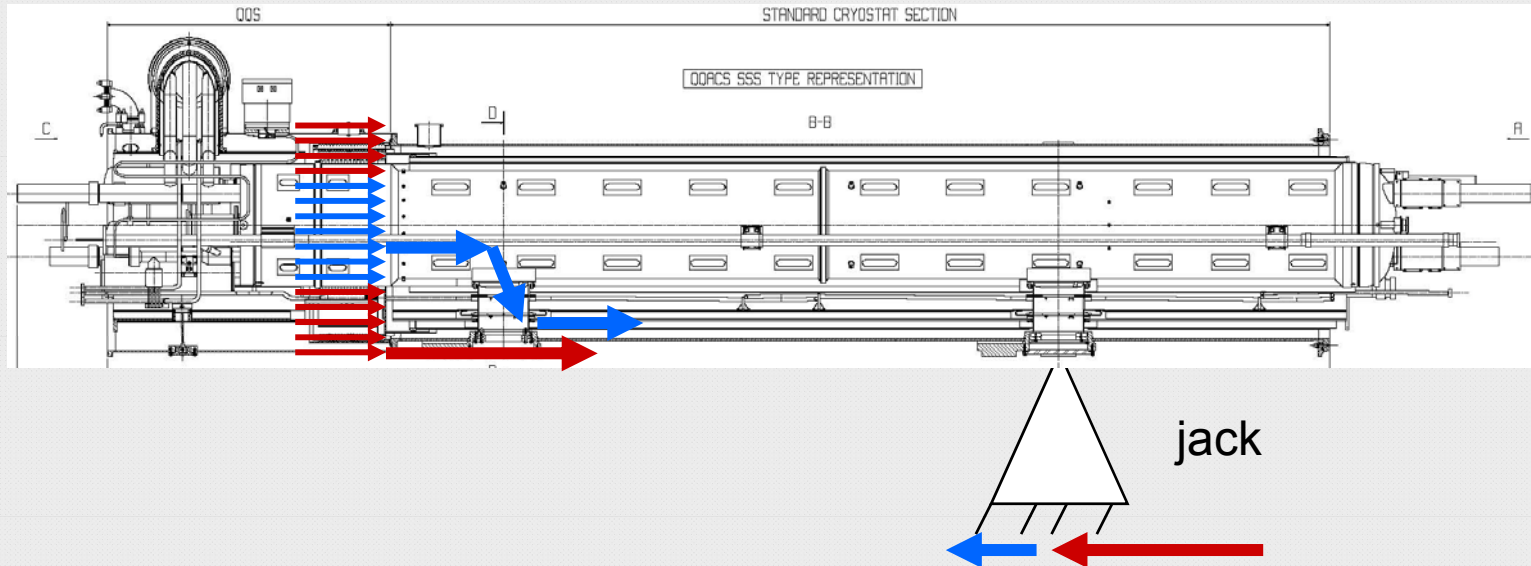
- Vacuum sectorisation for one LHC sector

Vacuum sectorization:  Magnet vacuum barriers  Jumper vacuum barriers  QRL vacuum barriers

QRL vacuum jacket



- Vacuum barrier in 13 SSS / sector (Q11R&L, Q15R&L, Q19R&L, Q23R&L, Q27R&L, Q31R&L, Q33R)
- A total of 104 SSS with vacuum barrier



- Vacuum vessel/vacuum barrier designed for **0.15 MPa internal pressure**
- Supporting system should withstand loads induced by differential pressure on both sides of vacuum barrier:
 - Nominal operation: up to $\Delta p = 0.1 \text{ MPa}$
 - Exceptional : up to $\Delta p = 0.15 \text{ MPa}$
- $\Delta p = 0.1 \text{ MPa}$ across vac. Barrier $\rightarrow 80 \text{ kN}$ at the jacks (tested value)

- Supporting system should withstand
 - Nominal operation up to **80 kN** longitudinally (\equiv **0.1 MPa**)
 - Exceptional operation up to **120 kN** longitudinally (\equiv **0.15 MPa**)
- Actual SSS supporting system:
 - Designed for **80 kN** and tested in the tunnel for a longitudinal load up to **90 kN**
 - Test done once in surface building up to **120 kN** (not documented)



Sonia Bartolome et al., tests done in the LHC tunnel, June 2003

- Actual SSS supporting system:
 - Tested failure tensile loads of anchors **120 kN to 150 kN**
 - Ok for nominal operation
 - Failure limit for exceptional conditions (**~ 150 kN**)
 - No concrete damage observed

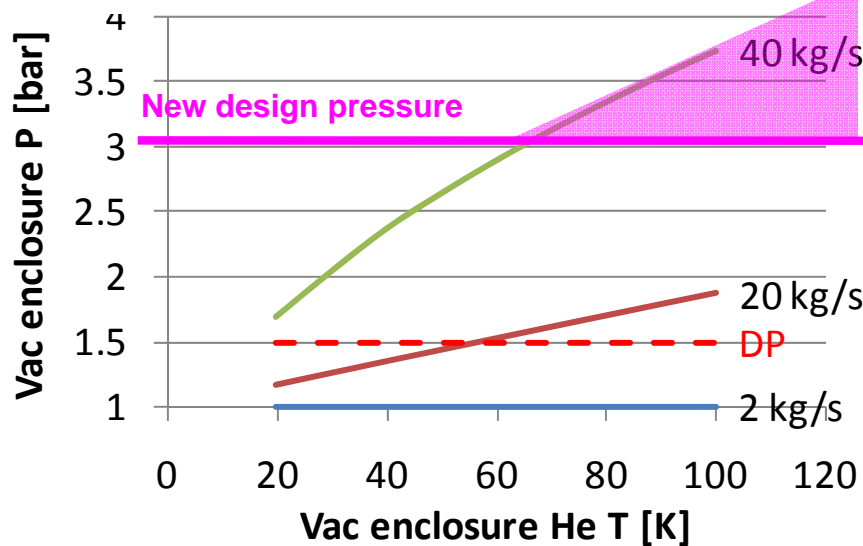


- Sect.3-4 incident: estimate (see pres. Ph. Lebrun session 01) pressure inside vessels (on one side of vacuum barrier): **0.7 MPa (x 4.6 design pressure)**
 - => Improvements of security relief valves proposed (see pres. V. Parma session 04) different form warm / cold sectors
- Updated design pressure (see pres. V. Parma session 04)

New configuration on cold sectors:

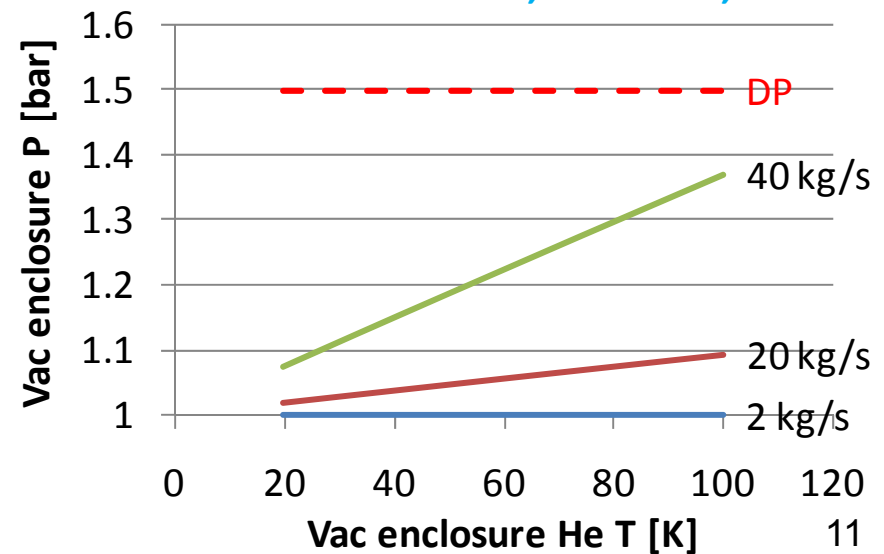
13 DN100, 2 DN90, 4 DN63

(DP: Design Pressure)



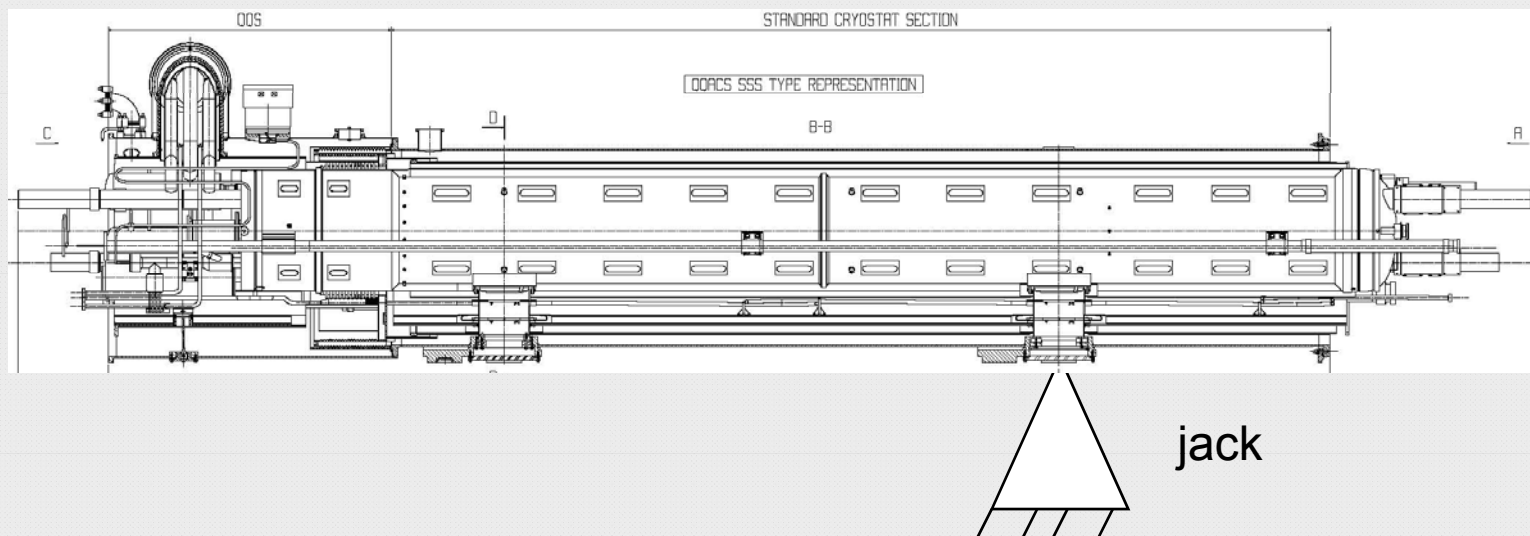
New configuration on warm sectors:

12 DN200, 4 DN100, 2 DN90



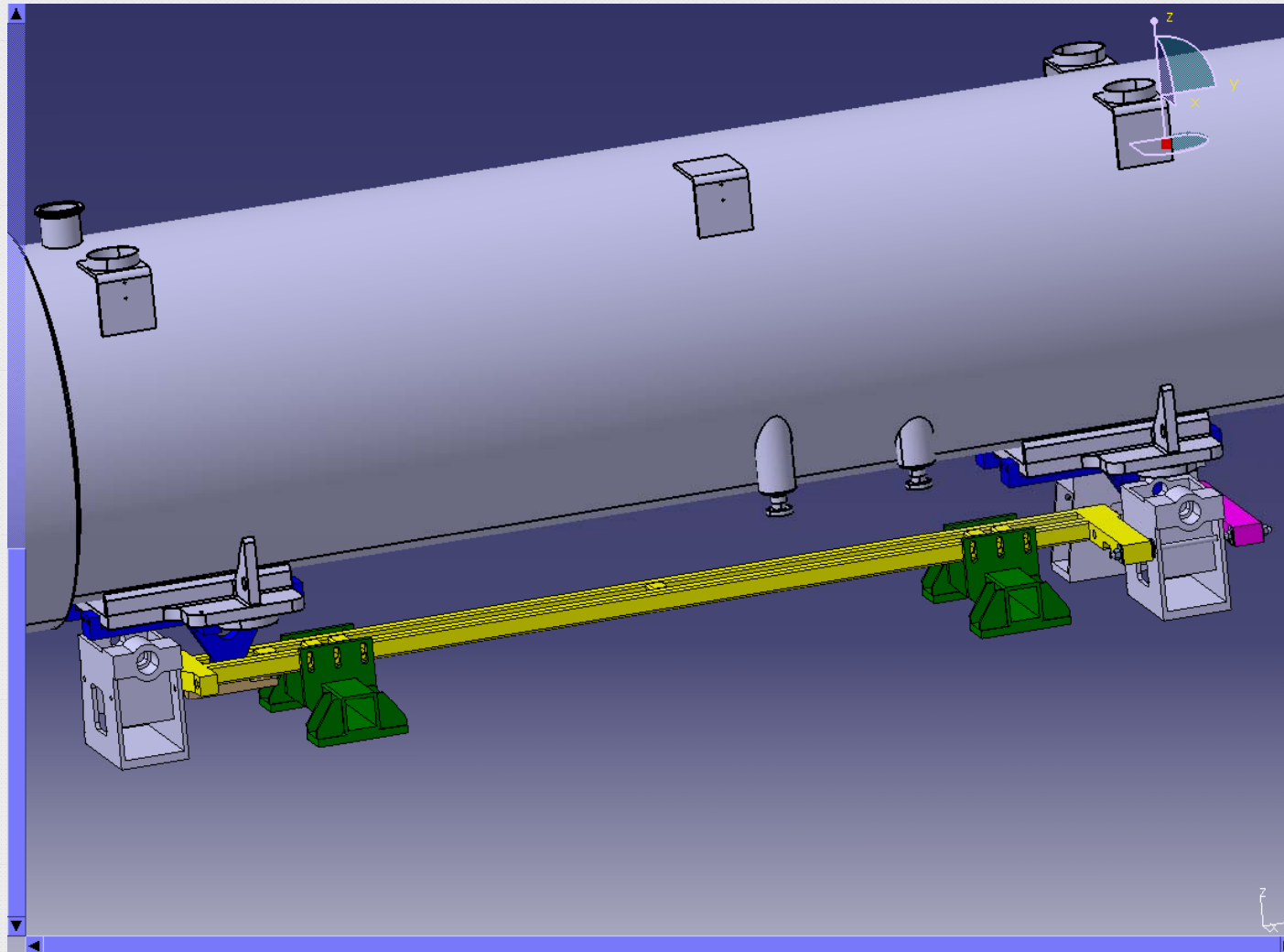
Updated requirements and improved SSS supporting

- Updated design pressure **0.3 MPa** for SSS anchoring. Why?
 - Covers an important area of possible events
 - Very high but feasible value of longitudinal loads to be considered for the new anchor design - **240 kN**;
 - The chain of elements **vacuum barrier / cold foot / jack** should be equilibrated
 - Design of vacuum barrier for **0.15 MPa** with security factor **3** => confident that it withstands **0.3 MPa**
 - Cold foot tests showed no failure up to **70 kN** equivalent to **0.3 MPa**

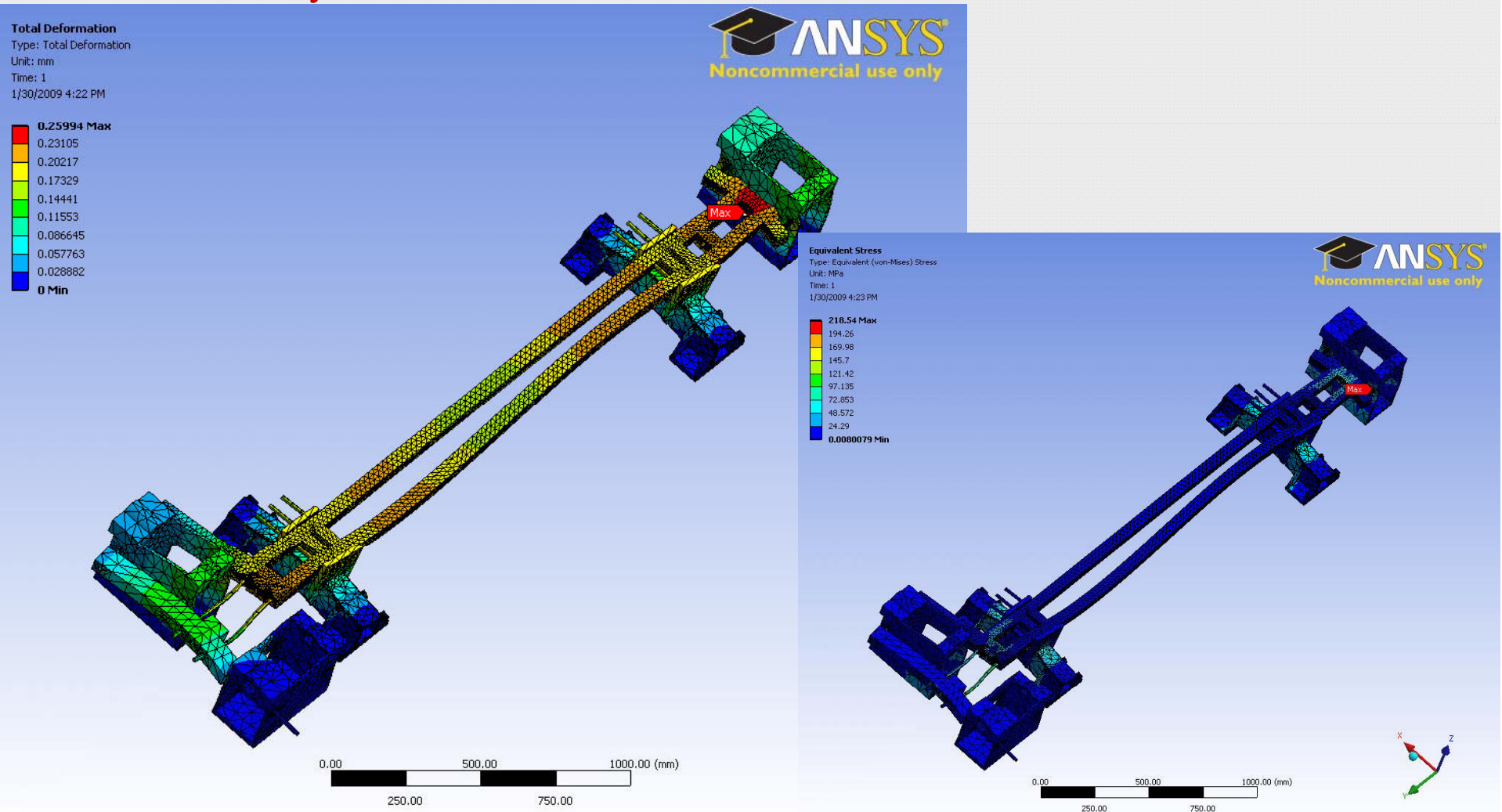


- Requirements for the design of the improved SSS anchors
 - Withstand longitudinal load of **240 kN**
 - Possibility to install the system on SSS already on jacks
 - Reduced space under the SSS – very difficult for drilling
 - Accessibility for alignment
 - Estimation of realignment every year
 - Allow thermal contraction of vacuum tank in case of accident
 - Allow space for other foreseen equipment under the SSS
 - Uninstalling the system should allow SSS removal if needed
 - Transport / installation zones to be taken into account
 - Optimize price
 - Feasibility within general planning

- Several solutions have been studied
 - 1st solution – distribution of the longitudinal load among the 3 jacks

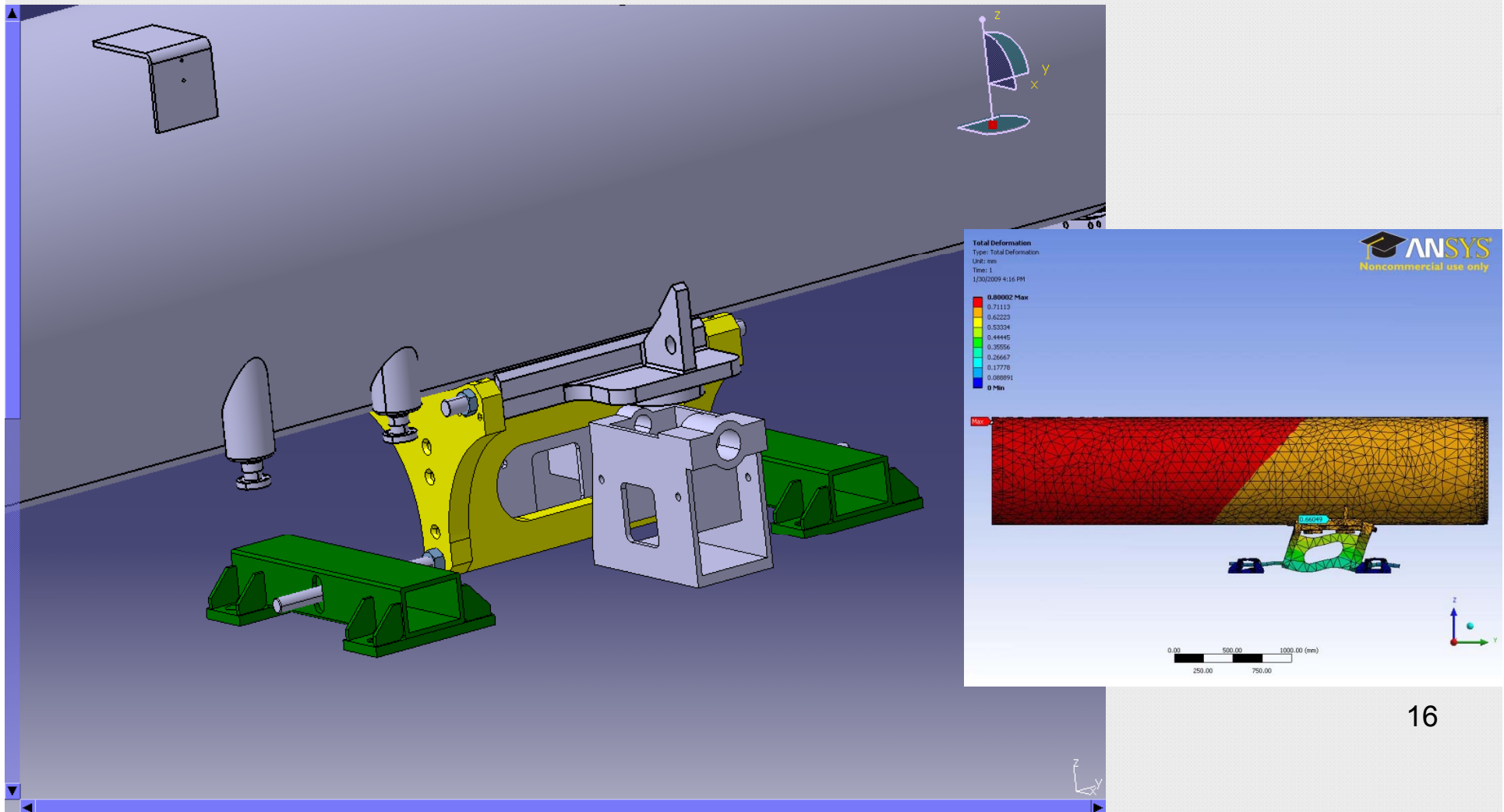


- Several solutions have been studied
 - 1st solution – distribution of the longitudinal load among the 3 jacks
 - **No cryostat thermal contraction allowed**



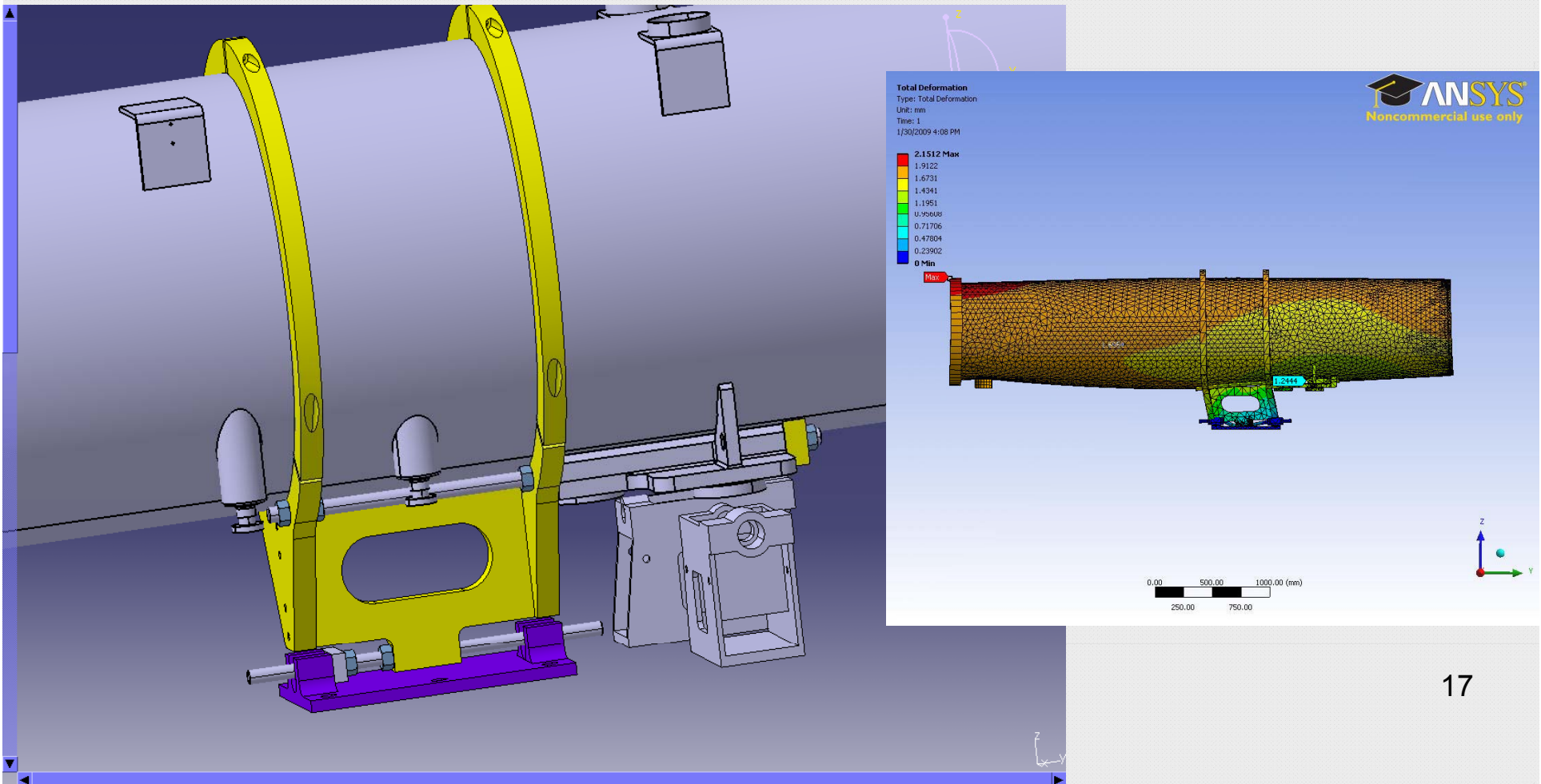
Updated requirements and improved SSS supporting

- 2nd solution – bloc additional fixation to the ground – only shear loads transmitted to the floor
- **Poor accessibility to jacks for alignment**

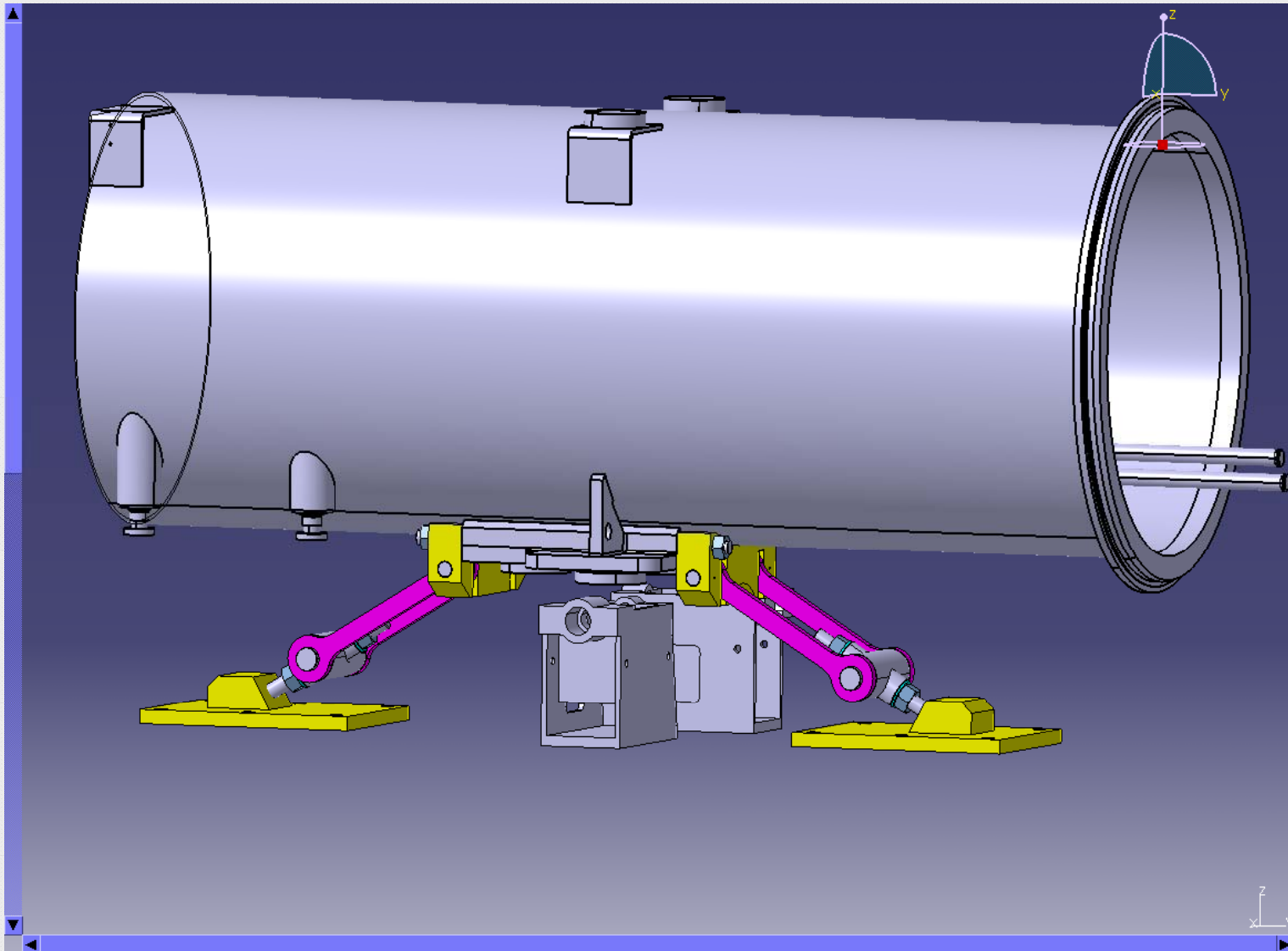


Updated requirements and improved SSS supporting

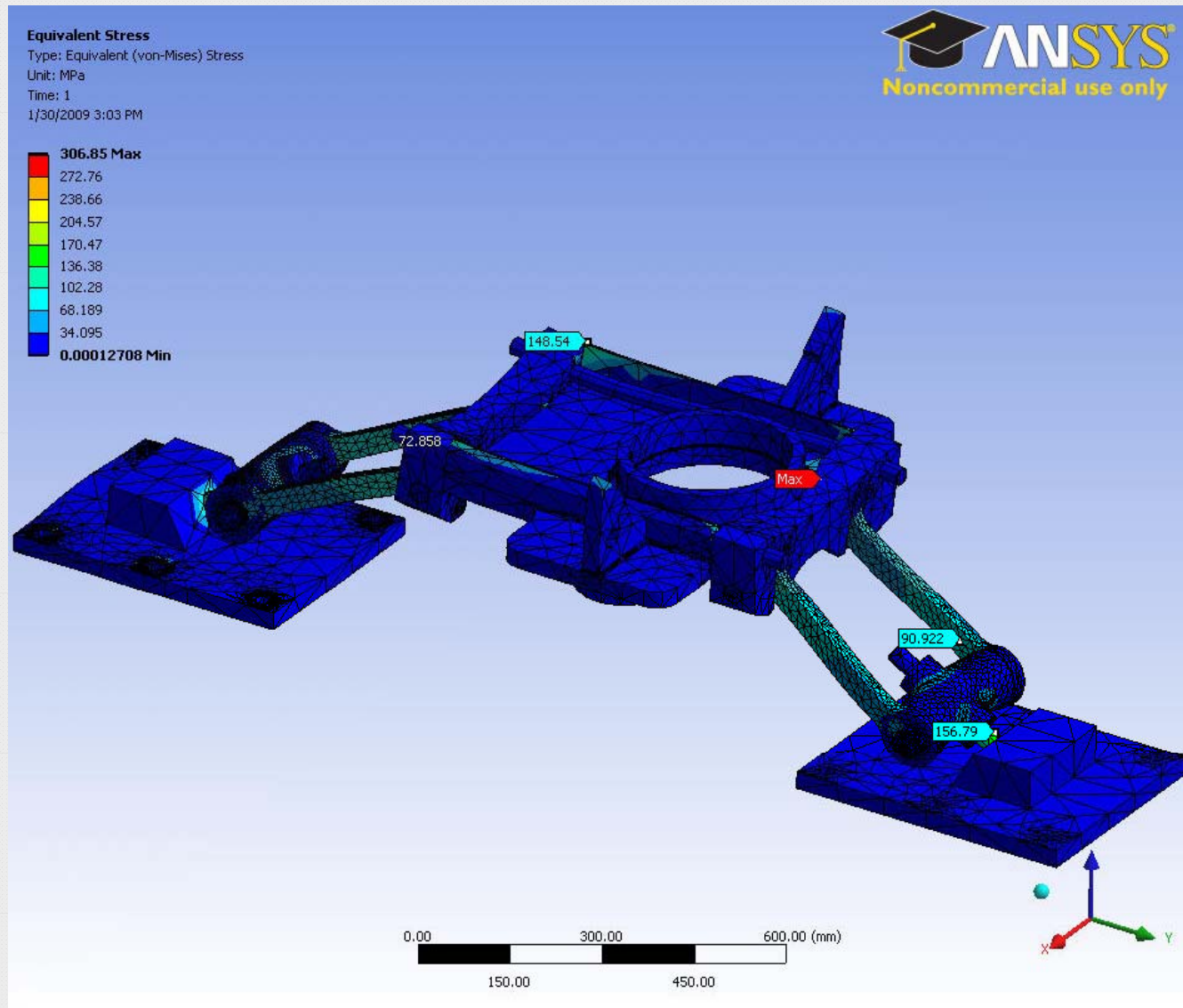
- 3rd solution – bloc additional fixation to the ground and to the cryostat – only shear loads transmitted to the floor
- **Necessitates special installation procedure (monitored by geometers) to avoid vacuum tank deformation**



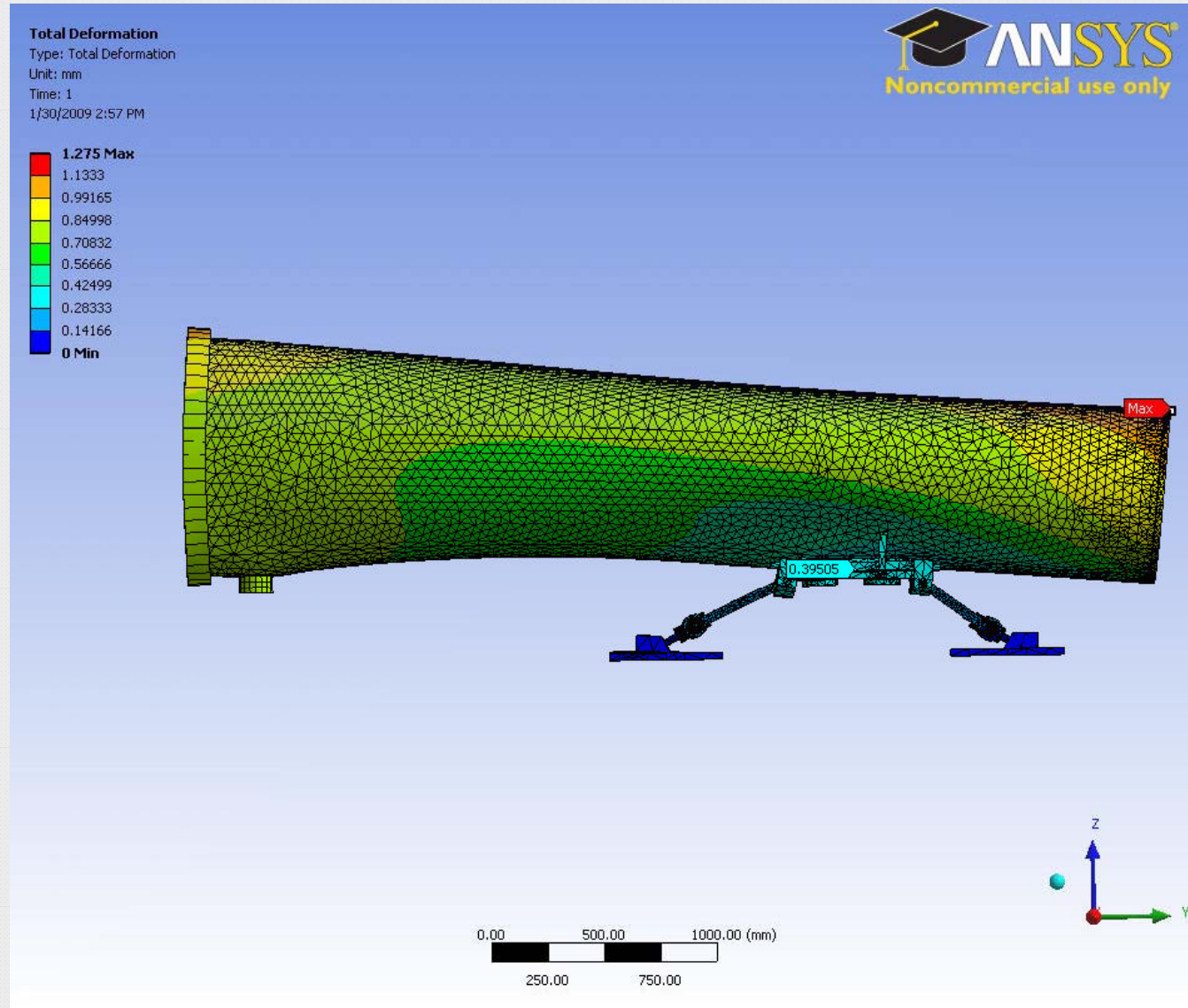
- 4rd solution – the final one



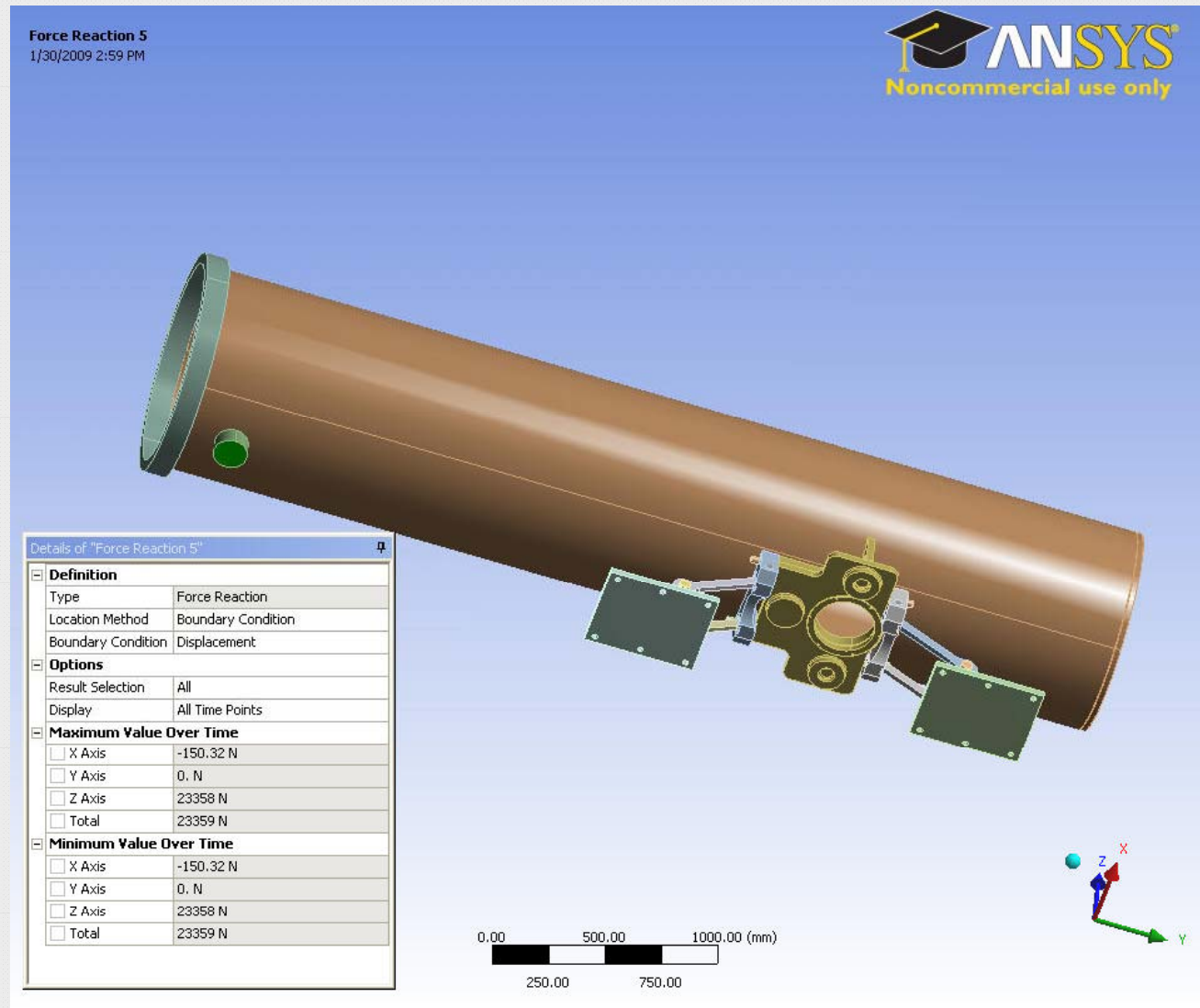
- Final solution – equivalent stress



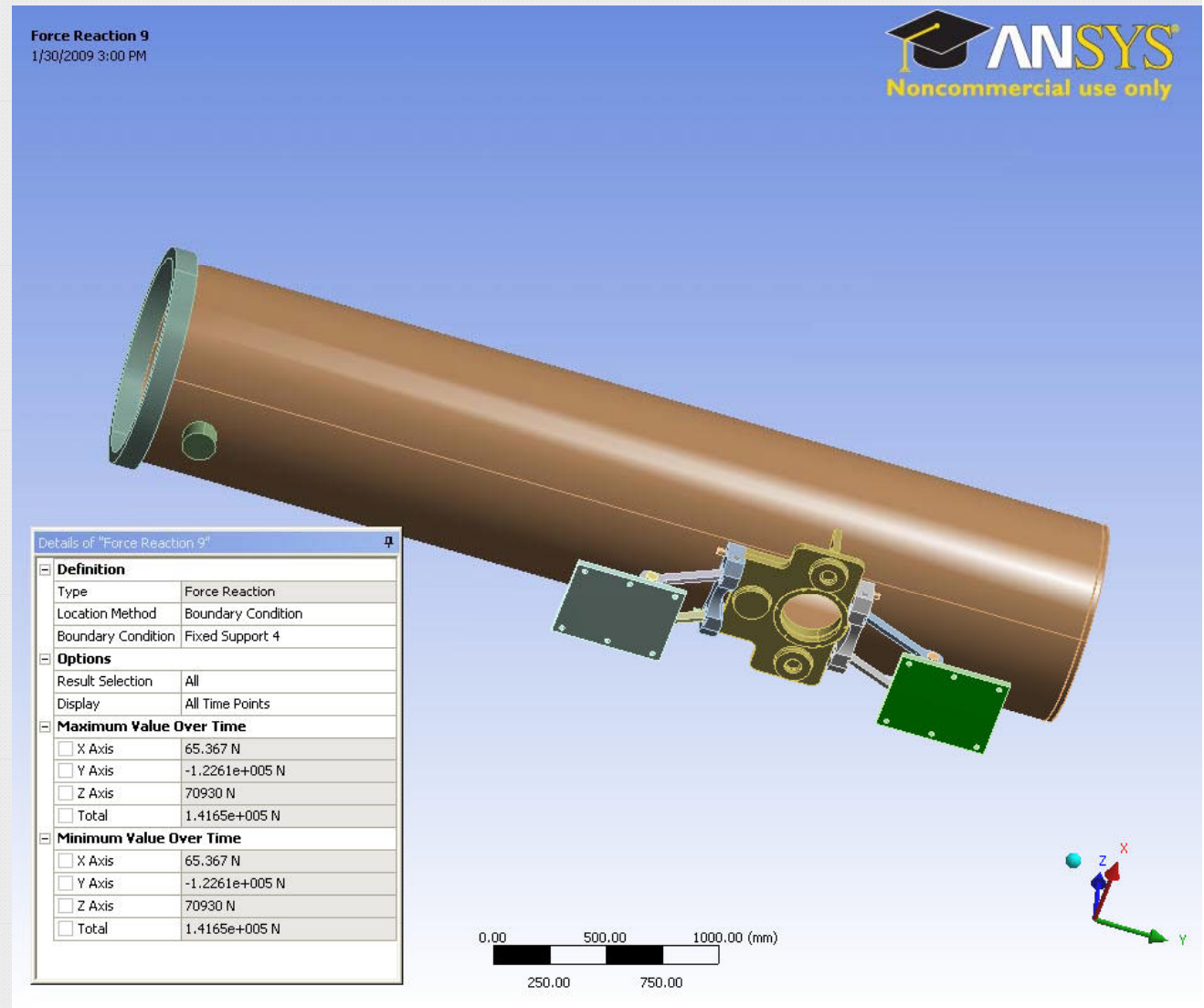
– Final solution – deformation



- Final solution – reaction loads
- Contact on single jack guaranteed



- Final solution – reaction loads
- Ground fixation system tested this morning in SX4



- Final solution – one ground fixation system tested in SX4
- Up to **380 kN** applied longitudinally and **230 kN** applied vertically (traction) during **10 min** (1.5 x design load if only one side charged)
=> no visible damage observed



M. Guinchard and A. Foreste, tests done in SX4, February 2009

- Prototype
 - Manufacturing complete prototype w7-8
 - Test prototype w9

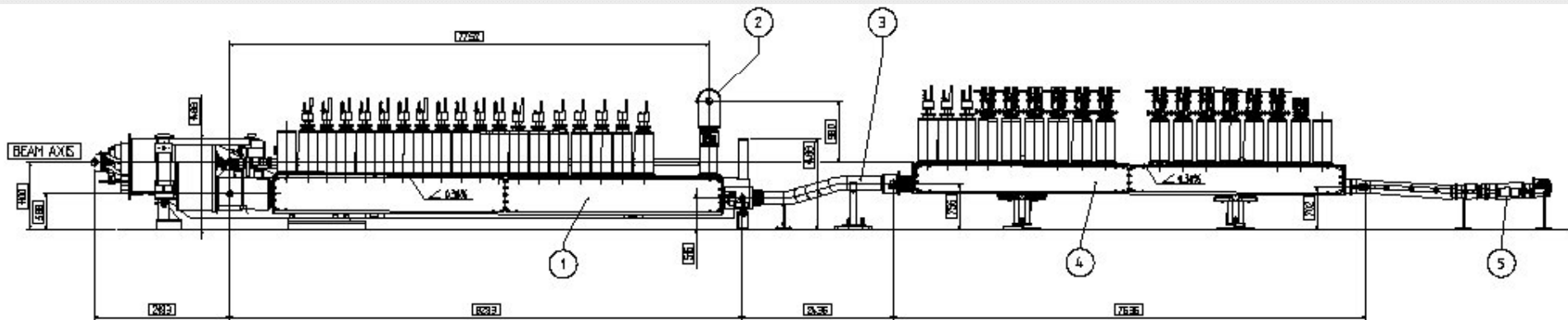
- LHC installation
 - Hypothesis
 - Conservative hypothesis that drilling not allowed when liquid helium
 - Installation = same risk as alignment operations (ok with liquid helium)

 - Drilling 2 weeks / sector starting in week 11 for sector 2-3
 - Overall installation 2 weeks / sector within the general planning
 - Alignment check of SSS after system installation: a total of 25 days ok with general planning

- 104 systems to be manufactured and installed
 - System: 104 x 5'000 CHF 520'000 CHF
 - Ground fixation: 42'000 CHF
 - Manpower
 - Drilling: 104 x 4 x 6 x 62 CHF 155'000 CHF
 - Installation: 104 x 2 x 8 x 62 CHF 103'000 CHF
 - Equipment for drilling and installation: 27'000 CHF
 - Alignment: 20'000 CHF

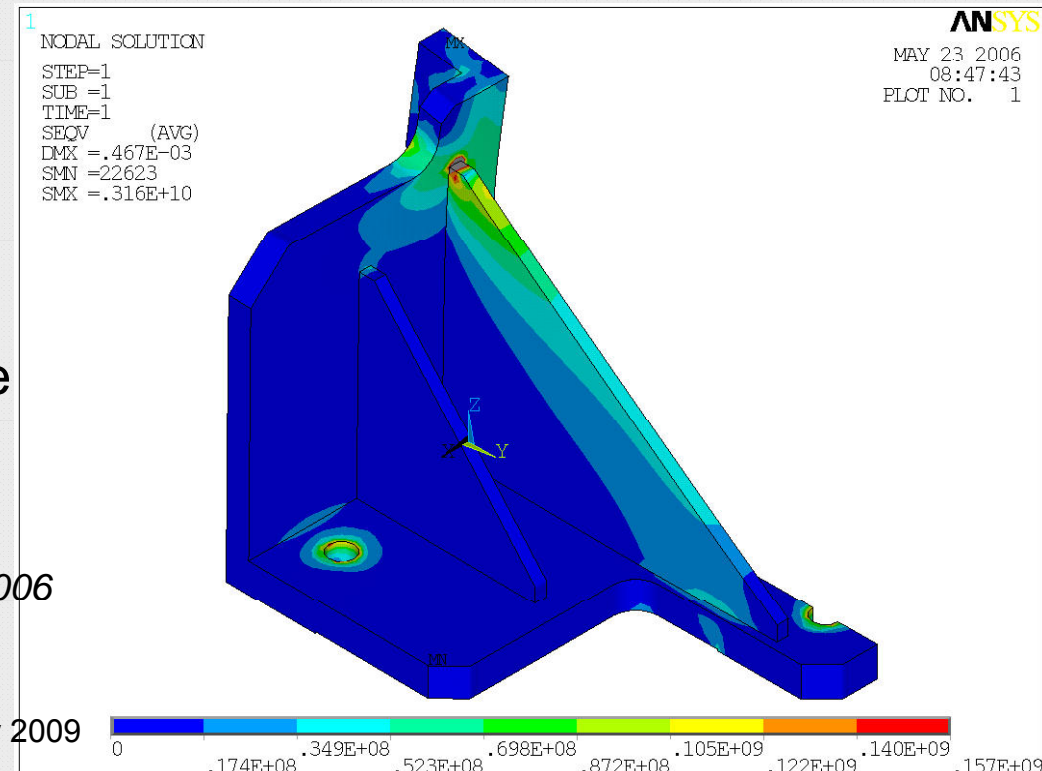
 - Total for 8 sectors 867'000 CHF
-
- *Rmq transport operations not included*

- The anchoring of SSS with vacuum barrier have been discussed
- If new cryostat design pressure 0.3 MPa instead of 0.15 MPa, what about the other equipments?
- DFBA



- DFBA
 - Calculations done by A. Bertarelli in 2006 for a vessel design pressure of 0.15 MPa absolute (0.05 MPa relative)
 - The new design pressure of 0.3 Mpa (0.2 MPa relative) multiplies the applied loads by **a factor 4**
 - Shuffling module vacuum vessel – with the new design pressure the tank will plastify locally but should not get to failure
 - The “negative fixator” (external support) will fail
 - Fixation very difficult to improve due to lack of space

*Alessandro Bertarelli
DFBA calculations done in 2006*



- The design of the improved anchoring of SSS with vacuum barrier has been presented
- It was designed to withstand **240 kN** longitudinally, equivalent to **0.3 MPa** of differential pressure on both sides of the vacuum barrier
- The system is foreseen to be installed in “warm” sectors too as an additional safety device
- The installation of the equipments will be within the global planning
- The total cost will be of about **867'000 CHF**, transport not included
- Open questions
 - What happens if $\Delta p > 0.3 \text{ MPa}$? : cold foot, vacuum barrier damaged before external anchoring damage...
 - We are very confident that vacuum barrier and cold foot withstand the load equivalent to **0.3 MPa** but it has never been demonstrated
 - Next week point could be the DFBA...
 - What about other elements (such as all “special” cryostats of the LSS, jumper vacuum barrier ...)?

Thank you !

... in particular Lucio for his patience and advices