#### Fast electron beam heating in solid targets

#### Rory J. Garland Supervisors: A. P. L. Robinson(RAL) & M. Borghesi(QUB)

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#### Outline

#### 1 Introduction

#### 2 Simulations



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#### Motivation

- TNSA
- Fast Ignition ICF
- WDM
- Astrophysical Experiments

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# Applications



Figure : TNSA

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#### Applications Fast Ignition



Figure : Direct Drive vs Direct Drive Fast Ignition

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• Generated from  $\mathbf{j} \times \mathbf{B}$  heating.

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- Maxwell-Jüttner distribution

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- Temperature scales with:

$$T(MeV) = 0.511 \left( \sqrt{1 + rac{I_{18}\lambda_{\mu m}^2}{1.37}} - 1 
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Propagate through the target

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#### What are Fast Electron Beams?

- Generated from **j** × **B** heating.
- Maxwell-Jüttner distribution
- Temperature scales with:  $T(MeV) = 0.511 \left( \sqrt{1 + \frac{l_{18}\lambda_{\mu m}^2}{1.37}} - 1 \right)$
- Propagate through the target
- Generation of Electric and Magnetic Fields

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- Current Neutrality  $(j_f \approx -j_B)$

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- Propagate through the target
- Generation of Electric and Magnetic Fields
- Current Neutrality  $(j_f \approx -j_B)$
- Return current leads to ohmic heating of the target

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#### Current Work on fast electron transport

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#### Current Work on fast electron transport

Reduction of the fast electron radius

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#### Current Work on fast electron transport

## Reduction of the fast electron radius

Resistive guiding:

$$\frac{\delta \mathbf{B}}{\delta t} = \eta \nabla \times \mathbf{j}_{f} + \frac{\nabla(\eta) \times \mathbf{j}_{f}}{\nabla(\eta) \times \mathbf{j}_{f}}$$
(1)

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 How fast-electron based heating scales with key experimental parameters

#### Fast electron heating

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#### Fast electron heating

# Fast electron heating makes a large assumption: a Spitzer like resistivity

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#### Fast electron heating

Fast electron heating makes a large assumption: a Spitzer like resistivity

$$T \propto \frac{\beta^{\frac{4}{5}} I_L^{\frac{2}{5}} t_h^{\frac{2}{5}}}{\lambda^{\frac{4}{5}} n_i^{\frac{2}{5}}}.$$
 (2)

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#### Fast electron heating

Fast electron heating makes a large assumption: a Spitzer like resistivity

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While this is an accurate representation of a plasma, it does not clearly represent the cold target.

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By treating the target via cold resistivity, it is possible to arrive at two different resistivities:

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- By treating the target via cold resistivity, it is possible to arrive at two different resistivities:
- Constant resitivity:

$$T \propto \frac{\beta^2 I_L \tau_L}{Z n_i \lambda_L} \tag{3}$$

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#### Another alternative

- By treating the target via cold resistivity, it is possible to arrive at two different resistivities:
- Constant resitivity:

$$T \propto \frac{\beta^2 I_L \tau_L}{Z n_i \lambda_L} \tag{3}$$

Square root resistivity:

$$T \propto \frac{\beta^4 I_L^2 \tau_L^2}{Z^2 n_i^2 \lambda_L^2} \tag{4}$$

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- By treating the target via cold resistivity, it is possible to arrive at two different resistivities:
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The aim of this work is to preform simulations on a variety of targets to see which model is best suited towards it.

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### Outline



#### 2 Simulations



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#### ZEPHYROS - Hybrid-PIC code

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- ZEPHYROS Hybrid-PIC code
- Follows Davies(2002) rigid beam model

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- ZEPHYROS Hybrid-PIC code
- Follows Davies(2002) rigid beam model
- Calculates electric field from resistive Ohms Law and by considering current neutrality can arrive at equations for the Electric and Magnetic fields.

• 
$$\mathbf{E} = -\eta \mathbf{j}_f + \frac{\eta}{\mu_0} \nabla \times \mathbf{B}$$

$$\frac{\delta \mathbf{B}}{\delta t} = \eta \nabla \times \mathbf{j}_f + \nabla(\eta) \times \mathbf{j}_f + \frac{\eta}{\mu_0} \nabla^2 \mathbf{B} - \frac{1}{\mu_0} \nabla \eta \mathbf{B}$$

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- Follows Davies(2002) rigid beam model
- Calculates electric field from resistive Ohms Law and by considering current neutrality can arrive at equations for the Electric and Magnetic fields.

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$$\mathbf{E} = -\eta \mathbf{j}_f + \frac{\eta}{\mu_0} \nabla \times \mathbf{B}$$

- $\mathbf{I} \frac{\delta \mathbf{B}}{\delta t} = \eta \nabla \times \mathbf{j}_f + \nabla(\eta) \times \mathbf{j}_f + \frac{\eta}{\mu_0} \nabla^2 \mathbf{B} \frac{1}{\mu_0} \nabla \eta \mathbf{B}$
- Manually enter a resistivity model

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Simulation Setup i

 $\blacksquare$  200  $\times$  200  $\times$  200 grid used with cells being 0.1  $\mu m$  in length.

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- 4  $\times$  10<sup>7</sup> particles

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- Beam radius of 10 $\mu$ m.

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- Angle of Divergence: 60°(1.047rad).

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- Initial Parameters followed Taranis laser parameters
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- Angle of Divergence: 60°(1.047rad).
- β =of 0.4

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# ZEPHYROS(II)

Simulation Setup i

 $\blacksquare$  200  $\times$  200  $\times$  200 grid used with cells being 0.1  $\mu m$  in length.

- 4  $\times$  10<sup>7</sup> particles
- Initial Parameters followed Taranis laser parameters
- Beam radius of 10 $\mu$ m.
- Angle of Divergence: 60°(1.047rad).
- β =of 0.4
- Laser Pulse duration of  $5.6 \times 10^{-13}$ s.

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# ZEPHYROS(II)

Simulation Setup i

 $\blacksquare$  200  $\times$  200  $\times$  200 grid used with cells being 0.1  $\mu m$  in length.

- 4  $\times$  10<sup>7</sup> particles
- Initial Parameters followed Taranis laser parameters
- Beam radius of 10 $\mu$ m.
- Angle of Divergence: 60°(1.047rad).
- β =of 0.4
- Laser Pulse duration of  $5.6 \times 10^{-13}$ s.
- Targets used: AI, Ti, Au & CH

Simulation Setup ii

Run	$I(Wcm^{-2})$	$\lambda(\mu m)$	$n_i(cm^{-3})$	Fast e- Temp (MeV)
А	2×10 <sup>19</sup>	1.053	See table 2	1.61
В	9.25×10 <sup>19</sup>			
С	$5.55 \times 10^{19}$			
D	3.33×10 <sup>19</sup>			
E	$1.2 \times 10^{19}$			
F	7.2×10 <sup>18</sup>			
G	4.32×10 <sup>18</sup>			
Н		4.875		9.02
1		2.925		5.22
J		1.755		2.95
К		0.6318		0.824
L		0.379		0.388
М		0.227		0.166
N			See table 2	
0			See table 2	
Р			See table 2	
Q			See table 2	
R			See table 2	
S			See table 2	

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### Outline



#### 2 Simulations



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## Heating Profiles



Can be seen from the 3 figures that the heating profiles are consistent.



## Heating at $2\mu$ m





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# Heating(II) <sup>2 µm</sup>

 $T \propto \frac{\beta^{\frac{4}{5}} I_{L}^{\frac{2}{5}} t_{h}^{\frac{2}{5}}}{\lambda^{\frac{4}{5}} n_{i}^{\frac{2}{5}}}$  $T \propto \frac{\beta^{2} I_{L} \tau_{L}}{Z n_{i} \lambda_{L}}$  $T \propto \frac{\beta^{4} I_{L}^{2} \tau_{L}^{2}}{Z^{2} n_{i}^{2} \lambda_{L}^{2}}$ 

Run	I	$\lambda$	ni
Al	1.17037	1.3973	0.9461
Ti	1.31882	1.4853	1.1457
Au	1.71775	1.6205	1.6167
CH	0.89455	1.1440	0.4761

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#### Heating(III) <sup>4 µm</sup>

 $T \propto \frac{\beta^{\frac{4}{5}} I_{L}^{\frac{2}{5}} t_{h}^{\frac{2}{5}}}{\lambda^{\frac{4}{5}} n_{i}^{\frac{2}{5}}}$  $T \propto \frac{\beta^{2} I_{L} \tau_{L}}{Z n_{i} \lambda_{L}}$  $T \propto \frac{\beta^{4} I_{L}^{2} \tau_{L}^{2}}{Z^{2} n_{i}^{2} \lambda_{L}^{2}}$ 

Run	I	$\lambda$	ni
Al	1.54547	1.74238	1.35978
Ti	1.71326	1.74842	1.48347
Au	1.71396	1.31961	1.61393
СН	0.89452	1.14852	0.49701

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# Heating(IV)

 $T \propto \frac{\beta^{\frac{4}{5}} I_{L}^{\frac{2}{5}} t_{h}^{\frac{2}{5}}}{\lambda^{\frac{4}{5}} n_{i}^{\frac{2}{5}}}$  $T \propto \frac{\beta^{2} I_{L} \tau_{L}}{Z n_{i} \lambda_{L}}$  $T \propto \frac{\beta^{4} I_{L}^{2} \tau_{L}^{2}}{Z^{2} n_{i}^{2} \lambda_{L}^{2}}$ 

Run	I	$\lambda$	n <sub>i</sub>
Al	1.41015	1.29582	1.35218
Ti	1.52150	1.36827	1.34533
Au	1.23550	0.60065	1.2817
CH	0.88295	1.11727	0.50418

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## Strong Heating Limit

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$T \propto \frac{\beta^{\frac{4}{5}} I_L^{\frac{5}{5}} t_h^{\frac{5}{5}}}{\lambda^{\frac{4}{5}} n_i^{\frac{2}{5}}}$	
$T\propto rac{eta^2 I_L  au_L}{Z n_i \lambda_L}$	
$T\propto rac{eta^4 l_L^2  au_L^2}{Z^2 n_i^2 \lambda_L^2}$	

Run	I	$\lambda$	ni
Al(10eV)	1.17037	1.3973	0.9461
Al(50eV)	1.06293	1.1934	0.7301
Al(100eV)	0.96880	1.1934	0.5593
Ti(10eV)	1.4308	1.4853	1.6153
Ti(50eV)	1.07748	1.177	0.6947
Ti(100eV)	0.97502	1.0041	0.6947
Au(10eV)	1.60688	1.1132	1.2631
Au(50eV)	1.31637	0.7412	0.9605
Au(100eV)	1.24259	0.2969	0.7802

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#### Conclusion

 Assumed Spitzer resistivity for solid targets has shown to be an incorrect assumption

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#### Conclusion

- Assumed Spitzer resistivity for solid targets has shown to be an incorrect assumption
- Results show that these targets are far better modelled via a cold temperature resistivity.

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#### **Questions?**

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