

# **TCTW Collimator Design**

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Engineering Department



#### Outlook

- Introduction
  - Design highlights
  - Analyses of collimator robustness
  - Testing
  - Summary



#### Introduction





- Challenge: Embed an electric wire in a TCTP collimator jaw to compensate longrange Beam-Beam effects
- Requirements:
- High DC current (up to 350 A)
- Thin wire ( $\emptyset_{CU} \le 2.5 \text{ mm}$ )
- In-jaw wire (depth ≤ 3 mm)
- Maintain TCTP complete functionality!





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- Brazing maximizes wire cooling
- 2.48mm **Increase of diameter** where the wire is not in direct 0.26mm 🔨 contact with the jaw (extremities)
- Also **clamped to cooling pipes** when it's not in the jaw

MgO

Cu

316L

Total diameter: 3.6mm

X 0.41mm

3.45mm

0.365mm

Cu

316L

Total diameter : 5mm

I = 1000 mm





### Jaw Assembling



 Brazingsofmbly cable //inischtening cup / cable cooling system / sockets





- The collimator resistance should be not jeopardized by the insertion of the wire
- Stresses on the TCTW have to be comparable to those of a standard TCTP for the following load cases:
  - **1.** Assembling
  - 2. Nominal operation under beam slow losses
  - **3.** Accidental scenario asynchronous beam dump







- **1.** Assembling
  - Stresses on the Inermet block given by the fixing screws (1.5 kN/screw)
  - Presence of the gap wire/Wblock prevents stress arise on the thin wall
  - Stresses negligible in both cases (for reference, yield stress of Inermet is 650 MPa)







#### 2. Nominal operation – 1h beam life time

- In nominal operation, particles of the beam external halo transfer their energy to the collimator under the form of **thermal energy**, which induces thermal stresses and deflection
- Deformations are also induced by the self-weight (1m girder simply supported at the extremities)
- On top of that, during BBLRC-dedicated MD, a strong joule effect is produced on the wire (1kW on a thin wire!)
  Maximum Temperature: 161.15 ° C





#### HILUMI LARGE HADRON COLLIDER

# **Engineering Calculations**

- 2. Nominal operation 1h beam life time
  - Thermal-induced sagitta is comparable between TCTP and TCTW in nominal operation
  - Stresses are low in both cases
  - Larger deformation during MD given by wire heating up by joule effect



![](_page_10_Picture_0.jpeg)

![](_page_10_Picture_1.jpeg)

#### 3. Accidental scenario – asynchronous beam dump

- Target: same onset of damage between TCTP and TCTW
- At 7 TeV, this is estimated in 5E9 protons for TCTP
- Simulations repeated on TCTW for the following beam parameters (55 cm β\* optics)

![](_page_10_Figure_7.jpeg)

![](_page_10_Picture_9.jpeg)

![](_page_11_Figure_1.jpeg)

**LHC Collimation** 

Project

![](_page_12_Picture_0.jpeg)

![](_page_12_Picture_1.jpeg)

### Testing

- The final configuration is the best solution found by numerical and experimental means
- Several laboratory tests to choose between different configurations (e.g. clamped BBLRC wire, brazed, different "T" shapes, etc.)
- Electrical functionality of wires during bending evaluated
- Testing of brazing wire/"T" support
- Although for the final configuration stresses between TCTP and TCTW are comparable, 1 mm is the minimum thickness of W defined
- Too many risks at lower thickness during machining, transport, manipulation (W alloys are brittle!)

![](_page_12_Picture_9.jpeg)

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![](_page_13_Picture_0.jpeg)

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![](_page_14_Picture_1.jpeg)

### Testing

- Mechanical tests on preliminary configurations (clamped wire)
- EN/MME mechanical laboratory

![](_page_14_Figure_5.jpeg)

![](_page_14_Picture_6.jpeg)

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![](_page_15_Picture_0.jpeg)

![](_page_15_Picture_1.jpeg)

# Testing

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![](_page_15_Picture_4.jpeg)

#### NO influence on electrical resistivity $\sqrt{}$

![](_page_15_Picture_6.jpeg)

Influence of **bending process** on electrical performance of cables

#### **BPM Cables tooling**

![](_page_16_Picture_0.jpeg)

![](_page_16_Picture_1.jpeg)

#### **Summary**

- The design of a tertiary collimator with embedded BBLRC (TCTW) has been presented
- The TCTW maintains the complete functionality of a standard TCTP
- One of the main challenges is to evacuate the very high heat load generated by joule effect on the wire (1 kW on the wire only – higher than the design load of a full TCTP jaw!)
- This is done by brazing the wire to a "T" shape insert, and by increasing the wire diameter and clamping it to the cooling pipes when it's outside of the jaw
- Numerical calculations and experimental tests show that the TCTW accepts the same load scenarios of a TCTP without losing in safety
- Nevertheless, the minimum thickness of the Inermet jaw has been defined in 1 mm, to take into account possible accidental loads coming during transport and manipulation of the blocks, and to ease machining
- Extensive R&D done on further aspects of BBLRC installation: bake-out compatibility, impedance and beam cleaning analyses, development of new LVDTs less sensitive to EM effects from the wire

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![](_page_17_Picture_2.jpeg)

![](_page_17_Picture_3.jpeg)

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