



Summary of Work Package 8- Power distribution

Marc Weber

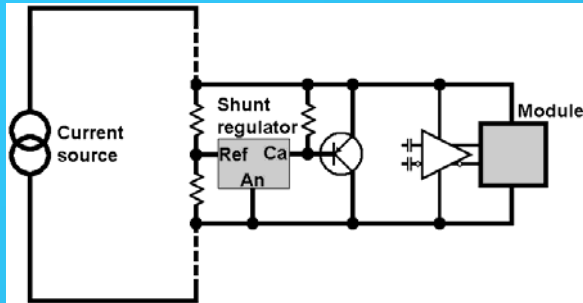


- Pace of power distribution R&D remains very high
- Lot's of progress, but technical challenges are huge
(only a fraction of results can be mentioned)
- Healthy competition between serial powering and DC-DC conversion
- Good communication, many informal meetings, free exchange of information between WP8 members and wider powering community
- Many in depth talks on next Tuesday within ACES 2009

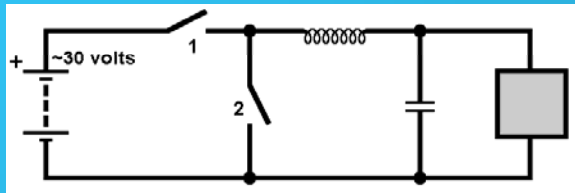
How to get the power in ?

reduce current through power cables by

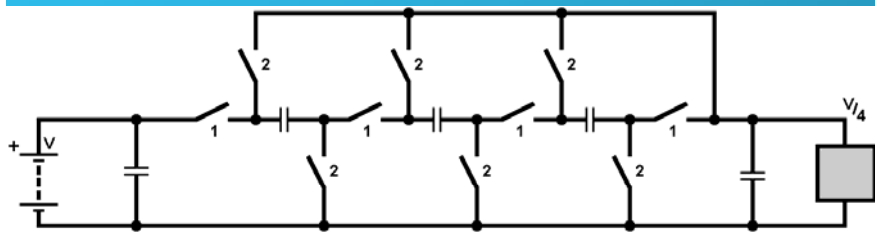
a) "recycling" of current (SP) oder b) "high-voltage power transmission (DC-DC)



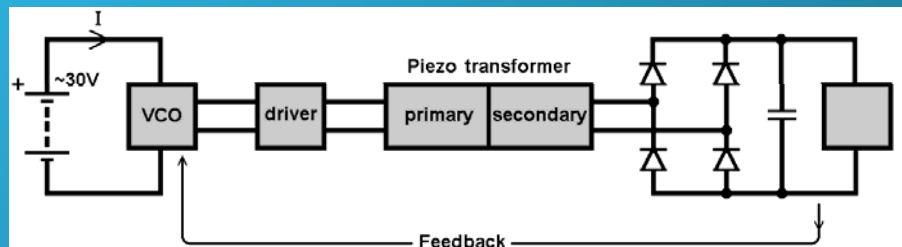
Serial powering



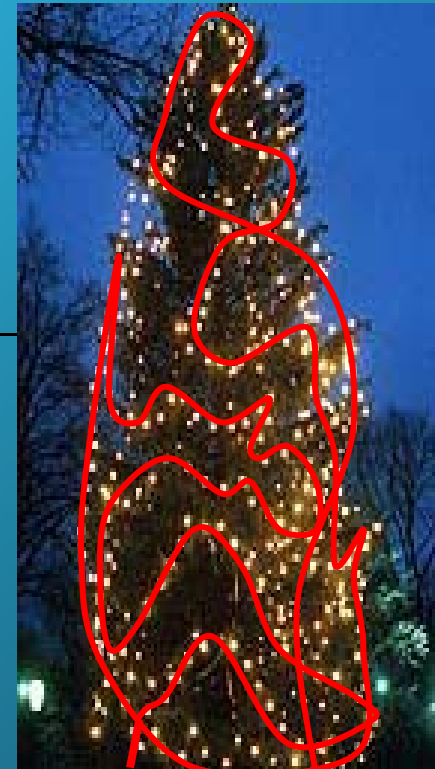
DC-DC buck converter



DC-DC charge pump



Piezo transformer



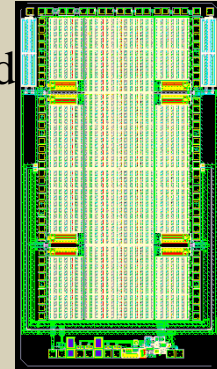
Power supply

Some highlights of DC-DC conversion R&D

- Progress on **radiation-hard technologies**
- Lot's of progress on **DC-DC topology choices** and **converter design**
- Convergence on **Two-stage conversion scheme**
- **Custom air-coil inductors with PCB technology**
- **Integrated DC-DC charge pumps**
- Wealth of **test results with large-scale silicon detectors**

Semiconductor technology (1)

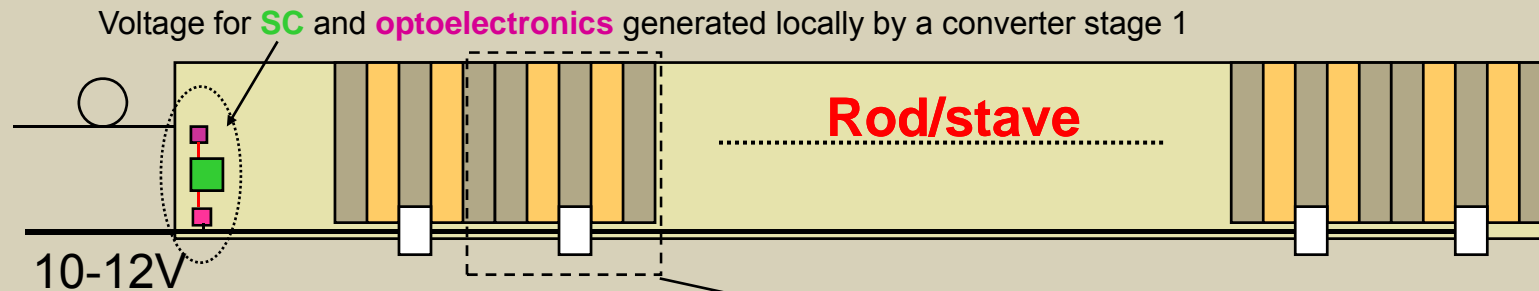
- The converter requires the use of a technology offering both low-voltage and high-voltage (15-20V) transistors
- Properties of high-voltage transistors largely determine converter's performance
 - Need for small R_{on} , and small gate capacitance (especially C_{gd}) for given R_{on} !
- Survey of available options covered 5 technologies
- Best results with 0.25 μ m SGB25V GOD technology from IHP



Prototype in 0.35 μ m

Tech Node (μ m)	Trans type	Max Vds (V)	Vgs (V)	Tox (nm)	$R_{on} \cdot \mu$ m (k Ω m \cdot μ m)	Status
0.35	Lateral	14	3.5	7	8	Tested
	Vertical	80	3.5	7	33	
0.18	Lateral	20	5.5	12	4.75	Tested
0.13	Lateral	20	4.8	8.5	7	Tested
0.25	Lateral	20	2.5	5	4-5	Tested
0.18	Lateral	20	1.8	4.5	9.3	First MPW April 09

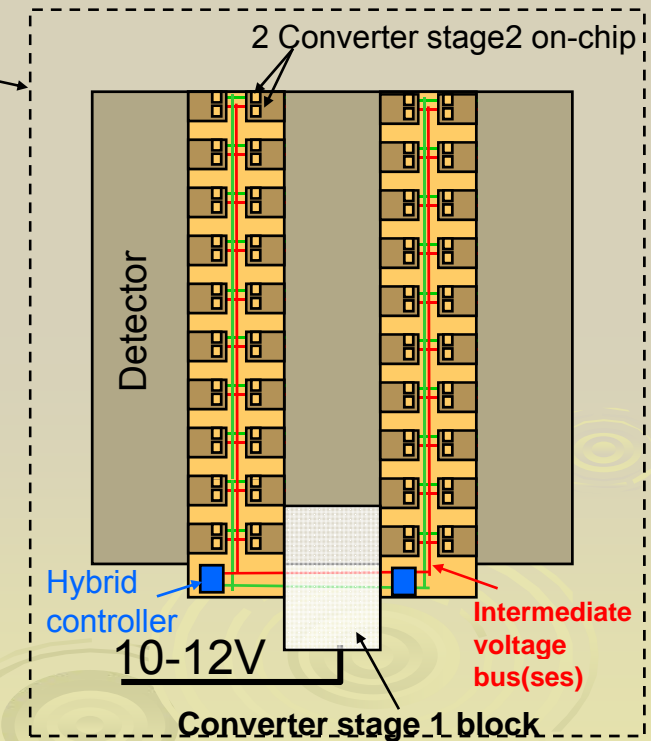
Proposed distribution scheme (ATLAS Short Strip concept)



Scheme based on 2 conversion stations:
 Stage 1 at the module level
 Stage 2 on-chip

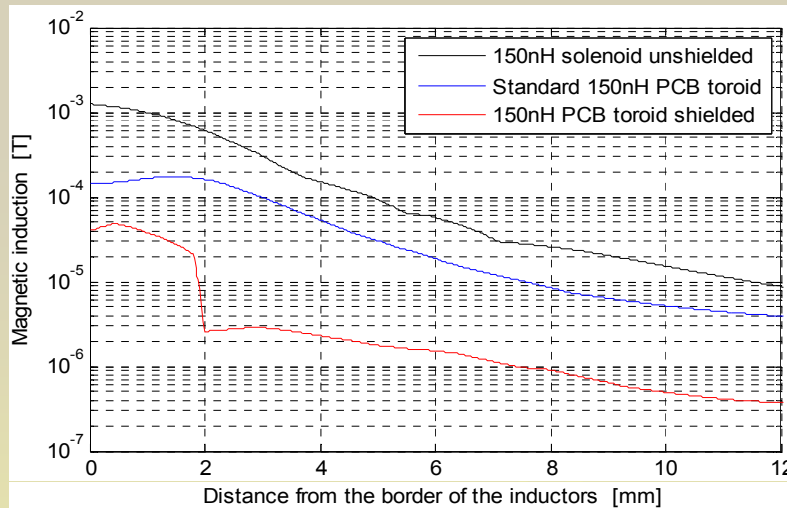
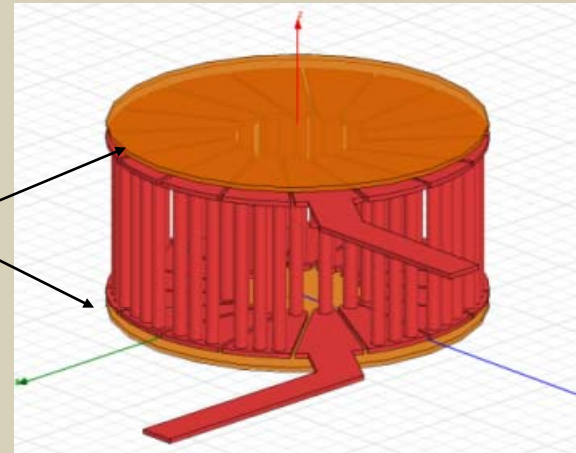
Summary of features

- Modular approach, very flexible – building blocks can be custom assembled following system requirements
- Each module turned on-off independently by SC
- Each FE chip turned on-off independently by HC
- Easy, gradual detector turn on procedure
- Conventional grounding scheme
- Conventional detector powering
- Very efficient to provide only required power to every system component, at appropriate voltage



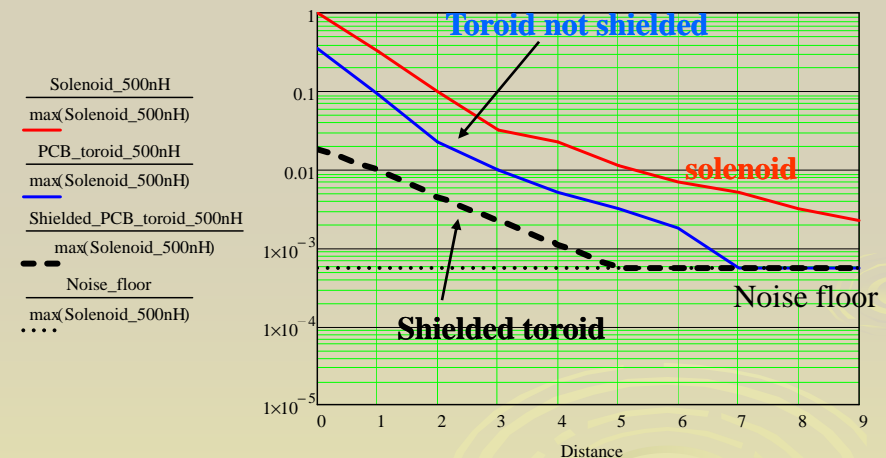
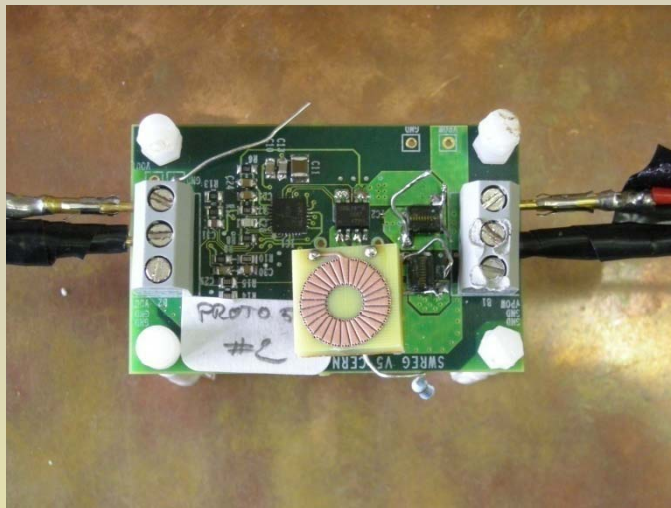
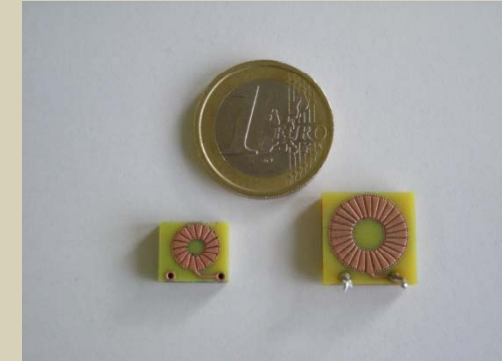
“Optimized” PCB toroid (1)

- Custom design exploiting PCB technology: easy to manufacture, characteristics well reproducible
- Design can be optimized for low volume, low ESR, minimum radiated noise
- With the help of simulation tools (Ansoft Maxwell 3D and Q3D Extractor), we estimated inductance, capacitance and ESR for different designs. This guided the choice of the samples to manufacture as prototypes
- The addition of two Al layers (top, bottom) shields the parasitic radiated field efficiently



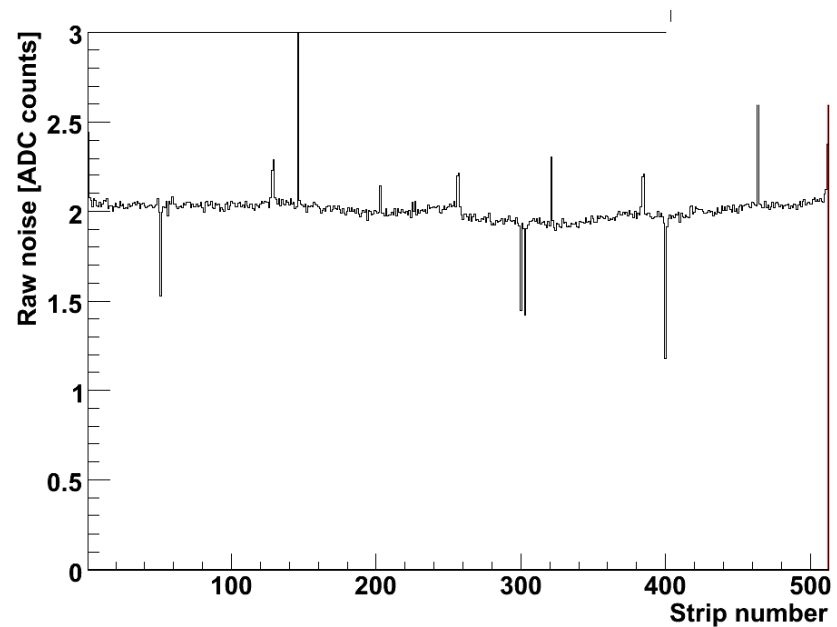
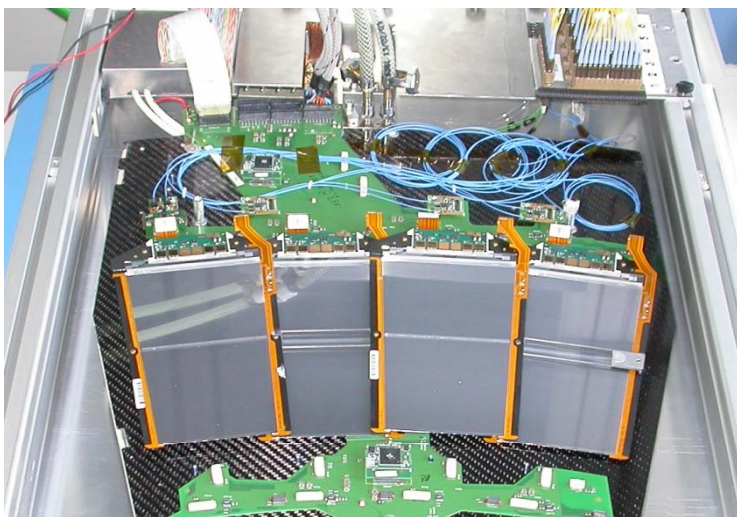
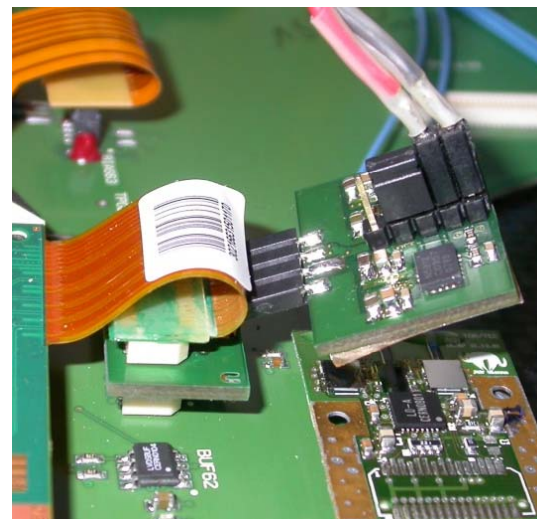
“Optimized” PCB toroid (2)

- First samples manufactured at the CERN PCB shop
- Inductance, shield efficiency, ESR in agreement with simulation
- ESR can be decreased still by 2x by “filling” the vias – this has not yet been done
- Now that the concept has been validated, we prepare for a prototype run with all the final characteristics (ESR, volume, shield material)

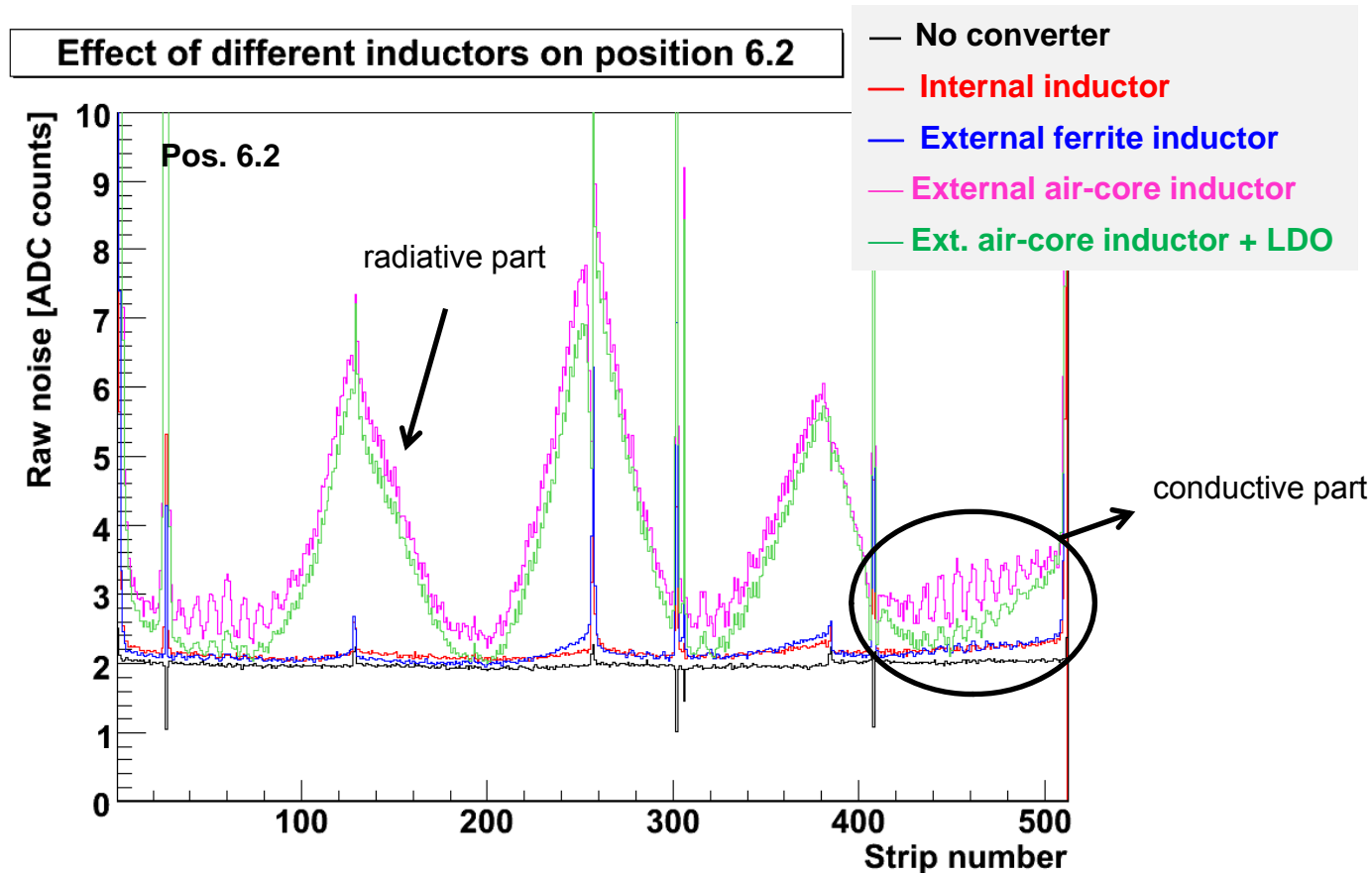


Measurement in the lab: Normalized current induced in 1 Cu loop at increasing distance from the inductor (cm)

System Test with a TEC Petal

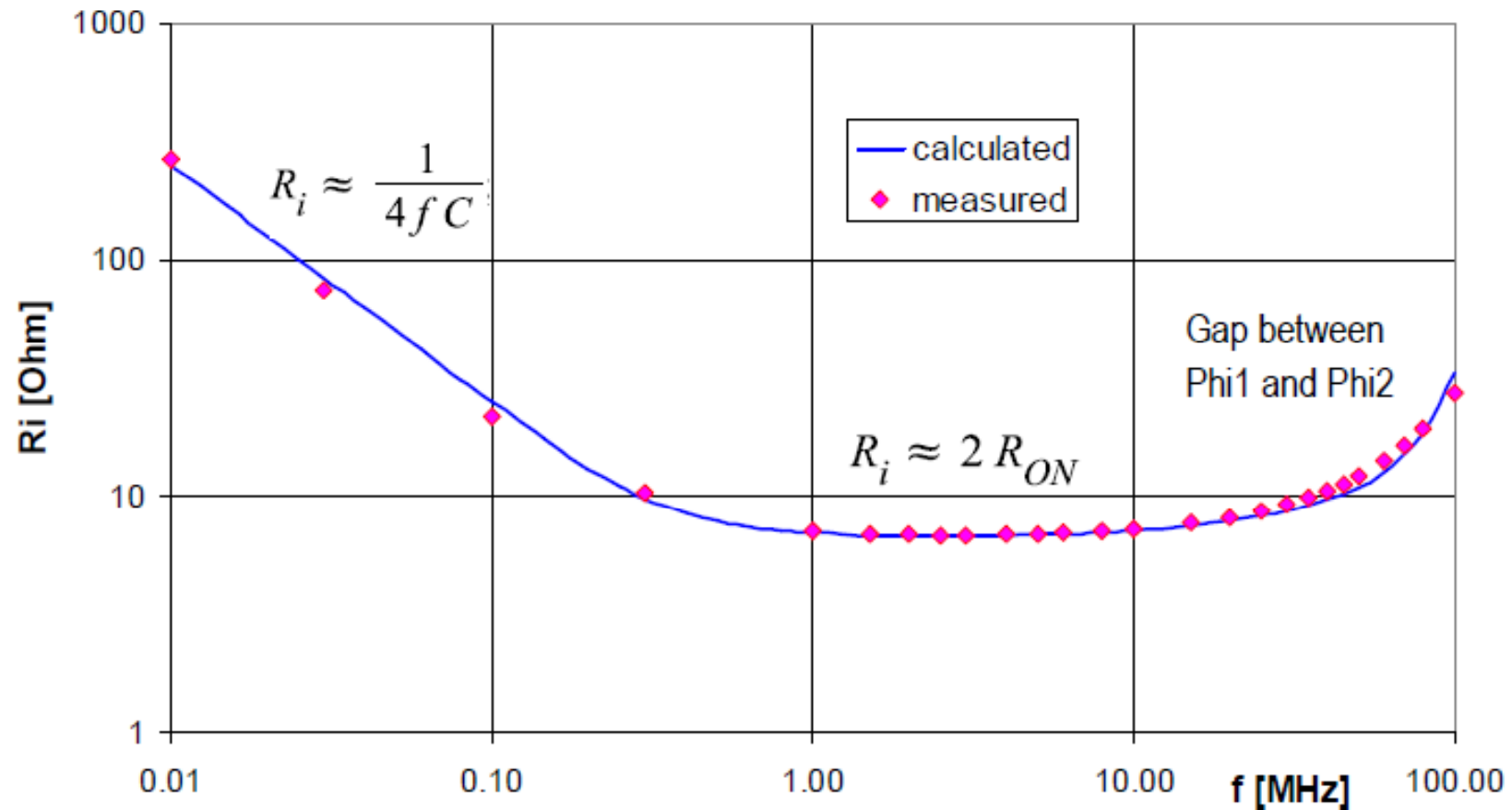


System Test with Commercial DC-DC Converters



- internal or external ferrite core inductor: 10% noise increase
- air-core inductor: huge noise increase, interference with module both radiative and conductive
- “radiative part” can be reproduced by an air core coil converter (not connected to a module) above hybrid
- “conductive part” can be reproduced by noise injection into the cables (see later)

Output Resistance



Vin = 2.5V

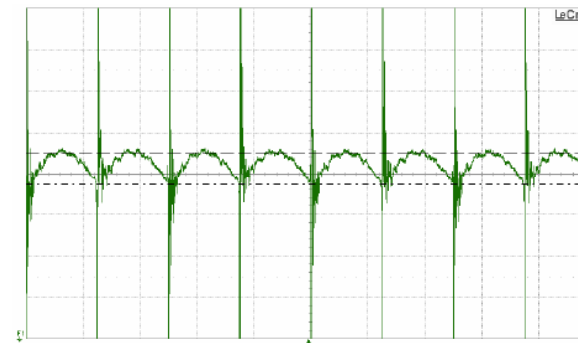
C = 100 nF

Iout = 24 mA

Ron = 3.3 Ohm

Summary

- over 80% efficiency at 20 MHz switching frequency
- better efficiency with lower R_{on} → bigger FETs
- area on chip: $10'000 \mu\text{m}^2$ ($100 \mu\text{m} \times 100 \mu\text{m}$)
- output voltage too small ($V_{out} = 1.1\text{V}$ @ $V_{in} = 2.5\text{V}$ and $I_{out} = 24 \text{mA}$)
- not adjustable, no voltage regulation



Output Voltage
200 ns/div
5 mV/div

$f = 4 \text{MHz}$; $C = 10 \text{nF}$; $I_{out} = 25 \text{mA}$; Ripple: 4mVpp (smaller at higher freq)

→ ripple is not a problem

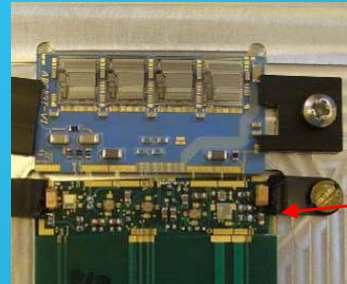
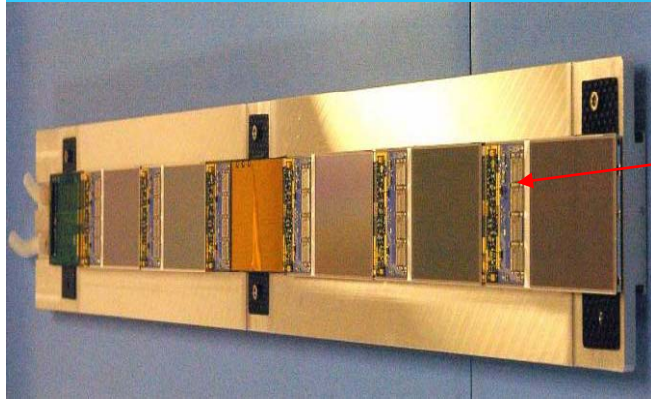
spikes ? frequency outside the sensitive frequency range

Some highlights of serial powering R&D

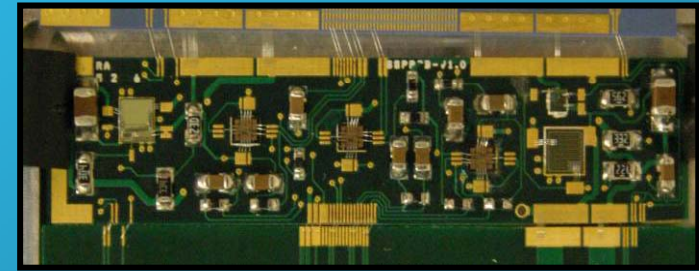
- **Serial powering supermodule system architecture**
much better understood
- **Protection schemes** are emerging
- **Custom shunt regulator circuitry** became available and seems to be functional
- **AC – LVDS coupling** of data and control and command signals much better understood

SP with commercial electronics

1) Supermodule with SP (LBNL and RAL)



BeO MCM and SP PCB



PCB with SP circuitry, 38 mm x 9 mm

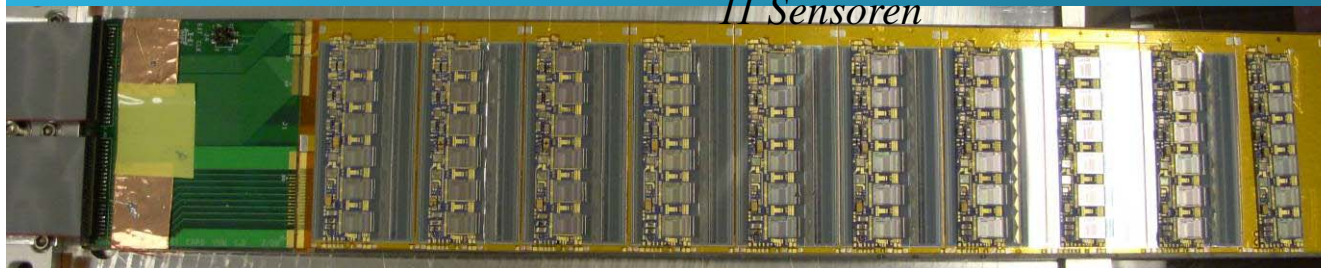
Results: 1) no noise, robust system 2) Can bias sensors with a common HV line
3) AC (Multidrop) LVDS working well

2) Large supermodule with SP

30 MCMs with SP

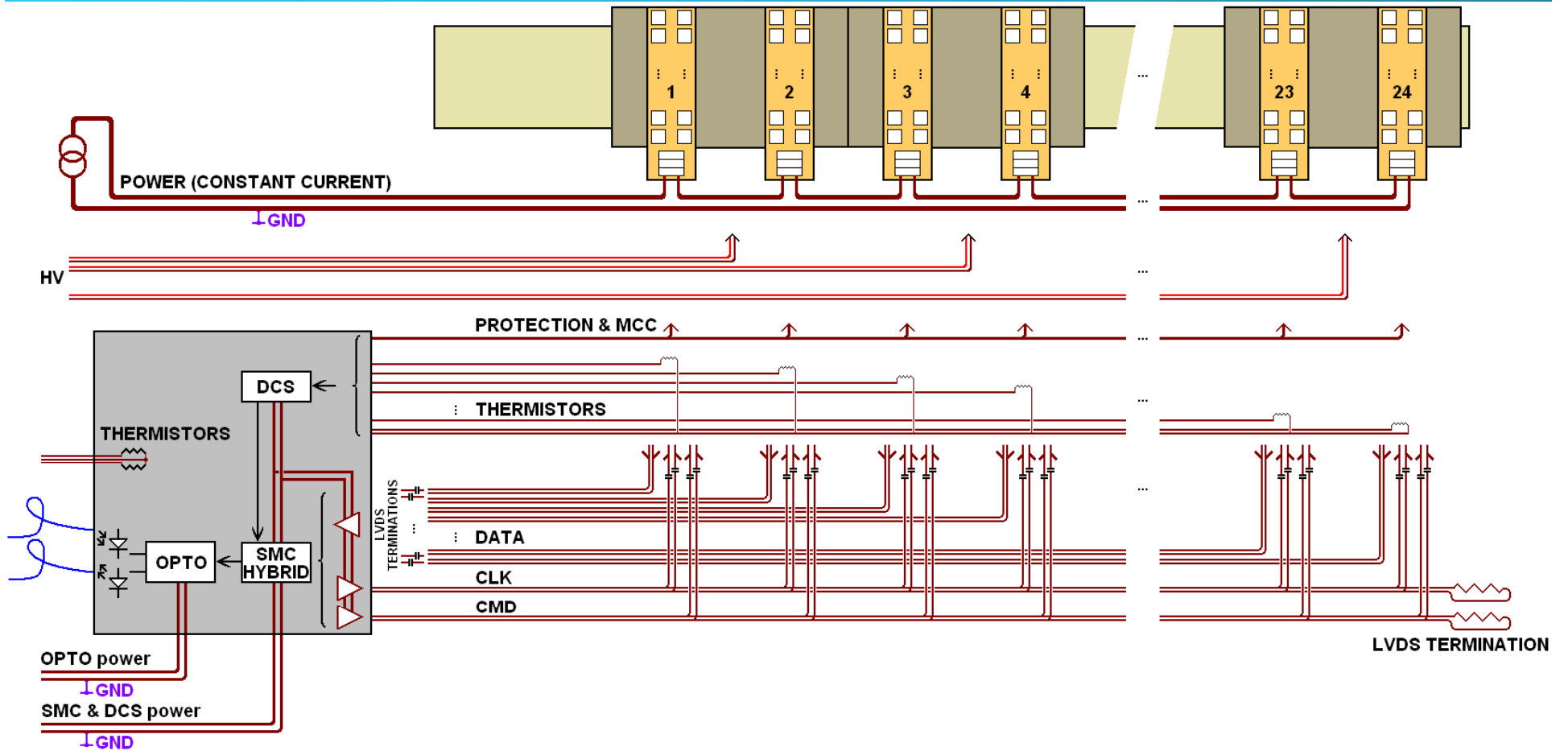
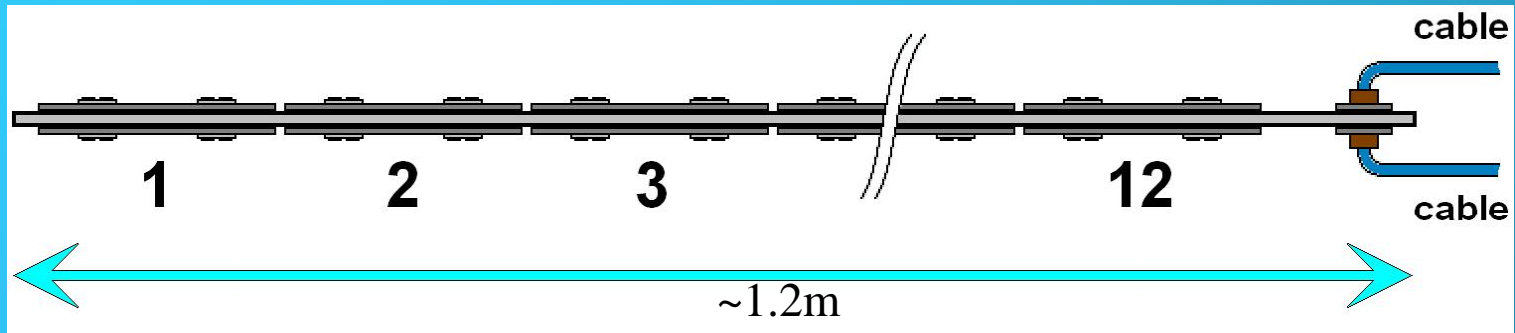


11 Sensoren



Results : 4) Long SP chain working well

Supermodule architecture

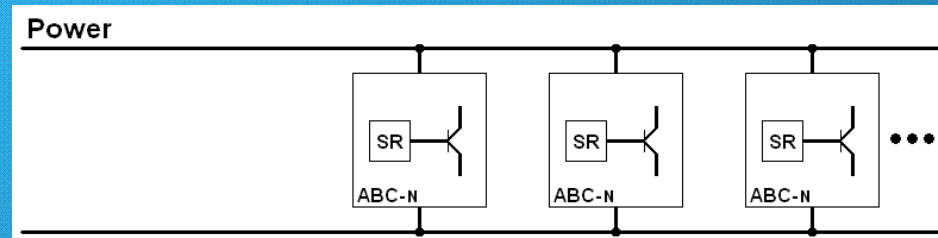


SP ASIC Design: ABC-Next and SPi

Need radiation-hard SP ASICs with small dynamic impedance. Which architecture is best?

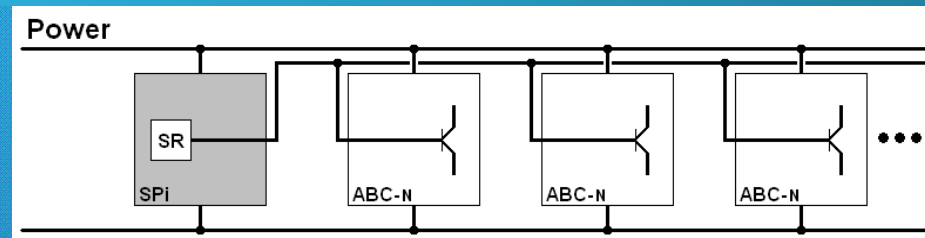
W scheme

Each ABC-N has its own shunt regulator & transistor(s)



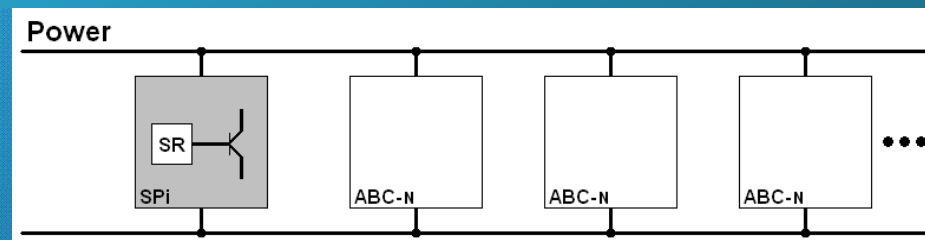
M scheme

Just one shunt regulator – Use each ABC-N transistor(s)



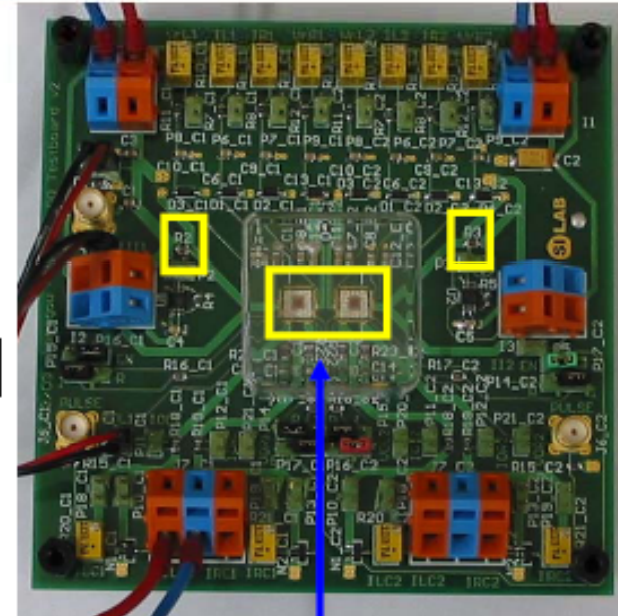
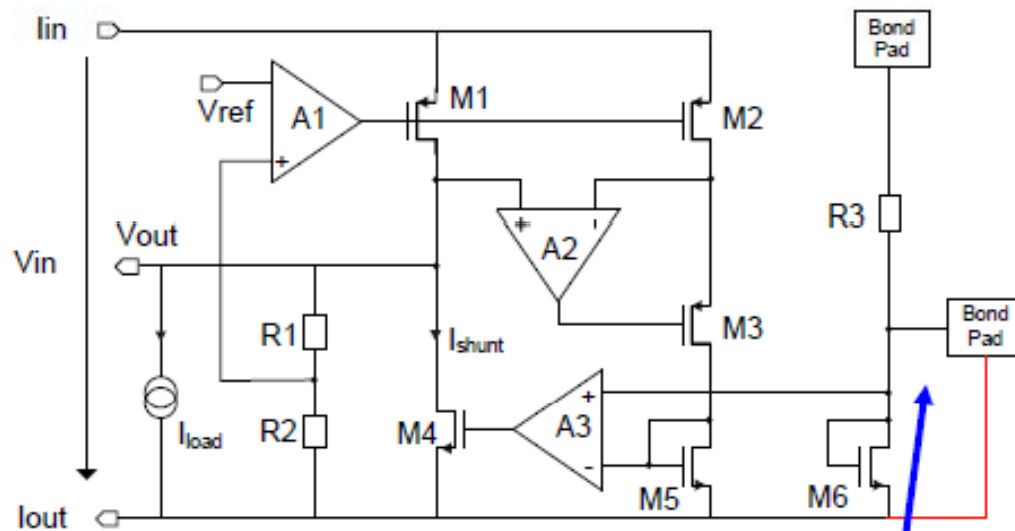
SPi scheme

Just one shunt regulator and transistor



SR = Shunt regulator
Linear regulators and other connections omitted

**New territory for particle physics.
Great interest of IC designers**

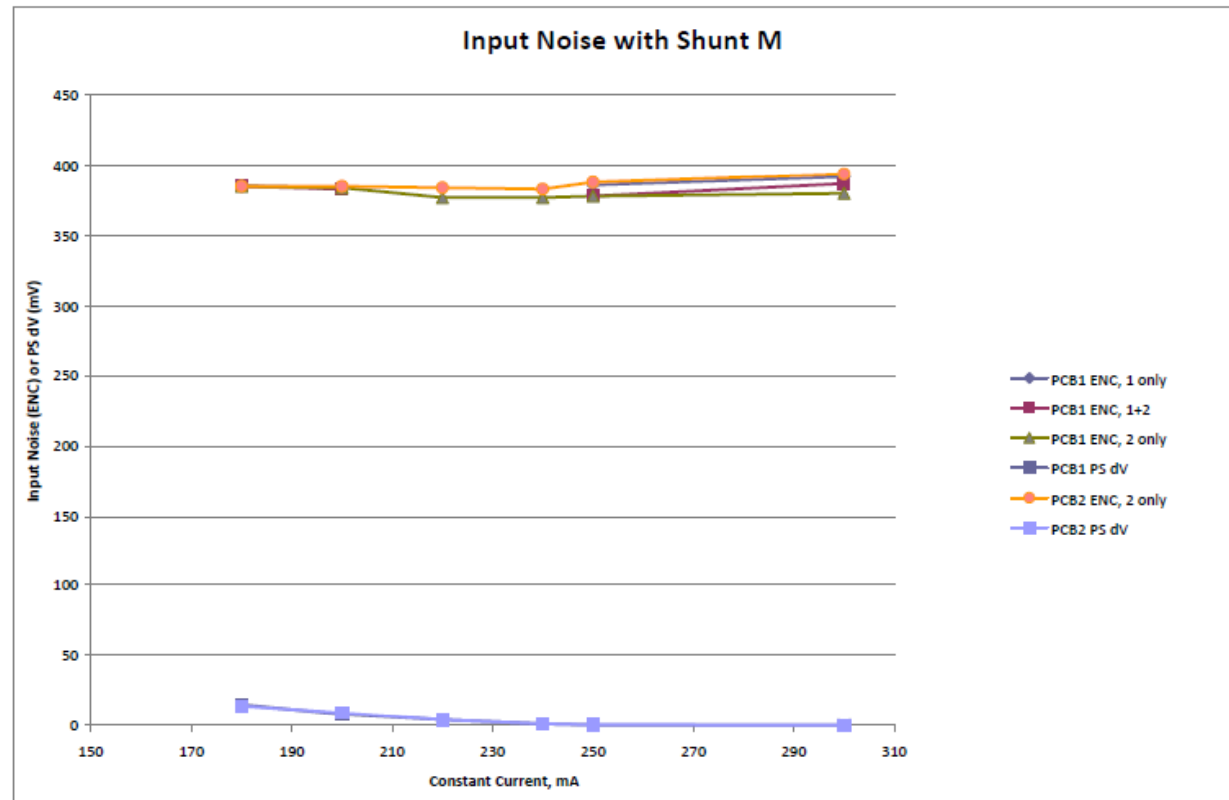
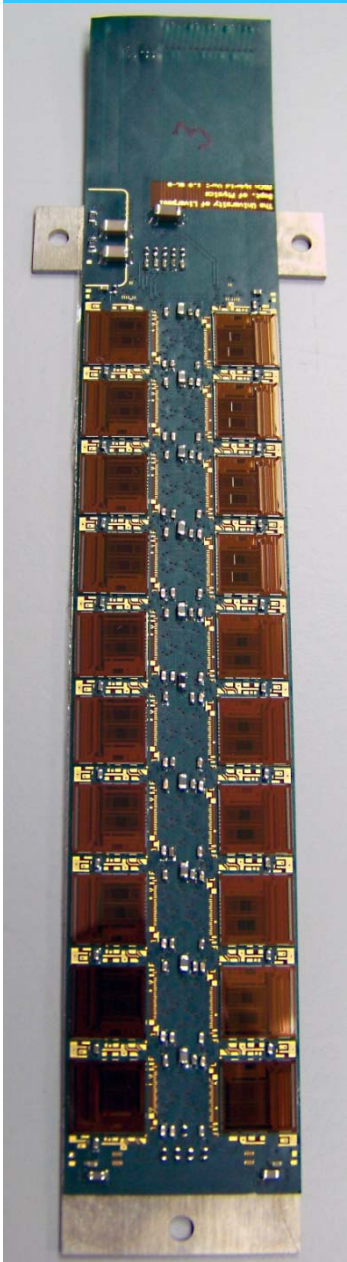


- direct measurement of shunt current distribution is not possible
→ regulators are connected in parallel on-chip
- shunt capability can be switched-off by defining zero reference current
→ use of special dedicated bond pads
- two SHULDO test chips connected in parallel on PCB level
→ each test chips has one operational regulator and one regulator switched-off
- shunt current is measured by 10 mOhm series resistors & instrumentation opamp

ABC-Next with SP blocks for W and M scheme

Both schemes are being evaluated. Preliminary tests on single chips (rather than hybrid) are looking good.

Chips and SP blocks are functional and noise performance is OK



SPi is stand-alone IC with all relevant SP elements:

1) Shunt regulator 2) Shunt transistor 3) LVDS ports

plus - Shunt current sensing ADC

- Over-current protection

- Linear regulators

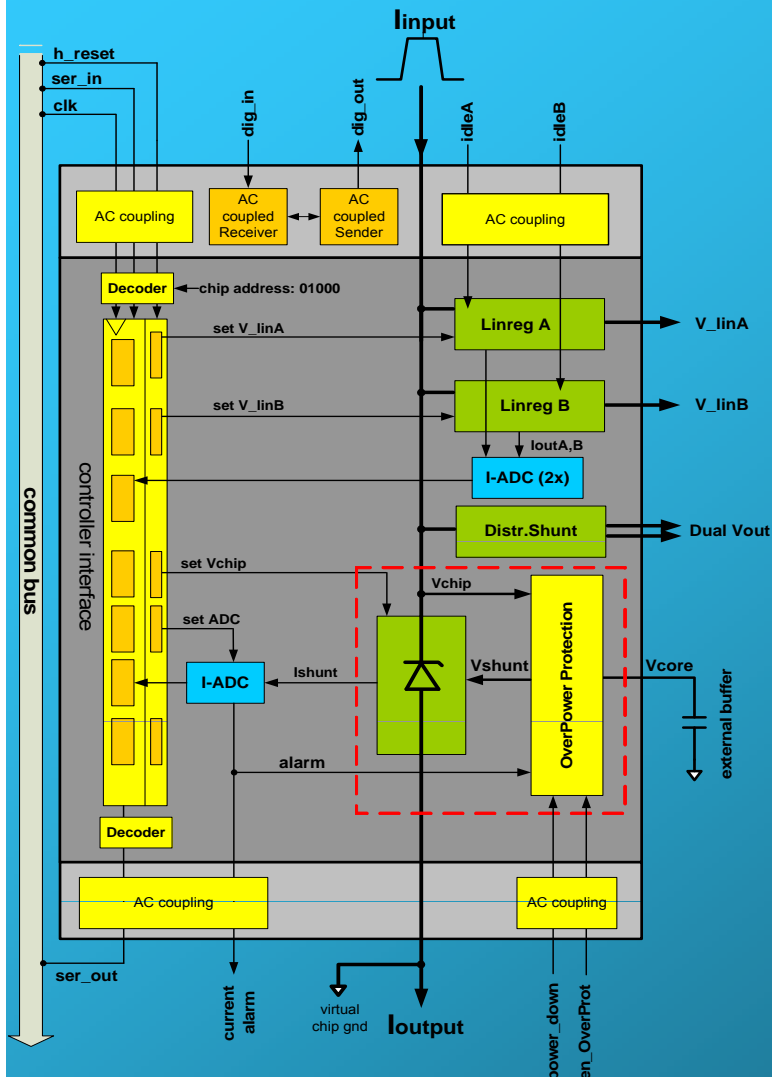
suitable for 1.2 V to 2.5 V

technology: TSMC 0.25 μ m CMOS

area: ~ 14 mm²

max. current through shunt transistor: 1-3 A

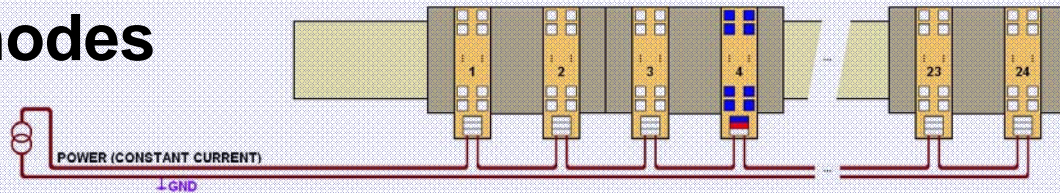
SPi makes SP straightforward.



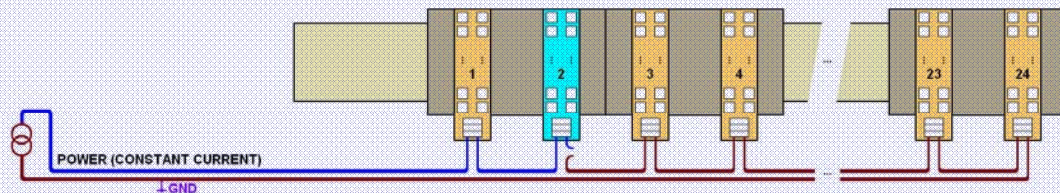
Why add protection?

Power failure modes

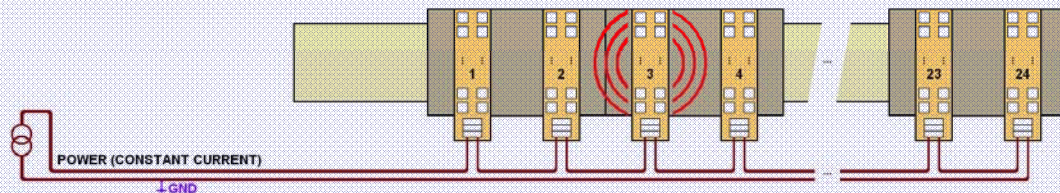
Open circuit module



Wire bonding failure

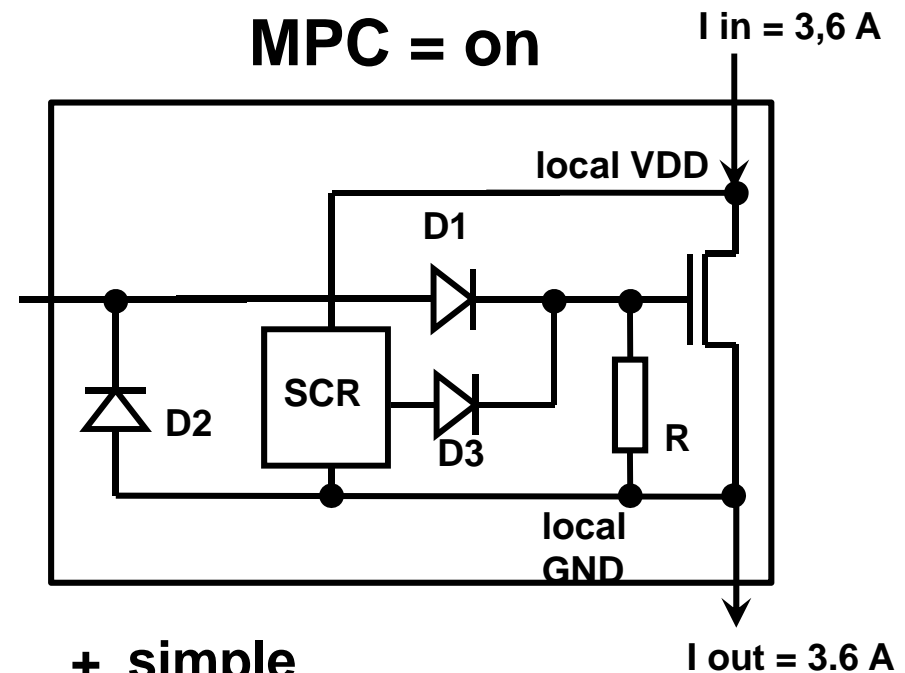
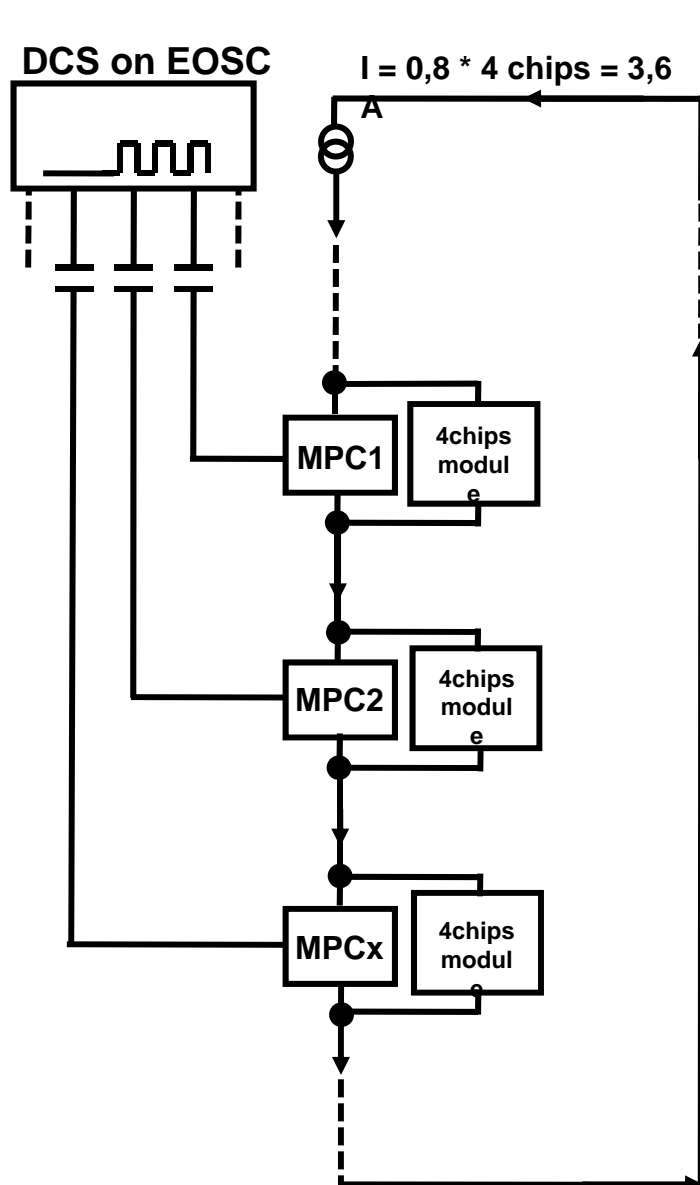


Noisy module



Without protection, one failed module can adversely affect the operation of all other modules on stave
Demonstration staves are very reliable - Protection is not strictly necessary

Serial powering scheme



- + simple
- + control & monitor
- + fast auto-response

default state = OC

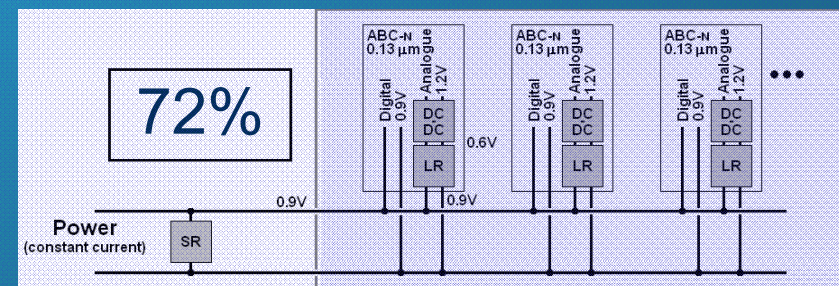
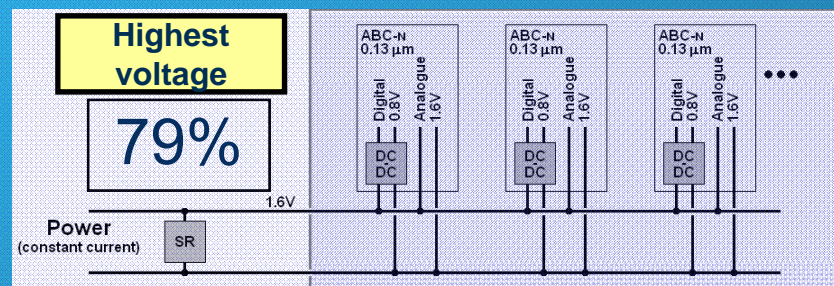
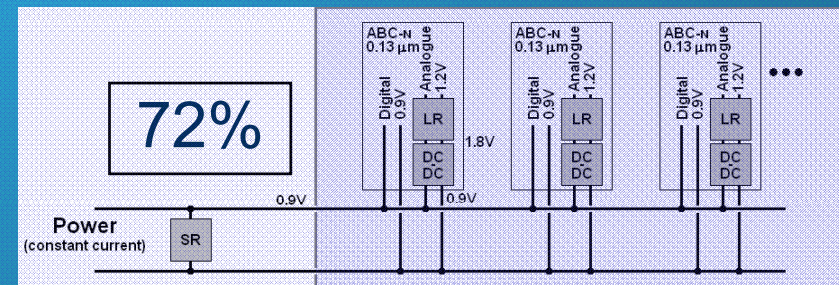
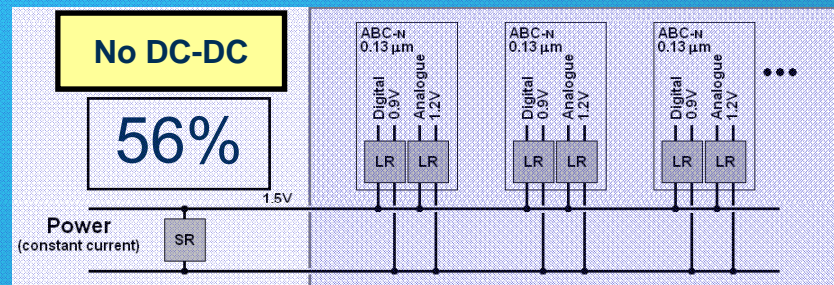
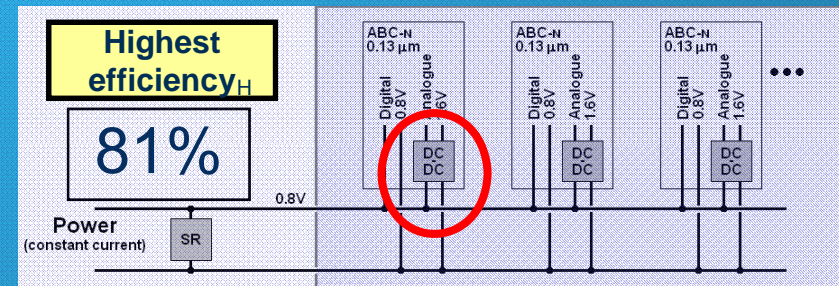
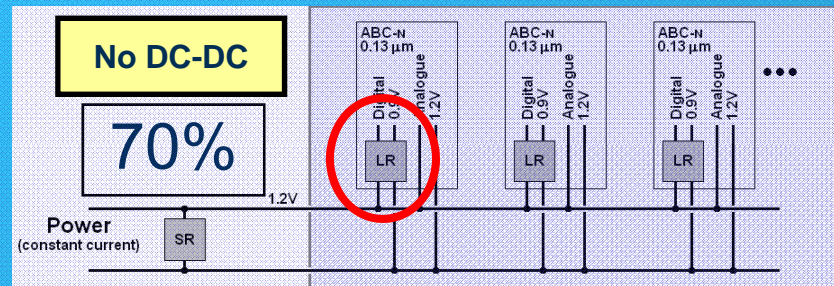
OC = Open Circuit (ie switch is "off", module powered)

- 1 AWG 36 line / module

Need both analog and digital voltage

How? There are many choices. So far $V_{\text{analog}} < V_{\text{digital}}$ in future : $V_{\text{analog}} = 1.2 \text{ V}$, $V_{\text{digital}} = 0.9 \text{ V}$

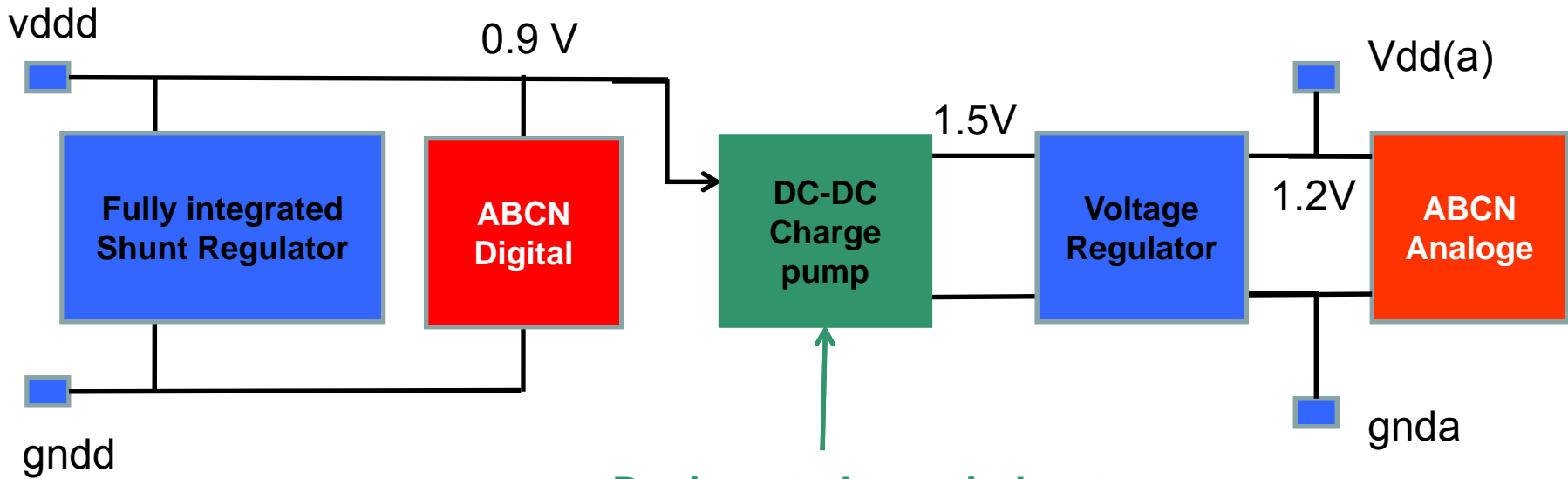
Efficiency =: ABC-N power consumption/total consumption at rack power supply



SR = Shunt Regulator, LR = Linear Regulator, DC-DC = DC to DC voltage conversion

Possible schema of power management in ABCN (130 nm)

3



Design study carried out by M. Bochenek

Possibly most efficient system compatible with serial powering

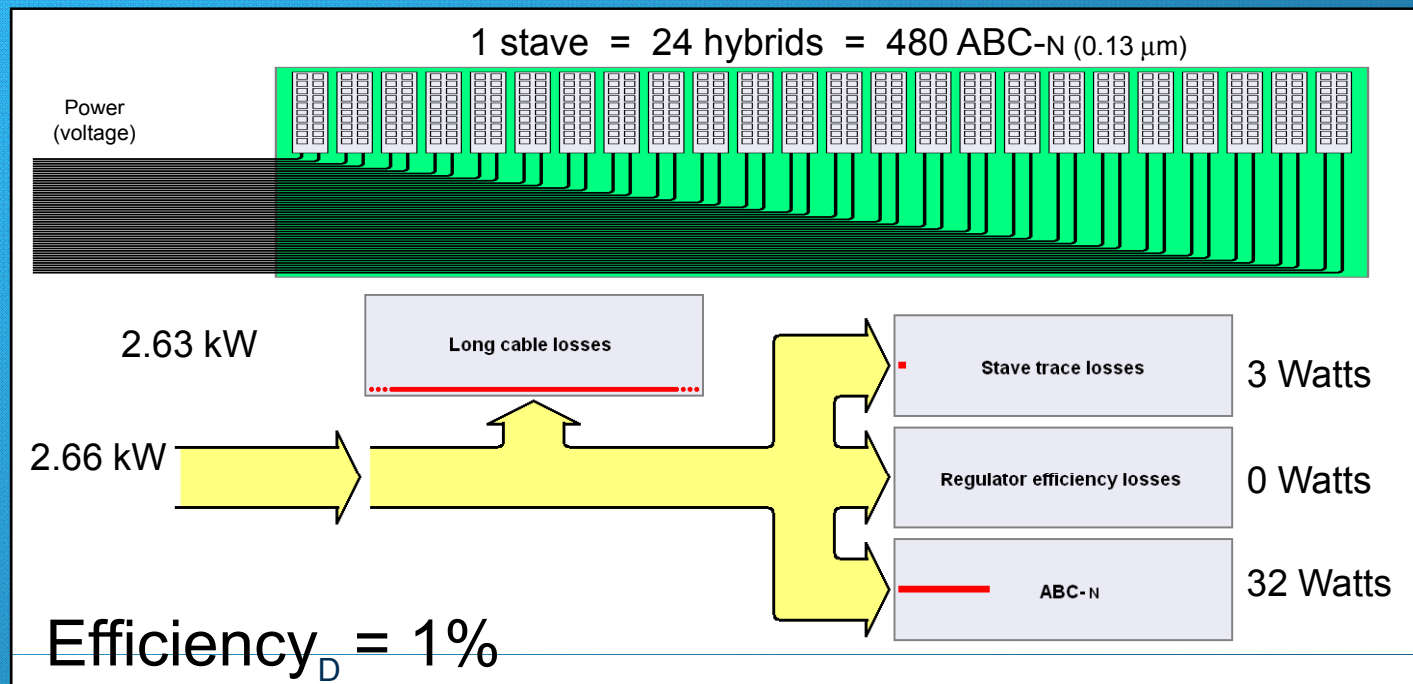
Power efficiency IP

24 cables for digital power, 24 cables for analog. Also “sense wires”.

($I_{\text{analog}} = 0.32 \text{ A}$, $I_{\text{digital}} = 1.02 \text{ A}$, cable resistance (both ways) 2 Ohms)

Efficiency =: ABC-N power consumption/total consumption (cables, regulator, ABC-N)

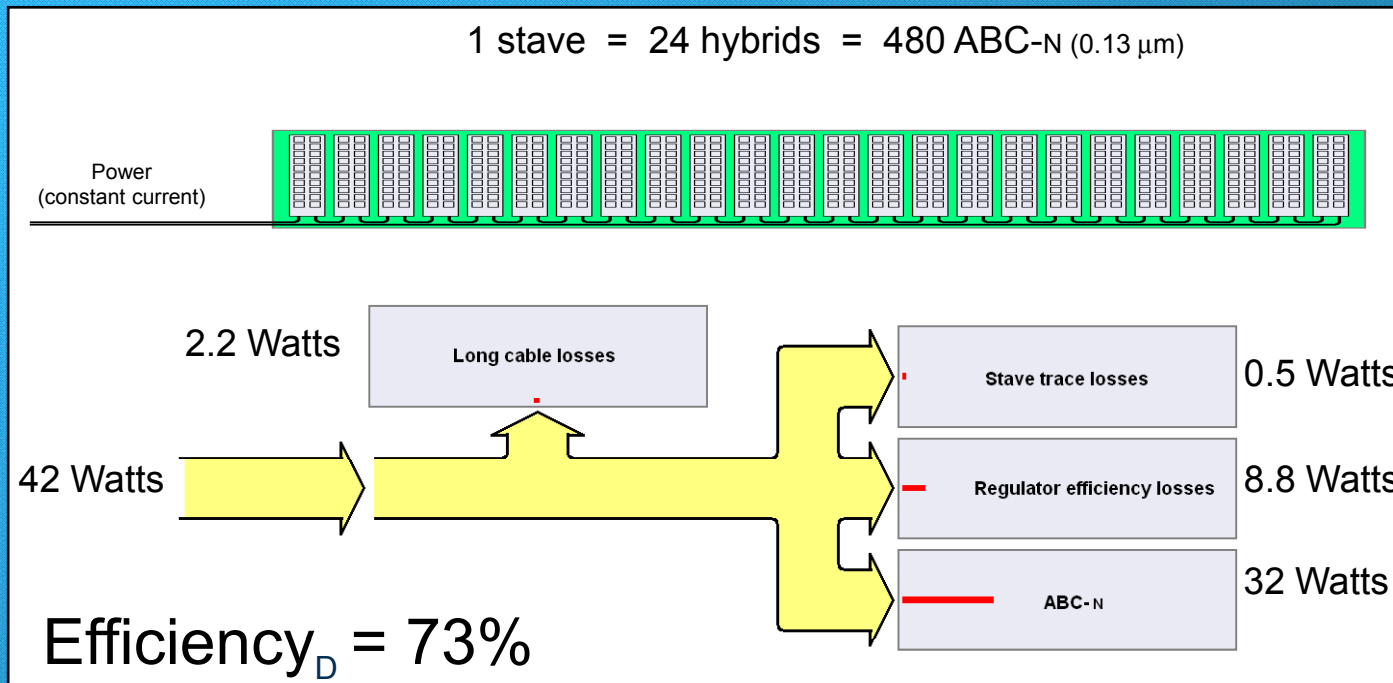
Independent powering (100% hybrid efficiency)



Power efficiency SP

1 cable for digital plus analog current. Only minimal cable losses!

Serial powering a stave, (higher voltage, with DC-DC / 2 for digital)



Cables assumed to be 2 ohms total for each power line pair

Regulator power = $(1/\text{eff}_H - 1) \times \text{ABC power}$

Stave supply current = $(32 + 8.5)\text{watts} / (1.6\text{volts} \times 24)$
= 1.1amps

Numbers rounded

Summary and next steps

- **Characterize various ASICs designs** for both DC-DC and SP
- **Move on to more realistic technologies** (e.g. 130 nm CMOS)
- **Understand system architecture better**
- **Gain practical experience with “full system” prototypes**
(sensors, readout chips, hybrids, modules, supermodules)

Huge progress, but

The more progress we make, the larger the challenge seems to become...Still looking good