Diagnostic of coherent transition radiation for measuring microbunch formation in AWAKE

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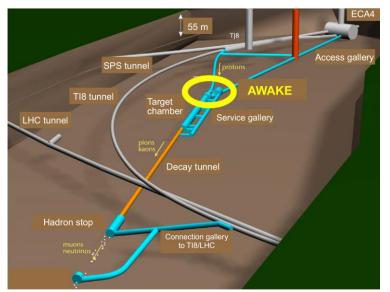
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Paris
LA³Net – Novel Accelerators





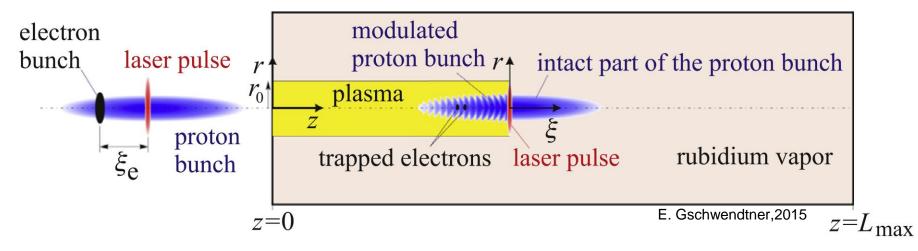


Outline

- The Self-Modulation Instability (SMI)
- TR and CTR basics
- CTR from Self-Modulation Instability (SMI) in AWAKE
- Overview of CTR-diagnostics
- Frequency-analysis with heterodyne measurement
 - Outlook



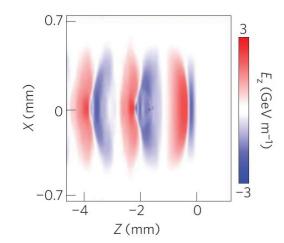
Self-modulation instability (SMI)

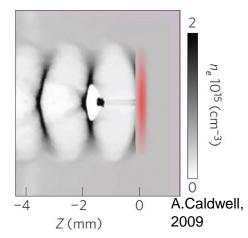


Reducing 12 cm bunch to micro-bunches:

Self-modulation Instability

radially modulated bunch density, with plasma-wavelength



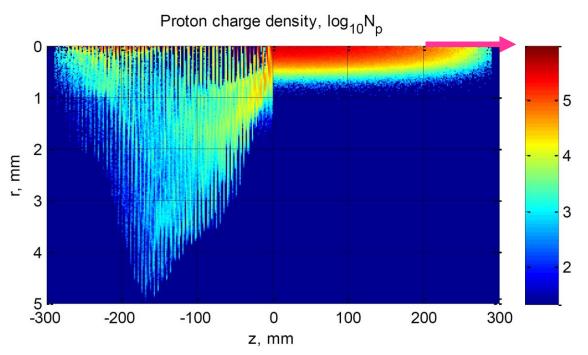


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Indirect Measurement of SMI

Analyze p+-bunch with microbunch-train after plasma cell



3 Methods:

- Measurement of bunch-size on scintillating screen
- Optical transition radiation: direct signal from each proton
- Coherent transition radiation: Measure electric field component from charge density modulation





Transition radiation

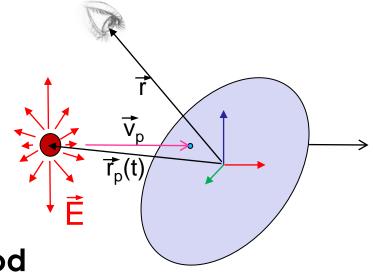
Relativistic particles incident on metallic / dielectric surface

→ Radiation from induced surface-currents

Approaches (e.g.):

- Virtual photon method
- Surface-current method

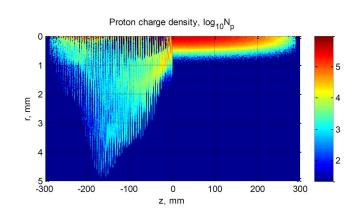
Investigate effects of near-field and finite screen







AWAKE CTR-simulations



Using p+-distribution from beam-plasma PIC-simulation Summing up fields of each p⁺

Proton-bunch modulated at plasma wavelength

CTR-signal at plasma frequency

COHERENT transition radiation:

Vary Plasma density between n=10¹⁴ cm⁻³ and n=10¹⁵ cm⁻³

→ Plasma frequency between

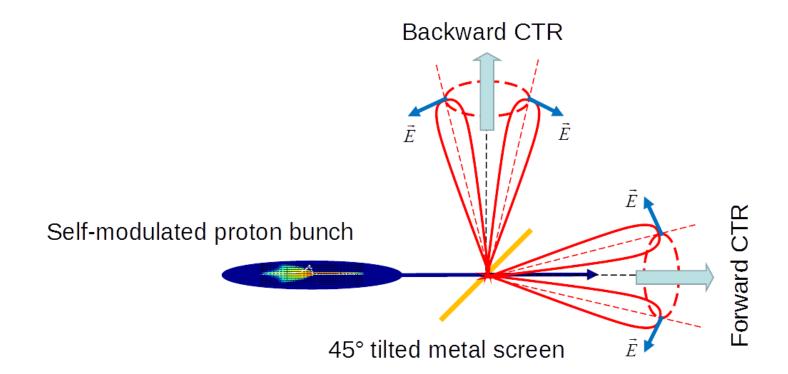
$$f_{plasma}$$
 = 90GHz and

$$f_{plasma} = 300GHz$$
.





Coherent Transition radiation



Self-modulation Instability

- → radially modulated bunch density
- → Radially polarized CTR-electric field





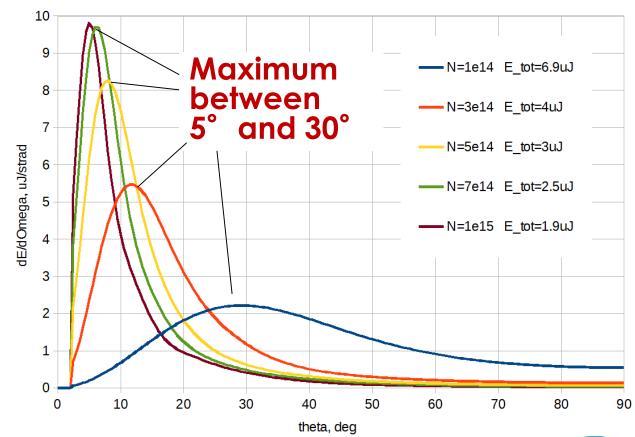
CTR-signal from SMI

Simulation of CTR-radiation in AWAKE:

- Ginzburg-Frank
- Surface current method.

At angle much larger than $1/\gamma$!

Angular CTR-energy distribution





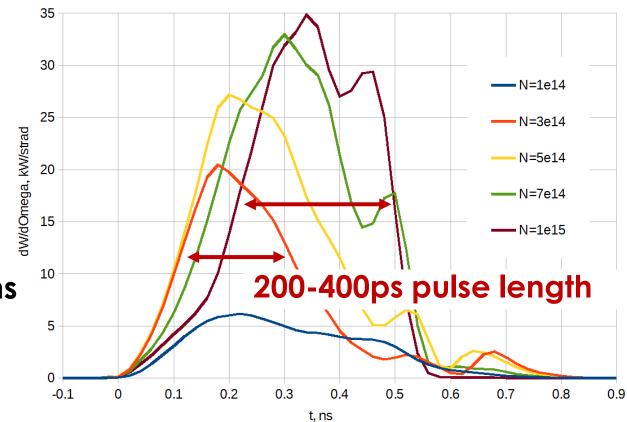


CTR from SMI in AWAKE

Temporary evolution of CTR-pulse

Strong signal: $\sim 5-30$ kW/strad at angle $\theta(E_{max})$

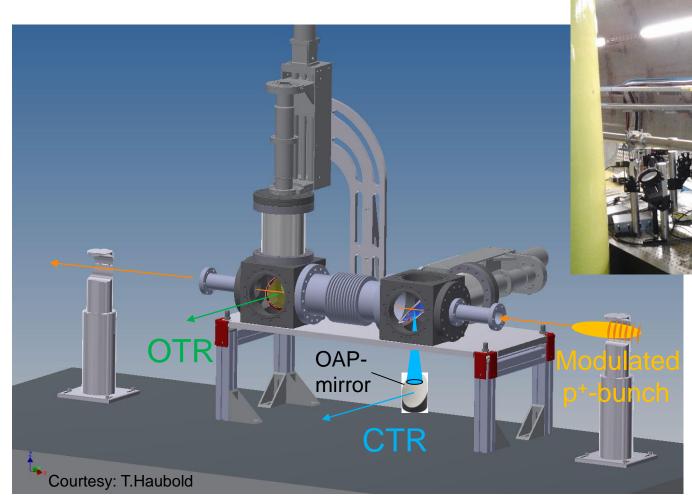
Short pulse with ~50-100 oscillations at 90-300GHz





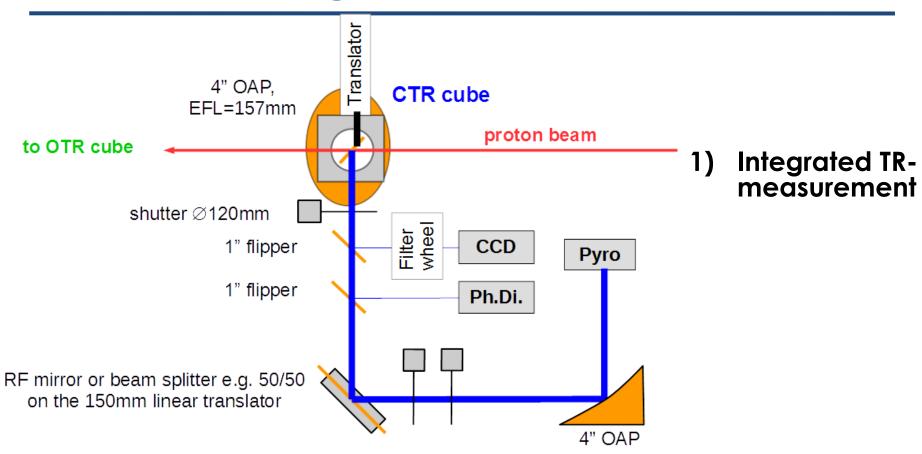


Diagnostics for SMI-CTR

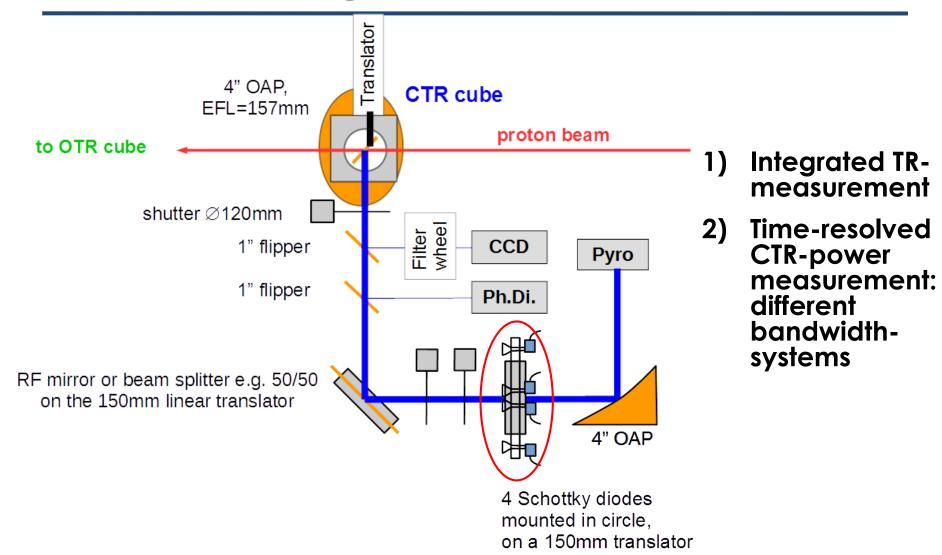




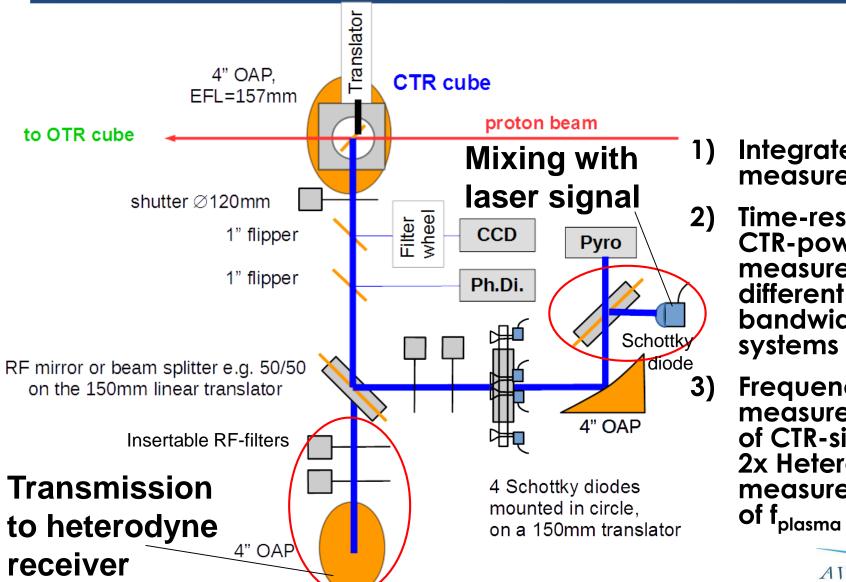










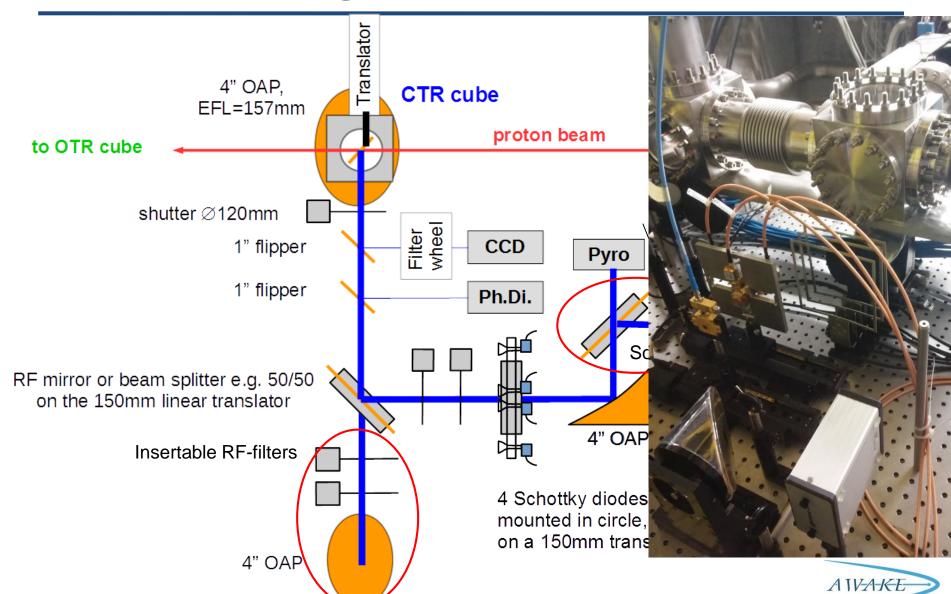


Integrated TRmeasurement

Time-resolved **CTR-power** measurement: different bandwidthsystems

Frequencymeasurement of CTR-signal: 2x Heterodyne measurements



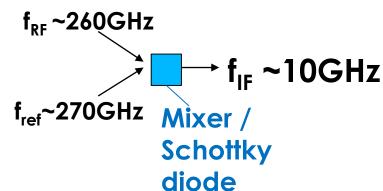


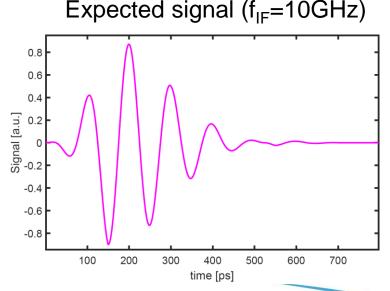
2x Heterodyne Measurement

 Down-mixing CTR-signal by known reference:

$$f_{IF} = f_{RF} - f_{ref}$$

- Measurement of signal
 f_{IF} ~ 10-20 GHz on fast oscilloscope
 (20-40GHz bandwidth)
- Beamline at 15m distance from oscilloscope (shielding)

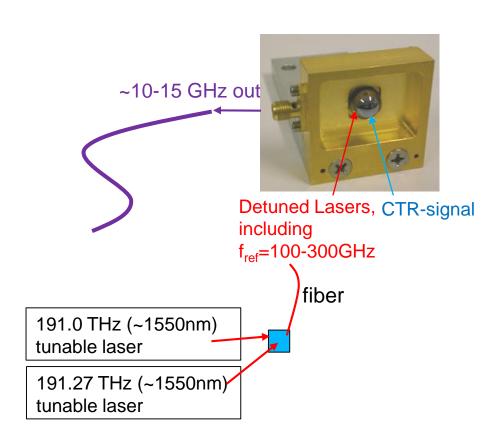




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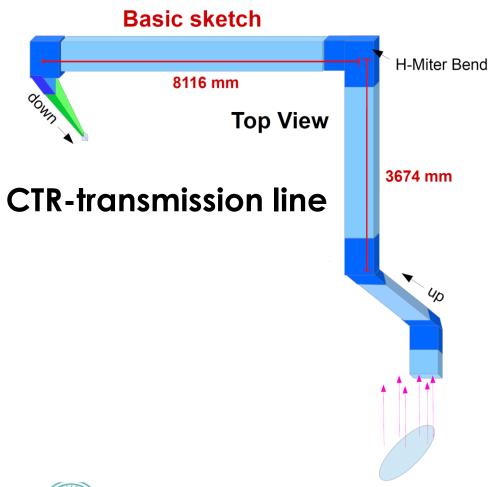
Heterodyne Measurement 1

- Mixing of reference with CTR close to beamline
- Reference signal by mixing slightly detuned lasers
- Transmission of f_{IF}~10-20GHz in low-loss coaxial cables
- Tunable over entire CTR frequency-range





Heterodyne Measurement 2



Mixing of reference with CTR close to oscilloscope

WR90 rectangular waveguide (23x10mm) with 'tall' TE₁₀-mode:

Best compromise between

- Ohmic losses
- Miter bend losses
- Taper losses



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Heterodyne Measurement 2

- Reference signal by frequency-multiplied tunable local oscillaterTransmission of RF over 15m
- Only over less than one waveguide-bandwidth
- Better signal efficiency

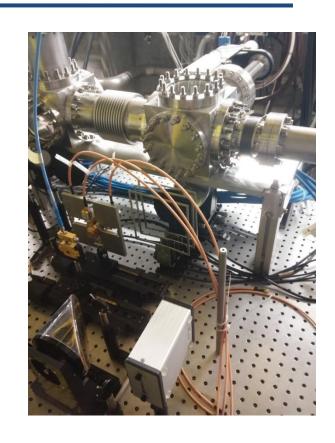






Status & Outlook

- All diagnostics close to beamline installed and commissioned
- RF-transmission line installation in next weeks
- First SMI-experiments for 1 week in December 2016





Summary & Planning

- Essential measurement of microbunch-train due to SMI
- CTR-simulations predict strong signal plasmafrequency, at larger angles
- Variety of diagnostics for integrated, timeresolved and frequency-resolved measurement
- Two kinds of heterodyne measurement
- First measurements expected end of this year



Thank you for your attention!







Details of CTR-calculation

Single particle Ginzburg-Frank (GF) formula - valid for infinite screen and far-field

Spectral components of electric and magnet fields are:

$$\vec{E_{0\omega}}(\vec{r}) = \frac{eZ_0}{(2\pi)^{3/2}} \frac{e^{i\omega(t_z - R(t_z)/c)}}{R} \frac{\vec{s} \times \vec{s} \times \vec{\beta}}{1 - (\vec{s}\vec{\beta})^2}, \qquad \vec{B_{0\omega}}(\vec{r}) = \frac{\vec{n} \times \vec{E_{\omega}}(\vec{r})}{c}$$

$$\vec{B_{0\omega}}(\vec{r}) = \frac{\vec{n} \times \vec{E_{\omega}}(\vec{r})}{c}$$

Spectral energy density angular distribution:

$$\frac{d^2W_0}{d\omega d\Omega} = \frac{e^2Z_0}{4\pi^3} \left| \frac{\vec{s} \times \vec{s} \times \vec{\beta}}{1 - (\vec{s}\vec{\beta})^2} \right|^2 = \frac{e^2Z_0}{4\pi^3} \left(\frac{\beta \sin \theta}{1 - \beta^2 \cos^2 \theta} \right)^2$$

Far-field CTR for a bunch:

$$\vec{E}_{\omega}(\vec{r}) = \sum \vec{E}_{0\omega}(\vec{r}, t_s) = \frac{e^{ikr}}{r} \frac{eZ_0}{(2\pi)^{3/2}} \frac{\vec{s} \times \vec{s} \times \vec{\beta}}{1 - (\vec{s} \vec{\beta})^2} \sum e^{i\sigma_s}$$

$$\frac{d^2W}{d\omega d\Omega} = \frac{d^2W_0}{d\omega d\Omega} \left| \sum e^{i\phi_s} \right|^2 \approx \frac{d^2W_0}{d\omega d\Omega} (N + N(N-1) \left| F\left(\frac{\omega}{V}\sin\theta, \frac{\omega}{V}\right) \right|^2)$$
 - **G**

Surface current (SC) method - valid for flat screen of any shape and any distance towards observer

Vector-potential of the surface field $\vec{E}_{\epsilon}(\omega)$ as a source:

$$\vec{A}_{\omega} = -\frac{1}{2\pi} \int \frac{e^{ikR}}{R} [\vec{n} \times \vec{E}_{z}] d^{2} \vec{r}_{z}$$
 $\vec{R} = \vec{r} - \vec{r}_{z}$

Spectral components of electric and magnetic fields:

$$\vec{E}_{\omega}$$
=- rot \vec{A}_{ω} \vec{B}_{ω} = $\frac{i}{ck}(\nabla \operatorname{div} + k^2)\vec{A}_{\omega}$

$$\vec{E}_{\omega} = \frac{k^2}{2\pi} \int \frac{e^{ikR}}{(kR)^2} (ikR - 1) [\vec{s} \times \vec{n} \times \vec{E}_s(\vec{r}_s)] d^2 \vec{r}_s$$

$$\begin{split} \vec{E}_{\omega} &= \frac{k^2}{2\pi} \int \frac{e^{ikR}}{(kR)^2} (ikR - 1) [\vec{s} \times \vec{n} \times \vec{E}_s(\vec{r}_s)] d^2 \vec{r}_s \\ \vec{B}_{\omega} &= -\frac{ik^2}{2\pi c} \int \frac{e^{ikR}}{(kR)^3} \{ [\vec{n} \times \vec{E}_s] (k^2 R^2 + ikR - 1) - \vec{s} (\vec{s} \cdot [\vec{n} \times \vec{E}_s]) (k^2 R^2 + 3ikR - 3) \} d^2 \vec{r}_s \end{split}$$

Virtual photons approach as a particular case of SC method:

$$kR \gg 1$$
, $\theta \ll 1$ $(\vec{s} \cdot \vec{E} \approx 0$, $\vec{s} \cdot \vec{n} \approx 0$, $\vec{s} \cdot [\vec{n} \times \vec{E}] \approx 0$

$$\vec{E}_{\omega} = -\frac{ik}{2\pi} \int \frac{e^{ikR}}{R} \vec{E}_{z} d^{2} \vec{r}_{z} \qquad \vec{B}_{\omega} = \frac{\vec{n} \times \vec{E}_{\omega}}{C}$$

$$\vec{B}_{\omega} = \frac{\vec{n} \times \vec{E_{\omega}}}{c}$$



CTR-Transmission line

