

CRYOGENIC HAZARD AT ESS

STRATEGY, SAFETY STUDIES AND LESSONS LEARNT

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CERN Cryogenic Safety – HSE seminar, 21-23 September 2016

AGENDA

- 1 Overview of the **ESS ODH Safety process and implementation** [ESS-0038692](#)
- 2 **Safety studies and concept against Oxygen Deficiency Hazard** in the accelerator tunnel
- 3 **Results and lessons learnt from the Computational Fluid Dynamics (CFD)** simulations in the accelerator tunnel
- 4 **Upcoming activities and challenges**

Introduction



Ion source

Target

2014: construction work started on the site

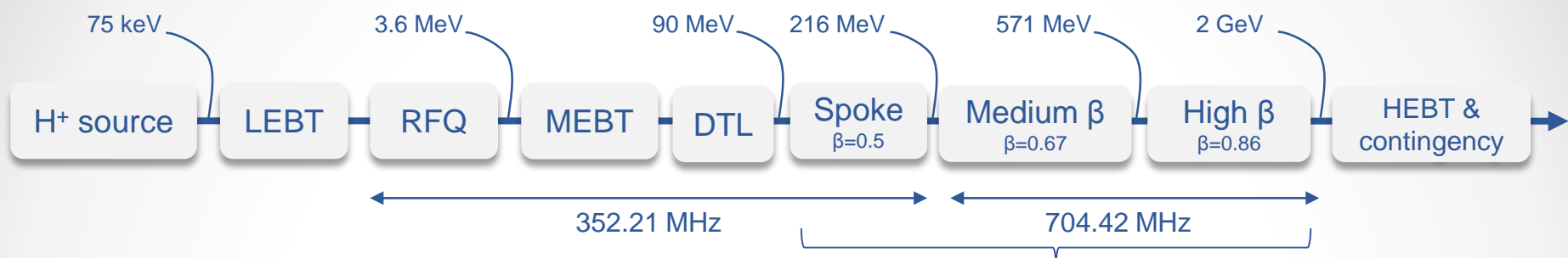
2019: first neutrons on instruments

2023: ESS starts user program

2025: ESS construction complete

Introduction

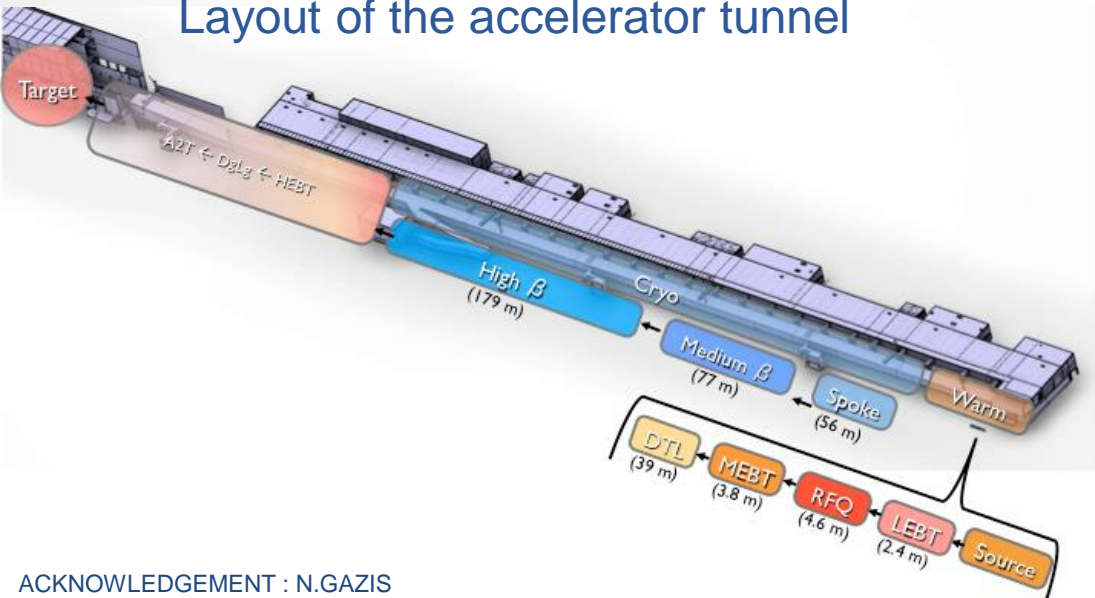
Main parameters of the ESS Linac



Helium inventory (nominal operation)
 Elliptical CM - 1014 kg
 Spoke CM - 277 kg
 CDS - 215 kg



Layout of the accelerator tunnel



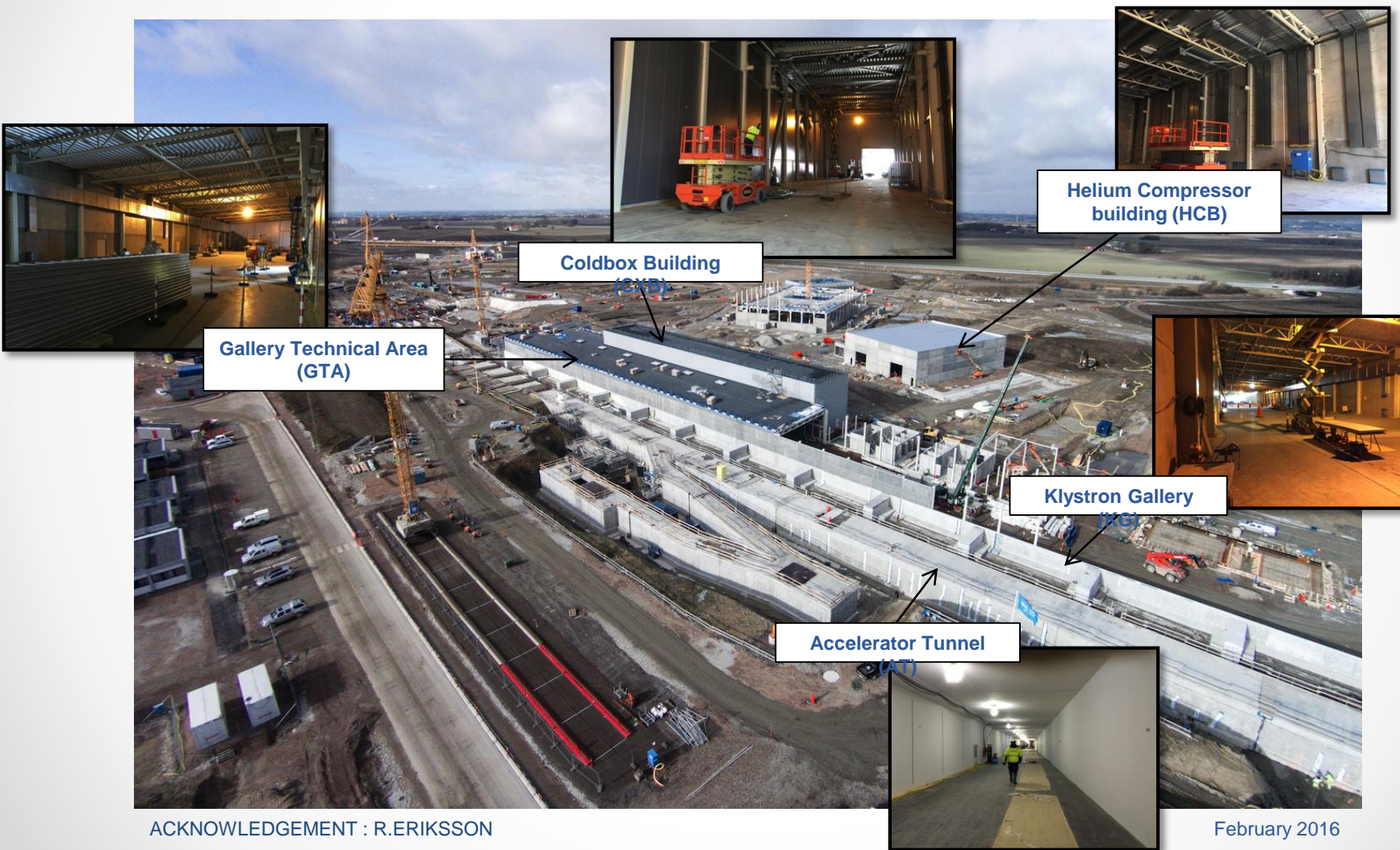
Parameters	ESS LINAC
E [GeV]	2
P _{average} [MW]	5
I _{pulse} [mA]	62.5
f _{rep} [Hz]	14
t _{pulse} [ms]	2.86

First beam on target at 572 MeV in **June 2019**

Full beam power in **2022-2023**

Introduction

View of the accelerator buildings

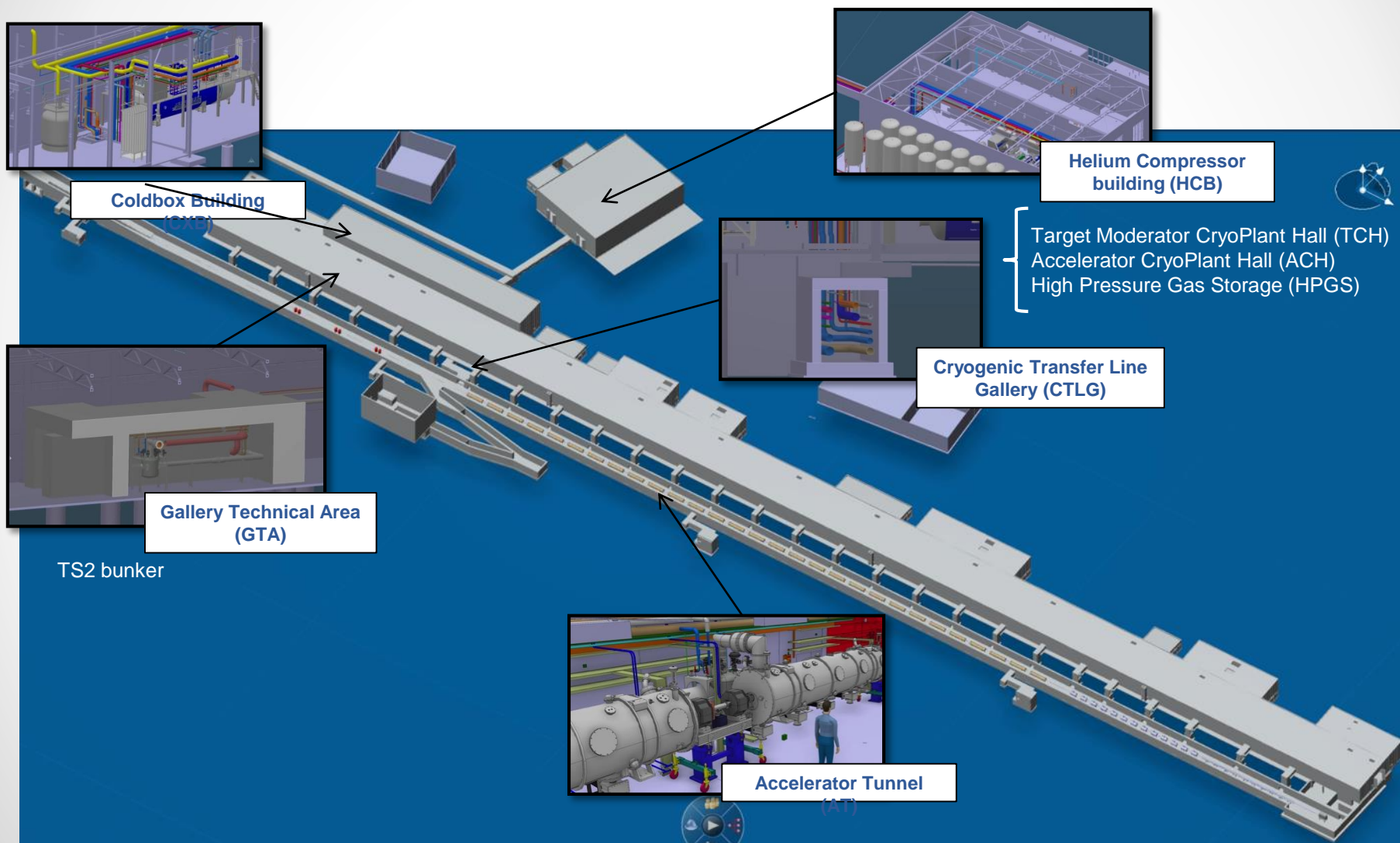


ACKNOWLEDGEMENT : R.ERIKSSON

February 2016

Introduction

View of the accelerator buildings (3D model)




ODH Safety process & implementation

Overview and progress

Mainly inspired by
FESHM 4240: Oxygen Deficiency Hazard

Objectives

- Enforcement of the ODH safety process at ESS
- Description of the following:
 - ✓ **Applicable rules** (EU, Swedish, ESS)
 - ✓ ODH calculation **methodology**
 - ✓ List of **control measures** (training, PPE, ventilation, etc.)
 - ✓ **Cryogenic Safety Committee**
 - ✓ Content of the **Safety File**



ESS
EUROPEAN
 COLLIDER
 SOURCE

Description: H&E 211
 Document No: H&E 211-1
 Date: 11-28-99 2013-11-11

Oxygen Deficiency Hazard (ODH)
 Safety Process & Implementation

	Name	Affiliation
Authors	N. Lind, D. Pagan, A. Wronski	
Reviewers	K. Hink, L. Conroy, C. Oates, M. Everett, P. Jacobson, M. Lindros, L. Tschelidze, B. Winter	
Approver		

Distribution: <<add names>>

ESS-0038692



Description: H&E 211
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 Date: 11-28-99 2013-11-11

$$F = \sum_{i=1}^n P_i$$

ϕ = the 10^{-6} fatality rate per hour
 P_i = the expected failure rate of the event per hour
 F_i = the probability of a fatality due to event

The summation shall be taken over all events, which may cause oxygen deficiency and result in fatality.

When possible, the value of F shall be determined by operating experience at ESS; otherwise data from similar systems elsewhere or other relevant values shall be used. Estimates of equipment failure rates are given in Appendix.

The value of F is the probability that a person will die if the lowest oxygen... The value depends on the oxygen concentration. For convenience of calculation, an approximate relationship between the value of F and the lowest attainable oxygen concentration has been developed (Figure 1).

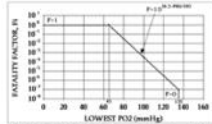


Figure 1: Fatality probability as a function of the lowest oxygen concentration (partial pressure)

The lowest attainable concentration is used, rather than an average, since that minimum value is conservative and the time dependence of the concentration is normally not well known.

If the lowest oxygen concentration is greater than 18%, then the value of F is zero, that is, all exposures above 18% are defined to be "safe" and do not contribute to fatality.

It is assumed that all exposures to 18% oxygen or lower do contribute to fatality and the value of F is designed to reflect this dependence. **If the lowest attainable oxygen concentration is 18%, then the value of F is 10.** This value would cause ϕ to be 10^{-5} per hour if the expected rate of occurrence of the event were 1 per hour.

As decreasing concentrations, the value of F should increase until, at some point, the **probability of fatality becomes unity.** That point has been selected to be 8.8% oxygen, the concentration at which the amount of consciousness is expected.

4.1 ODH Class vs. fatality rate

The classification or the ODH class depends on the ODH fatality rate as ϕ as shown in the table below:

ODH Class	ϕ (hr ⁻¹)
0	<10 ⁻⁷
I	>10 ⁻⁷ but <10 ⁻⁶
II	>10 ⁻⁶ but <10 ⁻⁵

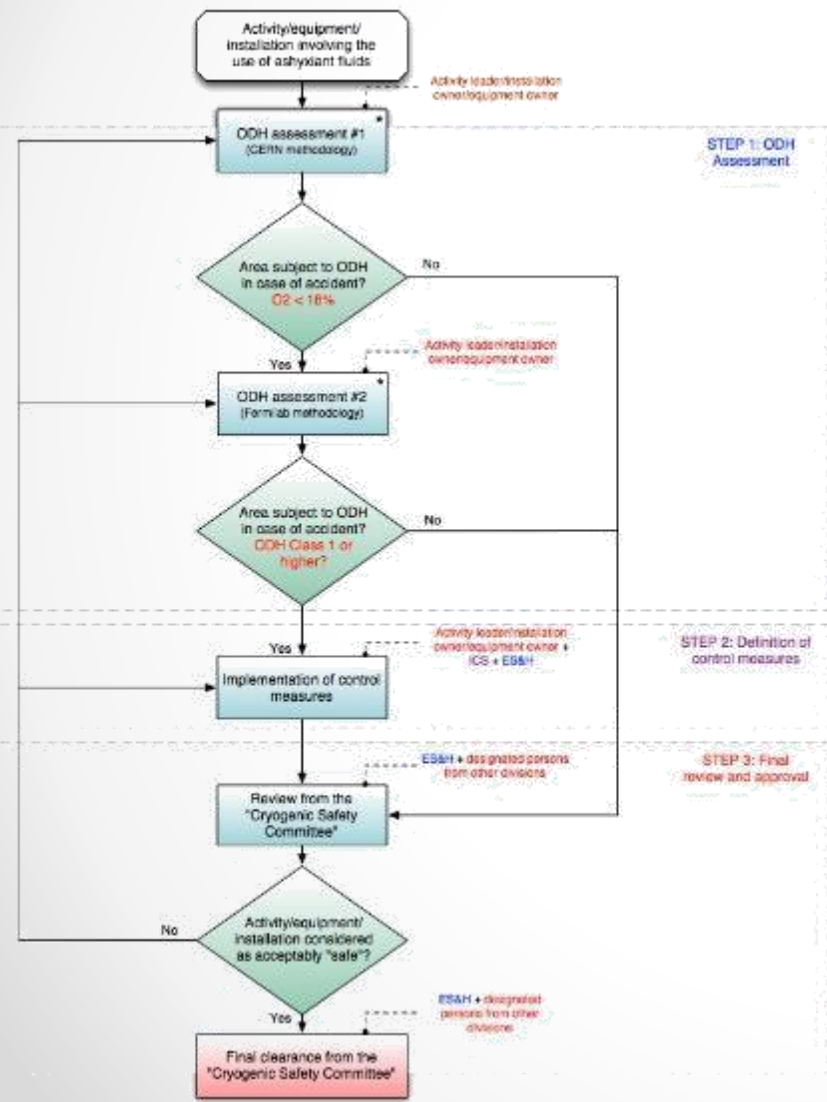
The risk assessment should also consider the benefit of existing active control systems such as forced ventilation or any supply shut-off valves that are automatically activated by area monitor readings or system failure indicators. Systems must be designed to be activated before oxygen concentration in the area drops below 18%. Although such systems or any forced ventilation system reduces overall risk, they are also subject to failure and this shall be factored into the risk assessment.



ESS wide

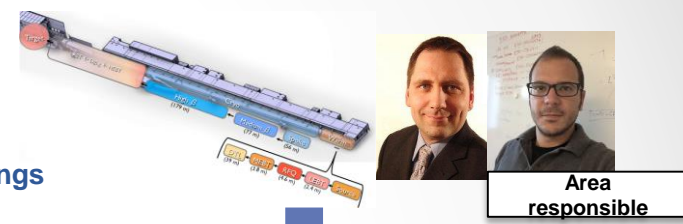
ODH Safety process & implementation

Example of implementation



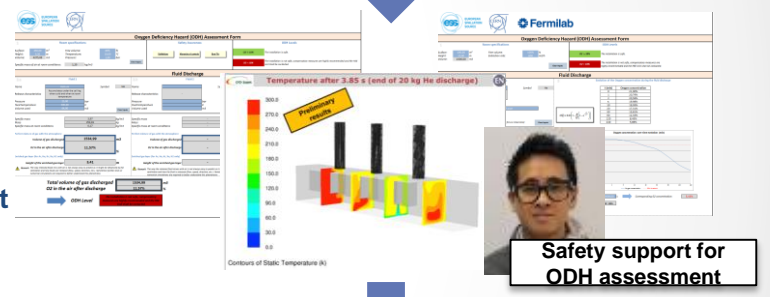
1

Accelerator buildings



2

ODH assessment



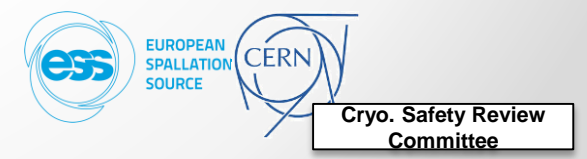
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Control measures



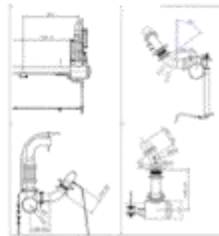
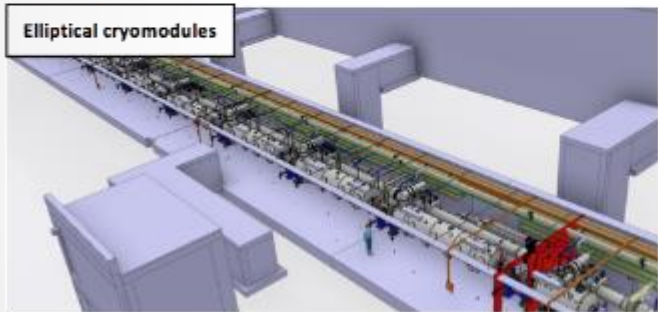
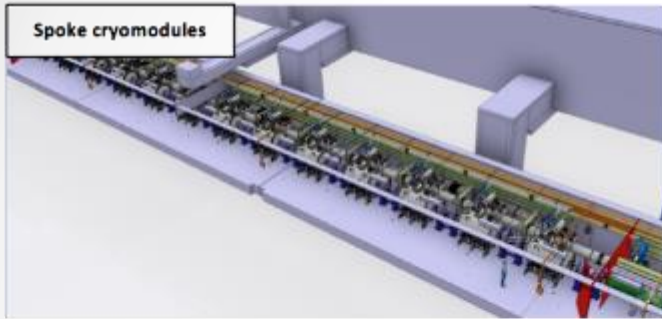
4

Review & approval
September 16th 2016



* For specific and complex cases, further ODH analyses such as Computational Fluid Dynamics (CFD) might be necessary

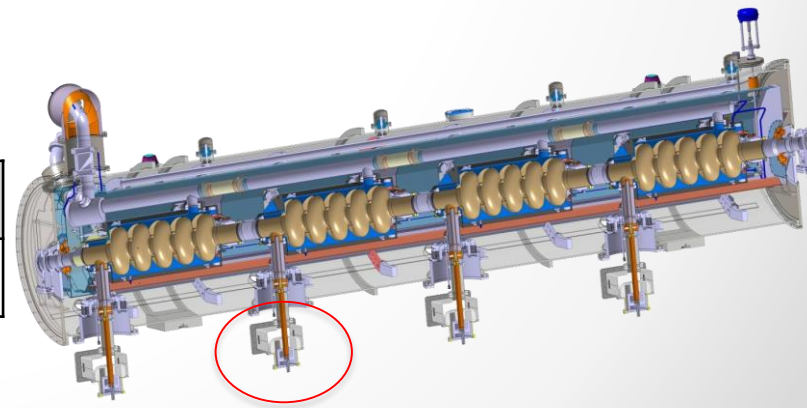
Results from the preliminary ODH assessment [ESS-0063324](#)



Most credible accidental scenario



sudden loss of the beam vacuum leading to the release of the full helium inventory from one cryomodule (e.g. rupture of one of the power coupler ceramic windows)



Ground surface	Height	Volume	Temperature	Pressure	Ventilation rate
3600 m ²	3.5 m	12 600 m ³	18°C	1 atm	25 200 m ³ /h

Results from the preliminary ODH assessment [ESS-0063324](#)

Step 1: steady-state calculation model

$$C = \frac{0,21(V - V_{gas})}{V}$$

Fluid	State	Volume	Operational pressure	Temperature
Helium (High- β elliptical cryomodule)	Liquid	0.226 m ³	Max 1.43 bara	2 K



Volume of gas discharged: **203 m³**

O₂ in the air after discharge: **20%**

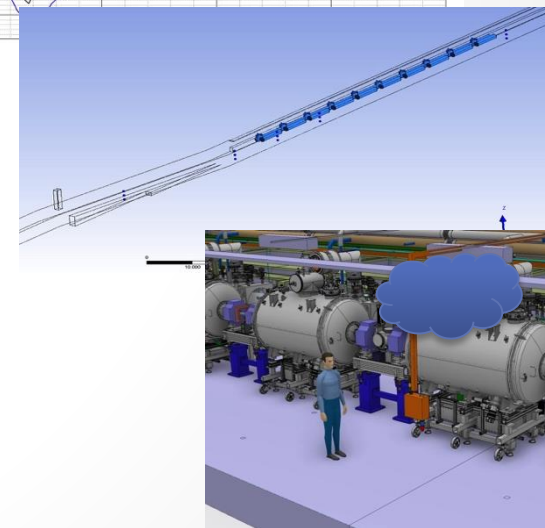
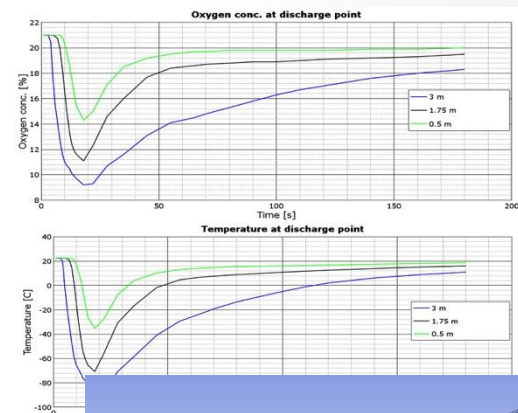
ODH CLASS 0

Special case: due to the particular geometry (low height and presence of a dead-end in the A2T area) of the tunnel and the numbers of helium discharge points in the tunnel, it was decided to perform a **CFD simulation** in order to estimate the temperature, the oxygen concentration as well as the pressure evolution at various locations and times in the tunnel in case of a release of helium

Accelerator tunnel

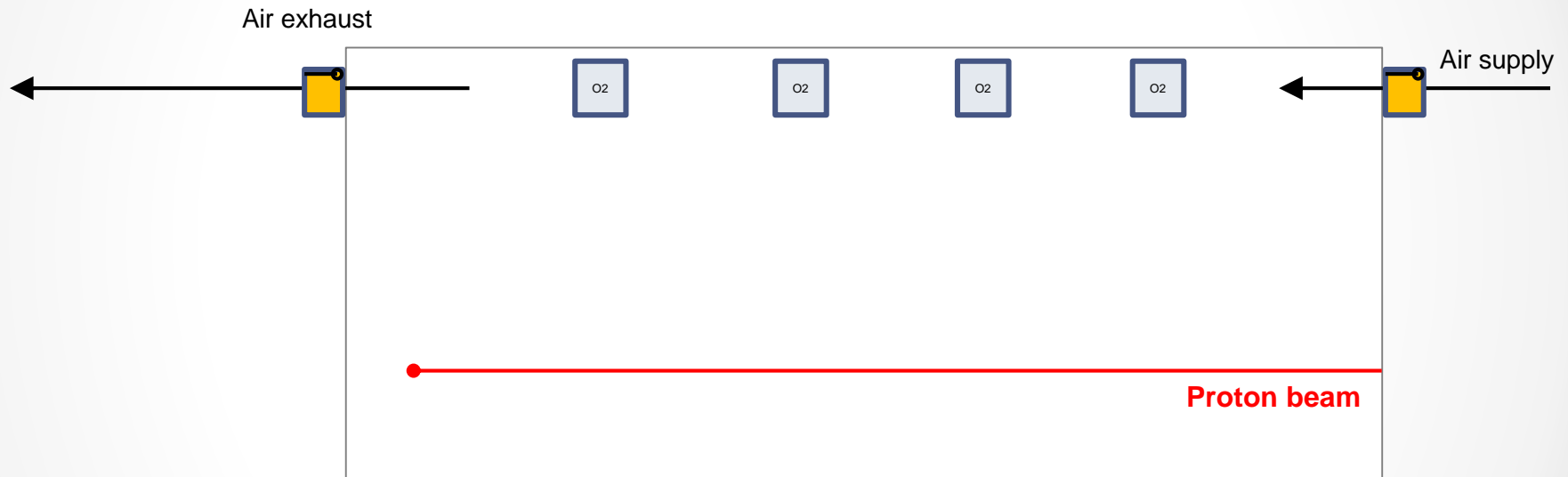
ODH studies – CFD simulation of helium discharge

- ① **Temperature and O₂ concentration** need to be evaluated locally (close to the He discharge points) as well as pressure rise
- ② Assessment of **human evacuation** (pathway, time) in case of a helium release
- ③ Help in the decision-making to CF for the **design of the ventilation system**
- ④ Help in the definition of the **access procedure** to the LINAC (warm-up, cool-down, steady-state)



Accelerator tunnel

Conceptual design for the air management system



 Fire damper

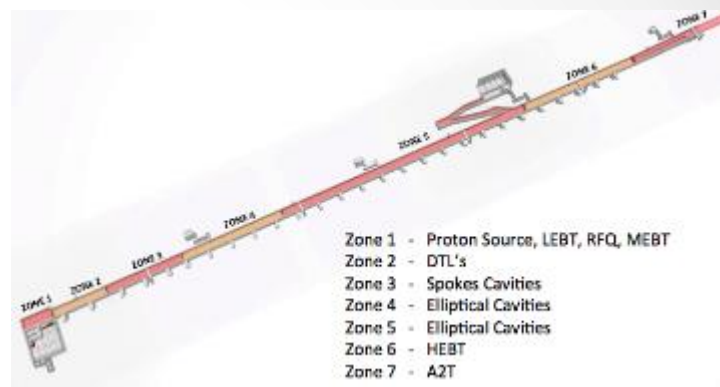
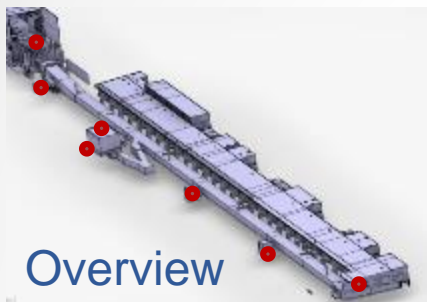
 O₂ detector – Oxigraf 4 port multiport sampling (laser diode technology)



ODH is not relevant during beam operation

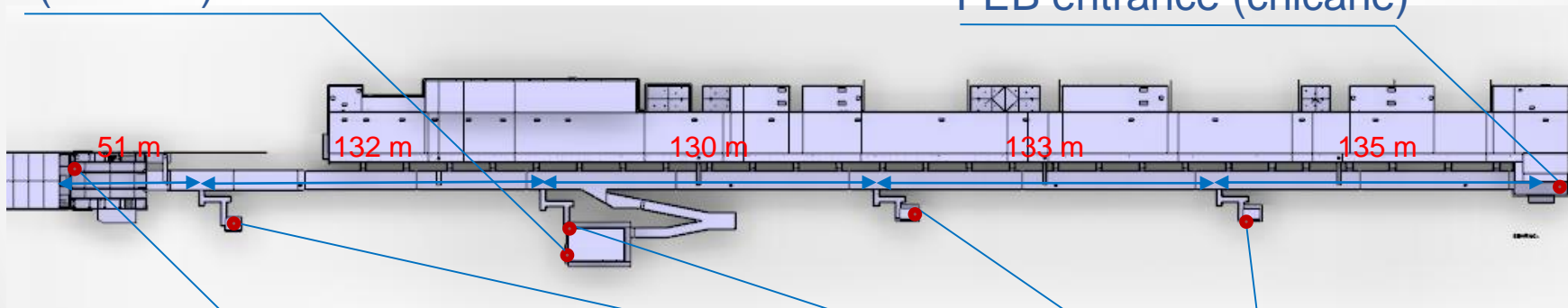
Accelerator tunnel

Layout of the ODH monitoring system



HEBT entrance (chicane)

FEB entrance (chicane)



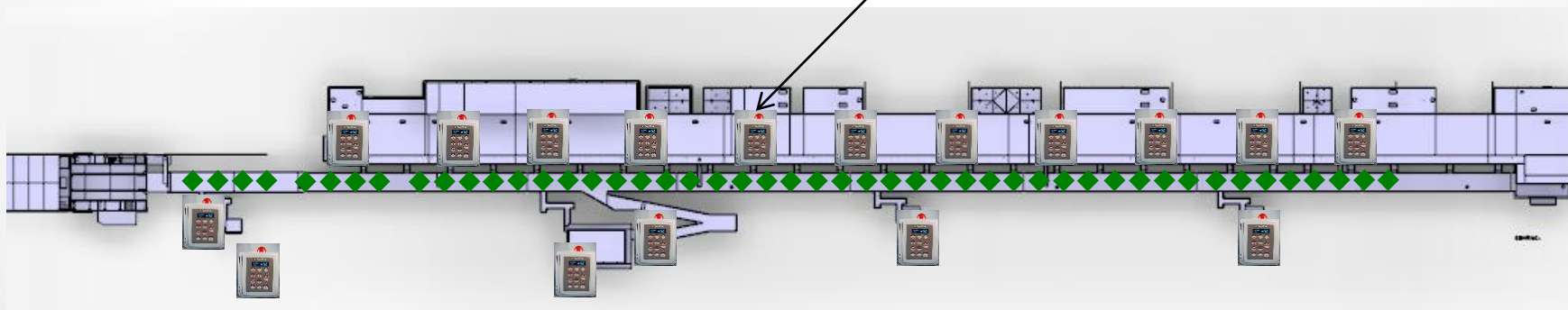
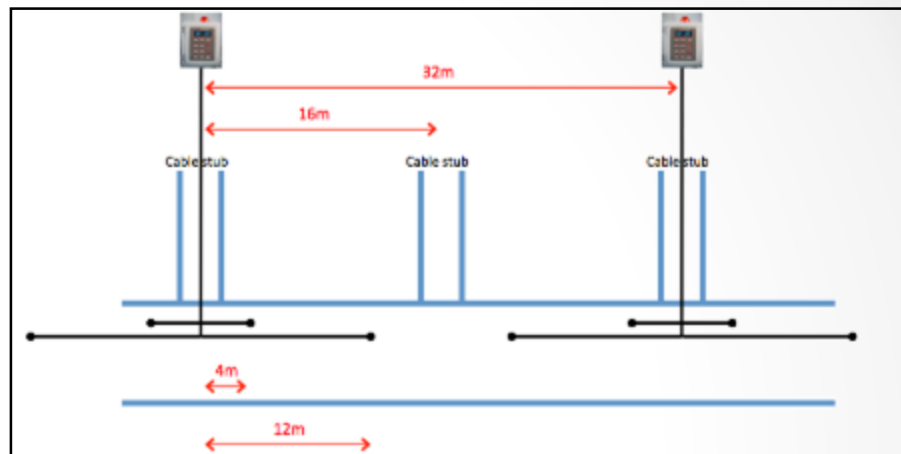
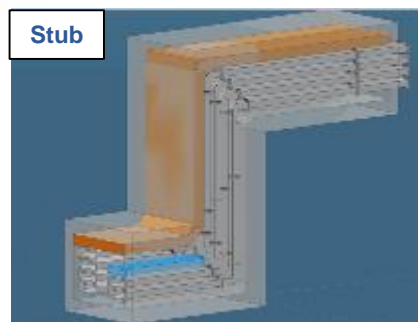
A2T egress



Emergency exits

Accelerator tunnel

Layout of the ODH monitoring system



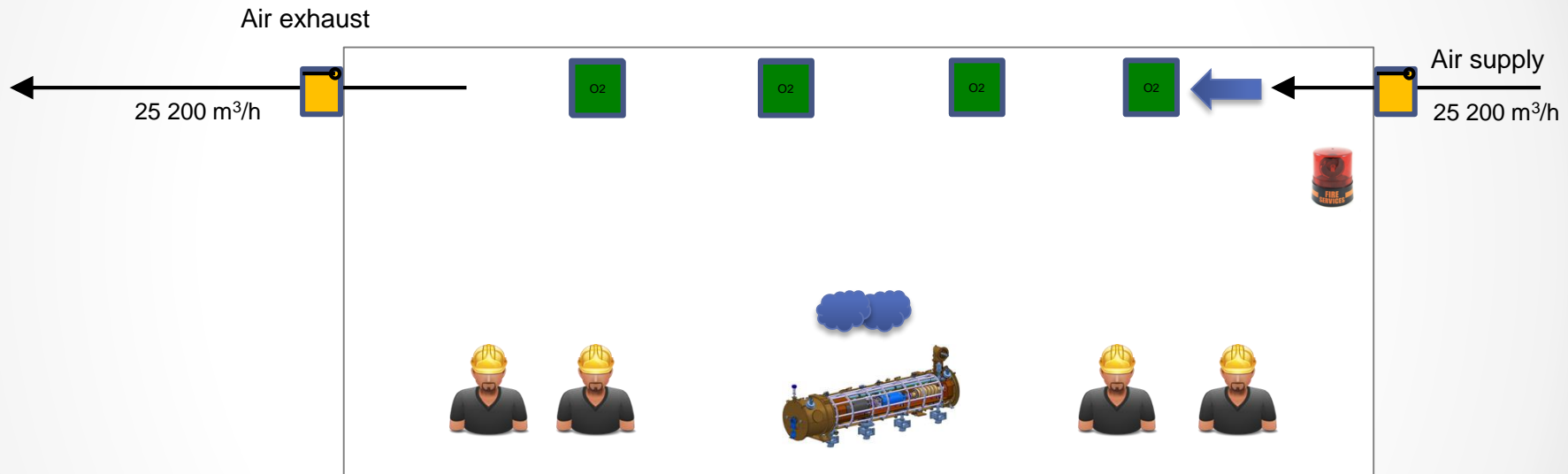
- ✓ Accelerator tunnel **14 x 4** port Oxigraf Model O2iM oxygen deficiency Monitors mounted at high level.
- ✓ Accelerator Tunnel exits and entrances **6 x 1** port Oxigraf Model O2iM oxygen deficiency Monitors mounted at high level.
- ✓ **50** Accelerator Beam Off Stations + **30** strobes and sirens.



Accelerator tunnel

Conceptual design for the air management system

≈140 hours of maintenance/year



If a Helium discharge occurs, **it will be partly handled by the ventilation system...**

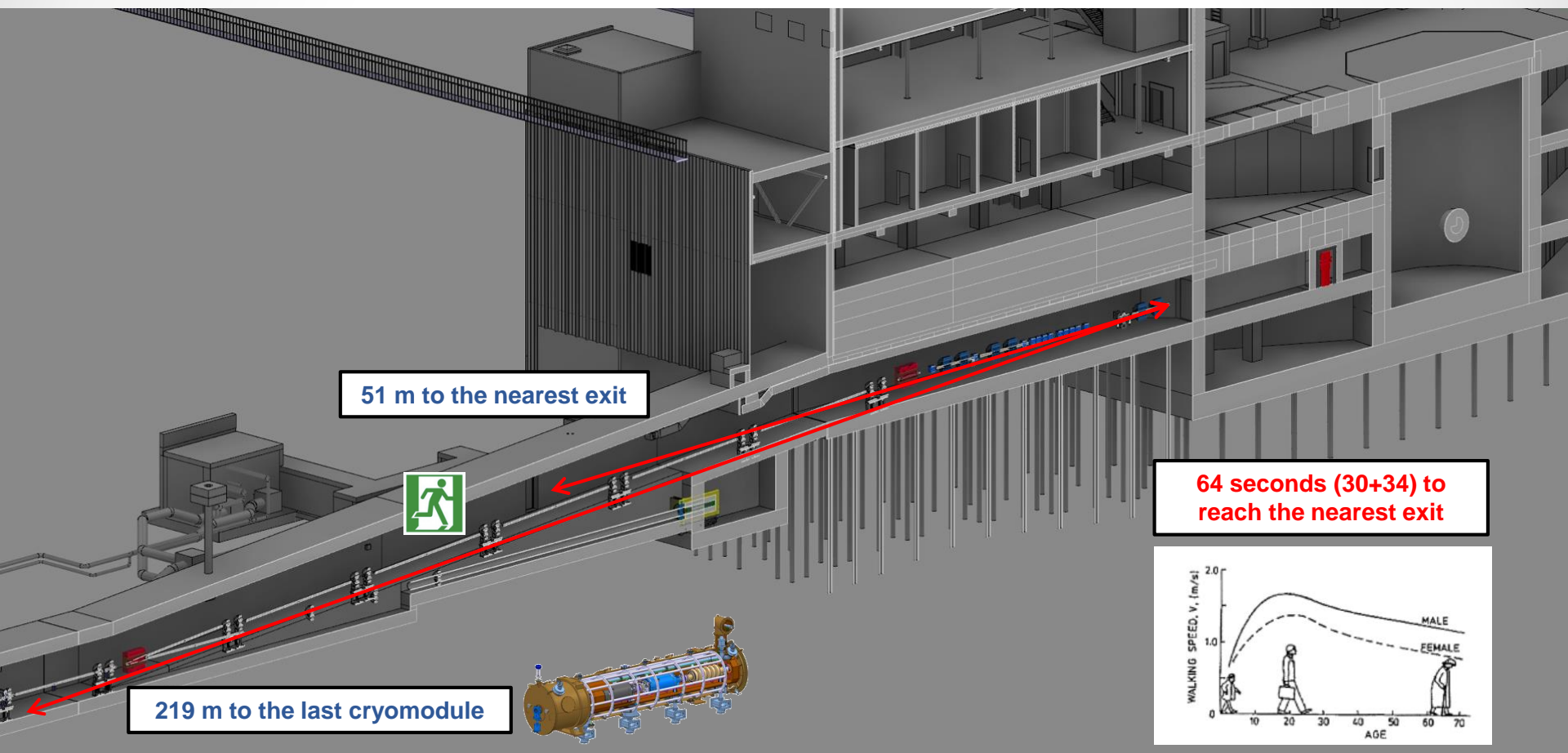


Lesson learnt from CERN's visit (2 July 2015)

→ air speed from the ventilation **should not exceed 1 m.s⁻¹** to facilitate evacuation

Accelerator tunnel

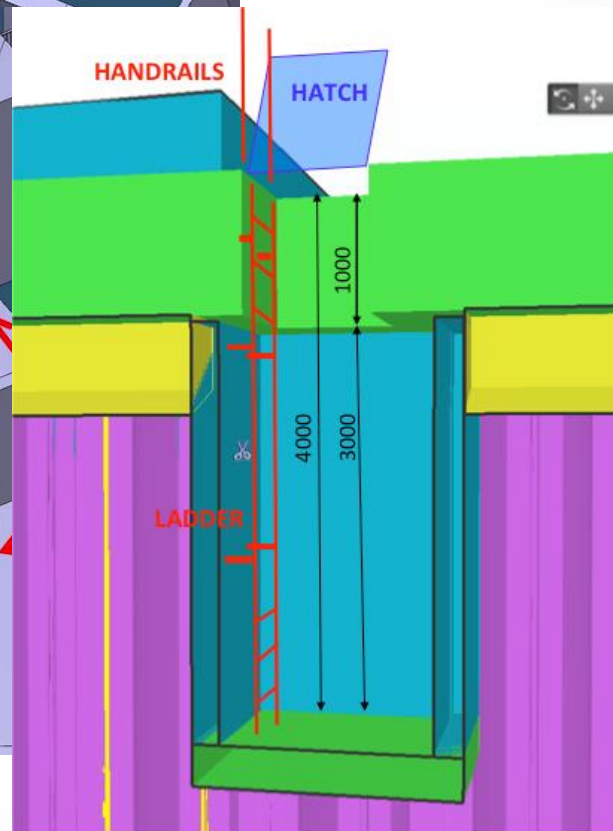
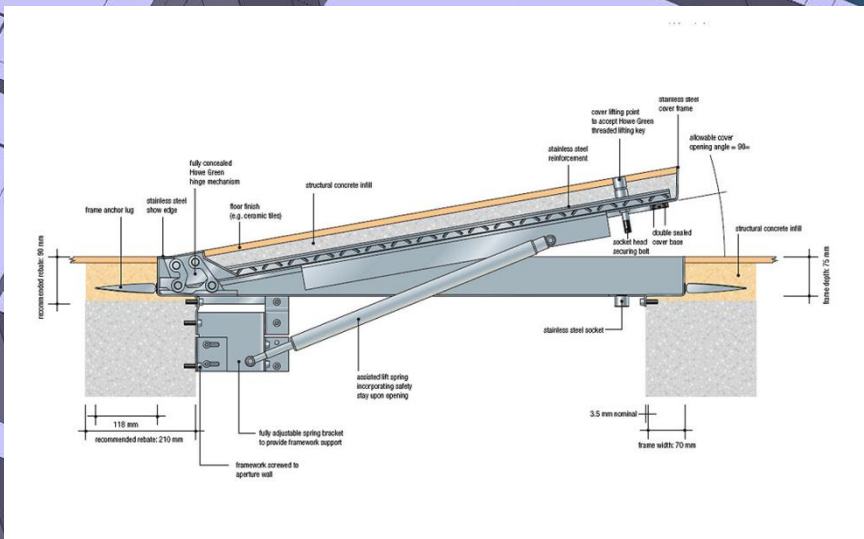
Safety issue in the A2T area



Accelerator tunnel

Safety issue in the A2T area

Decision taken on December 7th to implement the safety hatch in the A2T area



ACKNOWLEDGEMENT : N.GAZIS

Accelerator tunnel

CFD simulations

Failure scenarios considered (during access)

Scenario 1

Rupture of the power coupler's window or beam line



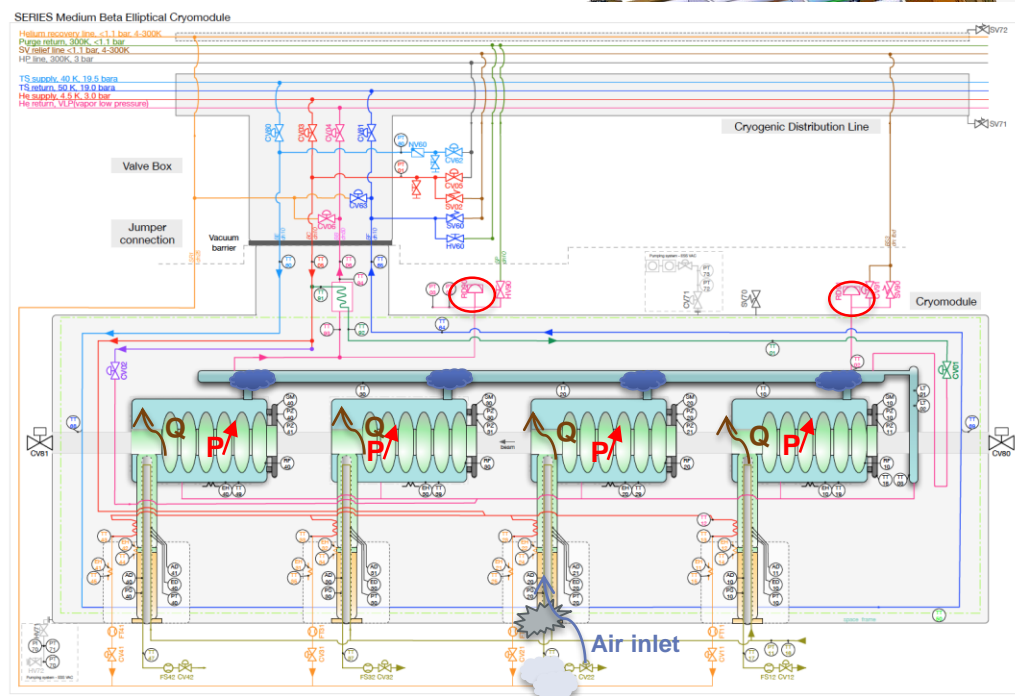
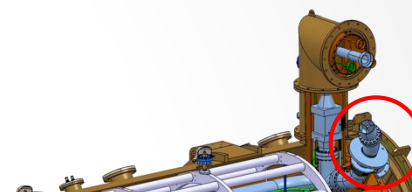
Loss of the content of 1 High- β^* cryomodule (28,4 kg at 2 K and 2. bara)



Discharge of GHe through the 2 rupture disks located on the LHe line (1,9 s)



Max. mass flow rate = 15,2 kg.s⁻¹



*the loss of 2 High-Beta cryomodules has not been considered thanks to the CLOSE position of the gate valves in-between cryomodules during access

Accelerator tunnel

CFD simulations

Failure scenarios considered (during access)

Scenario 2

Rupture of the insulation vacuum vessel of 1 High- β cryomodule



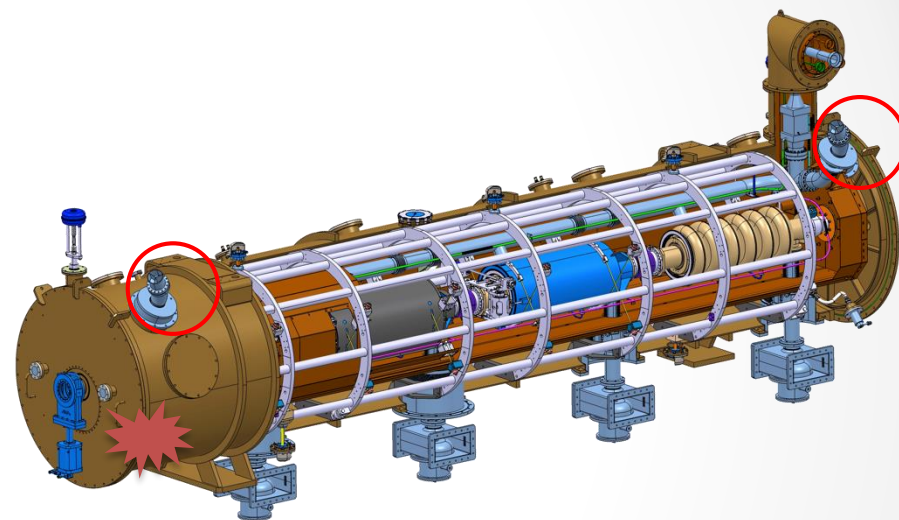
Loss of the content of 1 High- β * cryomodule (28,4 kg at 2 K and 2.04 bara)



Discharge of GHe through the 2 rupture disks located on the LHe line (11,8 s)



Max. mass flow rate = 2,4 kg/s



*the loss of 2 High-Beta cryomodules has not been considered thanks to the CLOSE position of the gate valves in-between cryomodules during access

Accelerator tunnel

CFD simulations

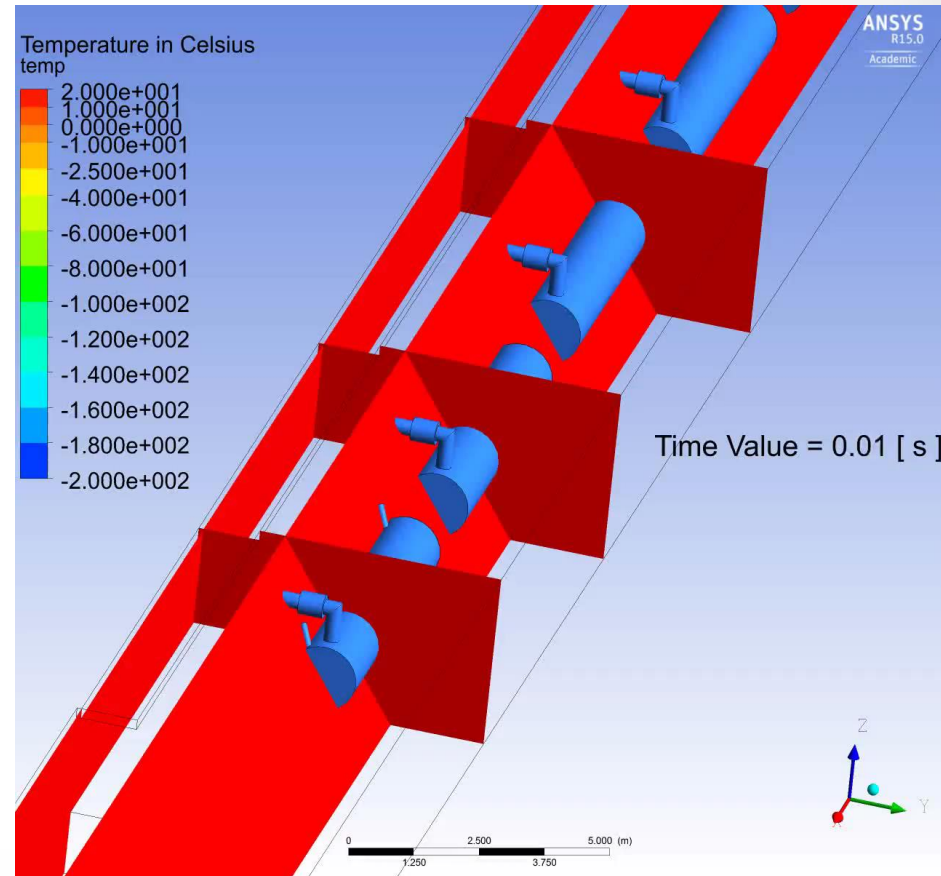
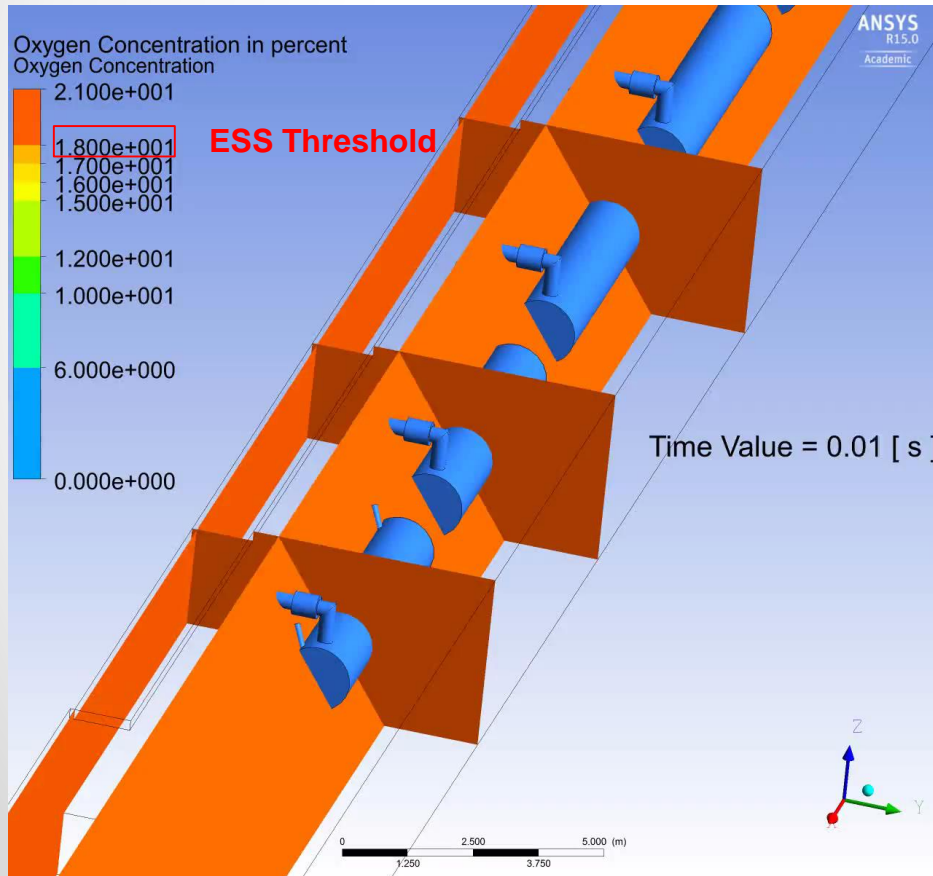
Assumptions

- GHe released at **5 K** (coldest value from the designer)
- **Constant mass flow rates** from the burst disks
- **Atmospheric pressure** in the tunnel
- **100% leak tightness** in the tunnel
- Walls and equipment held at a constant temperature of **22.5 °C**
- Constantly forced ventilation (about **0.3 – 0.4 m.s⁻¹** in the tunnel)
- **Simplified geometry**
- CDS and cryomodules installed in the **contingency space**
- **Cryogenic helium properties** from the *NIST Chemistry WebBook*
- The simulation software **CFX** (ANSYS) is used

Accelerator tunnel

CFD simulations

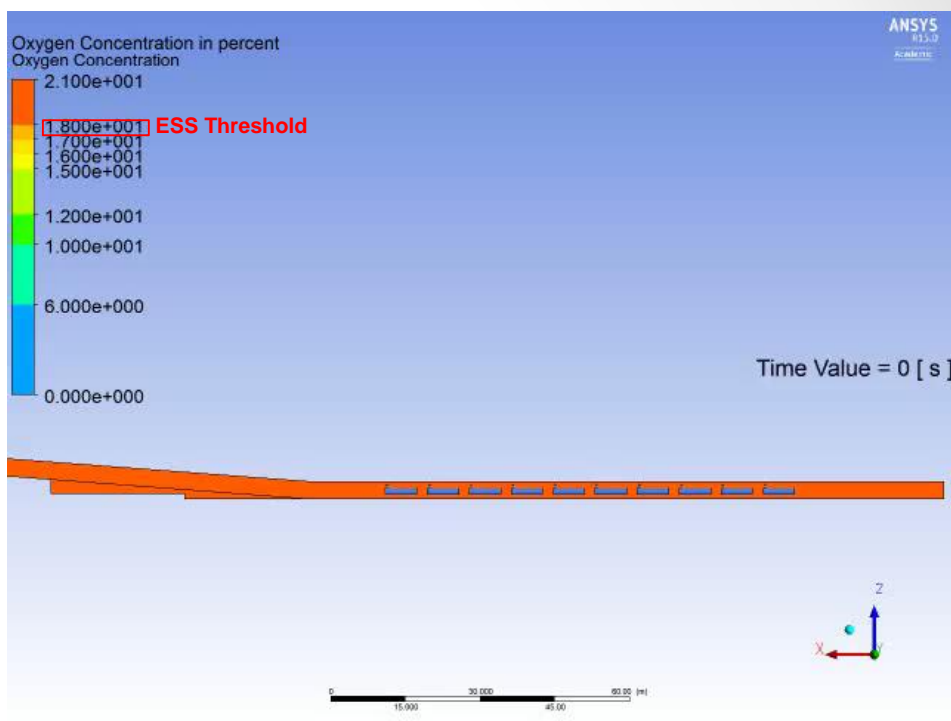
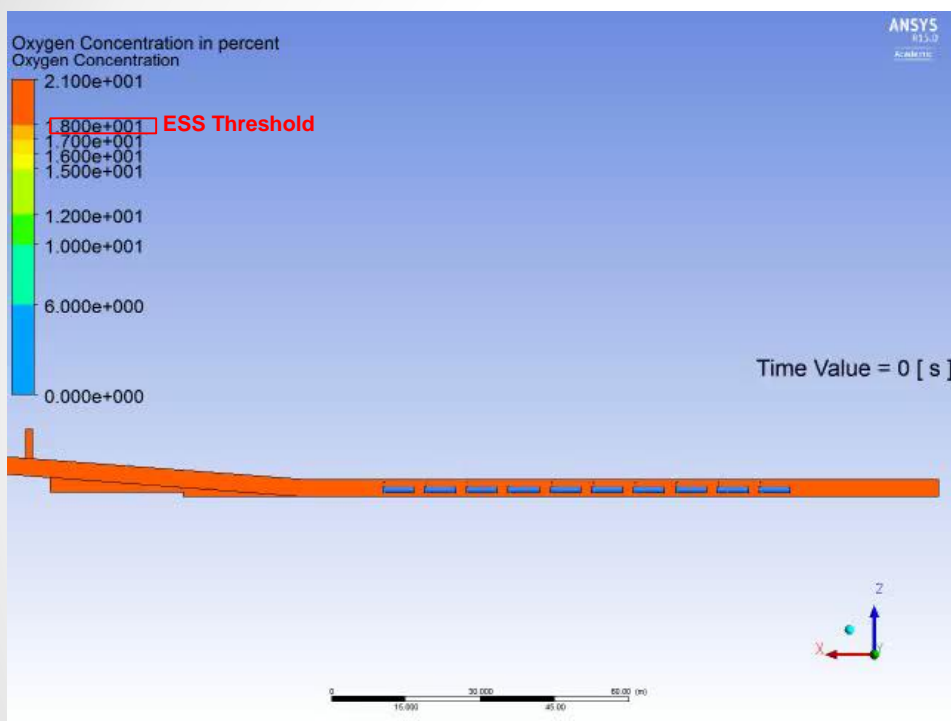
Scenario 1 (15.2 kg.s⁻¹ during 2 s) – rupture of the beam line



Accelerator tunnel

CFD simulations

Scenario 2 (2.4 kg.s⁻¹ during 2 s) – rupture of the vacuum vessel of a High-β



Mass flow rate: 2,4 kg.s⁻¹
Volume: 28,8 kg
Leak duration: 12 s
Location: contingency space (A2T area)
Ventilation mode: ON – 25 200 m³/h

Mass flow rate: 2,4 kg.s⁻¹
Volume: 28,8 kg
Leak duration: 12 s
Location: contingency space (A2T area)
Ventilation mode: OFF

ESS Cryogenic Safety Workshop February 10-11, 2016

Highlights

Objective: share experience and technical expertise with cryogenic and safety experts regarding cryogenic safety in accelerator tunnels

7 institutes represented

2-days workshop

10 recommendations addressed to ESS

Presentations available here: <https://indico.esss.lu.se/event/438/>



ESS Cryomodules Safety Review June 9, 2016

Highlights

Objective: evaluate the design of the Spoke and Elliptical cryomodules against failures and risks to humans and equipment during operation



*The design of the collector is however still in a preliminary state, and it is was not possible for the committee to review the solution in depth. **The committee supports the continuation of this work with high priority, as well as the evaluation of the impact of this system on the cryomodule design and integration aspects in the tunnel.***

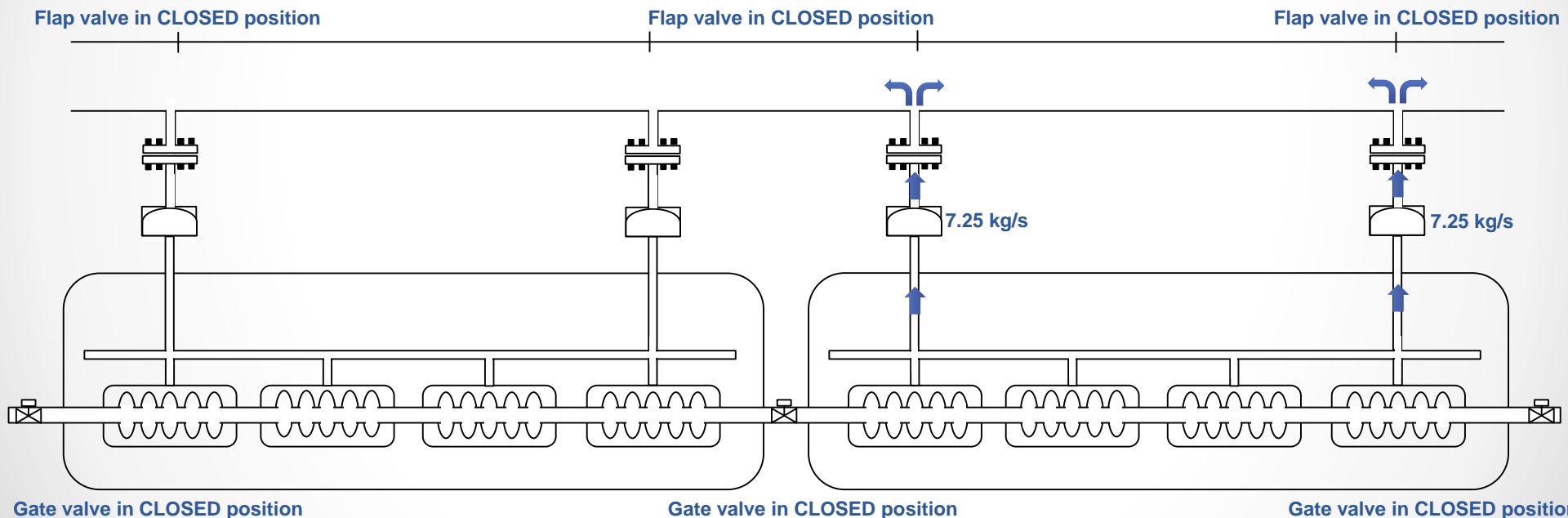
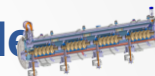
Presentations and report from the committee available here: <https://indico.esss.lu.se/event/542/>

Accelerator tunnel

Conceptual design of the Helium collection header

Access Mode

Most credible accidental scenario: loss of one High- β cryomodule

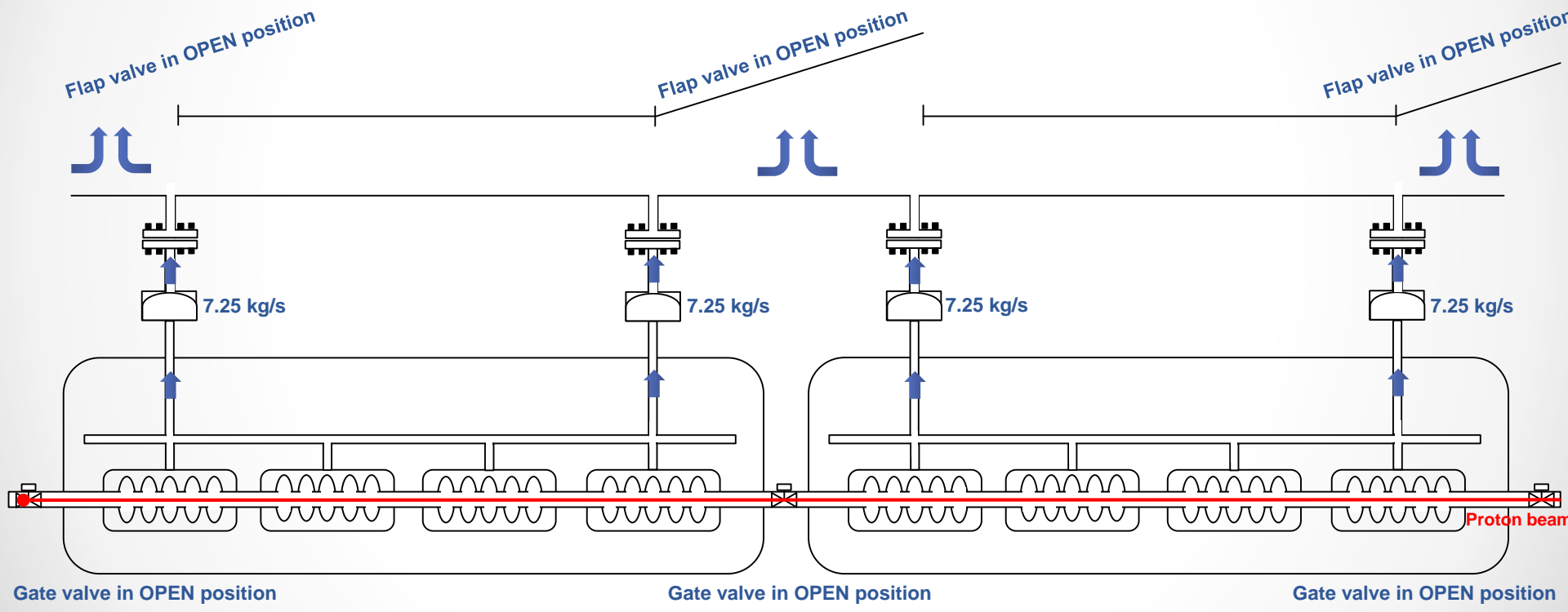


Accelerator tunnel

Conceptual design of the Helium collection header

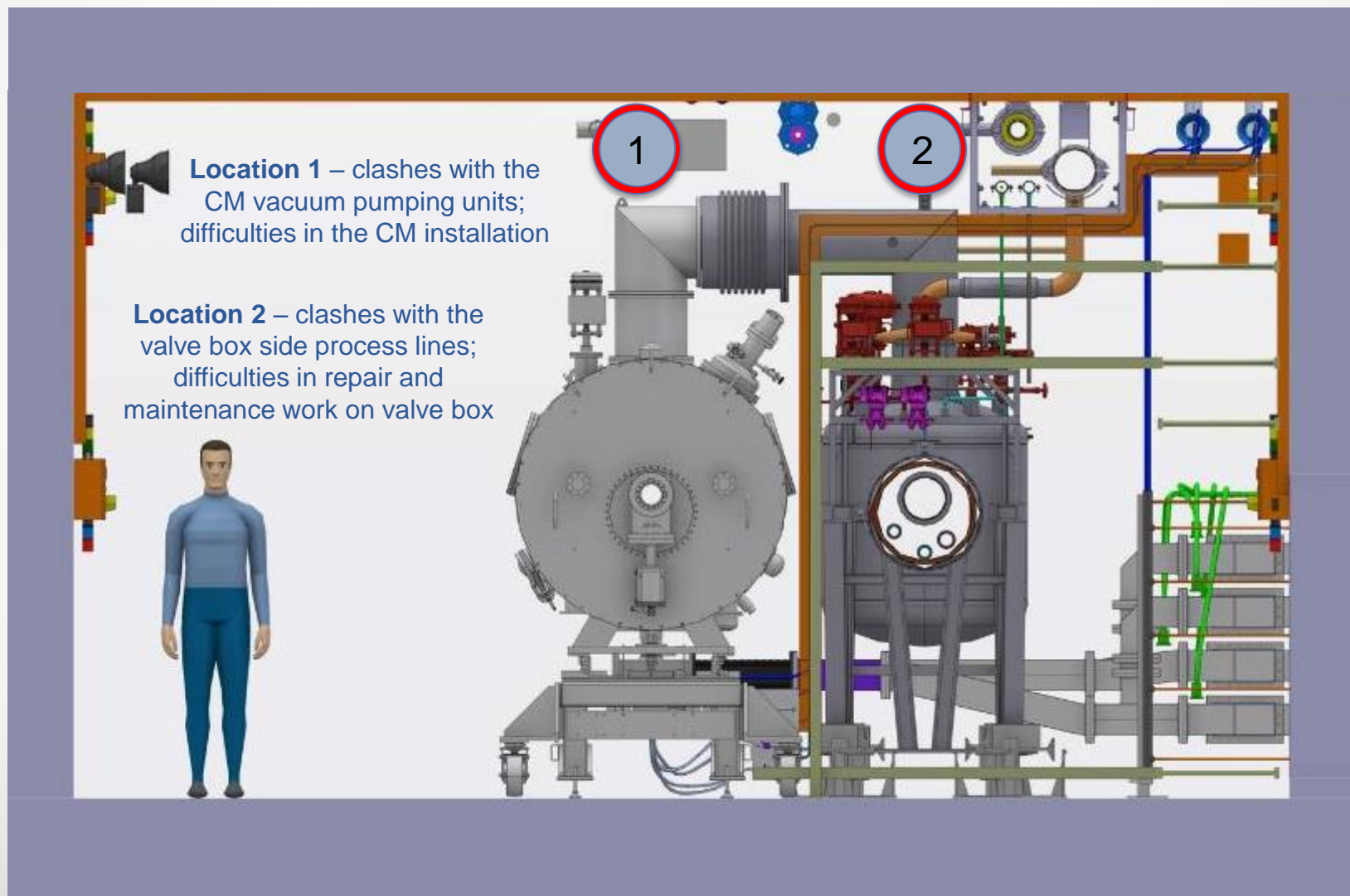
Beam Mode

Most credible accidental scenario: loss of six High-β cryomodules



Accelerator tunnel

Conceptual design of the Helium collection header



Accelerator tunnel

Conceptual design of the Helium collection header

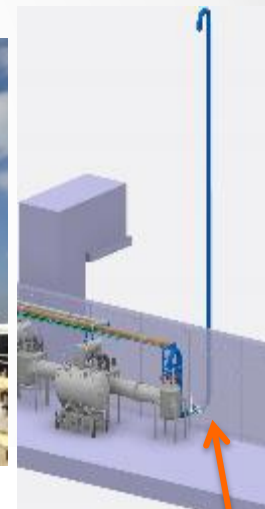
Cold box room vent line



Total length of the collector < 400 m



CDS vent line

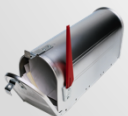


Accelerator tunnel

310 m

Design report expected for mid-November

ANY QUESTIONS



Contact: duy.phan@esss.se

BACK-UP SLIDES