Outline:

- Signal generation → transfer impedance
- Capacitive *button* BPM for high frequencies
- Capacitive *shoe-box* BPM for low frequencies
- Electronics for position evaluation
- BPMs for measurement of closed orbit, tune and further lattice functions
- Summary

A *B*eam *P*osition *M*onitor is an non-destructive device for bunched beams

It has a low cut-off frequency i.e. dc-beam behavior can not be monitored
The abbreviation BPM and pick-up PU are synonyms

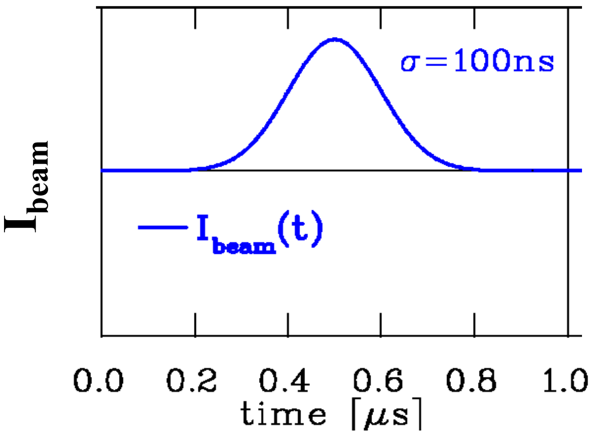
1. It delivers information about the transverse center of the beam

- ***Trajectory:*** Position of an individual bunch within a transfer line or synchrotron
- ***Closed orbit***: central orbit averaged over a period much longer than a betatron oscillation
- ***Single bunch position*** → determination of parameters like tune, chromaticity, ***β***-function
- Bunch position on a large time scale: bunch-by-bunch → turn-by-turn → averaged position
- Time evolution of a single bunch can be compared to 'macro-particle tracking' calculations
- Feedback: fast bunch-by-bunch damping ***or*** precise (and slow) closed orbit correction

2. Information on longitudinal bunch behavior

- **Bunch shape and evolution** during storage and acceleration
- For proton LINACs: the beam **velocity** can be determined by two BPMs
- For electron LINACs: **Phase** measurement by Bunch Arrival Monitor
- ***Relative*** low current measurement down to 10 nA.

Time domain: **Recording of a voltage as a function of time:**



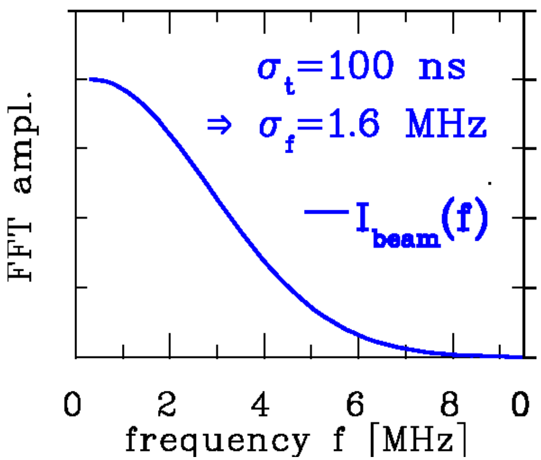
Instrument:

Oscilloscope

Fourier Transformation:

$$\tilde{f}(\omega) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} f(t) e^{-i\omega t} dt$$

Frequency domain: **Displaying of a voltage as a function of frequency:**



Instrument:

Spectrum Analyzer

Fourier Transformation

of time domain data

<u>Care:</u> Contains amplitude

***<u>and</u>* phase**

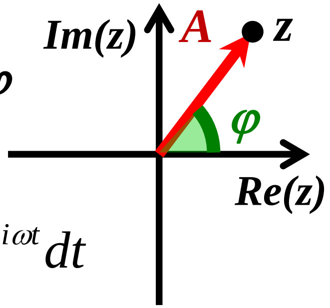
Fourier Transform.: $\tilde{f}(\omega) \equiv \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} f(t) e^{-i\omega t} dt$ **Inv. F. T.:** $f(t) \equiv \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} \tilde{f}(\omega) e^{i\omega t} d\omega$

tech. *DFT(f)* or *FFT(f)* tech. *IDFT(f)*

$\Rightarrow$ a process can be described either with $f(t)$ '**time domain**' or $\tilde{f}(\omega)$ '**frequency domain**'

$\rightarrow$ tech.: DFT is discrete FT, FFT is a dedicated algorithm for **fast** calculation with 2^n increments

No loss of information: If $\tilde{f}(\omega) = \frac{1}{\sqrt{2\pi}} \int f(t) e^{-i\omega t} dt$ exists, than $f(t) = \frac{1}{2\pi} \int\int f(\tau) e^{i\omega(t-\tau)} d\omega d\tau$



FT is complex: $\tilde{f}(\omega) \in C$ $\rightarrow$ tech. amplitude $A(\omega) = |\tilde{f}(\omega)|$ and phase φ

For $f(t) \in R$ $\Rightarrow$ ***A(ω)*** is even and ***φ(ω)*** is odd function of ***ω***

Similarity Law: For ***a≠0*** it is for ***f(at):*** $|1/a| \cdot \tilde{f}(\omega / a) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} f(at) e^{-i\omega t} dt$

$\rightarrow$ the properties can be scaled to any frequency range; 'shorter time signal have wider FT'

Differentiation Law: $(i\omega)^n \cdot \tilde{f}(\omega) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} f^{(n)}(t) e^{-i\omega t} dt$

$\rightarrow$ differentiation in time domain corresponds to multiplication with ***iω*** in frequency domain

Convolution Law: For $f(t) = f_1(t) * f_2(t) \equiv \int_{-\infty}^{\infty} f_1(\tau) \cdot f_2(t-\tau) d\tau$

$\Rightarrow$ $\tilde{f}(\omega) = \tilde{f}_1(\omega) \cdot \tilde{f}_2(\omega)$ $\rightarrow$ convolution be expressed as multiplication of FT

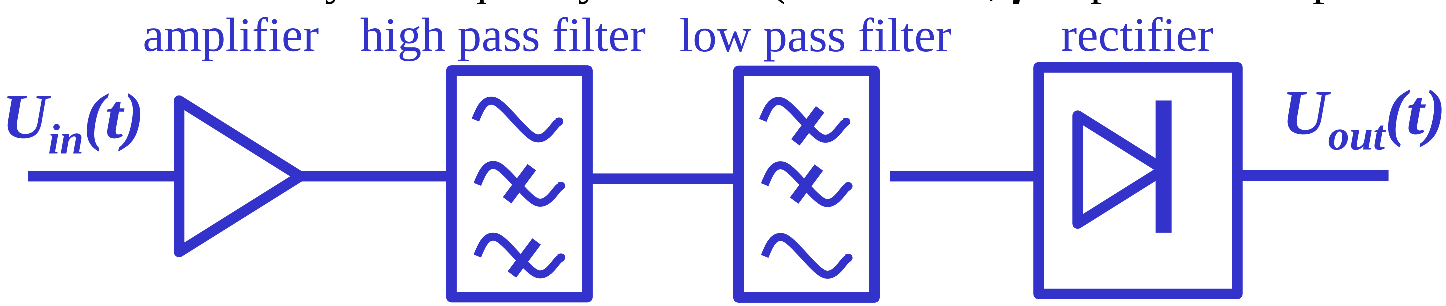
Convolution Law: For $f(t) = f_1(t) * f_2(t) \equiv \int_{\infty}^{\infty} f_1(\tau) \cdot f_2(t-\tau) d\tau$

$\Rightarrow \quad \tilde{f}(\omega) = \tilde{f}_1(\omega) \cdot \tilde{f}_2(\omega)$

→ convolution in time domain can be expressed as multiplication of FT in frequency domain

Application: Chain of electrical elements calculated in frequency domain more easily

parameters are more easy in frequency domain (bandwidth, ***f***-dependent amplification.....)



Engineering formulation for <u>finite</u> number of discrete samples:

Digital Fourier Transformation.: ***DFT(f)***

Fast Fourier Transformation: *FFT(f)*, special numerical algorithm for $\boldsymbol{2^n}$ samples

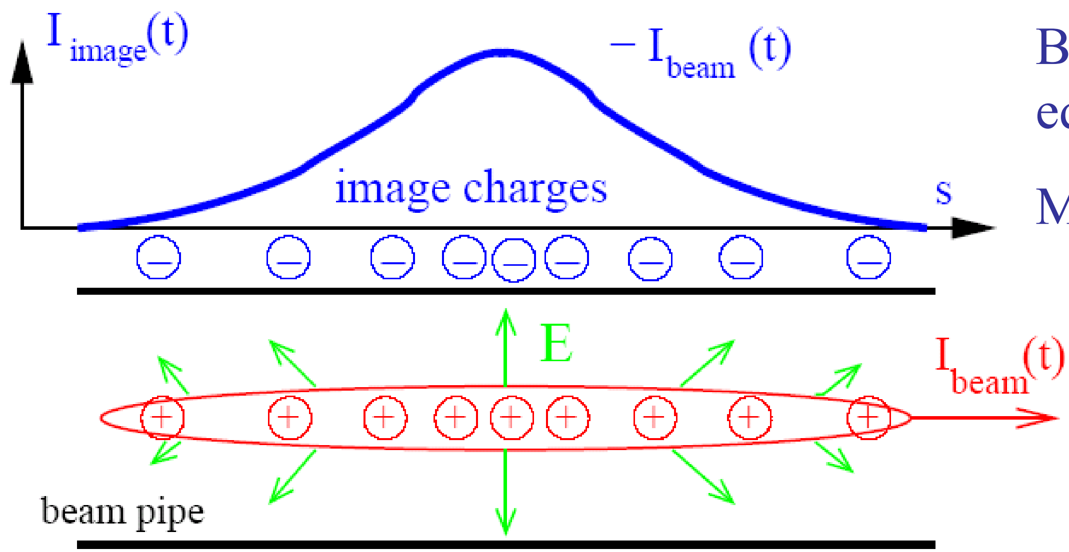
Transfer function *H(ω)* and ***h(t)*** describe of electrical elements

Calculation with ***H(ω)*** in frequency domain or

h(t) time domain → 'Finite Impulse Response' FIR filter or 'Infinite Impulse Response' IIR filter

Pick-Ups for bunched Beams

The image current at the beam pipe is monitored on a high frequency basis i.e. the ac-part given by the bunched beam.



Beam Position Monitor **BPM** equals Pick-Up **PU**

Most frequent used instrument!

For relativistic velocities, the electric field is transversal:

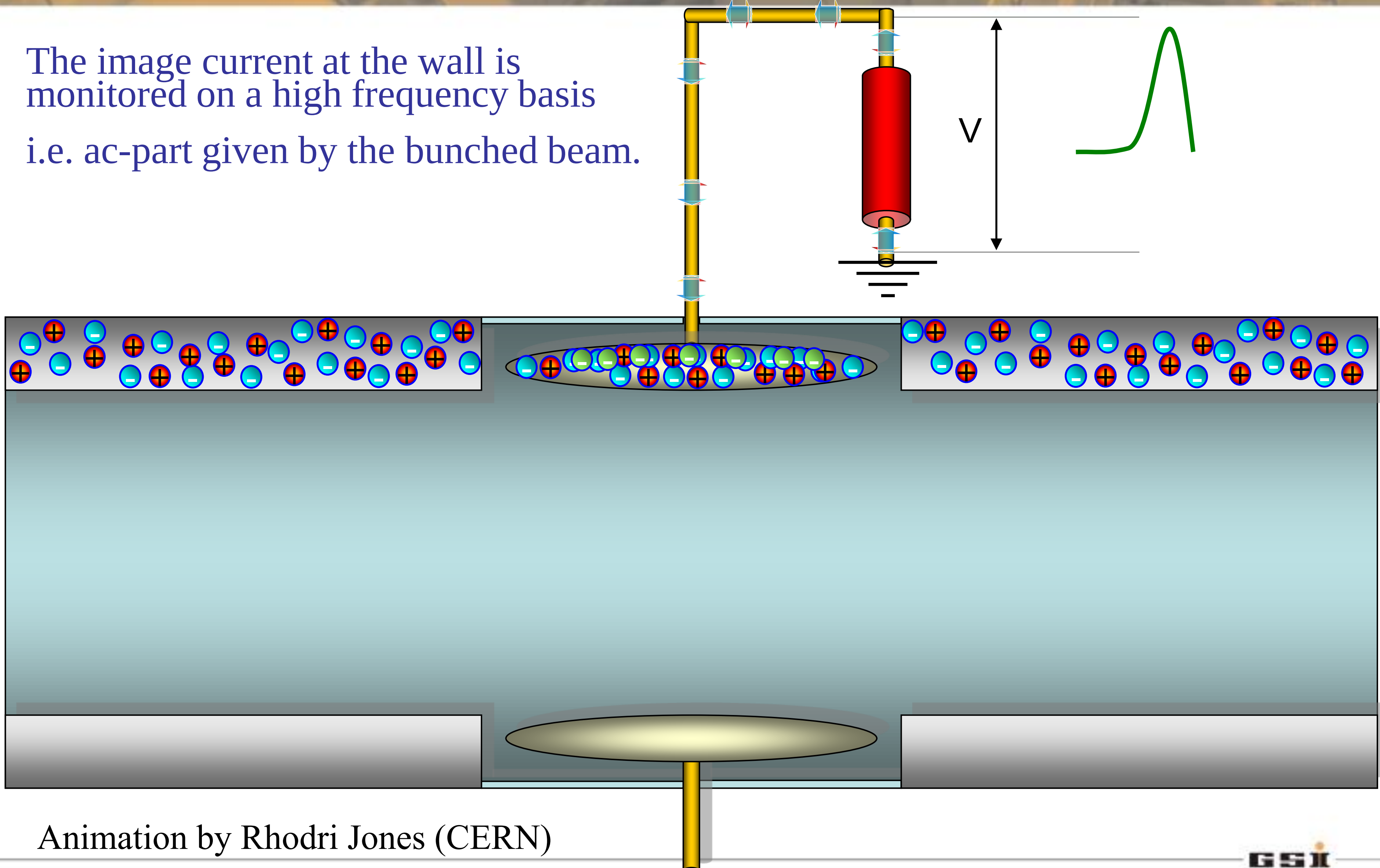
$$E_{\perp,lab}(t) = \gamma \cdot E_{\perp,rest}(t')$$

- **Signal treatment for capacitive pick-ups:**
  - Longitudinal bunch shape
  - Overview of processing electronics for Beam Position Monitor (BPM)
- **Measurements:**
  - Trajectory and closed orbit determination
  - Tune and lattice function measurements (synchrotron only).

Principle of Signal Generation of capacitive BPMs

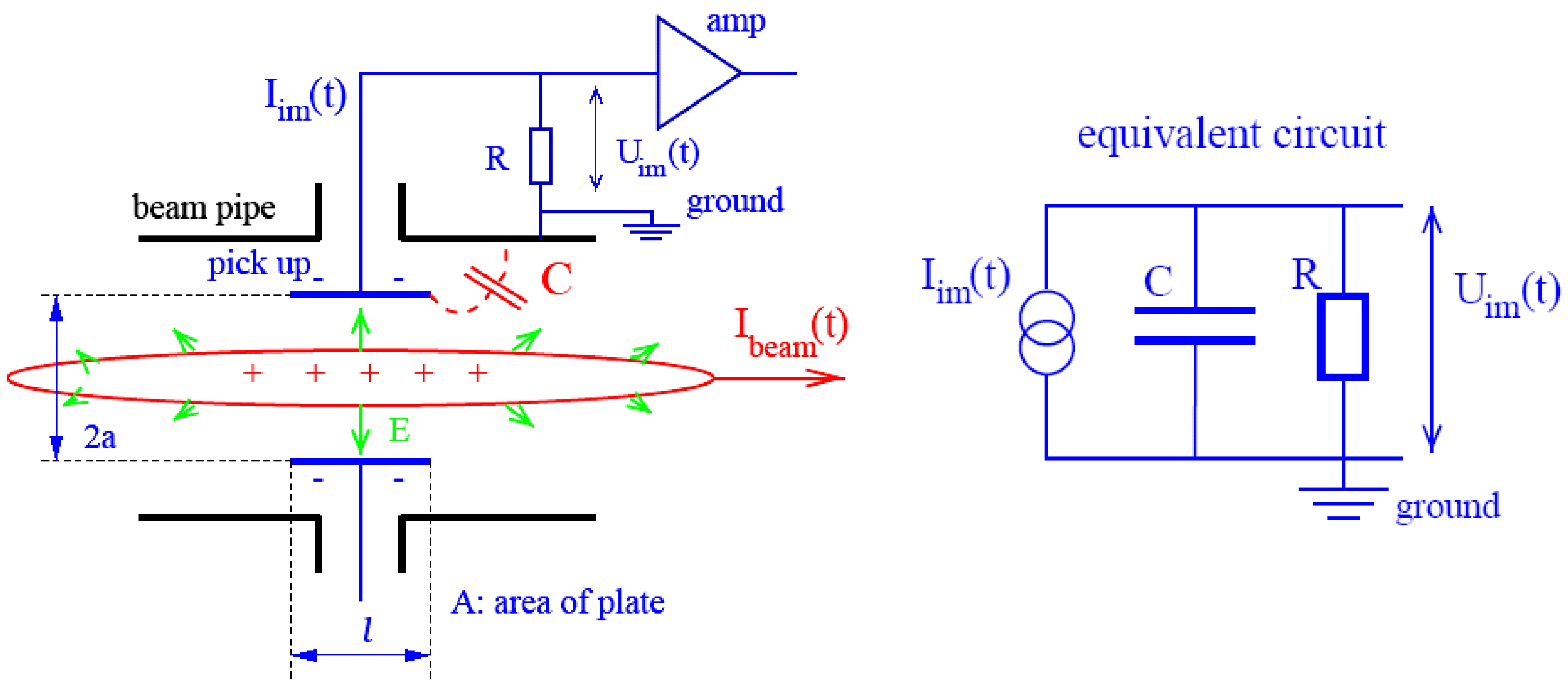
The image current at the wall is monitored on a high frequency basis

i.e. ac-part given by the bunched beam.



Animation by Rhodri Jones (CERN)

The wall current is monitored by a plate or ring inserted in the beam pipe:



The image current I_{im} at the plate is given by the beam current and geometry:

$$I_{im}(t) = -\frac{dQ_{im}(t)}{dt} = \frac{-A}{2\pi a l} \cdot \frac{dQ_{beam}(t)}{dt} = \frac{-A}{2\pi a} \cdot \frac{1}{\beta c} \cdot \frac{dI_{beam}(t)}{dt} = \frac{A}{2\pi a} \cdot \frac{1}{\beta c} \cdot i\omega I_{beam}(\omega)$$

Using a relation for Fourier transformation: $I_{beam} = I_0 e^{-i\omega t} \Rightarrow dI_{beam}/dt = -i\omega I_{beam}$.

At a resistor ***R*** the voltage U_{im} from the image current is measured.
The transfer impedance Z_t is the ratio between voltage U_{im} and beam current I_{beam} in ***frequency domain***: $U_{im}(\omega) = R \cdot I_{im}(\omega) = Z_t(\omega, \beta) \cdot I_{beam}(\omega)$.

Capacitive BPM:

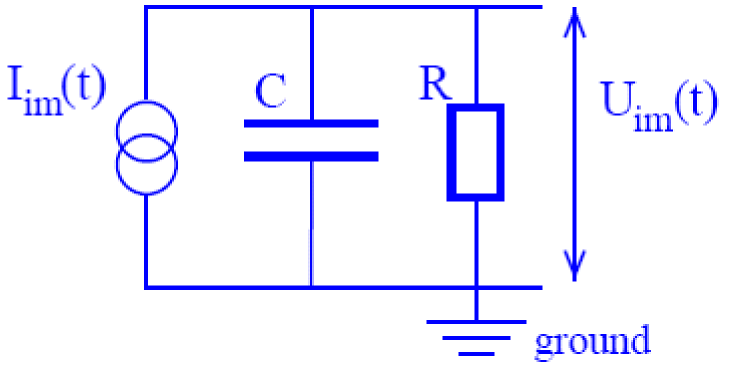
- The pick-up capacitance ***C***:
  plate ↔ vacuum-pipe and cable.
- The amplifier with input resistor ***R***.
- The beam is a high-impedance current source:

$$U_{im} = \frac{R}{1+i\omega RC} \cdot I_{im}$$

$$= \frac{A}{2\pi a} \cdot \frac{1}{\beta c} \cdot \frac{1}{C} \cdot \frac{i\omega RC}{1+i\omega RC} \cdot I_{beam}$$

$$\equiv Z_t(\omega, \beta) \cdot I_{beam}$$

equivalent circuit



$$\frac{1}{Z} = \frac{1}{R} + i\omega C \Leftrightarrow Z = \frac{R}{1+i\omega RC}$$

This is a high-pass characteristic with $\omega_{cut} = 1/RC$:

Amplitude: $|Z_t(\omega)| = \frac{A}{2\pi a} \cdot \frac{1}{\beta c} \cdot \frac{1}{C} \cdot \frac{\omega / \omega_{cut}}{\sqrt{1+\omega^2/\omega^2_{cut}}}$ **Phase:** $\varphi(\omega) = \arctan(\omega_{cut}/\omega)$

The high-pass characteristic for typical synchrotron BPM:

$$U_{im}(\omega)=Z_t(\omega)\cdot I_{beam}(\omega)$$

$$|Z_t| = \frac{A}{2\pi a}\cdot\frac{1}{\beta c}\cdot\frac{1}{C}\cdot\frac{\omega/\omega_{cut}}{\sqrt{1+\omega^2/\omega^2_{cut}}}$$

$$\varphi = \arctan(\omega_{cut}/\omega)$$

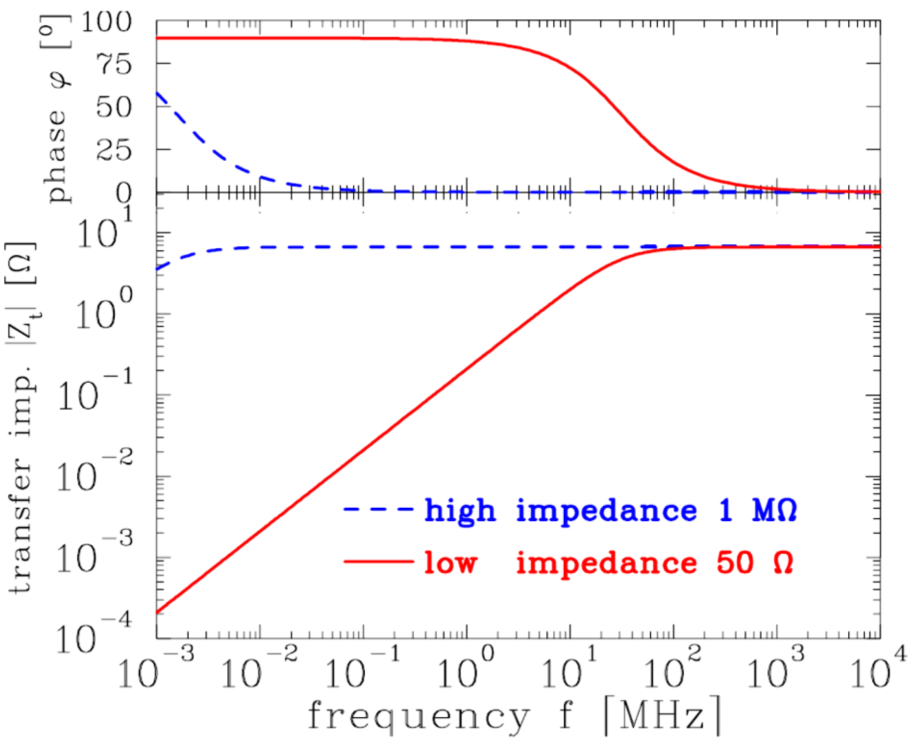
Parameter for shoe-box BPM:

C=100pF, l=10cm, β=50%

$f_{cut}=\omega/2\pi=(2\pi RC)^{-1}$

for R=50 Ω ⇒ f_{cut}= 32 MHz

for R=1 MΩ ⇒ f_{cut}= 1.6 kHz



Large signal strength → **high impedance**

Smooth signal transmission → **50 Ω**

Depending on the frequency range ***and*** termination the signal looks different:

- ***High frequency range $\omega >> \omega_{cut}$:***

$$Z_t \propto \frac{i\omega/\omega_{cut}}{1+i\omega/\omega_{cut}} \to 1 \Rightarrow U_{im}(t) = \frac{1}{C}\cdot\frac{1}{\beta c}\cdot\frac{A}{2\pi a}\cdot I_{beam}(t)$$

$\Rightarrow$ **direct image** of the bunch. Signal strength $Z_t \propto A/C$ i.e. nearly independent on length

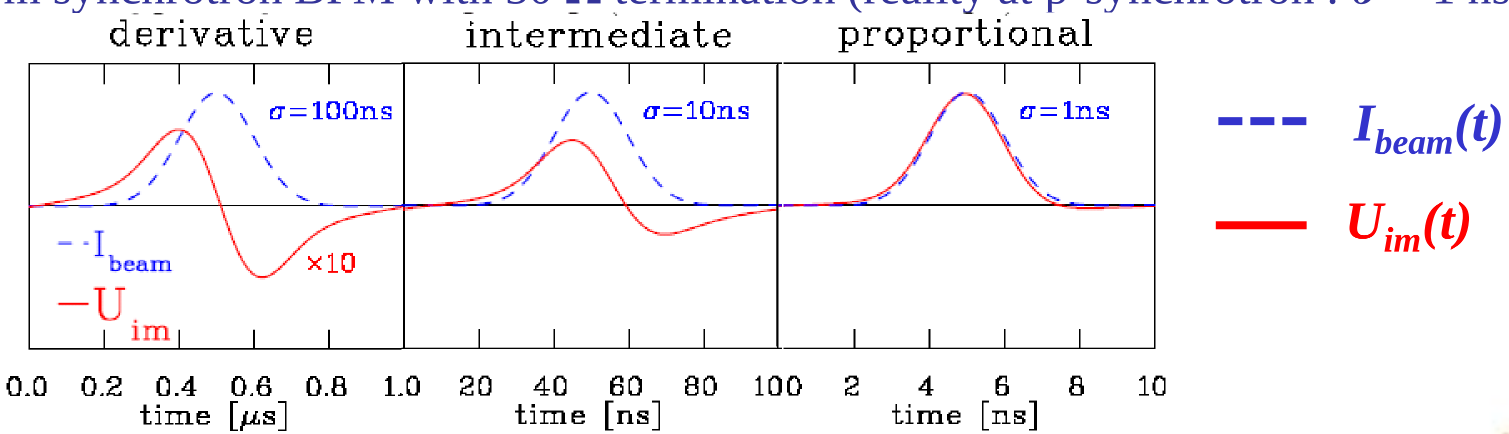
- ***Low frequency range $\omega << \omega_{cut}$:***

$$Z_t \propto \frac{i\omega/\omega_{cut}}{1+i\omega/\omega_{cut}} \to i\frac{\omega}{\omega_{cut}} \Rightarrow U_{im}(t) = R\cdot\frac{A}{\beta c\cdot 2\pi a}\cdot i\omega I_{beam}(t) = R\cdot\frac{A}{\beta c\cdot 2\pi a}\cdot\frac{dI_{beam}}{dt}$$

$\Rightarrow$ **derivative** of bunch, single strength $Z_t \propto A$, i.e. (nearly) independent on C

- ***Intermediate frequency range $\omega \approx \omega_{cut}$:*** Calculation using Fourier transformation

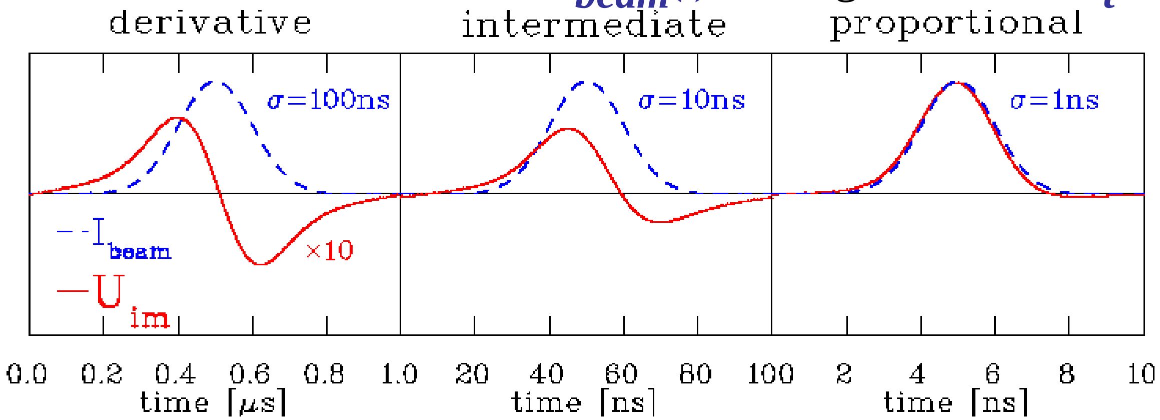
Example from synchrotron BPM with 50 Ω termination (reality at p-synchrotron : σ>>1 ns):



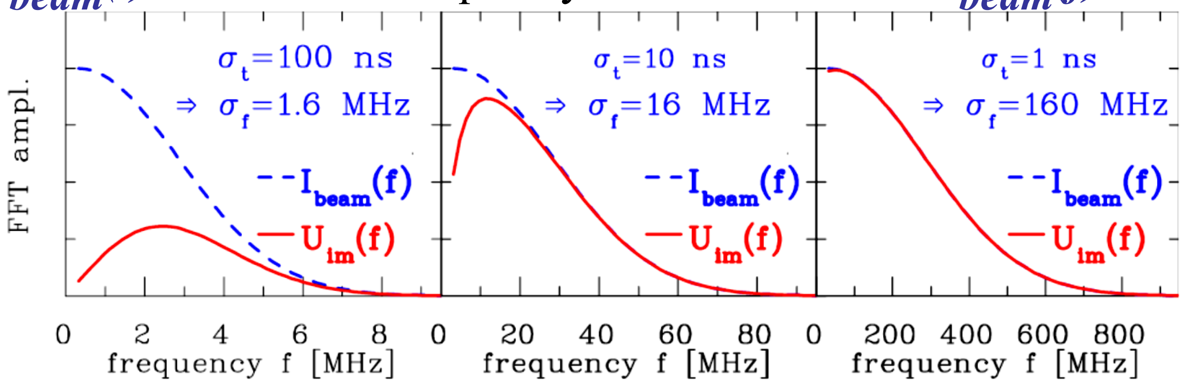
Calculation of Signal Shape (here single bunch)

The transfer impedance is used in frequency domain! The following is performed:

1. Start: Time domain Gaussian function $I_{beam}(t)$ having a width of σ_t



2. FFT of $I_{beam}(t)$ leads to the frequency domain Gaussian $I_{beam}(f)$ with $\sigma_f=(2\pi\sigma_t)^{-1}$

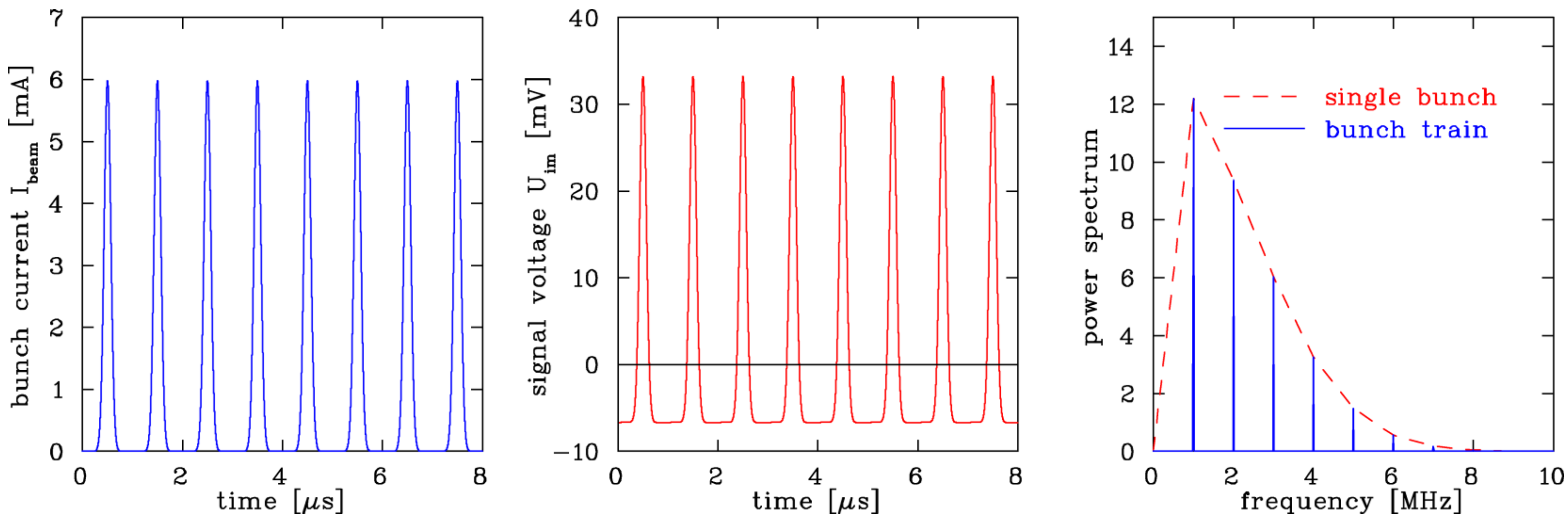


3. Multiplication with $Z_t(f)$ with f_{cut}=32 MHz leads to $U_{im}(f) = Z_t(f) \cdot I_{beam}(f)$

4. Inverse FFT leads to $U_{im}(t)$

Calculation of Signal Shape: Bunch Train

Example for low energy proton synchr.: Train of bunches with R=1 MΩ $\Rightarrow f >> f_{cut}$



Calculation: $I_{beam}(t) \xrightarrow{\text{FFT}} I_{beam}(\omega) \rightarrow U_{im}(\omega) = Z_{tot}(\omega) \cdot I_{beam}(\omega) \xrightarrow{\text{invFFT}} U_{im}(t)$

Parameter: R**=1 MΩ** $\Rightarrow f_{cut}$**=2kHz,** Z_t**=5Ω all buckets filled, no amp**

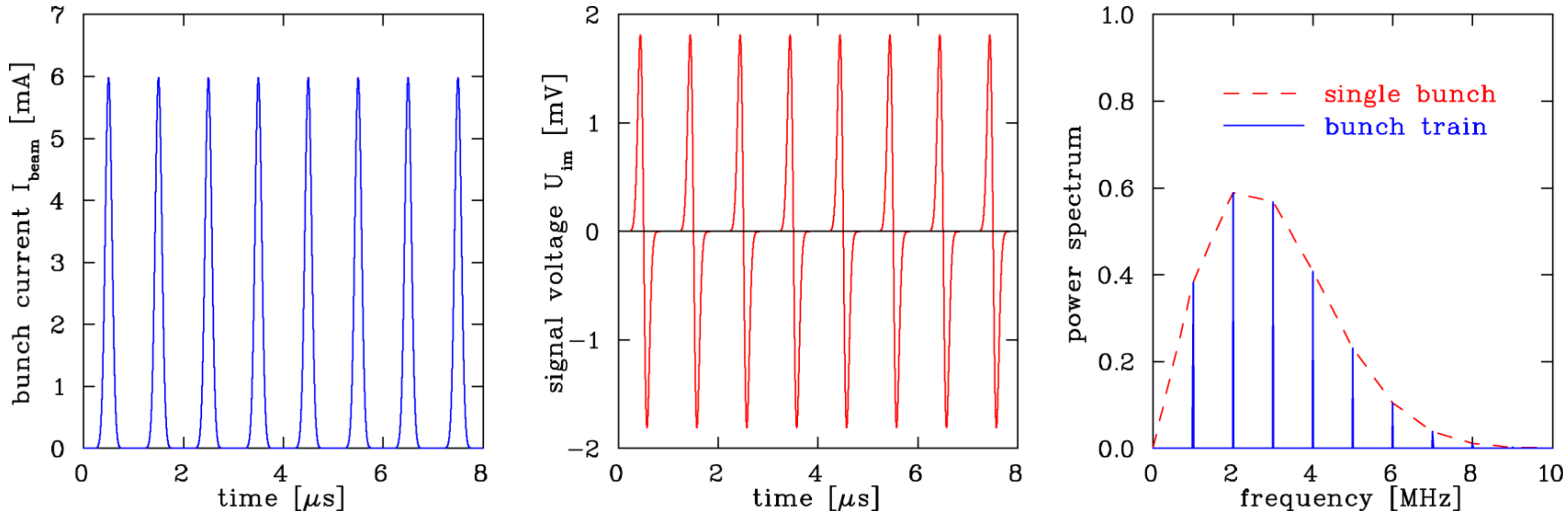
C=100pF, l=10cm, β=50%, σ_t=100 ns $\Rightarrow \sigma_l$=15m

- Fourier spectrum is composed of lines separated by acceleration f_{rf}
- Envelope given by single bunch Fourier transformation
- Baseline shift due to ac-coupling

Remark: 1 MHz< f_{rf} <10MHz $\Rightarrow$ Bandwidth ≈100MHz=10·f_{rf} for broadband observation

Synchrotron filled with 8 bunches accelerated with $\boldsymbol{f_{acc}}$=1 MHz

BPM terminated with $\boldsymbol{R}$=50 Ω $\Rightarrow f_{acc} \ll f_{cut}$:

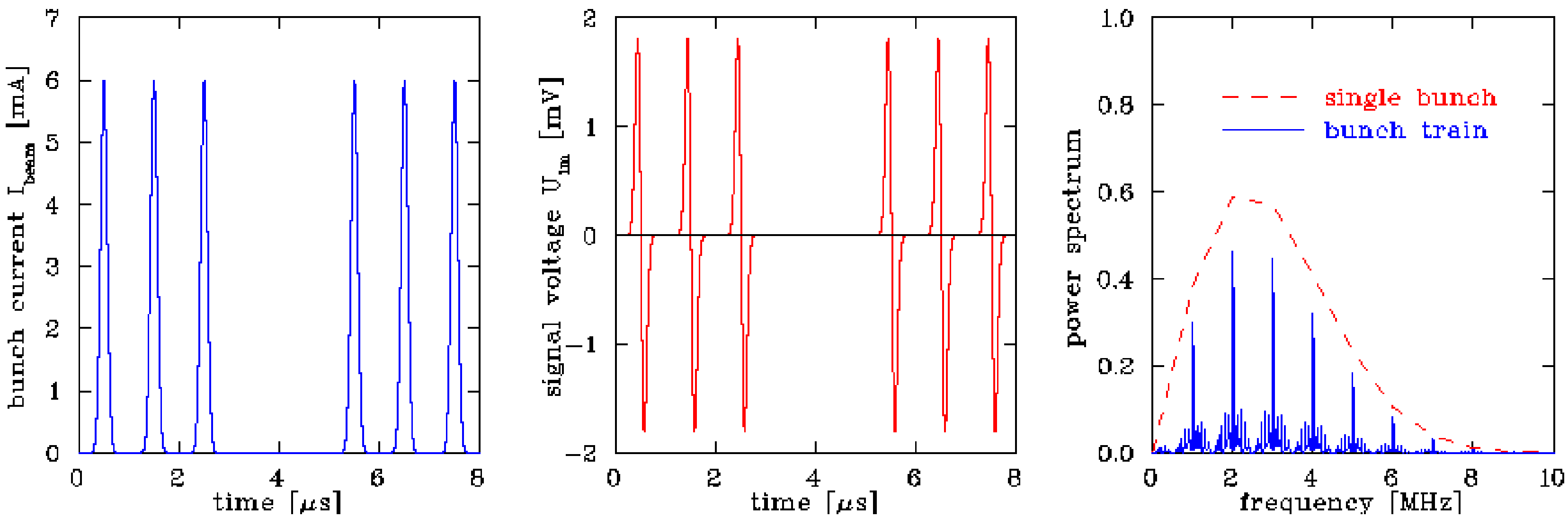


Parameter: $\boldsymbol{R}$=50 Ω ⇒ $\boldsymbol{f_{cut}}$=32 MHz, all buckets filled

C=100pF, l=10cm, β=50%, σ_t=100 ns ⇒ σ_l=15m

- Fourier spectrum is concentrated at acceleration harmonics with single bunch spectrum as an envelope.
- Bandwidth up to typically 10*$\boldsymbol{f_{acc}}$

Synchrotron during filling: Empty buckets, R=50 Ω:

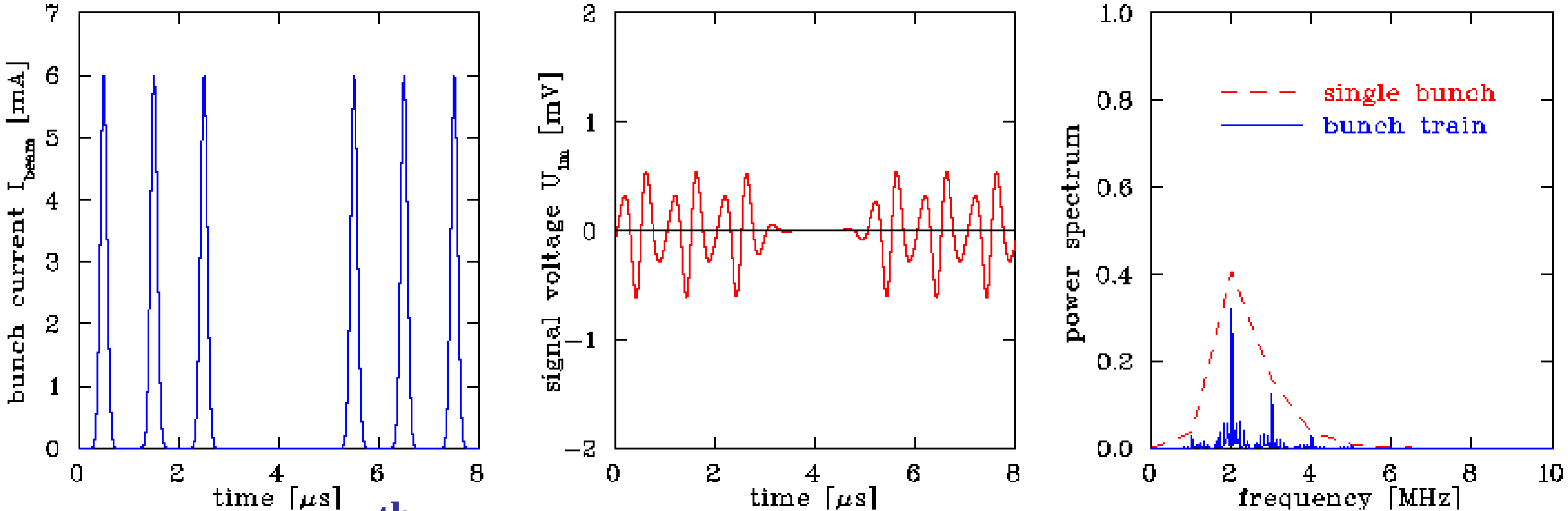


Parameter: *R*=50 Ω ⇒ f_{cut}=32 MHz, 2 empty buckets

C=100pF, *l*=10cm, *β*=50%, σ_t=100 ns ⇒ σ_l=15m

- Fourier spectrum is more complex, harmonics are broader due to sidebands

Effect of filters, here bandpass:



Parameter: R=50 Ω, 4th order Butterworth filter at f_{cut}=2 MHz

C=100pF, l=10cm, β=50%, σ=100 ns

- Ringing due to sharp cutoff
- Other filter types more appropriate

*n^{th} order Butterworth filter, math. simple, but **not** well suited:*

$$|H_{low}| = \frac{1}{\sqrt{1+(\omega/\omega_{cut})^{2n}}} \quad \text{and} \quad |H_{high}| = \frac{(\omega/\omega_{cut})^n}{\sqrt{1+(\omega/\omega_{cut})^{2n}}}$$

$$H_{filter} = H_{high} \cdot H_{low}$$

Generally: $Z_{tot}(\omega) = H_{cable}(\omega) \cdot H_{filter}(\omega) \cdot H_{amp}(\omega) \cdot \ldots \cdot Z_t(\omega)$

Remark: For numerical calculations, time domain filters (FIR and IIR) are more appropriate

Examples for differentiated & proportional Shape

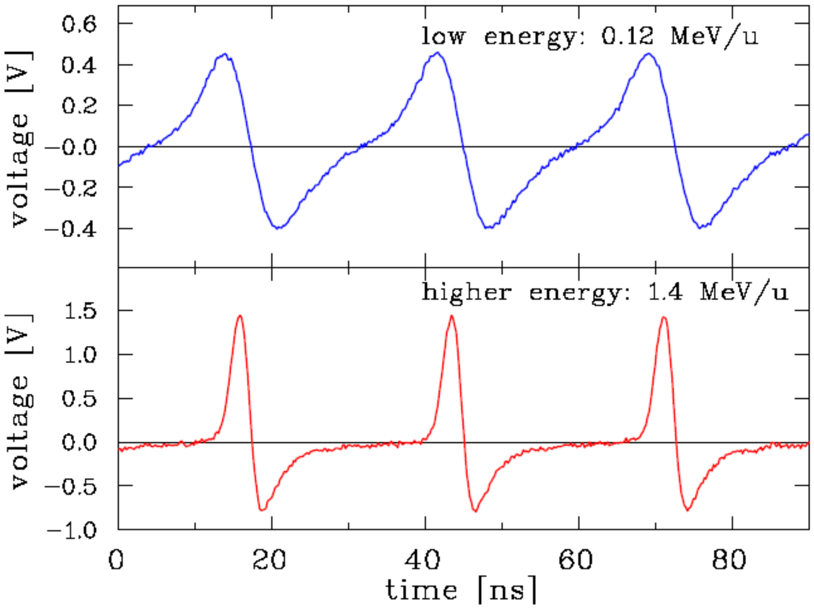
Proton LINAC, e⁻-LINAC&synchrotron:

100 MHz < f_{rf} < 1 GHz typically

R=50 Ω processing to reach bandwidth

$C\approx 5$ pF ⇒ $f_{cut} = 1/(2\pi RC) \approx$ 700 MHz

Example: 36 MHz GSI ion LINAC



Proton synchrotron:

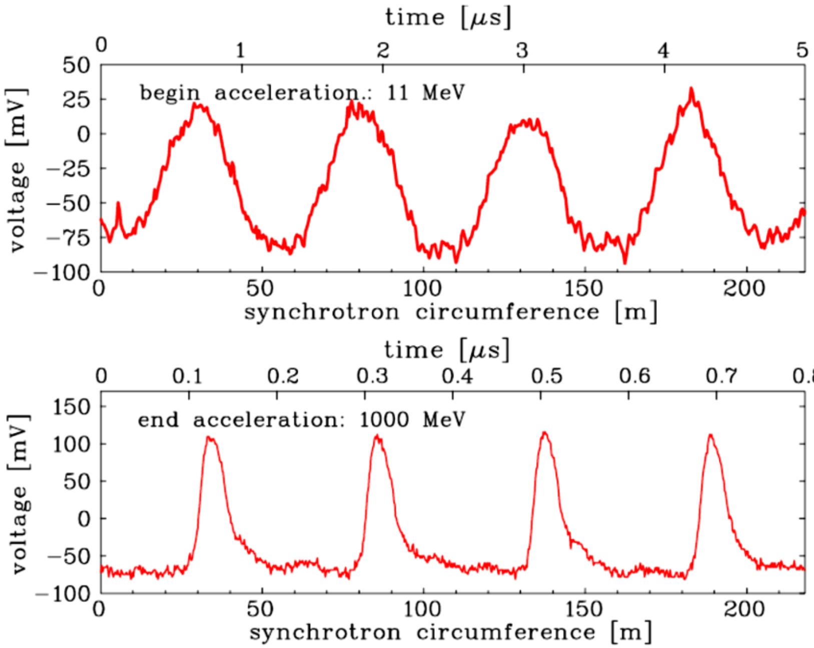
1 MHz < f_{rf} < 30 MHz typically

R=1 MΩ for large signal i.e. large Z_t

$C\approx 100$ pF ⇒ $f_{cut} = 1/(2\pi RC) \approx$10 kHz

Example: non-relativistic GSI synchrotron

f_{rf} : 0.8 MHz → 5 MHz



Remark: During acceleration the bunching-factor is increased: 'adiabatic damping'.

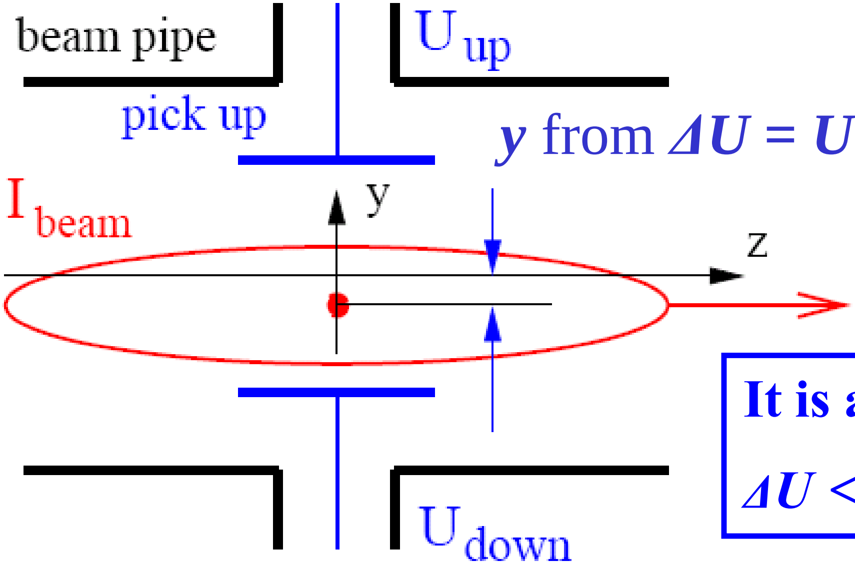
The difference voltage between plates gives the beam's center-of-mass
→**most frequent application**

'Proximity' effect leads to different voltages at the plates:

$$y = \frac{1}{S_y(\omega)} \cdot \frac{U_{up} - U_{down}}{U_{up} + U_{down}} + \delta_y(\omega)$$

$$\equiv \frac{1}{S_y} \cdot \frac{\Delta U_y}{\Sigma U_y} + \delta_y$$

$$x = \frac{1}{S_x(\omega)} \cdot \frac{U_{right} - U_{left}}{U_{right} + U_{left}} + \delta_x(\omega)$$

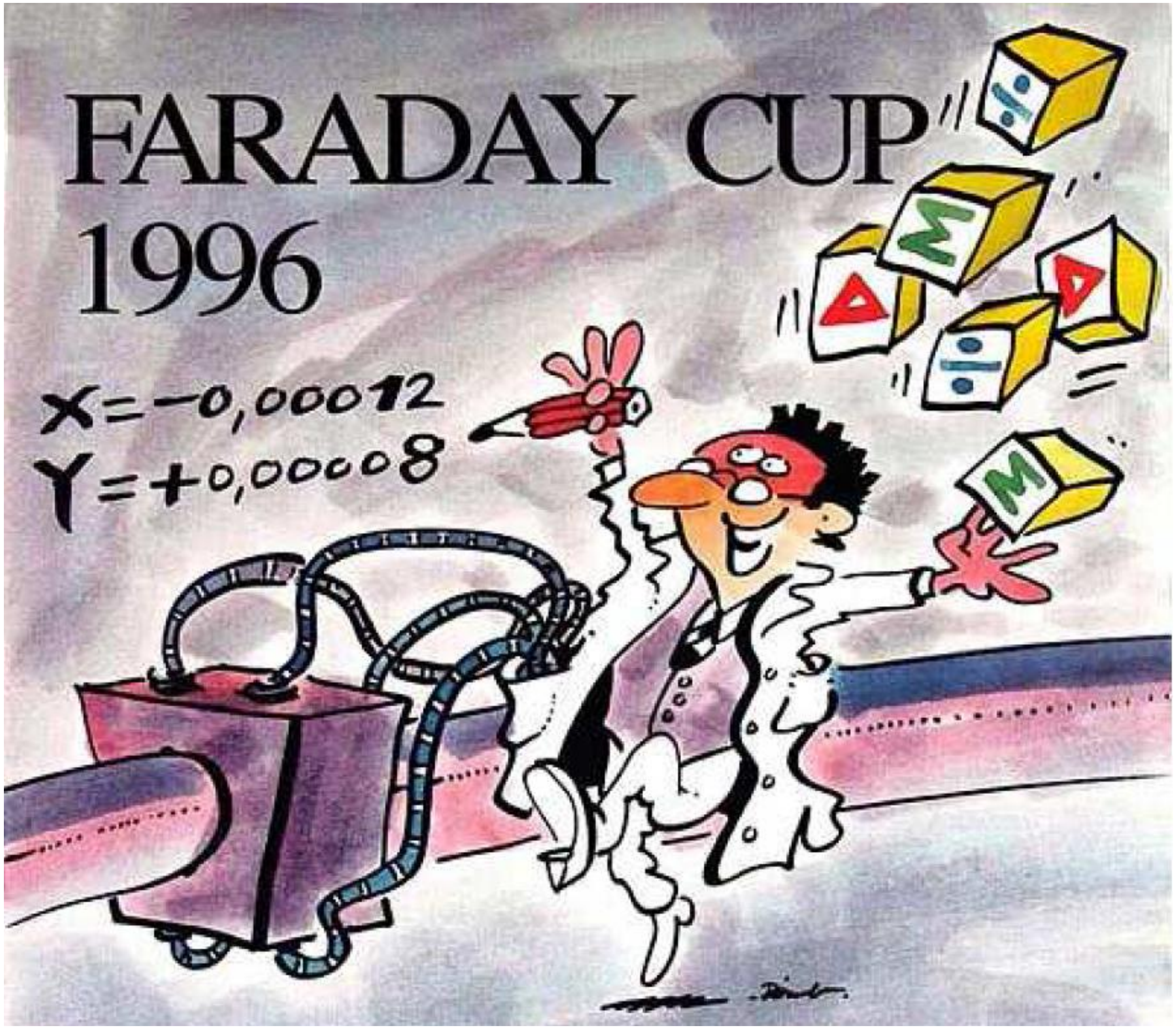


y **from** $\Delta U = U_{up} - U_{down}$

It is at least:
$\Delta U \ll \Sigma U / 10$

S(ω,x) is called **position sensitivity,** sometimes the inverse is used ***k(ω,x)=1/S(ω,x)***
S is a geometry dependent, non-linear function, which have to be optimized
Units: ***S***=[%/mm] and sometimes ***S***=[dB/mm] or ***k***=[mm].

The Artist View of a BPM



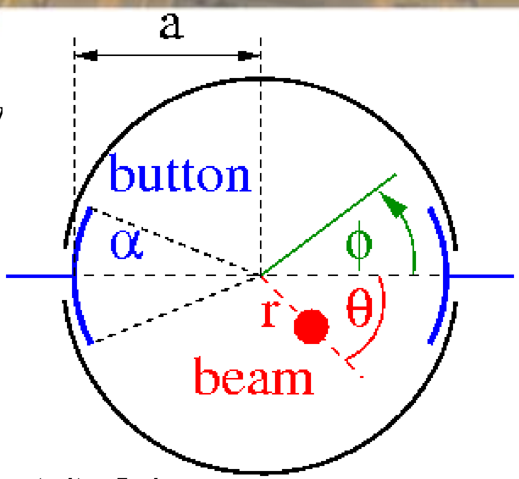
Outline:

- ➢ Signal generation → transfer impedance
- ➢ Capacitive ***button*** BPM for high frequencies

  used at most proton LINACs and electron accelerators
- ➢ Capacitive *shoe-box* BPM for low frequencies
- ➢ Electronics for position evaluation
- ➢ BPMs for measurement of closed orbit, tune and further lattice functions
- ➢ Summary

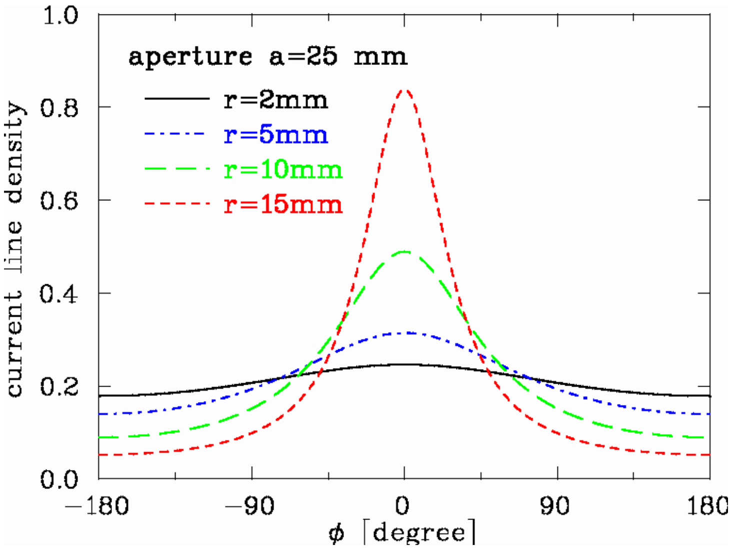
‘Proximity effect’: larger signal for closer plate

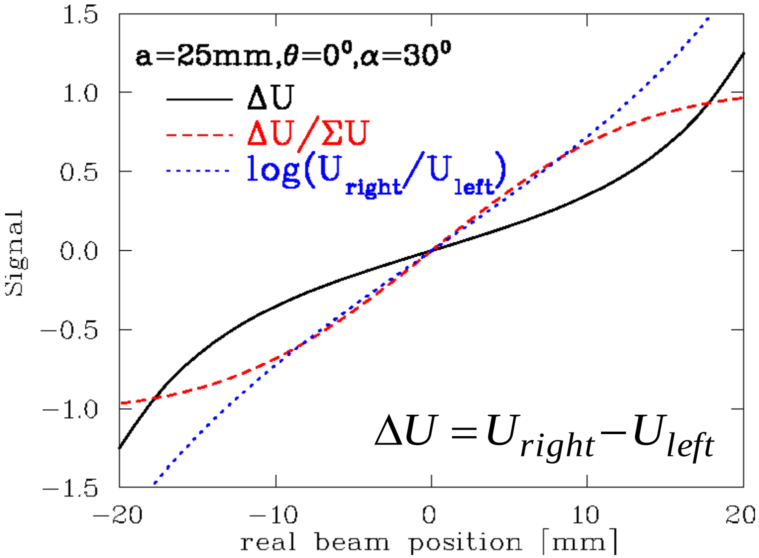
Ideal 2-dim model: Cylindrical pipe → image current density via ‘image charge method’ for ‘pensile’ beam:

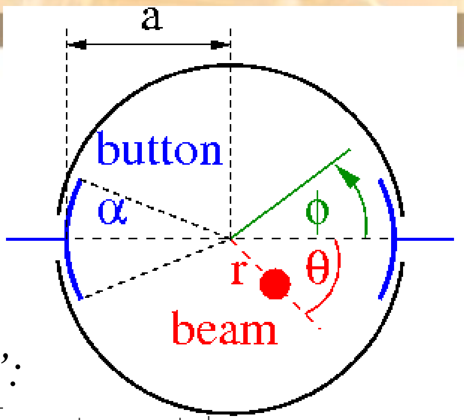


$$j_{im}(\phi) = \frac{I_{beam}}{2\pi a} \cdot \left(\frac{a^2 - r^2}{a^2 + r^2 - 2ar \cdot \cos(\phi - \theta)} \right)$$

Image current: Integration of finite BPM size: $I_{im} = a \cdot \int_{-\alpha/2}^{\alpha/2} j_{im}(\phi) d\phi$





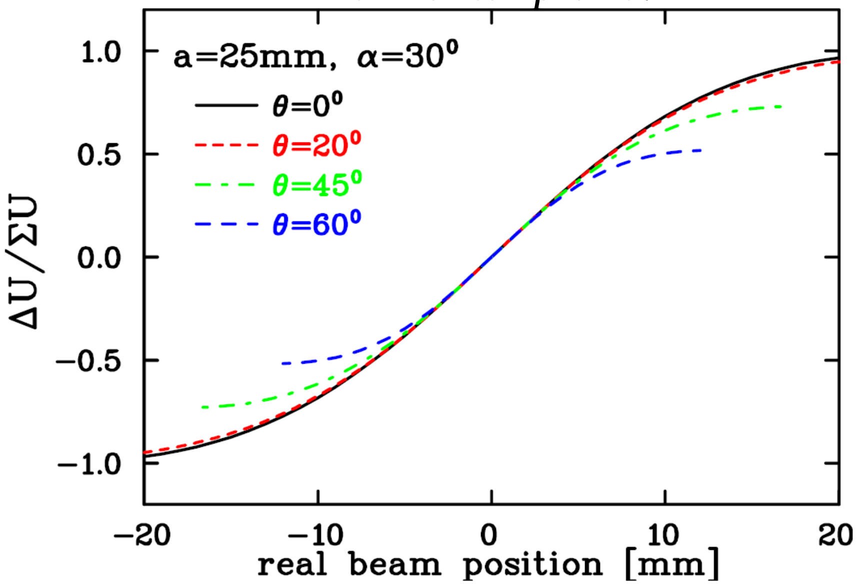


Ideal 2-dim model: Non-linear behavior and hor-vert coupling:

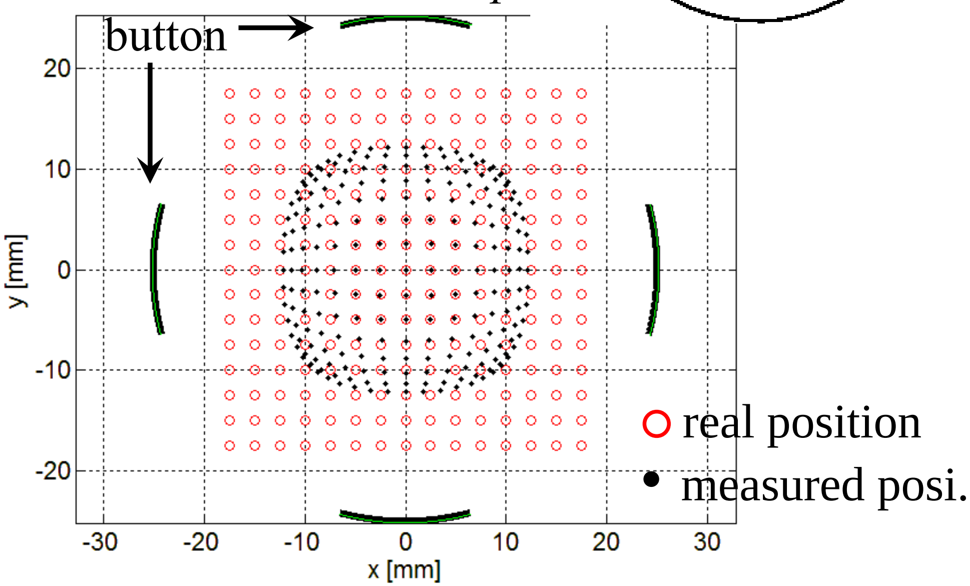
Sensitivity: $x=1/S \cdot \Delta U/\Sigma U$ with S [%/mm] or [dB/mm]

For this example: center part S=7.4%/mm ⇔ $k=1/S$=14mm

Horizontal plane:



'Position Map':



The measurement of U delivers: $x = \frac{1}{S_x} \cdot \frac{\Delta U}{\Sigma U}$ → here $S_x = S_x(x, y)$ i.e. non-linear.

Button BPM Realization

LINACs, e⁻-synchrotrons: 100 MHz < f_{rf} < 3 GHz → bunch length ≈ BPM length

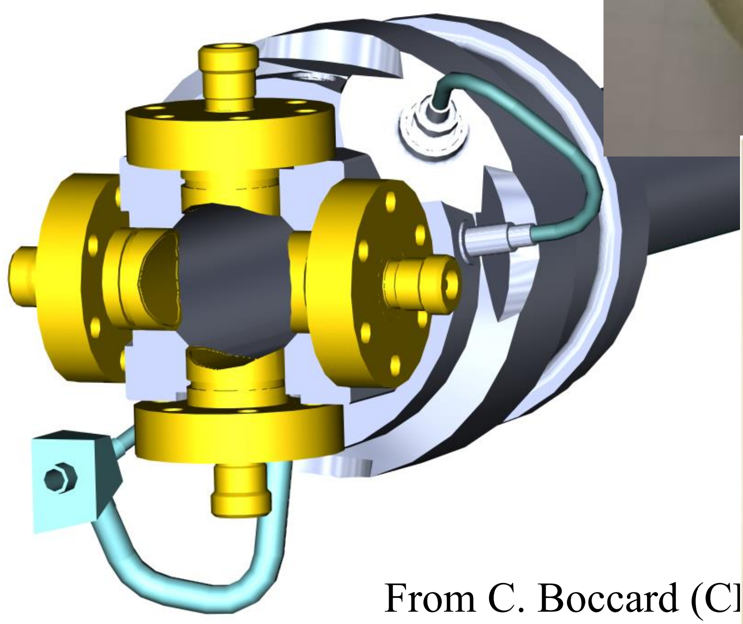
→ 50 Ω signal path to prevent reflections

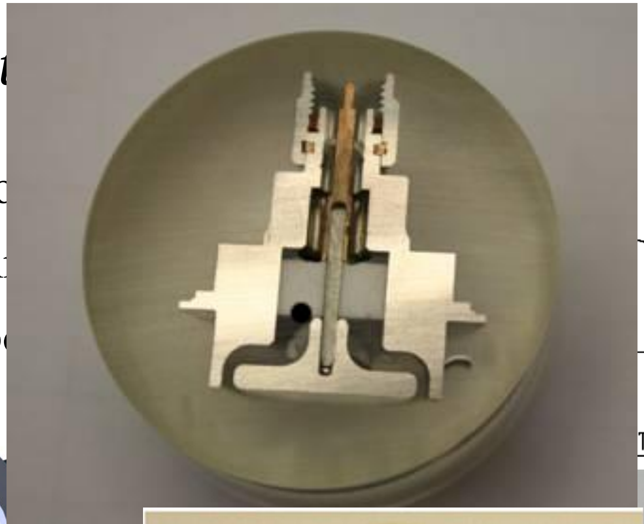
Button BPM with 50 Ω ⇒ $U_{im}(t$

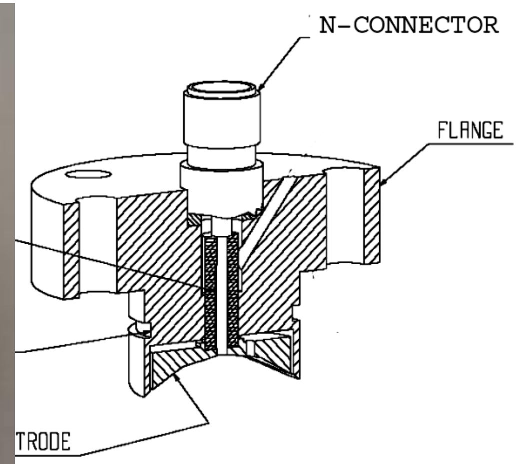
Example: LHC-type inside cryo

∅24 mm, half aperture a=25 m

⇒ f_{cut}=400 MHz, Z_t = 1.3 Ω ab



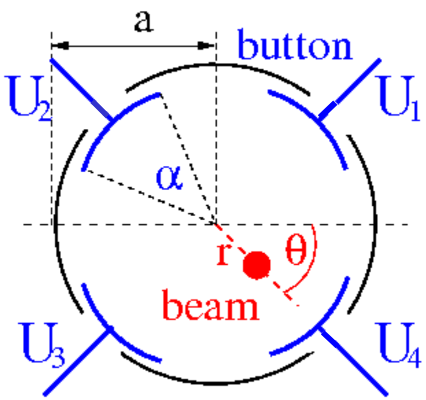




From C. Boccard (Cl

The button BPM can be rotated by 45^0 to avoid exposure by synchrotron light:

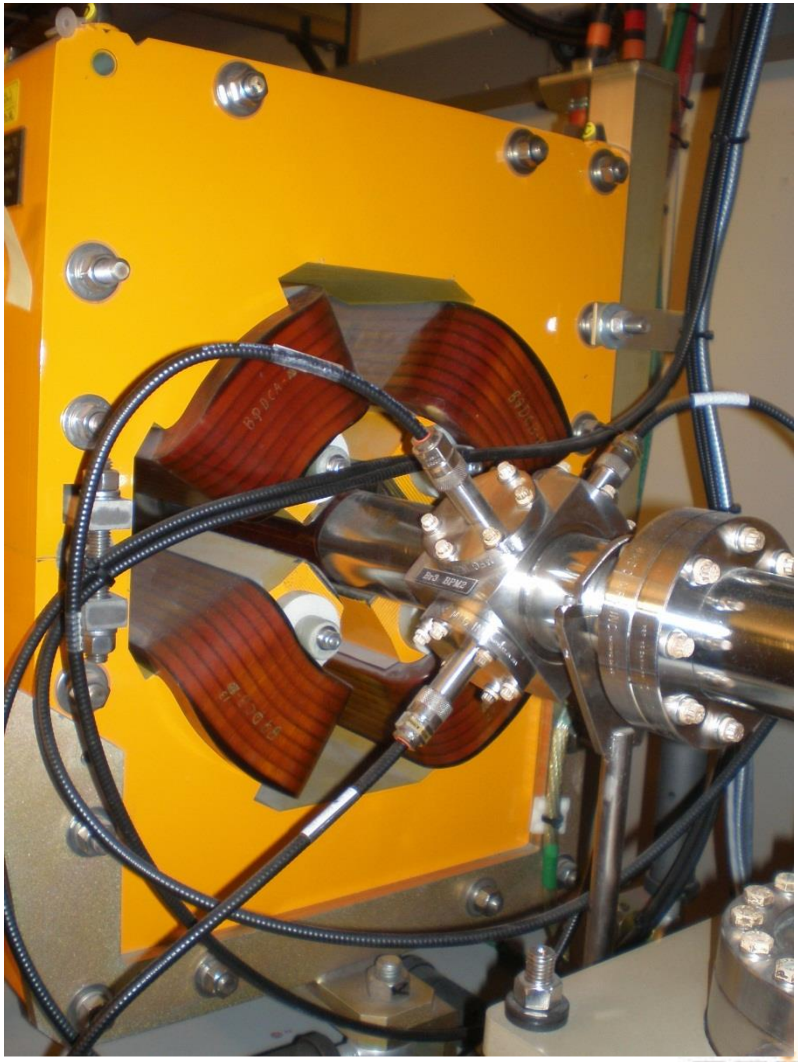
Frequently used at boosters for light sources



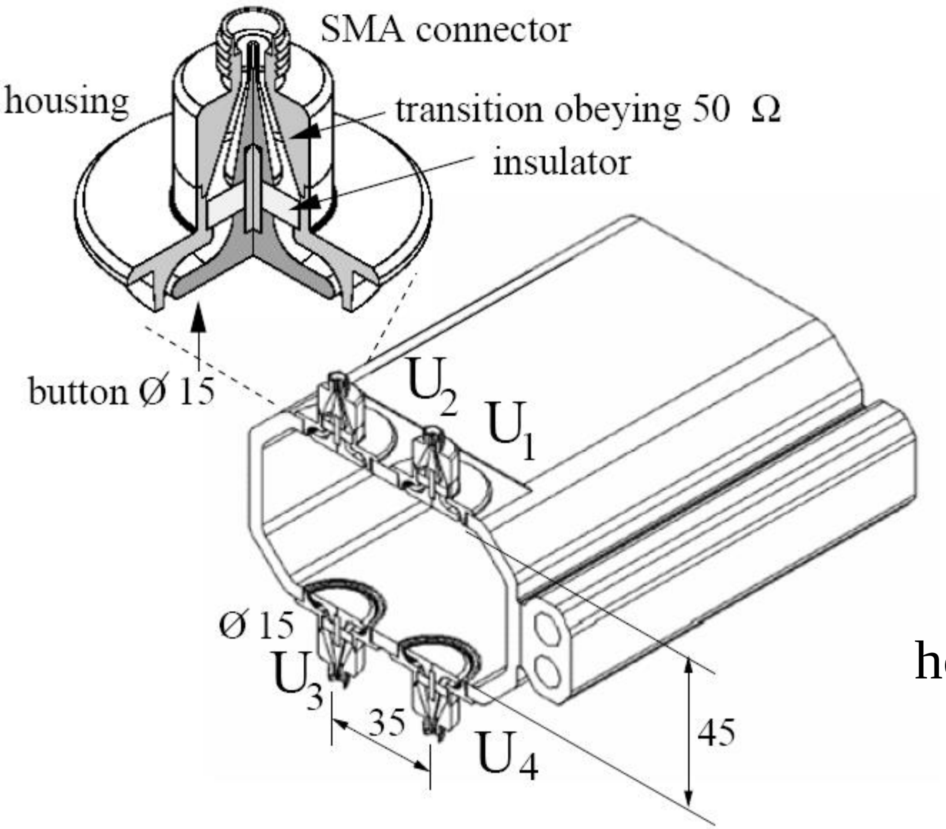
$$\text{horizontal}: x = \frac{1}{S} \cdot \frac{(U_1 + U_4) - (U_2 + U_3)}{U_1 + U_2 + U_3 + U_4}$$

$$\text{vertical}: \quad y = \frac{1}{S} \cdot \frac{(U_1 + U_2) - (U_3 + U_4)}{U_1 + U_2 + U_3 + U_4}$$

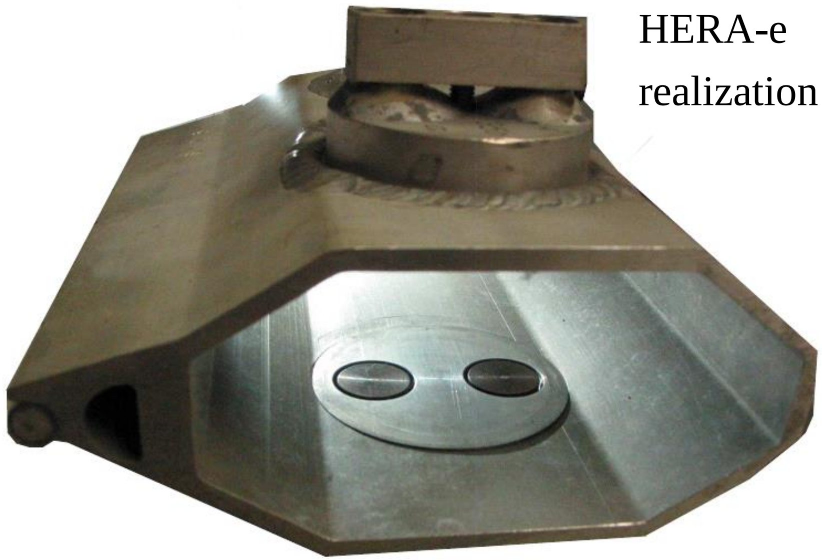
Example: Booster of ALS, Berkeley



Due to synchrotron radiation, the button insulation might be destroyed
⇒buttons only in vertical plane possible ⇒ increased non-linearity



PEP-realization



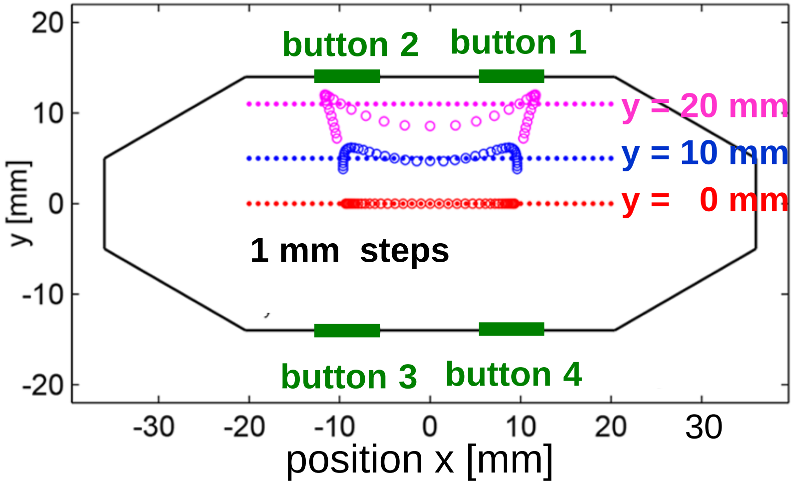
HERA-e realization

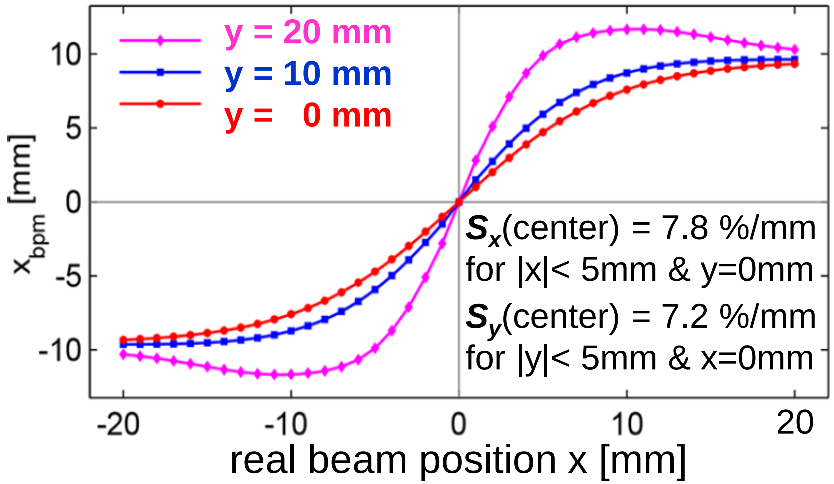
$$\text{horizontal}: x = \frac{1}{S_x} \cdot \frac{(U_1 + U_4) - (U_2 + U_3)}{U_1 + U_2 + U_3 + U_4}$$

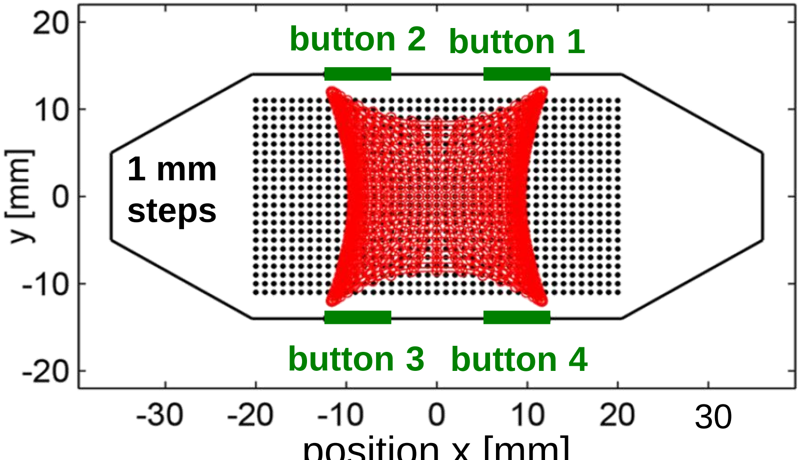
$$\text{vertical}: y = \frac{1}{S_y} \cdot \frac{(U_1 + U_2) - (U_3 + U_4)}{U_1 + U_2 + U_3 + U_4}$$

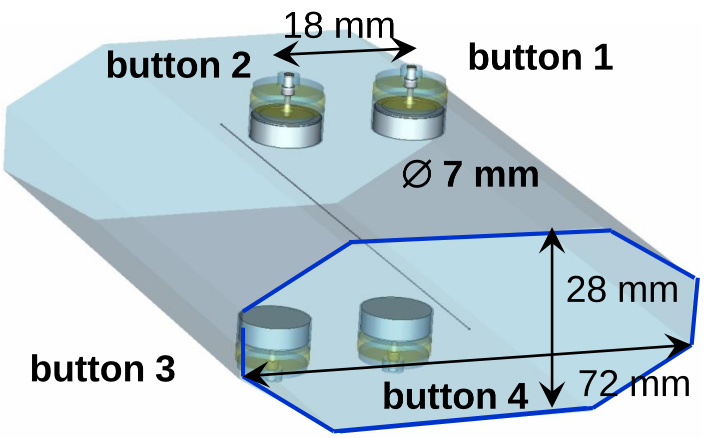
Example: Simulation for ALBA light source for 72 x 28 mm² chamber

Optimization: horizontal distance and size of buttons









Result: non-linearities and xy-coupling occur in dependence of button size and position

Outline:

- Signal generation → transfer impedance
- Capacitive *button* BPM for high frequencies

  used at most proton LINACs and electron accelerators
- Capacitive *shoe-box* BPM for low frequencies

  used at most proton synchrotrons due to linear position reading
- Electronics for position evaluation
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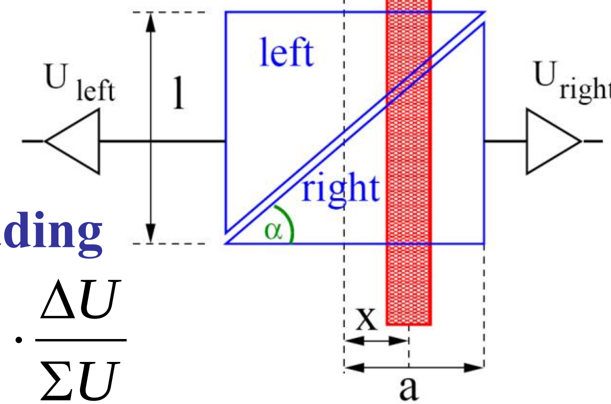
- Summary

Frequency range: 1 MHz < f_{rf} < 10 MHz ⇒ bunch-length >> BPM length.

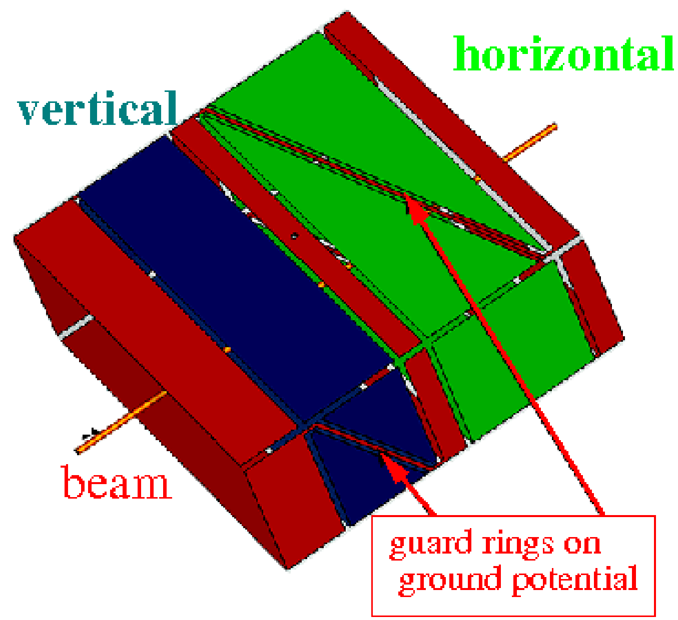
Signal is proportional to actual plate length:

$$l_{right} = (a+x)\cdot\tan\alpha, \quad l_{left} = (a-x)\cdot\tan\alpha$$

$$\Rightarrow \quad x = a \cdot \frac{l_{right} - l_{left}}{l_{right} + l_{left}}$$

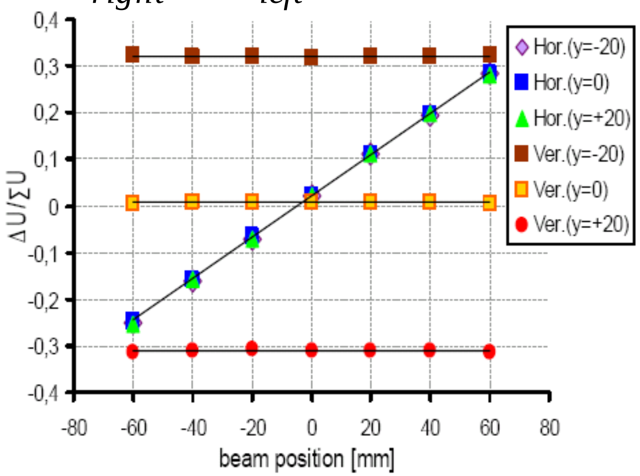


Size: 200x70 mm²



In ideal case: linear reading

$$x = a \cdot \frac{U_{right} - U_{left}}{U_{right} + U_{left}} \equiv a \cdot \frac{\Delta U}{\Sigma U}$$



Shoe-box BPM:

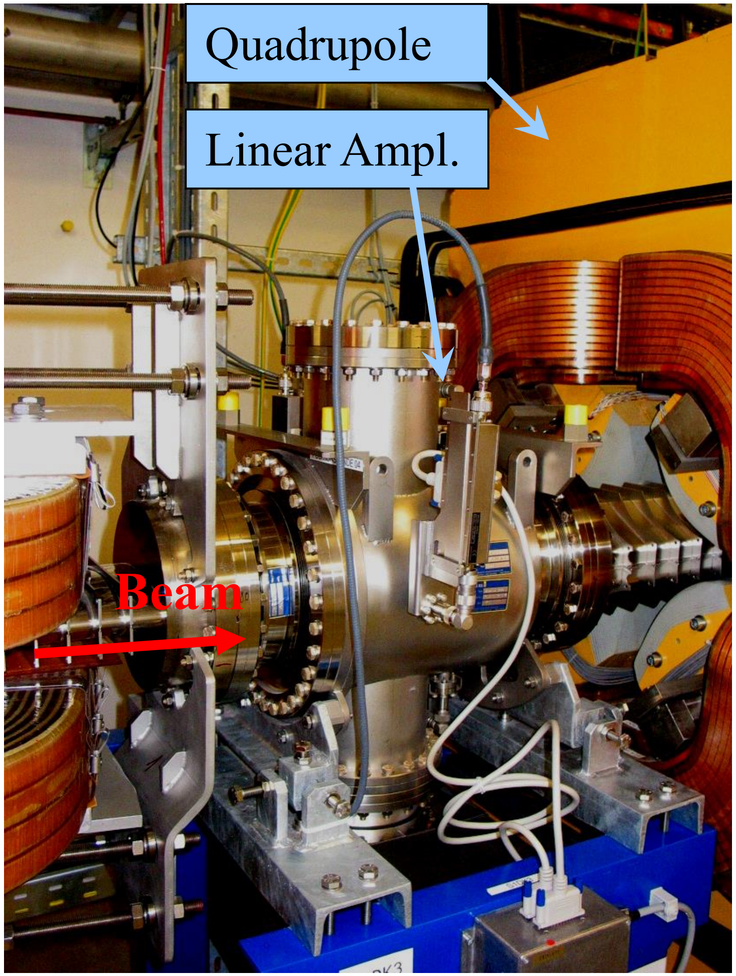
Advantage: Very linear, low frequency dependence
i.e. position sensitivity ***S*** is constant

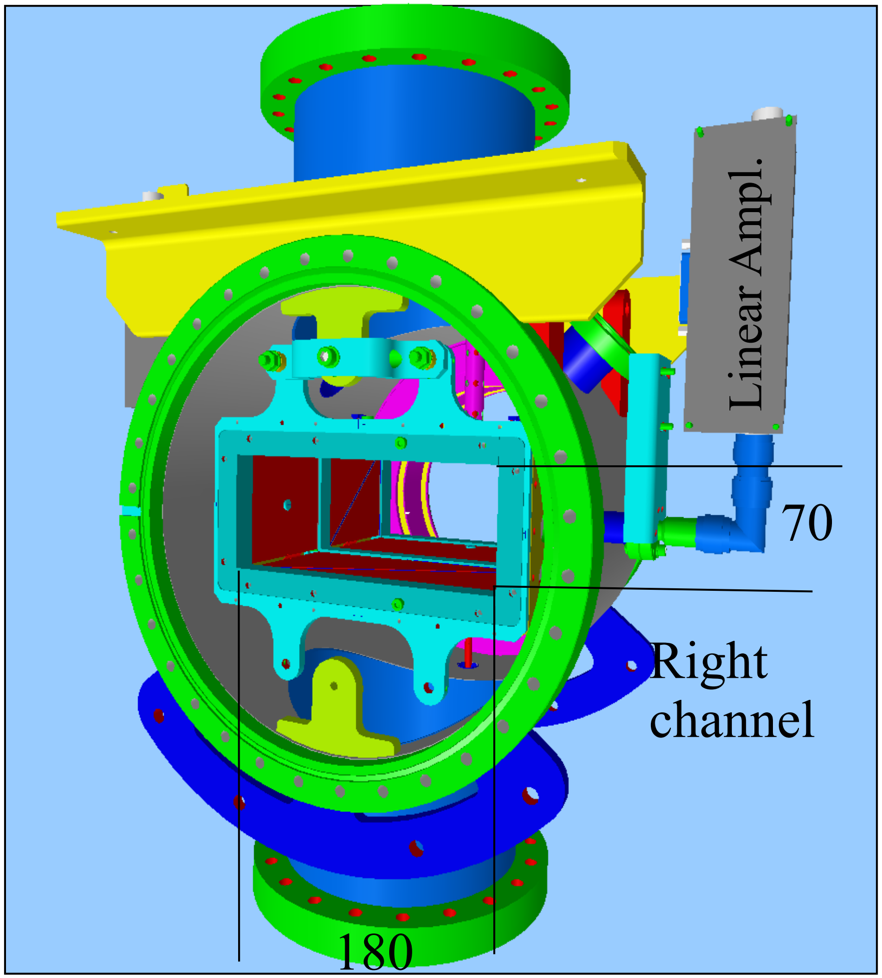
Disadvantage: Large size, complex mechanics
high capacitance

Technical Realization of a Shoe-Box BPM

Technical realization at HIT synchrotron of 46 m length for 7 MeV/u→ 440 MeV/u

BPM clearance: 180x70 mm^2, standard beam pipe diameter: 200 mm.





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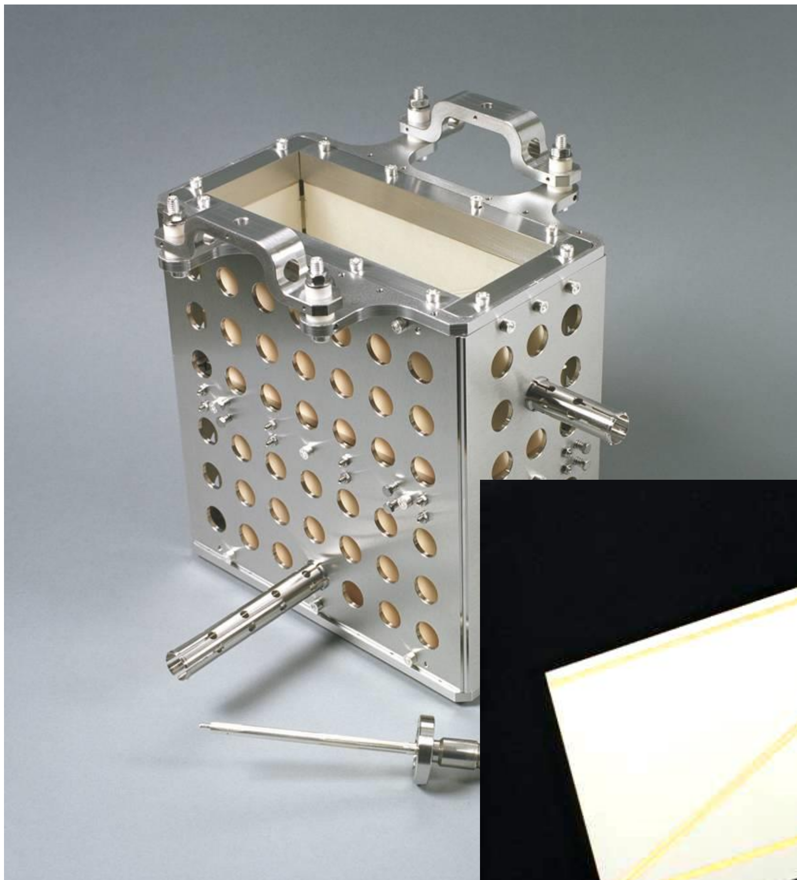
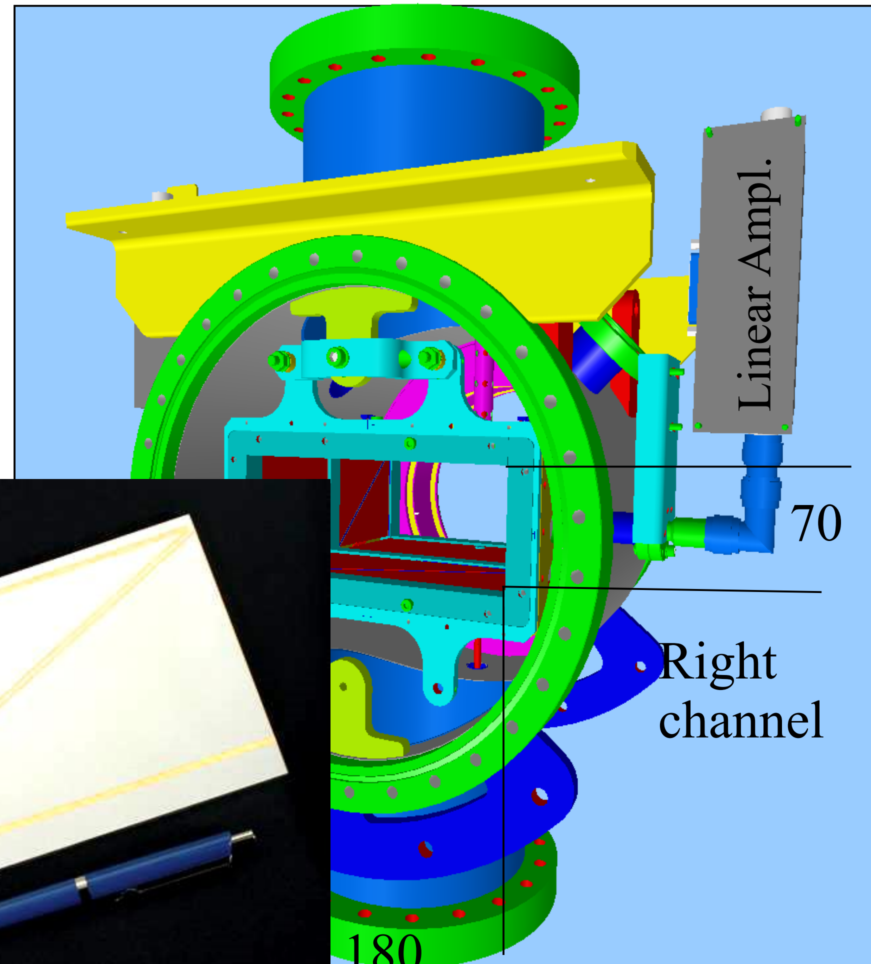
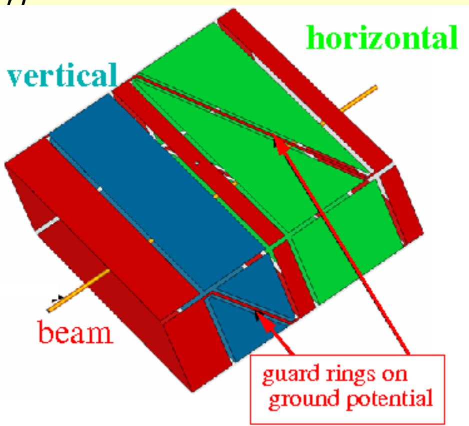
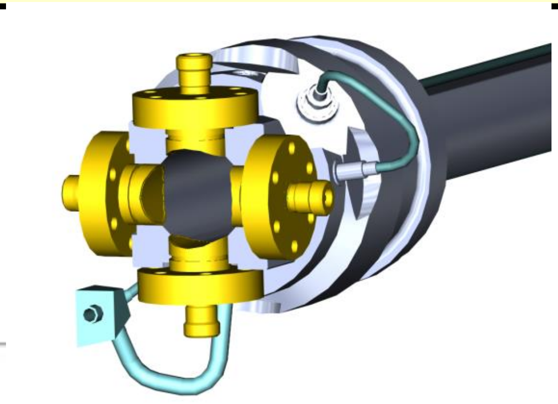




Comparison Shoe-Box and Button BPM

	Shoe-Box BPM	Button BPM
Precaution	Bunches longer than BPM	Bunch length comparable to BPM
BPM length (typical)	10 to 20 cm length per plane	∅1 to 5 cm per button
Shape	Rectangular or cut cylinder	Orthogonal or planar orientation
Bandwidth (typical)	0.1 to 100 MHz	100 MHz to 5 GHz
Coupling	1 MΩ or ≈1 kΩ (transformer)	50 Ω
Cutoff frequency (typical)	0.01… 10 MHz (C=30…100pF)	0.3… 1 GHz (C=2…10pF)
Linearity	Very good, no x-y coupling	Non-linear, x-y coupling
Sensitivity	Good, care: plate cross talk	Good, care: signal matching
Usage	At proton synchrotrons, $f_{rf} < 10$ MHz	All electron acc., proton Linacs, $f_{rf} > 100$ MHz





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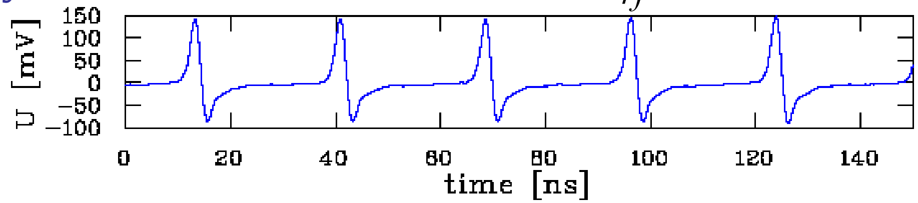
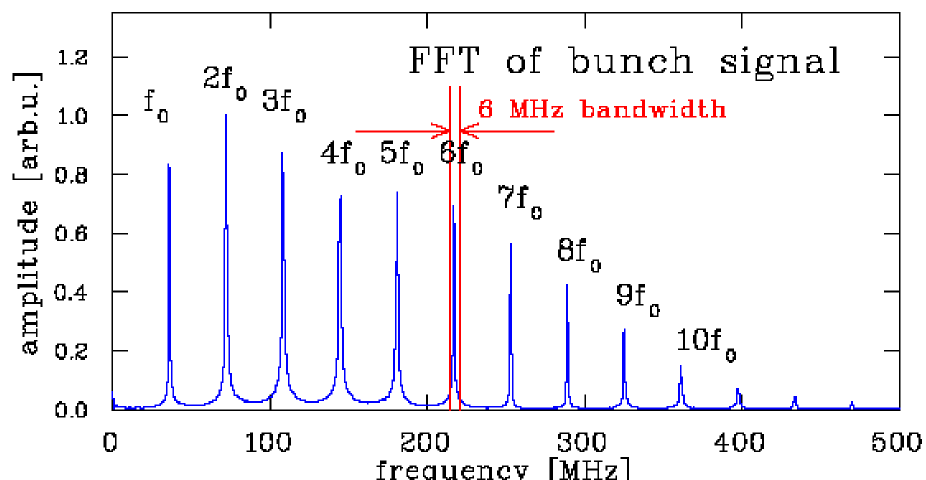
1. Signal voltage given by: $U_{im}(f) = Z_t(f) \cdot I_{beam}(f)$
2. Position information from voltage difference: $x = 1/S \cdot \Delta U / \Sigma U$
3. Thermal noise voltage given by: $U_{eff}(R, \Delta f) = \sqrt{4k_B \cdot T \cdot R \cdot \Delta f}$

$\Rightarrow$ Signal-to-noise $\Delta U_{im}/U_{eff}$ is influenced by:

- Input signal amplitude
  $\rightarrow$ large or matched Z_t
- Thermal noise at R=50 Ω for T=300 K
  (for shoe box R = 1 kΩ …1 MΩ)
- Bandwidth Δf
  $\Rightarrow$ Restriction of frequency width because the power is concentrated on the harmonics of f_{rf}

Example: GSI-LINAC with f_{rf}=36 MHz

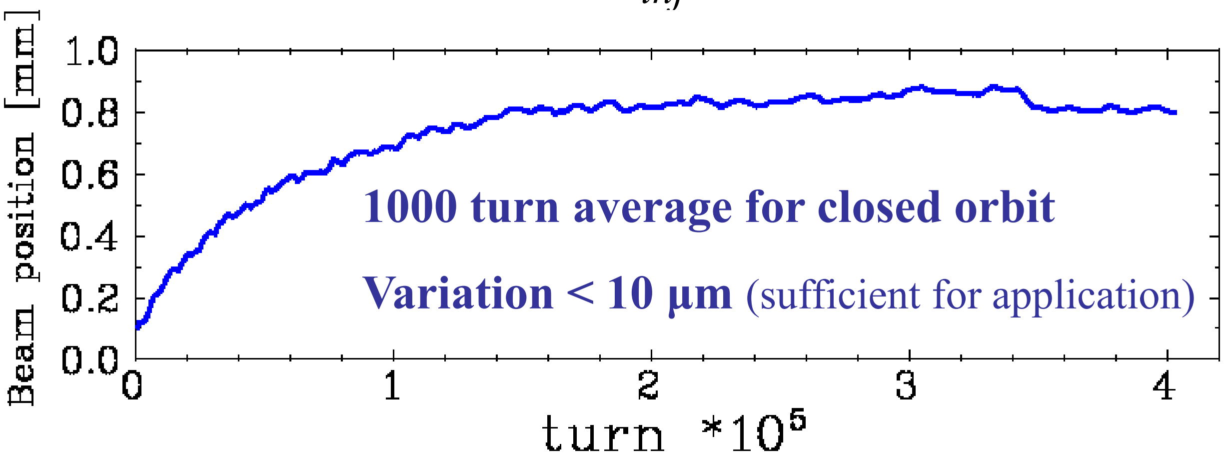




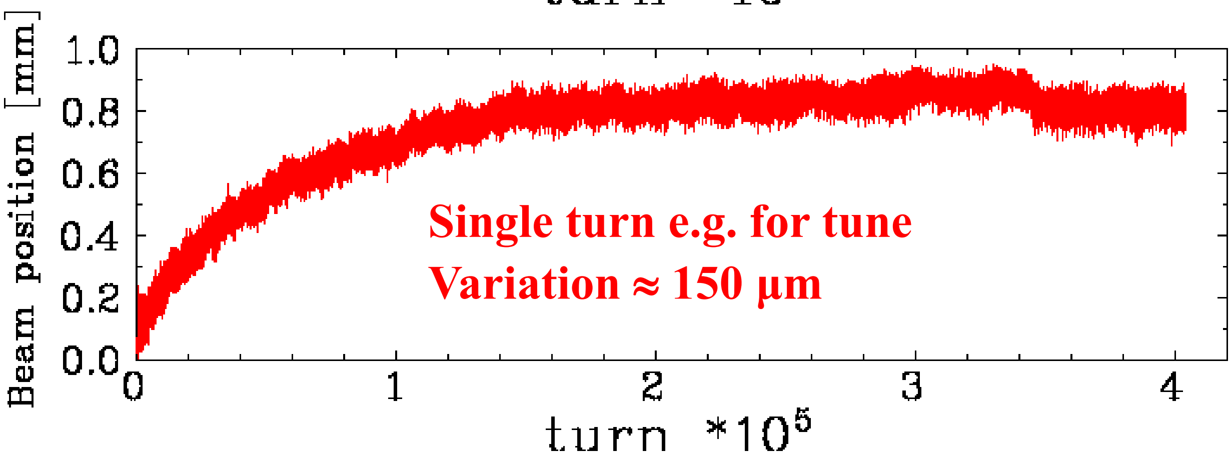
Remark: Additional contribution by non-perfect electronics typically a factor 2

Moreover, pick-up by electro-magnetic interference can contribute $\Rightarrow$ good shielding required

Example: GSI Synchr.: U^{73+}, E_{inj}=11.5 MeV/u→ 250 MeV/u within 0.5 s, 10^9 ions

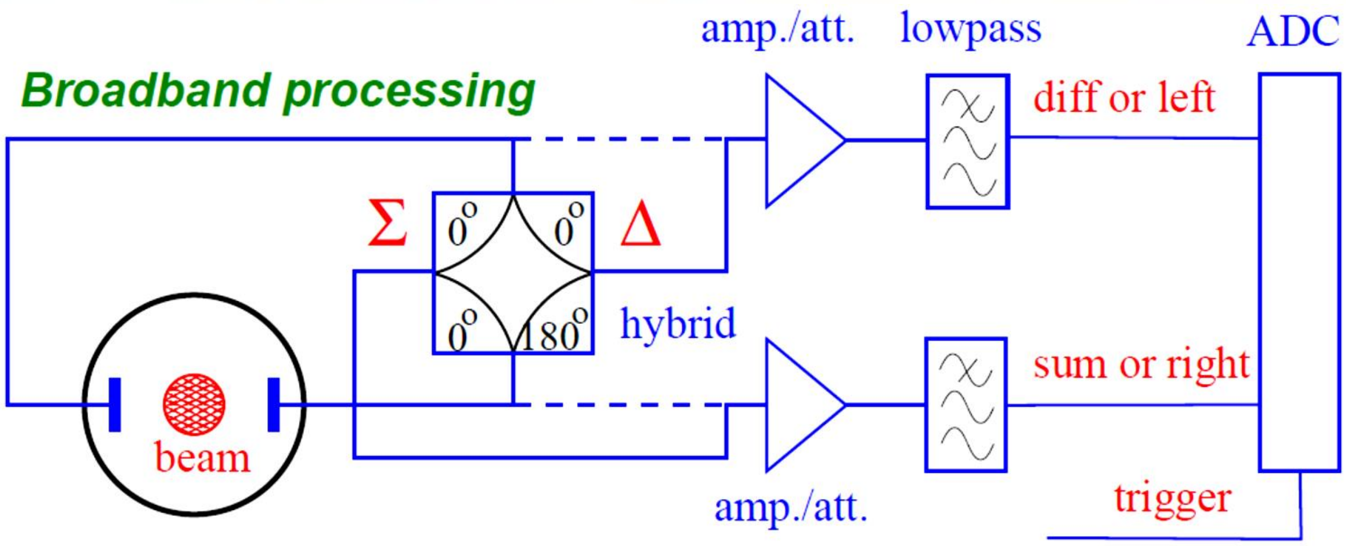


- Position resolution < 30 µm (BPM half aperture *a*=90 mm)
- average over 1000 turns corresponding to ≈1 ms or ≈1 kHz bandwidth



- Turn-by-turn data have much larger variation

However: not only noise contributes but additionally **beam movement** by betatron oscillation
⇒ broadband processing i.e. turn-by-turn readout for tune determination.

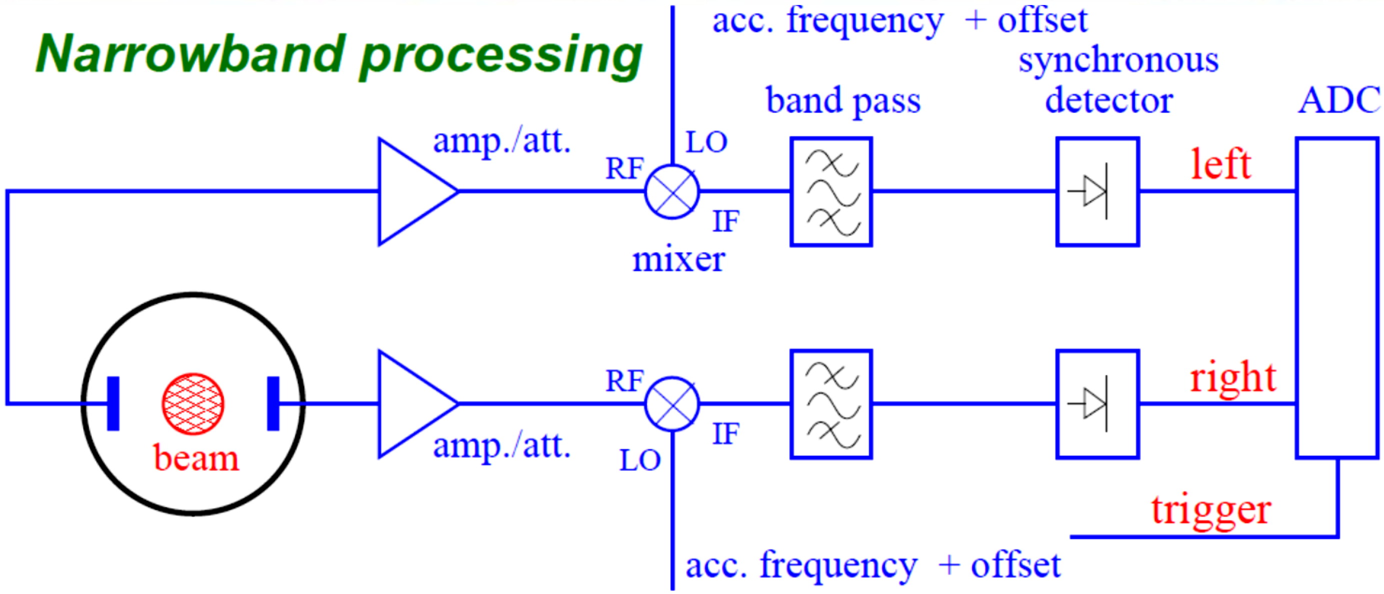


- Hybrid or transformer close to beam pipe for analog ΔU & ΣU generation or U_{left} & U_{right}
- Attenuator/amplifier
- Filter to get the wanted harmonics and to suppress stray signals
- ADC: digitalization ⟶ followed by calculation of of $\Delta U / \Sigma U$

Advantage: Bunch-by-bunch possible, versatile post-processing possible

Disadvantage: Resolution down to ≈ 100 µm for shoe box type , i.e. ≈0.1% of aperture, resolution is worse than narrowband processing

Narrowband Processing for improved Signal-to-Noise



Narrowband processing equals heterodyne receiver (e.g. AM-radio or spectrum analyzer)

- Attenuator/amplifier
- Mixing with accelerating frequency $f_{rf} \Rightarrow$ signal with sum and difference frequency
- Bandpass filter of the mixed signal (e.g at 10.7 MHz)
- Rectifier: synchronous detector
- ADC: digitalization $\longrightarrow$ followed calculation of $\Delta U/\Sigma U$

Advantage: spatial resolution about 100 time better than broadband processing

Disadvantage: No turn-by-turn diagnosis, due to mixing = 'long averaging time'

For non-relativistic p-synchrotron: $\rightarrow$ variable f_{rf} leads via mixing to constant intermediate freq.

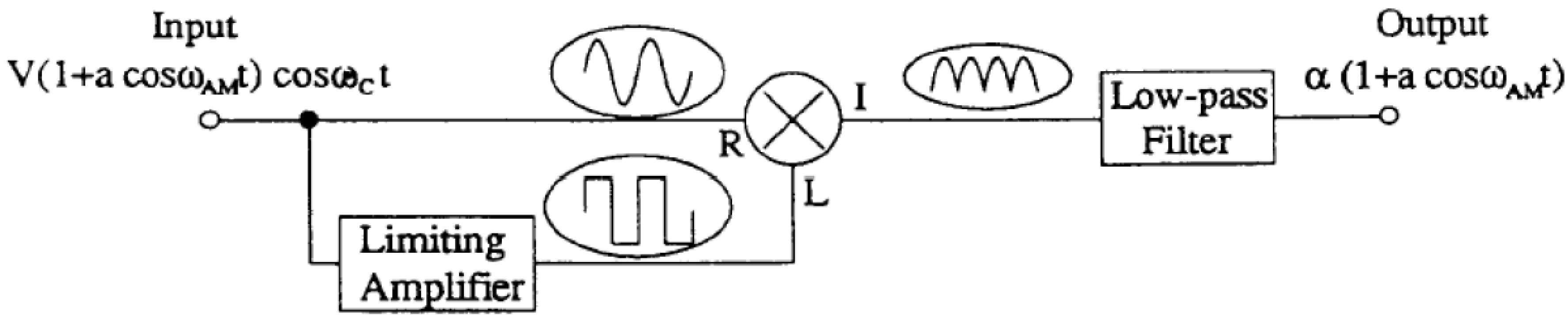
Mixer: A passive rf device with

- Input RF (radio frequency): Signal of investigation $A_{RF}(t) = A_{RF}\cos\omega_{RF}t$
- Input LO (local oscillator): Fixed frequency $A_{LO}(t) = A_{LO}\cos\omega_{LO}t$
- Output IF (intermediate frequency)

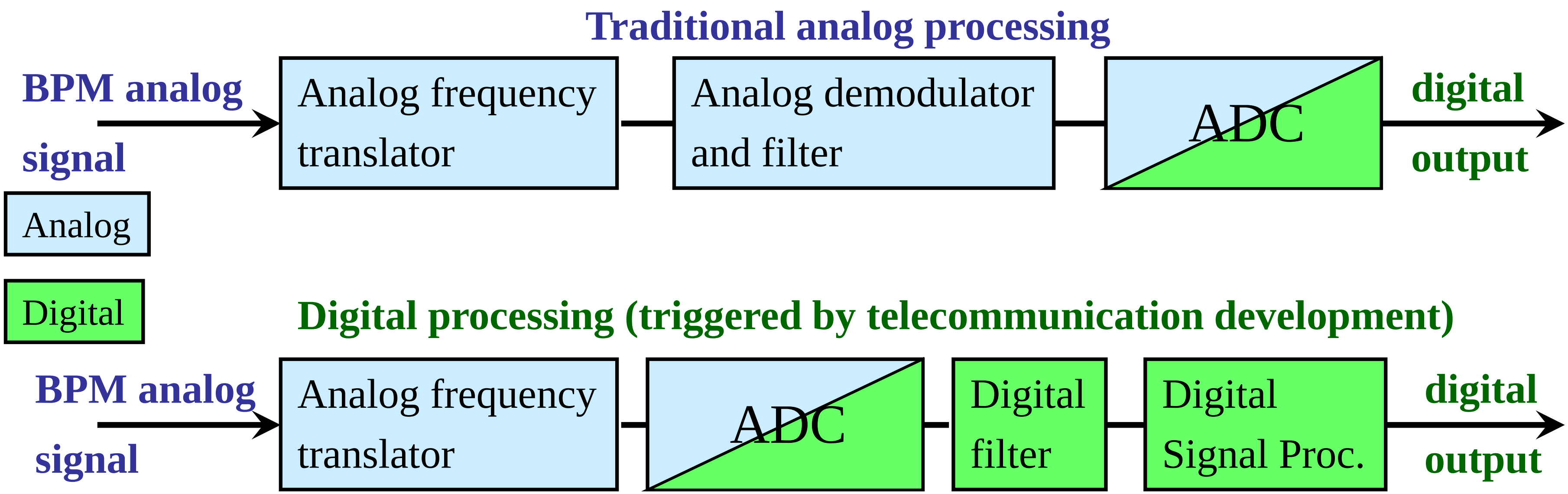
$$A_{IF}(t) = A_{RF}\cdot A_{LO}\cos\omega_{RF}t\cdot\cos\omega_{LO}t$$
$$= A_{RF}\cdot A_{LO}\left[\cos(\omega_{RF}-\omega_{LO})t + \cos(\omega_{RF}+\omega_{LO})t\right]$$

$\Rightarrow$ Multiplication of both input signals, containing the sum and difference frequency.

Synchronous detector: A phase sensitive rectifier



Modern instrumentation uses **digital** techniques with extended functionality.



Digital receiver as modern successor of super heterodyne receiver

- Basic functionality is preserved but implementation is very different
- Digital transition just after the amplifier & filter or mixing unit
- Signal conditioning (filter, decimation, averaging) on FPGA

Advantage of DSP: Versatile operation, flexible adoption without hardware modification

Disadvantage of DSP: **non**, good engineering skill requires for development, expensive

Comparison of BPM Readout Electronics (simplified)

Type	Usage	Precaution	Advantage	Disadvantage
Broadband	p-sychr.	Long bunches	Bunch structure signal Post-processing possible Required for fast feedback	Resolution limited by noise
Narrowband	all synchr.	Stable beams >100 rf-periods	High resolution	No turn-by-turn Complex electronics
Digital Signal Processing	all	Several bunches ADC 125 MS/s	Very flexible High resolution **Trendsetting technology for future demands**	Limited time resolution by ADC → undersampling complex and expensive

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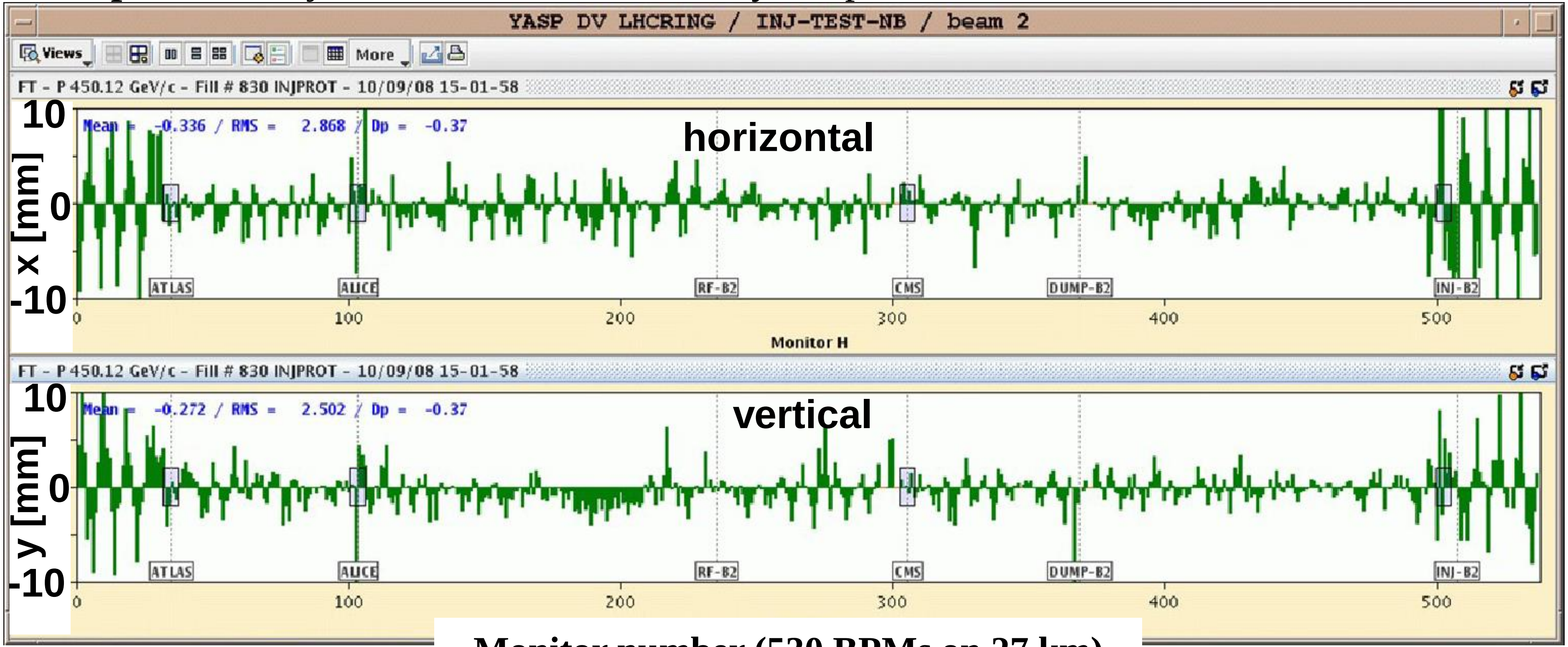
- Electronics for position evaluation
  analog signal conditioning to achieve small signal processing
- **BPMs for measurement of closed orbit, tune and further lattice functions**
  frequent application of BPMs
- Summary

Trajectory:

The position delivered by an **individual bunch** within a transfer line or a synchrotron.

Main task: Control of matching (center and angle), first-turn diagnostics

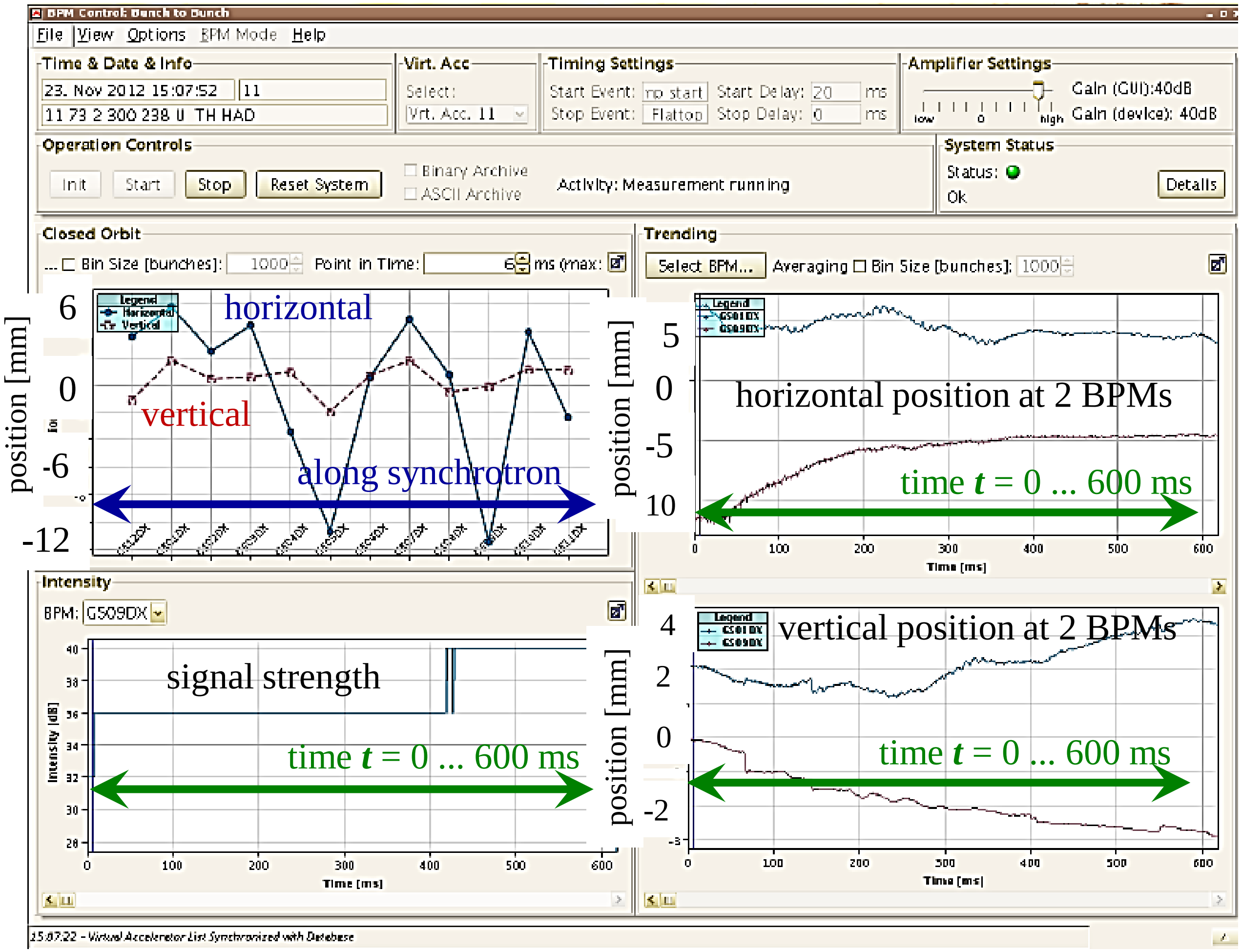
Example: LHC injection 10/09/08 i.e. first day of operation !



Monitor number (530 BPMs on 27 km)

From R. Jones (CERN)

Single bunch position averaged over 1000 bunches → closed orbit with ms time steps.
It differs from ideal orbit by misalignments of the beam or components.
Example: GSI-synchrotron at two BPM locations, 1000 turn average during acceleration:



Closed orbit:

Beam position
averaged over many turns
(i.e. betatron oscillations).
The result is the basic tool
for alignment & stabilzation

Remark as a role of thumb:

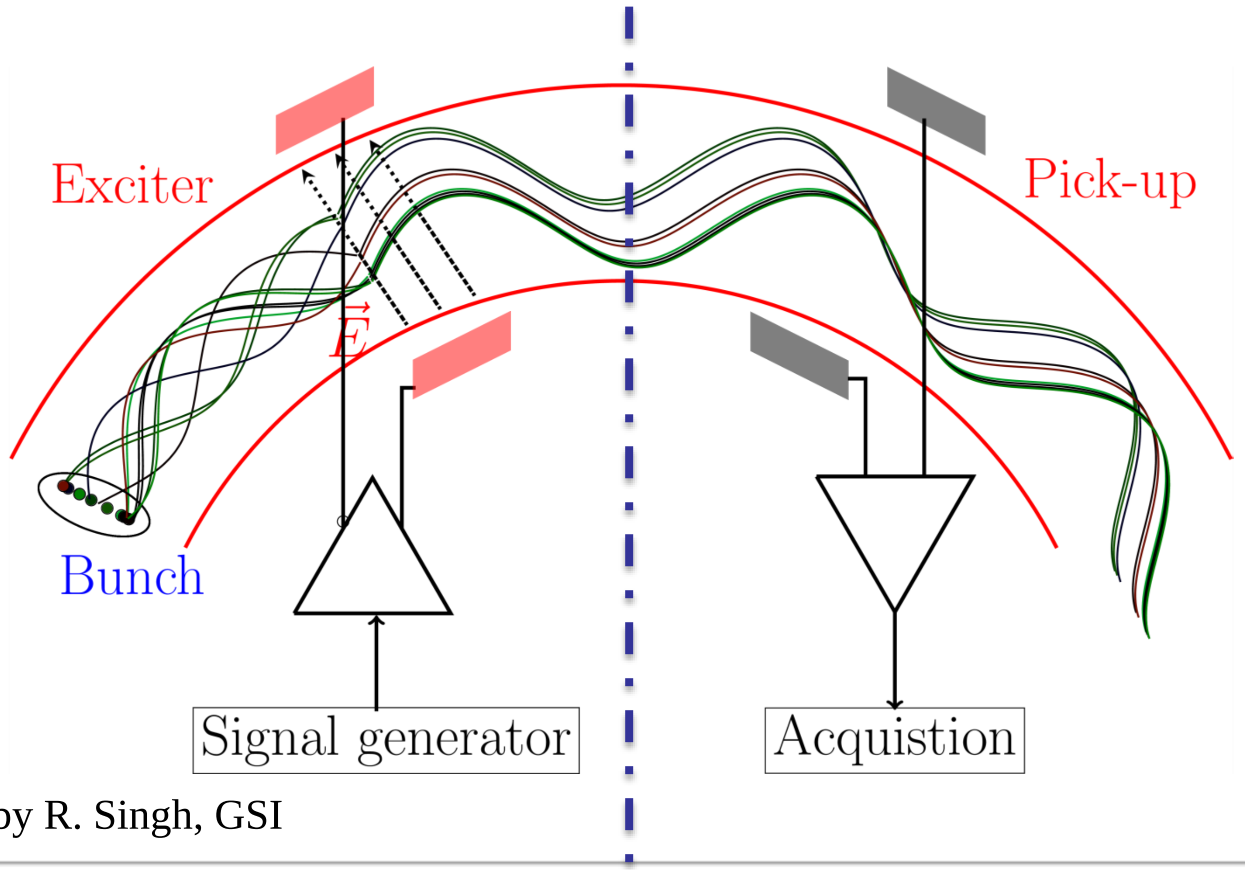
Number of BPMs within
a synchrotron: $N_{BPM} \approx 4 \cdot Q$
Relation BPMs ↔ tune due to
close orbit stabilization feedback
(justification outside of the scope
of this lecture)

Coherent excitations are required for the detection by a BPM

Beam particle's ***in-coherent*** motion ⇒ center-of-mass stays constant

Excitation of **all** particles by rf ⇒ ***coherent*** motion

⇒ center-of-mass variation turn-by-turn



Graphics by R. Singh, GSI

The tune Q is the number of betatron oscillations per turn.

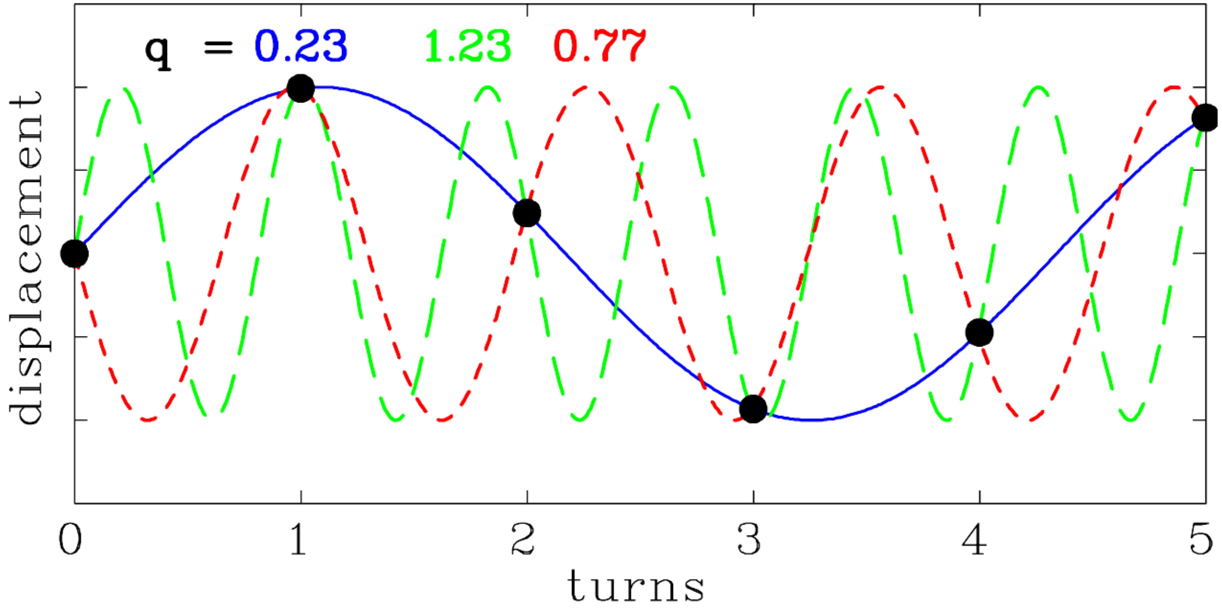
The betatron frequency is $f_\beta = Qf_0$.

Measurement: excitation of ***coherent*** betatron oscillations + position from one BPM.

From a measurement one gets only the non-integer part q of Q with $Q=n\pm q$.

Moreover, only $0 < q < 0.5$ is the unique result.

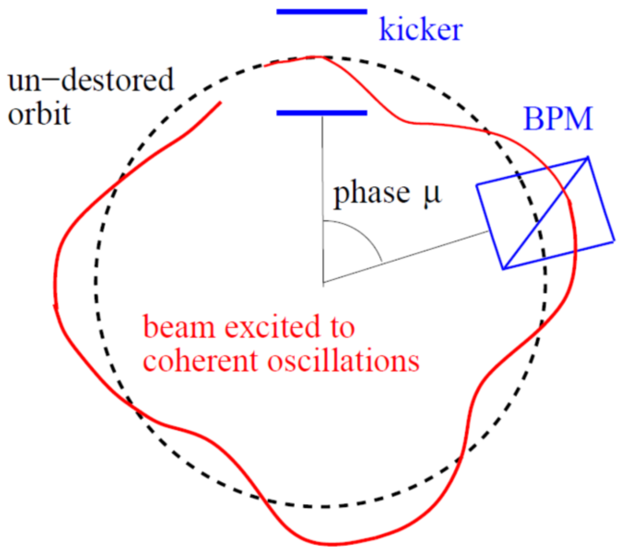
Example: Tune measurement for six turns with the three lowest frequency fits:

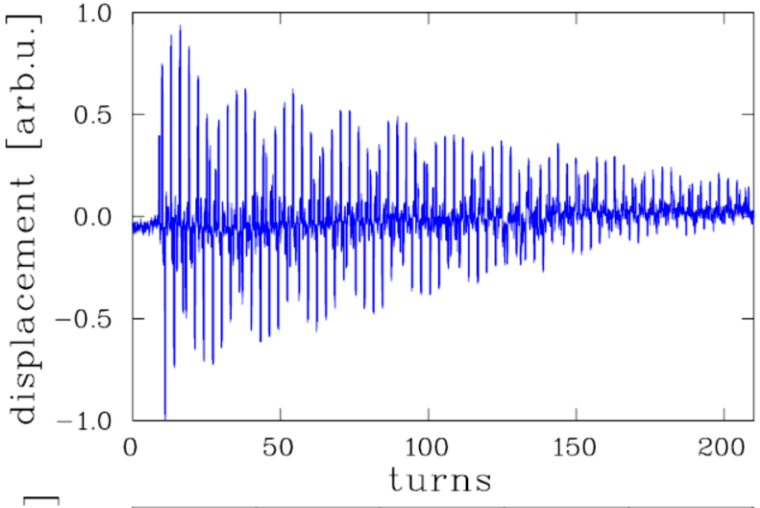


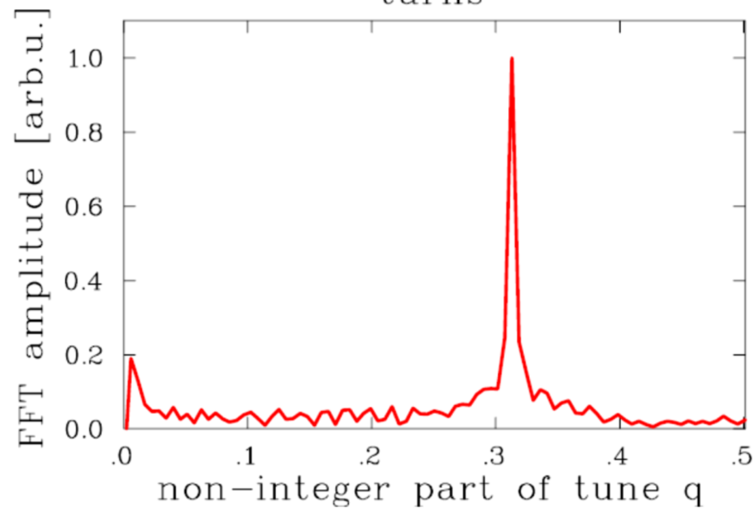
To distinguish for $q < 0.5$ or $q > 0.5$:

Changing the tune slightly, the direction of q shift differs.

The beam is excited to coherent betatron oscillation
→ the beam position measured each revolution ('turn-by-turn')
→ Fourier Trans. gives the non-integer tune ***q***.
Short kick compared to revolution.



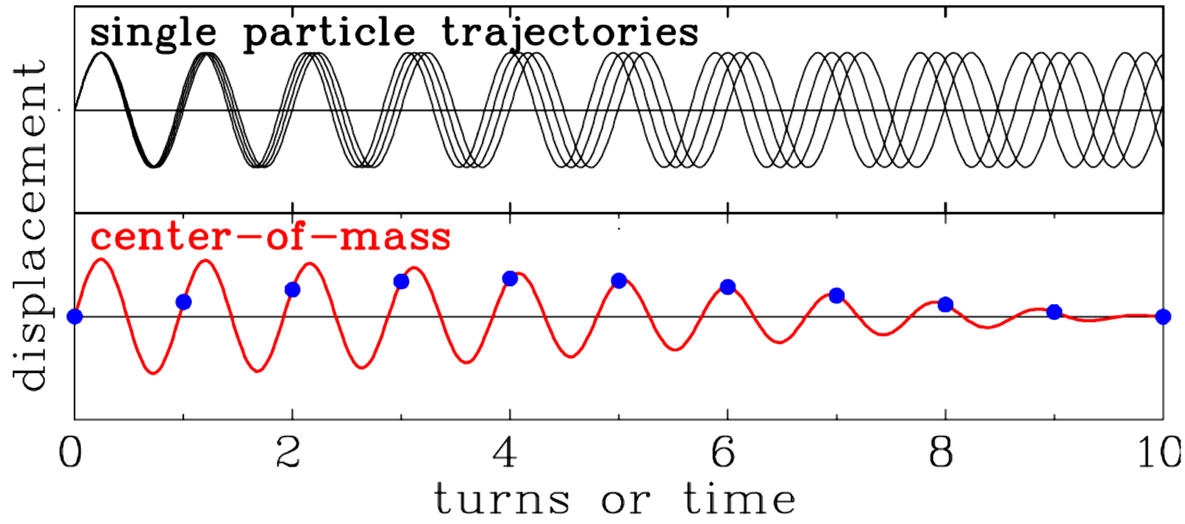




The de-coherence time limits the **resolution**:
N non-zero samples
⇒ General limit of discrete FFT: $\Delta q > \frac{1}{2N}$

N = 200 turn ⇒ ***Δq*** > 0.003 as resolution
(tune spreads are typically ***Δq*** ≈ 0.001!)

The particles are excited to betatron oscillations, but due to the spread in the betatron frequency, they getting out of phase ('Landau damping'):



Scheme of the individual trajectories of four particles after a kick (top) and the resulting ***coherent*** signal as measured by a pick-up (bottom).

⇒ Kick excitation leads to limited resolution

Remark: The tune spread is much lower for a real machine.

Instead of one kick, the beam can be excited by a sweep of a sine wave, called 'chirp'

→ **B**eam **T**ransfer **F**unction (BTF) Measurement

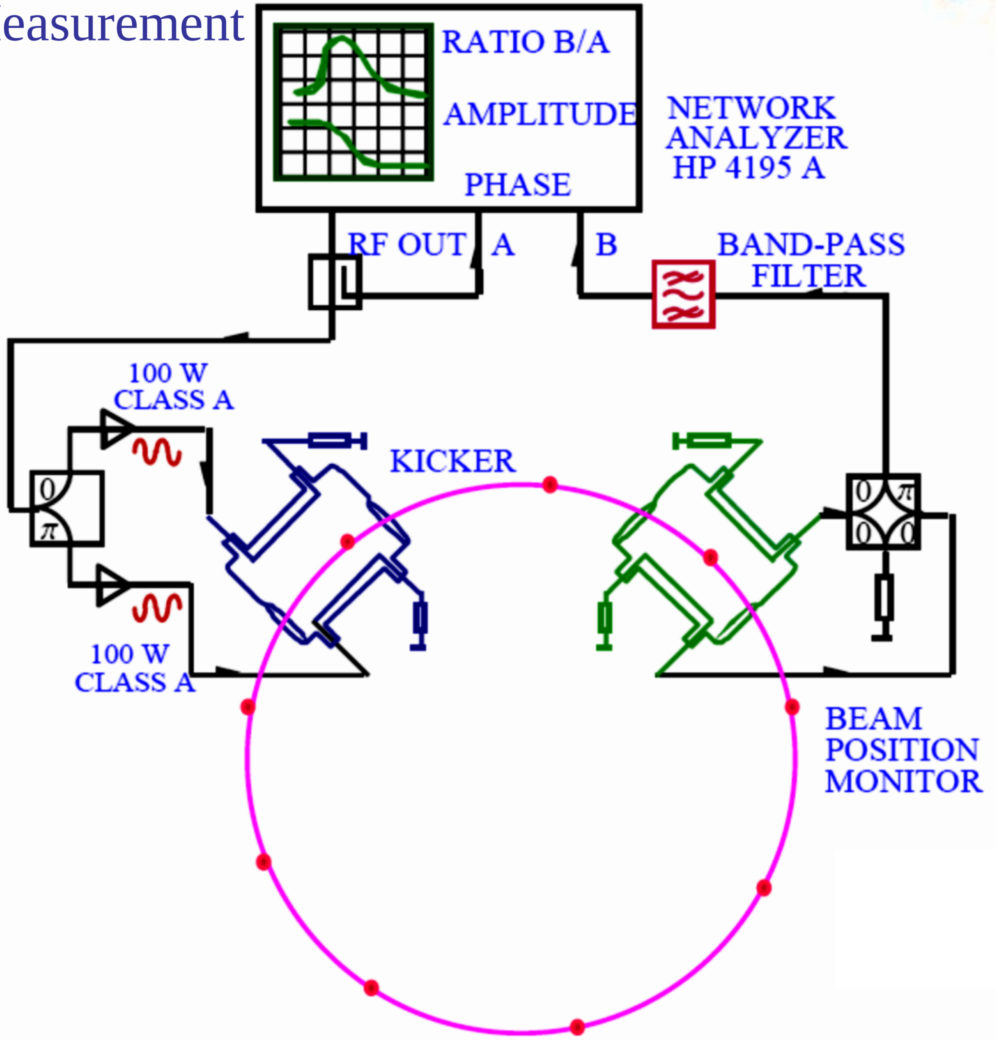
as the velocity response to a kick

Prinziple:

Beam acts like a driven oscillator!

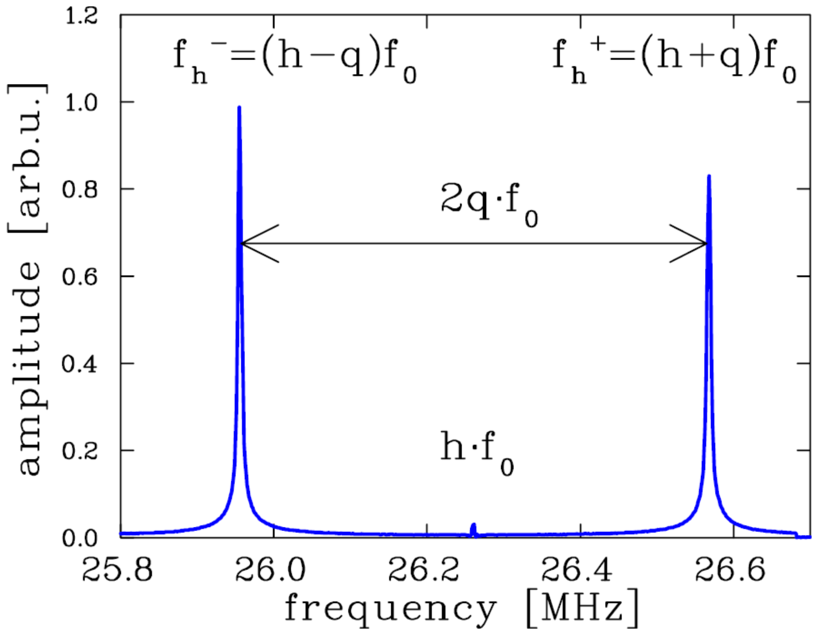
Using a network analyzer:

- RF OUT is feed to the beam by a kicker (reversed powered as a BPM)
- The position is measured at one BPM
- Network analyzer: amplitude and phase of the response
- Sweep time up to seconds due to de-coherence time per band
- resolution in tune: up to 10^{-4}

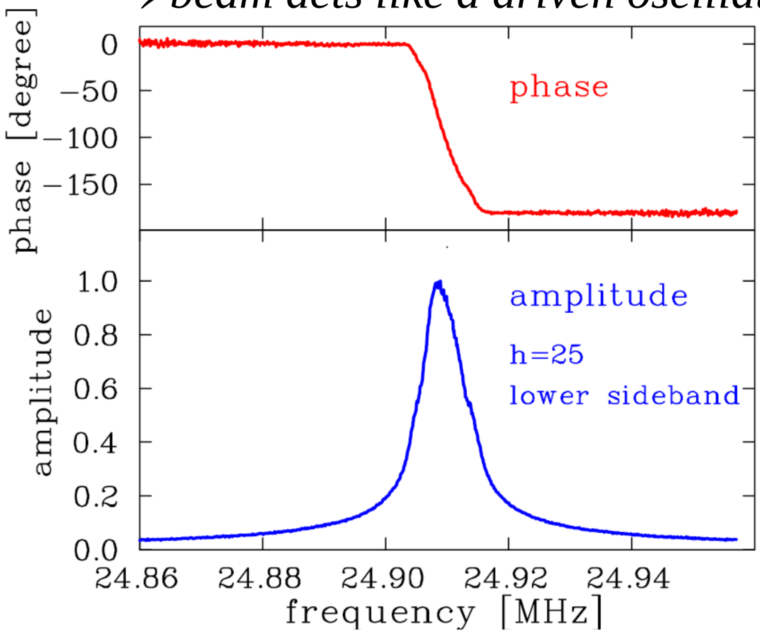


BTF measurement at the GSI synchrotron, recorded at the 25th harmonics.

A wide scan with both sidebands at $h=25^{th}$-harmonics:



A detailed scan for the ***lower*** *sideband → beam acts like a driven oscillator:*



From the position of the sidebands $q = 0.306$ is determined. From the width $\Delta f/f \approx 5 \cdot 10^{-4}$ the tune spread can be calculated via $\Delta f_h^- = \eta \frac{\Delta p}{p} \cdot h f_0 \left(h - q + \frac{\xi}{\eta} Q \right)$

Advantage: High resolution for tune and tune spread (also for de-bunched beams)

Disadvantage: Long sweep time (up to several seconds).

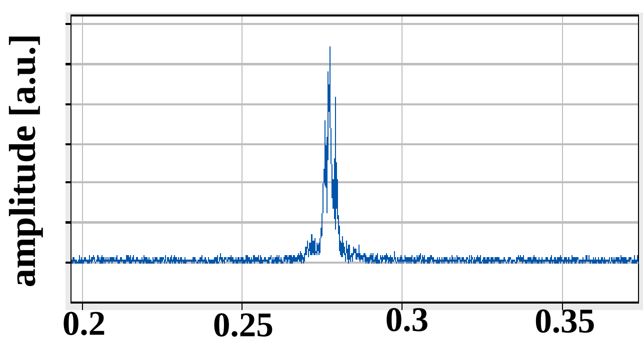
Instead of a sine wave, noise with adequate bandwidth can be applied

→ beam picks out its resonance frequency:

- broadband excitation with white noise of ≈ 10 kHz bandwidth
- turn-by-turn position measurement by fast ADC
- Fourier transformation of the recorded data

⇒ Continues monitoring with low disturbance

vertical tune at fixed time ≈ 15ms



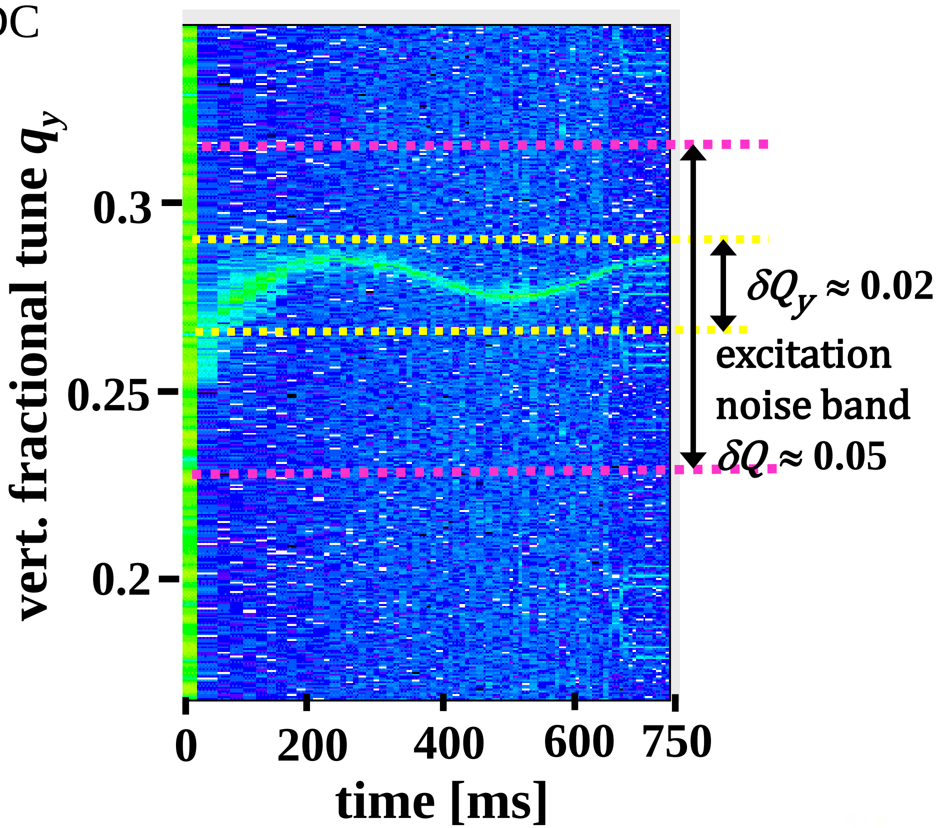
Advantage:

Fast scan with good time resolution

Disadvantage: Lower precision

Example: Vertical tune within 4096 turn duration ≃ 15 ms at GSI synchrotron 11 → 300 MeV/u in 0.7 s

vertical tune versus time



The position of dipoles and quadrupoles

- give the linear lattice functions
- at injection point ***D*** = 0 is favored
- chromatic correction with sextupoles,

Definition of dispersion ***D(s)***:

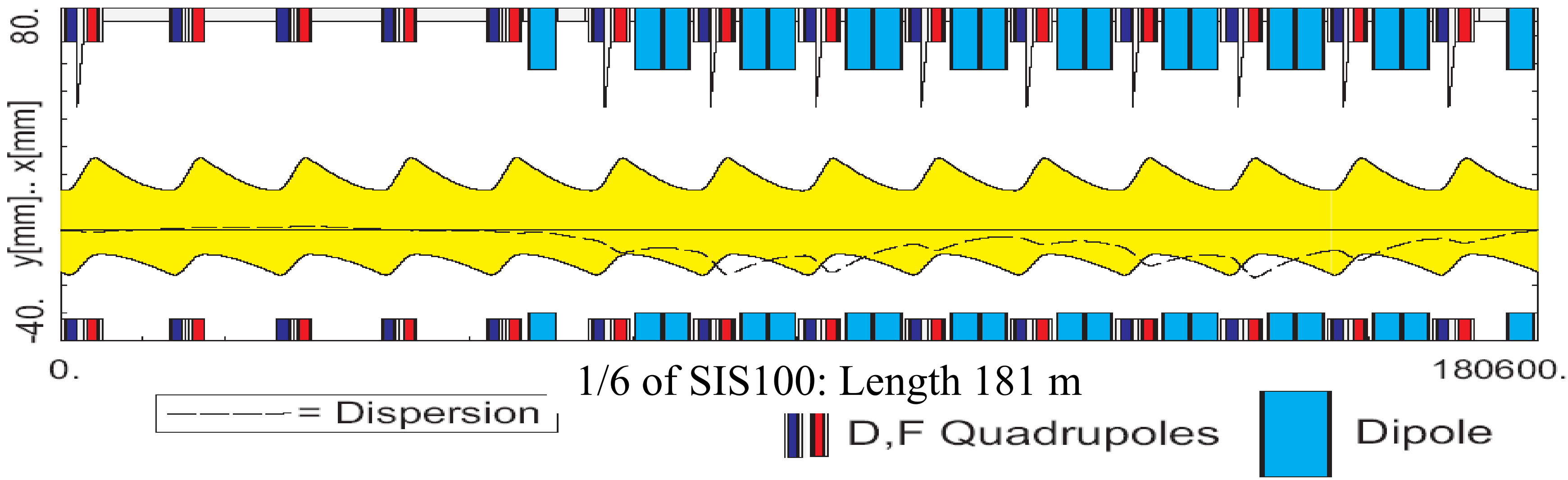
$$x_D(s) = D(s) \cdot \Delta p/p_0$$

Definition of chromaticity ξ per turn:

$$\Delta Q/Q_0 = \xi \cdot \Delta p/p_0$$

Example: GSI SIS100 ion synchrotron

Length [m]		1086
Energy [GeV]		0.2 → 2
Tune	h/v	18.84 / 18.73
Max. dispersion |***D***| [m]		1.73
Max. β–function [m]	h/v	19.6 / 19.6
Natural chromaticity ξ	h/v	-1.19 / -1.20
Injected emittance ε [mm mrad]	h/v	35 / 15
Injected $\Delta p/p_0$ [%]		0.05



1/6 of SIS100: Length 181 m

Excitation of coherent betatron oscillations: From the position deviation ***x_{ik}*** at the BPM ***i*** and turn ***k*** the ***β***-function ***$\beta(s_i)$*** can be evaluated.

The position reading is: ($\hat{x}_i$ amplitude, μ_i phase at i, Q tune, s_0 reference location)

$$x_{ik} = \hat{x}_i \cdot \cos(2\pi Qk + \mu_i) = \hat{x}_0 \cdot \sqrt{\beta(s_i)/\beta(s_0)} \cdot \cos(2\pi Qk + \mu_i)$$

→ a turn-by-turn position reading at many location (4 per unit of tune) is required.

The ratio of ***β***-functions at different location:

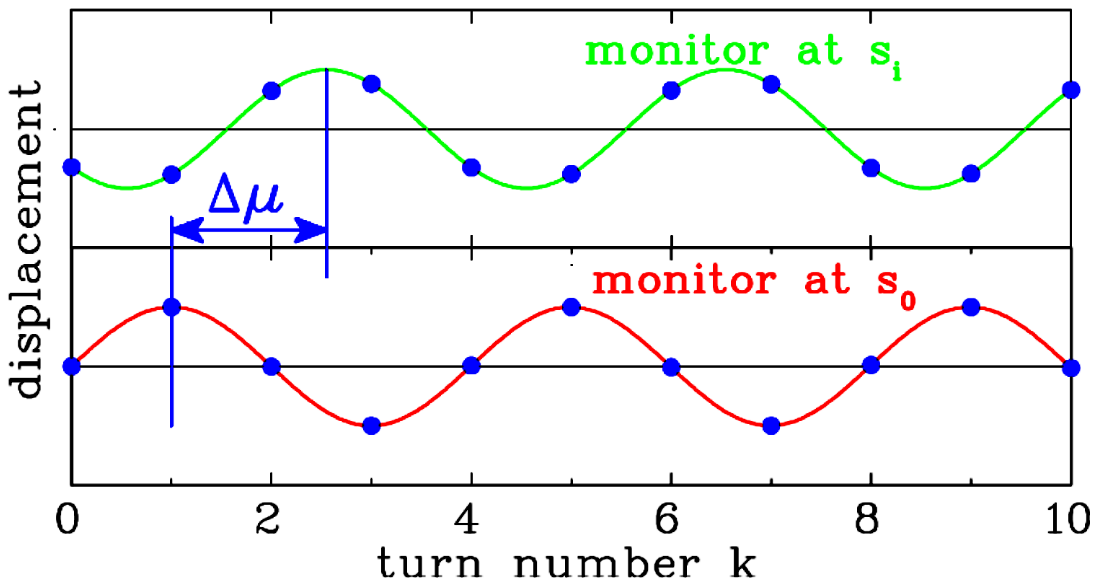
$$\frac{\beta(s_i)}{\beta(s_0)} = \left(\frac{\hat{x}_i}{\hat{x}_0}\right)^2$$

The phase advance is:

$$\Delta\mu = \mu_i - \mu_0$$

Without absolute calibration, ***β***-function is more precise:

$$\Delta\mu = \int_{S0}^{Si} \frac{ds}{\beta(s)}$$



Dispersion $D(s_i)$**:** Excitation of coherent betatron oscillations and change of momentum ***p*** by detuned rf-cavity:

→ Position reading at one location: $x_i = D(s_i) \cdot \frac{\Delta p}{p}$

→ Result from plot of x_i as a function of $\Delta p/p$ ⇒ slope is local dispersion $D(s_i)$.

Chromaticity ξ: Excitation of coherent betatron oscillations and change of momentum ***p*** by detuned rf-cavity:

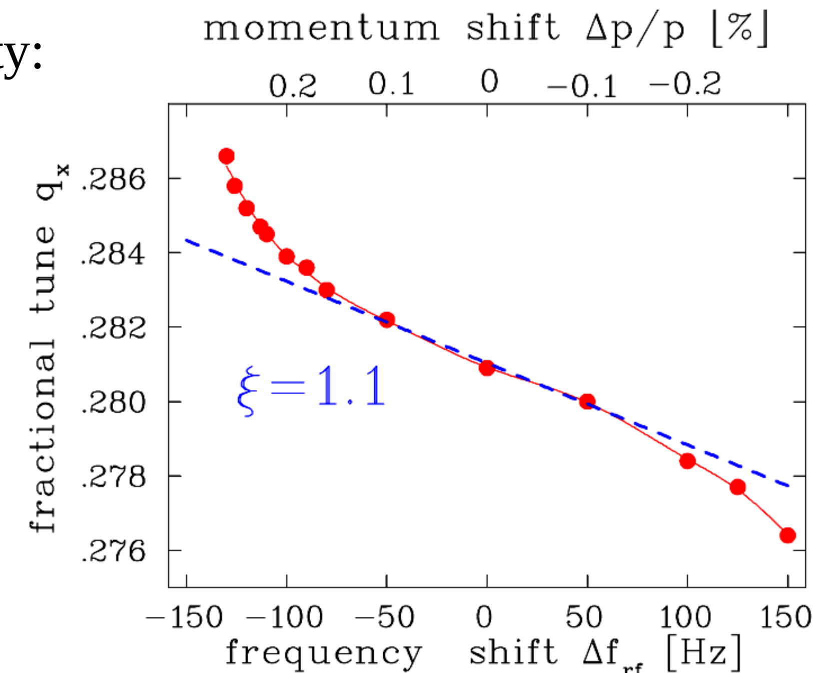
→ Tune measurement

(kick-method, BTF, noise excitation):

$$\frac{\Delta Q}{Q} = \xi \cdot \frac{\Delta p}{p}$$

Plot of $\Delta Q/Q$ as a function of $\Delta p/p$

⇒ slope is dispersion ξ.



Measurement at LEP

Summary Pick-Ups for bunched Beams

The electric field is monitored for bunched beams using rf-technologies ('frequency domain'). Beside transfromers they are the most often used instruments!

Differentiated or proportional signal: rf-bandwidth ↔ beam parameters

Proton synchrotron: 1 to 100 MHz, mostly 1 MΩ → proportional shape

LINAC, e−-synchrotron: 0.1 to 3 GHz, 50 Ω → differentiated shape

Important quantity: transfer impedance $Z_t(\omega, \beta)$.

Types of capacitive pick-ups:

Shoe-box (p-synch.), button (p-LINAC, e−-LINAC and synch.)

Remark: Stripline BPM as traveling wave devices are frequently used

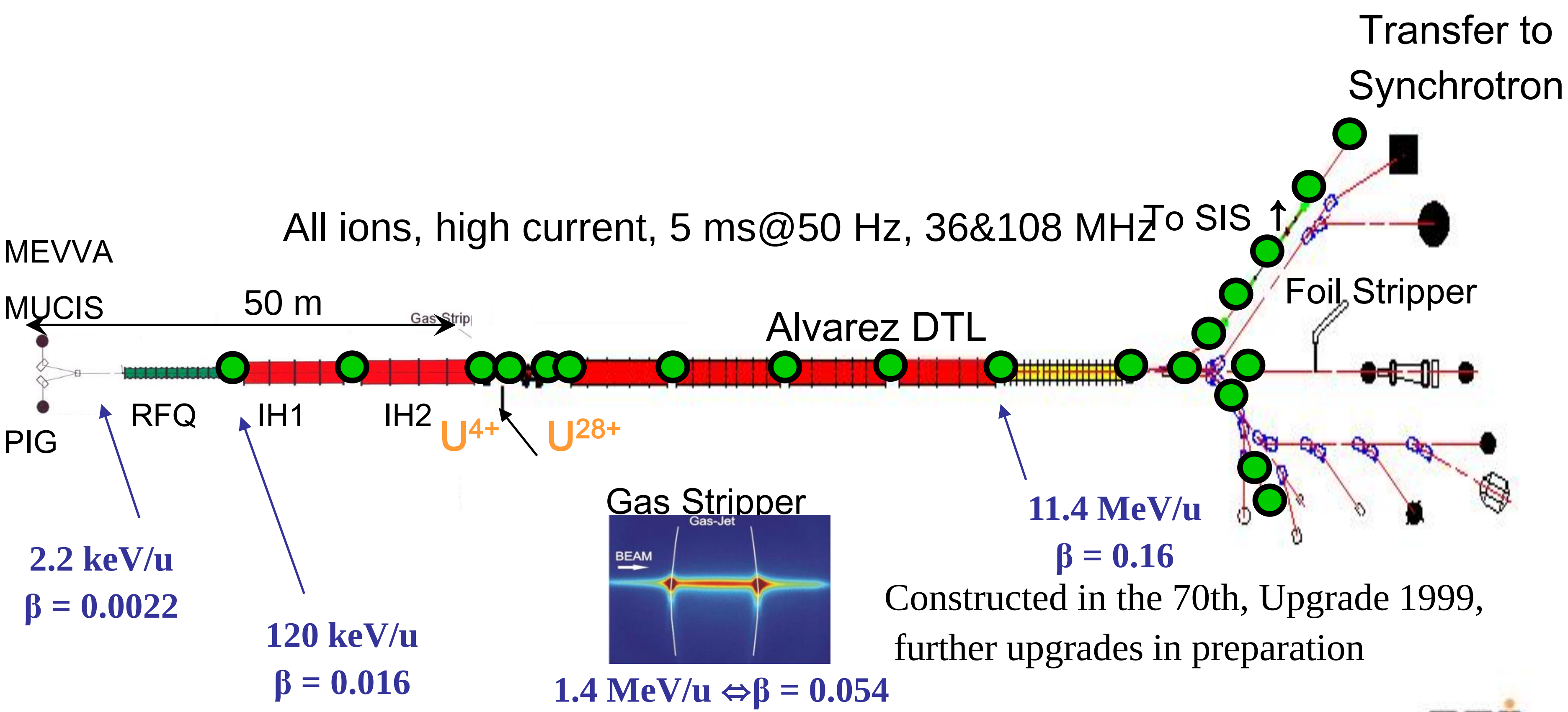
Position reading: difference signal of four pick-up plates (BPM):

- **Non-intercepting** reading of center-of-mass → online measurement and control
  slow reading → closed orbit, ***fast bunch-by-bunch***→ trajectory
- Excitation of ***coherent betatron oscillations*** and response measurement
  excitation by short kick, white noise or sine-wave (BTF)
  → tune q, chromaticity ξ, dispersion D etc.

Appendix GSI Ion LINAC: Position and mean beam energy Meas.

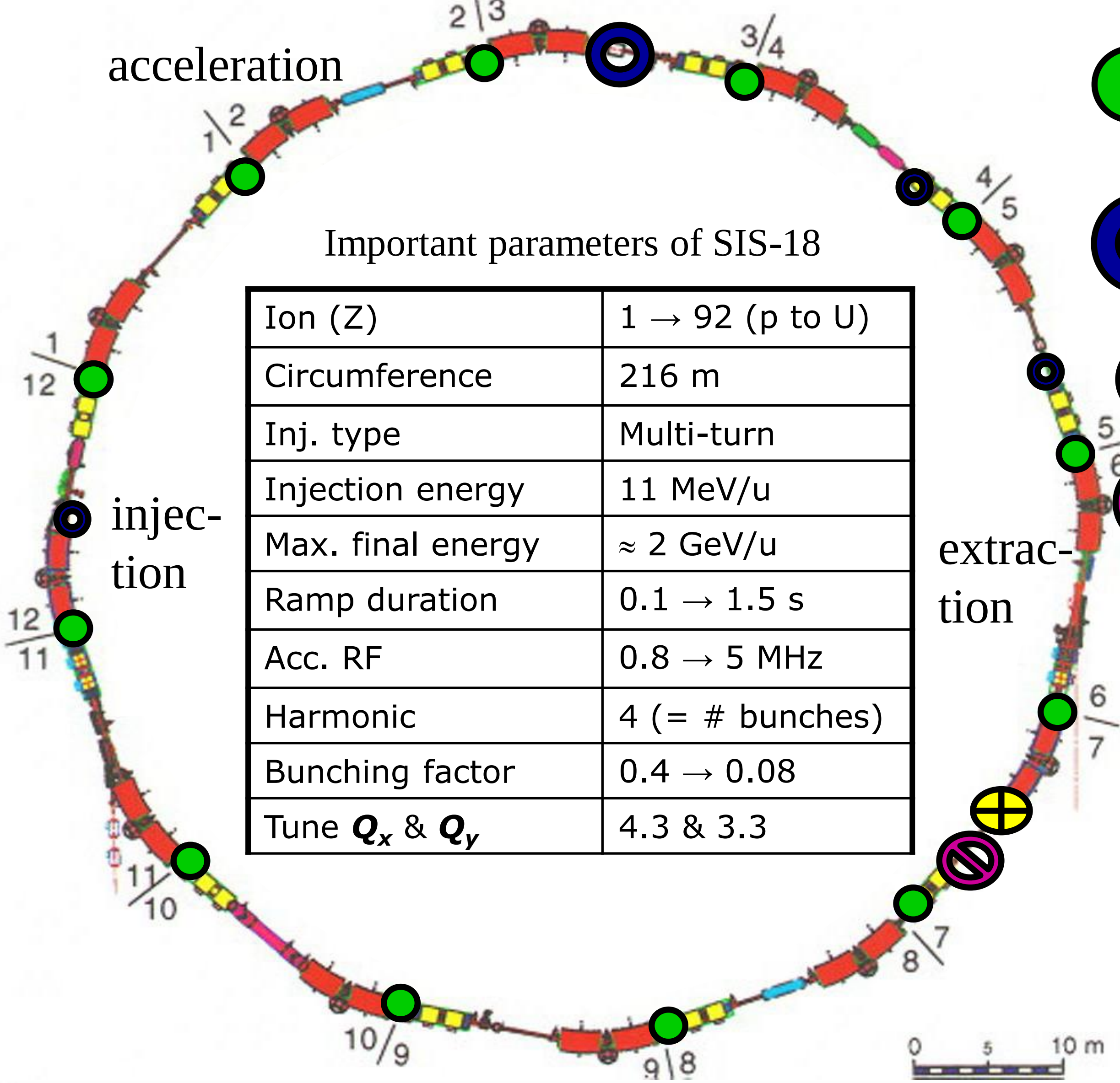
BPM: Capacitive type, for position and time-of-flight

total 25 device



Constructed in the 70th, Upgrade 1999, further upgrades in preparation

Appendix GSI Ion Synchrotron: Position, tune ect. Measurement



Important parameters of SIS-18

Ion (Z)	1 → 92 (p to U)
Circumference	216 m
Inj. type	Multi-turn
Injection energy	11 MeV/u
Max. final energy	≈ 2 GeV/u
Ramp duration	0.1 → 1.5 s
Acc. RF	0.8 → 5 MHz
Harmonic	4 (= # bunches)
Bunching factor	0.4 → 0.08
Tune Q_x & Q_y	4.3 & 3.3

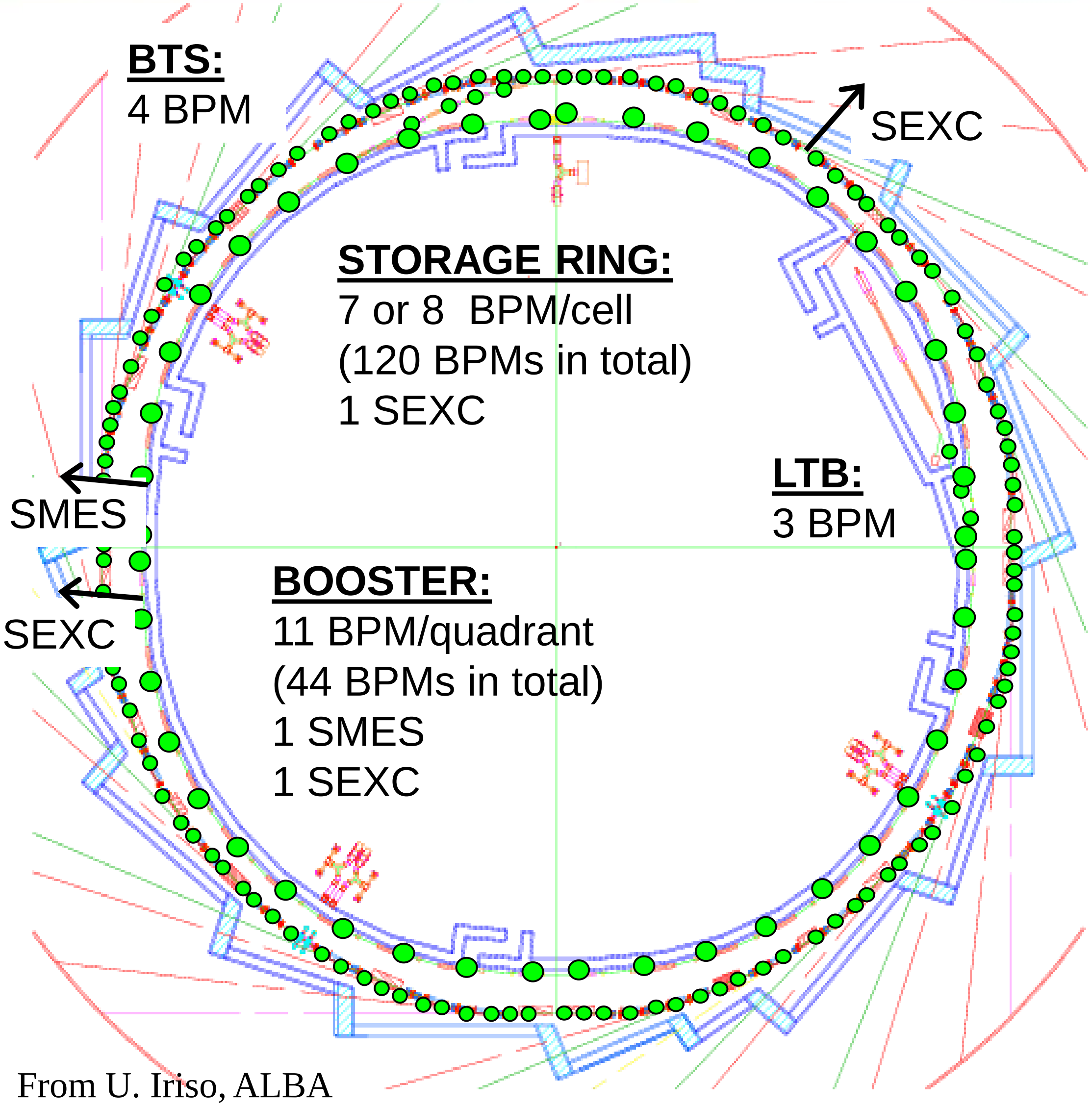
BPM: position 1 μs to s
12 devices

BPM: for tune measurement
1 device

Exciter: for tune excitation

Schottky pick-up:
Δp/p, Q, ξ ....
1 device

Appendix: Synchrotron Light F.ALBA: ´Position, tune ect. Meas.



From U. Iriso, ALBA

Beam position:

Center of mass

- Many locations!
- Frequent operating tool
- For position stabilization i.e. closed otbit feedback

Abbreviation:

Meas. Stripline → SMES
Exc. Stripline → SEXC
Button BPMs → BPM