JUAS Accelerator workshop 2016

Final presentation

Outlook

- Presentation of the task & introduction of the team
- Lattice design
- RF design
- Collective effects and correction
- Vacuum considerations
- Magnet considerations
- Transition considerations

Presentation of the task & introduction of the team

Presentation of the task and the basic layout

- Replacement for the PS machine at CERN
- Acceleration of protons from a momentum of 3.5 GeV/c to a momentum of 20 GeV/c
- For the basic accelerator lay out a 'rectangular' ring design (with four superperiods) was chosen
 - + Space for beam control, correction and instrumentation
 - + Space for acceleration, injection and extractions
 - + Space for future tasks the accelerator may have to handle

bending region

straight region

Presentation of the groups

- Design is a 'rectangular' ring (four super periods)
- The project was divided into three main groups
 - Lattice group
 - RF group
 - Collective effects group
- Special attention has been payed to the magnets, the vacuum and the crossing of the gamma transition

Lattice design

Lattice design – basic parameters

| Element | Number | Length | |
|------------------------|--------|--------|--|
| Focusing quadrupoles | 40 | 0,45m | |
| Defocusing quadrupoles | 40 | 0,45m | |
| Bending dipoles | 48 | 8m | |

$$\rho_d = \frac{L_d}{2\pi/N_d} = 61,12m \ (R = 150m)$$

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Lattice design - geometry

Horizontal plan view [X-Y plane]



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Lattice design – lattice optimization



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Average transversal dimension of the beam

$$\sigma_{x} = \sqrt{\varepsilon_{x} \cdot \beta_{x}} = 16.4mm$$
$$\sigma_{y} = \sqrt{\varepsilon_{y} \cdot \beta_{y}} = 11.6mm$$

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RF design

What we need Vs What we have:



 $\gamma_{transition} = 6.36$

Free Space
$$=\frac{250}{4}$$

For R.F = 64 m

| Objectives for the RF: | $\Delta E = 16.4 \; GeV$ | |
|---|--|--|
| . Get to 20 GeV/c. | $T_{REV(Inj)} = 3.25 \times 10^{-6} s$ | |
| . Get the intensity of 3 x 10 ¹³ Protons/Beam. | $T_{REV(Ext)}$ = 3.14 x 10 ⁻⁶ s $\rho = 61.115 m$ (Bending Radius) | |
| . Preserve the beam from the booster.0. Try not to blow things up0 | $\frac{dB}{dt} = \frac{B_{ext} - Binj}{T^*} = 3.6 [T/s]$ | |
| Circunference (m) | 982.48 | |
| Number of protons per pulse | 3E13 | |
| Cycling frequency (Hz) | 3.125 | |
| Momentum at injection (GeV/c) | 3.5 | |
| Momentum at extraction (GeV/c) | 20 | |
| Gamma at Injection | 3.86 | |
| Gamma at Extraction | 21.35 | |

| h | Numbe | $er \ of \ proton \ /puls$ | $es \ want$ | ed = 20 | $\in = 0.1 \pi eV.s$ |
|-----|----------------|------------------------------------|------------------|--------------------------------------|---|
| n = | Number o | of proton / pulses . | from bo | $\overline{ooster} = 20$ | $\Delta t = 51.2 ns$ $\Delta E = 3.9 MeV$ |
| | | | | | |
| | Booster: | Number of rings | 4 | | |
| | (fast cycling) | Average radius | 37.5 | Circumference [m] | 235.619449 |
| | | Dipole occupation [fraction] | 0.28 | Length [m] | 65.97344573 |
| | | Extraction momentum [GeV/c] | 3.5 | Top field [T] | 1.111866667 |
| | | | | Gamma at extraction | 3.862040361 |
| | | | | Beta at extraction | 0.965895958 |
| | | | | Extraction kinetic energy [GeV] | 2.685323679 |
| | | | | Rigidity at extraction [Tm] | 11.674600 |
| | | Harmonia numbar | | Extraction revolution period [s] | 8.186139E-07 |
| | | Runching factor (neak/average) | 5 66 | Bunch lath/RE period | 4.000309E+00 |
| | | Denoming racion (pearvaverage) | 0.00 | Extracted bunch loth [s] | 5.12E-08 |
| | | | | Gap for kicker [s] | 1.54E-07 |
| | | Kicker rise or fall time [s] | 1.00E-07 | | |
| | | Assume multi-turn injection with 2 | 0 turns with 50% | % efficiency after bunching giving (| 6.E12 particles/ring |
| | | Particles per ring | 6.00E+12 | Particles/bunch | 1.50E+12 |
| | | Norm. Hemit. [π mm mrad] | 40 | Geom. H. emit.[π mm mrad] | 10.72291429 |
| | | Norm. V emit. [π mm mrad] | 20 | Geom. V. emit.[π mm mrad] | 5.361457143 |
| | | Longitudinal emittance [eV s] | 0.1 | | |



 $f_{rev(inj)} = 307 \text{KHz}$

 $f_{rev(_{ext})} = 318$ KHz

 $f_{RF(inj)} = 6.14$ MHz

 $f_{RF(ext)} = 6.36$ MHz

 $\frac{\Delta f_{RF}}{f_{RF}} = 3.6 \%$

CERN PS cavity



Courtesy of Metral

Consideration for Transition:

 $\gamma_{transition} = 6.36$ $\emptyset_s(After Transition) = \pi - 30^\circ$

Some Numbers:

 $Q_{Inj} = 8.29 \ x \ 10 - 4$ $Q_{ext} = 2.265 \ x \ 10 - 4$ Ramp Time = 0.25 second $(\Delta E)_{gain} = 200 \ KeV$

Number of Turns = 72500 *turn*

Group photo



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Collective effects and corrections

Eleonora Belli, Rodrigo Varela, Jay Kalinani

1. Tune control

Remind: the tune is the number of oscillations per turn *Avoid resonance conditions (integer tune)*



$$Q_x = 7.1$$
 $Q_y = 7.05$

$$Q = \frac{1}{2\pi} \oint \frac{ds}{\beta(s)} = \frac{\mu}{2\pi}$$



7.5000

1. Tune control (cont.)



 $\overline{2} \beta^2 \gamma^3 (2\epsilon_{x,y})$ 1.Coherent space charge 2. Incoherent space charge with $\frac{\Delta p}{D} = 10^{-3}$ @ 3.5GeV 3. Incoherent space charge with $\frac{\Delta p}{D} = 10^{-1}$ @3.5GeV 4. Incoherent space charge with $\frac{\Delta p}{D} = 10^{-3}$ @ 20GeV

 Nr_0

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3. Closed orbit prognosis and correction



3. Closed orbit prognosis



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3. Closed orbit correction

| CHOOSE PLANE : | | | |
|---|-------------------------|-------------------------------------|--------------------------------|
| Correct HORIZONTAL plane | Compute | Add a corrector | |
| Correct VERTICAL plane | _# corrPk-Pk [m] | Mean [m]RMS [m] | 15 correctors |
| CHOOSE MONITOR OPTION : | 00.060406 | 0.0000890.016453 | Expected closed orbit |
| 🗩 Use elements of types HPU, VPU, HVPU | 60.012841 | 0.0002460.002396 | |
| • Use entries to quadrupoles for positions (backup mode) | 8 0.012812 | -0.000179 0.002277 | \sim amplitude \approx 1cm |
| CHOOSE CORRECTOR OPTION : | 90.011170 100.011060 | 0.0000890.002162 0.0000500.00213 | |
| | | | |
| Use entries to quadrupoles for positions (backar mode) | 120.011004 | -0.000016 0.002120 | |
| Se use entries to quadrupoles for positions (backup mode) | 14 0.010635 | -0.000061 0.002069 | |
| Edit monitor and/or corrector lists | | 0.002014 | |
| NO. OF CORRECTORS TO BE USED : | | | |
| Enter min. no. of correctors to be used 6 | | | |
| Enter max. no. of correctors to be used 15 | | | |
| Total no. of monitors available = 103 | | | |
| Total no. of correctors available = 103 | | | |
| COMPUTATIONAL METHOD : | | | |
| C Least Squares Fit + Gauss-Jordan (fast) | | | |
| Singular Value Decomposition Fit (safe) | SELECT ONE SOLUTION | N IN THE LIST BOX THEN CLICK OK | |
| C Least Squares Fit + Householder Trans. + Tri-diag. | OK | Cancel | |

3. Closed orbit correction (cont.)



Pk-Pk amplitude $\approx 1 cm$

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Vacuum consideration

Vacuum considerations

| | MAIN WINDOW | | | | | | | | | | | |
|---------------------|--------------|-------------|-------------|-------------------------------|-------------|-----------|--------|--------|---------|-------------|---------------|------------|
| Options | File C | alculations | Aids | Tables | Graphs | Output | : Help | | | | | |
| Sele | ction: | | | Conventio | onal magn | et desig | n aid | OK | | | | |
| Center Are | | | | Conventio | onal magn | et cost a | aid | | | | | |
| Center Arc | | | | Eddy curre | ent calcula | ator | | ring | je- | field Off | | |
| | | | | Water coo | pied coil d | osign ai | d | Iro | m | aticity eqn | Non-space cha | rge optics |
| | Eile e | , had | | Vacuum d | lesign aid. | -) | < | ,_F | т | ATTICE EI | EMENTS (On | Arrico |
| Quit | Tree la | ame ioas | | RF cavity r | oerforman | ec aid | | | T | ATTICE EL | EMENTS (OI | -AXIS) |
| User title: Qu Halc | | | | RFQ period performance aid | | | | | | | | |
| | | | Halo collir | Halo collimation design aid | | | - | | | | | |
| Alias | Unit | | | Emittance | growth ca | alculato | r | 1 | | Hor. Mbend | Vert. Mbend | Edge ang |
| | no.] | I | | Relativisitic data calculator | | | 4 | 4 | [rad] 5 | [rad] 6 | [rad] | |
| | 1 | Center | | Analytic m | natching | | | 000 | 0 | 0.000000 | 0.000000 | 0.0 |
| | 2 | | | | | | | 0.0000 | 0 | 0.000000 | 0.000000 | 0.0 |
| Grid | 3 | | | |)) | | | 0.0000 | D | 0.000000 | 0.000000 | 0.0 |
| | 4 | QF1 | | | QU/ | ADR | | 0.4500 | 0 | 0.000000 | 0.000000 | 0.0 |
| | 5 | s0 | | | DRI | FT | | 1.440 | 5 | 0.000000 | 0.000000 | 0.0 |
| | 6 | Dip1 | | | SBE | END | | 8.0000 | 0 | 0.130900 | 0.000000 | 0.0 |
| Field | 7 | s0 | | | DRI | FT | | 1.4405 | 5 | 0.000000 | 0.000000 | 0.0 |
| 1 ieu | 8 | QD1 | | | QU/ | ADR | | 0.4500 | 0 | 0.000000 | 0.000000 | 0.0 |

VACUUM SYSTEM DESIGN AID

INTRODUCTION:

Equilibrium pressure calculation for an infinite array of uniformly spaced vacuum pumps connected to a vacuum pipe of circular or elliptical cross-section

| INPUT. | | OUTPUT | |
|---|--------------------------------|---|------------------------------|
| EVICI. | | 001101. | |
| Pump separation [m] = 10 | | Maximum pressure | [Torr] = 1.01E-0010 |
| Pump speed [1/s] = 50 | COMPUTE | Average pressure | [Torr] = 9.13E-0011 |
| Major half-width of pipe $[m] = 0.04$ | <u>ا</u> | Minimum pressure | [Torr] = 7.00E-0011 |
| Minor half-width of pipe $[m] = 0.0^{\circ}$ | 7 | Conductance of pipe (over separation lgth) | [l/s] = 13.72 |
| Specific surface area 'seen' by vacuum $[cm^2/m] = 35$ | | Specific conductance of pipe | [1 m/s] = 137.19 |
| Specific out-gassing rate | . 10 | | |
| $(enter #.#E##) [10rr I/s/cm^2] = [10.1]$ | -12 | | |
| Absolute temperature [K] = 300 | | | Copy data to clipboard |
| Molecular weight of residual gas = 28 | QUIT | | Copy data to notebook |
| · · · · · · · · · · · · · · · · · · · | | Paste time stamp | Load from notebook |
| NOTES | | | |
| - The specific surface area 'seen' by v | acuum should be increased to | account for shields, scre | ens, bellows etc. |
| - Some typical outgassing rates are: | Stainless steel baked for 24 h | nour at 300 deg. C | = 1 E -12 |
| 51 0 0 | Stainless steel, unbaked afte | r 100 hour pump-down | = 2 E -9 |
| | Copper after 10 hour pump-o | lown | = 5 E -9 |
| | Brass after 10 hour pump-do | wn | = 2.5 E -8 |
| | Teflon and aluminium after 1 | 0 hour pump-down | = 1 E -7 |
| | Araldites B, D and F after 10 | hour pump-down | = 8 E -7, 5 E -7, and 4 E -7 |
| | Nylon after 10 hour pump-do | own | = 4.5 E -6 |
| - Molecular weights: 2(H2), 28(N2), 3 | 2(02). | | |
| | | | |
| | | | |

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OUTPUT:

| Maximum pressure | [Torr] = 1.01E-0010 |
|---|---------------------|
| Average pressure | [Torr] = 9.13E-0011 |
| Minimum pressure | [Torr] = 7.00E-0011 |
| Conductance of pipe (over separation lgth) | [l/s] = 13.72 |
| Specific conductance of pipe | [l m/s] = 137.19 |

Pressure can be transformed to particle density:

P.V = N.k.T

10⁻¹⁰ Torr ~ 3 million particles/cm³

(1mbar ~0.75 Torr)

| Da | itei | Start | Einfügen | Seitenlayout | Formeln | Daten | Überprüfe | |
|----|--|------------|----------------|---------------|---------------|-------------|-----------|--|
| | | D25 | • (* | f_x | | | | |
| | | А | В | С | D | E | F | |
| 1 | 1 | 11:59:30 | | | | | | |
| 2 | VAC | UUM SYS | STEM DESIGN: | INPUT- can b | e reloaded, o | do not re-f | format | |
| 3 | Pum | p separa | ation [m] =5 | | | | | |
| 4 | Pum | p speed | [l/s] =50 | | | | | |
| 5 | Majo | or half-w | idth of pipe [| [m] =0.04 | | | | |
| 6 | Mind | or half-w | idth of pipe | [m] =0.07 | | | | |
| 7 | Spec | ific surfa | ace area 'seer | n' by vacuum | [cm^2/m] =35 | 5 | | |
| 8 | Spec | ific out- | gassing rate [| Torr I/s/cm^2 | 2] =10E-12 | | | |
| 9 | Abso | olute ter | nperature [K] | =300 | | | | |
| 10 | Mole | ecular w | eight of resid | ual gas =28 | | | | |
| 11 | | | | | | | | |
| 12 | | | | | | | | |
| 13 | VAC | UUM SYS | STEM DESIGN: | OUTPUT | | | | |
| 14 | Maxi | imum pr | essure [Torr] | = 4.30E-0011 | | | | |
| 15 | Average pressure [Torr] = 4.03E-0011 | | | | | | | |
| 16 | 5 Minimum pressure [Torr] = 3.50E-0011 | | | | | | | |
| 17 | 7 Conductance of pipe (over separation lgth) [l/s] = 27.44 | | | | | | | |
| 18 | Spec | ific cond | ductance of p | ipe [l m/s] = | 137.19 | | | |
| 19 | | | | | | | | |
| 20 | | | | | | | | |

Output can be saved in an EXEL-file



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$$P(x) = A_{q} \left\{ \frac{L_{x} - x^{2}}{2w} + \frac{L}{5} \right\}$$

$$P_{max} = A_{q} \left\{ \frac{L^{2}}{5w} + \frac{L}{5} \right\}$$

$$P_{av} = A_{q} \left\{ \frac{L^{2}}{12w} + \frac{L}{5} \right\}$$

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Magnet consideration

Dipoles

MAIN SPECIFICATIONS

| Bmax [T] | 1.09 |
|---------------------|-------|
| Bending Radius [mm] | 61500 |
| Bending Angle [°] | 7,44 |
| Magnet lenght [mm] | 8000 |

IRON YOKE SPECIFICATIONS

| Pole iron gap [mm] | 100 |
|---------------------|------|
| L overall [mm] | 8270 |
| L iron [mm] | 7870 |
| Pole width [mm] | 500 |
| Overall width [mm] | 1400 |
| Overall height [mm] | 1100 |

COIL SPECIFICATIONS

| Number of turns | 220 |
|---------------------------|---------|
| Nominal current [A] | 393 |
| Conductor type | Hollow |
| Conductor dimensions [mm] | 14 x 14 |
| Hole diamater [mm] | 8,5 |
| | |

WATER-COOLED COIL DESIGN AID ...

INTRODUCTION:

- Parameters are for a SINGLE water circuit.

It is left to the user to combine water circuits in series/parallel to get the overall temperature rise, power consumption, etc.
For circular conductors, set conductor height = width and the rounding radius = 0.5*width.

| INPUT: | | | OUTPUT FOR SINC | GLE WATER C | IRCUIT: |
|--|--|--|---|-----------------------------------|------------------------------------|
| Conductor height | [mm] = 17.15 | | Water speed | [m/s] = | 2.61263 |
| Conductor width | [mm] = 17.15 | | Water flow | [l/min] = | 13.83346 |
| Diameter of water hole | [mm] = 10.6 | | Water flow (turbul | ent/laminar) | TURBULENT |
| Radius of edge rounding | [mm] = 3 | COMPUTE | Water temp. rise | [deg C] = | 0.67739 |
| | [] | | Power dissipation | [watt] = | 652.822 |
| Conductor length in a single water circuit | [m] = 50 | | Resistance (hot) | [ohm] = | 0.004227 |
| Arailable water proceure | | | Current density | [A/mm^2] = | 1.98335 |
| for a single circuit | [bar] = 4 | | Conductor mass | [kg] = | 88.50347 |
| Input water temp. | [deg C] = 18 | _ | PROPOSION TRO | | |
| | | - | RESPONSE TIME: | | _ |
| Current | [A] = 393 | | If the cooling water | is cut off, then | the temperature |
| Conductor material: | Copper | | will rise at the rate | 01; 0.019 | [deg C/s] |
| | 🔿 Aluminium | | | | |
| | | | | Cop | y data to clipboar |
| Load from notebook Pa | ste time stamp | QUIT | | Cop | y data to noteboo |
| - NOTES: - Typical values for lattic temperature rise 10-30 d - For septa, parameters a | ce magnets: turbulent wa eg C. For air cooling, ke are more extreme: try not | ater flow at 3-5 m/s; c ep below 2 A/mm^2. to exceed a current d | urrent density 3-5 A/m lensity of 50 A/mm^2 (a | m^2; pressure abs. max. 90 A/r | drop 4-8 bar; mm^2); try not to |
| exceed a water velocity | of 10 m/s; try to use a so | quare conductor to fa | cilitate bends in both p | olanes. | |

- For high current densities, check the rate of temperature rise if the water stops and be sure the temperature interlock is fast enough to cut the current.

- The maximum length of conductor without a braze is limited by the maximum billet size for drawing (120 kg approx. for Cu).

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Qadrupoles

MAIN SPECIFICATIONS

| Maximum gradient [T/m] | 6,6 |
|--------------------------|-----|
| Magnet lenght [mm] | 450 |
| IRON YOKE SPECIFICATIONS | |
| Aperture diameter[mm] | 100 |
| L overall [mm] | 500 |
| Liron [mm] | 450 |
| Overall Width [mm] | 400 |

COIL FEATURES

| 36 | Number of turns per pole | | | |
|-----------|---------------------------|--|--|--|
| 183 | Nominal current [A] | | | |
| Hollow | Conductor type | | | |
| 9,4 x 9,4 | Conductor dimensions [mm] | | | |
| 5,83 | Hole diamater [mm] | | | |

WATER-COOLED COIL DESIGN AID ...

INTRODUCTION:

- Parameters are for a SINGLE water circuit.

It is left to the user to combine water circuits in series/parallel to get the overall temperature rise, power consumption, etc.
For circular conductors, set conductor height = width and the rounding radius = 0.5*width.

| INPUT: | | | OUTPUT FOR SIN | GLE WATER C | IRCUIT: |
|---|-----------------|---------|-----------------------|------------------|---------------------|
| Conductor height | [mm] = 9.4 | | Water speed | [m/s] = | 5.74642 |
| Conductor width | [mm] = 9.4 | | Water flow | [l/min] = | 9.29894 |
| Diameter of water hole | [mm] = 5.86 | | Water flow (turbu | lent/laminar) | TURBULENT |
| Dell's of sheep with a | | COMPUTE | Water temp. rise | [deg C] = | 0.09670 |
| Radius of edge rounding | [mm] = 3 | | Power dissipation | [watt] = | 62.645 |
| Conductor length in a single water circuit | [m] = 6 | | Resistance (hot) | [ohm] = | 0.001871 |
| Arailahla watar pressure | | | Current density | [A/mm^2] = | 3.41010 |
| for a single circuit | [bar] = 4 | | Conductor mass | [kg] = | 2.87629 |
| Input water temp. | [deg C] = 18 | | DESDONSE TRUE. | | |
| Current | [A] = 183 | | If the cooling water | is cut off, then | the temperature |
| Conductor material: | Copper | | will rise at the rate | 01; | [deg C/s] |
| | 🔿 Aluminium | | | | [9] |
| 1.00 | | | | Copy | y data to clipboard |
| Load from notebook P | aste time stamp | QUIT | | Cop | y data to notebook |
| NOTES: | | | | | |

- Typical values for lattice magnets: turbulent water flow at 3-5 m/s; current density 3-5 A/mm^2; pressure drop 4-8 bar; temperature rise 10-30 deg C. For air cooling, keep below 2 A/mm^2.

- For septa, parameters are more extreme: try not to exceed a current density of 50 A/mm^2 (abs. max. 90 A/mm^2); try not to exceed a water velocity of 10 m/s; try to use a square conductor to facilitate bends in both planes.

- For high current densities, check the rate of temperature rise if the water stops and be sure the temperature interlock is fast enough to cut the current.

- The maximum length of conductor without a braze is limited by the maximum billet size for drawing (120 kg approx. for Cu).

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Transition considerations

Gamma transition crossing I

Transition crossing without jump



Non adiabatic theory needed

 At transition, bunch length ↘ and momentum spread ↗

Main risk: losses in the beam

Gamma transition crossing II



-Gamma (beam) ——Gamma transition (with jump)

• Solution: create a jump in γ_{tr}

 How to: add quadrupoles to change the momentum compaction factor

 Problem: adding quadrupole changes the tune

Gamma transition crossing III



- Switch on the quadrupoles:
 - γ_{tr} increases
- Switch off or invert the polarity of the quadrupoles at the right time
 - γ_{tr} decreases suddenly
 - You have crossed transition
- The tune changes
 - You may cross resonances
 - To avoid it, one may want to change the tune before the gamma jump and reestablished it afterward

Gamma transition crossing

Do we have time to do this gamma jump?

• Assume a 30kV RF cavity, a $\dot{B} = 3.6 T/s$ and a $\gamma_{tr} = 6.36$

- Therefore $\Delta E = 10 MeV/turn$
- A $\Delta \gamma = 0,27$ means an increase in energy of $\Delta E = 250 MeV$ so we would need approximately 10 turns to operate the quadrupoles (about 300µs)

Thanks for your attention

Spare slides

Chromaticity correction

Gerardo Guillermo, Shuang Ruan, Geng Wang, Kedong Wang, Liping Yao

Chromaticity correction I

- In order to correct the chromaticity 2 sextupoles were added, one focusing and one defocussing
- The sextupoles where placed next to the defocussing quadropoles
- WinAGILE calculated the closed orbit parameters (without sextupoles):

| | CENTRAL ORBIT | | |
|-----------------------------|------------------|----------|--|
| | Circular machine | | |
| Circumference | [m] = | 943.0480 | |
| Horizontal tune | Qx = | 7.104830 | |
| Vertical tune | Qz = | 7.054848 | |
| Horizontal chromaticity | dQx/dp/p = | -8.513 | |
| Vertical chromaticity | dQz/dp/p = | -3.349 | |
| Gamma transition | gamma tr = | 6.36840 | |

Chromaticity correction II

- To steps to find the strength of the sextupoles are:
 - Go into calculations menu
 - Select correct chromaticity
 - In the menu select the desired chromaticity, e.g. 0.
 - Click on recompute, and it will display the strength needed
- After getting the values, it is recommended that you check it is feasible within technological restrictions.

| -1. ENTER DESIRED CHRO | MATICITIES: |
|----------------------------------|----------------------|
| Horizontal, dQx/dp/p = | = 0 |
| Vertical, dQz/dp/p = | 0 |
| | |
| 2. CHOOSE FROM INVENT | IORY: |
| | 2QF1 4 SD |
| CITUED aliak an unit in | 6Dip1 |
| inventory | 8QD1 |
| OD antes diseaths halow | 28QUADD1 33QUADE1 |
| the indices and | 35QUADD2 |
| increments to be used | 43QUADF2 |
| | |
| | , |
| 3. UNITS/SERIES AND ST | EP-SIZES TO BE USED: |
| Index of 1st unit or unit in 1st | st series 4 |
| Index of 2nd unit or unit in 2 | nd series |
| index of 2nd unit of unit in 2 | Ind Seller 3 |
| Step-size for 1st unit/series | = 0.010000 |
| Step-size for 2nd unit/sereis | . = 0.01 |
| | , |
| (Re-) (| Compute |
| | |
| dOx | /dp/p dOz/dp/p |
| Desired values = | |
| Obtained values = | |
| Residual errors = | |
| | |
| OK - accept new values | Reset original value |
| • | |