## Advanced Accelerator Physics Course

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## Low Emittance Machines

Part 2: Equilibrium Emittance and Storage Ring Lattice Design

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Lecture 1 summary

In Lecture 1, we:

- discussed the effects of synchrotron radiation on the (linear) motion of particles in storage rings;
- derived expressions for the damping times of the vertical, horizontal, and longitudinal emittances;
- discussed the effects of quantum excitation, and derived expressions for the equilibrium horizontal and longitudinal emittances in an electron storage ring in terms of the lattice functions and beam energy.

In this lecture, we shall:

- derive expressions for the natural (horizontal) emittance in four types of lattices:
- FODO;
- double-bend achromat (DBA);
- multi-bend achromats (MBA);
- theoretical minimum emittance (TME).
- discuss some aspects of the vertical emittance, including:
- the fundamental lower limit;
- generation of vertical emittance from betatron coupling and vertical dispersion (from magnet alignment errors);
- accurate calculation of the emittances;
- low-emittance tuning.

Part 2: Emittance and Lattice Design

Calculating the natural emittance in a lattice

Our first goal is to calculate the natural emittance in a lattice with magnets of given strengths, lengths and positions.

In Lecture 1, we showed that the natural emittance in a storage ring is given by:

$$
\begin{equation*}
\varepsilon_{0}=C_{q} \gamma^{2} \frac{I_{5}}{j_{x} I_{2}} \tag{1}
\end{equation*}
$$

where $C_{q}$ is the quantum radiation constant, $\gamma$ is the relativistic factor, $j_{x}$ is the horizontal damping partition number, and $I_{2}$ and $I_{5}$ are the second and fifth synchrotron radiation integrals.

Note that $j_{x}, I_{2}$ and $I_{5}$ are all functions of the lattice, and are independent of the beam energy.

In most storage rings, if the bends have no quadrupole component, the damping partition number $j_{x} \approx 1$.

In this case we just need to evaluate the two synchrotron radiation integrals:

$$
\begin{equation*}
I_{2}=\oint \frac{1}{\rho^{2}} d s, \quad I_{5}=\oint \frac{\mathcal{H}_{x}}{|\rho|^{3}} d s \tag{2}
\end{equation*}
$$

If we know the strength and length of all the dipoles in the lattice, it is straightforward to calculate $I_{2}$.

For example, if all the bends are identical, then in a complete ring (total bending angle $=2 \pi$ ):

$$
\begin{equation*}
I_{2}=\oint \frac{1}{\rho^{2}} d s=\oint \frac{B}{(B \rho)} \frac{d s}{\rho}=2 \pi \frac{B}{(B \rho)} \approx 2 \pi \frac{c B}{E / e}, \tag{3}
\end{equation*}
$$

where $E$ is the beam energy.
$I_{5}$ is more complicated: it depends on the lattice functions...

Case 1: natural emittance in a FODO lattice


Let us consider the case of a FODO lattice. To simplify the system, we use the following approximations:

- the quadrupoles are represented as thin lenses;
- the space between the quadrupoles is completely filled by the dipoles.

With these approximations, the lattice functions (Courant-Snyder parameters and dispersion) are completely determined by the following parameters:

- the focal length $f$ of a quadrupole;
- the bending radius $\rho$ of a dipole;
- the length $L$ of a dipole.

From the evolution of the lattice functions through a given FODO cell, we can find an (approximate) expression for $I_{5} / I_{2}$ : the details are given in Appendix A.

For small $\theta$, and if $\rho \gg 2 f$ (which is often the case) we find:

$$
\begin{equation*}
\frac{I_{5}}{I_{2}} \approx\left(1-\frac{L^{2}}{16 f^{2}}\right) \frac{8 f^{3}}{\rho^{3}} \tag{4}
\end{equation*}
$$

This result can be further simplified if $4 f \gg L$ (which is not always the case):

$$
\begin{equation*}
\frac{I_{5}}{I_{2}} \approx \frac{8 f^{3}}{\rho^{3}} \tag{5}
\end{equation*}
$$

Making the approximation $j_{x} \approx 1$ (since there is no quadrupole component in the dipole), and writing $\rho=L / \theta$, we have:

$$
\begin{equation*}
\varepsilon_{0} \approx C_{q} \gamma^{2}\left(\frac{2 f}{L}\right)^{3} \theta^{3} \tag{6}
\end{equation*}
$$

Notice how the emittance scales with the beam and lattice parameters:

- The emittance is proportional to the square of the energy.
- The emittance is proportional to the cube of the bending angle. Increasing the number of cells in a complete circular lattice reduces the bending angle of each dipole, and reduces the emittance.
- The emittance is proportional to the cube of the quadrupole focal length: stronger quads means lower emittance.
- The emittance is inversely proportional to the cube of the cell (or dipole) length.

Part 2: Emittance and Lattice Design

Case 1: natural emittance in a FODO lattice

The phase advance in a FODO cell is given by:

$$
\begin{equation*}
\cos \left(\mu_{x}\right)=1-\frac{L^{2}}{2 f^{2}} \tag{7}
\end{equation*}
$$

This means that a stable lattice must have:

$$
\begin{equation*}
\frac{f}{L} \geq \frac{1}{2} \tag{8}
\end{equation*}
$$

In the limiting case, $\mu_{x}=180^{\circ}$, and $f$ has the minimum value $f=L / 2$. Using the approximation (6):

$$
\varepsilon_{0} \approx C_{q} \gamma^{2}\left(\frac{2 f}{L}\right)^{3} \theta^{3}
$$

the minimum emittance in a FODO lattice is expected to be:

$$
\begin{equation*}
\varepsilon_{0} \approx C_{q} \gamma^{2} \theta^{3} \tag{9}
\end{equation*}
$$

However, as we increase the focusing strength, the approximations we used to obtain the simple expression for $\varepsilon_{0}$ start to break down...

Plotting the exact formula for $I_{5} / I_{2}$ as a function of the phase advance, we find that there is a minimum in the natural emittance, at $\mu_{x} \approx 137^{\circ}$.


Black line:
exact formula.

Red line:
approximation,

$$
\frac{I_{5}}{I_{2}} \approx\left(1-\frac{L^{2}}{16 f^{2}}\right) \frac{8 f^{3}}{\rho^{3}}
$$

It turns out that the minimum value of the natural emittance in a FODO lattice is given by:

$$
\begin{equation*}
\varepsilon_{0, \mathrm{FODO}, \min } \approx 1.2 C_{q} \gamma^{2} \theta^{3} \tag{10}
\end{equation*}
$$

Using Eq. (6), we estimate that a storage ring constructed from 16 FODO cells ( 32 dipoles) with $90^{\circ}$ phase advance per cell ( $f=L / \sqrt{2}$ ), and storing beam at 2 GeV would have a natural emittance of around 125 nm .

Many modern applications (including synchrotron light sources) demand emittances smaller by one or two orders of magnitude.

How can we design a lattice with a smaller natural emittance?

Looking at curly-H $\left(\mathcal{H}_{x}\right)$ in a FODO cell provides a clue...



Part 2: Emittance and Lattice Design

Case 1: natural emittance in a FODO lattice

The curly-H function remains at a relatively constant value throughout the lattice:


As a first attempt at reducing the natural emittance, we can try reducing the curly-H function in the dipoles, by designing a lattice that has zero dispersion at either end of a dipole pair.

The result is a double bend achromat (DBA) cell:


Part 2: Emittance and Lattice Design

Case 2: natural emittance in a DBA lattice

To calculate the natural emittance in a DBA, let us begin by considering the conditions for zero dispersion at the start and the exit of the cell.

Assume that the dispersion is zero at the start of the cell.

Place a quadrupole midway between the dipoles, to reverse the gradient of the dispersion.

By symmetry, the dispersion at the exit of the cell will be zero.

In the thin lens approximation, this condition can be written:

$$
\left(\begin{array}{cc}
1 & 0  \tag{11}\\
-1 / f & 1
\end{array}\right)\binom{\eta_{x}}{\eta_{p x}}=\binom{\eta_{x}}{\eta_{p x}-\frac{\eta_{x}}{f}}=\binom{\eta_{x}}{-\eta_{p x}}
$$

Hence the central quadrupole must have focal length:

$$
\begin{equation*}
f=\frac{\eta_{x}}{2 \eta_{p x}} \tag{12}
\end{equation*}
$$

The actual value of the dispersion (and its gradient) is determined by the dipole bending angle $\theta$, the bending radius $\rho$, and the drift length $L$ :

$$
\begin{equation*}
\eta_{x}=\rho(1-\cos \theta)+L \sin \theta, \quad \eta_{p x}=\sin \theta \tag{13}
\end{equation*}
$$

Is this style of lattice likely to have a lower natural emittance than a FODO lattice?

We can get some idea by looking at the curly-H function...


The curly-H function is much smaller in the DBA lattice (right) than in the FODO lattice (left).

Note that we use the same dipoles (bending angle and length) in both cases.

Let us calculate the minimum natural emittance of a DBA lattice, for given bending radius $\rho$ and bending angle $\theta$ in the dipoles.

To do this, we need to calculate the minimum value of:

$$
\begin{equation*}
I_{5}=\int \frac{\mathcal{H}_{x}}{\rho^{3}} d s \tag{14}
\end{equation*}
$$

in one dipole, subject to the constraints:

$$
\begin{equation*}
\eta_{x, 0}=\eta_{p x, 0}=0 \tag{15}
\end{equation*}
$$

where $\eta_{x, 0}$ and $\eta_{p x, 0}$ are the dispersion and gradient of the dispersion at the entrance of a dipole.

We know how the dispersion and the Courant-Snyder parameters evolve through the dipole, so we can calculate $I_{5}$ for one dipole, for given initial values of the Courant-Snyder parameters $\alpha_{x, 0}$ and $\beta_{x, 0}$.

Then, we simply have to minimise the value of $I_{5}$ with respect to $\alpha_{x, 0}$ and $\beta_{x, 0}$.

Again, the algebra is rather formidable, and the full expression for $I_{5}$ is not especially enlightening.

Therefore, we just quote the significant results...

We find that, for given $\rho$ and $\theta$ and with the constraints:

$$
\begin{equation*}
\eta_{x, 0}=\eta_{p x, 0}=0 \tag{16}
\end{equation*}
$$

the minimum value of $I_{5}$ is given by:

$$
\begin{equation*}
I_{5, \min }=\frac{1}{4 \sqrt{15}} \frac{\theta^{4}}{\rho}+O\left(\theta^{6}\right) \tag{17}
\end{equation*}
$$

This minimum occurs for values of the Courant-Snyder parameters at the entrance to the dipole given by:

$$
\begin{equation*}
\beta_{x, 0}=\sqrt{\frac{12}{5}} L+O\left(\theta^{3}\right), \quad \alpha_{x, 0}=\sqrt{15}+O\left(\theta^{2}\right) \tag{18}
\end{equation*}
$$

where $L=\rho \theta$ is the length of a dipole.

Case 2: natural emittance in a DBA lattice
Since we know that $I_{2}$ in a single dipole is given by:

$$
\begin{equation*}
I_{2}=\int \frac{1}{\rho^{2}} d s=\frac{\theta}{\rho} \tag{19}
\end{equation*}
$$

we can now write down an expression for the minimum emittance in a DBA lattice:

$$
\begin{equation*}
\varepsilon_{0, \mathrm{DBA}, \min }=C_{q} \gamma^{2} \frac{I_{5, \min }}{j_{x} I_{2}} \approx \frac{1}{4 \sqrt{15}} C_{q} \gamma^{2} \theta^{3} \tag{20}
\end{equation*}
$$

The approximation is valid for small $\theta$. Note that we have again assumed that, since there is no quadrupole component in the dipole, $j_{x} \approx 1$.

Compare the above expression with that for the minimum emittance in a FODO lattice (10):

$$
\begin{equation*}
\varepsilon_{0, \mathrm{FODO}, \min } \approx 1.2 C_{q} \gamma^{2} \theta^{3} \tag{21}
\end{equation*}
$$

We see that in both cases (FODO and DBA), the emittance scales with the square of the beam energy, and with the cube of the bending angle.

However, the emittance in a DBA lattice is smaller than that in a FODO lattice (for given energy and dipole bending angle) by a factor of roughly $4 \sqrt{15} \approx 15.5$.

This is a significant improvement... but can we do even better?

Case 3: natural emittance in a TME Iattice

For a DBA lattice, we imposed the constraints:

$$
\begin{equation*}
\eta_{x, 0}=\eta_{p x, 0}=0 \tag{22}
\end{equation*}
$$

To get a lower emittance, we can consider relaxing these constraints.

To derive the conditions for a "theoretical minimum emittance" (TME) lattice, we write down an expression for:

$$
\begin{equation*}
I_{5}=\int \frac{\mathcal{H}_{x}}{\rho} d s \tag{23}
\end{equation*}
$$

with arbitrary dispersion $\eta_{x, 0}, \eta_{p x, 0}$ and Courant-Snyder parameters $\alpha_{x, 0}$ and $\beta_{x, 0}$ in a dipole with given bending radius $\rho$ and angle $\theta$.

Then, we minimise $I_{5}$ with respect to $\eta_{x, 0}, \eta_{p x, 0}, \alpha_{x, 0}$ and $\beta_{x, 0} \ldots$

The result is:

$$
\begin{equation*}
\varepsilon_{0, \text { TME }, \min } \approx \frac{1}{12 \sqrt{15}} C_{q} \gamma^{2} \theta^{3} \tag{24}
\end{equation*}
$$

The minimum emittance is obtained with dispersion at the entrance to the dipole given by:

$$
\begin{equation*}
\eta_{x, 0}=\frac{1}{6} L \theta+O\left(\theta^{3}\right), \quad \eta_{p x, 0}=-\frac{\theta}{2}+O\left(\theta^{3}\right) \tag{25}
\end{equation*}
$$

and with Courant-Snyder functions at the entrance:

$$
\begin{equation*}
\beta_{x, 0}=\frac{8}{\sqrt{15}} L+O\left(\theta^{2}\right), \quad \alpha_{x, 0}=\sqrt{15}+O\left(\theta^{2}\right) \tag{26}
\end{equation*}
$$

The dispersion and beta function reach minimum values in the centre of the dipole:
$\eta_{x, \min }=\rho\left(1-2 \frac{\sin \frac{\theta}{2}}{\theta}\right)=\frac{L \theta}{24}+O\left(\theta^{4}\right), \quad \beta_{x, \min }=\frac{L}{2 \sqrt{15}}+O\left(\theta^{2}\right)$.

Part 2: Emittance and Lattice Design

Case 3: natural emittance in a TME lattice
By symmetry, we can consider a single TME cell to contain a single dipole, rather than a pair of dipoles as was necessary for the FODO and DBA cells.


Outside the dipole, the dispersion is relatively large. This is not ideal for a light source, since insertion devices at locations with large dispersion will blow up the emittance.

Note that the cell shown here does not achieve the exact conditions for a TME Iattice: a more complicated design would be needed for this.

Summary: natural emittance in FODO, DBA and TME lattices

| Lattice style | Minimum emittance | Conditions/comments |
| :--- | :---: | :---: |
| $90^{\circ}$ FODO | $\varepsilon_{0} \approx 2 \sqrt{2} C_{q} \gamma^{2} \theta^{3}$ | $\frac{f}{L}=\frac{1}{\sqrt{2}}$ |
| $137^{\circ}$ FODO | $\varepsilon_{0} \approx 1.2 C_{q} \gamma^{2} \theta^{3}$ | minimum emittance FODO |
| DBA | $\varepsilon_{0} \approx \frac{1}{4 \sqrt{15}} C_{q} \gamma^{2} \theta^{3}$ | $\beta_{x, 0} \approx \sqrt{12 / 5} L \quad \alpha \quad \eta_{x, 0} \approx \sqrt{15}$ |
| TME | $\varepsilon_{0} \approx \frac{1}{12 \sqrt{15}} C_{q} \gamma^{2} \theta^{3}$ | $\eta_{x, \min } \approx \frac{L \theta}{24} \quad \beta_{x, \min } \approx \frac{L}{2 \sqrt{15}}$ |

Part 2: Emittance and Lattice Design

Comments on lattice design for low emittance
The results we have derived have been for "ideal" lattices that perfectly achieve the stated conditions in each case.

Practical lattice designs rarely achieve the ideal conditions. In particular, the beta function in an achromat is usually not optimal for low emittance; and it is difficult to tune the dispersion for the ideal TME conditions.

The main reasons for this are:

- Beam dynamics issues generally impose a number of strong constraints on the design.
- Optimizing the lattice functions while meeting all the various constraints can require complex configurations of quadrupoles.

A particularly challenging constraint on design of a low-emittance lattice is the dynamic aperture.

Storage rings require a large dynamic aperture in order to achieve good injection efficiency and good beam lifetime.

However, low emittance lattices generally need low dispersion and beta functions, and hence require strong quadrupoles. As a result, the chromaticity can be large, and must be corrected by strong sextupoles.

Strong sextupoles lead to strongly nonlinear motion, and limit the dynamic aperture (the trajectories of particles at large betatron amplitudes or large energy deviations become unstable).

There are many other options besides FODO, DBA and TME for the style of the lattice.

Here, we will discuss (briefly):

- the use of the DBA lattice in third-generation synchrotron light sources;
- "detuning" a DBA lattice to reduce the emittance;
- the use of multi-bend achromats.

Lattices composed of DBA cells have been a popular choice for third generation synchrotron light sources, e.g. the ESRF.



The DBA structure provides a lower natural emittance than a FODO lattice with the same number of dipoles.

The long, dispersion-free straight sections provide ideal locations for insertion devices such as undulators and wigglers.

Part 2: Emittance and Lattice Design

## "Detuning" a DBA

If an insertion device, such as an undulator or wiggler, is placed in a storage ring at a location with large dispersion, then the dipole fields in the device can make a significant contribution to the quantum excitation $\left(I_{5}\right)$.

As a result, the insertion device can lead to an increase in the natural emittance of the storage ring.

By using a DBA lattice, we provide dispersion-free straights in which we can locate undulators and wigglers without blowing up the natural emittance.

However, there is some tolerance. In many cases, it is possible to "detune" the lattice from the strict DBA conditions, thereby allowing some reduction in natural emittance at the cost of some dispersion in the straights.

The insertion devices will then contribute to the quantum excitation; but depending on the lattice and the insertion devices, there may still be a net benefit.

Some light sources that were originally designed with zero-dispersion straights take advantage of tuning flexibility to operate with non-zero dispersion in the straights.

This provides a lower natural emittance, and better output for users. For example, the ESRF:


Part 2: Emittance and Lattice Design

In principle, it is possible to combine the DBA and TME lattices by having an arc cell consisting of more than two dipoles.

The dipoles at either end of the cell have zero dispersion (and gradient of the dispersion) at their outside faces, thus satisfying the achromat condition.

The lattice is tuned so that in the "central" dipoles, the Courant-Snyder parameters and dispersion satisfy the TME conditions.

Suppose that the dipoles all have the same bending radius (i.e. the same field strength), but can have different lengths.


In this case, we find (see Appendix B) that the minimum natural emittance in an $M$-bend achromat is given by:

$$
\begin{equation*}
\varepsilon_{0} \approx C_{q} \gamma^{2} \frac{1}{12 \sqrt{15}}\left(\frac{M+1}{M-1}\right) \theta^{3}, \quad 2<M<\infty \tag{28}
\end{equation*}
$$

where $\theta$ is the average bending angle per dipole.

The minimum emittance is achieved when the central bends are longer than the outer bends by a factor $\sqrt[3]{3}$.

Part 2: Emittance and Lattice Design

Example of a triple-bend achromat: the Swiss Light Source

The Swiss Light Source storage ring consists of 12 TBA cells.

The circumference is 288 m , and the beam energy is 2.4 GeV .

In the "zero-dispersion" mode, the natural emittance is 4.8 nm-rad.



Detuning the achromat to allow dispersion in the straights reduces the natural emittance by about 20\% (to 3.9 nm-rad).


Part 2: Emittance and Lattice Design

A 7-bend achromat: MAX IV



Note: vertical focusing provided by gradient in the bending magnets.
S.C. Leeman et al, "Beam dynamics and expected performance of Sweden's new storage-ring light source: MAX IV," PRST-AB 12, 120701 (2009).

| Beam energy | 3 GeV |
| :--- | :--- |
| Circumference | 528 m |
| Number of cells | 20 |
| Horizontal emittance (no IDs) | 0.326 nm |
| Horizontal emittance (with IDs) | 0.263 nm |

In principle, we can relax the constraint that the field strength in a dipole is constant along the length of the dipole.

Allowing a longitudinal variation in the strength provides another degree of freedom in reducing the emittance. We expect an optimised design to have the strongest field at the centre of the dipole, where the dispersion can be minimised.


|  | Uniform Bend | Variational Bend |  |
| :---: | :---: | :---: | :---: |
| Max B (T) | 1.2 | 2.0 | 5.10 |
| Length (m) | 0.96 | 1.5 | 1.5 |
| Bend angle | $2 \pi / 36$ | $2 \pi / 36$ | $2 \pi / 36$ |
| I2 | $3.173 \mathrm{e}-2$ | $3.139 \mathrm{e}-2$ | $6.887 \mathrm{e}-2$ |
| I5/I2 | $1.142 \mathrm{e}-4$ | $2.945 \mathrm{e}-5$ | $1.5793 \mathrm{e}-5$ |
| $\beta_{\mathrm{x} 0}$ (m) | 0.124 | 0.0803 | 0.0222 |
| $\eta_{\mathrm{x} 0}(\mathrm{~m})$ | $6.98 \mathrm{e}-3$ | $1.40 \mathrm{e}-3$ | $3.62 \mathrm{e}-4$ |

J. Guo and T. Raubenheimer, Proceedings of EPAC'02, Paris, France.

Recall that the natural (horizontal) emittance in a storage ring is given by:

$$
\begin{equation*}
\varepsilon_{0}=C_{q} \gamma^{2} \frac{I_{5}}{j_{x} I_{2}} . \tag{29}
\end{equation*}
$$

If the vertical motion is independent of the horizontal motion (i.e. if there is no betatron coupling) then we can apply the same analysis to the vertical motion as we did to the horizontal.

Then, if we build a ring that is completely flat (i.e. no vertical bending), then there is no vertical dispersion:

$$
\begin{equation*}
\eta_{y}=\eta_{p y}=0 \quad \therefore \quad \mathcal{H}_{y}=0 \quad \therefore \quad I_{5 y}=0 \tag{30}
\end{equation*}
$$

This implies that the vertical emittance will damp to zero.

Part 2: Emittance and Lattice Design

Fundamental lower limit on the vertical emittance
However, in deriving equation (29) for the natural emittance, we assumed that all photons were emitted directly along the instantaneous direction of motion of the electron.

In fact, photons are emitted with a distribution with angular width $1 / \gamma$ about the direction of motion of the electron.

This leads to some vertical "recoil" that excited vertical betatron motion, resulting in a non-zero vertical emittance.


A detailed analysis* leads to the following formula for the fundamental lower limit on the vertical emittance:

$$
\begin{equation*}
\varepsilon_{y, \min }=\frac{13}{55} \frac{C_{q}}{j_{y} I_{2}} \oint \frac{\beta_{y}}{|\rho|^{3}} d s . \tag{31}
\end{equation*}
$$

*T. Raubenheimer, SLAC Report 387 (1992)

To estimate a typical value for the lower limit on the vertical emittance, let us write equation (31) in the approximate form:

$$
\begin{equation*}
\varepsilon_{y, \min } \approx \frac{C_{q}\left\langle\beta_{y}\right\rangle}{4 j_{y} I_{2}} \oint \frac{1}{|\rho|^{3}} d s=\frac{\left\langle\beta_{y}\right\rangle}{4} \frac{j_{z}}{j_{y}} \frac{\sigma_{\delta}^{2}}{\gamma^{2}} \tag{32}
\end{equation*}
$$

Using some typical values $\left(\left\langle\beta_{y}\right\rangle=20 \mathrm{~m}, j_{z}=2, j_{y}=1\right.$, $\sigma_{\delta}=10^{-3}, \gamma=6000$ ), we find:

$$
\begin{equation*}
\varepsilon_{y, \text { min }} \approx 0.3 \mathrm{pm} . \tag{33}
\end{equation*}
$$

The lowest vertical emittance achieved so far in a storage ring is around a picometer, several times larger than the fundamental lower limit.

In practice, vertical emittance in a (nominally flat) storage ring is dominated by two effects:

- residual vertical dispersion, which couples longitudinal and vertical motion;
- betatron coupling, which couples horizontal and vertical motion.

The dominant causes of residual vertical dispersion and betatron coupling are magnet alignment errors, in particular:

- tilts of the dipoles around the beam axis;
- vertical alignment errors on the quadrupoles;
- tilts of the quadrupoles around the beam axis;
- vertical alignment errors of the sextupoles.

Betatron coupling describes the dependence of the vertical motion of a particle on its horizontal motion (and vice-versa).

In a storage ring, betatron coupling often comes from skew quadrupole fields generated by rotation (tilt) errors on quadrupoles and vertical alignment errors on sextupoles.


A rigorous treatment of coupling can be complex; but it is possible to use simplified models to derive approximate expressions for the equilibrium emittances in the presence of coupling.

Part 2: Emittance and Lattice Design

## Betatron coupling

One possible approach is as follows:

1. Write down the equations of motion for a single particle in a beamline containing coupling.
2. Look for a "steady state" solution to the equations of motion, in which the horizontal and vertical actions are each constants of the motion.
3. Assume that the actions in the steady state solution are the equilibrium emittances (since $\varepsilon=\langle J\rangle$ ), and that the sum of the horizontal and vertical emittances equals the natural emittance of the "ideal" lattice (i.e. the natural emittance of the lattice in the absence of errors).

This procedure can give some useful results, but because of the approximations involved, the formulae are not always very accurate.

The details of the calculation are given in Appendix C. Here, we simply quote the results.

The horizontal and vertical emittances in the presence of coupling generated by skew quadrupoles in a lattice are:

$$
\begin{equation*}
\varepsilon_{x, y}=\frac{\varepsilon_{0}}{2}\left(1 \pm \frac{1}{\sqrt{1+\kappa^{2} / \Delta \nu^{2}}}\right) \tag{34}
\end{equation*}
$$

where the upper (lower) sign applies for the horizontal
(vertical) emittance, $\varepsilon_{0}$ is the natural emittance, and $\Delta \nu$ is the difference in the fractional parts of the betatron tunes.

The "coupling strength" $\kappa$ is found from:

$$
\begin{equation*}
\kappa e^{i \chi}=\frac{1}{2 \pi} \oint e^{i\left(\mu_{x}-\mu_{y}\right)} k_{s} \sqrt{\beta_{x} \beta_{y}} d s \tag{35}
\end{equation*}
$$

Part 2: Emittance and Lattice Design

## Betatron coupling: example

As an illustration, we can plot the vertical emittance as a function of the "tune split" $\Delta \nu$, in a model of the ILC damping rings, with a single skew quadrupole (located at a point of zero dispersion - why?).

The tunes are controlled by adjusting the regular (normal) quadrupoles in the lattice:


Note: the "simulation" results are based on emittance calculation using Chao's method, which we shall discuss later.

The presence of skew quadrupole errors in a storage ring affects the betatron tunes. In Appendix $D$, it is shown that the measured betatron tunes $\nu_{ \pm}$are given (in terms of the tunes $\nu_{x}$ and $\nu_{y}$ in the absence of errors) by:

$$
\begin{equation*}
\nu_{ \pm}=\frac{1}{2}\left(\nu_{x}+\nu_{y} \pm \sqrt{\kappa^{2}+\Delta \nu^{2}}\right) . \tag{36}
\end{equation*}
$$

This provides a useful method for measuring the coupling strength $\kappa$ in a real lattice:


Part 2: Emittance and Lattice Design

Vertical dispersion and vertical emittance
Vertical emittance can also be generated by vertical dispersion, in the same way that horizontal emittance can be generated by horizontal dispersion.

If we know the vertical dispersion all around the ring, then to calculate the vertical emittance we can simply modify the formula for the natural emittance (see Lecture 1):

$$
\begin{equation*}
\varepsilon_{y}=C_{q} \gamma^{2} \frac{I_{5 y}}{j_{y} I_{2}} \tag{37}
\end{equation*}
$$

where $j_{y}$ is the vertical damping partition number (usually, $j_{y}=1$ ), and the synchrotron radiation integrals are given by:

$$
\begin{equation*}
I_{2}=\oint \frac{1}{\rho^{2}} d s \tag{38}
\end{equation*}
$$

and:

$$
\begin{equation*}
I_{5 y}=\oint \frac{\mathcal{H}_{y}}{|\rho|^{3}} d s, \quad \text { where } \quad \mathcal{H}_{y}=\gamma_{y} \eta_{y}^{2}+2 \alpha_{y} \eta_{y} \eta_{p y}+\beta_{y} \eta_{p y}^{2} \tag{39}
\end{equation*}
$$

If the vertical dispersion is generated randomly, then we can assume that it will not be correlated with the curvature $1 / \rho$ of the reference trajectory ${ }^{\dagger}$.

Then, we can write:

$$
\begin{equation*}
I_{5 y} \approx\left\langle\mathcal{H}_{y}\right\rangle \oint \frac{1}{|\rho|^{3}} d s=\left\langle\mathcal{H}_{y}\right\rangle I_{3} \tag{40}
\end{equation*}
$$

Hence, we can write for the vertical emittance:

$$
\begin{equation*}
\varepsilon_{y} \approx C_{q} \gamma^{2}\left\langle\mathcal{H}_{y}\right\rangle \frac{I_{3}}{j_{y} I_{2}} \tag{41}
\end{equation*}
$$

It is convenient to use:

$$
\begin{equation*}
\sigma_{\delta}^{2}=C_{q} \gamma^{2} \frac{I_{3}}{j_{z} I_{2}} \tag{42}
\end{equation*}
$$

which gives:

$$
\begin{equation*}
\varepsilon_{y} \approx \frac{j_{z}}{j_{y}}\left\langle\mathcal{H}_{y}\right\rangle \sigma_{\delta}^{2} \tag{43}
\end{equation*}
$$

$\dagger$ This is not the case for the horizontal dispersion!
50 Part 2: Emittance and Lattice Design

Now, note the similarity between the action:

$$
\begin{equation*}
2 J_{y}=\gamma_{y} y^{2}+2 \alpha_{y} y p_{y}+\beta_{y} p_{y}^{2} \tag{44}
\end{equation*}
$$

and the curly-H function:

$$
\begin{equation*}
\mathcal{H}_{y}=\gamma_{y} \eta_{y}^{2}+2 \alpha_{y} \eta_{y} \eta_{p y}+\beta_{y} \eta_{p y}^{2} \tag{45}
\end{equation*}
$$

This implies that we can write:

$$
\begin{equation*}
\eta_{y}=\sqrt{\beta_{y} \mathcal{H}_{y}} \cos \phi_{\eta y}, \quad \therefore \quad\left\langle\frac{\eta_{y}^{2}}{\beta_{y}}\right\rangle=\frac{1}{2}\left\langle\mathcal{H}_{y}\right\rangle . \tag{46}
\end{equation*}
$$

Combining equations (43) and (46) gives a useful (approximate) relationship, between the vertical dispersion and the vertical emittance:

$$
\begin{equation*}
\varepsilon_{y} \approx 2 \frac{j_{z}}{j_{y}}\left\langle\frac{\eta_{y}^{2}}{\beta_{y}}\right\rangle \sigma_{\delta}^{2} \tag{47}
\end{equation*}
$$

The formulae we have derived so far are useful for making rough estimates of the sensitivity to particular types of error.

For detailed studies, including modelling and simulations, we need more accurate formulae for computing the vertical emittance in a storage ring with a given set of alignment errors.

Methods for computing the equilibrium emittances in complex lattices (including lattices with errors), include:

- radiation integrals generalised to the normal modes;
- Chao's method: A. Chao, "Evaluation of beam distribution parameters in an electron storage ring," J. Appl. Phys. 50, 595-598 (1979);
- the 'envelope’ method (Appendix E): K. Ohmi, K. Hirata, K. Oide, "From the beam-envelope matrix to the synchrotron radiation integrals," Phys. Rev. E 49, 751-765 (1994).

Part 2: Emittance and Lattice Design

Ultra-low emittance tuning

In practice, tuning a storage ring to achieve a vertical emittance of no more than a few picometres is a considerable challenge.

This cannot be done just by survey alignment of the magnets: beam-based methods are also required. However, precise alignment of the magnets is always the first step.

A variety of beam-based methods for tuning storage rings have been developed over the years.

A typical procedure might look as follows..

Step 1: Align the magnets by a survey of the ring.

Typically, quadrupoles need to be aligned to better than a few tens of microns, and sextupoles to better than a couple of hundred microns.


Part 2: Emittance and Lattice Design

## Ultra-Iow emittance tuning

Step 2: Determine the positions of the BPMs relative to the quadrupoles.

This is known as "beam-based alignment" (BBA): the beam is steered to a position in each quadrupole such that changing the quadrupole strength has no effect on the orbit.


Step 3: Correct the orbit (using steering magnets) so that it is as close as possible to the centres of the quadrupoles.

Step 4: Correct the vertical dispersion (using steering magnets and/or skew quadrupoles, and measuring at the BPMs) as close to zero as possible.

Step 5: Correct the coupling, by adjusting skew quadrupoles so that an orbit "kick" in one place (from any orbit corrector) has no effect on the orbit in the other plane.

Usually, these last three steps need to be iterated several (or even many) times.

Part 2: Emittance and Lattice Design

Ultra-low emittance tuning: ORM analysis
Results from the tuning procedure described above can be limited by errors on the BPMs, which can affect dispersion and coupling measurements.

A useful technique for overcoming such limitations is to apply Orbit Response Matrix (ORM) analysis. This can be used to determine a wide range of magnet and diagnostics parameters, including coupling errors and BPM tilts.



ORM analysis in KEK ATF.

Left: measured orbit response matrix.

Right: residuals between measured ORM and machine model.

The natural emittance in a storage ring is determined by the balance between the radiation damping (given by $I_{2}$ ) and the quantum excitation (given by $I_{5}$ ).

The quantum excitation depends on the lattice functions. Different "styles" of lattice can be used, depending on the emittance specification for the storage ring.

In general, for small bending angle $\theta$ the natural emittance can be written as:

$$
\begin{equation*}
\varepsilon_{0} \approx F C_{q} \gamma^{2} \theta^{3} \tag{48}
\end{equation*}
$$

where $\theta$ is the bending angle of a single dipole, and the numerical factor $F$ is determined by the lattice style...

$$
\varepsilon_{0} \approx F C_{q} \gamma^{2} \theta^{3}
$$

| Lattice style | $F$ |
| :--- | :--- |
| $90^{\circ}$ FODO | $2 \sqrt{2}$ |
| $137^{\circ}$ FODO | 1.2 |
| Double-bend achromat (DBA) | $\frac{1}{4 \sqrt{15}}$ |
| Multi-bend achromat | $\frac{1}{12 \sqrt{15}}\left(\frac{M+1}{M-1}\right)$ |
| TME | $\frac{1}{12 \sqrt{15}}$ |

Achromats have been popular choices for storage ring lattices in third-generation synchrotron light sources for two reasons:

- they provide lower natural emittance than FODO lattices;
- they provide zero-dispersion locations appropriate for insertion devices (wigglers and undulators).

Light sources have been built using double-bend achromats (e.g. ESRF, APS, SPring-8, DIAMOND, SOLEIL) and triple-bend achromats (e.g. ALS, SLS).

Increasing the number of bends in an achromat cell ("multiple-bend achromats") and "detuning" an achromat (to allow some dispersion in the straights) can help to achieve a lower emittance.

Part 2: Emittance and Lattice Design

## Summary (4)

The opening angle of the synchrotron radiation places a lower limit (typically, a fraction of a picometre) on the vertical emittance.

In practice, the vertical emittance is dominated by alignment and tuning errors (betatron coupling and vertical dispersion).

Natural emittances of a few nanometres are typical in storage rings for third generation light sources.

Storage rings for light sources often operate with vertical emittances of order $1 \%$ (or less) of the horizontal (natural) emittance: this requires careful tuning and correction of alignment errors.

In terms of $f, \rho$ and $L$, the horizontal beta function at the horizontally-focusing quadrupole is given by:

$$
\begin{equation*}
\beta_{x}=\frac{4 f \rho \sin \theta(2 f \cos \theta+\rho \sin \theta)}{\sqrt{16 f^{4}-\left[\rho^{2}-\left(4 f^{2}+\rho^{2}\right) \cos 2 \theta\right]^{2}}}, \tag{49}
\end{equation*}
$$

where $\theta=L / \rho$ is the bending angle of a single dipole.
The dispersion at a horizontally-focusing quadrupole is given by:

$$
\begin{equation*}
\eta_{x}=\frac{2 f \rho\left(2 f+\rho \tan \frac{\theta}{2}\right)}{4 f^{2}+\rho^{2}} . \tag{50}
\end{equation*}
$$

By symmetry, at the centre of a quadrupole, $\alpha_{x}=\eta_{p x}=0$.

## Appendix A: Evaluating $I_{5}$ in a FODO lattice

We also know how to evolve the lattice functions through the lattice, using the transfer matrices, $M$.

For the Courant-Snyder parameters:

$$
\begin{equation*}
A\left(s_{1}\right)=M A\left(s_{0}\right) M^{\top} \tag{51}
\end{equation*}
$$

where $M=M\left(s_{1} ; s_{0}\right)$ is the transfer matrix from $s_{0}$ to $s_{1}$, and:

$$
A=\left(\begin{array}{cc}
\beta_{x} & -\alpha_{x}  \tag{52}\\
-\alpha_{x} & \gamma_{x}
\end{array}\right) .
$$

The dispersion can be evolved (over a distance $\Delta s$, with constant bending radius $\rho$ ) using:

$$
\begin{equation*}
\binom{\eta_{x}}{\eta_{p x}}_{s_{1}}=M\binom{\eta_{x}}{\eta_{p x}}_{s_{0}}+\binom{\rho\left(1-\cos \frac{\Delta s}{\rho}\right)}{\sin \frac{\Delta s}{\rho}} \tag{53}
\end{equation*}
$$

For a thin quadrupole, the transfer matrix is: $M=\left(\begin{array}{cc}1 & 0 \\ -1 / f & 1\end{array}\right)$.
For a dipole, the transfer matrix is: $M=\left(\begin{array}{cc}\cos \frac{s}{\rho} & \rho \sin \frac{s}{\rho} \\ -\frac{1}{\rho} \sin \frac{s}{\rho} & \cos \frac{s}{\rho}\end{array}\right)$.
We now have all the information we need to find an expression for $I_{5}$ in the FODO cell.

However, the algebra is rather formidable. The result is most easily expressed as a power series in the dipole bending angle, $\theta$ :

$$
\begin{equation*}
\frac{I_{5}}{I_{2}}=\left(4+\frac{\rho^{2}}{f^{2}}\right)^{-\frac{3}{2}}\left[8-\frac{\rho^{2}}{2 f^{2}} \theta^{2}+O\left(\theta^{4}\right)\right] . \tag{54}
\end{equation*}
$$

## Appendix A: Evaluating $I_{5}$ in a FODO lattice

For small $\theta$, the expression for $I_{5} / I_{2}$ can be written:

$$
\begin{equation*}
\frac{I_{5}}{I_{2}} \approx\left(1-\frac{\rho^{2}}{16 f^{2}} \theta^{2}\right)\left(1+\frac{\rho^{2}}{4 f^{2}}\right)^{-\frac{3}{2}}=\left(1-\frac{L^{2}}{16 f^{2}}\right)\left(1+\frac{\rho^{2}}{4 f^{2}}\right)^{-\frac{3}{2}} . \tag{55}
\end{equation*}
$$

This can be further simplified if $\rho \gg 2 f$ (often the case):

$$
\begin{equation*}
\frac{I_{5}}{I_{2}} \approx\left(1-\frac{L^{2}}{16 f^{2}}\right) \frac{8 f^{3}}{\rho^{3}}, \tag{56}
\end{equation*}
$$

and still further simplified if $4 f \gg L$ (less often the case):

$$
\begin{equation*}
\frac{I_{5}}{I_{2}} \approx \frac{8 f^{3}}{\rho^{3}} . \tag{57}
\end{equation*}
$$

For simplicity, we consider the case where the dipoles all have the same bending radius (i.e. they all have the same field strength), but they vary in length.


Assuming that each arc cell has a fixed number, $M$, of dipoles, and $\theta=2 \pi / M N_{\text {cells }}$, the bending angles satisfy:

$$
\begin{equation*}
2 \alpha+(M-2) \beta=M \tag{58}
\end{equation*}
$$

Since the synchrotron radiation integrals are additive, for an $M$-bend achromat, we can write:

$$
\begin{align*}
& I_{5, \text { cell }} \approx \frac{2}{4 \sqrt{15}} \frac{(\alpha \theta)^{4}}{\rho}+\frac{(M-2)}{12 \sqrt{15}} \frac{(\beta \theta)^{4}}{\rho}=\frac{6 \alpha^{4}+(M-2) \beta^{4}}{12 \sqrt{15}} \frac{\theta^{4}}{\rho}  \tag{60}\\
& I_{2, \text { cell }} \approx 2 \frac{\alpha \theta}{\rho}+(M-2) \frac{\beta \theta}{\rho}=[2 \alpha+(M-2) \beta] \frac{\theta}{\rho} \tag{59}
\end{align*}
$$

## Appendix B: Multiple-bend achromats

Hence, in an $M$-bend achromat:

$$
\begin{equation*}
\frac{I_{5, \text { cell }}}{I_{2, \text { cell }}} \approx \frac{1}{12 \sqrt{15}}\left[\frac{6 \alpha^{4}+(M-2) \beta^{4}}{2 \alpha+(M-2) \beta}\right] \theta^{3} . \tag{61}
\end{equation*}
$$

Minimising the ratio $I_{5} / I_{2}$ with respect to $\alpha$ gives:

$$
\begin{equation*}
\frac{\alpha}{\beta}=\frac{1}{\sqrt[3]{3}}, \quad \frac{6 \alpha^{4}+(M-2) \beta^{4}}{2 \alpha+(M-2) \beta} \approx \frac{M+1}{M-1} . \tag{62}
\end{equation*}
$$

The central bending magnets should be longer than the outer bending magnets by a factor $\sqrt[3]{3}$.

Then, the minimum natural emittance in an $M$-bend achromat is given by:

$$
\begin{equation*}
\varepsilon_{0} \approx C_{q} \gamma^{2} \frac{1}{12 \sqrt{15}}\left(\frac{M+1}{M-1}\right) \theta^{3}, \quad 2<M<\infty \tag{63}
\end{equation*}
$$

Note that $\theta$ is the average bending angle per dipole.

Our goal is to find the equations of motion for a particle in a coupled storage ring, and by solving these equations, to show equation (34).

We will use Hamiltonian mechanics. In this formalism, the equations of motion for the action-angle variables (with path length $s$ as the independent variable) are derived from the Hamiltonian:

$$
\begin{equation*}
H=H\left(\phi_{x}, J_{x}, \phi_{y}, J_{y} ; s\right) \tag{64}
\end{equation*}
$$

using Hamilton's equations:

$$
\begin{array}{cc}
\frac{d J_{x}}{d s}=-\frac{\partial H}{\partial \phi_{x}}, & \frac{d J_{y}}{d s}=-\frac{\partial H}{\partial \phi_{y}} \\
\frac{d \phi_{x}}{d s}=\frac{\partial H}{\partial J_{x}}, & \frac{d \phi_{y}}{d s}=\frac{\partial H}{\partial J_{y}} \tag{66}
\end{array}
$$

For a particle moving along a linear, uncoupled beamline, the Hamiltonian is:

$$
\begin{equation*}
H=\frac{J_{x}}{\beta_{x}}+\frac{J_{y}}{\beta_{y}} . \tag{67}
\end{equation*}
$$

## Appendix C: Equations of motion in a coupled storage ring

The first step is to derive an appropriate form for the Hamiltonian in a storage ring with skew quadrupole perturbations.

In Cartesian variables, the equations of motion in a skew quadrupole can be written:

$$
\begin{array}{cl}
\frac{d p_{x}}{d s}=k_{s} y, & \frac{d p_{y}}{d s}=k_{s} x \\
\frac{d x}{d s}=p_{x}, & \frac{d y}{d s}=p_{y} \tag{69}
\end{array}
$$

where:

$$
\begin{equation*}
k_{s}=\frac{1}{B \rho} \frac{\partial B_{x}}{\partial x} . \tag{70}
\end{equation*}
$$



These equations can be derived from the Hamiltonian:

$$
\begin{equation*}
H=\frac{1}{2} p_{x}^{2}+\frac{1}{2} p_{y}^{2}-k_{s} x y . \tag{71}
\end{equation*}
$$

We are interested in the case where there are skew quadrupoles distributed around a storage ring.

The "focusing" effect of a skew quadrupole is represented by a term in the Hamiltonian:

$$
\begin{equation*}
k_{s} x y=2 k_{s} \sqrt{\beta_{x} \beta_{y}} \sqrt{J_{x} J_{y}} \cos \phi_{x} \cos \phi_{y} . \tag{72}
\end{equation*}
$$

This implies that the Hamiltonian for a beam line with distributed skew quadrupoles can be written:

$$
\begin{equation*}
H=\frac{J_{x}}{\beta_{x}}+\frac{J_{y}}{\beta_{y}}-2 k_{s}(s) \sqrt{\beta_{x} \beta_{y}} \sqrt{J_{x} J_{y}} \cos \phi_{x} \cos \phi_{y} . \tag{73}
\end{equation*}
$$

The beta functions and the skew quadrupole strength are functions of the position $s$. This makes it difficult to solve the equations of motion exactly.

Therefore, we simplify the problem by "averaging" the Hamiltonian:

$$
\begin{equation*}
H=\omega_{x} J_{x}+\omega_{y} J_{y}-2 \bar{\kappa} \sqrt{J_{x} J_{y}} \cos \phi_{x} \cos \phi_{y} . \tag{74}
\end{equation*}
$$

Here, $\omega_{x}, \omega_{y}$ and $\bar{\kappa}$ are constants.

## Appendix C: Equations of motion in a coupled storage ring

$\omega_{x}$ and $\omega_{y}$ are the betatron frequencies, given by:

$$
\begin{equation*}
\omega_{x, y}=\frac{1}{C} \int_{0}^{C} \frac{d s}{\beta_{x, y}} \tag{75}
\end{equation*}
$$

For reasons that will become clear shortly, we re-write the coupling term, to put the Hamiltonian in the form:

$$
\begin{equation*}
H=\omega_{x} J_{x}+\omega_{y} J_{y}-\bar{\kappa}_{-} \sqrt{J_{x} J_{y}} \cos \left(\phi_{x}-\phi_{y}\right)-\bar{\kappa}_{+} \sqrt{J_{x} J_{y}} \cos \left(\phi_{x}+\phi_{y}\right) \tag{76}
\end{equation*}
$$

The constants $\bar{\kappa}_{ \pm}$represent the skew quadrupole strength averaged around the ring. However, we need to take into account that the kick from a skew quadrupole depends on the betatron phase. Thus, we write:

$$
\begin{equation*}
\bar{\kappa}_{ \pm} e^{i \chi}=\frac{1}{C} \int_{0}^{C} e^{i\left(\mu_{x} \pm \mu_{y}\right)} k_{s} \sqrt{\beta_{x} \beta_{y}} d s \tag{77}
\end{equation*}
$$

where $\mu_{x}$ and $\mu_{y}$ are the betatron phase advances from the start of the ring.

Now suppose that $\bar{\kappa}_{-} \gg \bar{\kappa}_{+}$. (This can occur, for example, if $\omega_{x} \approx \omega_{y}$, in which case all the skew quadrupole perturbations will add together in phase.) Then, we can simplify things further by dropping the term in $\bar{\kappa}_{+}$ from the Hamiltonian:

$$
\begin{equation*}
H=\omega_{x} J_{x}+\omega_{y} J_{y}-\bar{\kappa}_{-} \sqrt{J_{x} J_{y}} \cos \left(\phi_{x}-\phi_{y}\right) \tag{78}
\end{equation*}
$$

We can now write down the equations of motion:

$$
\begin{align*}
\frac{d J_{x}}{d s} & =-\frac{\partial H}{\partial \phi_{x}}=\bar{\kappa}_{-} \sqrt{J_{x} J_{y}} \sin \left(\phi_{x}-\phi_{y}\right)  \tag{79}\\
\frac{d J_{y}}{d s} & =-\frac{\partial H}{\partial \phi_{y}}=-\bar{\kappa}_{-} \sqrt{J_{x} J_{y}} \sin \left(\phi_{x}-\phi_{y}\right)  \tag{80}\\
\frac{d \phi_{x}}{d s} & =\frac{\partial H}{\partial J_{x}}=\omega_{x}+\frac{\bar{\kappa}_{-}}{2} \sqrt{\frac{J_{x}}{J_{y}}} \cos \left(\phi_{x}-\phi_{y}\right)  \tag{81}\\
\frac{d \phi_{y}}{d s} & =\frac{\partial H}{\partial J_{y}}=\omega_{y}+\frac{\bar{\kappa}_{-}}{2} \sqrt{\frac{J_{y}}{J_{x}}} \cos \left(\phi_{x}-\phi_{y}\right) \tag{82}
\end{align*}
$$

Part 2: Emittance and Lattice Design

## Appendix C: Equations of motion in a coupled storage ring

Even after all the simplifications we have made, the equations of motion are still rather difficult to solve. Fortunately, however, we do not require the general solution. In fact, we are only interested in the properties of some special cases.

First of all, we note that the sum of the actions is constant:

$$
\begin{equation*}
\frac{d J_{x}}{d s}+\frac{d J_{y}}{d s}=0 \quad \therefore \quad J_{x}+J_{y}=\text { constant } \tag{83}
\end{equation*}
$$

This is true in all cases.
Going further, we notice that if $\phi_{x}=\phi_{y}$, then the rate of change of each action falls to zero, i.e.:

$$
\begin{equation*}
\text { if } \quad \phi_{x}=\phi_{y} \quad \text { then } \quad \frac{d J_{x}}{d s}=\frac{d J_{y}}{d s}=0 \tag{84}
\end{equation*}
$$

This implies that if we can find a solution to the equations of motion with $\phi_{x}=\phi_{y}$ for all $s$, then the actions will remain constant.

## Appendix C: Equations of motion in a coupled storage ring

From the equations of motion, we find that if:

$$
\begin{equation*}
\phi_{x}=\phi_{y} \quad \text { and } \quad \frac{d \phi_{x}}{d s}=\frac{d \phi_{y}}{d s} \tag{85}
\end{equation*}
$$

then:

$$
\begin{equation*}
\frac{J_{y}}{J_{x}}=\frac{\sqrt{1+\bar{\kappa}_{-}^{2} / \Delta \omega^{2}}-1}{\sqrt{1+\bar{\kappa}_{-}^{2} / \Delta \omega^{2}}+1} \tag{86}
\end{equation*}
$$

where $\Delta \omega=\omega_{x}-\omega_{y}$.
If we further use $J_{x}+J_{y}=J_{0}$, where $J_{0}$ is a constant, then we have the fixed point solution:

$$
\begin{align*}
& J_{x}=\frac{1}{2}\left(1+\frac{1}{\sqrt{1+\bar{\kappa}_{-}^{2} / \Delta \omega^{2}}}\right) J_{0}  \tag{87}\\
& J_{y}=\frac{1}{2}\left(1-\frac{1}{\sqrt{1+\bar{\kappa}_{-}^{2} / \Delta \omega^{2}}}\right) J_{0} \tag{88}
\end{align*}
$$

## Appendix C: Equations of motion in a coupled storage ring

Note the behaviour of the fixed-point actions as we vary the "coupling strength" $\bar{\kappa}_{-}$and the betatron tunes (betatron frequencies).

The fixed-point actions are well-separated for $\bar{\kappa}_{-} \ll \Delta \omega$, but approach each other for $\bar{\kappa}_{-} \gg \Delta \omega$.

The condition at which the tunes are equal (or differ by an exact integer) is known as the difference coupling resonance.


Recall that the emittance may be defined as the betatron action averaged over all particles in the beam:

$$
\begin{equation*}
\varepsilon_{x}=\left\langle J_{x}\right\rangle, \quad \text { and } \quad \varepsilon_{y}=\left\langle J_{y}\right\rangle . \tag{89}
\end{equation*}
$$

Now, synchrotron radiation will damp the beam towards an equilibrium distribution. In this equilibrium, we expect the betatron actions of the particles to change only slowly, i.e. on the timescale of the radiation damping, whis is much longer than the timescale of the betatron motion.

In that case, the actions of most particles must be in the correct ratio for a fixed-point solution to the equations of motion. Then, if we assume that $\varepsilon_{x}+\varepsilon_{y}=\varepsilon_{0}$, where $\varepsilon_{0}$ is the natural emittance of the storage ring, we must have for the equilibrium emittances:

$$
\begin{align*}
& \varepsilon_{x}=\frac{1}{2}\left(1+\frac{1}{\sqrt{1+\bar{\kappa}_{-}^{2} / \Delta \omega^{2}}}\right) \varepsilon_{0}  \tag{90}\\
& \varepsilon_{y}=\frac{1}{2}\left(1-\frac{1}{\sqrt{1+\bar{\kappa}_{-}^{2} / \Delta \omega^{2}}}\right) \varepsilon_{0} \tag{91}
\end{align*}
$$

Hence, we have shown equation (34).
Part 2: Emittance and Lattice Design

## Appendix D: Tune shifts from skew quadrupole perturbations

To estimate the effect of a skew quadrupole perturbation on the betatron tunes, we use the Hamiltonian (78). If we consider a particle close to the fixed point solution, we can assume that $\phi_{x}=\phi_{y}$, so that the Hamiltonian becomes:

$$
\begin{equation*}
H=\omega_{x} J_{x}+\omega_{y} J_{y}-\bar{\kappa}_{-} \sqrt{J_{x} J_{y}} . \tag{92}
\end{equation*}
$$

The normal modes describe motion that is periodic with a single well-defined frequency. In the absence of coupling, the transverse normal modes correspond to motion in just the horizontal or vertical plane. When coupling is present, the normal modes involve combination of horizontal and vertical motion.

Let us write the Hamiltonian (92) in the form:

$$
H=\left(\begin{array}{ll}
\sqrt{J_{x}} & \sqrt{J_{y}}
\end{array}\right) A\binom{\sqrt{J_{x}}}{\sqrt{J_{y}}}, \text { where } A=\left(\begin{array}{cc}
\omega_{x} & -\frac{1}{2} \bar{\kappa}_{-}  \tag{93}\\
-\frac{1}{2} \bar{\kappa}_{-} & \omega_{y}
\end{array}\right) .
$$

The normal modes can be constructed from the eigenvectors of the matrix $A$, and the frequency of each mode is given by the corresponding eigenvalue.

From the eigenvalues of $A$, we find that the normal mode frequencies are:

$$
\begin{equation*}
\omega_{ \pm}=\frac{1}{2}\left(\omega_{x}+\omega_{y} \pm \sqrt{\bar{\kappa}_{-}^{2}+\Delta \omega^{2}}\right) . \tag{94}
\end{equation*}
$$

The envelope method for computing the beam emittances is based on finding the equilibrium distribution described by the "Sigma matrix" (the matrix of second order moments of the dynamical variables):

$$
\Sigma=\left(\begin{array}{cccccc}
\left\langle x^{2}\right\rangle & \left\langle x p_{x}\right\rangle & \langle x y\rangle & \left\langle x p_{y}\right\rangle & \langle x z\rangle & \langle x \delta\rangle  \tag{95}\\
\left\langle p_{x} x\right\rangle & \left\langle p_{x}^{2}\right\rangle & \left\langle p_{x} y\right\rangle & \left\langle p_{x} p_{y}\right\rangle & \left\langle p_{x} z\right\rangle & \left\langle p_{x} \delta\right\rangle \\
\langle y x\rangle & \left\langle y p_{x}\right\rangle & \left\langle y^{2}\right\rangle & \left\langle y p_{y}\right\rangle & \langle y z\rangle & \langle y \delta\rangle \\
\left\langle p_{y} x\right\rangle & \left\langle p_{y} p_{x}\right\rangle & \left\langle p_{y} y\right\rangle & \left\langle p_{y}^{2}\right\rangle & \left\langle p_{y} z\right\rangle & \left\langle p_{y} \delta\right\rangle \\
\langle z x\rangle & \left\langle z p_{x}\right\rangle & \langle z y\rangle & \left\langle z p_{y}\right\rangle & \left\langle z^{2}\right\rangle & \langle z \delta\rangle \\
\langle\delta x\rangle & \left\langle\delta p_{x}\right\rangle & \langle\delta y\rangle & \left\langle\delta p_{y}\right\rangle & \langle\delta z\rangle & \left\langle\delta^{2}\right\rangle
\end{array}\right) .
$$

This can be conveniently written as:

$$
\begin{equation*}
\Sigma_{i j}=\left\langle x_{i} x_{j}\right\rangle, \tag{96}
\end{equation*}
$$

where $\Sigma_{i j}$ is the $(i, j)$ component of the Sigma matrix, and the set $x_{i}$ (for $i=1 \ldots 6$ ) are the dynamical variables. The brackets $\langle\cdot\rangle$ indicate an average over all particles in the bunch.

In the absence of coupling, the sigma matrix will be block diagonal. We are interested in the more general case, where coupling is present.

Appendix E: The envelope method for computing emittances

The emittances and the lattice functions can be calculated from the sigma matrix, and vice-versa.

Consider the (simpler) case of motion in one degree of freedom. The sigma matrix in this case is:

$$
\Sigma=\left(\begin{array}{cc}
\left\langle x^{2}\right\rangle & \left\langle x p_{x}\right\rangle  \tag{97}\\
\left\langle p_{x} x\right\rangle & \left\langle p_{x}^{2}\right\rangle
\end{array}\right)=\left(\begin{array}{cc}
\beta_{x} & -\alpha_{x} \\
-\alpha_{x} & \gamma_{x}
\end{array}\right) \varepsilon_{x} .
$$

Note that given a Sigma matrix, we can compute the emittance as follows. First, define the matrix $S$ :

$$
S=\left(\begin{array}{cc}
0 & 1  \tag{98}\\
-1 & 0
\end{array}\right)
$$

Then, the eigenvalues of $\Sigma S$ are $\pm i \varepsilon_{x}$. (The proof of this is left as an exercise.)

Now, we can show that (under certain assumptions) the emittance is conserved as a bunch is transported along a beam line.

The linear transformation in phase space coordinates of a particle in the bunch between two points in the beam line can be represented by a matrix M:

$$
\begin{equation*}
\binom{x}{p_{x}} \mapsto M\binom{x}{p_{x}} . \tag{99}
\end{equation*}
$$

If (for the moment) we neglect radiation and certain other effects, and consider only the Lorentz force on particles from the external electromagnetic fields, then the transport is symplectic.

Physically, this means that the phase-space volume of the bunch is conserved as the bunch moves along the beam line.

Mathematically, it means that $M$ is a symplectic matrix, i.e. $M$ satisfies:

$$
\begin{equation*}
M^{\top} S M=S \tag{100}
\end{equation*}
$$

Part 2: Emittance and Lattice Design

Appendix E: The envelope method for computing emittances

Now consider how the Sigma matrix transforms. Since it is written as the product of the phase-space coordinates averaged over the bunch, we have:

$$
\begin{equation*}
\binom{x}{p_{x}} \mapsto M\binom{x}{p_{x}}, \quad \therefore \quad \Sigma \mapsto M \Sigma M^{\top} . \tag{101}
\end{equation*}
$$

Since $S$ is a constant matrix, it immediately follows that:

$$
\begin{equation*}
\Sigma S \mapsto M \Sigma M^{\top} S \tag{102}
\end{equation*}
$$

Then, using the fact that $M$ is symplectic, we have:

$$
\begin{equation*}
\Sigma S \mapsto M \Sigma S M^{-1} \tag{103}
\end{equation*}
$$

This is a similarity transformation of $\Sigma S$ : the eigenvalues of any matrix are conserved under a similarity transformation. Therefore, since the eigenvalues of $\Sigma S$ give the emittance of the bunch, it follows that the emittances are conserved under linear, symplectic transport.

The above discussion immediately generalises to three degrees of freedom.
We define the matrix $S$ in three degrees of freedom by:

$$
\S=\left(\begin{array}{cccccc}
0 & 1 & 0 & 0 & 0 & 0  \tag{104}\\
-1 & 0 & 0 & 0 & 0 & 0 \\
0 & 0 & 0 & 1 & 0 & 0 \\
0 & 0 & -1 & 0 & 0 & 0 \\
0 & 0 & 0 & 0 & 0 & 1 \\
0 & 0 & 0 & 0 & -1 & 0
\end{array}\right)
$$

The six eigenvalues of $\Sigma S$ are then:

$$
\begin{equation*}
\pm i \varepsilon_{x}, \quad \pm i \varepsilon_{y}, \quad \pm i \varepsilon_{z} \tag{105}
\end{equation*}
$$

These quantities are all conserved under linear, symplectic transport.
Even if, as is generally the case, the Sigma matrix is not block-diagonal (i.e. if there is coupling present), then we can still find three invariant emittances using this method, without any modification.

Part 2: Emittance and Lattice Design

## Appendix E: The envelope method for computing emittances

If $M$ is a matrix that represents the linear single-turn transformation at some point in a storage ring, then an invariant or "matched" distribution is one that satisfies:

$$
\begin{equation*}
\Sigma \mapsto M \Sigma M^{\top}=\Sigma \tag{106}
\end{equation*}
$$

(In general, all the particles in the bunch change position in phase space after one turn around the ring: but for a matched distribution, the second order moments remain the same.)

This is not sufficient to determine the beam emittances - though this condition will determine the lattice functions (which can be found from the eigenvectors of $\Sigma S$ ).

In other words, the matched distribution condition determines the shape of the bunch, but not the size of the bunch. This makes sense: after all, in a proton storage ring, we can have a matched bunch of any emittance.

However, in an electron storage ring, we know that radiation effects will damp the emittances to some equilibrium values.

We shall now show how to apply the concept of a matched distribution, when radiation effects are included, to find the equilibrium emittances in an electron storage ring.

In an electron storage ring, we must make two modifications to the single-turn transformation to account for radiation effects:

1. The matrix $M$ will no longer be symplectic: this accounts for radiation damping.
2. As well as first-order terms in the transformation (represented by the matrix $M$ ), there will be zeroth-order terms: these will turn out to correspond to the quantum excitation.

The condition for a matched distribution should then be written:

$$
\begin{equation*}
\Sigma=M \Sigma M^{\top}+D, \tag{107}
\end{equation*}
$$

where $M$ and $D$ are constant, non-symplectic matrices that represent the first-order and zeroth-order terms in the single-turn transformation, respectively.

This equation is sufficient to determine the Sigma matrix uniquely - in other words, using just this equation (with known $M$ and $D$ ) we can find the bunch emittances and the matched lattice functions.

Part 2: Emittance and Lattice Design

## Appendix E: The envelope method for computing emittances

The envelope method for finding the equilibrium emittances in a storage ring consists of three steps:

1. Find the first-order terms $M$ and zeroth-order terms $D$ in the single-turn transformation:

$$
\begin{equation*}
\Sigma \mapsto M \Sigma M^{\top}+D . \tag{108}
\end{equation*}
$$

2. Use the matching condition:

$$
\begin{equation*}
\Sigma=M \Sigma M^{\top}+D, \tag{109}
\end{equation*}
$$

to determine the Sigma matrix.
3. Find the equilibrium emittances from the eigenvalues of $\Sigma S$.

Note: strictly speaking, since $M$ is not symplectic, the emittances are not invariant as the bunch moves around the ring. Therefore, we may expect to find a different emittance at each point around the ring. However, if radiation effects are fairly small, then the variations in the emittances will also be small.

As an illustration of the transformation matrices $M$ and $D$, we shall consider a thin "slice" of a dipole.

The thin slice of dipole is an important case:

- in most storage rings, radiation effects are only significant in dipoles;
- "complete" dipoles can be constructed by concatenating the maps for a number of slices.

Once we have a map for a thin slice of dipole, we simply need to concatenate the maps for all the elements in the ring, to construct the map for a complete turn starting at any point.

## Appendix E: The envelope method for computing emittances

Recall that the transformation for the phase space variables in the emission of radiation carrying momentum $d p$ is:

$$
\begin{array}{ccc}
x \mapsto x & y \mapsto y & z \mapsto z \\
p_{x} \mapsto\left(1-\frac{d p}{P_{0}}\right) p_{x} & p_{y} \mapsto\left(1-\frac{d p}{P_{0}}\right) p_{y} & \delta \mapsto \delta-\frac{d p}{P_{0}} \tag{110}
\end{array}
$$

where $P_{0}$ is the reference momentum. In general, $d p$ is a function of the coordinates.

To find the transformation matrices $M$ and $D$, we find an explicit expression for $d p / P_{0}$, and then write down the above transformations to first order.

