

EXACT SOLUTIONS FOR AN EXPANDING AND ROTATING, REHADRONIZING FIREBALL

- WITH LATTICE QCD EQUATION OF STATE -

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Motivation

- ▶ Deeper understanding of rehadronization
- ▶ More accurate description of the fireball evolution
- ▶ Previous analytic solutions are single-component
- ▶ A multi-component scenario is realistic
- ▶ First create a simplified, non-relativistic model
- ▶ Relativistic generalizations on progress

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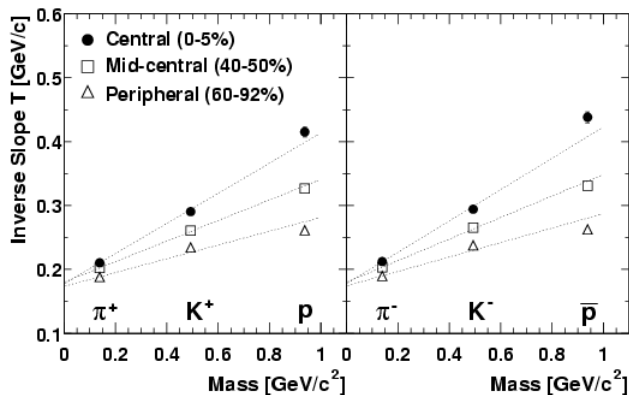
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$$T = T_f + m \langle u_t \rangle^2 \implies T_i = T_f + m_i \langle u_t \rangle^2 \quad (1)$$

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Basic equations of non-relativistic hydrodynamics

$$\frac{\partial n}{\partial t} + \nabla (n\mathbf{v}) = 0, \quad (2)$$

$$\frac{\partial \varepsilon}{\partial t} + \nabla (\varepsilon\mathbf{v}) = -p\nabla\mathbf{v}, \quad (3)$$

$$mn \left(\frac{\partial}{\partial t} + \mathbf{v}\nabla \right) \mathbf{v} = -\nabla p. \quad (4)$$

Basic equations of relativistic hydrodynamics

$$\partial_\mu (nu^\mu) = 0, \quad (5)$$

$$\partial_\nu T^{\mu\nu} = 0. \quad (6)$$

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Before the rehadronization

There's no particle conservation!

$$\varepsilon = T\sigma - p + \mu n \implies \varepsilon = T\sigma - p + \sum_i \mu_i n_i, \quad (7)$$

Since

$$\mu_i = 0, \quad (8)$$

$$\varepsilon + p = T\sigma, \quad (9)$$

$$d\varepsilon = Td\sigma, \quad (10)$$

from the energy conservation:

$$\frac{\partial \sigma}{\partial t} + \nabla \cdot (\mathbf{v}\sigma) = 0. \quad (11)$$

II. BASIC EQUATIONS

Euler equation ($\mu = 0$, $n \rightarrow 0$, $v \ll c = 1$) [3]:

$$(\varepsilon + p)(\partial_t + \mathbf{v}\nabla)\mathbf{v} = T\sigma(\partial_t + \mathbf{v}\nabla)\mathbf{v} = -\nabla p. \quad (12)$$

Equation of state (from lattice QCD [2]):

$$\varepsilon = \kappa_{QCD}(T)p. \quad (13)$$

Energy conservation \implies diff. eq. of temperature [3]:

$$\frac{1 + \kappa}{T} \left[\frac{d}{dT} \frac{\kappa T}{1 + \kappa} \right] (\partial_t + \mathbf{v}\nabla) T + \nabla \mathbf{v} = 0. \quad (14)$$

II. BASIC EQUATIONS

After the rehadronization

It was known for one component ($T \ll m \implies \mu \approx m$):

$$\varepsilon + p = \mu n + T\sigma \approx mn. \quad (15)$$

For the multi-component scenario:

$$mn = \sum_i m_i n_i, \quad (16)$$

$$p = \sum_i p_i. \quad (17)$$

But $p \ll mn$ thus:

$$\varepsilon \approx \sum_i m_i n_i \quad (18)$$

II. BASIC EQUATIONS

Euler equation:

$$\sum_i m_i n_i (\partial_t + \mathbf{v} \nabla) \mathbf{v} = - \sum_i \nabla p_i. \quad (19)$$

Equation of state:

$$\varepsilon = \kappa_{HRG}(T)p, \quad (20)$$

$$\lim_{T \rightarrow T_f} \kappa_{HRG}(T) = 3/2 \quad (21)$$

Diff. equation of temperature [3]:

$$\left[\frac{d}{dT} \kappa T \right] (\partial_t + \mathbf{v} \nabla) T + T \nabla \mathbf{v} = 0. \quad (22)$$

III. EQUATION OF STATE

3 classes of solutions:

- ▶ $T(t, \mathbf{r}) = T(t)$
- ▶ $\kappa = \text{const.}$
- ▶ $\frac{d}{dT}(\kappa T) = \text{const.}$ (new!)

Differential equations for κ :

For sQGP phase:

$$\frac{d}{dT} \left[\frac{T\kappa(T)}{1 + \kappa(T)} \right] = \frac{\kappa_Q}{1 + \kappa(T)} \quad (23)$$

For hadron gas phase:

$$\frac{d}{dT} [T\kappa(T)] = \frac{\kappa_c T_c - \kappa_f T_f}{T_c - T_f} \quad (24)$$

III. EQUATION OF STATE

Solutions:

For sQGP phase:

$$\kappa_{QM}(T) = \frac{\kappa_Q \left(\frac{T}{T_c}\right)^{1+\kappa_Q} + \frac{\kappa_c - \kappa_Q}{\kappa_c + 1}}{\left(\frac{T}{T_c}\right)^{1+\kappa_Q} - \frac{\kappa_c - \kappa_Q}{\kappa_c + 1}}, \quad (25)$$

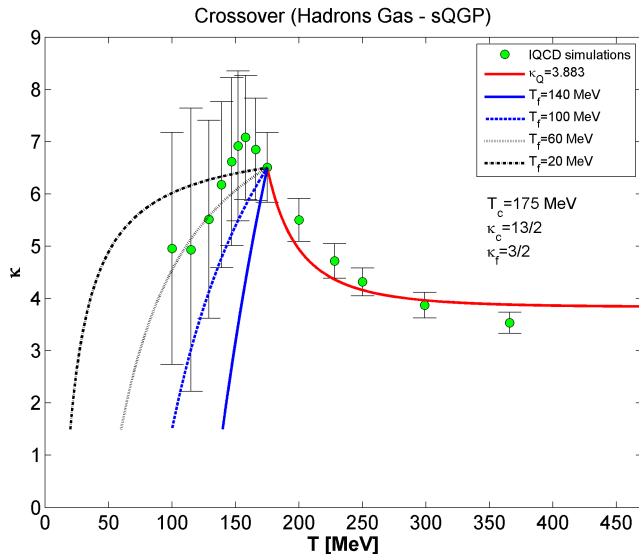
For hadron gas phase:

$$\kappa_{HM}(T) = \frac{\kappa_c T_c - \kappa_f T_f}{T_c - T_f} - \frac{\kappa_c - \kappa_f}{T_c - T_f} \frac{T_c T_f}{T}, \quad (26)$$

where

$$\kappa_f = 3/2. \quad (27)$$

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<i>Curves</i>	χ^2/NDF	CL [%]
$\kappa_Q = 3.833$	6.48/4	16.6
$T_f = 140 \text{ MeV}$	86.56/6	$1.6 \cdot 10^{-14}$
$T_f = 100 \text{ MeV}$	7.71/6	26.0
$T_f = 60 \text{ MeV}$	1.35/6	96.9
$T_f = 20 \text{ MeV}$	1.22/6	97.6

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ANSATZ

We are looking for a solution, which allows us to use the same scaling for each component of the hadron gas, therefore the gas expands collectively.

$$\{X_i, Y_i, Z_i\} = \{X, Y, Z\}, \quad \forall i. \quad (32)$$

Ideal gas approximation:

$$p = \sum_i p_i = T \sum_i n_i, \quad (33)$$

replace it to the Euler-equation:

$$\sum_i m_i n_i (\partial_t + \mathbf{v} \nabla) \mathbf{v} = -T \sum_i \nabla n_i. \quad (34)$$

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Multi-component solution

The expression of entropy density [3]:

$$\sigma(\mathbf{r}, t) = \sigma_r \frac{V_r}{V} e^{-s/2} = \frac{\sigma_r}{n_{i,r}} n_i(\mathbf{r}, t) \quad (35)$$

Let's follow Landau's argument:

$$\frac{\sigma(\mathbf{r}, t)}{\sigma_r} = \frac{n_i(\mathbf{r}, t)}{n_{i,r}} \implies \sigma \sim \sigma_r \quad (36)$$

$$n_i(\mathbf{r}, t) = n_{i,r} \frac{V_r}{V} e^{-s/2} = n_{i,r} \left(\frac{X_r Y_r Z_r}{XYZ} \right) e^{-s/2} \quad (37)$$

where

$$s = \frac{r_x^2}{X^2} + \frac{r_y^2}{Y^2} + \frac{r_z^2}{Z^2}. \quad (38)$$

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The velocity field without and with rotation:

$$v_x = \frac{\dot{X}(t)}{X(t)} r_x, \quad v_y = \frac{\dot{Y}(t)}{Y(t)} r_y, \quad v_z = \frac{\dot{Z}(t)}{Z(t)} r_z, \quad (39)$$

$$v_x = \frac{\dot{R}(t)}{R(t)} r_x - \omega r_y, \quad v_y = \frac{\dot{R}(t)}{R(t)} r_y + \omega r_x, \quad v_z = \frac{\dot{Z}(t)}{Z(t)} r_z. \quad (40)$$

In the rotational case we use $X(t) = Y(t) = R(t)$ symmetry, and

$$\omega = \omega_0 (R_0/R)^2. \quad (41)$$

The temperature profile has spatial homogeneity:

$$T_A = T(t),$$

$$T_r = T_A(t_r) = T_B(t_r) \approx T_c \approx 175 \text{ MeV}.$$

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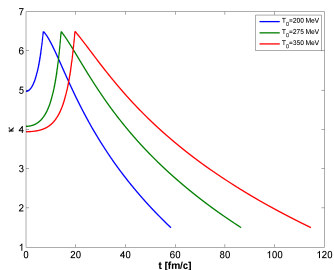
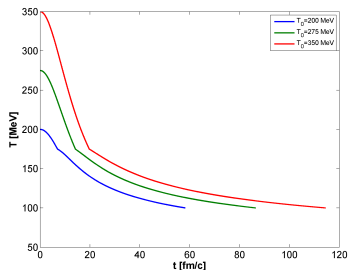
Time dependence

$$R_0 = Z_0 = 5 \text{ fm}$$

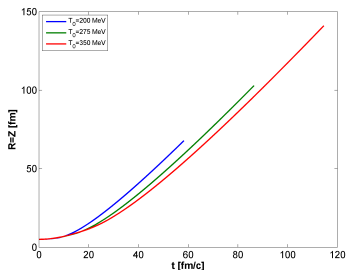
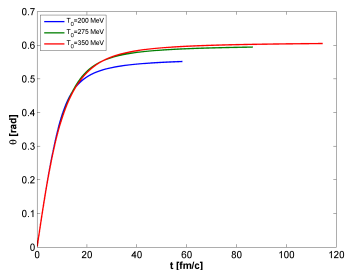
$$\dot{R}_0 = \dot{Z}_0 = 0$$

$$\theta_0 = 0, \quad \omega_0 = 0.05 \text{ c/fm}$$

$$T_f = 100 \text{ MeV}, \quad \langle m \rangle = 280 \text{ MeV}$$



IV. CROSSOVER



At the chemical freezeout temperature:

$$\frac{1}{1 + \kappa_c} < \frac{T_c}{\langle m \rangle} \quad (43)$$

The medium has a second "explosion", that starts just after the conversion to the hadron gas!

CONCLUSION

Non-relativistic approximation breaks down when \dot{R} and \dot{Z} becomes too large, search for relativistic generalization started!

V. OBSERVABLES

Inverse slope	Single-component	Multi-component
Without rot.[4]	$T_x = T_f + m\dot{X}_f^2$ $T_y = T_f + m\dot{Y}_f^2$ $T_z = T_f + m\dot{Z}_f^2$	$T_{x,i} = T_f + m_i\dot{X}_f^2$ $T_{y,i} = T_f + m_i\dot{Y}_f^2$ $T_{z,i} = T_f + m_i\dot{Z}_f^2$
With rot. [5]	$T_x = T_f + m(\dot{R}_f^2 + \omega_f^2 R_f^2)$ $T_y = T_f + m(\dot{R}_f^2 + \omega_f^2 R_f^2)$ $T_z = T_f + m\dot{Z}_f^2$	$T_{x,i} = T_f + m_i(\dot{R}_f^2 + \omega_f^2 R_f^2)$ $T_{y,i} = T_f + m_i(\dot{R}_f^2 + \omega_f^2 R_f^2)$ $T_{z,i} = T_f + m_i\dot{Z}_f^2$

Simple method:

$$m \rightarrow m_i$$

$$T_j \rightarrow T_{j,i}$$

Linear m_i dependence:

$$T_{j,i} = k_1 \cdot m_i + k_2 \quad (44)$$

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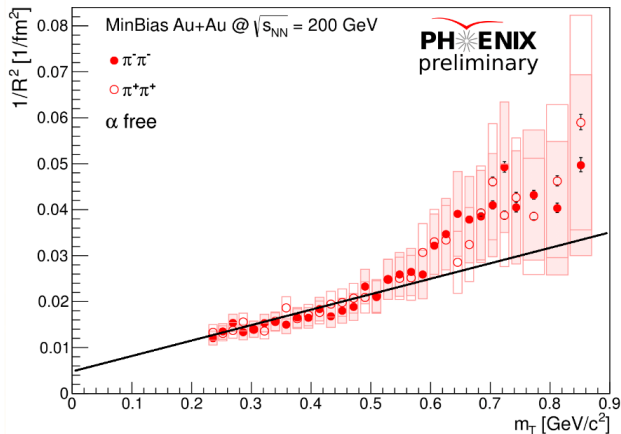
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$$R_{j,i}^{-2} = c_1 \cdot m_i + c_2 \quad (47)$$

VI. SUMMARY

- ▶ Rehadronization: crossover \implies simple boundary conditions
- ▶ Take into consideration the multi-component scenario
- ▶ Introduce scales independently from the type of particles
- ▶ Gain a similar dynamical equation to the one-component case
- ▶ The multi-component scenario does not complicate the description
- ▶ Difference: mean mass weighted by the number of particles
- ▶ The hadron gas has an exploding dynamics
- ▶ We need the relativistic formalism
- ▶ $\theta_f(T_0)$ is on progress
- ▶ Inverse slope parameters: $T \longrightarrow T_i$
- ▶ HBT-radii: $R \longrightarrow R_i$

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- [1] PHENIX Collaboration: *arXiv:nucl-ex/0307022*
- [2] Sz. Borsányi, G. Endrődi et al.: *arXiv:1007.2580*
- [3] T. Csörgő, M.I. Nagy: *arXiv:1309.4390*
- [4] T. Csörgő, S.V. Akkelin et al.: *arXiv:hep-ph/0108067v4*
- [5] T. Csörgő, M.I. Nagy, I.F. Barna: *arXiv:1511.02593v1*
- [6] D. Kincses: *talk at CPOD 2016*

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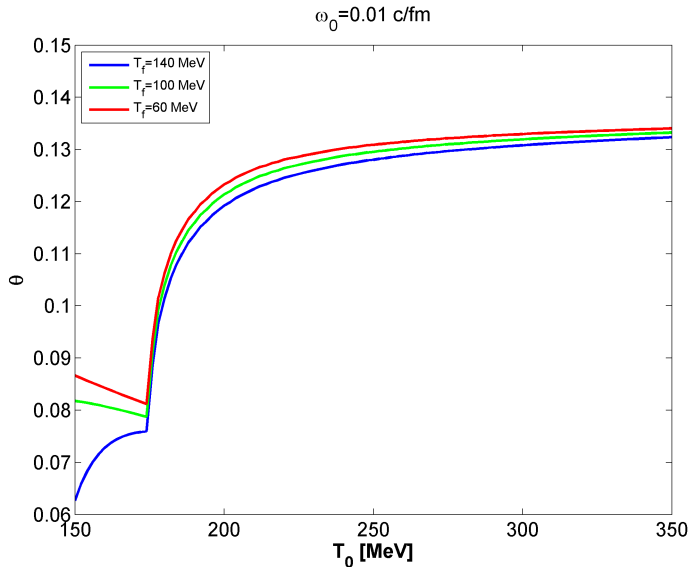
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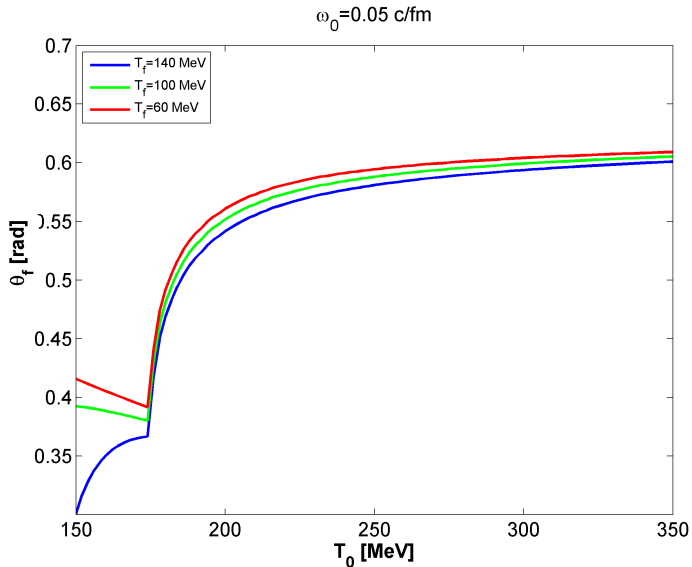
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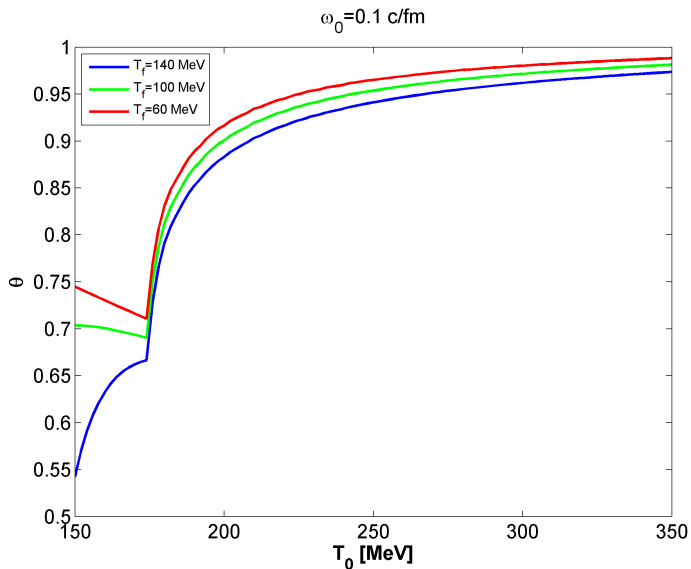
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