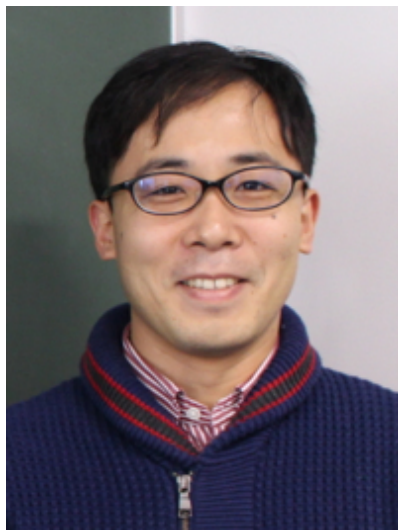


Hard Hydro Loops (HHLs) and long-time tails from
hydro-kinetics,
for a Bjorken expansion

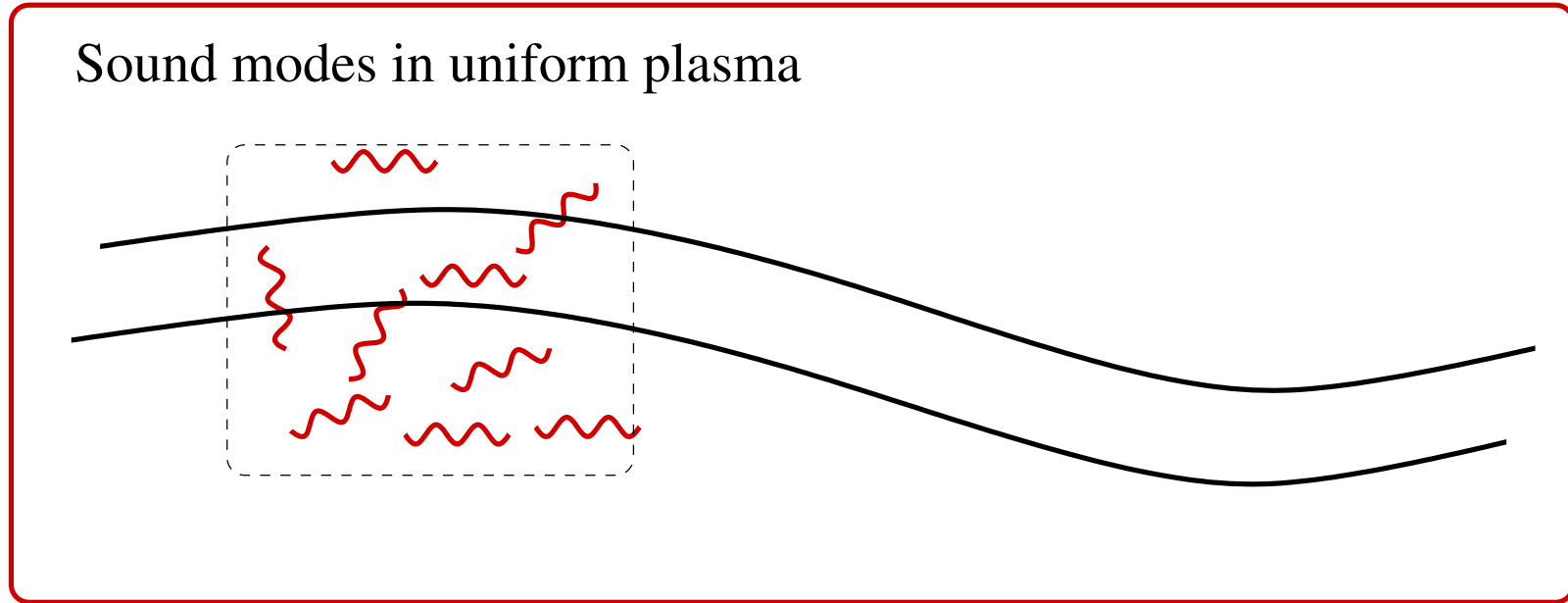
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- Yukinao Akamatsu, Aleksas Mazeliauskas, DT, arXiv:1606.07742



Thermal fluctuations:



These hard sound modes are part of the bath, giving to the pressure and shear viscosity

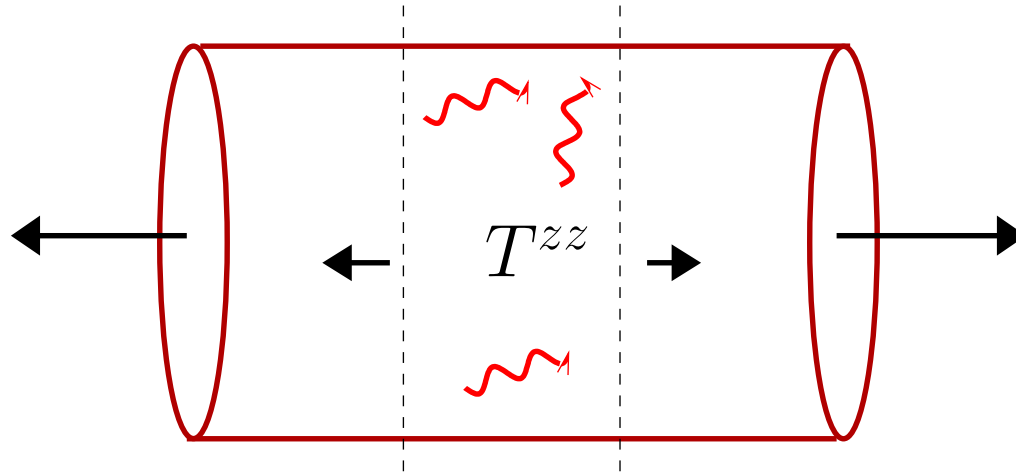
$$N_{ee}(\mathbf{k}, t) \equiv \underbrace{\langle e^*(\mathbf{k}, t)e(\mathbf{k}, t) \rangle}_{\text{energy-density fluc}} = (e + p)T/c_s^2$$

$$N_{gg}(\mathbf{k}, t) \equiv \underbrace{\langle g^{*i}(\mathbf{k}, t)g^j(\mathbf{k}, t) \rangle}_{\text{momentum, } g^i \equiv T^{0i}} = (e + p)T\delta^{ij}$$

In an expanding system these correlators will be driven out of equilibrium.

This changes the evolution of the slow modes.

A Bjorken expansion



1. The system has an expansion rate of $\partial_\mu u^\mu = 1/\tau$
2. The hydrodynamic expansion parameter is

$$\epsilon \equiv \frac{\gamma_\eta}{\tau} \ll 1 \quad \gamma_\eta \equiv \frac{\eta}{e + p}$$

and corrections to hydrodynamics are organized in powers of ϵ

$$T^{zz} = p \left[1 + \underbrace{\mathcal{O}(\epsilon)}_{\text{1st order}} + \underbrace{\mathcal{O}(\epsilon^2)}_{\text{2nd order}} + \dots \right]$$

High k modes are brought to equilibrium by the dissipation and noise

The transition regime:

- There is a wave number where the damping rate competes with the expansion

$$\underbrace{\gamma_\eta k^2}_{\text{damping rate}} \sim \underbrace{\frac{1}{\tau}}_{\text{expansion rate}}$$

and thus the transition happens for:

$$\gamma_\eta \equiv \eta / (e + p)$$


$$k \sim k_* \equiv \frac{1}{\sqrt{\gamma_\eta \tau}} \quad \text{need } k \gg k_* \text{ to reach equilibrium!}$$

- This is an intermediate scale $k_* \equiv 1 / (\tau \sqrt{\epsilon})$,

$$\epsilon \equiv \eta / (e + p) \tau$$

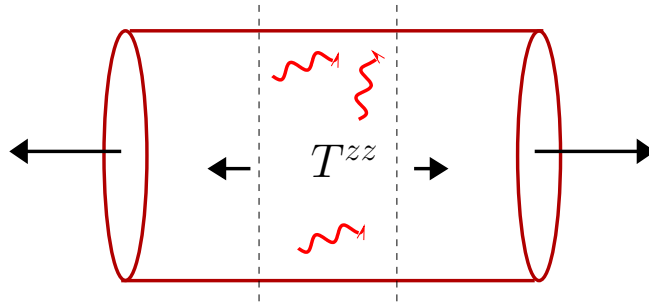
These inequalities are the same and hold whenever hydro applies

$$\frac{1}{\tau} \ll k_* \ll \frac{1}{\ell_{\text{mfp}}}$$

$$\frac{1}{\tau} \ll \frac{1}{\tau} \frac{1}{\sqrt{\epsilon}} \ll \frac{1}{\tau} \frac{1}{\epsilon}$$


Want to develop a set of hydro-kinetic equations for $k \sim k_*$
using the scale separation $\epsilon \ll \sqrt{\epsilon} \ll 1$

Estimate of longitudinal pressure from non-equilibrium modes



$$\Delta T^{zz} \sim \underbrace{\frac{1}{2}T}_{\text{energy / mode}} \times \underbrace{k_*^3}_{\text{number of non-eq modes}}$$

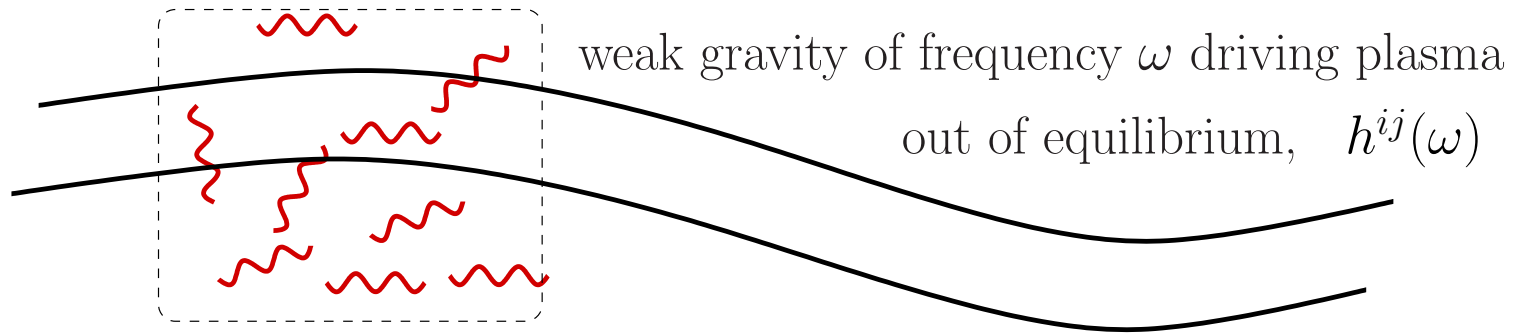
- Using $e + p = sT$ we estimate

$$\frac{\Delta T^{zz}}{e + p} \sim \frac{1}{s} \frac{1}{(\gamma_\eta \tau)^{3/2}}$$

- The full result will be:

$$\frac{\langle T^{zz} \rangle}{e + p} = \left[\underbrace{\frac{p}{e + p}}_{\sim 1} - \underbrace{\frac{4}{3} \frac{\gamma_\eta}{\tau}}_{\text{1st order}} + \underbrace{\frac{1.08318}{s (4\pi \gamma_\eta \tau)^{3/2}}}_{\text{3/2 order}} + \underbrace{\frac{(\lambda_1 - \eta \tau_\pi)}{e + p} \frac{8}{9\tau^2}}_{\text{2nd order}} \right]$$

The correction is suppressed by $s =$ the number of degrees of freedom



Hydro prediction

$$\langle T^{ij} \rangle = p h^{ij} - \eta \left(\overbrace{\nabla^i u^j}^{\text{cov-deriv}} + \nabla^j u^i - \frac{2}{3} \nabla \cdot u \right) + \text{2nd order}$$

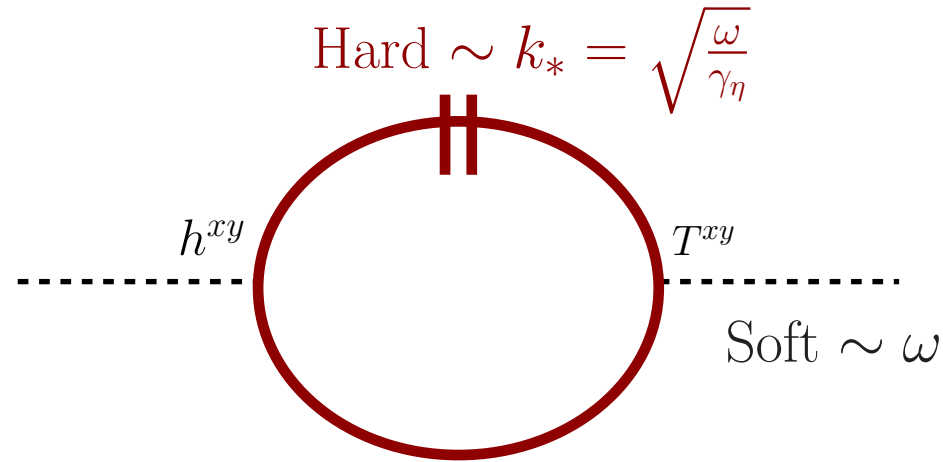
So

$$\langle T^{xy}(\omega) \rangle = \left[p - \overbrace{i\omega\eta}^{\text{1st order}} + \overbrace{(\eta\tau_\pi - \frac{1}{2}\kappa)\omega^2}^{\text{2nd order}} \right] h^{xy}(\omega)$$

Thermal fluctuations are not included, and are driven slightly out of equilibrium for $k \sim k_*$

$$\gamma_\eta k_*^2 \sim \omega \quad \text{and they are hard} \quad \omega \ll k_* \sim \sqrt{\frac{\omega}{\gamma_\eta}} \ll \frac{1}{\ell_{\text{mfp}}}$$

Include hard thermal fluctuations with $k_* \sim \sqrt{\omega/\gamma_\eta}$ as loops

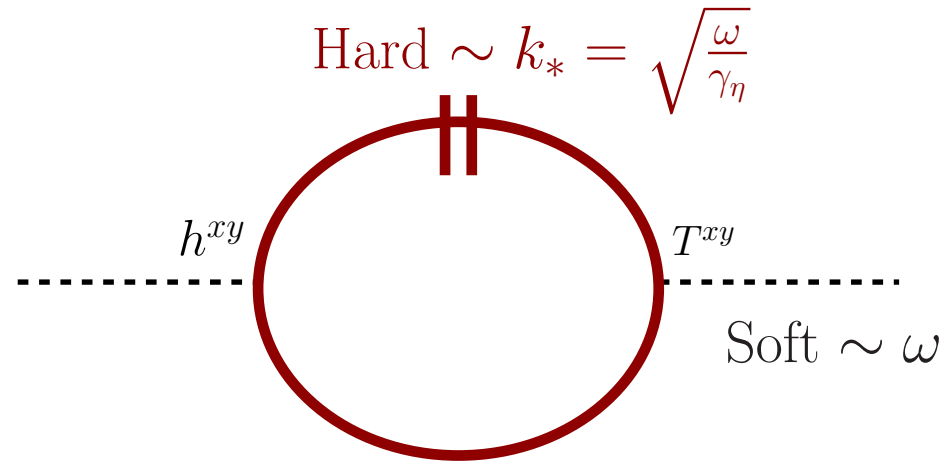


Evaluate the “Hard Hydro Thermal Loop”

$$\langle T^{xy}(\omega) \rangle = \left[p - \underbrace{i\omega\eta}_{\text{1st order}} + \underbrace{\frac{(7 + (3/2)^{3/2})}{240\pi} T \left(\frac{\omega}{\gamma_\eta}\right)^{3/2}}_{\text{3/2 order}} + \mathcal{O}(\omega^2) \right] h^{xy}(\omega)$$

The correction is of order

$$\Delta T^{xy} \sim \frac{1}{2} T k_*^3 h^{xy}$$



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I will follow Uli with hydrodynamics!

(by deriving HHTL loops from hydro Kinetic Theory)

Developing hydro-kinetics – Brownian motion

Random Walk



$$\frac{dp}{dt} = -\eta p + \xi \quad \langle \xi(t)\xi(t') \rangle = 2TM\eta \delta(t - t')$$

1. Then we want to calculate

$$N(t) = \langle p^2(t) \rangle$$

2. Integrate the equation for short times

$$p(t + \Delta t) = -\eta p(t)\Delta t + \int_t^{t+\Delta t} \xi(t') dt'$$

3. Compute $\langle p(t + \Delta t) p(t + \Delta t) \rangle$ and find an equation

$$\frac{\Delta N}{\Delta t} = -2\eta \left[N - \underbrace{TM}_{\text{equilibrium}} \right]$$

Developing hydro-kinetics – linearized hydro in a uniform system

1. Evolve fields of linearized hydro with bare parameters $p_0(\Lambda)$, $\eta_0(\Lambda)$, $s_0(\Lambda)$ etc

$$\phi_a(\mathbf{k}) \equiv \left(e(\mathbf{k}), g^x(\mathbf{k}), g^y(\mathbf{k}), g^z(\mathbf{k}) \right)$$

2. Then the equations are schematically exactly the same

$$\frac{d\phi_a(\mathbf{k})}{dt} = \underbrace{\mathcal{L}_{ab}(\mathbf{k})}_{\text{ideal}} \phi_b(\mathbf{k}) + \underbrace{D_{ab}\phi_b}_{\text{1st visc}} + \xi_a \quad \langle \xi_a \xi_b \rangle = 2T\mathcal{D}_{ab}(\mathbf{k})\delta(t - t')$$

3. Break up the equations into eigen modes of \mathcal{L}_{ab} , and analyze exactly same way:

$$\begin{array}{ccc} \underbrace{\text{right moving sound}} & \underbrace{\text{left moving sound}} & \underbrace{\text{two diffusion modes}} \\ \lambda_+ = +ic_s k & \lambda_- = -ic_s k & \lambda_T = 0 \end{array}$$

So for k in the z direction, work with the following linear combos (eigenvects)

$$\phi_A \equiv \left[\underbrace{c_s e(\mathbf{k}) \pm g^z(\mathbf{k})}_{\phi_+ \text{ and } \phi_-}, \underbrace{g^x(\mathbf{k})}_{\equiv \phi_{T_1}}, \underbrace{g^y(\mathbf{k})}_{\equiv \phi_{T_2}} \right]$$

The kinetic equations in flat space

1. The relevant correlators are e.g.

$$N_{++}(\mathbf{k}, t) = \langle \phi_+^*(\mathbf{k}) \phi_+(\mathbf{k}) \rangle \quad N_{T_1 T_1} = \langle \phi_{T_1}^*(\mathbf{k}) \phi_{T_1}(\mathbf{k}) \rangle$$

2. Thus

$$\frac{dN_{++}}{dt} = -\frac{4}{3}\gamma_\eta k^2 [N_{++} - N_{++}^{\text{eq}}]$$
$$\frac{dN_{T_1 T_1}}{dt} = -2\gamma_\eta k^2 [N_{T_1 T_1} - N_{T_1 T_1}^{\text{eq}}]$$

and similar equations for N_{--} and $N_{T_2 T_2}$. Here

$$N_{T_1 T_1}^{\text{eq}} \equiv (e + p)T \quad \text{and} \quad N_{++}^{\text{eq}} \equiv (e + p)T$$

3. Neglect off diagonal components of density matrix in eigen-basis

$$\frac{dN_{+T_1}}{dt} = \underbrace{-ic_s k}_{\lambda_A - \lambda_B} N_{+T_1} \quad \Leftarrow \text{Rapidly rotating.}$$

Now we will do the same for a perturbed and expanding system

Case 1: Kinetic equations for perturbed system (HHTLs)

1. Turn on a weak gravitational perturbations, $h_{ij} = h(t) \text{diag}(1, 1, -2)$

$$\partial_t N_{++}(k) = - \underbrace{\frac{4}{3} \gamma_\eta k^2 [N_{++} - N_{++}^{\text{eq}}]}_{\text{damping}} + \underbrace{\partial_t h (\sin^2 \theta_k - 2 \cos^2 \theta_k)}_{\text{perturbation } h_{ij} \hat{k}^i \hat{k}^j} N_{++}$$

2. Solve the equations to first order in the gravitational, e.g.

$$\delta N_{++} = \frac{i\omega h (\sin^2 \theta_k - 2 \cos^2 \theta_k)}{-i\omega + \frac{4}{3} \gamma_\eta K^2}$$

3. Calculate the stress tensor

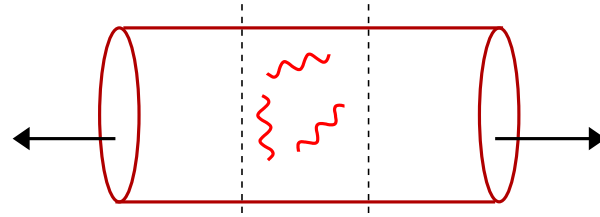
$$\delta T^{ij} = (e + p) \langle v^i v^j \rangle = \int \frac{d^3 K}{(2\pi)^3} \frac{\langle g^i(\mathbf{k}) g^j(-\mathbf{k}) \rangle}{e + p}$$

4. Find an HTL like expression

$$\langle \delta T^{xx} + \delta T^{yy} - 2\delta T^{zz} \rangle \supset h \int \frac{d^3 K}{(2\pi)^3} \delta N_{++} \underbrace{(\sin^2 \theta - 2 \cos^2 \theta)}_{\hat{k}^x \hat{k}^x + \hat{k}^y \hat{k}^y - 2\hat{k}^z \hat{k}^z}$$

Precisely reproduces hard hydro loop calculation!

Case 2: Kinetic equations for a Bjorken expansion – Hard Hydro Loops (HHLs)



- The hydrodynamic field fields $\phi_a = (c_s e, g^x, g^y, \tau g^\eta)$ are:

$$\phi_a(\tau, \mathbf{k}_\perp, \kappa) = \int d^2\mathbf{x} \int d\eta e^{i\mathbf{k}_\perp \cdot \mathbf{x}_\perp + i\kappa\eta} \phi_a(\tau, \mathbf{x}_\perp, \eta)$$

- The equations take the form:

$$\frac{d}{d\tau} \phi_a(\mathbf{k}_\perp, \kappa) = \underbrace{\mathcal{L}_{ab}}_{\text{ideal}} \phi_b + \underbrace{D_{ab} \phi_b}_{\text{viscous}} + \underbrace{\mathcal{P}_{ab}}_{\text{perturb}} + \underbrace{\xi_a}_{\text{noise}}$$

The previous analysis goes through with a no complications, $\lambda = \pm i c_s k, 0$

$$\mathcal{P}_{ab} = \frac{1}{\tau} \begin{pmatrix} 1 + c_s^2 & & & \\ & 1 & & \\ & & 1 & \\ & & & 2 \end{pmatrix}$$

The kinetic equations and approach to equilibrium:

- The kinetic equations and approach to equilibrium

$$\frac{\partial}{\partial \tau} N_{++} = - \frac{1}{\tau} \left[\underbrace{2 + c_{s0}^2 + \frac{\kappa^2/\tau^2}{k_{\perp}^2 + \kappa^2/\tau^2}}_{\text{perturbation} = 2\mathcal{P}_{++}} \right] N_{++} - \underbrace{\frac{\frac{4}{3}\eta_0}{s_0 T_0} \left(k_{\perp}^2 + \frac{\kappa^2}{\tau^2} \right)}_{\text{damping to equilibrium}} \left[N_{++} - \frac{s_0 T_0^2}{2c_{s0}^2 \tau} \right],$$

$$\frac{\partial}{\partial \tau} N_{T_2 T_2} = - \frac{2}{\tau} \left[\underbrace{1 + \frac{k_{\perp}^2}{k_{\perp}^2 + \kappa^2/\tau^2}}_{\text{perturbation} = 2\mathcal{P}_{T_2 T_2}} \right] N_{T_2 T_2} - \underbrace{\frac{2\eta_0}{s_0 T_0} \left(k_{\perp}^2 + \frac{\kappa^2}{\tau^2} \right)}_{\text{damping to equilibrium}} \left[N_{T_2 T_2} - \frac{s_0 T_0^2}{\tau} \right].$$

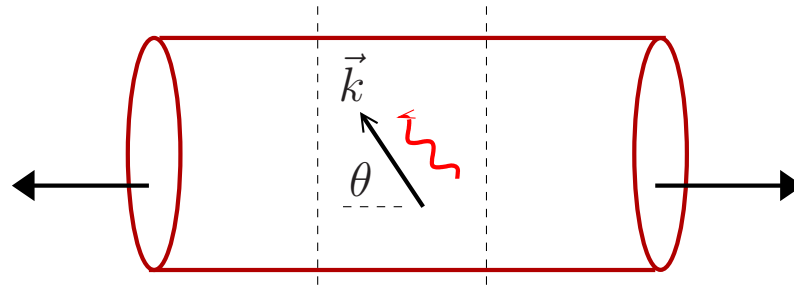
and similar equations for the other modes

- For large k , we solve, and the modes approximately equilibrate:

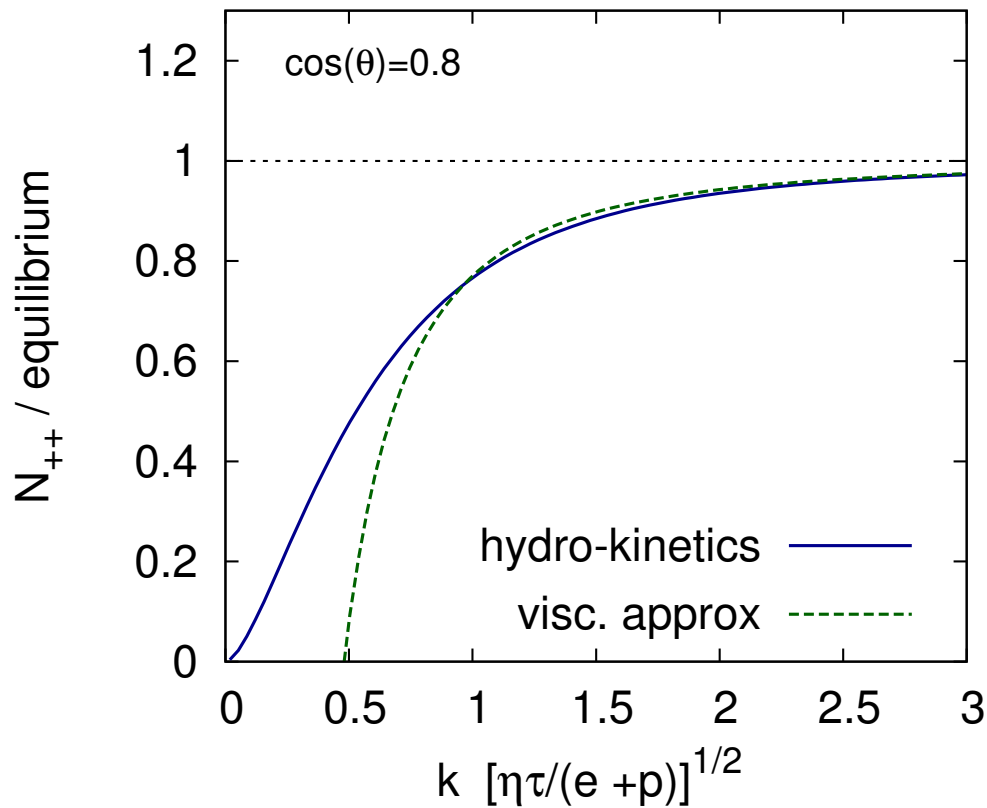
$$N_{++} \simeq \frac{s_0 T_0^2}{2c_{s0}^2 \tau} \left[\underbrace{1}_{\text{equilibrium}} + \underbrace{\frac{s_0 T_0}{\frac{4}{3}\eta_0 (k_{\perp}^2 + \kappa^2/\tau^2)} \left(c_{s0}^2 - \frac{\kappa^2/\tau^2}{k_{\perp}^2 + \kappa^2/\tau^2} \right)}_{\text{first viscous correction analogous to } \delta f} + \dots \right]$$

Now we solved these kinetic equations numerically

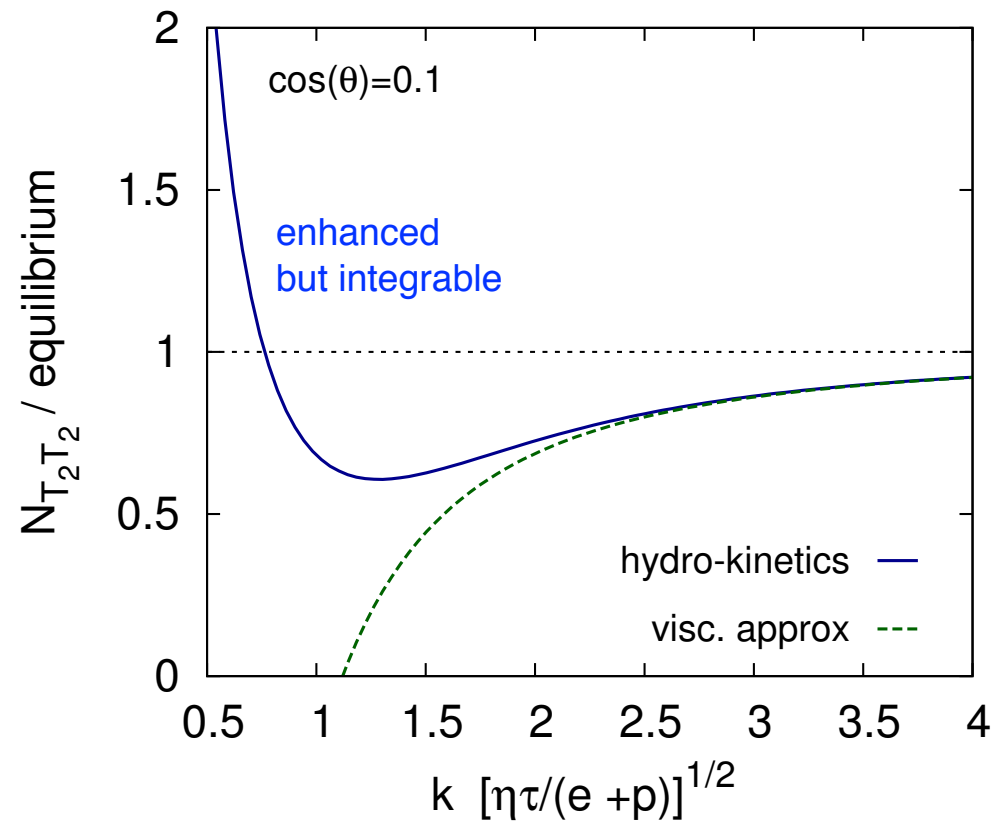
The non-equilibrium steady state at late times:



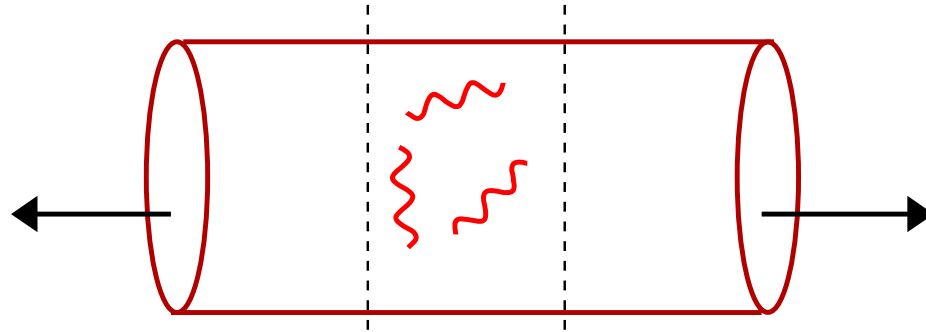
Sound Modes



Transverse modes



The evolution of the background



$$\frac{dT^{\tau\tau}}{d\tau} = -\frac{T^{\tau\tau} + T^{zz}}{\tau}$$

where

$$T_{\text{hydro}}^{zz} = \underbrace{p_0(\Lambda)}_{\text{Ideal}} - \underbrace{\frac{\frac{4}{3}\eta_0(\Lambda)}{\tau}}_{\text{first order}} + \underbrace{(\lambda_1 - \eta\tau_\pi)\frac{8}{9\tau^2}}_{\text{second order}} + \dots$$

In addition the fluctuations give another contribution:

$$T_{\text{flucts}}^{zz} = (e + p) \langle v^z v^z \rangle$$

Evaluating the fluctuation contribution:

$$\begin{aligned}
 \frac{T_{\text{flucts}}^{zz}}{e+p} &= \langle v^z v^z \rangle \\
 &= \int \frac{d^2 k_{\perp} d\kappa}{(2\pi)^3} \frac{1}{(e_o + p_o)^2} [N_{++} \cos^2 \theta + N_{T_2 T_2} \sin^2 \theta] \\
 &= \frac{T_o \Lambda^3}{6\pi^2} - \left(\frac{17\Lambda}{120\pi^2} \frac{s_o T_o^2}{\eta_o(\Lambda)} \right) \frac{4}{3} \frac{1}{\tau} + \text{finite}
 \end{aligned}$$

Thus the full stress is then:

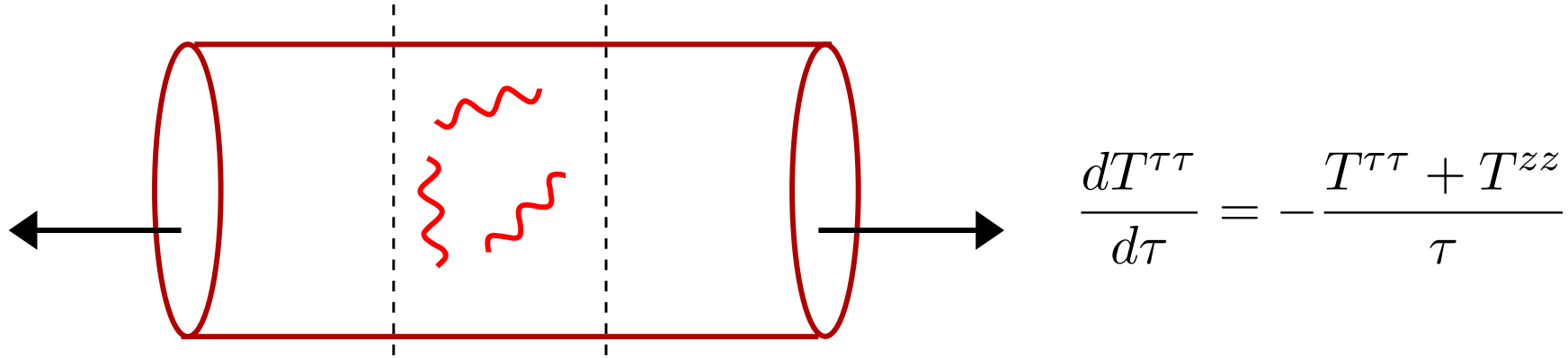
compare Kovtun, Moore, Romatschke

$$\begin{aligned}
 T^{zz} &= T_{\text{hydro}}^{zz} + T_{\text{flucts}}^{zz} & p_{\text{phys}} &\equiv p_0(\Lambda) + \frac{T_o \Lambda^3}{6\pi^2} \\
 &= p_{\text{phys}} - \frac{4}{3} \frac{\eta_{\text{phys}}}{\tau} + \text{finite} & \eta_{\text{phys}} &\equiv \eta_0(\Lambda) + \left(\frac{17\Lambda}{120\pi^2} \frac{s_o T_o^2}{\eta_o(\Lambda)} \right)
 \end{aligned}$$

where the physical quantities, p_{phys} and η_{phys} , are independent of Λ

What's the finite correction?

Final result for a Bjorken expansion:



$$\frac{dT^{\tau\tau}}{d\tau} = -\frac{T^{\tau\tau} + T^{zz}}{\tau}$$

$$\frac{\langle T^{zz} \rangle}{e+p} = \left[\underbrace{\frac{p}{e+p}}_{\sim 1} - \underbrace{\frac{4\gamma_\eta}{3\tau}}_{\text{1st order}} + \underbrace{\frac{1.08318}{s(4\pi\gamma_\eta\tau)^{3/2}}}_{\text{3/2 order}} + \underbrace{\frac{(\lambda_1 - \eta\tau_\pi) 8}{e+p 9\tau^2}}_{\text{2nd order}} \right]$$

From which much can be wrought or wrung . . .

Numerical results:

Take representative numbers

$$\frac{(\lambda_1 - \eta\tau\pi)}{e + p} \simeq -0.8 \left(\frac{\eta}{e + p} \right)^2 \quad \frac{T^3}{s} \simeq \frac{1}{13.5}$$

For $\eta/s = 1/4\pi$ find:

$$\frac{T^{zz}}{e + p} = \frac{1}{4} \left[1. - \underbrace{0.092}_{\text{first}} \left(\frac{4.5}{\tau T} \right) + \underbrace{0.034}_{\text{3/2 order } \simeq 30\%} \left(\frac{4.5}{\tau T} \right)^{3/2} - \underbrace{0.0009}_{\text{second}} \left(\frac{4.5}{\tau T} \right)^2 \right]$$

while for $\eta/s = 2/4\pi$ we have:

$$\frac{T^{zz}}{e + p} = \frac{1}{4} \left[1. - \underbrace{0.185}_{\text{first}} \left(\frac{4.5}{\tau T} \right) + \underbrace{0.013}_{\text{3/2 order } \simeq 10\%} \left(\frac{4.5}{\tau T} \right)^{3/2} - \underbrace{0.0034}_{\text{second}} \left(\frac{4.5}{\tau T} \right)^2 \right]$$

Fluctuation contribution is a correction to first order hydro

but larger than second order in practice

Summary

1. For wavenumbers of order

$$k \sim \sqrt{\frac{e + p}{\eta\tau}}$$

the system transitions to equilibrium

2. Worked out an alternate description of hydro with noise:

- Hydro + hydro-kinetics

$$\begin{aligned}\partial_\mu (T_{\text{hydro}}^{\mu\nu} + T_{\text{flucts}}^{\mu\nu}) &= 0 \\ \partial_\tau N_{\text{flucts}}(\mathbf{k}, \tau) &= \dots\end{aligned}$$

This should be generalized to a general flows.

3. How is the non-linear $T_{\text{flucts}}^{\mu\nu}$ imprinted on the particles?

$$\delta f_{\text{flucts}} = \text{????}$$

4. Fluctuating hydro is much more important than second order hydro in practice!