



Magnets for SPS +

Fast Ramping Design Issues moving towards a design.

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thanks to
Arjan Verweij,
Bernhard Auchmann,
Amalia Ballarino
Peter Limon
&
Nuria Catalan Lasheras



What's coming up

- ◆ GSI & possible PS & SPS upgrades.
- ◆ Strand & Cable designs.
- ◆ Changing aperture its affect on losses.
- ◆ 1 or 2 layer design.
- ◆ Temperature change during cycles.
- ◆ Longer magnet heat less / use less superconductor .
- ◆ How to get the heat out, some ideas (lots of questions).
- ◆ Warm or cold Iron hysteresis losses.
- ◆ Eddy currents in wedges select materials.
- ◆ Fatigue and some history.
- ◆ How long could it take.
- ◆ Things to do!
- ◆ Conclusions.

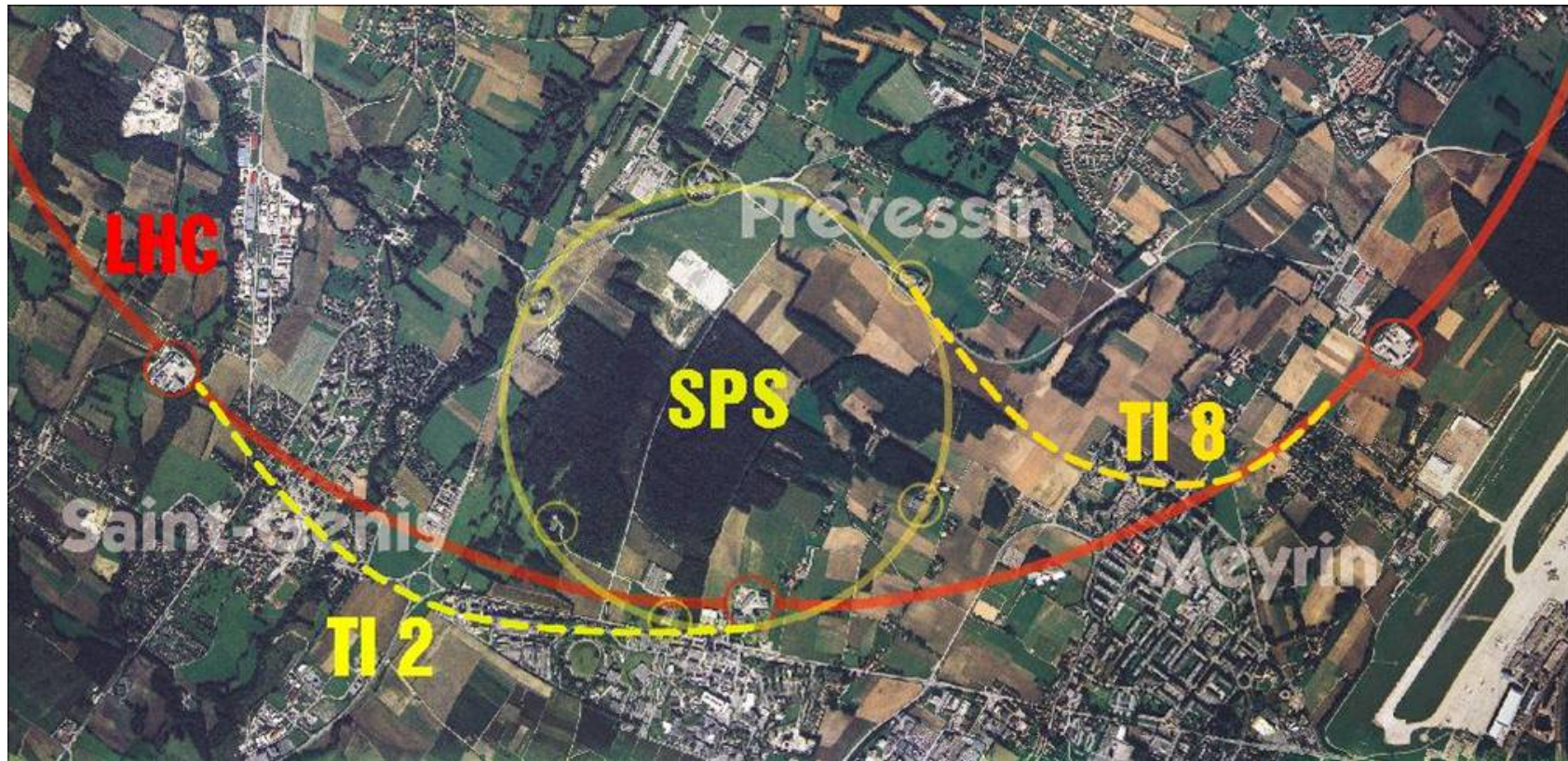


Magnet spec's for GSI & LHC possible upgrade.

	SIS 100	PS II	SIS 300	SPS II
◆ Peak field	2T	3T	6	4.5
◆ dB/dT [T/s]	4	3.5	1	1.5
◆ Cycles (20 years)	200M	60M	1 M	1 M
◆ Rad. load [W/m]	1	10	1	10
◆ Peak load [W/m]	3	30	3	30
◆ Magnet length [m]	2.9	4	2.9	6
◆ No. of dipoles	108	100	108	750

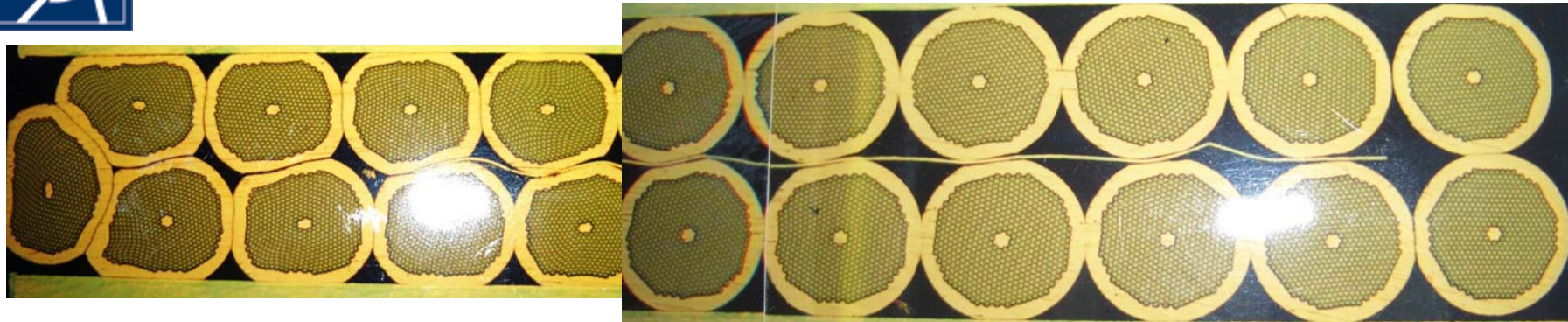


LHC INJECTION LINES : 5.6 km, about 700 to 750 Magnet's



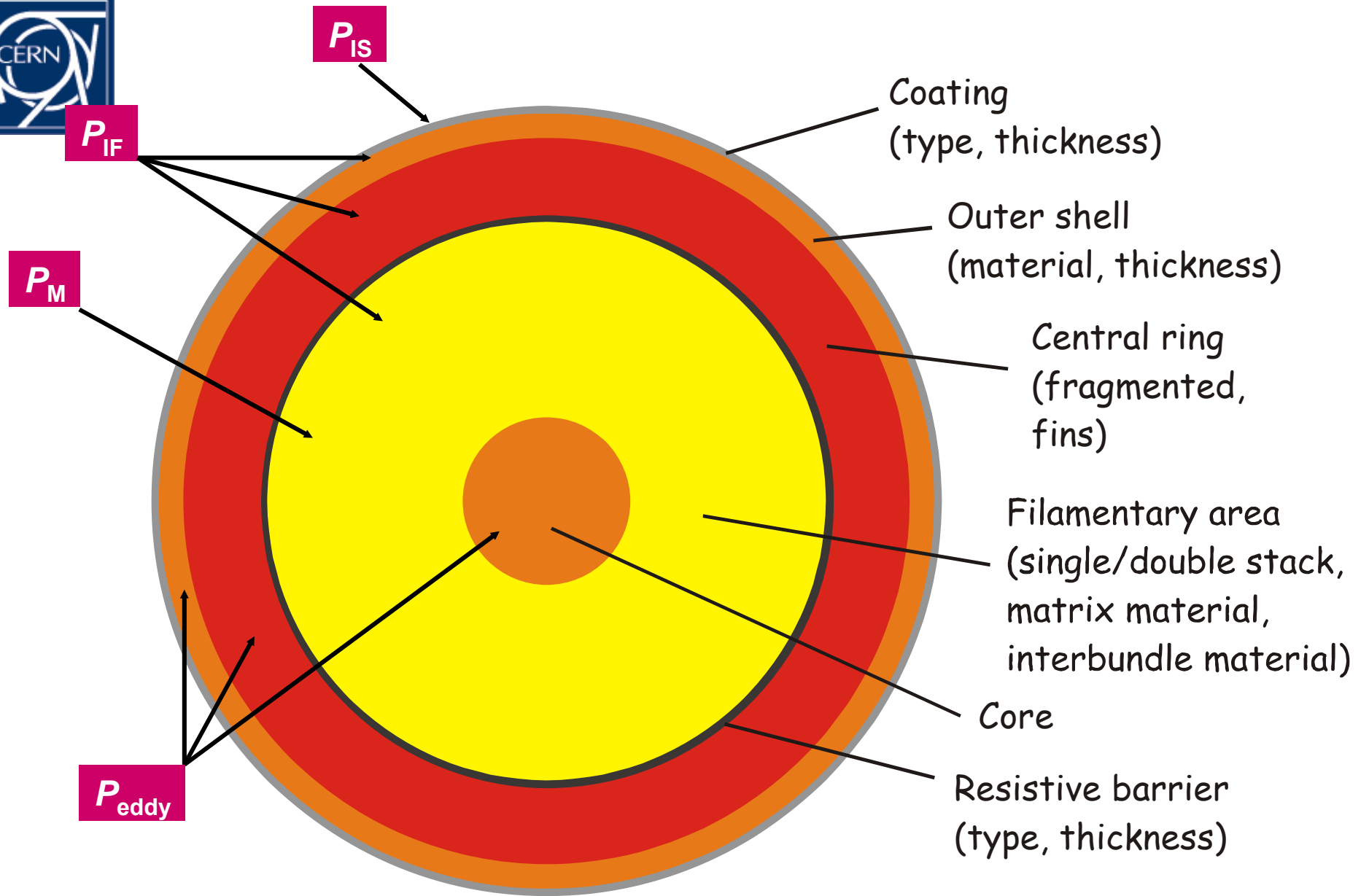


Cable design



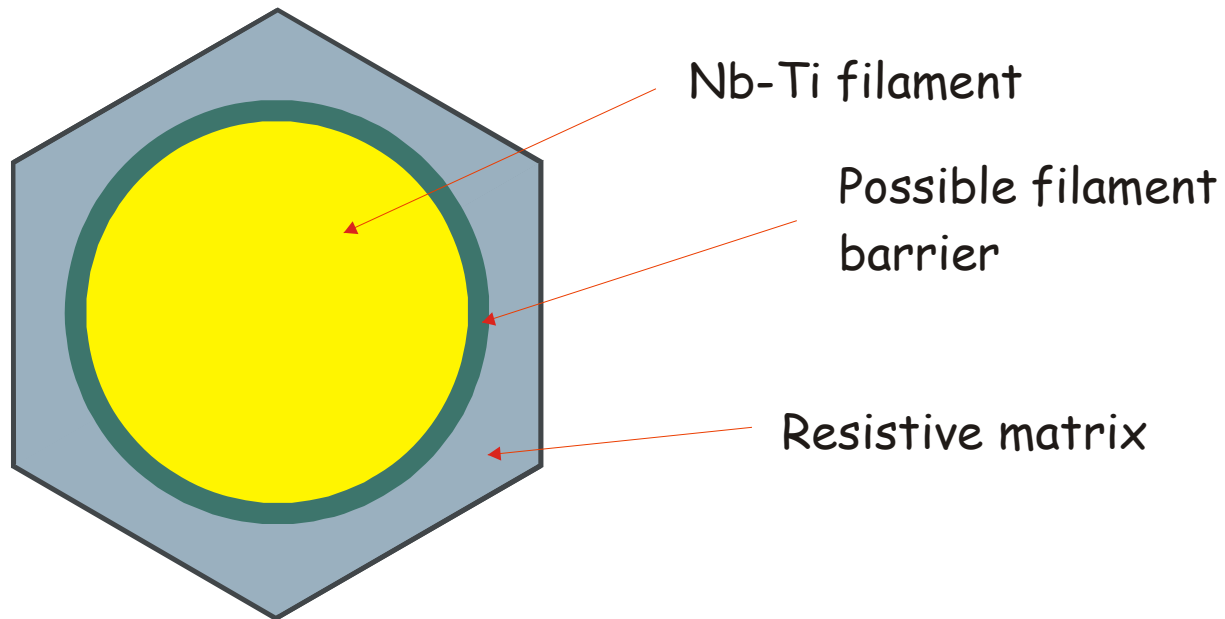
- ◆ Cable width : 10mm to 20mm wide
- ◆ Up to 40 Small strands: 0.5, to 1.0 mm diameter
- ◆ Filaments in resistive matrix, with Fragmented Copper core and band for protection
- ◆ Small filaments : 3 μm or 1 μm
- ◆ filament twist pitch: 6 x strand diameter.
- ◆ Cable twist pitch : 7 x cable width.
- ◆ Cable thin edge compaction: 0.78 max (but don't do it)
- ◆ Cable fat edge compaction : 0.95 min
- ◆ Foil through center of cable to control R_c
- ◆ Coating on strand to control R_a





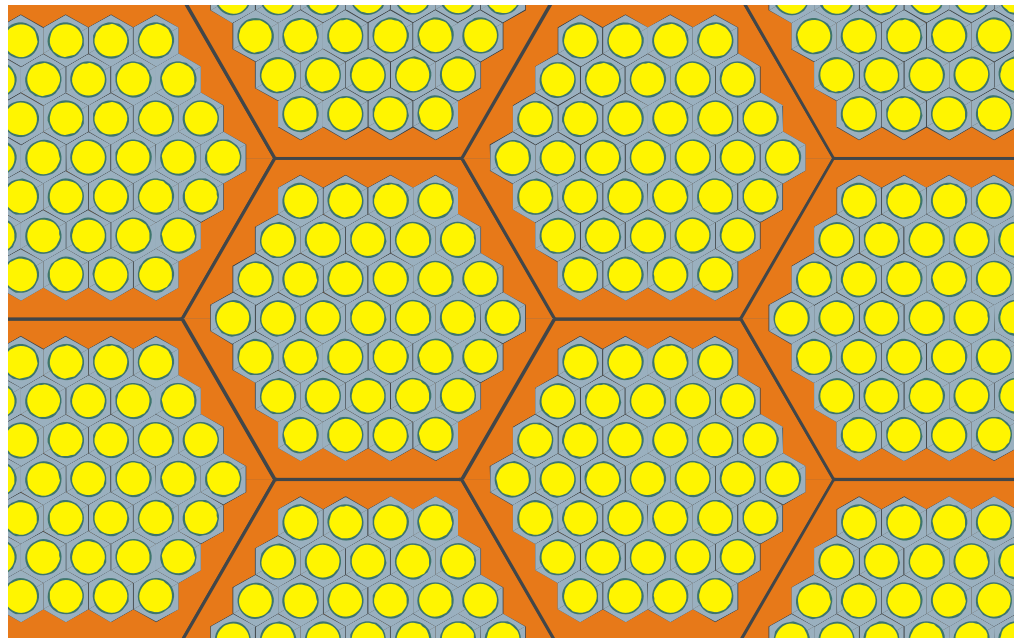


Small filaments : 3 μm or 1 μm





Filamentbundles with interbundle Cu





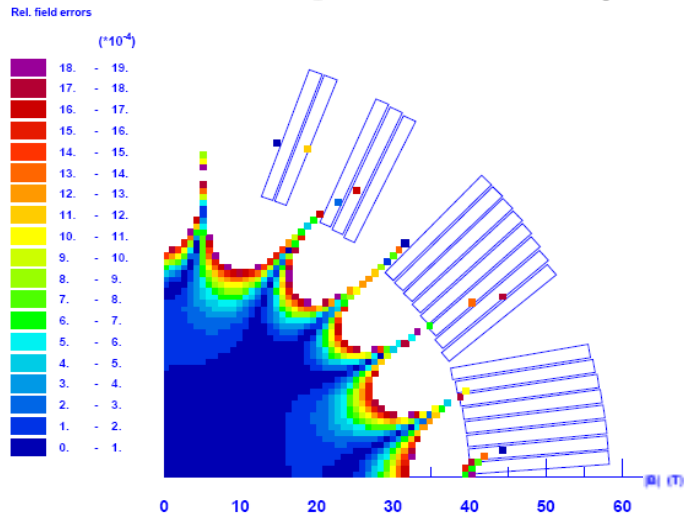
Fragmented central ring
(Cu hexagons with resistive barriers)



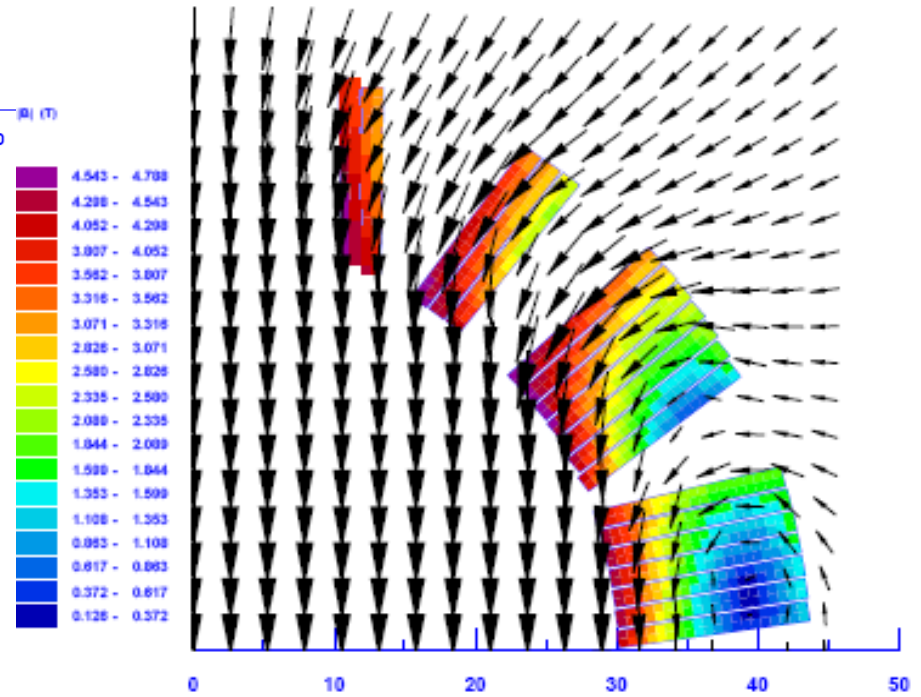
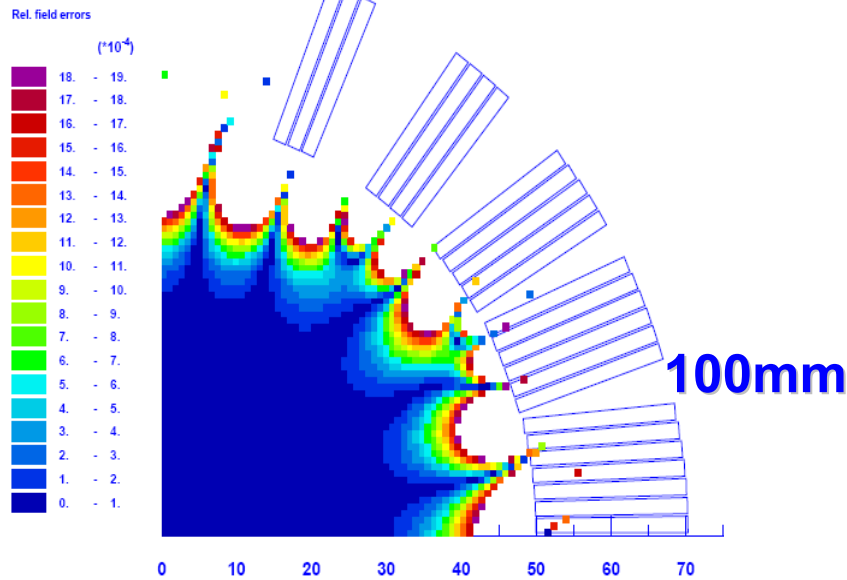
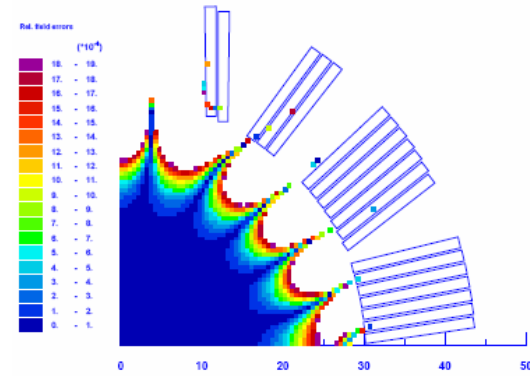


Magnet aperture

80mm

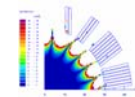
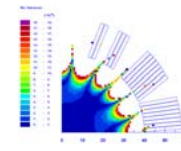
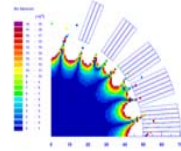
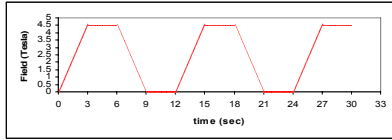


60 mm





Losses for the 100, 80 & 60mm



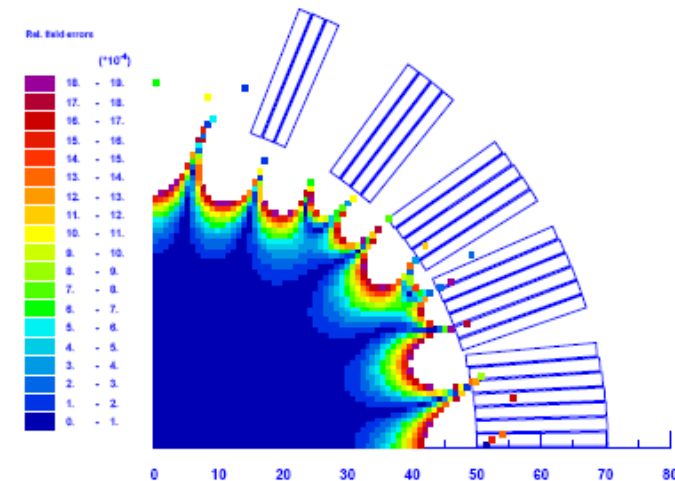
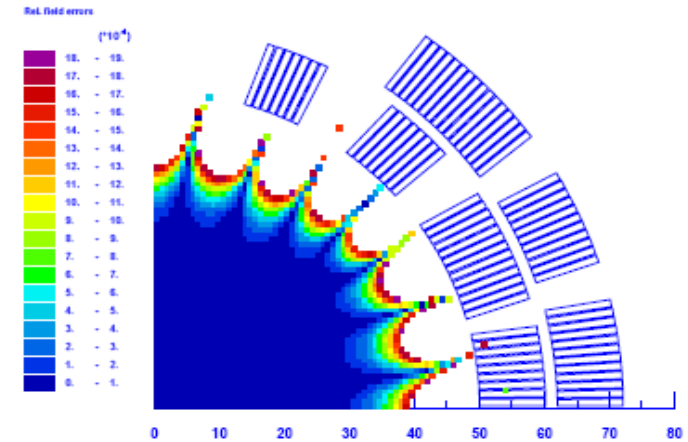
Design name		100 1layer		80 1 Layer		60 1 Layer
Number of layers	-	1		1		1
Strand diameter	mm	0.9		0.9		0.67
Current at central field	A	12414		11898		10374
Inductance	mH/m	1.602		1.1299		0.8477
Stored energy at operating current	kJ/m	123		80		46
Ramp voltage for a magnet of 6 m	V	40		27		18
Matrix		Cu	CuNi + frag	Cu	CuNi	Cu
Ra to keep P_IS_a=1 W/m	uOhm	120	120	64	64	21
Rc to keep P_IS_c=1 W/m	uOhm	9500	9500	4900	4900	1600
Average loss during field sweep in W/m						
P_M	W/m	4.79	4.79	3.85	3.85	1.93
P_IF	W/m	6.73	0.61	5.46	1.93	1.49
P_eddy	W/m	0.25	0.25	0.58	0.58	0.16
P_IS_a	W/m	1	1	1	1	1
P_IS_c	W/m	1	1	1	1	1
TOTAL	W/m	13.77	7.65	11.89	8.36	5.58
TOTAL, averaged over 1 cycle (TARGET: 5)	W/m	6.885	3.825	5.945	4.18	2.79
dT_ramp	K	1.84	0.95	1.72	0.87	1.05
P_iron, averaged over 1 cycle	W/m	2.83	2.83	1.72	1.72	1.02



1 or 2 Layer coil design?

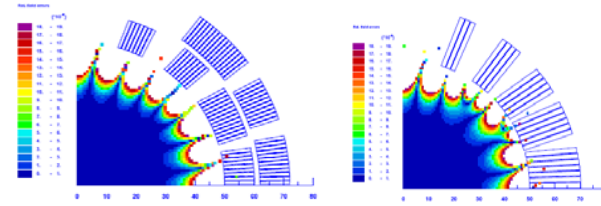
4.5 T magnets, cycling time of 12 sec

Design name		2 layer 100mm	1 layer 100mm
Bore diameter	mm	100	100
Strand diameter	mm	0.5	0.9
Number of Filament	-	11,111	36,000
Number of strands in the cable	-	40	40
Cable width	mm	10.19	18.31
Central field	T	4.5	4.5
Current at central field	A	3,879	12,414
Operating temperature	K	4.8	4.8
Inner radius yoke	mm	110	110
Outer radius yoke	mm	260	260
Inductance	mH/m	17.38	1.602
Stored energy at operating current	kJ/m	131	123
Ramp voltage for a magnet of 6 m	V	135	40





1 or 2 Layer coil design, losses

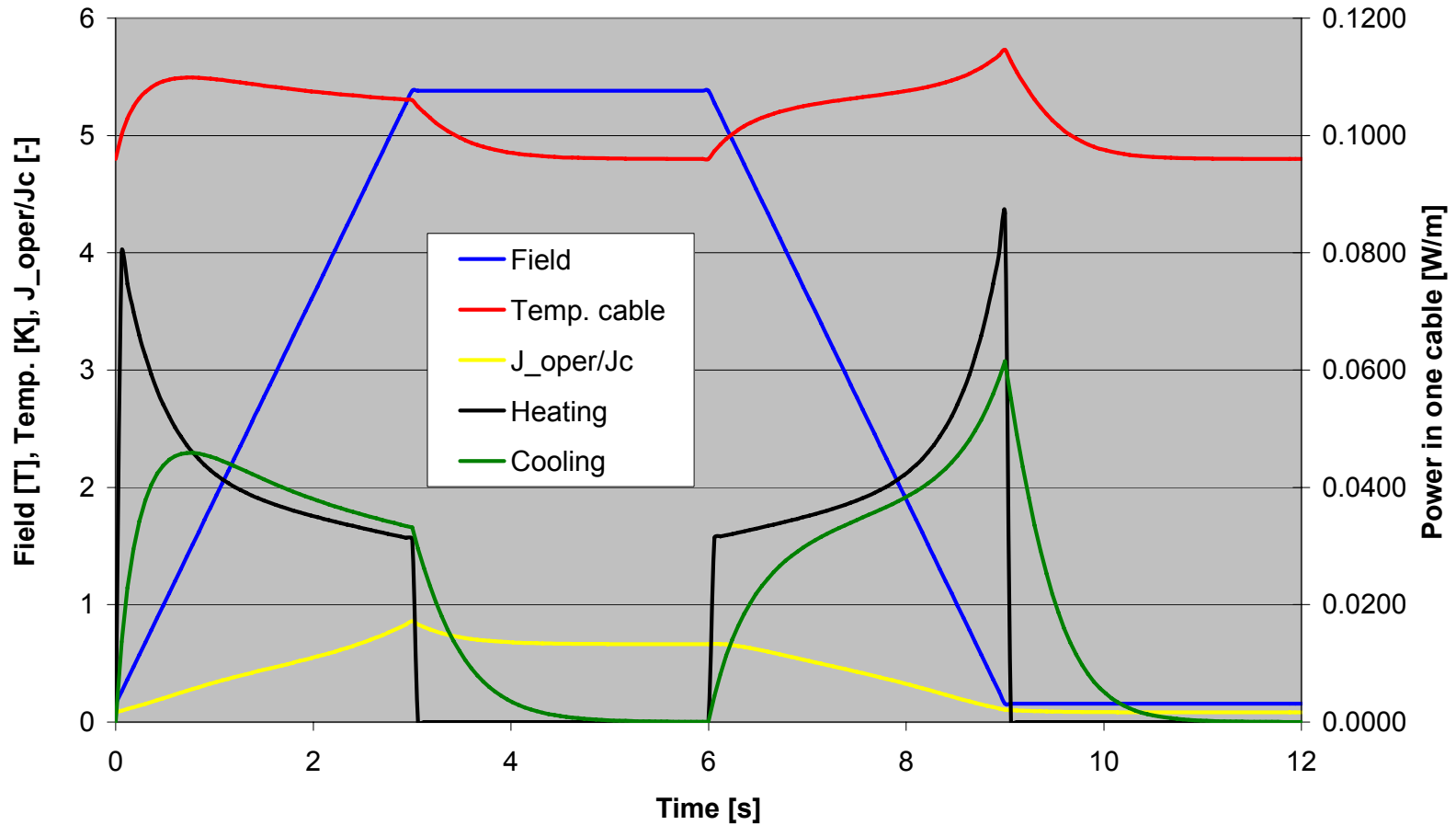


Loss parameters used		2 layer 100mm ap	1 layer 100mm ap	
Filament diameter	um	3	3	3
Matrix		Cu	Cu	CuNi
Central ring		Cu	Cu	Fragm. Cu
Ra * 1 mm ²	uOhm*mm ²	50	50	50
Rc * 1 mm ²	uOhm*mm ²	5000	5000	5000
Ra	uOhm	110	34	34
Rc	uOhm	11000	3400	3400
Jc at 4.2K, 5T	A/mm ²	2600	2600	2600
Average loss during field sweep in W/m		2 layer 100mm	1 layer 100mm	
P_M	W/m	4.68	4.79	4.79
P_IF	W/m	2.08	6.73	0.61
P_eddy	W/m	0.23	0.25	0.25
P_IS_a	W/m	1.25	3.56	3.56
P_IS_c	W/m	0.99	2.78	2.78
TOTAL	W/m	9.23	18.11	11.99
TOTAL, averaged over 1 cycle (TARGET: 5)	W/m	4.615	9.055	5.995
dT_ramp	K	0.39	2.05	0.82
J_oper/J_c at Bpeak, T=Tbath	%	60	59	59
J_oper/J_c at Bpeak, T=Tbath+dT_ramp	%	73	>100	92
P_iron, averaged over 1 cycle	W/m	2.83	2.83	2.83
J_Cu_Quench (TARGET: <=1200)	A/mm ²	827	815	1190



Temperature fluctuation during operation of 80mm 2 layer design

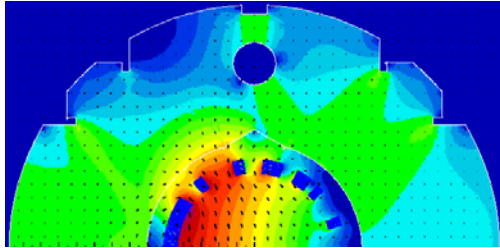
3 um fil, Cu matrix, Ra=140 uOhm, Rc=11 mOhm



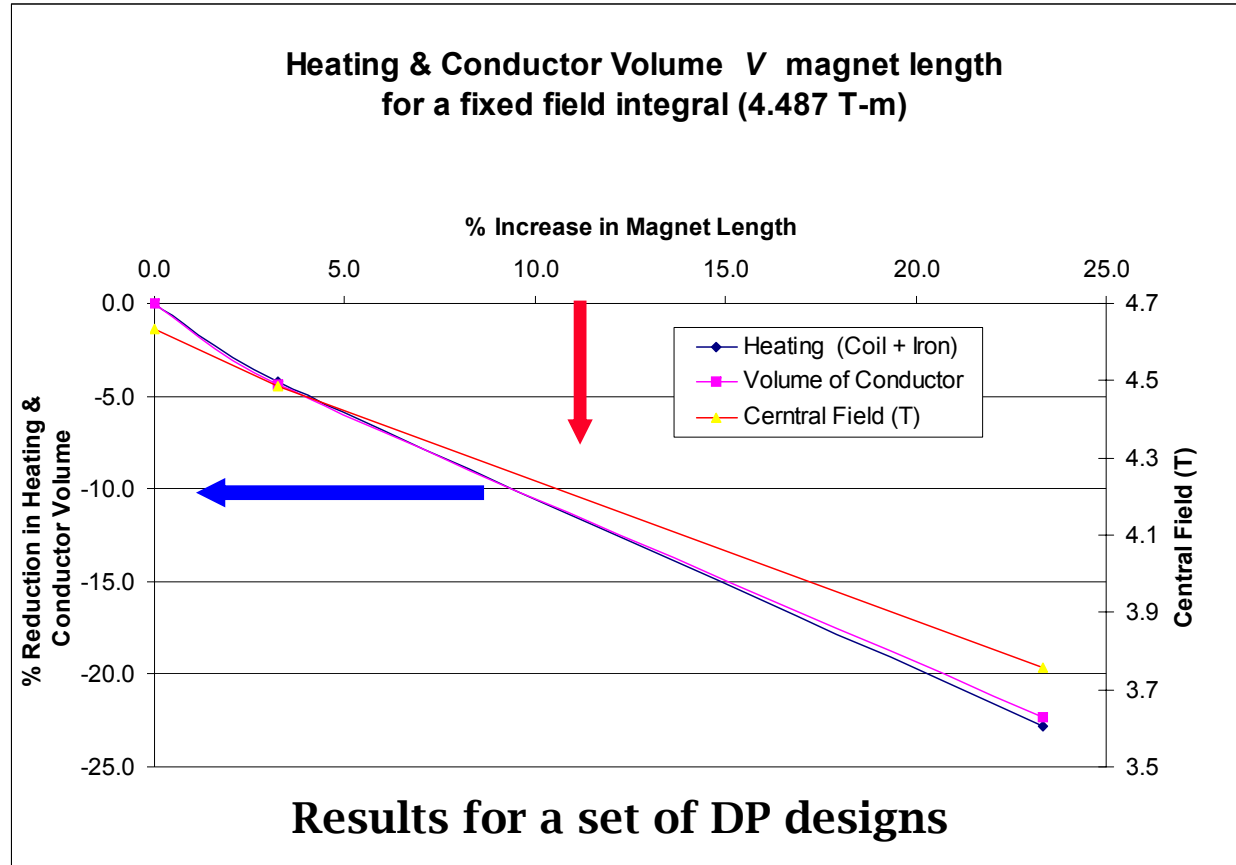


CFM?

Longer Magnet Generate Less Heat and use Less Superconductor!



Combining the Quad into the DP the effective length on the DP could be as much as 11% longer including a 5% quad corrector Without using up any more space than is currently occupied.

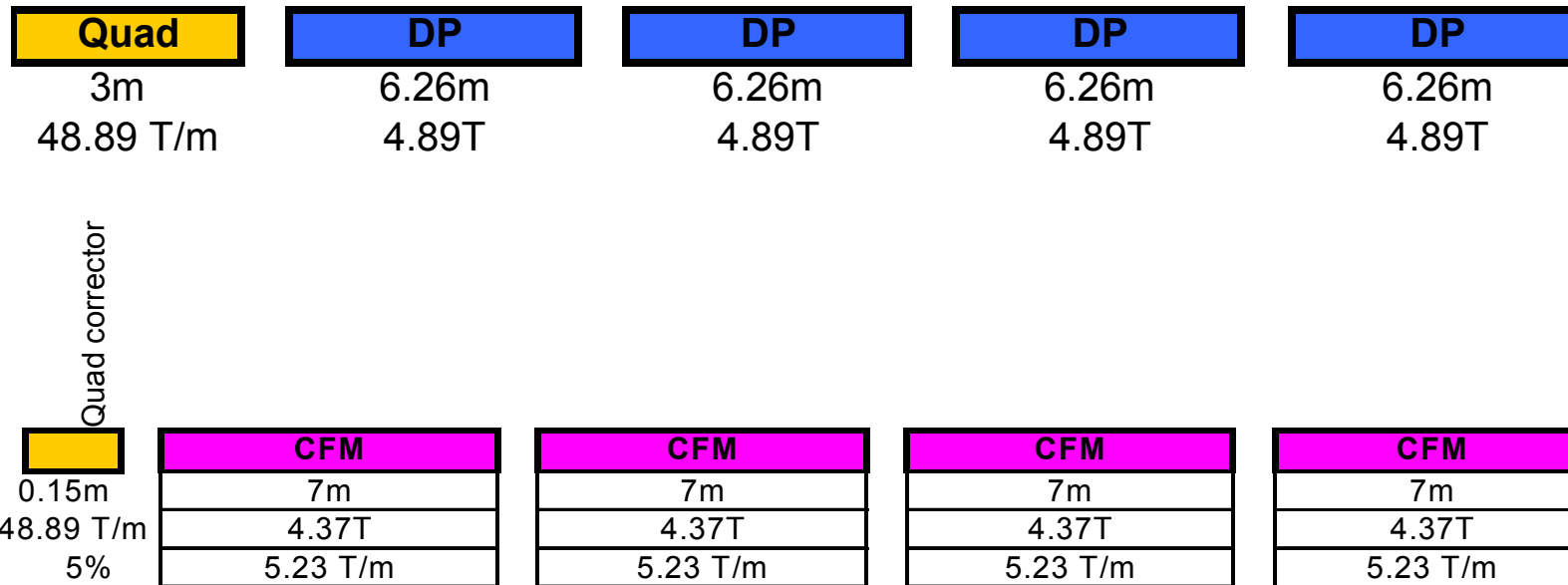


But,But,But! Field quality of CFM, tune in SPS, Scaling is correct for DP but not yet studied for CFM.



CFM

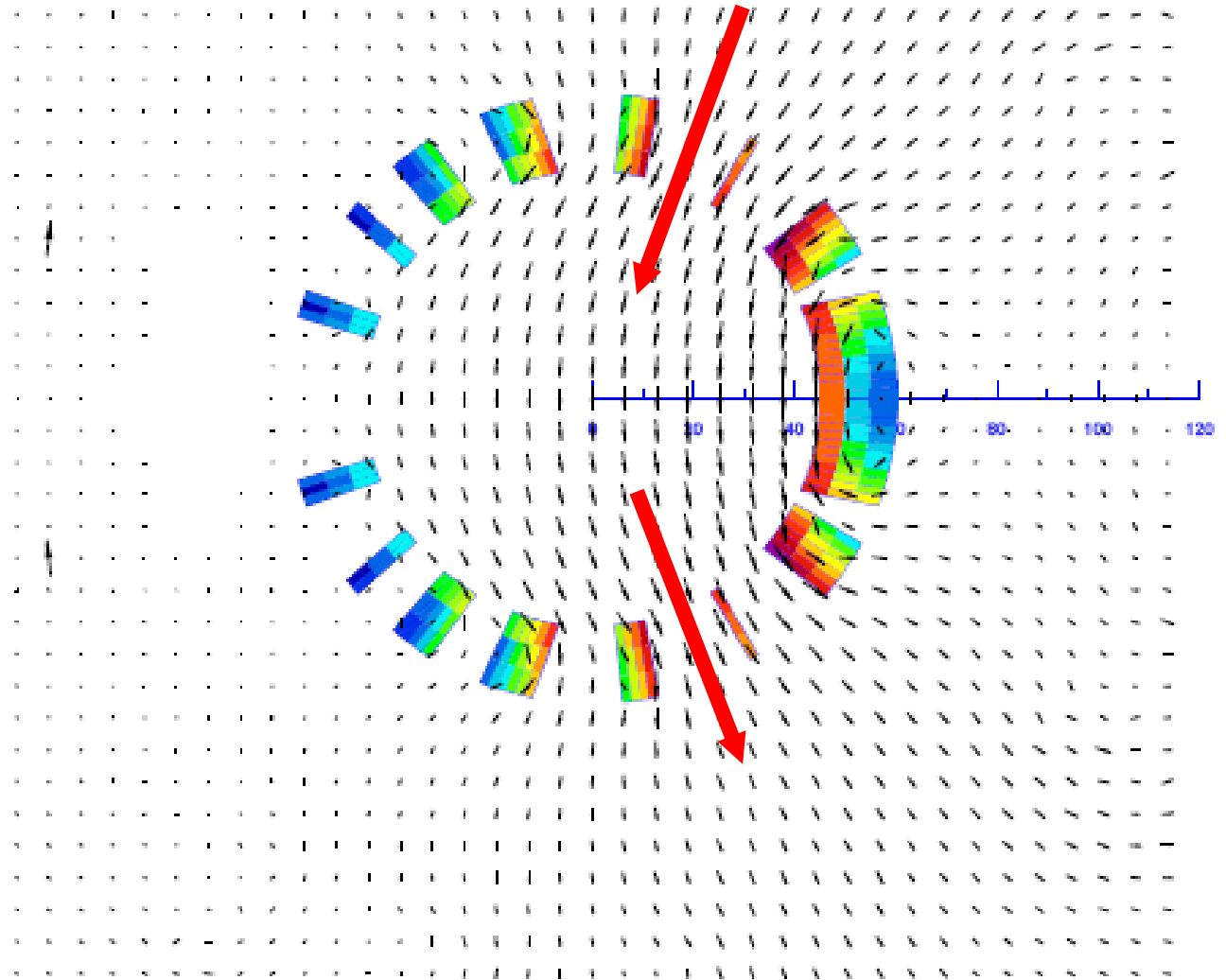
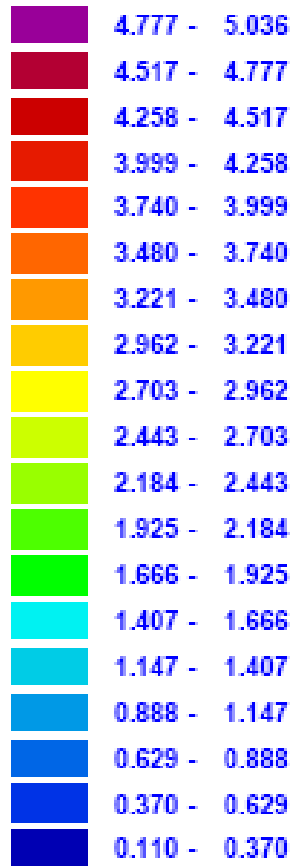
SPS + half cell at 1 Tev





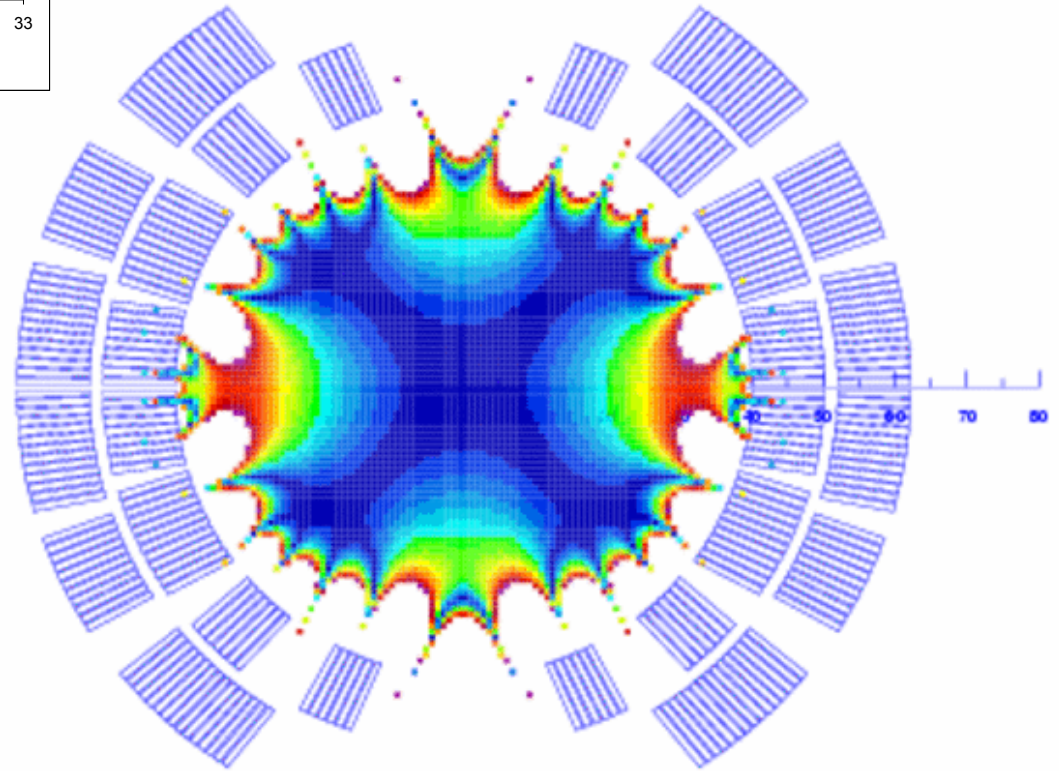
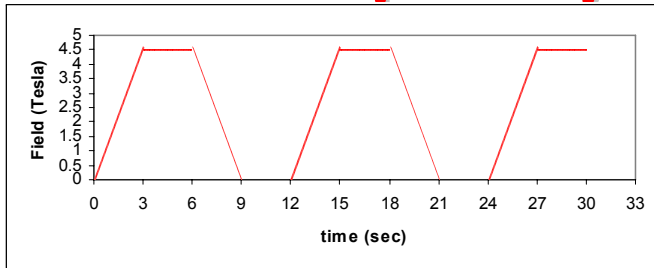
CFM

$|B|$ (T)





Field quality during ramping



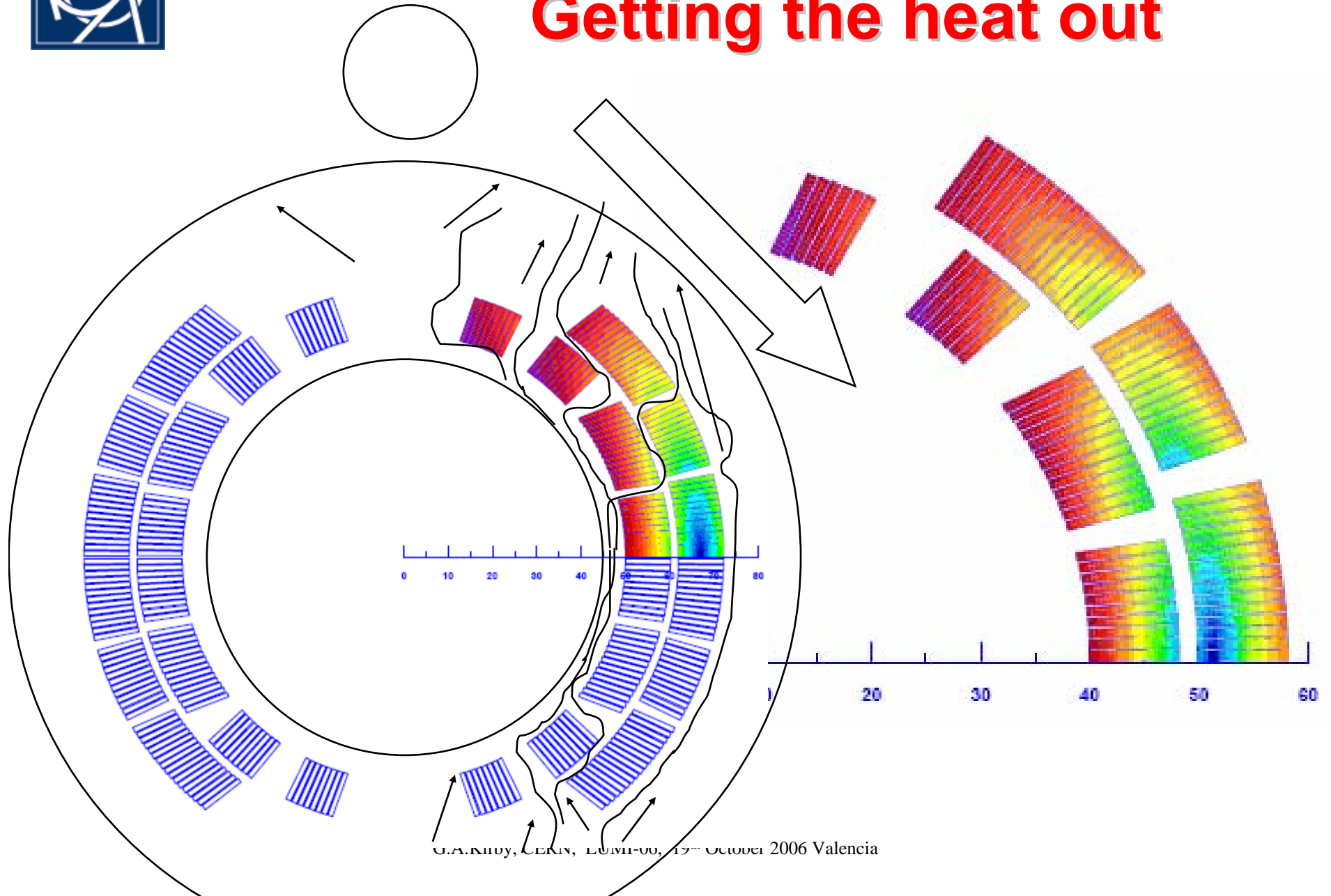


Comparison of cooling modes

- ◆ Pool boiling (~ 1 W/m)
- ◆ Forced convection of superfluid helium (~ 1 W/m)
- ◆ Static pressurized He II LHC ($\sim 1-10$ W/m) < 2.2 K
 - LHC @ 1.9K has 10W/m with a temperature change of 0.1K so this could be a possible cooling mode.
 - However R_c & R_a are still not fixed and vary by orders of magnitude. If due to the very low C_p at 1.8k the temperature rise will be above 2.2K the system would fail.
 - More work is needed.
- ◆ **Forced convection of supercritical helium ($\sim 1-10$ W/m) 2.2K to 5K**
 - This cooling mode seems to be a safer option, but relies on pumping supercritical helium through channels in the magnet.
 - Easy to implement for low heat loads, Single phase Mass flows of $O(W/0.1 \text{ kg/s})$, High heat load possible at the expense of T-margin and high ΔP , Cross-flow construction needed for high heat loads.
- ◆ **Needs work to carefully check which mode works and the costs**



Getting the heat out

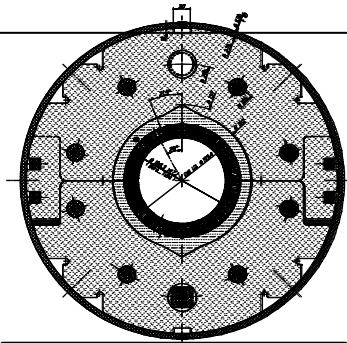




Getting the heat out

$$Q = \dot{M} \cdot C_p \cdot \Delta T_{Helium}$$

$$Buoyancy = V \cdot (\rho_{4.8K} - \rho_{4.5K}) \cdot g$$



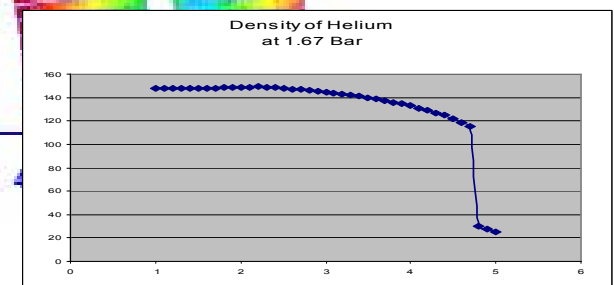
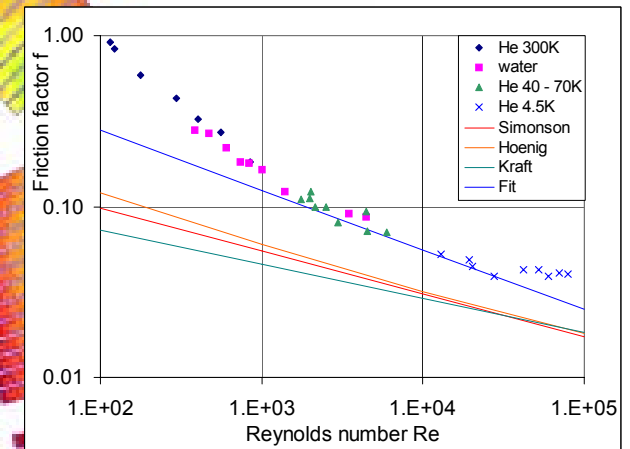
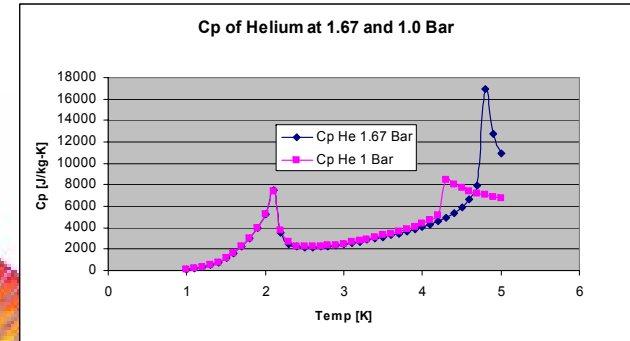
$$\dot{M} = A_h \sqrt{\frac{PD_h \rho}{2f}}$$

With 10 W/m we must move about 4 L/min of helium through the coil, with a bath temp 4.5K and T max 4.8K.

Natural convection
Thermosyphon effect
pushes the helium
through the coil to the
heat exchanger tube
with a driving pressure
of about 180 N/m²

If we assume 1 mm diameter cooling channels though the coil, we will need about 2500 channels per meter to extract the 10 W/m at 4.8K. This is a tube every 3mm or 33% open magnet structure.

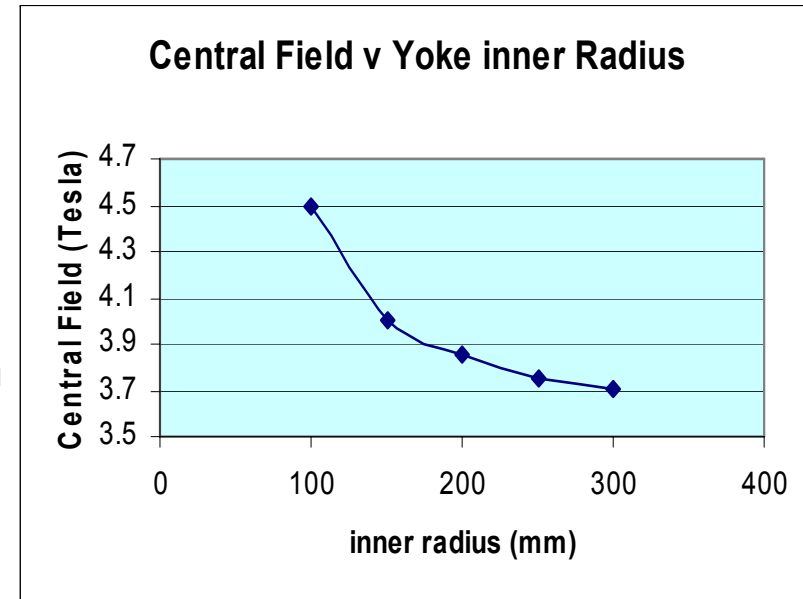
We don't have such channels in our LHC magnet, needs careful design and testing!!





Yoke, cold or warm

- ◆ At 1.5 T/s the hysteresis losses averaged over 1 cycle in the iron are between 1.02 W/m for the 60mm aperture up to 2.83 W/m for the 100mm aperture. So can we eliminate this heat load?
- ◆ A warm iron inner radius design
- ◆ Collars, support tube, cryostat cold-warm support = warm iron inner radius 200mm.
- ◆ We loose 0.8 Tesla central field in the 100mm aperture design.
- ◆ To replace this lost field and maintain the same short sample % we need to add about 20% extra superconductor.
- ◆ For this design what we gain with the iron losses we loose with the Superconductor losses and cost. Plus the Rc & Ra could make a bigger diff.



Cable losses only

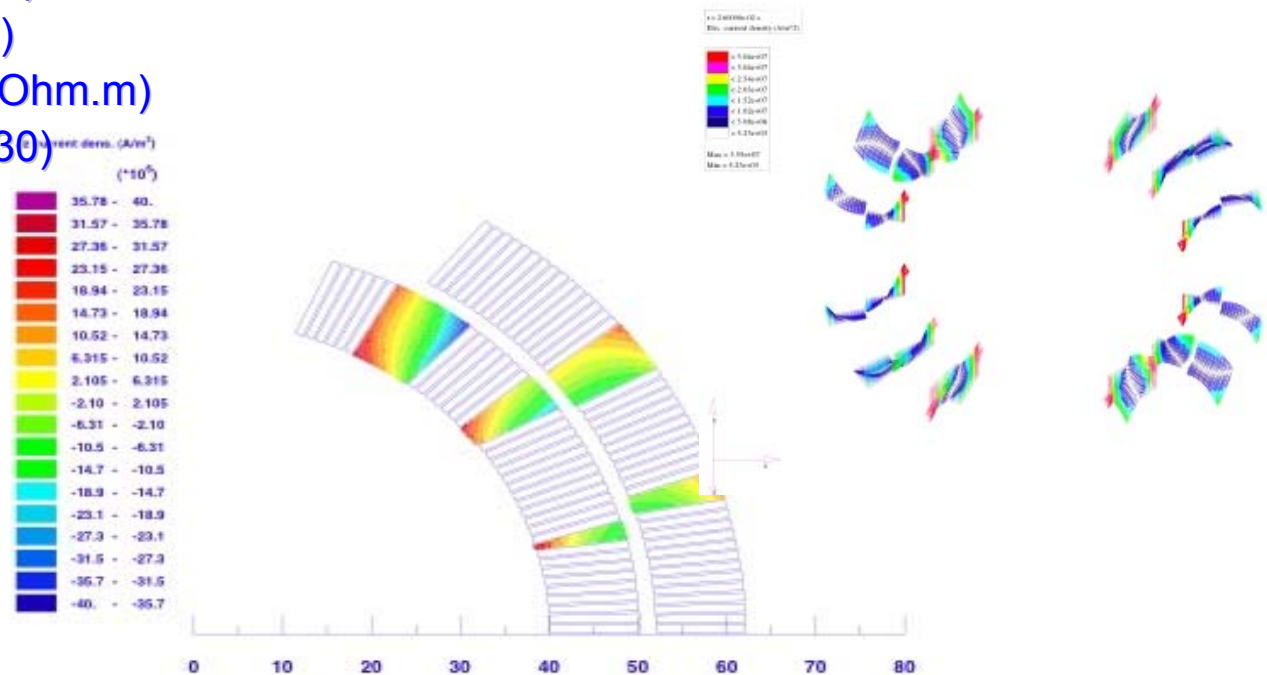
		Cold Iron	Warm Iron
P_M	W/m	4.68	5.62
P_IF	W/m	2.08	3.02
P_eddy	W/m	0.23	0.33
P_IS_a	W/m	1.25	1.81
P_IS_c	W/m	0.99	1.44
TOTAL	W/m	9.23	12.21

2.9



Wedges and eddy current effect on internal heating and field quality.

- ◆ calculated losses and impact on field quality for 3 materials
- ◆ copper with 1.7×10^{-10} (Ohm.m)
- ◆ bronze with 3.0×10^{-8} (Ohm.m)
- ◆ stainless steel with 5.0×10^{-7} (Ohm.m)
- ◆ GRP very big $e_{10} + (20 \text{ or } 30)$



- ◆ The losses
- ◆ copper: **22.03W/m**
- ◆ bronze: 0.1248W/m
- ◆ stainless steel: 7.49mW/m
- ◆ the **impact on field quality is not negligible for copper**. the eddy- current density is at about 1/10 of the transport current density in the cables -> delta b3 of about **2 units**. For the others materials there is no effect of eddy-currents on field quality.

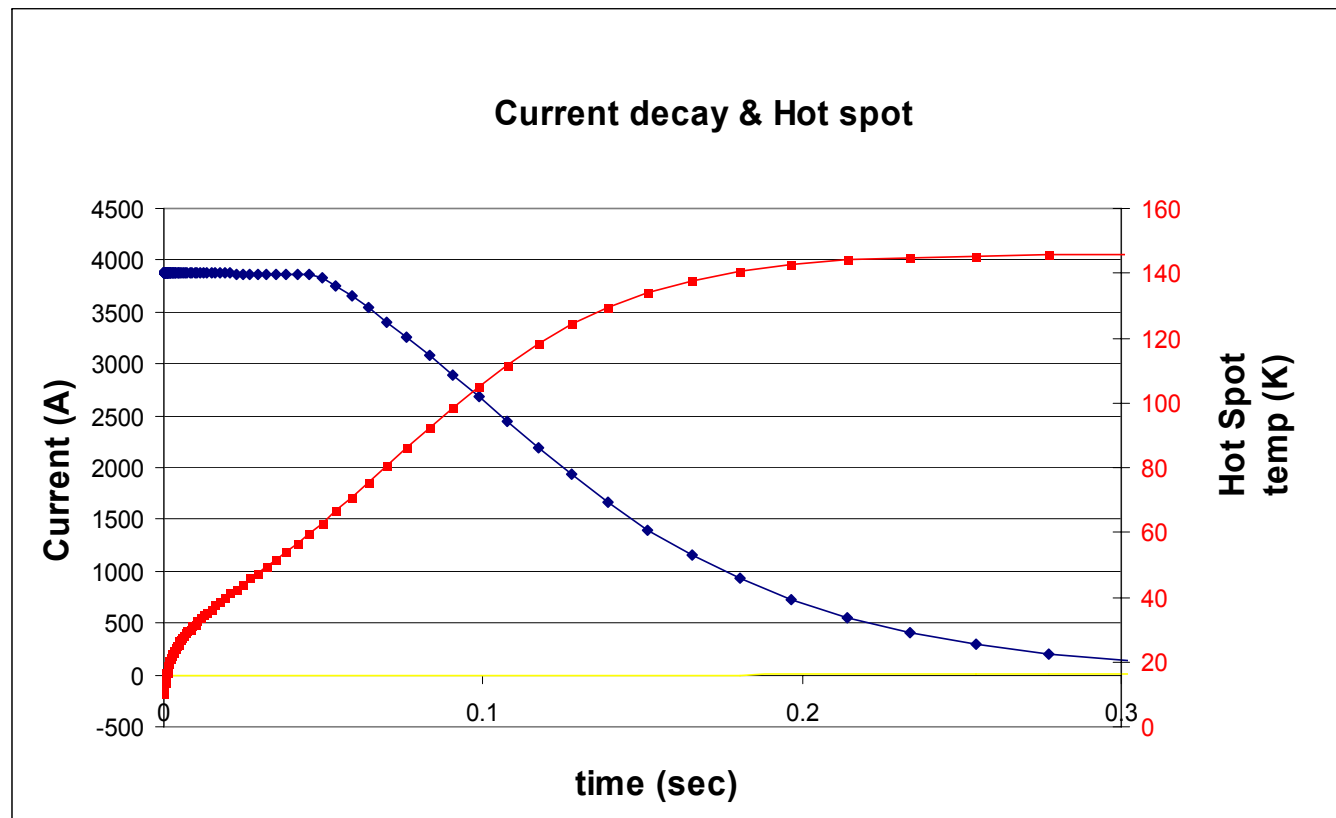
BEMFEM * ROXIE...



Quench simulation

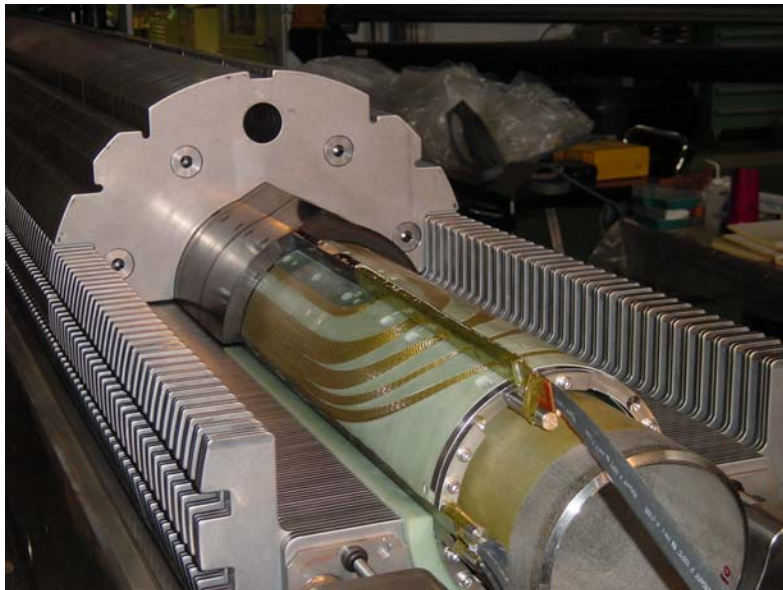
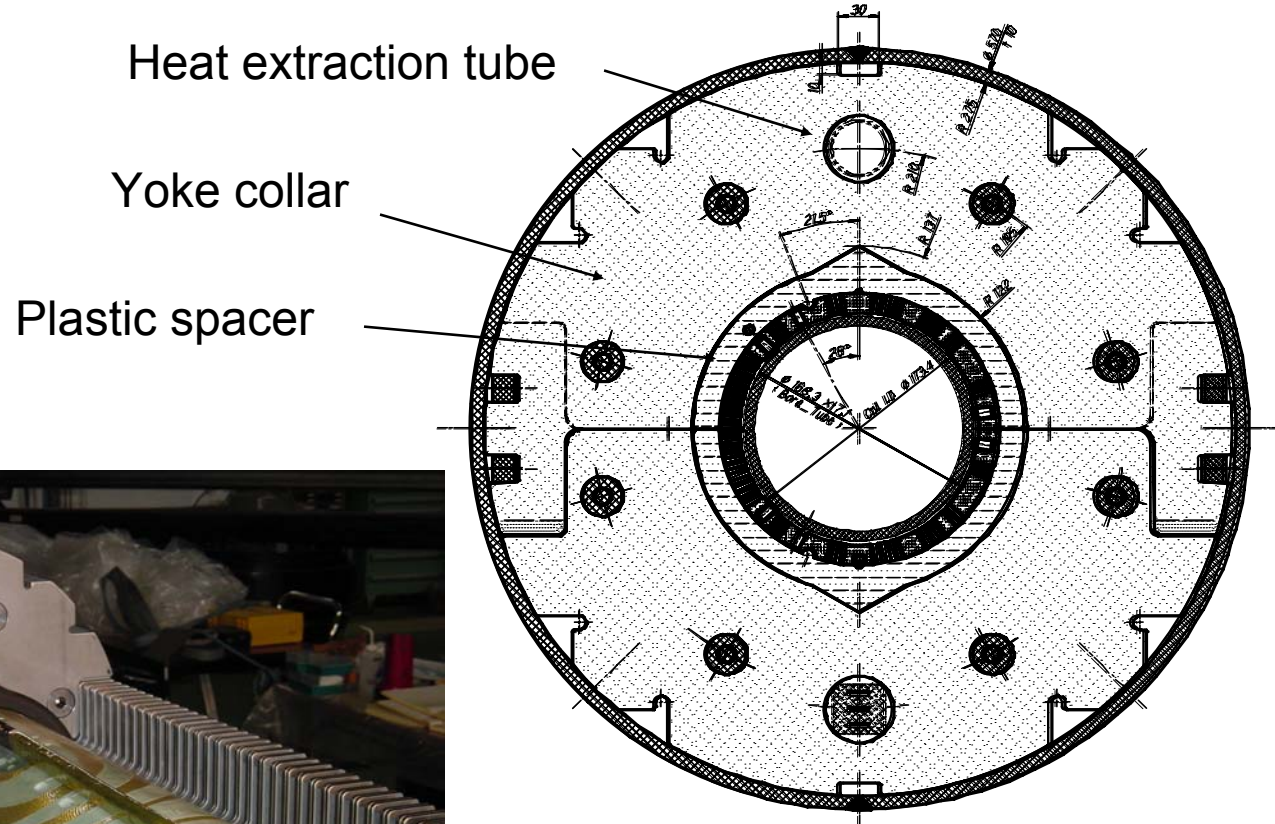
- 100 mm 2 layer design
- Quench heaters only no dump
- 0.045s detection delay
- 6m long magnet
- No cooling to the bath assumed

Look very,
too safe?





Magnet mechanical design



Photographs & sketched thanks to KEK.



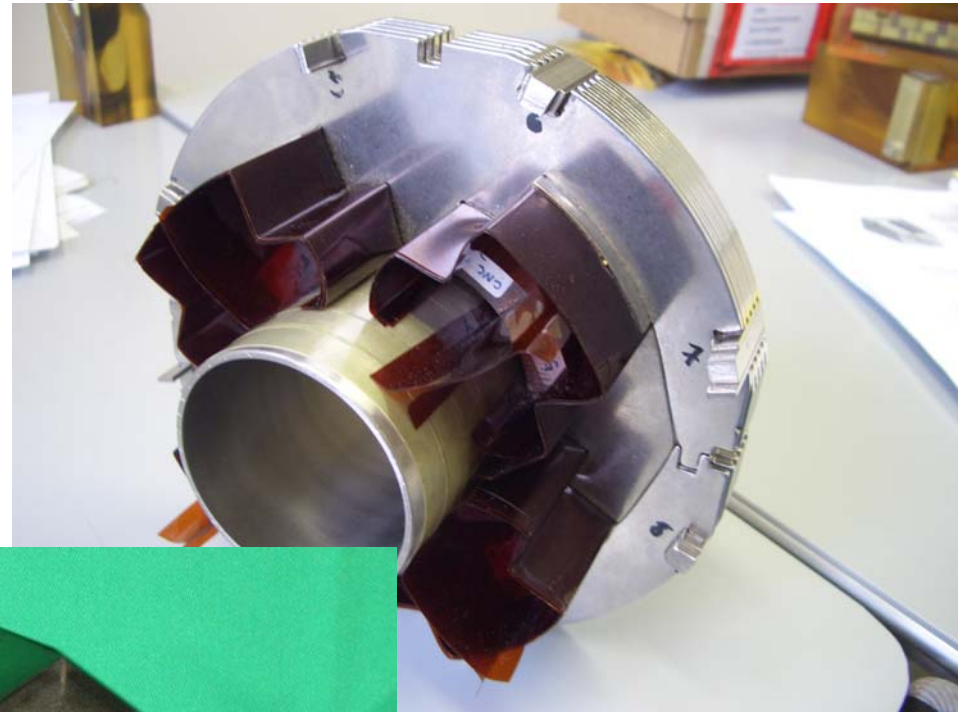
Plastic spacers

Get the heat out: No kapton sheets for ground insulation to stop the flow of Helium through the magnet.

Labyrinth design will give $\gg 5\text{Kv}$ to ground insulation.

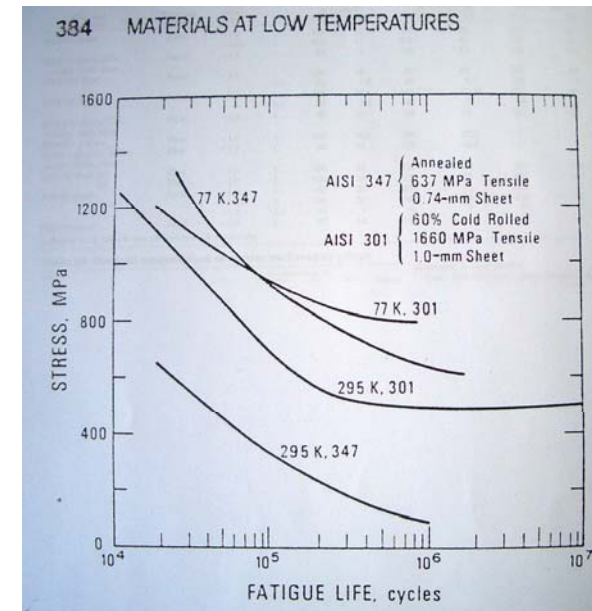
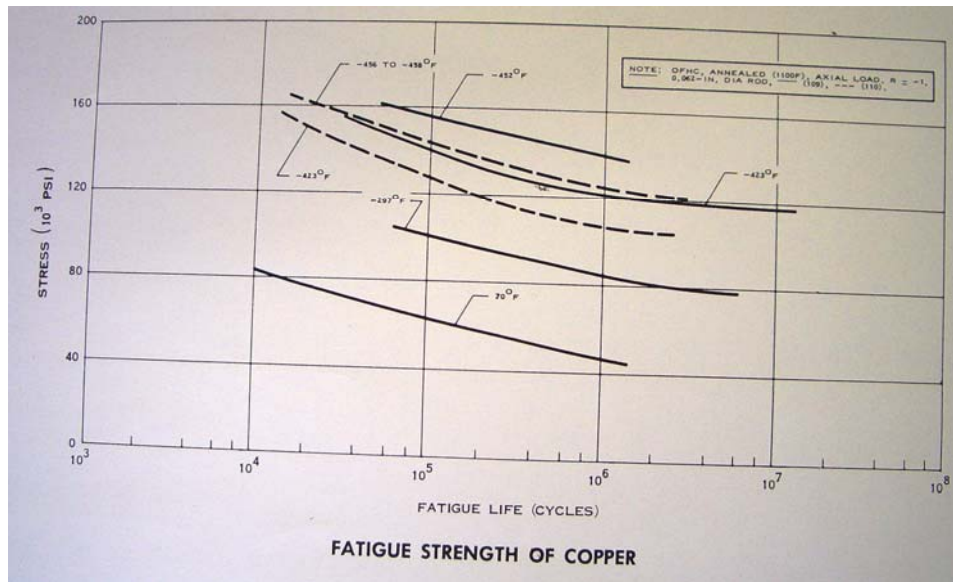
Inexpensive and fast to assemble

Bent apertures?

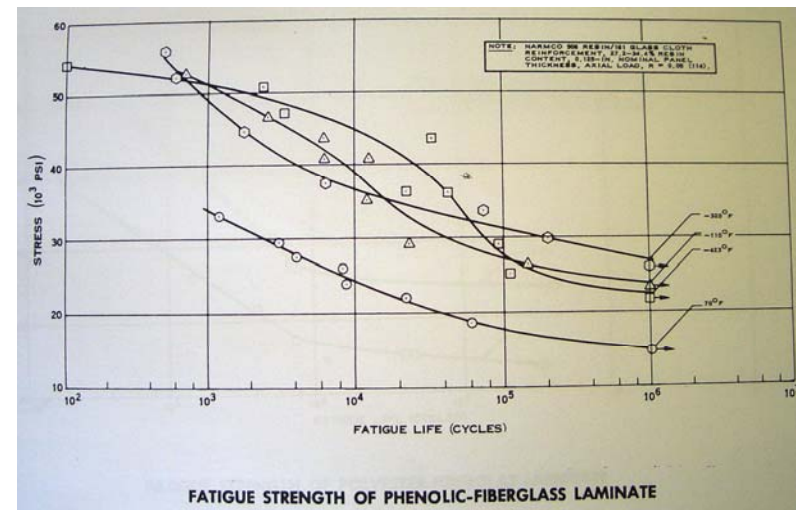




Fatigue 10^6 Cycles material data



- ◆ Some Fatigue data can be found for low temperatures.
- ◆ Fatigue life increases with lower temperature.
- ◆ 77k tests not 4k are the norm.





Fatigue at Fermilab

- ◆ After about 10^5 cycles Fermilab repaired all the TeV magnet, after they started to fail from Fatigue due to a moving current lead.





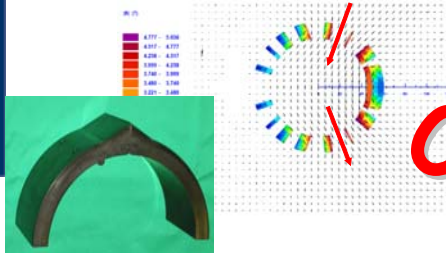
How long to develop and build the magnets

- ◆ 2 years to design and get the new strand materials for first model.
- ◆ 2 to 3 years to perform sensible fatigue and heat extraction testing with improved models.
- ◆ 3 to 4 years to build the 750 magnets.
- ◆ 10 years project! From when you start!

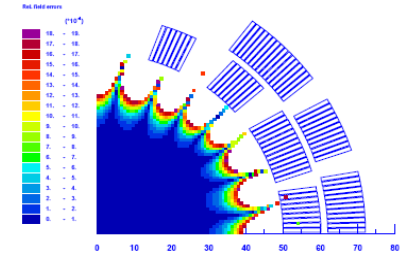
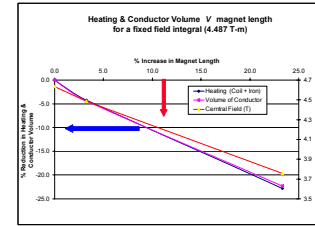


Things to do

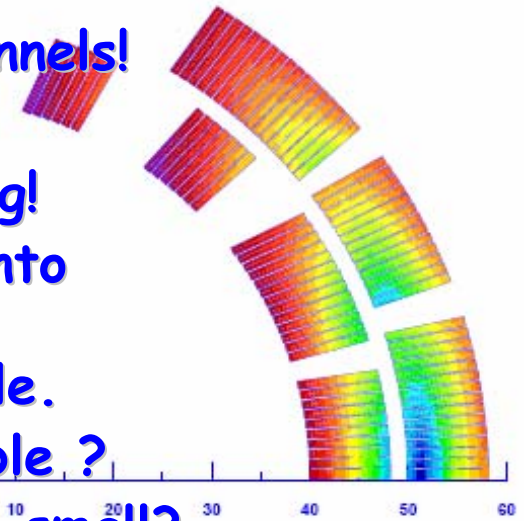
- ◆ Study Combined Function Magnet for SPS.
- ◆ How to get the heat out of a Horizontal Magnet!! study this 4.5K or 1.8K!
- ◆ Develop an open insulation system.
- ◆ Develop a Quench heater that lets Helium through the coil at 4L/min/m.
- ◆ Get superconductor ASAP!!! CuNi or Cu and make a very short test magnet.
 - Test to find R_c & R_a values in the magnet!
 - Test heat extraction, measure temp fluctuation.
 - Fatigue test station. set up accelerated fatigue cycling tests M cycles (one or two years).



Conclusions



- ◆ 2 layer design!
- ◆ GRP or Stainless steel wedges with big channels!
- ◆ Cold Iron!
- ◆ Fatigue is important! Needs design & testing!
- ◆ Aperture keep as small as possible taking into account the beam? 60 80 100?
- ◆ Beam losses push aperture as big as possible.
- ◆ Field quality during ramping seem controllable ?
- ◆ Bend the magnet to help keep the aperture small?
- ◆ Get the heat out! Very open coil / insulation.
- ◆ Long Magnets have lower heating & less conductor!
a CFM design?



Filamentbundles with interbundle Cu

