## Feedback on quench heaters versus energy extraction on HL corrector magnets

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## Introduction

- Following recommendations from the HL-LHC Magnet Circuits Review, energy extraction is under discussion for a number of corrector circuits as an alternative to quench heaters:
- Orbit correctors in IT (MCBXFA/B)
- Super-ferric quadrupole in IT (MQSXF)
- Orbit correctors in D2 (MCBRD)
- As a decision has not yet been taken for these circuits, a strategy for all them is due for the development work within the upcoming months


## The MCBXF magnet

## CIEMAT collaboration

- CERN project engineer: J. C. Perez

| Magnet | Units | MCBXFB |  | MCBXFA |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  <br> Outer Dipole (OD) parameters |  | ID | OD | ID | OD |
| Nominal field (Stand-alone) | T | 2.11 | 2.23 | 2.11 | 2.23 |
| Nominal Field (Combined) | T | 3.07 |  | 3.07 |  |
| Nominal current | A | 1630 | 1490 | 1530 | 1395 |
| Coil peak field | T | 4.1 (ID) |  | 3.9 (ID) |  |
| Working point | \% | 50.1 (ID) |  | 47 (ID) |  |
| Static self-inductance (nominal current) | mH | 59.2 | 134.8 | 108.5 | 247 |
| Magnetic stored energy (nom. Current) | kJ | 78.6 | 149.6 | 127 | 240.3 |
| Aperture | mm | 156 | 230 | 156 | 230 |
| Iron yoke Inner Diameter | mm | 316 |  | 316 |  |
| Iron yoke Outer Diameter | mm | 614 |  | 614 |  |
| Total number of turns | - | 140 | 191 | 140 | 191 |
| Cable length needed for each pole/coil | m | 357 | 481 | 637 | 863 |
| Turns per block in inner layer | - | 50/10/11 | 45/39/21 | 50/10/11 | 45/39/21 |
| Turns per block in outer layer | - | 28/28/13 | 43/38/5 | 28/28/13 | 43/38/5 |
|  |  | Ciomme |  |  | Rodrigue |

## Protection

- Energy extraction on crowbar
- at the limit for protection of the long magnet
- Results from simulations:
- Here 50 V assumed, i.e. resistance of $30 \mathrm{~m} \Omega$
- One gets 410 K at $108 \%$ of nominal ...

| Hot spot <br> temperatures <br> (K) | Magnet type | Combined <br> powering | Stand-alone <br> powering |
| :---: | :---: | :---: | :---: |
| Inner dipole | Short | 196 | 220 |
|  | Long | 267 | $\mathbf{3 0 5}$ |
| Outer dipole | Short | 232 | 260 |
|  | Long | $\mathbf{3 1 1}$ | $\mathbf{3 5 5}$ |

## Simulation features

- Some features are not modelled:
- The vertical transverse thermal conductivity is not properly modelled due to the spacers (optimistic).
- Quench-back is not included, but it is not likely to help because the current decay is slow (pessimistic).
- Adiabatic boundary conditions (pessimistic).
- AC losses in nearby metallic parts are not included (pessimistic).
- An approximate field map is used.
- Uncertainty about material properties (mainly resin and Nomex).


## Heaters in short prototype

- Decision is taken, that the ongoing short prototype will be equipped with heaters on blocks 4 \& 5:
- To be on the safe side.
- To check the assembly feasibility.
- To ease assembly of internal voltage taps.



## Protection strategy

- Heaters will be explored
- The coil is impregnated, hence the heater will be impregnated with the coil
- The presence of double collaring implies difficulties, so if an energy extraction with reasonable cost is available this would reduce the risk
- We should consequently also explore energy extraction at 100 V or larger voltage

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## Energy Extraction Systems

TE/MPE is now envisaging the following alternatives in order to propose solutions in the 1 to 2 kA range:

- as a by-product of the large effort put in place for the manufacturing of 7.5 kA , IGBT-modules for SM18, IGBT-based systems have been designed also for these lower currents and a prototype is under construction with minor additional efforts
- an Addendum is being prepared with the Łodz University of Technology (PL) - existing Framework Agreement- as to study and possibly develop energy extraction systems based on vacuum switches with different commutation techniques


## HL-LHC EE (some) alternatives



Bipolar 1 kA, IGBT-based system developed by MPE/EE (two basic modules).

Crossing through zero is not a trivial issue in this case (to be further discussed with EPC)


Switch system based on natural commutation, as developed by the Łodz University of Technology


3kV Vacuum circuit breakers family, 250, 400, 800 A for electrical railway traction vehicles (ŁUT, Łodz, Poland)

## Quench Heater Discharge Supplies (HDS)

- The plan is to use the same units as the ones existing for LHC
- Bipolar $\pm 450 \mathrm{~V}, 7.05 \mathrm{mF}$
- High reliability shown during years of LHC operation (around 1/mil/year)
- Time for switching of thyristors in conduction has to be reduced to 1 ms from 4 to 5 ms at present
- Relays to be replaced by solid-state devices
- Units have been sent to KEK and similar ones are being used at FNAL for the tests of the models and prototypes



## EE vs QH comparison

## Quench heater

- Intrusive element in magnet structure
Low maintenance
- Heaters cost about 2 kCHF/meter of magnet
- Power supply costs about 5 kCHF/unit (to this, cost of QH + wiring is to be added)
High availability
- Connections to be consolidated
Development costs (?)
Less space (19", 6U) (x 2 units/magnet?)

Energy extraction

- External element
- Yearly maintenance (if mechanical)
- Permanent losses (if IGBT)
- EE system costs about 32 kCHF/unit - based on IGBT systems
- High availability

Development costs (estimated to 200kCHF)
Space is one full rack/system (700x900x2000mm)

## Summary of conclusions

- Heaters will be used on the first model
- Important feedback on the magnet manufacturing
- Test results will allow to refine the model
- Contribution of AC losses and quench back
- Maybe the extraction at 50 V (crow-bar) is enough
- Extraction on larger voltages (larger resistance, above $50 \mathrm{~m} \Omega$ ) should continue to be explored
- This implies energy extraction external to crow-bar
- TE/MPE will proceed with development on the different axis
- Then (end of 2017) a decision will be taken for MCBXF
- Same strategy to be applied to the other magnets


## Many thanks for your attention!

