



# **Penning transfers:**

## **survey of available data, life-time of excited states, pressure dependence**

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# Introduction

## ➤ Mixtures used in proportional counters:

Ne, Ar, He .... + Methane, Ethane, Isobutane ...

## ➤ Non-ionising interactions:

UV photons emitted from excited states

## ➤ High gas gains (up to $10^6$ ):

before reaching a continuous discharge

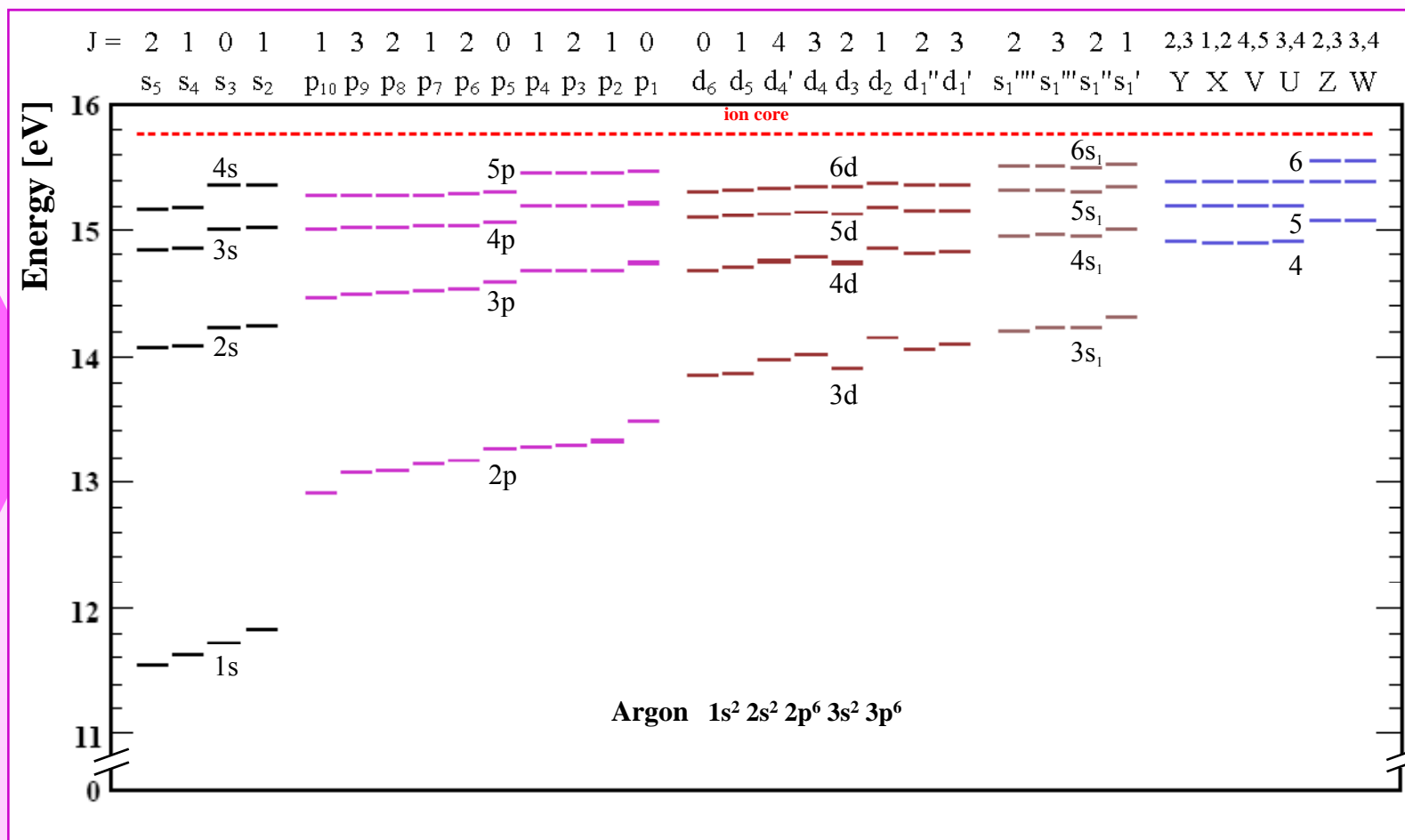
# Penning effect

- **Excited noble gas atoms can transfer their energy:**  
if they do not decay before collisions !!!
- **Excitation energy > ionisation energy of admixture:**
- **Number of the generated electron-ion pairs increase:**  
low  $W$  and  $F$  in the mixtures  
improvement in the detector energy resolution

# Investigated Penning gas mixtures

- 1- Argon – Ethane
- 2- Argon – Isobutane
- 3- Argon – Propane
- 4- Argon – Methane
- 5- Argon – Acetylene
- 6- Argon – CO<sub>2</sub>
- 7- Argon – Xenon

# Schematic view of the energy levels for Argon I



# Methodology

➤ A computer program has been developed:  
single wire proportional counter

➤ Gas gain:

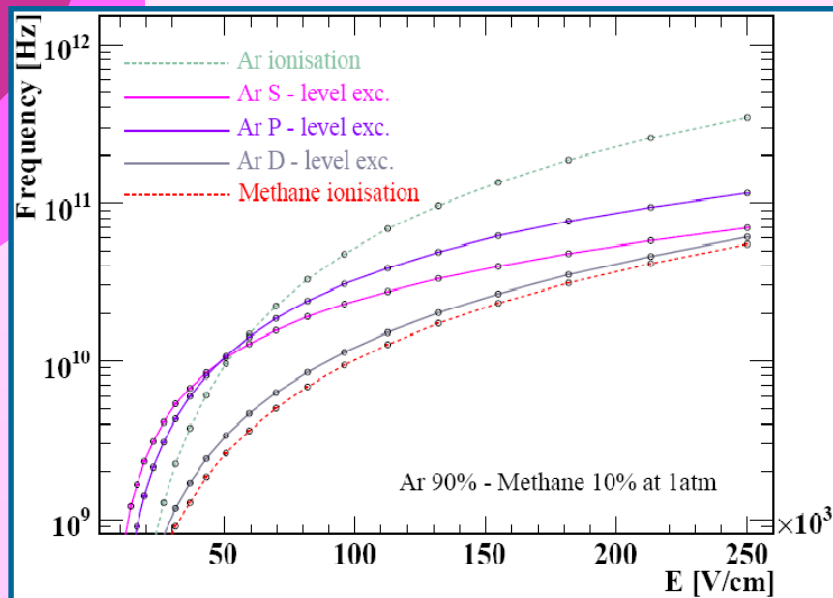
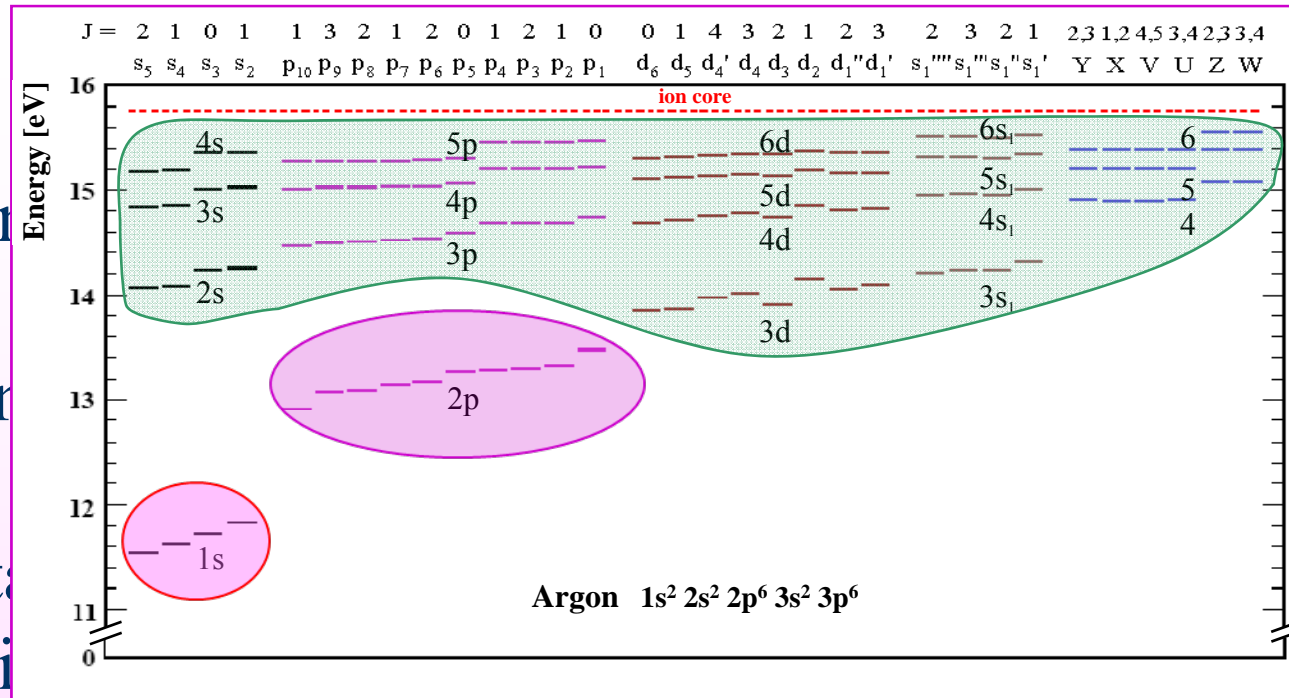
$$G = e^{\int_{r_a}^{r_b} \alpha(E(r)) * dr}$$

➤ Electric field strength  $E(r)$  at the radius  $r$  :

$$E(r) = \frac{V}{r \log(r_a / r_c)}$$

# Magboltz:

- To find Townsend
- Magboltz does not
- But, it gives detailed level structure and ionisations



S - level exc. (11.55 eV)  $\longrightarrow$  1s excited levels

P - level exc. (13.0 eV)  $\longrightarrow$  2p excited levels

D - level exc. (14.0 eV)  $\longrightarrow$  combinations of s, p, d excited levels

# $\alpha_{\text{Penning}}$

Using this information a *Penning-corrected* ionization coefficient ( $\alpha_{\text{Penning}}$ ) for *all energetically allowed* Penning transfers can be given by:

$$\alpha_{\text{Penning}} = \alpha \frac{(f_{\text{ion(Ar)}} + f_{\text{ion(admix.)}} + \sum_i (P(i) * f_{\text{exc\_Ar}}(i)))}{(f_{\text{ion(Ar)}} + f_{\text{ion(admix.)}})}$$

Here Penning transfer probability P is defined as the fraction of the energy in the excited states that will cause further ionisations by the Penning processes.

Since this energy transfer fraction is *a priori not known*, the experimental data are used as a guide. P is found by a fitting procedure that achieves the matching between the gains calculated from  $\alpha_{\text{Penning}}$  and the measured gains.

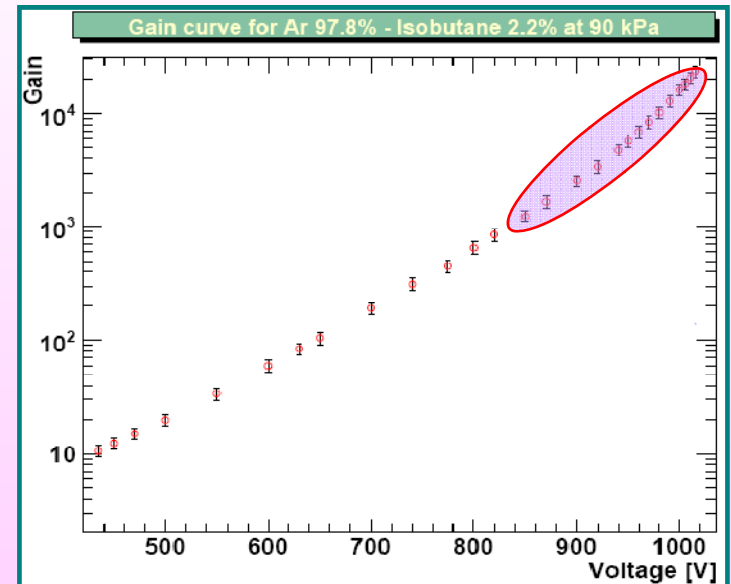


# Photon feedback term

- **Over-exponential growth at high potentials:**  
secondary avalanches due to insufficient quenching of UV photons

- $G_{\text{total}}$  :  
including photon feedback

$$G_{\text{tot}} = \frac{G}{1 - P_{\gamma} * G}$$



$P_{\gamma}$  is the probability that an ionisation in the primary avalanche produces a photon which leads to a secondary avalanche.

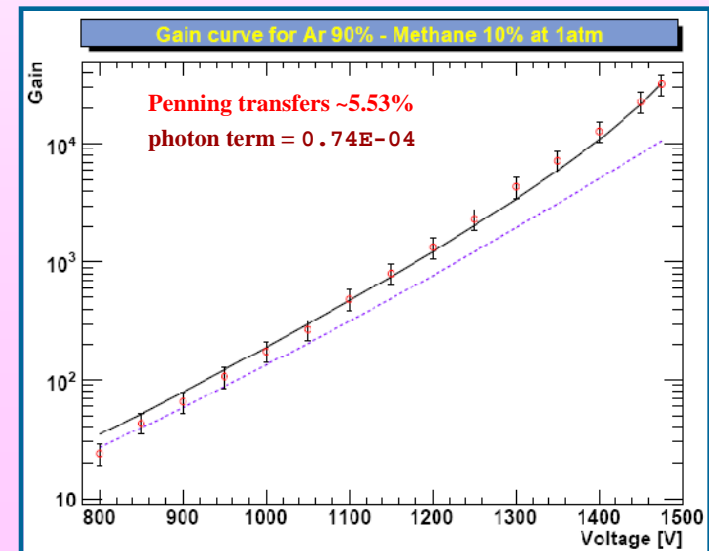
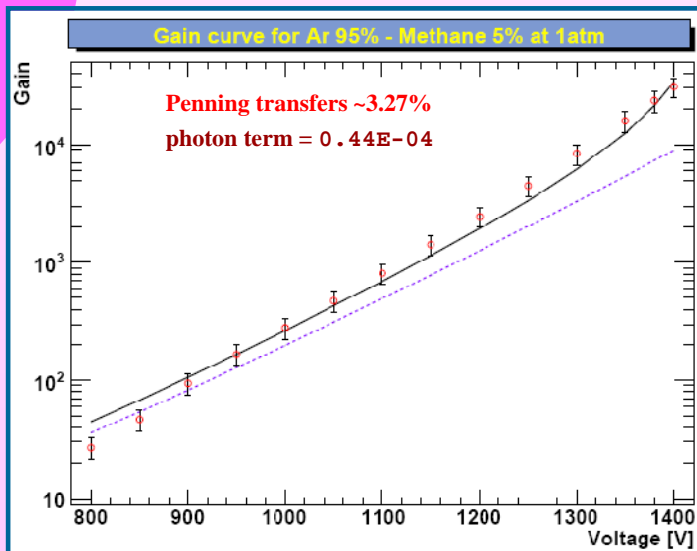
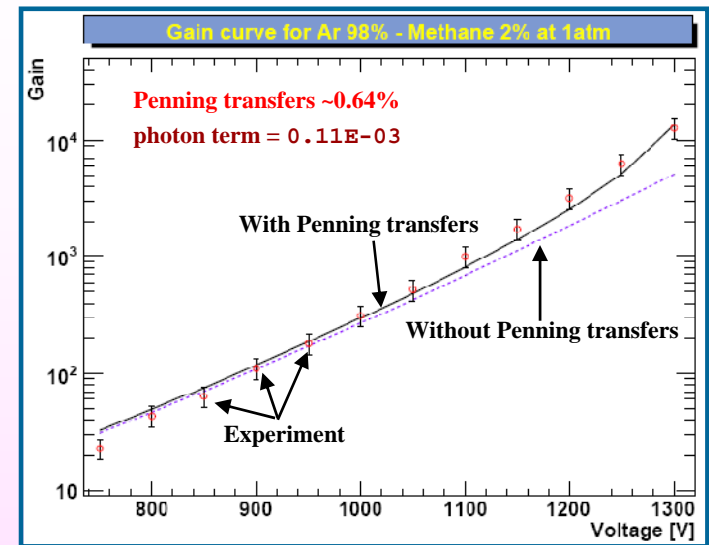
# Argon – Methane mixtures

$$I_{\text{Methane}} = 12.99 \text{ eV}$$

Possible Penning Transfers:



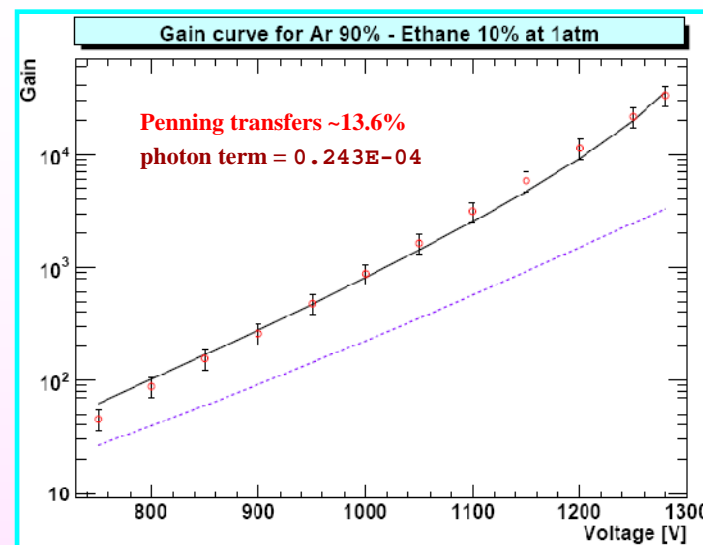
Ar + 2%, 5%, 10% Methane



# Argon – Ethane mixture

$$I_{\text{Ethane}} = 11.52 \text{ eV}$$

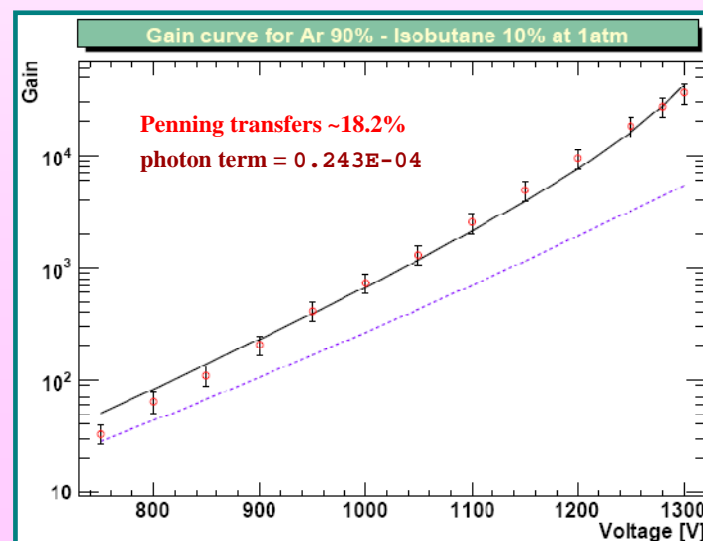
Possible Penning Transfers:



# Argon – Isobutane mixture

$$I_{\text{Isobutane}} = 10.67 \text{ eV}$$

Possible Penning Transfers:



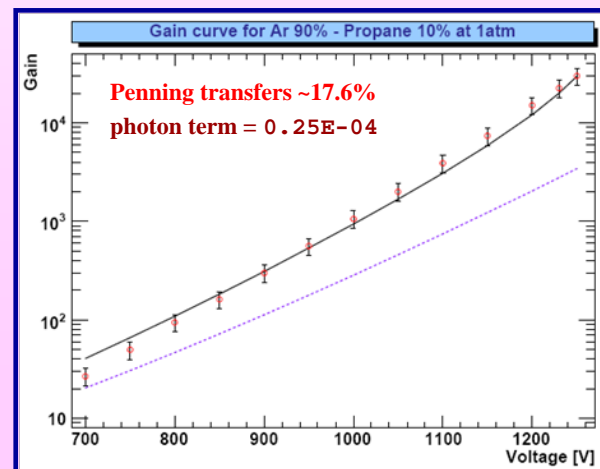
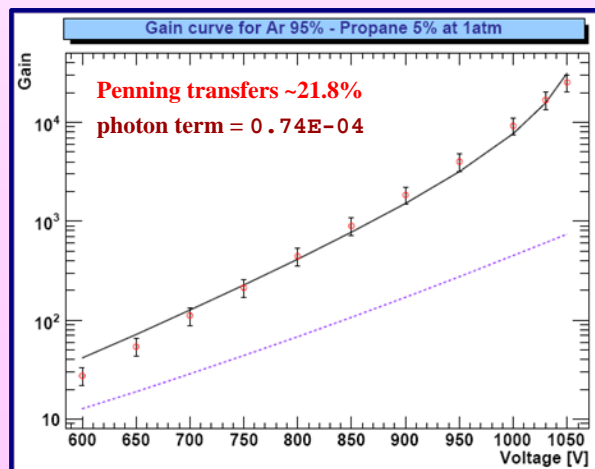
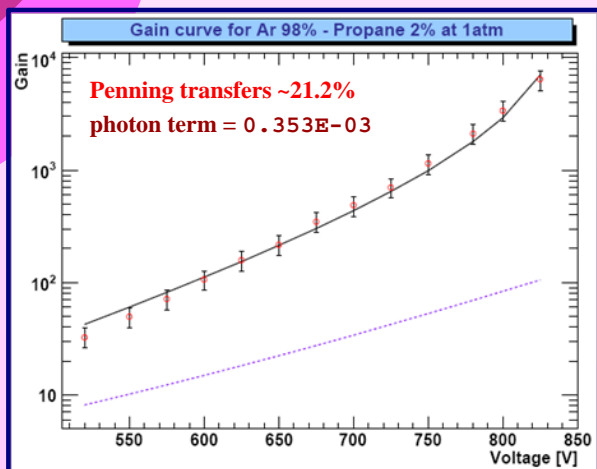
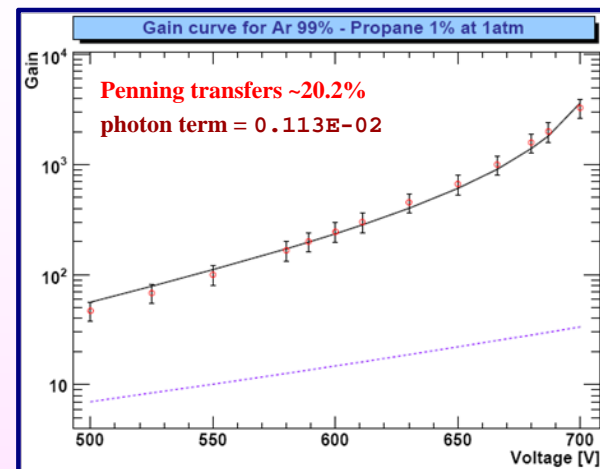
# Argon – Propane mixtures

$$I_{\text{Propane}} = 10.95 \text{ eV}$$

Possible Penning Transfers:



Ar + 1%, 2%, 5%, %10 Propane



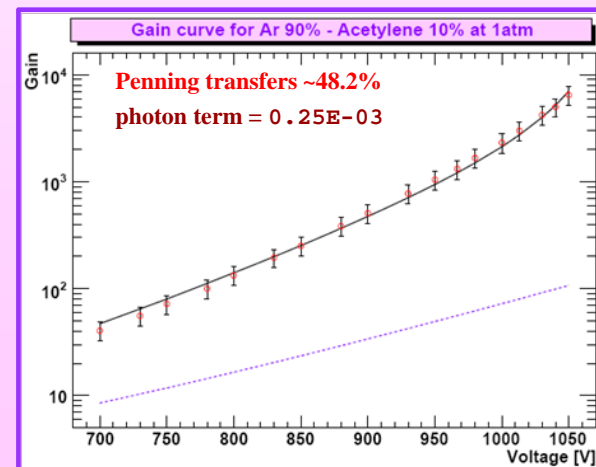
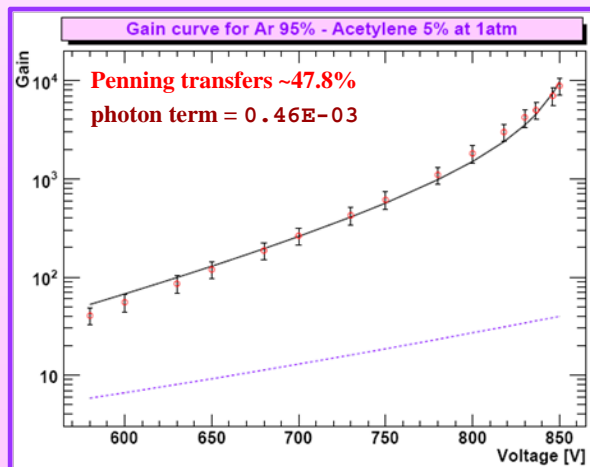
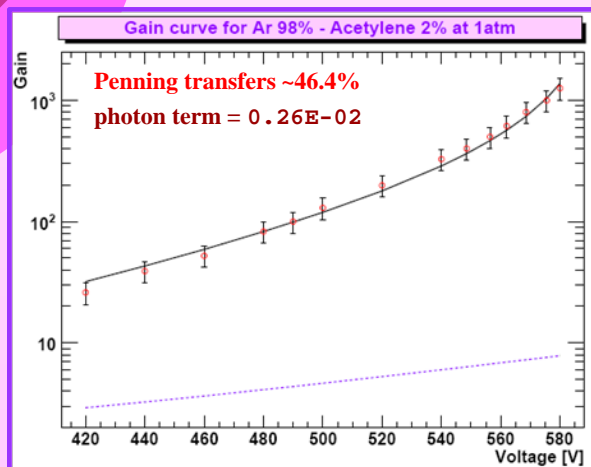
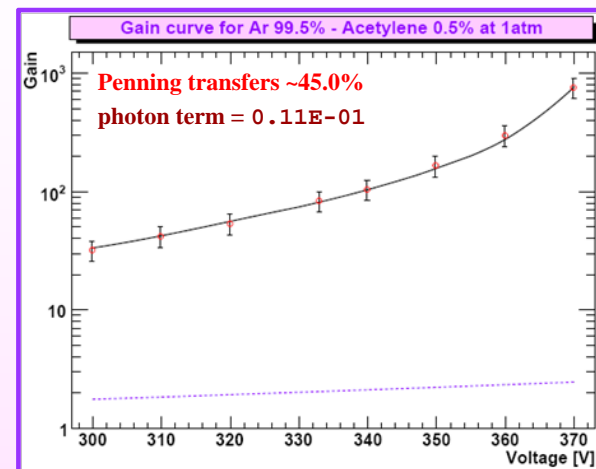
# Argon – Acetylene mixtures

$$I_{\text{Acetylene}} = 11.42 \text{ eV}$$

Possible Penning Transfers:



Ar + 0.5%, 2%, 5%, 10% Acetylene



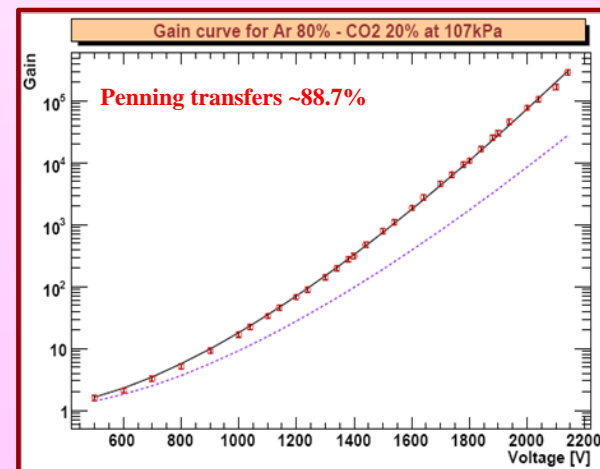
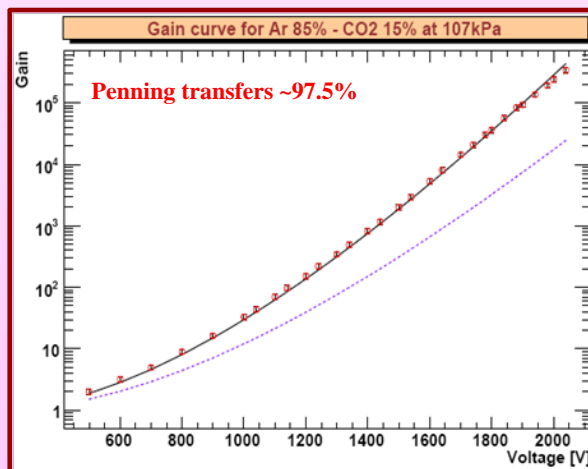
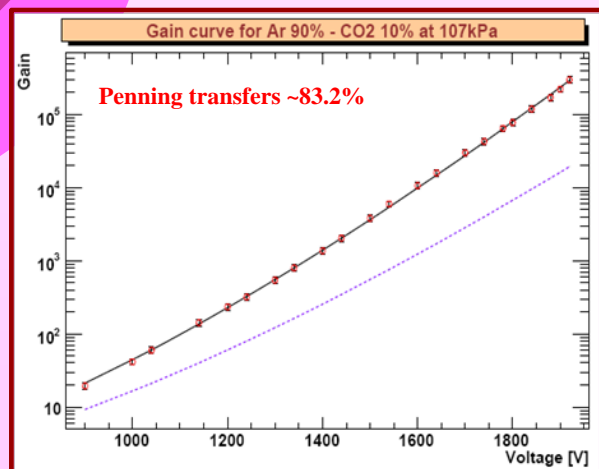
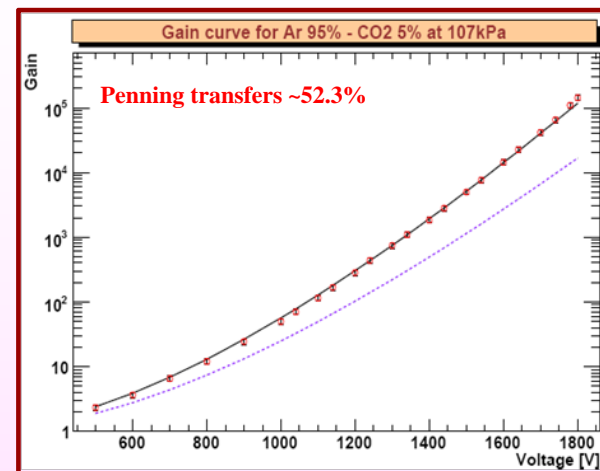
# Argon – CO<sub>2</sub> mixtures

$$I_{\text{CO}_2} = 13.77 \text{ eV}$$

Possible Penning Transfers:

Ar\* (only D level exc.)  $\longrightarrow$  CO<sub>2</sub>

Ar + 5%, 10%, 15%, 20% CO<sub>2</sub>



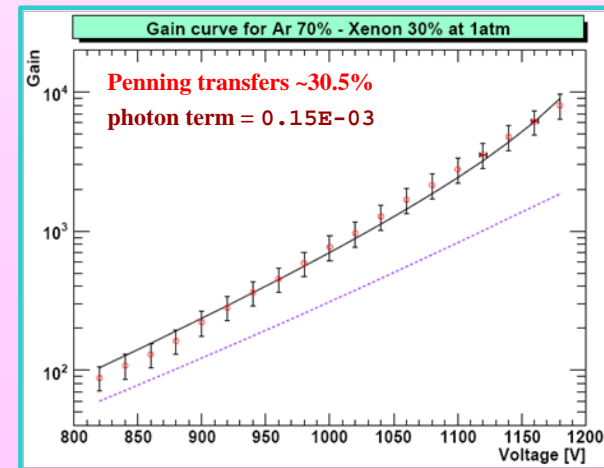
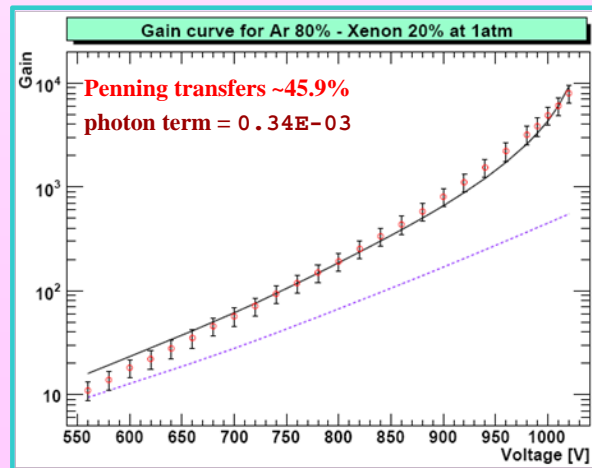
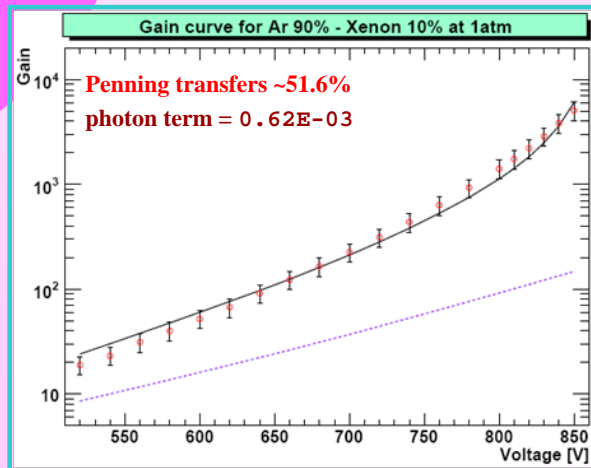
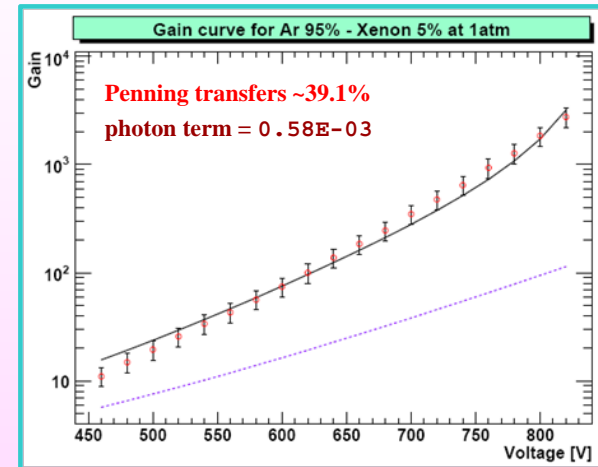
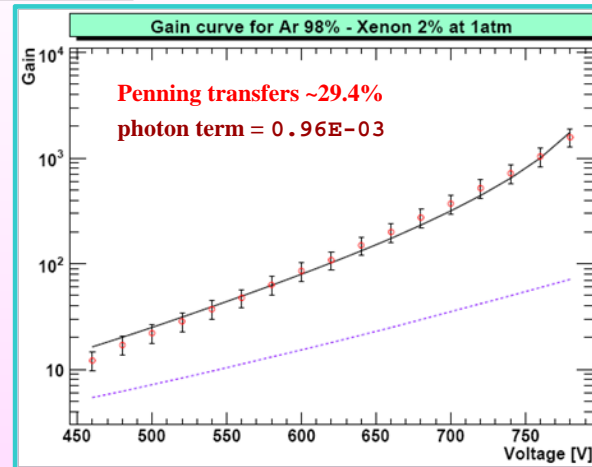
# Argon – Xenon mixtures

$$I_{\text{Xenon}} = 12.13 \text{ eV}$$

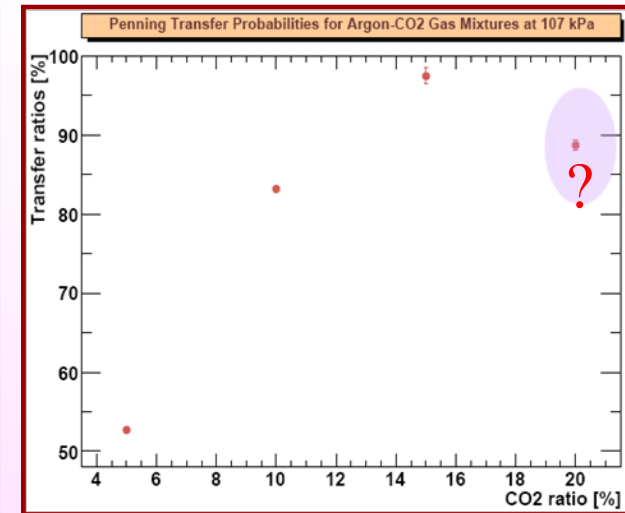
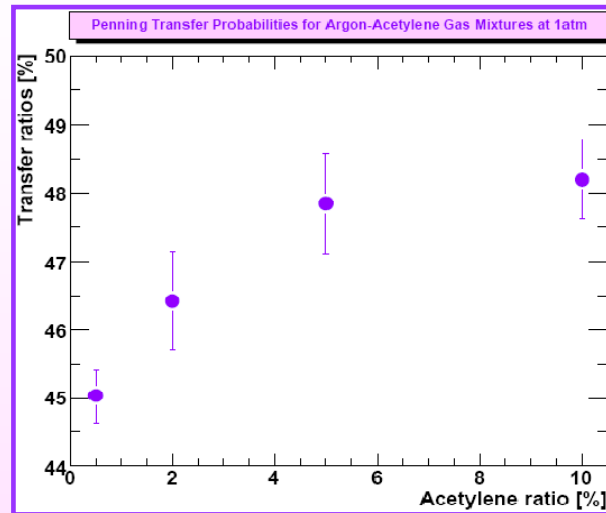
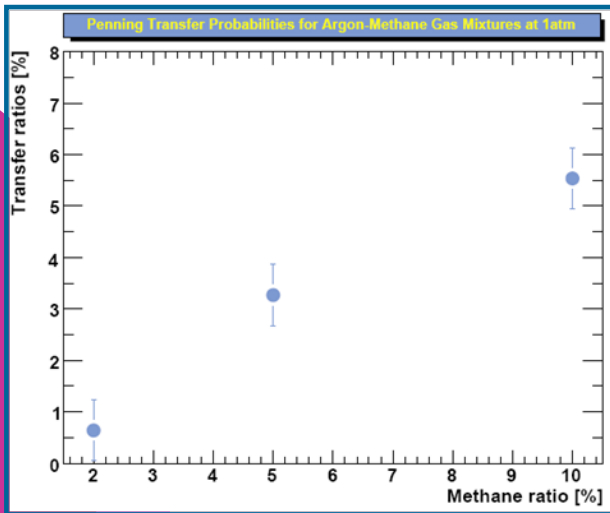
Possible Penning Transfers:



Ar + 5%, 10%, 15%, 20% Xe



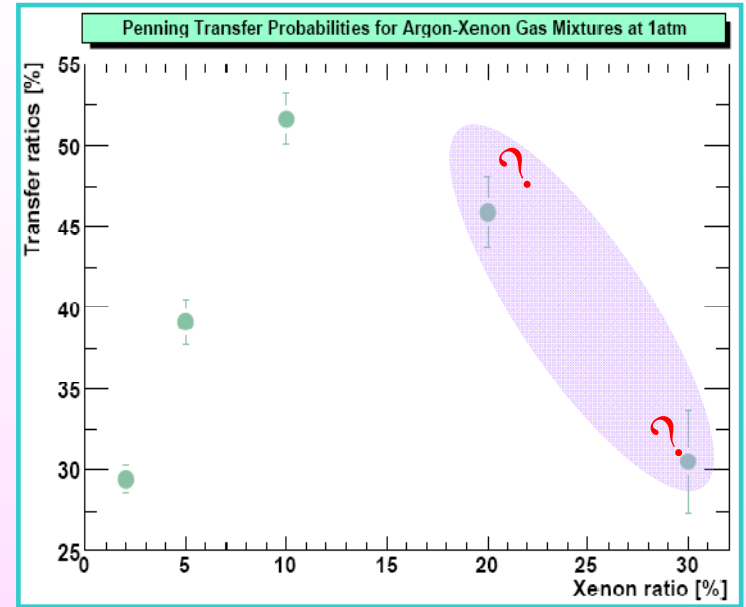
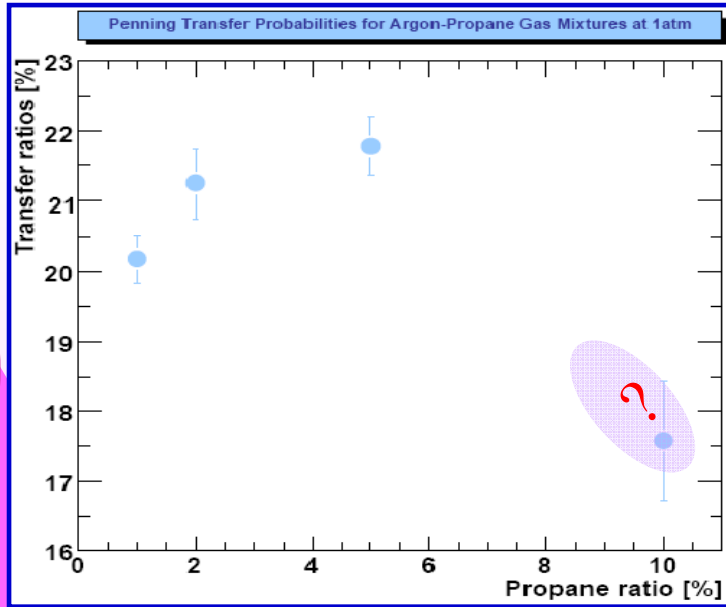
# Concentration dependence



- Probabilities increase with increasing percentage of the admixture.
  - High probabilities for Acetylene mixtures.
  - The highest probabilities for CO<sub>2</sub> admixtures ?
  - Decrease for 20% CO<sub>2</sub> concentration ?
- } **X sections ?**



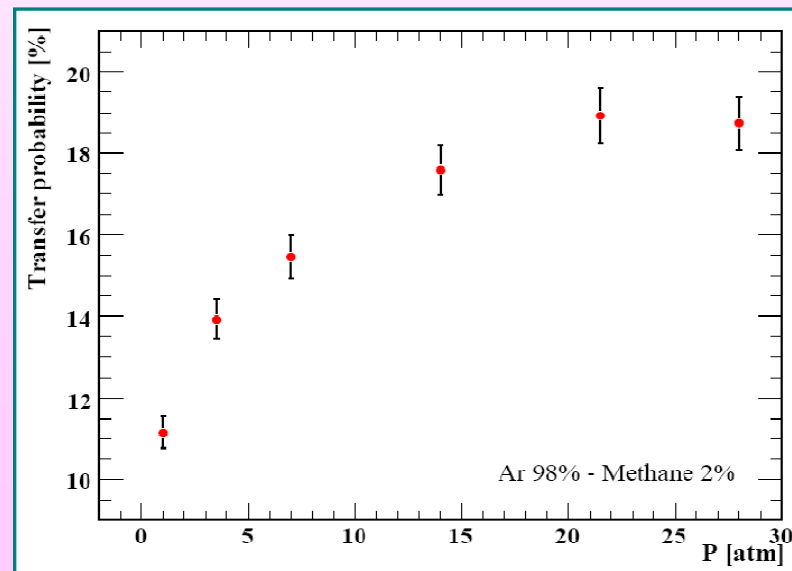
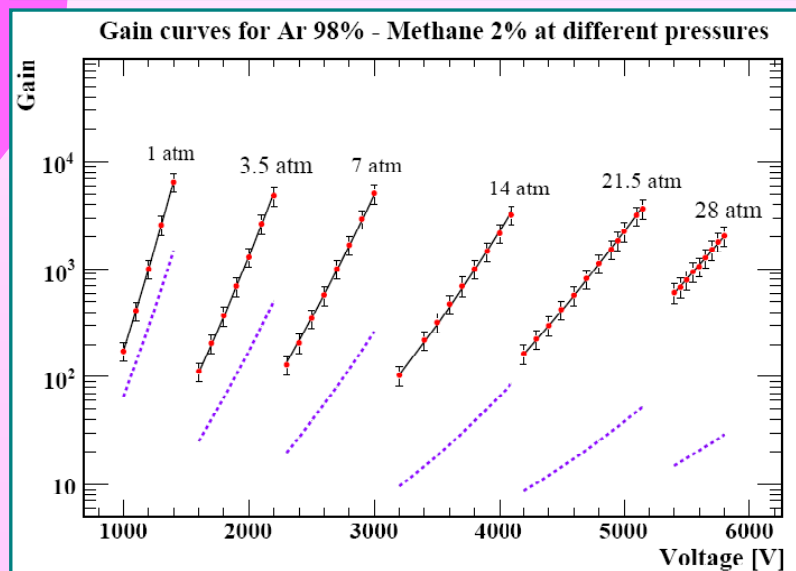
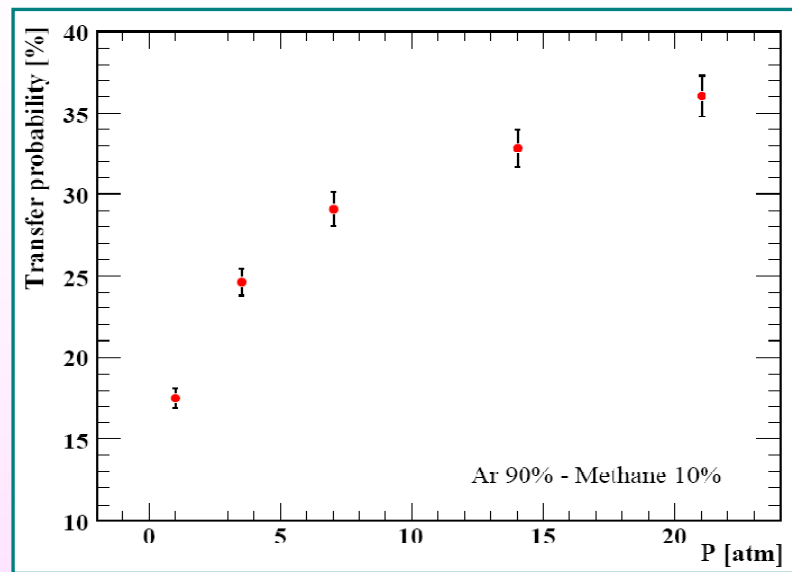
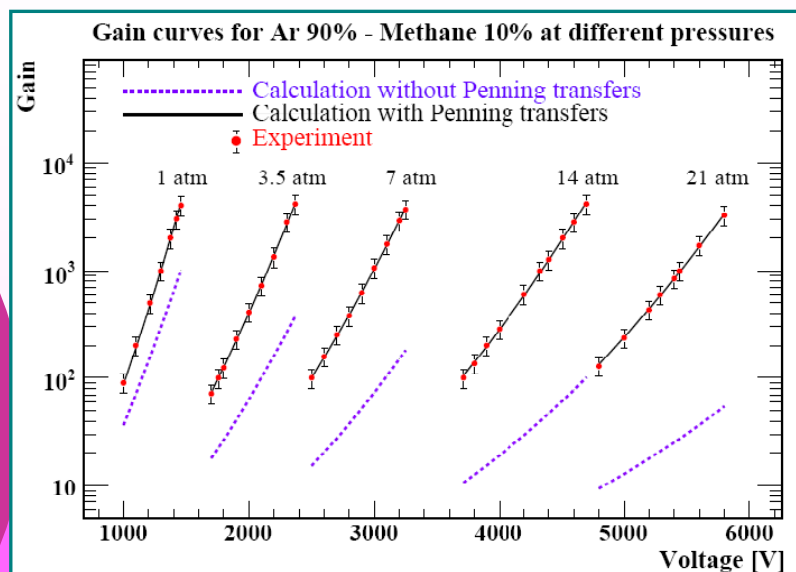
# Concentration dependence (continue)



- Decrease for 10% Propane concentration ?
- High probabilities for Xe admixtures ?
- Decrease for 20% and 30% Xe concentrations ?

**X sections ?**

# Pressure dependence



# Pressure dependence (continue)

- Since the time between collisions decreases by increasing pressure, the number of ionising collisions with excited argon atoms increases. As a consequence, the Penning transfer probabilities increase at higher pressures.
- We assume that the transfer probability is related to the chance that an excited atom (or molecule) meets a recipient before it decays spontaneously in the  $t_{\text{decay}}$  time.
- We are trying to find correct fit function for pressure dependence.
- We have already calculated mean collision times  $t_{\text{coll}}$  of argon with investigated admixtures (*from kinetic theory*).
- We have also extracted the decay modes and lifetimes for each excited state of argon (*using approximately 40 papers published in this topic*).

# Lifetime of the excited states

Levels		Energy [eV]	Lifetimes [ns]	
jK	Paschen		Experimental	Theoretical
4s (3/2) <sub>1</sub>	1s <sub>4</sub>	11.624	8.44 <sup>a</sup>	8.60 <sup>a</sup>
4s' (1/2) <sub>1</sub>	1s <sub>2</sub>	11.828	2.14 <sup>a</sup>	2.15 <sup>a</sup>
4p (1/2) <sub>1</sub>	2p <sub>10</sub>	12.907	32.4 <sup>b</sup>	32.2 <sup>c</sup>
4p (5/2) <sub>3</sub>	2p <sub>9</sub>	13.076	25.3 <sup>b</sup>	25.2 <sup>c</sup>
4p (5/2) <sub>2</sub>	2p <sub>8</sub>	13.095	26.8 <sup>b</sup>	27.0 <sup>c</sup>
4p (3/2) <sub>1</sub>	2p <sub>7</sub>	13.153	24.8 <sup>b</sup>	25.8 <sup>c</sup>
4p (3/2) <sub>2</sub>	2p <sub>6</sub>	13.172	24.4 <sup>b</sup>	25.3 <sup>c</sup>
4p (1/2) <sub>0</sub>	2p <sub>5</sub>	13.273	21.6 <sup>b</sup>	22.0 <sup>c</sup>
4p' (3/2) <sub>1</sub>	2p <sub>4</sub>	13.283	26.4 <sup>b</sup>	26.0 <sup>c</sup>
4p' (3/2) <sub>2</sub>	2p <sub>3</sub>	13.302	25.0 <sup>b</sup>	25.5 <sup>c</sup>
4p' (1/2) <sub>1</sub>	2p <sub>2</sub>	13.328	24.2 <sup>b</sup>	24.8 <sup>c</sup>
4p' (1/2) <sub>0</sub>	2p <sub>1</sub>	13.480	19.5 <sup>b</sup>	18.5 <sup>c</sup>
3d (1/2) <sub>0</sub>	3d <sub>6</sub>	13.845	-----	54.2 <sup>a</sup>
3d (1/2) <sub>1</sub>	3d <sub>5</sub>	13.864	94.0 <sup>a</sup>	40.8 <sup>a</sup>
3d (7/2) <sub>4</sub>	3d <sub>4</sub> '	13.979	72.0 <sup>d</sup>	52.0 <sup>a</sup>
3d (7/2) <sub>3</sub>	3d <sub>4</sub>	14.013	55.0 <sup>d</sup>	50.8 <sup>a</sup>
3d (3/2) <sub>2</sub>	3d <sub>3</sub>	13.903	3.48 <sup>a</sup>	57.6 <sup>a</sup>
3d (3/2) <sub>1</sub>	3d <sub>2</sub>	14.153	40.0 <sup>d</sup>	9.0 <sup>a</sup>
3d (5/2) <sub>2</sub>	3d <sub>1</sub> "	14.063	68.0 <sup>d</sup>	49.9 <sup>a</sup>
3d (5/2) <sub>3</sub>	3d <sub>1</sub> '	14.099	54.0 <sup>d</sup>	49.0 <sup>a</sup>
3d' (5/2) <sub>2</sub>	3s <sub>1</sub> "	14.214	51.9 <sup>e</sup>	49.9 <sup>a</sup>
3d' (5/2) <sub>3</sub>	3s <sub>1</sub> "	14.236	-----	49.7 <sup>a</sup>
3d' (3/2) <sub>2</sub>	3s <sub>1</sub> "	14.234	49.9 <sup>e</sup>	48.3 <sup>a</sup>
3d' (3/2) <sub>1</sub>	3s <sub>1</sub> '	14.304	53.3 <sup>e</sup>	3.36 <sup>a</sup>

5s (3/2) <sub>2</sub>	2s <sub>3</sub>	14.068	-----	42.1 <sup>a</sup>
5s (3/2) <sub>1</sub>	2s <sub>4</sub>	14.090	17.5 <sup>a</sup>	4.74 <sup>a</sup>
5s' (1/2) <sub>0</sub>	2s <sub>3</sub>	14.241	61.0 <sup>d</sup>	43.9 <sup>a</sup>
5s' (1/2) <sub>1</sub>	2s <sub>2</sub>	14.255	10.1 <sup>a</sup>	3.2 <sup>a</sup>
5p (1/2) <sub>1</sub>	3p <sub>10</sub>	14.464	170.0 <sup>f</sup>	166.0 <sup>f</sup>
5p (5/2) <sub>3</sub>	3p <sub>9</sub>	14.499	150.0 <sup>f</sup>	122.0 <sup>f</sup>
5p (5/2) <sub>2</sub>	3p <sub>8</sub>	14.506	165.0 <sup>f</sup>	129.0 <sup>f</sup>
5p (3/2) <sub>1</sub>	3p <sub>7</sub>	14.525	170.0 <sup>f</sup>	109.0 <sup>f</sup>
5p (3/2) <sub>2</sub>	3p <sub>6</sub>	14.529	175.0 <sup>f</sup>	192.0 <sup>f</sup>
5p (1/2) <sub>0</sub>	3p <sub>5</sub>	14.588	95.0 <sup>f</sup>	73.0 <sup>f</sup>
5p' (3/2) <sub>1</sub>	3p <sub>4</sub>	14.681	180.0 <sup>f</sup>	127.0 <sup>f</sup>
5p' (3/2) <sub>2</sub>	3p <sub>3</sub>	14.688	175.0 <sup>f</sup>	123.0 <sup>f</sup>
5p' (1/2) <sub>1</sub>	3p <sub>2</sub>	14.687	170.0 <sup>f</sup>	123.0 <sup>f</sup>
5p' (1/2) <sub>0</sub>	3p <sub>1</sub>	14.738	80.0 <sup>f</sup>	83.0 <sup>f</sup>
4d (1/2) <sub>0</sub>	4d <sub>9</sub>	14.694	120.0 <sup>g</sup>	124.0 <sup>g</sup>
4d (1/2) <sub>1</sub>	4d <sub>8</sub>	14.711	74.0 <sup>a</sup>	113.0 <sup>a</sup>
4d (7/2) <sub>4</sub>	4d <sub>4</sub> '	14.757	226.0 <sup>g</sup>	230.0 <sup>g</sup>
4d (7/2) <sub>3</sub>	4d <sub>4</sub>	14.781	285.0 <sup>g</sup>	297.0 <sup>g</sup>
4d (3/2) <sub>2</sub>	4d <sub>3</sub>	14.743	147.0 <sup>g</sup>	384.0 <sup>g</sup>
4d (3/2) <sub>1</sub>	4d <sub>2</sub>	14.859	200.0 <sup>h</sup>	234.0 <sup>i</sup>
4d (5/2) <sub>2</sub>	4d <sub>1</sub> "	14.809	360.0 <sup>f</sup>	348.0 <sup>f</sup>
4d (5/2) <sub>3</sub>	4d <sub>1</sub> '	14.834	350.0 <sup>f</sup>	335.0 <sup>f</sup>
4d' (5/2) <sub>2</sub>	4s <sub>1</sub> "	14.955	295.0 <sup>f</sup>	275.0 <sup>f</sup>
4d' (5/2) <sub>3</sub>	4s <sub>1</sub> "	14.972	310.0 <sup>g</sup>	317.0 <sup>g</sup>
4d' (3/2) <sub>2</sub>	4s <sub>1</sub> "	14.953	223.0 <sup>g</sup>	259.0 <sup>g</sup>
4d' (3/2) <sub>1</sub>	4s <sub>1</sub> '	15.004	71.9 <sup>h</sup>	3.78 <sup>a</sup>

# Lifetime of the excited states (continue)

Levels jK	Paschen	Energy [eV]	Lifetimes [ns]	
			Experimental	Theoretical
6s (3/2) <sub>2</sub>	3s <sub>5</sub>	14.839	72.0 <sup>f</sup>	92.0 <sup>f</sup>
6s (3/2) <sub>1</sub>	3s <sub>4</sub>	14.848	-----	5.73 <sup>a</sup>
6s' (1/2) <sub>0</sub>	3s <sub>3</sub>	15.014	75.0 <sup>f</sup>	90.0 <sup>f</sup>
6s' (1/2) <sub>1</sub>	3s <sub>2</sub>	15.022	-----	32.6 <sup>a</sup>
4f (5/2) <sub>2,3</sub>	4Y <sub>2,3</sub>	14.907	-----	47.0 <sup>a</sup> - 51.0 <sup>a</sup>
4f (7/2) <sub>1,2</sub>	4X <sub>1,2</sub>	14.902	-----	43.3 <sup>a</sup> - 48.3 <sup>a</sup>
4f (9/2) <sub>4,5</sub>	4V <sub>4,5</sub>	14.904	-----	46.9 <sup>a</sup> - 45.4 <sup>a</sup>
4f (7/2) <sub>3,4</sub>	4U <sub>3,4</sub>	14.909	-----	49.3 <sup>a</sup> - 49.6 <sup>a</sup>
4f' (5/2) <sub>2,3</sub>	4Z <sub>2,3</sub>	15.083	-----	46.6 <sup>a</sup> - 50.5 <sup>a</sup>
4f' (7/2) <sub>3,4</sub>	4W <sub>3,4</sub>	15.083	-----	46.7 <sup>a</sup> - 47.6 <sup>a</sup>
6p (1/2) <sub>1</sub>	4p <sub>10</sub>	15.011	324.0 <sup>f</sup>	325.0 <sup>f</sup>
6p (5/2) <sub>3</sub>	4p <sub>9</sub>	15.023	282.0 <sup>i</sup>	276.0 <sup>a</sup>
6p (5/2) <sub>2</sub>	4p <sub>8</sub>	15.026	266.0 <sup>j</sup>	284.0 <sup>j</sup>
6p (3/2) <sub>1</sub>	4p <sub>7</sub>	15.034	280.0 <sup>j</sup>	296.0 <sup>j</sup>
6p (3/2) <sub>2</sub>	4p <sub>6</sub>	15.036	257.7 <sup>i</sup>	257.0 <sup>i</sup>
6p (1/2) <sub>0</sub>	4p <sub>5</sub>	15.060	171.0 <sup>f</sup>	151.0 <sup>f</sup>
6p' (3/2) <sub>1</sub>	4p <sub>4</sub>	15.202	-----	263.0 <sup>a</sup>
6p' (3/2) <sub>2</sub>	4p <sub>3</sub>	15.205	255.2 <sup>j</sup>	256.0 <sup>j</sup>
6p' (1/2) <sub>1</sub>	4p <sub>2</sub>	15.201	266.7 <sup>j</sup>	250.0 <sup>j</sup>
6p' (1/2) <sub>0</sub>	4p <sub>1</sub>	15.224	190.0 <sup>f</sup>	197.0 <sup>f</sup>
5d (1/2) <sub>0</sub>	5d <sub>6</sub>	15.101	116.0 <sup>g</sup>	127.0 <sup>g</sup>
5d (1/2) <sub>1</sub>	5d <sub>5</sub>	15.118	73.2 <sup>h</sup>	111.0 <sup>a</sup>

5d (7/2) <sub>4</sub>	5d <sub>4</sub> '	15.131	255.0 <sup>g</sup>	218.0 <sup>g</sup>
5d (7/2) <sub>3</sub>	5d <sub>4</sub>	15.146	320.0 <sup>g</sup>	337.0 <sup>g</sup>
5d (3/2) <sub>2</sub>	5d <sub>3</sub>	15.137	205.0 <sup>g</sup>	437.0 <sup>g</sup>
5d (3/2) <sub>1</sub>	5d <sub>2</sub>	15.190	-----	2.69
5d (5/2) <sub>2</sub>	5d <sub>1</sub> "	15.161	330.0 <sup>g</sup>	582.0 <sup>g</sup>
5d (5/2) <sub>3</sub>	5d <sub>1</sub> '	15.167	475.0 <sup>g</sup>	592.0 <sup>g</sup>
5d' (5/2) <sub>2</sub>	5s <sub>1</sub> ""	15.313	227.0 <sup>g</sup>	235.0 <sup>g</sup>
5d' (5/2) <sub>3</sub>	5s <sub>1</sub> '''	15.319	247.0 <sup>g</sup>	275.0 <sup>g</sup>
5d' (3/2) <sub>2</sub>	5s <sub>1</sub> ''	15.296	134.0 <sup>g</sup>	146.0 <sup>g</sup>
5d' (3/2) <sub>1</sub>	5s <sub>1</sub> '	15.351	87.8 <sup>h</sup>	0.97 <sup>a</sup>
7s (3/2) <sub>2</sub>	4s <sub>5</sub>	15.181	133.3 <sup>i</sup>	99.3 <sup>a</sup>
7s (3/2) <sub>1</sub>	4s <sub>4</sub>	15.185	59.7 <sup>i</sup>	15.1 <sup>a</sup>
7s' (1/2) <sub>0</sub>	4s <sub>3</sub>	15.358	-----	99.2 <sup>a</sup>
7s' (1/2) <sub>1</sub>	4s <sub>2</sub>	15.359	38.8 <sup>i</sup>	15.7 <sup>a</sup>
7p (3/2) <sub>2</sub>	5p <sub>6</sub>	15.285	367.2 <sup>i</sup>	-----
7p (1/2) <sub>0</sub>	5p <sub>5</sub>	15.298	309.1 <sup>i</sup>	-----
6d (1/2) <sub>0</sub>	6d <sub>6</sub>	15.308	167.0 <sup>g</sup>	162.0 <sup>g</sup>
6d (1/2) <sub>1</sub>	6d <sub>5</sub>	15.313	281.4 <sup>k</sup>	-----
6d (7/2) <sub>4</sub>	6d <sub>4</sub> '	15.331	297.0 <sup>g</sup>	267.0 <sup>g</sup>
6d (7/2) <sub>3</sub>	6d <sub>4</sub>	15.346	500.0 <sup>g</sup>	572.0 <sup>g</sup>
6d (5/2) <sub>3</sub>	6d <sub>1</sub> '	15.353	295.0 <sup>g</sup>	803.0 <sup>g</sup>
6d' (5/2) <sub>2</sub>	6s <sub>1</sub> ""	15.512	295.0 <sup>g</sup>	299.0 <sup>g</sup>
6d' (3/2) <sub>2</sub>	6s <sub>1</sub> ''	15.506	210.0 <sup>g</sup>	224.0 <sup>g</sup>
8s (3/2) <sub>2</sub>	5s <sub>5</sub>	-----	256.0 <sup>i</sup>	-----
7d (1/2) <sub>0</sub>	7d <sub>6</sub>	15.439	116.2 <sup>h</sup>	-----
7d (1/2) <sub>1</sub>	7d <sub>5</sub>	15.443	212.0 <sup>k</sup>	-----
7d (7/2) <sub>4</sub>	7d <sub>4</sub> '	15.450	353.0 <sup>g</sup>	363.0 <sup>g</sup>
7d (7/2) <sub>3</sub>	7d <sub>4</sub>	15.455	309.7 <sup>h</sup>	-----



***Thank you ...***