

Synchrotron radiation

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and

Diamond Light Source

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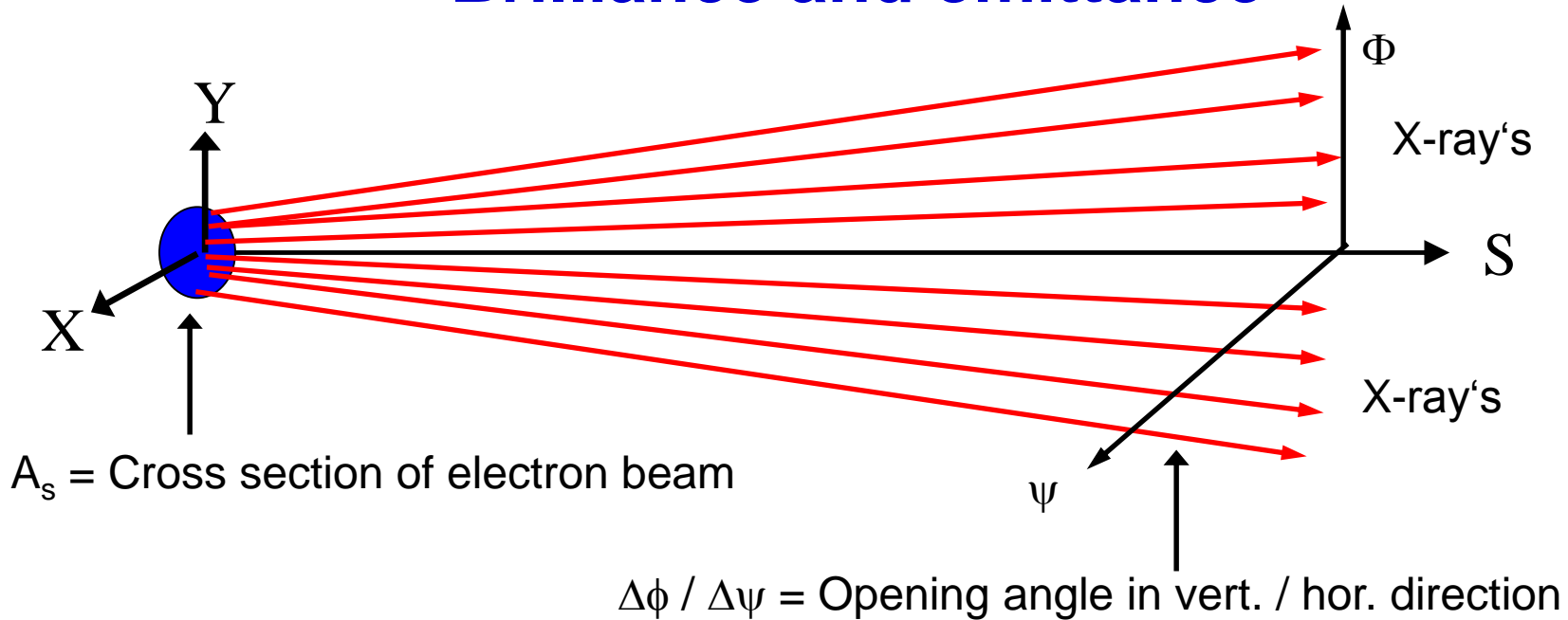
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Brilliance and emittance



Flux = Photons / (s • BW)

Brilliance = Flux / ($A_s \cdot \Delta\Phi \cdot \nabla\psi$) , [Photons / (s • mm² • mrad² • BW)]

$$\text{brilliance} = \frac{\text{flux}}{4\pi^2 \Sigma_x \Sigma_{x'} \Sigma_y \Sigma_{y'}}$$

$$\Sigma_x = \sqrt{\sigma_{x,e}^2 + \sigma_{ph,e}^2} \quad \sigma_x = \sqrt{\varepsilon_x \beta_x + (D_x \sigma_\varepsilon)^2}$$

$$\Sigma_{x'} = \sqrt{\sigma_{x',e}^2 + \sigma_{ph,e}'^2} \quad \sigma_{x'} = \sqrt{\varepsilon_x / \beta_x + (D'_x \sigma_\varepsilon)^2}$$

The brilliance represents the number of photons per second emitted in a given bandwidth that can be refocus by a perfect optics on the unit area at the sample.

Diffraction limit storage rings (I)

The brilliance of a storage ring based synchrotron light source can be increased by reducing the emittance of the beam, up to the limit where the natural diffraction prevents any further reduction of the photon beam size and divergence.

This is called diffraction limited storage ring.

In the expression appearing in the denominator of the brilliance

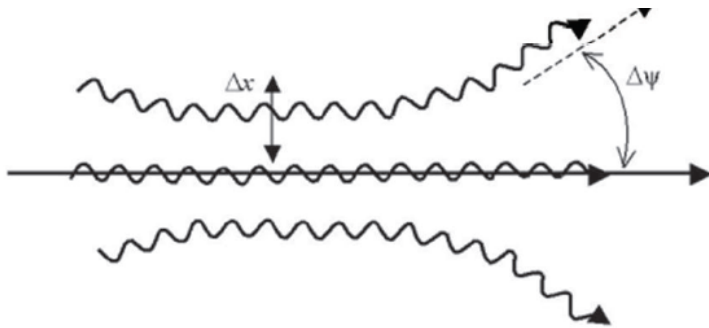
$$\begin{aligned}\Sigma_x &= \sqrt{\sigma_{x,e}^2 + \sigma_{ph,e}^2} & \sigma_x &= \sqrt{\varepsilon_x \beta_x + (D_x \sigma_\varepsilon)^2} \\ \Sigma_{x'} &= \sqrt{\sigma_{x',e}^2 + \sigma_{ph,e}'^2} & \sigma_{x'} &= \sqrt{\varepsilon_x / \beta_x + (D'_x \sigma_\varepsilon)^2}\end{aligned}$$

the natural photon beam size σ_{ph} and divergence σ'_{ph} dominate over the size and divergence of the electron beam

The condition for diffraction limit depends on the wavelength. To see this we must consider the photon beam size and divergence.

ID radiation beam size (I)

Usually the undulator radiation is approximated as the fundamental e.m. mode of a Gaussian beam. For the fundamental Gaussian mode we have



K-J Kim in *Characteristics of Undulator Radiation*, AIP 1989

Coherent beam of wavelength λ
 focused to spot size Δx will diffract with
 angle $\Delta\psi = \sim \lambda/\Delta x$

Time-harmonic electric field of form $E(\mathbf{x};z)e^{-i\omega t}$ satisfies wave equation

$$\left[\frac{\partial^2}{\partial z^2} + \left(\frac{\partial}{\partial \mathbf{x}} \right)^2 + k^2 \right] E(\mathbf{x}; z) = 0, \quad k = \frac{\omega}{c} = \frac{2\pi}{\lambda} \quad \mathbf{x} = (x, y)$$

The Gaussian beam size and divergence of such mode are given by the relations

$$E_k(x, 0) = E_k(0, 0) \exp\left(\frac{-x^2}{2\sigma_{Ex}^2}\right) \quad \mathcal{E}_k(\psi, 0) = \mathcal{E}_k(0, 0) \exp\left(\frac{-\psi^2}{2\sigma_{\mathcal{E}\psi}^2}\right)$$

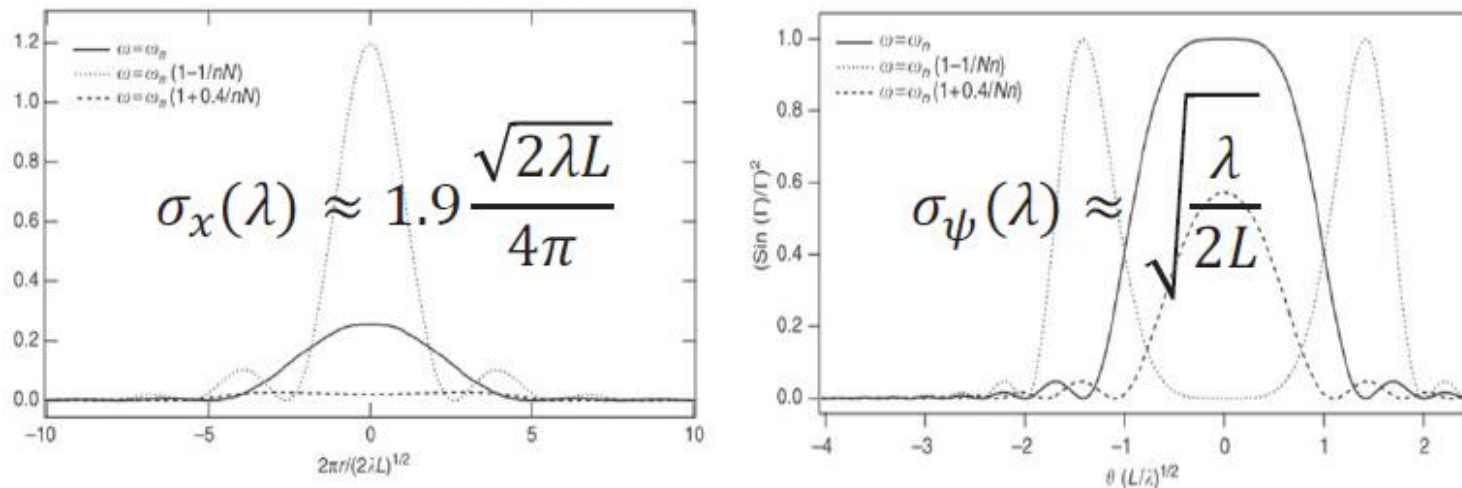
$$\sigma_{\mathcal{E}\psi} = \frac{1}{k\sigma_{Ex}} = \frac{\lambda}{2\pi\sigma_{Ex}} \Rightarrow \sigma_{Ex}\sigma_{\mathcal{E}\psi} = \frac{\lambda}{2\pi}$$

ID radiation beam size (II)

The undulator radiation is not strictly speaking a Gaussian mode (especially in helical undulators). However its angular distribution can be fitted with that of a Gaussian mode and the corresponding beam size and divergence are extracted from the fit:

Fitting Gaussian profiles to spatial and angular profiles for **undulator radiation** at λ :

P. Elleaume, in *Wigglers, Undulators, and Their Applications*, 2003.



The diffraction limited emittance of the photon beam of the undulator radiation generated by a filament beam is given by the product

$$\sigma_x \cdot \sigma_\psi \sim 1.9 \frac{\sqrt{2\lambda L}}{4\pi} \cdot \sqrt{\frac{\lambda}{2L}} \sim \frac{\lambda}{2\pi}$$

Diffraction limit storage rings (II)

The contribution to the photon beam size and divergence due to a finite electron beam size and divergence add in quadrature (still within the Gaussian approximation for both).

The condition for **diffraction limit** is then given by

$$\varepsilon_{x,y}(e^-) \ll \varepsilon_r(\lambda) = \frac{\lambda}{2\pi}$$

The condition for diffraction limit depends on the wavelength. Usually it is quoted that of 1 Angstrom (hard X rays) the emittance should be less than 8 pm ($\lambda/4\pi$).

The brilliance reads

$$\text{brilliance} = \frac{\text{flux}}{4\pi^2 \Sigma_x \Sigma_{x'} \Sigma_y \Sigma_{y'}} \Rightarrow \frac{\text{flux}}{\lambda^2 / 4}$$

Diffraction limit storage rings (III)

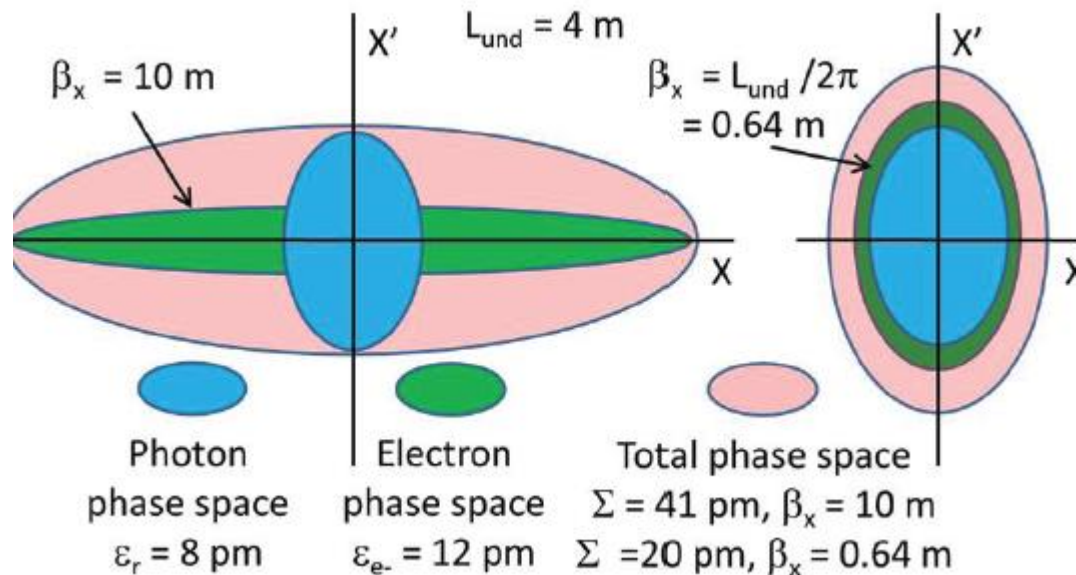
Notice that the transverse emittance is minimised when the electron beam size and divergence are matched to the photon beam size and divergence, hence

$$\frac{\sigma_r(\lambda)}{\sigma'_r(\lambda)} = \frac{\sigma_{x,y}(e^-)}{\sigma'_{x,y}(e^-)} \Rightarrow \beta_{x,y} = \frac{L}{\pi}$$

Note: many authors cite

$$\beta_{x,y} = \frac{L}{2\pi}$$

This requires a special design of the optics in the ID straight sections



Diffraction limit storage rings (IV)

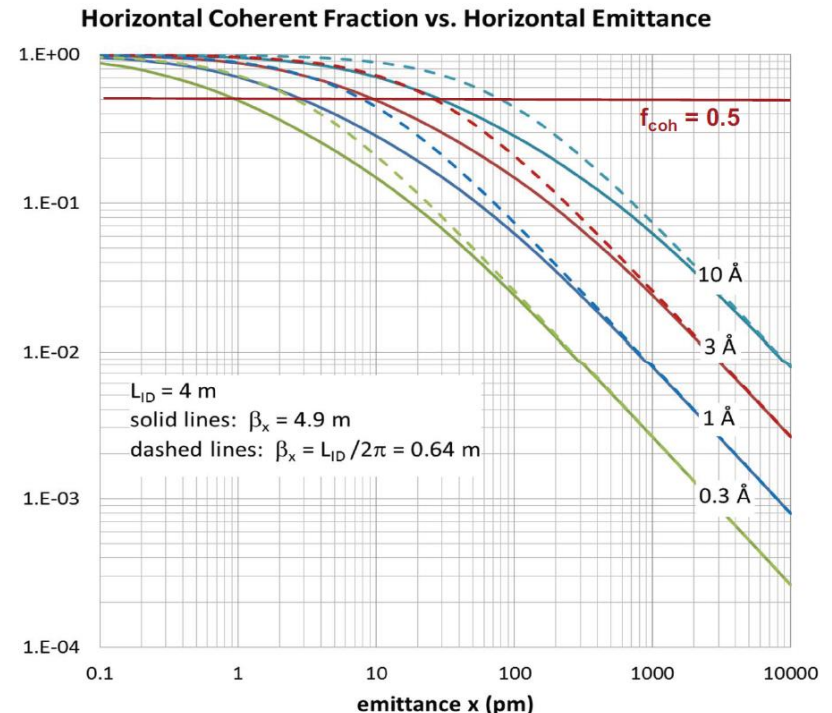
Reducing the emittance increases also the transverse coherence of the radiation

The coherent fraction is defined as the ratio of the photon flux which is diffraction limited, hence

$$f_{coh}(\lambda) = \frac{\lambda / 4\pi}{(\varepsilon_x(e^-) \oplus \varepsilon_r(\lambda))} \cdot \frac{\lambda / 4\pi}{(\varepsilon_y(e^-) \oplus \varepsilon_r(\lambda))}$$

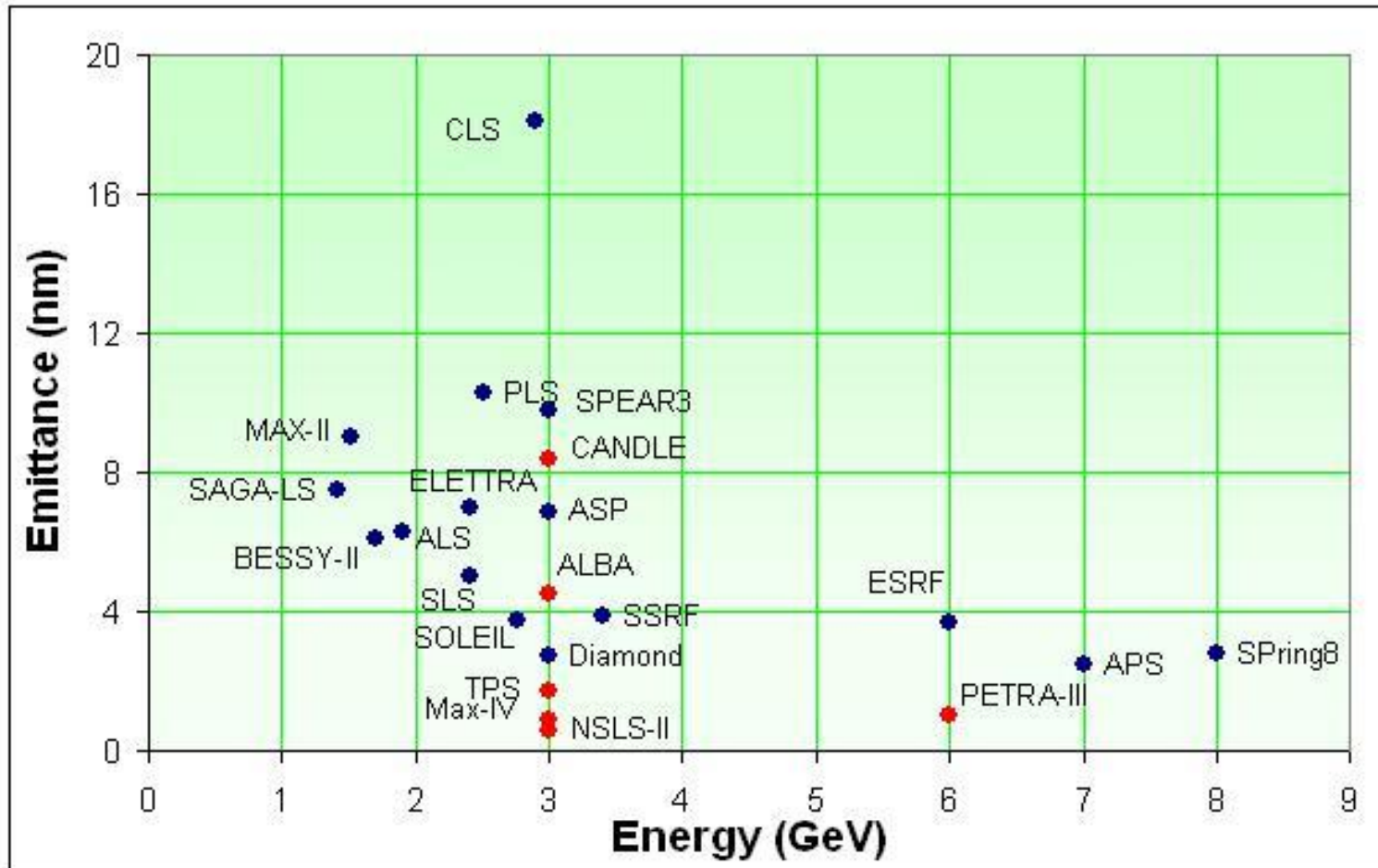
A source where the electron beam has the same size and divergence of the photon beam correspond to a coherent fraction of only 50% (in each plane!)

Smaller electron beam emittances are necessary to increase the coherent fraction (beside increasing the brilliance)



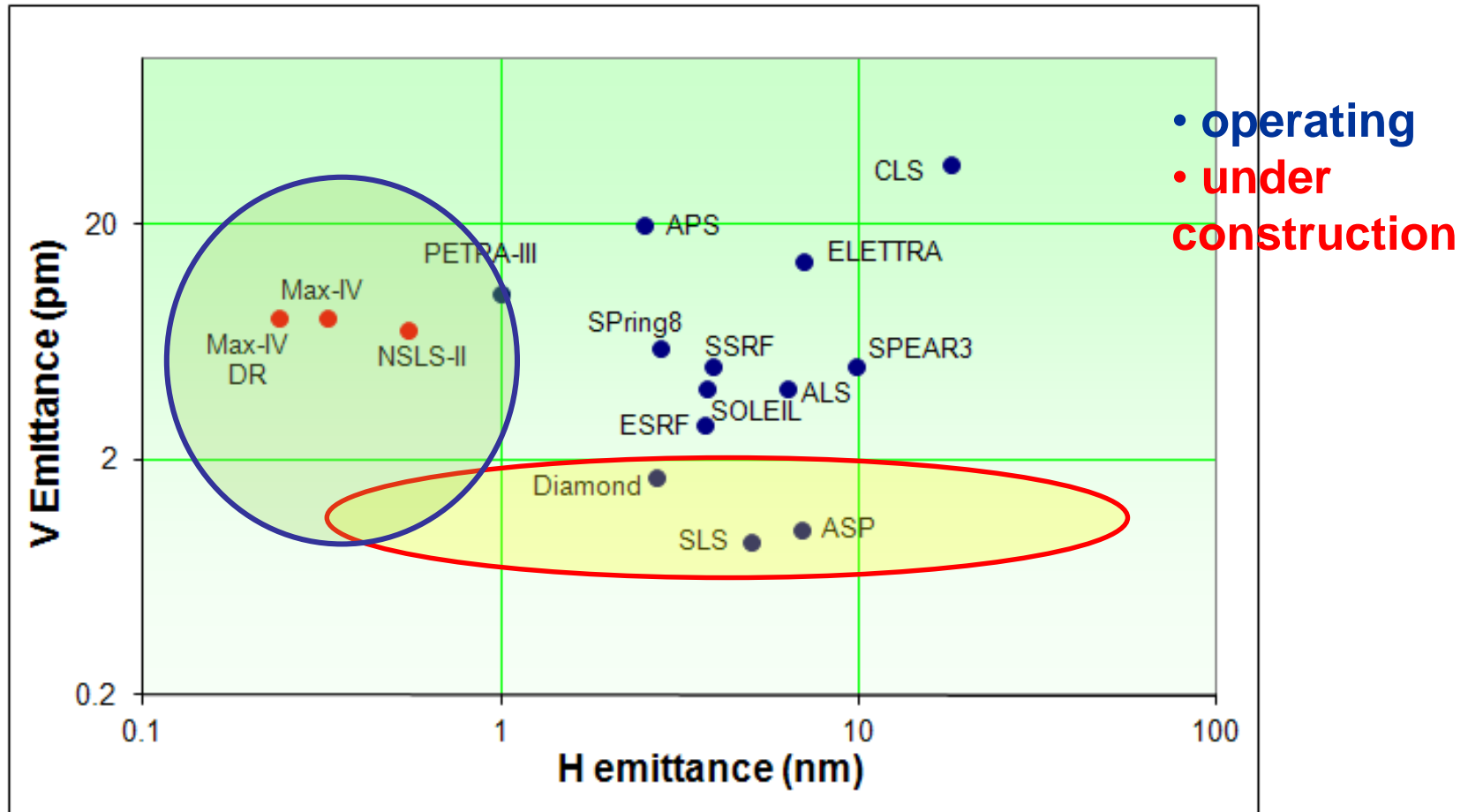
Emittance of third generation light sources

The brilliance of the photon beam is determined (mostly) by the electron beam emittance that defines the source size and divergence. The horizontal emittance of existing light sources are very far from the diffraction limit



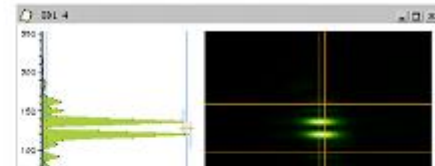
Emittance of third generation light sources

The emittance in the vertical plane however has been reduced to the pm range in several light sources. This radiation is diffraction limited in the vertical plane up to the hard X-rays

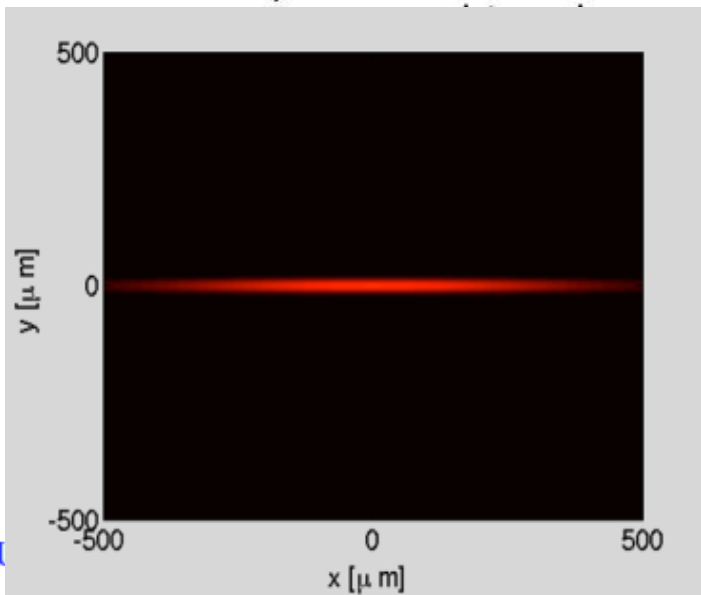


Records for smallest vertical emittance (2011-2014)

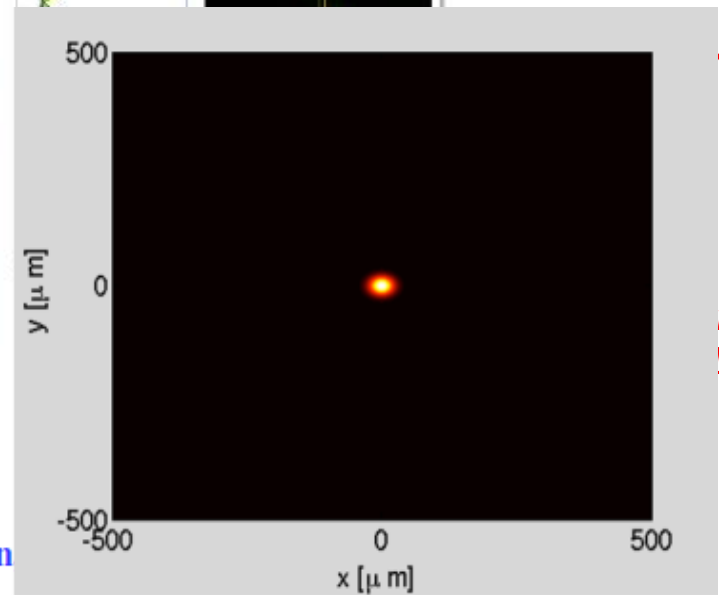
- Beam size $3.6 \pm 0.6 \mu\text{m}$
- Emittance $0.9 \pm 0.4 \text{ pm}$
- SLS beam cross section (in short undulator straight, 2σ)



SLS



PAC2014, Dresden



VERTICAL EMITTANCE AT THE QUANTUM LIMIT

0.35 pm

R. Dowd, Y-R. E. Tan, Australian Synchrotron, Clayton, Australia

K. P. Wootton, University of Melbourne, Parkville, Australia

Low Emittance lattices

Lattice design has to provide low emittance **and** adequate space in straight sections to accommodate long Insertion Devices

$$\varepsilon_x = C_q \frac{\gamma^2}{J_x \rho} \langle H \rangle_{\text{dipole}} \quad H(s) = \gamma D^2 + 2\alpha D D' + \beta D'^2$$

Minimise β and D and be close to a waist in the dipole $C_q = \frac{55}{32\sqrt{3}} \frac{\hbar}{mc} = 3.84 \cdot 10^{-13} \text{m}$

Zero dispersion in the straight section was used especially in early machines

avoid increasing the beam size due to energy spread

hide energy fluctuation to the users

allow straight section with zero dispersion to place RF and injection

decouple chromatic and harmonic sextupoles

DBA and TBA lattices provide low emittance with large ratio between

Length of straight sections

Circumference

Flexibility for optic control for apertures (injection and lifetime)

3rd generation storage ring LS and damping rings

Specific lattices are used in synchrotron light sources

- (FODO)
- TME like lattices
- DBA
- TBA
- QBA
- MBA
- controlled dispersion in straight sections

Other specific techniques are used for reducing the emittance, using

- gradient dipoles
- longitudinal gradient dipoles
- insertion devices and damping wigglers (NSLS-II) MAX IV, Pep-X

Low emittance lattices

Low emittance and adequate space in straight sections to accommodate long Insertion Devices are obtained in

Double Bend Achromat (DBA)

Triple Bend Achromat (TBA)

DBA used at:

ESRF,
ELETTRA,
APS,
SPring8,
Bessy-II,
Diamond,
SOLEIL,
SPEAR3

...

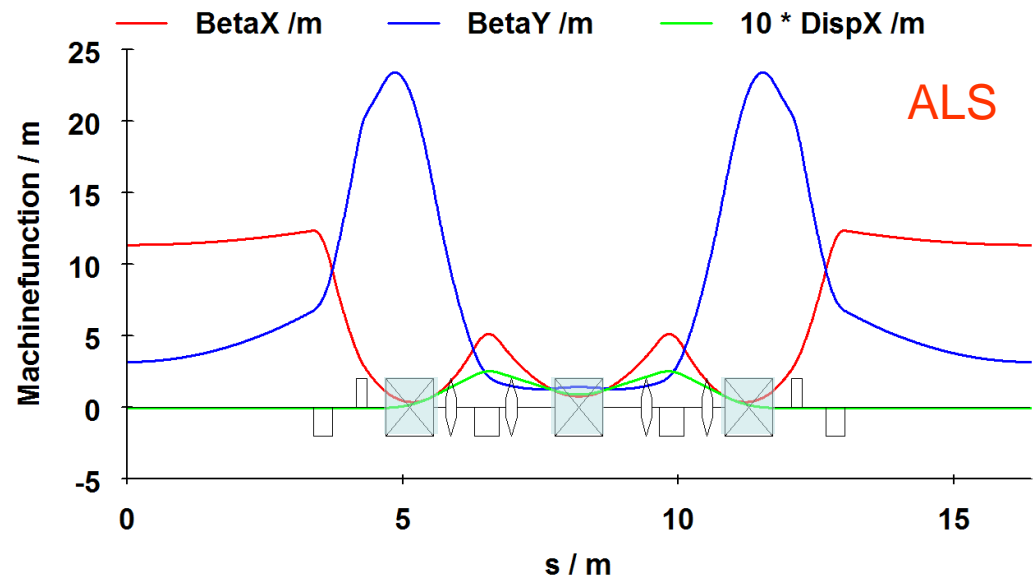
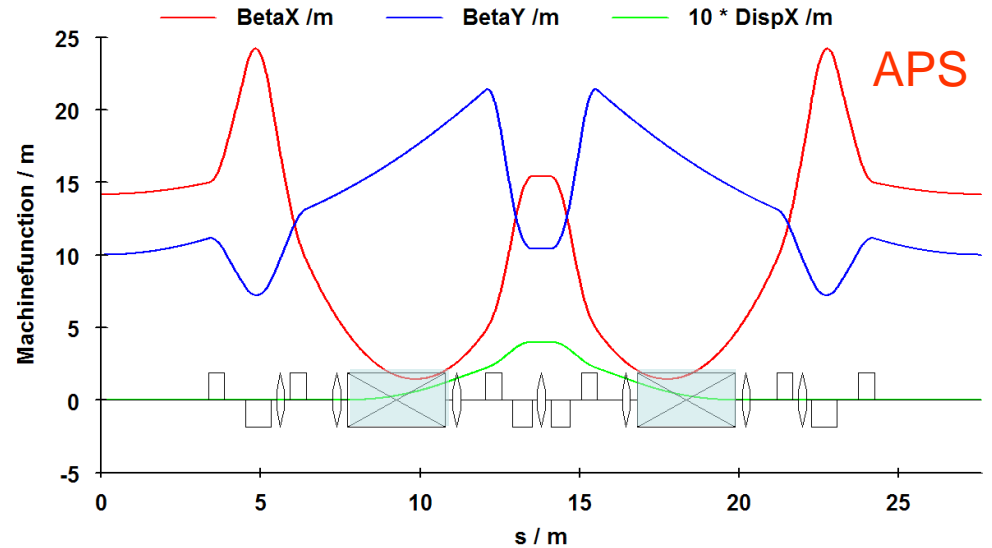
TBA used at

ALS,
SLS,
PLS,
TLS
...

$$\varepsilon_x = F \frac{C_q \gamma^2 \theta_b^3}{J_x} \propto \frac{1}{N_b^3}$$

$$F_{MEDBA} = \frac{1}{4\sqrt{15}}$$

$$F_{MEDBA-disp} = \frac{1}{12\sqrt{15}}$$



Breaking the achromatic condition

Leaking dispersion in straight sections reduces the emittance

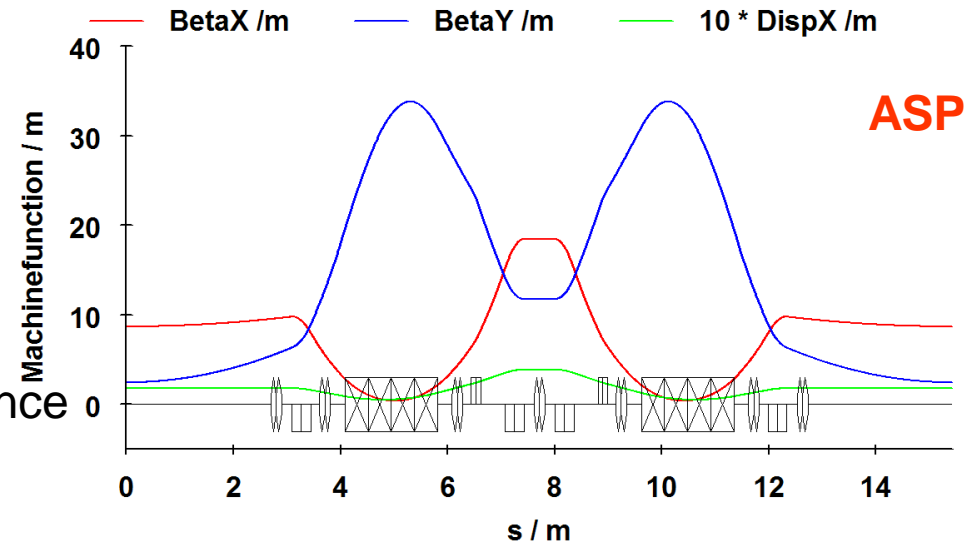
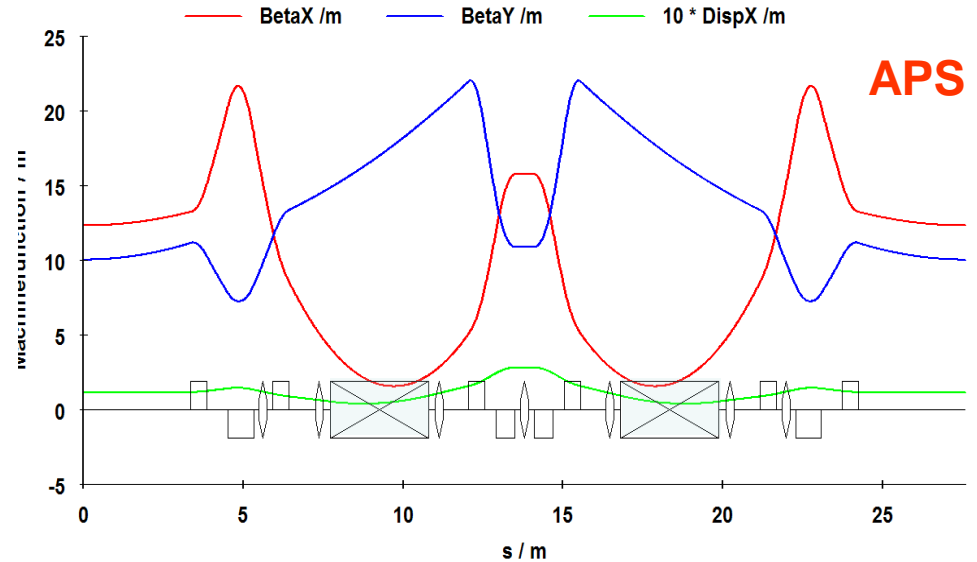
ESRF	7 nm → 3.8 nm
APS	7.5 nm → 2.5 nm
SPring8	4.8 nm → 3.0 nm
SPEAR3	18.0 nm → 9.8 nm
ALS (SB)	10.5 nm → 6.7 nm

$$F_{MEDBA} = \frac{1}{4\sqrt{15}} \quad F_{MEDBA-disp} = \frac{1}{12\sqrt{15}}$$

The emittance is reduced but the dispersion in the straight section increases the beam size

$$\sigma_x = \sqrt{\varepsilon_x \beta_x + (\sigma_E D_x)^2}$$

Need to make sure the effective emittance and ID effects are not made worse



Low emittance lattices

New designs envisaged to achieve sub-nm emittance involve

Damping Wigglers

Petra-III: 1 nm

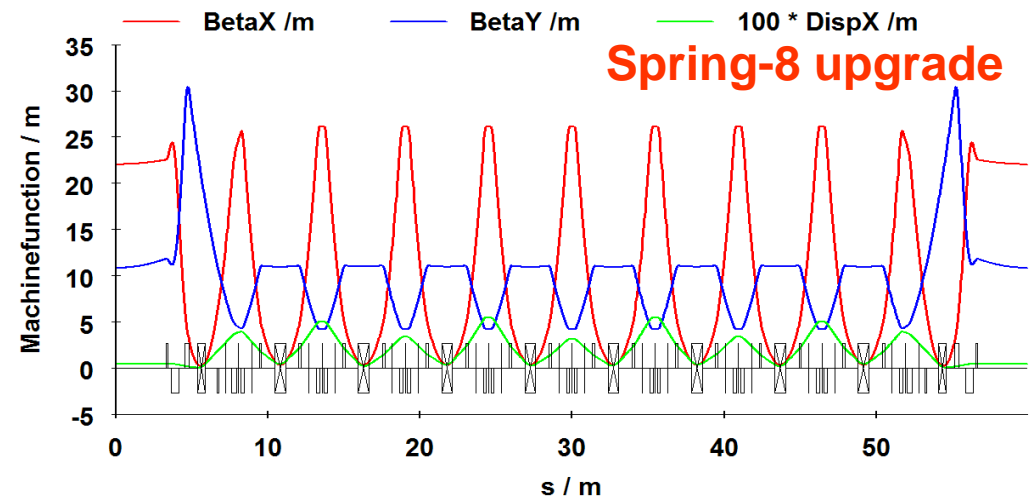
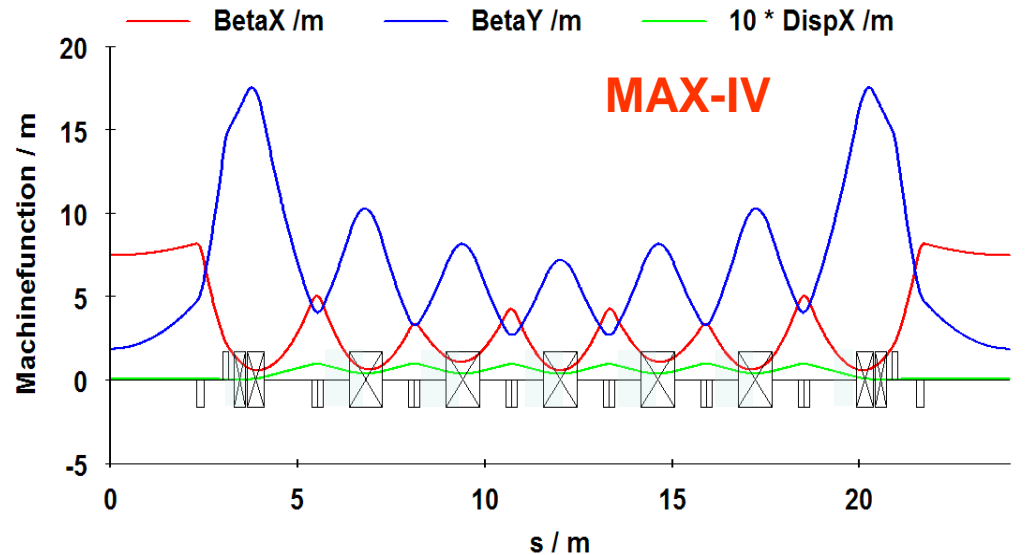
NSLS-II: 0.5 nm

MBA

MAX-IV (7-BA): 0.5 nm

Spring-8 (10-BA): 83 pm (2006)

10-BA had a DA -6.5 mm $+9$ mm
reverted to a QBA (160 pm)
now 6BA with 70 pm



Where is the equilibrium emittance generated?

The formula for the emittance tells us that the emittance is generated in the dipoles (and insertion devices), i.e. in the elements where radiation is generated.

In fact emittance is determined by the equilibrium between radiation diffusion and radiation damping

$$\varepsilon_x = C_q \frac{\gamma^2}{J_x \rho} \langle H \rangle_{\text{dipole}} \quad H(s) = \gamma \mathcal{D}^2 + 2\alpha \mathcal{D} \mathcal{D}' + \beta \mathcal{D}'^2$$

We can try to tailor the optics functions in each single dipole in order to reduce the value of $\langle H \rangle_{\text{dip}}$. Indeed it is possible to show that there is a minimum emittance condition

This condition can be used to generate TME-like lattice with long straight sections by using matching sections.

Let us start with a single dipole...

Minimum emittance from a single dipole (I)

We want the general expression for $\langle H \rangle_{\text{dipoles}}$ in terms of the initial optics function, at the beginning of the dipole. In this way

$$\varepsilon_x = \frac{\gamma^2}{J_x \rho} \langle H \rangle_{\text{dipole}} \quad H(s) = \gamma \mathcal{D}^2 + 2\alpha \mathcal{D} \mathcal{D}' + \beta \mathcal{D}'^2$$

becomes a function of

$$(\alpha_0, \beta_0, D_0, D'_0)$$

since γ_0 will be uniquely defined by α_0 and β_0 . The TME condition is found by setting the gradient of $\langle H \rangle_{\text{dipoles}}$ to zero with respect to $(\alpha_0, \beta_0, D_0, D'_0)$.

It is often common to operate with achromatic condition in the straight section, which means fixing D_0 and D'_0 to zero at the entrance or at the exit of the magnet. In doing so we lose two fit parameters, since $(D_0, D'_0) = (0, 0)$, and accordingly the minimum emittance value will be higher than that achieved in the general case.

Let us see how the optics functions evolve in a sector bending magnet

Minimum emittance from a single dipole (II)

If the dipole radius is ρ and the gradient is K we let

$$k(s) = \frac{1}{\rho^2} - K$$

and naming

$$\phi = \sqrt{|k|} \quad S(s) = \sin(\phi s) \quad C(s) = \cos(\phi s)$$

The optics functions in the dipole evolve as

$$\beta(s) = \beta_0 C^2 - 2\alpha_0 \frac{CS}{\phi} + \gamma_0 \frac{S^2}{\phi^2}$$

$$\alpha(s) = -\frac{1}{2} \frac{d\beta}{ds} = \beta_0 \phi CS + \alpha_0 (C^2 - S^2) - \gamma_0 \frac{CS}{\phi}$$

$$\gamma(s) = \beta_0 \phi^2 S^2 + 2\alpha_0 \phi CS + \gamma_0 C^2$$

and the dispersion in the sector bend reads

$$D(s) = D_0 C + \frac{D'_0}{\phi} S + \frac{1}{\rho \phi^2} (1 - C) \quad D'(s) = D'_0 C + (1 - D_0 \rho \phi^2) \frac{S}{\rho \phi}$$

Minimum emittance from a single dipole (III)

Using the previous equations we can compute the dispersion invariant and integrate it over the dipole length. Check this as an exercise!

$$\begin{aligned} \langle H(\beta_0, \alpha_0, D_0, D'_0) \rangle_{\text{dipoles}} &= \gamma_0 D_0^2 + 2\alpha_0 D_0 D'_0 + \beta_0 D'^2_0 + \\ &+ \frac{2L}{\rho} \left[-(\gamma_0 D_0 + \alpha_0 D'_0) \frac{\phi L - \sin \phi L}{\phi^3 L^2} + (\alpha_0 D_0 + \beta_0 D'_0) \frac{1 - \cos \phi L}{\phi^2 L^2} \right] + \\ &+ \frac{L^2}{\rho^2} \left[\gamma_0 \frac{3\phi L - 4\sin \phi L + \sin \phi L \cos \phi L}{2\phi^5 L^3} - \alpha_0 \frac{(1 - \cos \phi L)^2}{\phi^4 L^3} + \beta_0 \frac{\phi L - \cos \phi L \sin \phi L}{2\phi^3 L^3} \right] \end{aligned}$$

This expression is usually simplified in the literature. Assume that

- no combined function gradient exists, i.e. $K = 0$
- the bend angle is small. Approximate $\theta = L/\rho \ll 1$

$$\begin{aligned} \langle H(\beta_0, \alpha_0, D_0, D'_0) \rangle_{\text{dipoles}} &= \rho \theta^3 \left\{ \gamma_0 L \frac{D_0^2}{(\theta L)^2} + 2\alpha_0 \frac{D_0}{\theta L} \frac{D'_0}{\theta} + \frac{\beta_0}{L} \frac{D'^2_0}{\theta^2} + \right. \\ &+ \frac{1}{\rho \theta^2} \left[\left(\alpha_0 \frac{2(1 - \cos \theta)}{\theta^2} - \gamma_0 L \frac{2(\theta - \sin \theta)}{\theta^3} \right) D_0 + \left(\beta_0 \frac{2(1 - \cos \theta)}{\theta^2} - \alpha_0 D'_0 L \frac{2(\theta - \sin \theta)}{\theta^3} \right) D'_0 \right] + \\ &+ \left. \frac{1}{\rho \theta} \left[\beta_0 \frac{2\theta - \sin 2\theta}{4\theta^3} - \alpha_0 L \frac{3 - 4\cos \theta + \cos 2\theta}{\theta^4} + \gamma_0 L^2 \frac{6\theta - 8\sin \theta + \sin 2\theta}{4\theta^5} \right] \right\} \end{aligned}$$

Minimum emittance from a single dipole (IV)

We now look for the initial optic functions that minimise the previous expression. Making the gradient of $\langle H \rangle_{\text{dipole}}$ zero we obtain the following results

$$\langle H \rangle_{\text{dipoles}} = \frac{1}{12\sqrt{15}} \rho \theta^3$$

This minimum is reached for the following set of optics functions computed at the centre of the dipoles

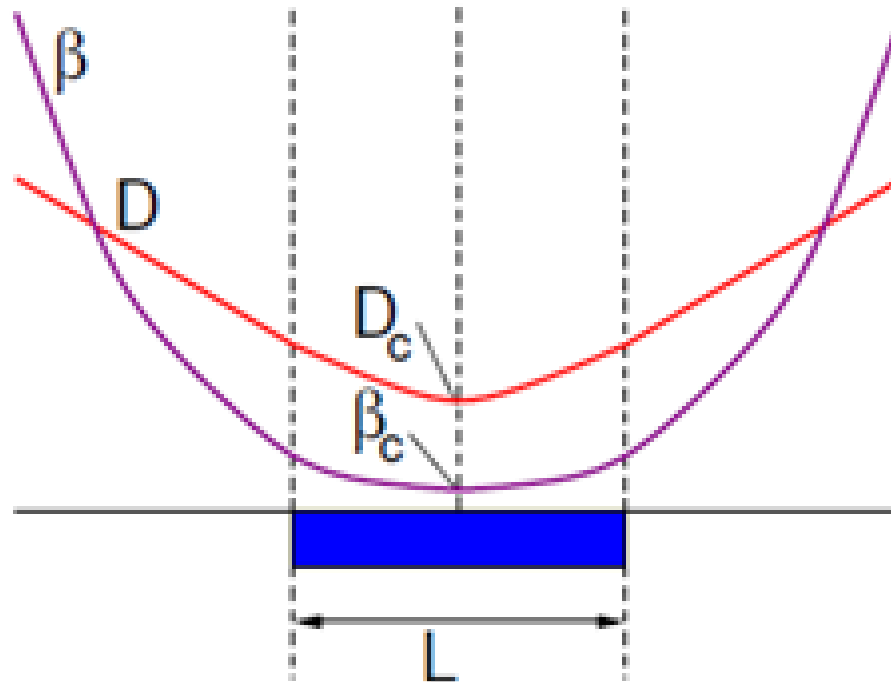
$$\beta_c = \frac{L}{2\sqrt{15}} \quad \alpha'_c = 0 \quad D_c = \frac{L\theta}{24} = \frac{L^2}{24\rho} \quad D'_c = 0$$

This optics gives the **theoretical minimum emittance** (TME) in the limit of small dipole angle

$$\varepsilon_x = \frac{1}{12\sqrt{15}} \frac{C_q \gamma^2 \theta^3}{J_x} \quad \text{theoretical minimum emittance}$$

Minimum emittance from a single dipole (V)

The optics through the dipole looks like



Courtesy A. Streun

To build now a full lattice we can flank this dipole by a matching sections to create a full ring, repeating periodically the TME-cell

Since $\varepsilon \propto \theta^3$ many small angle bending are favoured to reach smaller emittances

The dispersion is non zero in the straight section and it cannot be zeroed without further dipoles

Minimum emittance from a single dipole (VI)

If we start with an achromatic condition at the beginning (or end) of the dipole we must find a minimum of $\langle H \rangle$ dipoles as a function of

$$(\alpha_0, \beta_0) \text{ with } (D_0, D'_0) = (0, 0)$$

The average of the dispersion invariant is

$$\langle H \rangle_{\text{dipoles}} = \frac{1}{4\sqrt{15}} \rho \theta^3 \quad \text{this is three time larger than the TME}$$

The condition for the minimum emittance and requires that the focus of the beta function ($\alpha_f = 0$), i.e. the minimum of β is reached in the first half of the dipole and occurs at

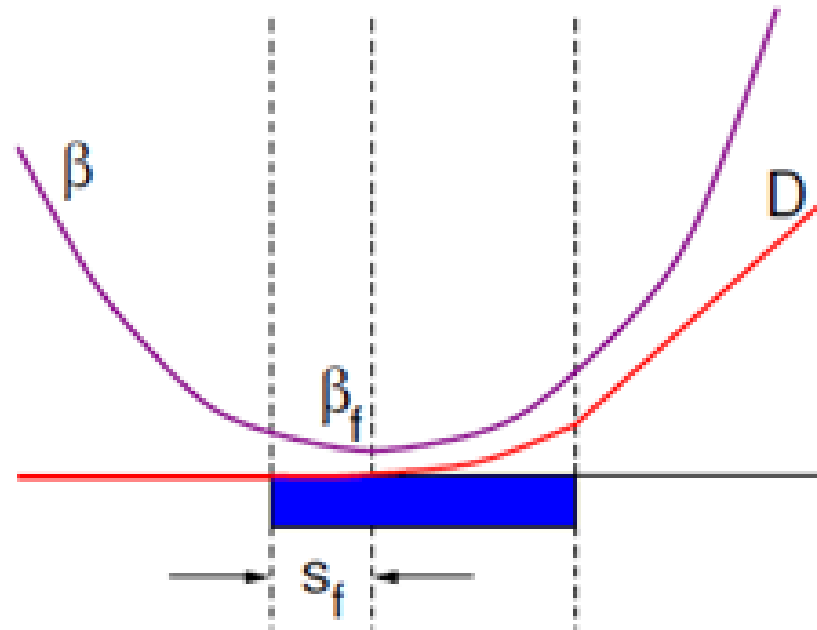
$$s_f = \frac{3}{8}L \quad \text{and } \beta \text{ reads} \quad \beta_f = \frac{1}{8} \sqrt{\frac{3}{5}}L$$

In this case, the values of the optics functions at the entrance of the dipole are

$$\beta_0 = 2L \sqrt{\frac{3}{5}} \quad \alpha_0 = \sqrt{15} \quad D_0 = D'_0 = 0$$

Minimum emittance from a single dipole (VII)

The optics through the dipole looks like



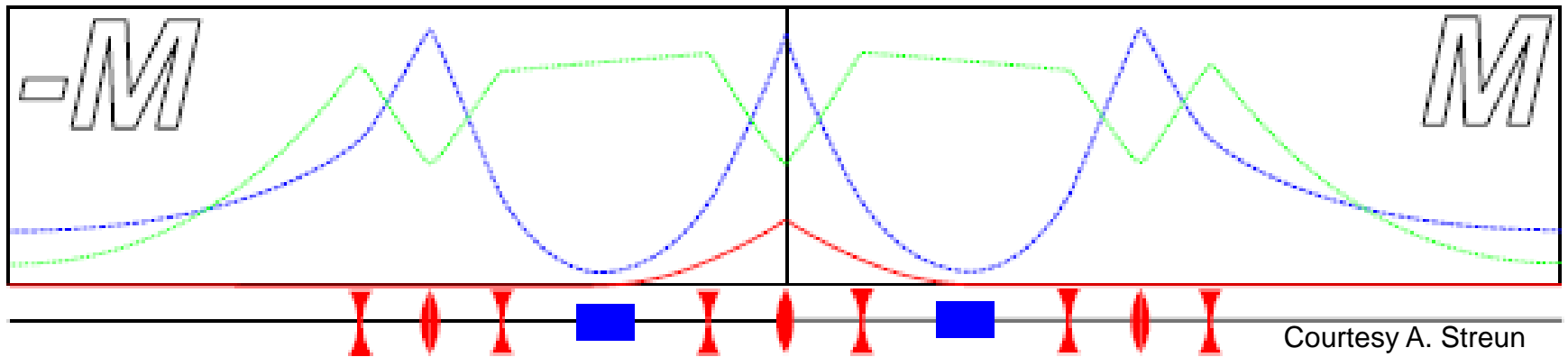
Courtesy A. Streun

To close the dispersion this cell can be repeated mirror symmetrically using a quadrupoles. This is the simplest form of a double bend achromat called **Chashman-Green** lattice

Since $\varepsilon \propto \theta^3$ many small angle bending are favoured to reach smaller emittances

Double bend achromat

A matching section can be added to tailor the optics for an insertion device as in



This is the basic structure of a DBA lattice used in many light sources

The horizontal emittance reached in medium size machines is in the order of few nm

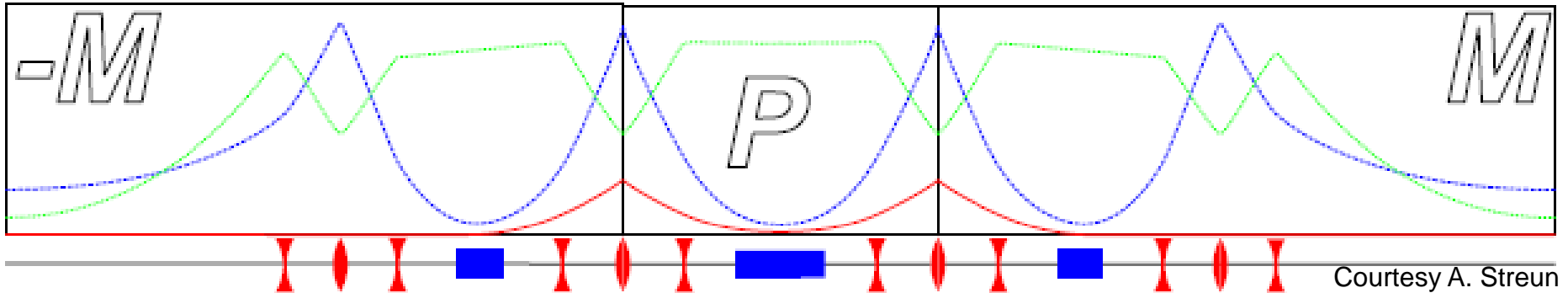
$$\varepsilon_x = F \frac{C_q \gamma^2 \theta_b^3}{J_x}$$

$$F_{MEDBA} = \frac{1}{4\sqrt{15}}$$

DBA
theoretical minimum emittance

Triple bend achromat

A TME cell can be added in between a DBA cell to generate a TBA cell



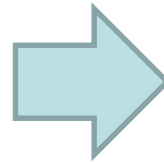
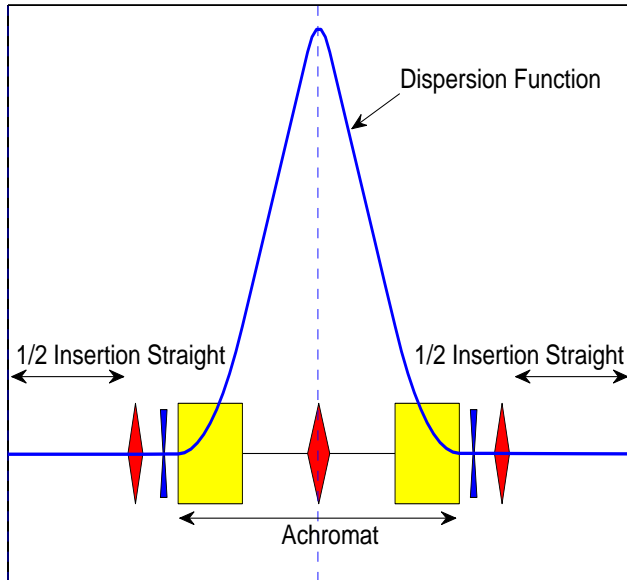
Notice that we cannot naively assume that the minimum emittance of the TBA is the average of the TME of a DBA and one TME cell.

We need to match the optics function between the two cells and this proves to be impossible if we use only quadrupoles and leave the same type of dipole, i.e. same strength and same length. In particular we cannot match the dispersion invariant at the dipole ends

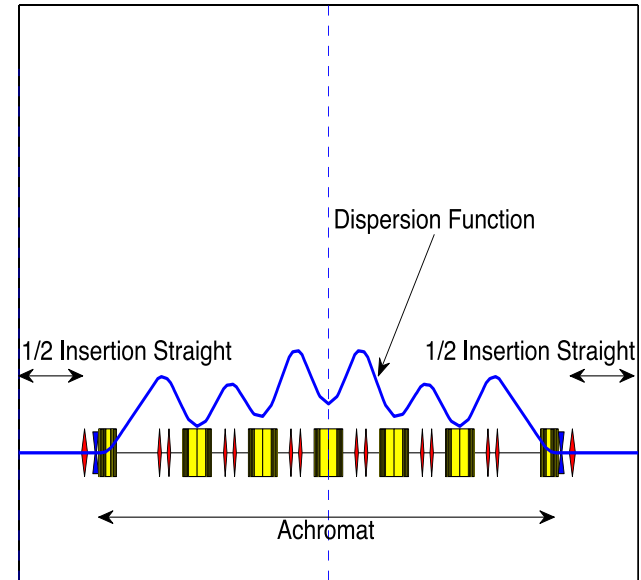
The condition for matching with minimum emittance require the external dipole to be shorter by $1/\sqrt{3}$.

Low emittance with multiple bend achromats

DBA



7BA



Simplified explanation

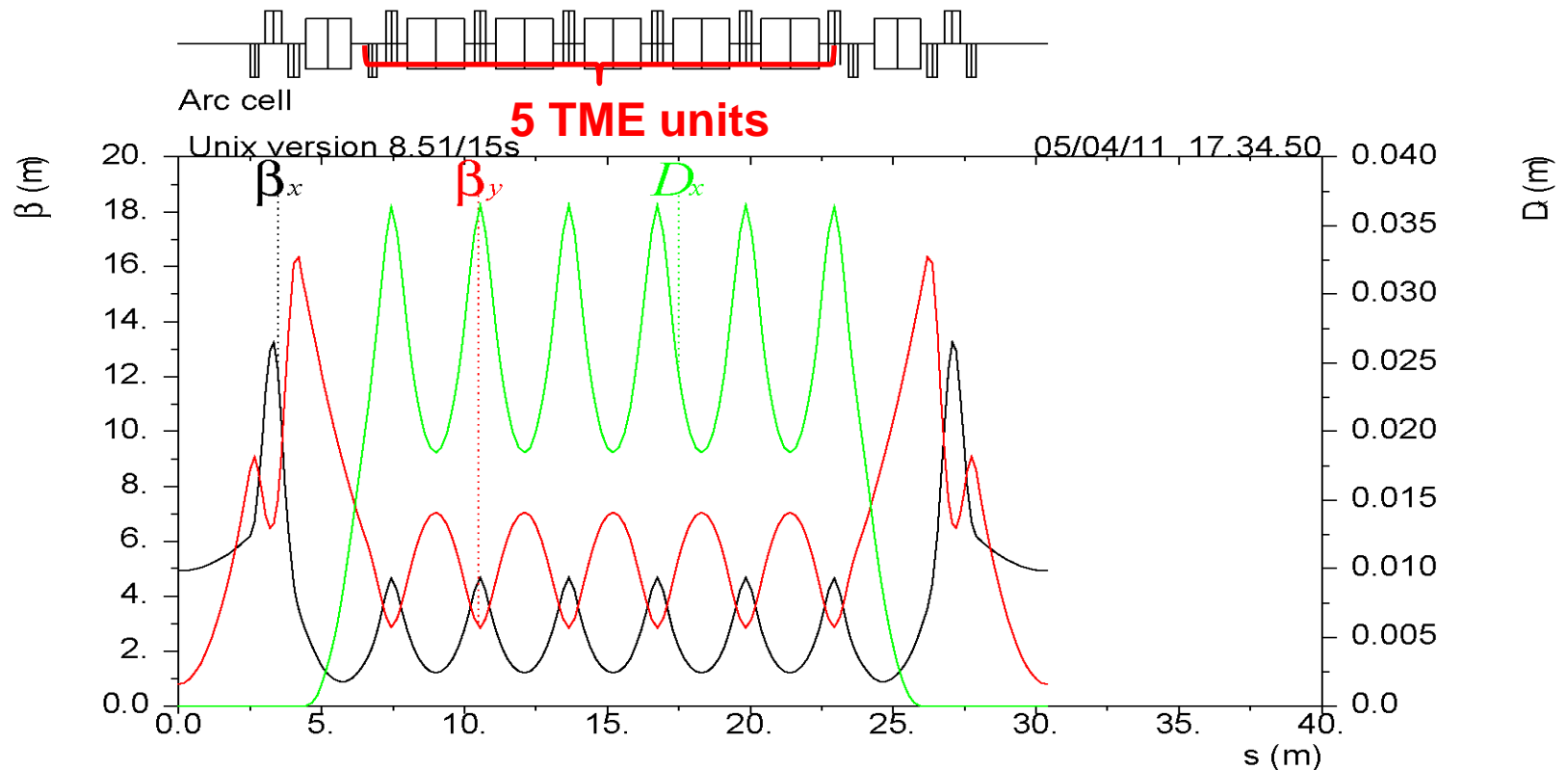
- Emittance is driven by randomness of photon emission in presence of dispersive (energy-dependent) orbits – electron recoils randomly
- Breaking up dipoles and putting focusing (quadrupoles) between the parts allows reducing the amplitude of dispersive orbits – smaller electron recoils

Multi bend achromat

In much the same way more than one TME cell can be added in between a DBA cell to generate a MBA cell

With many small bending magnets the overall scaling of the emittance $\varepsilon \propto \theta^3$ will generate very small emittances

As the Pep-X lattice a 7BA with 5 TME cells



Summary

The formula for the emittance can be summarised as

$$\varepsilon_x = F \frac{C_q \gamma^2 \theta_b^3}{J_x} \propto \frac{1}{N_b^3}$$

where

$$F_{\text{TME}} = \frac{1}{12\sqrt{15}}$$

$$\varepsilon_{\text{METBA}} \approx 0.66 \varepsilon_{\text{MEDBA}}$$

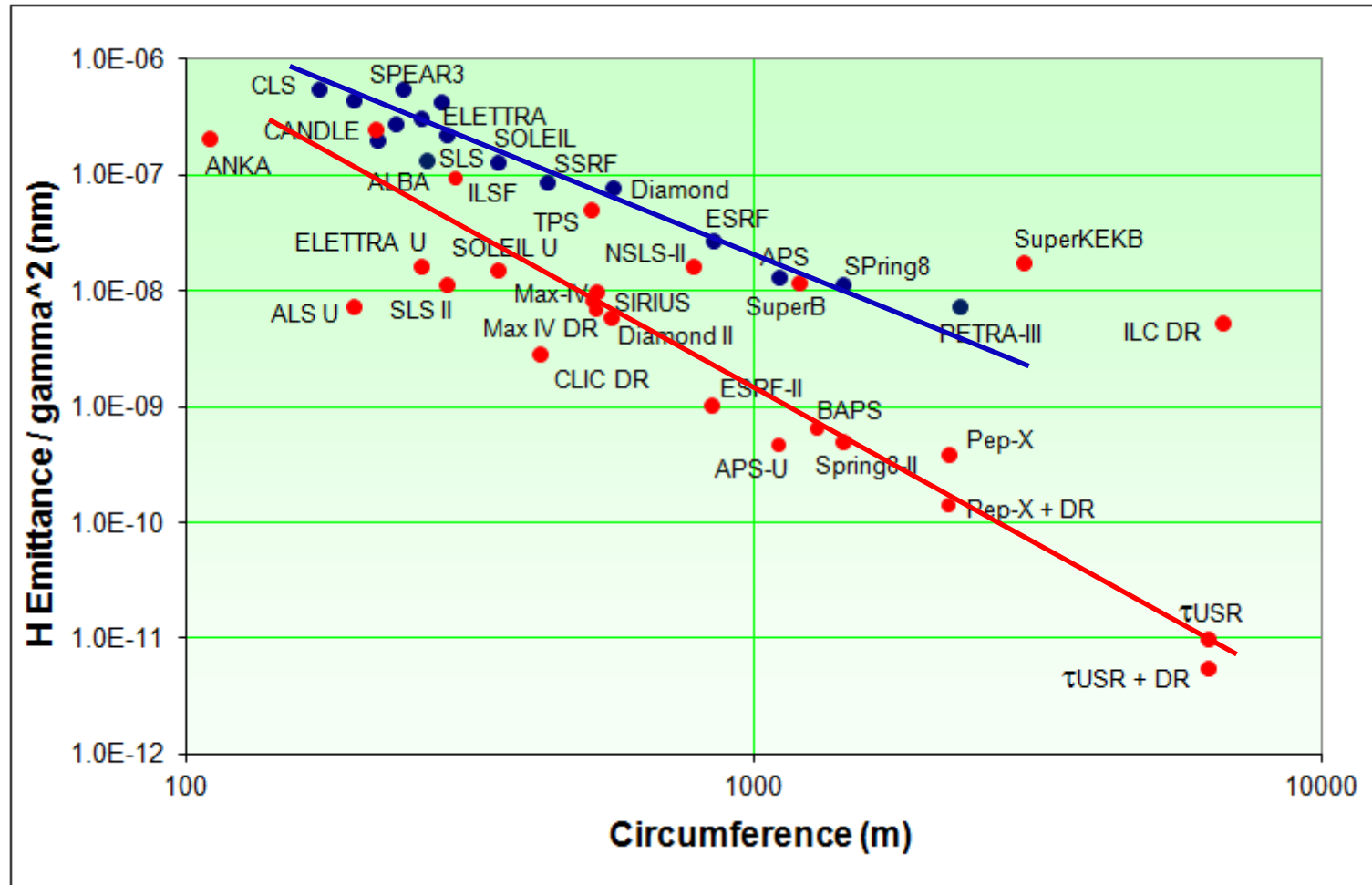
$$F_{\text{MEDBA}} = \frac{1}{4\sqrt{15}}$$

$$\varepsilon_{\text{MEQBA}} \approx 0.55 \varepsilon_{\text{MEDBA}}$$

In general we can say that the emittance scaling with the cubic power of the bending angle favours rings with a large number of bending and therefore, broadly speaking with a large circumference C .

$$\varepsilon_x = F \frac{C_q \gamma^2 \theta_b^3}{J_x} \propto \frac{1}{N_b^3} \propto \frac{1}{C^3}$$

Emittance vs circumference



The design of the most recent synchrotron light sources pushes the emittance close to the diffraction limit at hard X-rays also in the horizontal plane

Further emittance reduction: damping wigglers (I)

Insertion device can have a strong impact on the equilibrium beam properties, namely on the emittance

The IDs modify the radiation integrals. The modification to the equilibrium beam properties can be computed from the modification to the radiation integrals (usually $I_4 \ll I_2$)

$$\varepsilon_x = C_q \gamma^2 \frac{I_5}{I_2 - I_4} = C_q \gamma^2 \frac{I_{5,\text{arcs}} + I_{5,\text{ID}}}{I_{2,\text{arcs}} + I_{2,\text{ID}} - (I_{4,\text{arcs}} + I_{4,\text{ID}})} \sim C_q \gamma^2 \frac{I_{5,\text{arcs}} + I_{5,\text{ID}}}{I_{2,\text{arcs}} + I_{2,\text{ID}}}$$

Let us consider a insertion device made by a linear undulator with peak field B_{ID} and period λ_u . The curvature radius associated to the trajectory reads

$$\frac{1}{\rho} = \frac{1}{\rho_{\text{ID}}} \cos\left(\frac{2\pi s}{\lambda_u}\right) \quad \text{where} \quad \frac{1}{\rho_{\text{ID}}} = \frac{e}{p} B_{\text{ID}} = \frac{ec}{\beta E} B_{\text{ID}}$$

is the bending radius corresponding to the peak magnetic field B_{ID} of the ID.

Modification to the radiation integrals I_2 and I_3

The computation of the additional terms generated by the IDs requires some care. The radiation integrals depending only on the radius of curvature are straightforward

$$I_{2,ID} = \oint_{ID} \frac{1}{\rho^2} ds = \left\langle \frac{1}{\rho^2} \right\rangle_{ID} = \frac{1}{2} \sum_{i=1}^{N_{ID}} \frac{L_{i,ID}}{\rho_{i,ID}^2}$$

$$I_{3,ID} = \oint_{ID} \frac{1}{|\rho^3|} ds = \left\langle \frac{1}{\rho^3} \right\rangle_{ID} = \frac{4}{3\pi} \sum_{i=1}^{N_{ID}} \frac{L_{i,ID}}{\rho_{i,ID}^3}$$

where $L_{i,ID}$ the length of the ID. They both increase with the ID field and ID length.

The radiation integrals involving also the dispersion and the optics functions are usually calculated assuming either that the self-dispersion is negligible or, on the opposite end, that there is only the self-dispersion contribution.

Let us see how to compute the self dispersion generated by the ID:

Self dispersion in IDs

The ID, as any bending magnet, also modifies the dispersion function. The effect of the ID on the dispersion is usually characterised by the concept of self-dispersion, i.e. the dispersion generated by the ID in a straight section in absence of any other dispersion. The self dispersion in the ID is given by

$$D(s) = \left(\frac{\lambda_u}{2\pi}\right)^2 \frac{1}{\rho_{ID}} \cos\left(\frac{2\pi s}{\lambda_u}\right) \quad D'(s) = \left(\frac{\lambda_u}{2\pi}\right) \frac{1}{\rho_{ID}} \sin\left(\frac{2\pi s}{\lambda_u}\right)$$

When self dispersion dominates we have

$$I_{5,ID} = \frac{1}{\rho_{ID}^5} \left(\frac{2\pi}{\lambda_u}\right)^2 \oint_{ID} \left(\frac{\left(\frac{2\pi}{\lambda_u}\right)^2 \cos^5\left(\frac{2\pi}{\lambda_u} s\right)}{\langle \beta_{i,ID} \rangle} + \langle \beta_{i,ID} \rangle \left| \cos^3\left(\frac{2\pi}{\lambda_u} s\right) \right| \sin^2\left(\frac{2\pi}{\lambda_u} s\right) \right) ds$$

The second term dominates the first, therefore we are left with

$$I_{5,ID} = \frac{\lambda_u^2}{15\pi^3 \rho_{ID}^5} \langle \beta_{x,ID} \rangle L$$

External dispersion in IDs

If the external dispersion is large and self dispersion can be neglected we have

$$I_{5,\text{ID}} = \oint_{\text{ID}} \frac{H}{|\rho^3|} ds = \frac{4}{3\pi} \sum_{i=1}^{N_{\text{ID}}} \frac{\langle H \rangle_{i,\text{ID}}}{|\rho_{i,\text{ID}}^3|} L_{i,\text{ID}}$$

The expression for $I_{5,\text{ID}}$ can be computed by using the value of the dispersion invariant $H_{i,\text{ID}}$ at the centre of the straight section which usually has a waist for the optics function, i.e. $\alpha_{i,\text{ID}} = 0$, therefore

$$\langle H \rangle_{i,\text{ID}} = \frac{D_{i,\text{ID}}^2}{\beta_{i,\text{ID}}} + \beta_{i,\text{ID}} D'_{i,\text{ID}}{}^2$$

The radiation integral reads

$$I_{5,\text{ID}} = \frac{4}{3\pi} \sum_{i=1}^{N_{\text{ID}}} \frac{L_{i,\text{ID}}}{|\rho_{i,\text{ID}}^3|} \left(\frac{D_{i,\text{ID}}^2}{\beta_{i,\text{ID}}} + \beta_{i,\text{ID}} D'_{i,\text{ID}}{}^2 \right)$$

Emittance reduction with IDs

Using the modified radiation integrals we can write down the expression for the equilibrium properties of the beam in a storage ring with IDs.

If I_5 is dominated by external dispersion, isomagnetic lattice, we can write

$$\frac{\varepsilon_{x,\text{ID}}}{\varepsilon_{x_0}} = \frac{1 + \frac{4}{3\pi} \frac{L}{2\pi\rho} \left(\frac{H_{\text{ID}}}{H} \right) \left(\frac{\rho}{\rho_{\text{ID}}} \right)^3}{1 + \frac{1}{2} \frac{L}{2\pi\rho} \left(\frac{\rho}{\rho_{\text{ID}}} \right)^2}$$

Thus the emittance can be increased or decreased depending on the relative values of H and r in the insertion device and in the bending magnets.

If I_5 is dominated by self-dispersion, in the isomagnetic case, we have

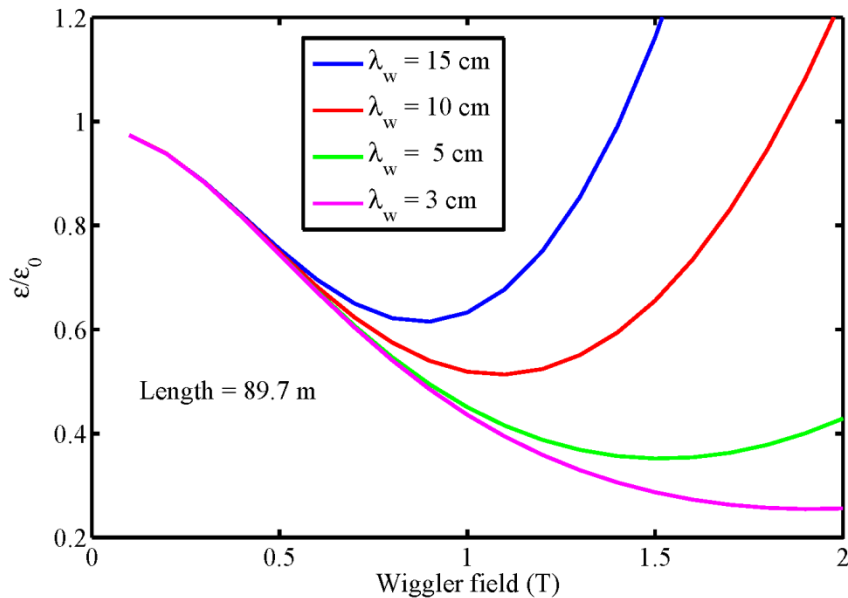
$$\frac{\varepsilon_{x,\text{ID}}}{\varepsilon_{x_0}} = \frac{1 + \frac{\lambda_u^2 \langle \beta_x \rangle L}{15\pi^3 \rho_{\text{ID}}^5 I_{5,\text{arcs}}}}{1 + \frac{1}{2} \frac{L}{2\pi\rho} \left(\frac{\rho}{\rho_{\text{ID}}} \right)^2}$$

Alternatively these expression can be used to define the limits on the insertion devices field in order not to change the equilibrium properties of the beam

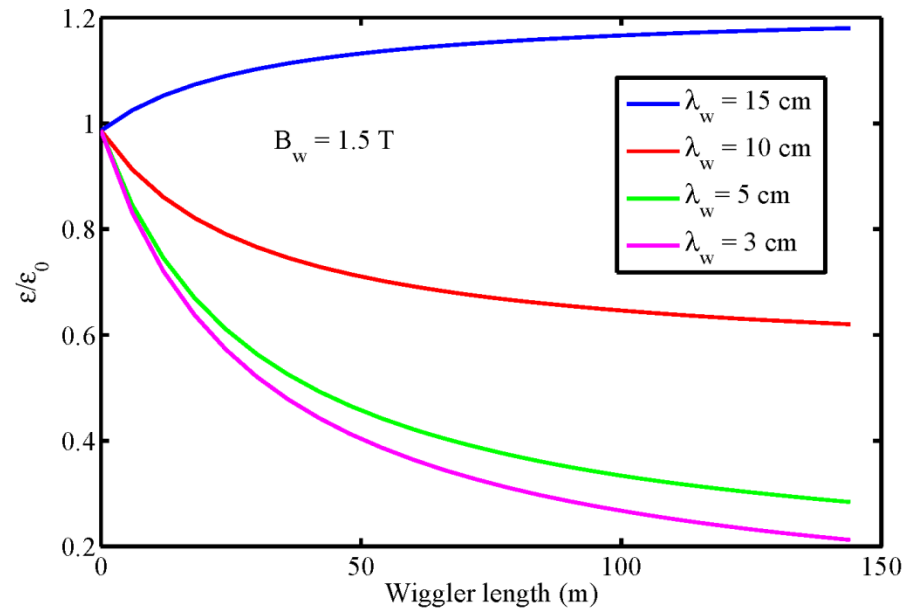
Example: Pep-X design

Emittance = 11 pm-rad at 4.5 GeV
with parameters $l_w=5$ cm, $B_w=1.5$ T

Wiggler Field Optimization



Wiggler Length Optimization



Average beta function at the wiggler section is 12.4 meter.

Energy spread change with IDs

In a similar way, using the radiation integral I_2 , I_3 , and I_4 can compute the modification to the energy spread as per

$$\left(\frac{\sigma_{\varepsilon, \text{ID}}}{U_s} \right)^2 = C_q \gamma^2 \frac{I_3}{2I_2 + I_4} = C_q \gamma^2 \frac{I_{3, \text{arcs}} + I_{3, \text{ID}}}{2(I_{2, \text{arcs}} + I_{2, \text{ID}}) + I_{4, \text{arcs}} + I_{4, \text{ID}}}$$

Since usually $I_4 \ll I_2$ we have

$$\left(\frac{\sigma_{\varepsilon, \text{ID}}}{U_s} \right)^2 = C_q \gamma^2 \frac{I_3}{2I_2} = C_q \gamma^2 \frac{I_{3, \text{arcs}} + I_{3, \text{ID}}}{2(I_{2, \text{arcs}} + I_{2, \text{ID}})}$$

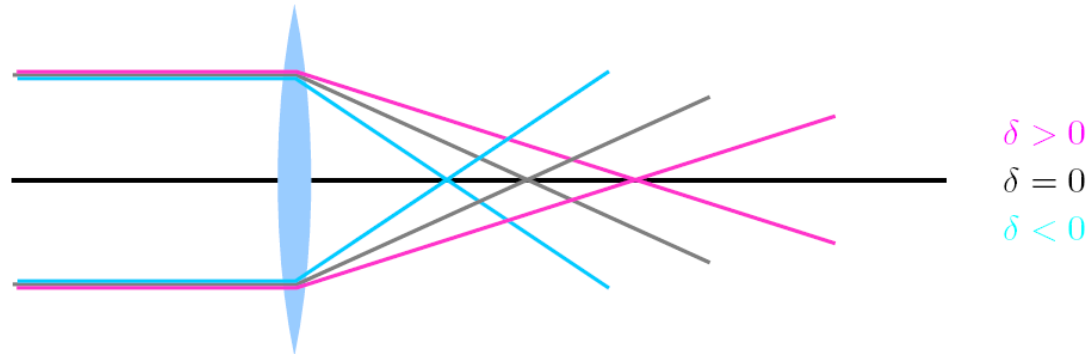
In this regime, the energy spread is defined by the radiation integrals that do not depend on the dispersion function. We have the ratio

$$\frac{\sigma'_{\varepsilon}}{\sigma_{\varepsilon}} = \left[\frac{1 + \frac{4}{3\pi} \frac{L_{\text{ID}}}{2\pi\rho} \left(\frac{\rho}{\rho_{\text{ID}}} \right)^3}{1 + \frac{1}{2} \frac{L_{\text{ID}}}{2\pi\rho} \left(\frac{\rho}{\rho_{\text{ID}}} \right)^2} \right]^{1/2}$$

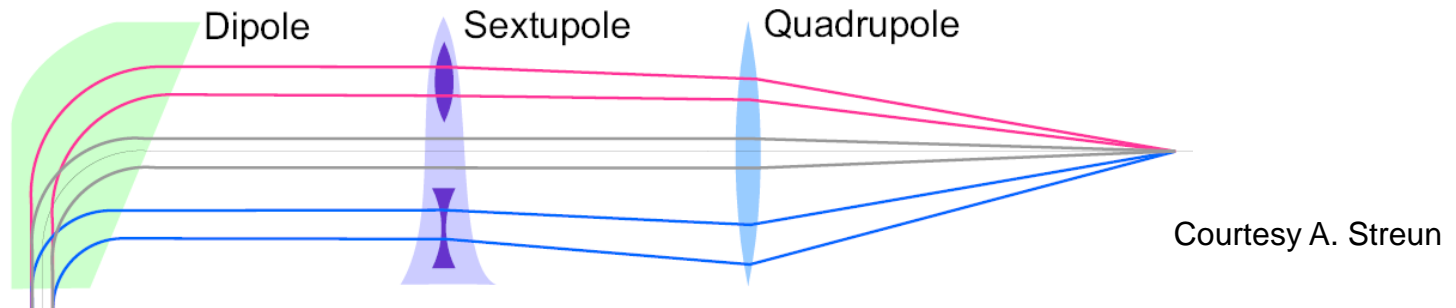
If the peak field in the ID is less than that of the bending magnets ($\rho_{\text{ID}} > \rho$) there is a reduction in energy spread, whereas if the peak ID field exceeds the bending magnet field ($\rho_{\text{ID}} < \rho$) the energy spread is increased.

Difficulties with low emittance lattices

Small emittance \rightarrow Strong quadrupoles \rightarrow Large (natural) chromaticity



\rightarrow strong sextupoles (sextupoles guarantee the focussing of off-energy particles)



strong sextupoles reduce the dynamic aperture and the Touschek lifetime

\rightarrow additional sextupoles are required to correct nonlinear aberrations

Nonlinear beam dynamics optimisation (I)

It is a complex process where the Accelerator Physicist is guided by

- (semi-)analytical formulae for the computation of nonlinear maps, detuning with amplitude and off-momentum, resonance driving terms
- numerical tracking: direct calculation of non linear tunes shifts with amplitude and off-momentum, **6D** dynamics aperture and the frequency analysis of the betatron oscillations

Many iterations are required to achieve a good solution that guarantees a good dynamic aperture for injection and a good Touschek lifetime

See lectures on nonlinear dynamics