





Kirk

Recent Progress of STF Coupler R&D for the ILC

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12/Jul/2016

- ILC-TDR
- Motivation
- RF design by HFSS
- Fabrication processes
- Incoming inspection
- Assembly work in clean room
- Low power test / Adjustment of inner conductor for lowest S_{11}
- High power test at test bench
- Inspection for heating area
- More inspection / Identification of cause for heating
- Summary / Future plan

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ILC-TDR (for Power coupler specification)

These figures are shown on Page 35 in ILC-TDR Vol.3 Part-II.



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In view of "Plug compatibility", the use of STF-II coupler has to be evaluated for 40mm diameter.

What is the most simple way for this change?

Input coupler performance in S1-G



Design of 40mm STF2 Coupler



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RF Design by HFSS

\blacklozenge Stroke of Q_L

◆Full simulation for test stand model

◆Full simulation for "Real" bellows model



Stroke of Q_L by full model



Result of Q_L stroke simulation





Pattern 1



Pattern 2



Pattern 3



Comparison of two types of ceramics



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HA95/HA95 (46.0mm)

窓をAHIOOAに変更する度に、突き出し量が増加し ていく傾向があることが分かる。Cold側よりも Warm側の影響の方が大きいようである。

HA95/AH100A (47.5mm)

AH100A/AH100A (51.5mm)

Full Test bench with "real" bellows model

実際のベローズ付きの完全なテストベンチモデルで計算する。ただし、テフロン板は入っていない。



Comparison of w/ and w/o bellows



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Copper plating condition for STF-2 couplers



Copper plating condition for 40mm STF coupler Same condition as couplers installed into STF-2 CM2a \$77<u>7777</u> 25 µm / Nickel strike Warm part 25 µm / Gold strike 25 µm / Gold strike 10 µm / Gold strike Cold part • • • • -0-

Specification of 40mm Couplers

| Coupler (TOSHIBA) | Product No. | Serial No. | Ceramic company | Ceramic color | Ceramic coating | Plating (for outer/inner conductor) |
|-------------------------|-------------|------------------|--------------------|------------------|-----------------|--|
| Warm #1, #2 (normal) | E42130 | 14L001 14L002 | NGK/NTK | White | TiN | Copper |
| Cold #1, #2 (normal) | E42130 | 14L001 14L002 | NGK/NTK | White | TiN | Copper |
| Cold #3, #4 (new) | E42130 | 14L003 14L004 | KYOCERA | Gray | free | Copper |



Reference on HA95 Ceramic (Kijima-san's Paper)



KEKB method

As fabricated (No-coating) \downarrow TiN coating (10nm) \downarrow Brazing @800°C \downarrow O₃ rinsing

STF method

As fabricated (No-coating) ↓ TiN coating (10nm) ↓ Brazing @800°C ↓ Ultra-pure water rinsing

We need to measure SEE of AH100A in various steps.

What's the difference among three rinsing processes? O₃ rinsing (KEKB) Ultra-pure water rinsing (STF) Ultrasonic rinsing (EU-XFEL)



We will also try three rinsing processes in STF.

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Delivery items













Big problem (To be sent back to TOSHIBA) \rightarrow But, no time to refabricate \rightarrow Go forward





Silver trace existed after brazing process \rightarrow No problem



Some black stains existed (maybe after chemical process) \rightarrow No problem



Waveguide system is fabricated by Furukawa C&B. They had Good copper plating.





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Ultra-pure water rinsing \rightarrow assembly work in Class10 \rightarrow Leak check \rightarrow Low power test \rightarrow Baking



Rinsing cold part by ultra-pure water





Drying cold part in Class 10



Head of inner conductor before/after rinsing



Never changed after ultra-pure water rinsing


Rinsing waveguide by ultra-pure water/ultra-sonic





Drying waveguide by ion gun in Class 10



Rinsing vacuum parts by ultra-pure water/ultra-sonic







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Rinsing vacuum parts by ultra-pure water/ultra-sonic



Drying vacuum parts by ion gun





Status in Class 10 at 1st day



Cleaning up warm part by air blow



Rinsing bolt/nut by ultra-pure water/ultra-sonic



Cleaning up warm part by ion gun



Putting bolt/nut in order





Status in Class 10 at 1st day



Putting indium wire



Connection of waveguide





Attachment of metal valve/vacuum gauge



Hexagonal seal



We used Hexagonal seal for the first time!

Cleaning up/jointing cold part



Jointing cold part



Torque: $7 \rightarrow 9 \rightarrow 11 \rightarrow 13$ N•m (two turns)

Attachment of electron probe



Leak check setup













Attachment of bellows pipe



Warm parts are connected each other for common vacuum.

Leak check for warm part



Leak rate : 8.9 x 10⁻¹¹ [Pa•m³/sec] (before baking) Back Ground : 8.2 x 10⁻¹¹ [Pa•m³/sec]

Pumping/Baking



100°C for 48 hours

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Attachment of doorknob



Low power test by N.A.



Adjustment of inner conductor



Comparison between Real data and HFSS



They are consistent or quite different each other?

There maybe some fabrication errors or unknown reasons.



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Goal for each RF condition at test bench

| RF Pulse Width [µsec] | RF Repetition Rate [Hz] | Max. Power [kW] | |
|---|--------------------------------|-----------------|--|
| 10 | 5 | 1200 | |
| 30 | 5 | 1200 | |
| 100 | 5 | 1200 | |
| 500 | 5 | 1200 | |
| 1500 (RDR spec.) | 5 800 | | |
| 1650 (TDR spec.) | 5 | 800 | |
| Max. power for above 1500µsec depends on vacuum level | | | |

Interlock List in High Power Test of 40mm Input Coupler

| I/L Item | mps # | Threshold |
|-------------------------|---------|---|
| Cooling water I/L | mps 60 | |
| Arc I/L #1 (up W.G.) | mps 90 | 2000 / 6500 |
| Arc I/L #2 (upstream) | mps 91 | 2000 / 7250 |
| Arc I/L #3 (downstream) | mps 92 | 2000 / 7480 |
| Arc I/L #4 (down W.G.) | mps 93 | 2500 / 6550 |
| Vacuum I/L | mps 103 | 2 x 10 ⁻⁴ [Pa] |
| VSWR V3 I/L | mps 100 | P _{for} < 1.3 [MW] @upstream |
| VSWR V3 I/L | mps 101 | P _{back} < 10 [kW] @upstream |
| VSWR V3 I/L | mps 102 | VSWR < 1.4 @upstream |
| VSWR V4 I/L | mps 110 | P _{for} < 1.3 [MW] @downstream |
| VSWR V4 I/L | mps 111 | P _{back} < 10 [kW] @downstream |
| VSWR V4 I/L | mps 112 | VSWR < 1.4 @downstream |

$$VSWR = \frac{1 + \sqrt{\frac{P_{backward}}{P_{forward}}}}{1 - \sqrt{\frac{P_{backward}}{P_{forward}}}} \qquad VSWR = 1.2 \Rightarrow \frac{P_{backward}}{P_{forward}} \cong 0.01$$

$$VSWR = 1.4 \Rightarrow \frac{P_{backward}}{P_{forward}} \cong 0.028$$

$$VSWR = 2.0 \Rightarrow \frac{P_{backward}}{P_{forward}} \cong 0.111$$

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Connection to waveguide system Pumping restarts (coupler has been under vacuum after assembly work in clean room)




30 µsec / 5 Hz



1650 µsec / 5 Hz



One-day trend graph for coupler conditioning (normal ceramic)

Pulse width : 10 [µsec] Rep. frequency : 5 [Hz]

Log Trend of 40Φ Input Coupler Conditioning ('16/1/27) Log Trend of 40Φ Input Coupler Conditioning ('16/1/27) Log Trend of 40Φ Input Coupler Conditioning ('16/1/27)



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One-day trend graph for coupler conditioning (normal ceramic)



One-day trend graph for coupler conditioning (normal ceramic)





Scattered Plot of 40 Φ Input Coupler Conditioning ('16/2/5) Scattered Plot of 40 Φ Input Coupler Conditioning ('16/2/5)

Scattered Plot of 40 Input Coupler Conditioning ('16/2/5) Scattered

Scattered Plot of 40Φ Input Coupler Conditioning ('16/2/5)



History of RF Conditioning for Normal ceramic coupler

| Date | Content | Result | | | | | |
|--------|--|--|--|--|--|--|--|
| 12/Jan | Preparation work | | | | | | |
| 15/Jan | Klystron #2 ON, RF ON, Power meter setting | 27.9 kW @10µsec/5Hz | | | | | |
| 18/Jan | | 43.0 kW @10µsec/5Hz | | | | | |
| 19/Jan | | 61.0 kW @10µsec/5Hz | | | | | |
| 20/Jan | | 149 kW @10μsec/5Hz | | | | | |
| 21/Jan | Arc I/L ON | 207 kW @10μsec/5Hz | | | | | |
| 22/Jan | | 312 kW @10µsec/5Hz | | | | | |
| 25/Jan | | 500 kW @10μsec/5Hz | | | | | |
| 26/Jan | | 861 kW @10μsec/5Hz | | | | | |
| 27/Jan | 10µsec/5Hz finished | 1200 kW (1hour keep) @10µsec/5Hz | | | | | |
| 28/Jan | | 1211 kW (1hour keep) @30µsec/5Hz | | | | | |
| 29/Jan | 30µsec/5Hz finished | 1215 kW @100µsec/5Hz | | | | | |
| 1/Feb | 100µsec/5Hz finished | 1216 kW (1hour keep) @100µsec/5Hz, 604 kW @500µsec/5Hz | | | | | |
| 2/Feb | 500µsec/5Hz finished | 1200 kW (1hour keep) @500µsec/5Hz | | | | | |
| 3/Feb | Fan x 2 ON | 818 kW (1hour keep) @1500µsec/5Hz | | | | | |
| 4/Feb | Fan x 4 ON, 1500µsec/5Hz finished | 607 kW @1650µsec/5Hz | | | | | |
| 5/Feb | | 708 kW (1hour keep) @1650µsec/5Hz | | | | | |

Summary of Conditioning time for each parameter (Φ 40mm No, 1 & 2)

| $\Delta t \ [\mu sec]([Hz])$ | Pf1 MAX [kW] | net time [h:m] | keep Pf1 Max[kW] | Keep time @Pf max [h:m] | Elapsed time [h:m] |
|------------------------------|--------------|----------------|------------------|-------------------------|--------------------|
| 10 (5) | 1200 | 58:52 | 1200 | 1:00 | 61:12 |
| 30 (5) | 1200 | 7:03 | 1200 | 1:00 | 8:03 |
| 100 (5) | 1200 | 6:11 | 1200 | 1:00 | 6:11 |
| 500 (5) | 1200 | 8:01 | 1200 | 1:00 | 11:23 |
| 1500 (5) | 800 | 6:46 | 800 | 1:00 | 7:32 |
| total | - | 86:53 | - | - | 94:21 |
| 1650(5) | 700 | 5:18 | 700 | 1:00 | 7:14 |
| total | - | 92:11 | _ | _ | 101:35 |



We moved to RF conditioning for new ceramic couplers, but, before that, we introduced two useful devices from CERN

Auto-conditioning Module by CERN



We connected RF_{in}, RF_{out} and Vacuum output (only one ch.) to this module. Mr. Charles Julie came to KEK, and helped us very well!

Vacuum Distributor by CERN



Good collaboration between CERN and KEK (Thank you very much again)



Vacuum distributor follows up the worse vacuum well! But, there is a little bit difference between actual and worse vacuum.

One-day trend graph for coupler conditioning (new ceramic)











Comparison of RF Conditioning History for Both Couplers

| Date | Result for Normal Ceramic | Date | Result for New Ceramic |
|--------|---|--------|--|
| 18/Jan | 43.0 kW @10µsec/5Hz | 24/Feb | 56.0 kW @10μsec/5Hz |
| 19/Jan | 61.0 kW @10µsec/5Hz | 25/Feb | 66.0 kW @10µsec/5Hz |
| 20/Jan | 149 kW @10µsec/5Hz | 26/Feb | 156.0 kW @10μsec/5Hz |
| 21/Jan | 207 kW @10µsec/5Hz | 29/Feb | 342.0 kW @10μsec/5Hz |
| 22/Jan | 312 kW @10µsec/5Hz | 1/Mar | 930.0 kW @10µsec/5Hz |
| 25/Jan | 500 kW @10µsec/5Hz | 2/Mar | 1200.0 kW @10µsec/5Hz 1200.0 kW @30µsec/5Hz |
| 26/Jan | 861 kW @10µsec/5Hz | 3/Mar | 1200.0 kW @100μsec/5Hz 1100.0 kW @500μsec/5Hz |
| 27/Jan | 1200 kW (1hour keep) @10µsec/5Hz | 4/Mar | 1200.0 kW @500µsec/5Hz 483 kW @1500µsec/5Hz |
| 28/Jan | 1211 kW (1hour keep) @30µsec/5Hz | 7/Mar | |
| 29/Jan | 1215 kW @100µsec/5Hz | 8/Mar | |
| 1/Feb | 1216 kW (1hour keep) @100µsec/5Hz, 604 kW @500µsec/5Hz | 9/Mar | Ilpdate! |
| 2/Feb | 1200 kW (1hour keep) @500µsec/5Hz | 10/Mar | NOUT |
| 3/Feb | 818 kW (1hour keep) @1500µsec/5Hz | 11/Mar | |
| 4/Feb | 607 kW @1650µsec/5Hz | 14/Mar | |
| 5/Feb | 708 kW (1hour keep) @1650µsec/5Hz | 15/Mar | |



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Daily Status of conditioning (4/Mar)

Pulse width : 500→1500 [µsec] Repetition rate : 5 [Hz]

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During 1.5ms RF conditioning, cold vacuum was suddenly worse. Then, we could not do power rise more.

We observed unusual heating around tapered pipe of cold part #3. It never changed even in lower RF duty cycle.

After disassembly of coupler, we didn't find anything. 12/Jul/2016



Daily Status of conditioning (23/Mar) Pulse width : 500 [µsec] Repetition rate : 5 [Hz]



⁽detailed inspection by T-mapping)





Unusual heating occurred at same position again after reversing coupler test stand!

Daily trend graph @8/Apr







500µsec/5Hz







Heating at Cold Part w/ New Ceramic Coupler



- ◆ Only new ceramic coupler
- Only tapered pipe at cold part
- No changed after long RF conditioning
- Many electron emission and worse vacuum as heating occurred
- ◆ No worse vacuum at warm part

We asked to TOSHIBA, "What's differences between them?" ↓ Their answer is... **"Both couplers were fabricated by same method"**

| | Test Series # | Upstream coupler | Downstream coupler | Heating location | | |
|---------|----------------------|------------------|--------------------|-------------------------------------|--|--|
| | 1 Cold #1 (normal) | | Cold #2 (normal) | No heating, but no monitoring | | |
| | 2 Cold #3 (new) | | Cold #4 (new) | Cold #3 heating, Cold #4 no heating | | |
| | 3 | Cold #4 (new) | Cold #3 (new) | Cold #3 heating, Cold #4 no heating | | |
| | 4 | Cold #4 (new) | Cold #2 (normal) | Cold #4 heating, Cold #2 no heating | | |
| | 5 | Cold #2 (normal) | Cold #4 (new) | Cold #4 heating, Cold #2 no heating | | |
| 2/In1/1 | 6 | Cold #3 (new) | Cold #4 (new) | Cold #3 heating, Cold #4 no heating | | |

Detailed inspection for unusual heating in Cold #3



| 2 | | Temperature | | | | | × | 2 | | | _ [|
|--|--|--|---|----------|------------|-------|---------|------------------------|-----------|----------------|---------|
| Temperature Time Range: 30r | | | min 🔻 | 2016/ | 03/23 13:4 | 42:12 | Coupler | | 2016/0 | 3/23 13:42 | |
| 40.00 40.00 | 40.00 40.00 40 | 40.00 | 40.00 40.00 | 40.00 | 4.00 | 40.00 | 40.00 | | | ┐┌温度— | |
| | | | 13:42:11 | | | | | Coupler Upstream Pf: | 394.91kW | #1: | 23.65° |
| | | | | remper | rature#1 | | 23.50°C | Coupler Unstream Phy | 20 32KW | #2: | 27.40° |
| | | الألوافيد فاستنا أخاصهما فادر ورعار فالمارد | Line of the state | Temper | rature#2 | | 27.70°C | Coupler opstream Pb. | 29.5287 | | 20.500 |
| | LILLING AND AND A THE REPORT | | | | rature#3 | | 21.25°C | Coupler Downstream Pf: | 310.60kW | #3: | 20.50% |
| | and the second | on the construction of the second second second | a shirter ships the section is being the thereit | | rature#4 | | 22.90°C | | | #4: | 23.20° |
| | and the second | white the section with the Mit | المريطية ويتقفر والمقورة الجويط أرجسون | | rature#5 | | 32.80°C | Vacuum | | #5. | 33 10% |
| | and the second se | an an an Antonia an Antonia an Antonia | Allendaria de la sere a la sere a | | rature#0 | | 24.25 C | Cold: | 4.47E-5Pa | #31 | 55.10 |
| and the second | And the state of t | de the standard and a state of the second state of the | Applift girlings girleft an frankriger att finde | | rature#9 | | 24.55°C | | | #6: | 24.55°(|
| | | | | Temper | rature#9 | | 30.70°C | warm: | 5.69E-5Pa | #7: | 36.85°(|
| and the state of the | AND A CONTRACTOR OF A DAMAGE AND A DAMAGE | | Allow the substitution of | Temper | rature#10 | | 22.45°C | | | #0. | 24 10% |
| | CONTRACTOR AND INCOMENTATION OF THE ADDRESS OF THE OWNER OF | difference in a second a factor of the | Second and set statement estiles as all | Temper | rature#10 | | 26.20°C | Arc | |] #0: | 24.10 (|
| | The start burner is a start of the start of | | a na antista da antist | | rature#12 | | 25.75°C | Arc#1: | 12.160mV | #9: | 30.25°(|
| | | | | - Temper | 44410#12 | | 25.75 C | A | 2 (27-2)/ | #10: | 21.70°0 |
| | | | | | | | | Arc#2: | -3.627mV | | 25.754 |
| 13:18:00 | 13:24:00 | 13:30:00 | 13:36:00 | | | | | Up: | 87.467mV | #11: | 25.75°C |
| 15.00 15.00 | 15.00 15.00 15 | 00 15.00 | 15.00 15.00 | 15.00 | 15.00 | 15.00 | 15.00 | | 20.007-01 | #12: | 25.15°(|
| | | ⊯ div | 5 | | | | | Down: | 10.667mV | | |



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We identified the highest heating location, and inspected there by some fiber-scopes.

Inspection tools for Cold part #3

- Digital borescope (J-SCOPE)
- Rigid borescope (OLYMPUS)
- Digital borescope (OLYMPUS)

Small blisters existed around heating area, but probably no correlation. Because, there was no evidence for cold part #4.







Courtesy of Tanaka-san

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Inspection for unusual heating by DESY magnet

I attached small DESY magnets around tapered pipe.





Just after magnets attachment, temperature rise stopped and decreased. But, when RF pulse width changed from 400 to 500 μ sec, there was no effect \downarrow Many electrons directly hit at tapered pipe! (No thermal conductivity)

CST simulation just recently started!









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Summary & Future Plan

- Plug-compatibility for STF-II coupler with normal ceramic is no problem
 - RF conditioning time is comparable for previous couplers
 - RF property is no problem, but Q_L measurement is not done yet
- New ceramic coupler had significant heating problem
 - This was observed for Only tapered pipe at cold part
 - Many electrons directly hit at tapered pipe
- Rinsing study (Ultrasonic or O_3) will be done (early next year)
- Range of Q_L will be checked





Scattered Plot of 40^Φ Input Coupler Conditioning ('16/1/27)





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Scattered Plot of 40Φ Input Coupler Conditioning ('16/1/27)





Scattered Plot of 40Φ Input Coupler Conditioning ('16/1/27)

Scattered Plot of 40Φ Input Coupler Conditioning ('16/3/2)





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Comparison of Normal/New ceramic coupler



Comparison of Normal/New ceramic coupler



Scattered Plot of 40Φ Input Coupler Conditioning ('16/1/29)





Scattered Plot of 40Φ Input Coupler Conditioning ('16/1/29)





Scattered Plot of 40Φ Input Coupler Conditioning ('16/1/29)

Scattered Plot of 40Φ Input Coupler Conditioning ('16/3/2)





Comparison of Normal/New ceramic coupler











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Scattered Plot of 40Φ Input Coupler Conditioning ('16/2/1)

Scattered Plot of 40Φ Input Coupler Conditioning ('16/3/3)









Scattered Plot of 40Φ Input Coupler Conditioning ('16/2/2)





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Scattered Plot of 40Φ Input Coupler Conditioning ('16/2/2)

Scattered Plot of 40Φ Input Coupler Conditioning ('16/3/4)













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横軸のスケールが異なることに注意



横軸のスケールが異なることに注意



peak #1 [mV] 6

P_{forward upstream} [kW]

Electron peak vs Power

[/m] [#/

peak

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Scattered Plot of 40¢ Input Coupler Conditioning ('16/3/4)

New ceramic

Pulse width : 500[µsec] Rep. frequency : 5 [Hz]

New ceramic

Scattered Plot of 40^Φ Input Coupler Conditioning ('16/3/23)



横軸のスケールが異なることに注意

Scattered Plot of 40Ф Input Coupler Conditioning ('16/3/23)



Scattered Plot of 40Φ Input Coupler Conditioning ('16/2/2)



















