

6th HL-LHC Collaboration Meeting – Paris

11T Dipole Magnet for the DS Regions Around IP7 for the Upgrade of the LHC Collimation System

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- Full-length 11T magnet prototype
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- Summary





The 11T Dipole in the HL-LHC Timeline





A few numbers – 11T Dipole Full Ass^y for IP7

ltem	LS2 (RRP) Cross-section 1	LS2 Spares (RRP – PIT) Cross-section 2	Total	
	C O I L S (including rework)			
 Model Prototype Series 	 18 (including 4 practice coils and 2 trial coils #110 - #201) 8, including 1 rework, 1 Cu coil and 2 low grade Sc coils 20 coils, including 4 rework 	 10 (7 PIT, 3 RRP) 7 (PIT) 10, including 2 rework 	 28 15 30 	
	COLLARED COILS			
ModelPrototypeSeries	 7, including single coil assembly 3, including 1 trial collaring with 2 low grade Sc coils 8 	 4 (3 PIT, 1 RRP) 2 (PIT) 4 (PIT) 	• 11 • 5 • 12	
M	AGNET MODEL OR COLD MAS	S (MBH)		
ModelPrototype	 9 (1 single coil, 6 single aperture, 2 two-in-one) 1 	 5 (4 SP, 1 DP) 1 (PIT) 	• 14 • 2	
Series	• 4	• 2	• 6	
	CRYOSTATING (LBH)			
 Prototype Series	• 1 • 4	• 1 • 2	• 2 • 6	
COLD TESTS				
 Model Prototype 11T Dipole Full Assembly Series 	 9 (1 single coil, 6 single aperture, 2 two-in-one) 1 1, with the prototype P001 and the first of series 4 	 5 (4 SP, 1 DP) 1 (PIT) - 2 	 14 2 1 6 	
	11 T DIPOLE FULL ASSEMB	LY		
• 11T Dipole Full Assembly	• 2	• 1	• 3	
	11T Dipole at 6th HI -L HC	Collaboration Meeting - E. Sava	5	

Schedule X-Section 1



11T Dipole at 6th HL-LHC Collaboration Meeting - F. Savary



11T Dipole for HiLumi LHC – Design features

- **Operational Conditions:**
 - T = 1.9 K
 - $I_{op} = 11.85 \text{ kA} \text{B} = 11.23 \text{ T}$
 - Ic [kA] B_{peak} = 11.77 T (with cryostat, strand self-field, and yoke cutback)
 - Load line margin \cong 20 % (operational point at 80.1% of Iss at 1.9 K with yoke cutback)
- Conductor, Nb₃Sn
 - **Strand** *Φ* **0.700 ± 0.003**:
 - RRP 108/127, keystone angle 0.79°
 - PIT (with Nb barrier), keystone angle 0.50°
- Cable mid-thickness 1.25 mm, 40 strands
- Cable insulation:
 - **1 layer of Mica tape** of 80 μ m thickness
 - **1 layer of S2-glass** of 75 μ m thickness









Conductor for Magnet Models 169 RRP Wire

0.7 mm RRP	Value		
Quantity [km]	220		
n° billets	13	14	
Layout	132/169	144/169 150/169	
Average I _c , RMS [A]	431 , 24	456 , 24	
<i>l_c</i> spec [A]	438		
Average RRR , RMS	185 , 64	172 , 30	
RRR spec	150		
Average <i>J_c</i> , <i>RMS</i> [A/mm ²]	2508 , 125	2408 , 146	
Average B_{c2}, RMS [T]	23.2 , 0.36	23.2 , 0.52	

RRP 132/169



RRP 144/169



RRP 150/169

- At 12 T the average I_c of the 132/169 is about 1% lower then specification;
- The 144/169 and the 150/169 meet the *I_c* specs but the Cu content is insufficient





Conductor for Series Magnets 108/127 RRP Wire



Placed two contracts: 500 km and 200 km of wire

- Received 320 km from first contract
 - Performance verified at CERN for 247 km
 - Cable for 3 coils have been produced at CERN



10

- Satisfy specification with margin; in particular the RRR is significantly larger than that of the 169 RRP layout → magnet stability
- Remaining material from first contract by January 2017
- First delivery from second contract by July 2017; all material by end 2017
- Bruker-EAS has identified a wire layout for the PIT conductor expected to meet the technical specification of the 11 T project
 - This PIT wire will be used to manufacture the two spare magnets



B. Bordini

X-section 2

Based on new cable geometry to guarantee **I** degradation below 5% for both PIT and RRP conductors

	Bare mid- thickness (mm)	Bare width (mm)	Keystone angle (degree)	I _c degradation %
1st Gen. Design	1.250 (1.307)	14.70 (14.85)	0.79 (0.81)	6-10
2 nd Gen. Design	1.250 (1.288)	14.70 (14.85)	0.50	3

Cable geometry and measured critical current degradation. Assumed dimensions after reaction in parentheses.

- (mm) 30 Coil ends mechanically and magnetically >20 optimized with few changes to previous design
- Iron yoke (also in X-section 1):
 - Outer diameter reduced from 550 to 540 mm
 - Assembly holes from one to two per quadrant
 - Yoke cutback implemented with non-magnetic yoke laminations (306 mm on connection side and 192 mm on non-connection side)

E. Nilsson, S. Izquierdo Bermudez et al.

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generation

20

40

x (mm)

2nd generation design

design

Coil Stress in CERN 2-in-1 X-Section



Model Programme





- MBHDP01 was re-tested, in "Thermal Cycle 2" or TC2
 - Magnet training memory
 - Quench protection study
 Goals
 - Magnetic measurements
- Summary
 - Magnet re-training effect of anti-cryostat and high MIITs quenches in TC1
 - Quench-back effect, observed in TC1, was confirmed
 - Magnetic measurement data are in a good agreement with the expectations and the data for single-aperture model MBHSP03
 Fermilab

A.V. Zlobin et al.

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Publications



Quench Performance and Field Quality of the FNAL Twin-Aperture 11 T Nb₃Sn Dipole Model for LHC Upgrades

S. Stoynev, N. Andreev, G. Apollinari, B. Auchmann, E. Barzi, S. Izquierdo Bermudez, R. Bossert, G. Chlachidze, J. DiMarco, M. Karppinen, F. Nobrega, I. Novitski, L. Rossi, F. Savary, D. Smekens, T. Strauss, D. Turrioni, G. Velev, A.V. Zlobin



October 9 - 14, 2016 Chicago, IL U.S.A.



🚰 Fermilab

Field quality measurements in the FNAL twin-aperture 11 T dipole for LHC upgrades*
T. Strauss, G. Apollinari, E. Barzi, G. Chlachidze, J. Di Marco, F. Nobrega, I. Novitski, S. Stoynev, D. Turrioni, G. Velev, A.V. Zlobin (FNAL);
B. Auchmann, S. Izquierdo Bermudez, M. Karppinen, L. Rossi, F. Savary, D. Smekens (CERN)

Model programme at CERN



The 11T magnet models













SP105, not shown

Model programme at CERN

- Model SP105 is currently under test in SM18
 - Quench heaters impregnated with the coils for better efficiency and validation of the final design (full-length)
 - Gelling and post-curing after impregnation of the coils was done under pressure ~3 bar
- Model SP106 is under construction
 - Interlayer quench heaters are added
 - Complement the QH installed on the outside surface of the coil, should improve further the quench protection, and add redundancy
 - A development, not for production



- To come as of next year: models with PIT, SP201-203, DP201, and possibly one with RRP, SP107
 - New cable geometry with reduced keystone angle (0.79° to 0.50°) in order to reduce critical current degradation due to cabling below 5%
 - Electro-magnetic and structural designs completed, 70% progress on 3D/2D CAD work



Quench performance, 1

 Tests results of the first Two-In-One at CERN, MBHDP101, made of the collared coils of SP102 and SP103 (end 2015 + beginning of 2016)





G. Willering

Quench performance, 2

Model SP104 (June-July 2016) Fast training of coil #112 with only 3 quenches Slow training of coil #113 with 17 quenches up to 11.7 kA Limited at 11.7 kA at nominal ramp rate V-cvcle Midplane limited at 4.3 K at 11.4 kA in coil 1134000 12000 I_{max} reached = 12.24 kA, 88% of I_{SS} @ 1.9 K 10000 Current (A) Holding current test @ 12 kA failed after 62 8000 6000 minutes, quench at layer jump of coil #113 4000 V-shaped pre-cycles trigger current 2000 redistribution, which allowed overcoming the 5 10 15 20 25 time (minutes) **limitation** @ the layer jump (like for the last point) 12 T - Ultimate 12 T - Ultimate Coil #113 inner laver mid-plane 13000 11.2 T - Nominal 12000 12000 11.2 T - Nominal Quench current[A] Quench current [A] 11000 11000 Coil #113 layer jump 10000 MBHSP101 10000 Thermal cycle 101 9000 MBHSP104 -MBHSP102 9000 Thermal cycle 102 MBHSP104 - 4.3 K Tests @ 1.9 K 8000 8000 Coil #112 — MBSP103 MBHSP104 7000 7000 0 5 10 15 20 25 30 15 20 25 30 35 11T Dipole at 6th HL-LHC Collaboration Meeting - F. Savary Quench number G. Willering

Quench performance, 3

- Model SP105, coils #114 and #115 (Nov. 2016 ongoing)
 - Fastest training so far with only 5 quenches to nominal current
 - Detraining in coil #114 @ layer jump and adjacent turns
 - Last quenches were all in the midplane at 12.3 kA in both coils simultaneous
 - Tests are ongoing with protection studies, quench integral, magnetic measurements, ramp rate dependency





Field quality 1: systematic

- Magnetic measurements on short models show:
 - TF as designed \rightarrow trimming ok
 - Iron saturation effects as expected on
 - TF
 - Affected multipoles (b_2)
- Persistent current effects on b₃ show a
 total variation, from injection to nominal, in the order of 20 units
- Systematic field errors mainly due to coil shimming



Average results from 3 magnets			
n	b _n	an	
2	-0.5	5.1	
3	8.0	-0.6	
4	-0.3	0.9	
5	1.4	-0.4	
6	0.0	0.3	
7	0.3	-0.1	
8	0.0	0.1	
9	0.8	0.0	
10	0.0	0.0	

Field quality 2: random

- Random components on multipoles
 - Precision of cable positioning under control
 - Measured standard deviation is in line with simulations of random block displacements of ± 60 µm









L. Fiscarelli, S. Izquierdo Bermudez 11T Dipole at 6th HL-LHC Collaboration Meeting - F. Savary

Full Length 11T Magnet



Instrumentation

One instrumentation capillary and cover flange <u>per aperture</u> for routing: V-Taps, quench heater, diode, and cryogenic instrumentation wiring





Work progress on the prototype

Most tooling available and operational, non-exhaustive list:

- Coil impregnation system, 3 short coils and 2 long coils were impregnated
- Ground insulation forming tooling operational, insulation formed and assembled on the practice coil made of copper cable and 1st low grade coil
- Assembly and rotation benches available and operational
- Collaring tooling just received, metrology and assembly on-going
- Welding press revamping close to completion (control system, hydraulics, and welding equipment), should be ready by the end of the year









Work progress on the prototype – Plan for series



For series production: procurement process recently initiated, aiming at placing a contract for the assembling activities of the collared coils, to be carried out in the CERN Large Magnet Facility (coil winding to start Oct.17)







Cold mass envelope compliance

 Approved structural analysis report (EDMS 1711518) on conformity of the cold mass envelope to the requirements of the European Pressure Equipment Directive 2014/68/EU per new European harmonised standard EN 13445 (Unfired Pressure Vessels)





Structural analysis of welds

33

\$0.70

11/14

Fig .1

Elastic structural analysis of linearized stresses components in new 11T dipole cold mass weld geometry for normal operation and test load conditions - OK

- Gross elasto-plastic assessment OK
- Fracture toughness critical value versus Leak before break criterion - Compliant
- Linear Fracture Mechanics crack growth rate and low cycle fatigue analysis, in line with filler metal material properties (AISI 1.4453).



Work progress on the cryostat

- 11T Prototype
 - Vacuum vessel: final machining at the contractor, leak test planned on 16th November, delivery expected 12th December
 - Bottom tray: machining done, all parts available, welding in December
- Bypass cryostat prototype
 - Order placed for the vacuum vessel, delivery in April 2016
 - Price enquiries on going for all other components
- Assembly and QA
 - Adaptations of cryostating designed, work starting in Dec.
 - Procedures for 11T cryostat done
 - Procedures for bypass cryostat on-going







Summary

- The successful tests of the two-in-one model MBHDP101 demonstrate feasibility of the upgrade of the LHC collimation system with 11 T dipoles for IP7 of LHC
- A lot of attention is required throughout the manufacturing process (recall low performance of SP104)
- Most of the tooling needed for the fabrication of the 11 T dipole is available and operational in the Large Magnet Facility @ CERN, in particular the reaction furnace and impregnation system have been successfully commissioned
- The construction of the first full length prototype is surely the next major milestone. The performance tests are planned in winter 2017
- The production schedule is a challenge





Thank you for your attention

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At CERN:

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Cavana E. (ASG Superconductors), Genestier T. (Alstom – G.E.), Letellier V. (Alstom – G.E.), Melhem Z. (Oxford Instruments), Revilak Ph. (BNG)



Spare slides



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Magnet models X-section 1

Coil #	Single aperture	Note	Test results	Double aperture
106 108	MBHSP102	Second single aperture magnet. Coil 106 from SP101	Reached ultimate current	MBHDP101 First 2 in 1 magnet Outer shell Ø 580 mm Reached ultimate current
109	MBHSP103	Third single aperture magnet	Reached ultimate current	
111		Third single aperture magnet		
112	New collared coil	single aperture collared coil		MBHDP102
113	assembly with coils #112 & #tbd	to be assembled with already tested coils	Not cold tested	Second 2 in 1 magnet Outer shell Ø 570 mm Cold powering tests
114	MBHSP105	Fifth single aperture magnet		Q1-2017
115		Impregnated QH traces, Multiple injection points & pressurized curing	Test ongoing Q4-2016	
116	MBHSP106	Sixth single aperture magnet	To be assembled	
117		Inter Layer QH, Multiple injection points & pressurized curing	Q1-2017 and tested Q2-2017	



Magnet models X-section 2

A new cable geometry is required for PIT in order to

reduce critical current degradation during cabling

HL-LHC PROJECT

Keystone angle 0.50 deg.



Coil #	Single aperture	Note	Remarks	Double aperture
202		First single aperture magnet	Coil winding scheduled	MBHDP201
203	MBHSP201 ♪	with PIT conductor & new X-section Spot Heaters integration for high MIIts tests	to start Q1-2017 Cold powering tests Q2-2017	Third 2 in 1 magnet First double aperture with PIT Outer shell Ø 570 mm Cold powering tests Q4_2017
204	ilidi	Second single aperture		
205	OND MBHSP202	magnet with PTT conductor & new X-section Spot Heaters integration for high MIIts tests	Coil winding scheduled to start Q2-2017	
206		Third single aperture magnet	Coil winding scheduled	
207	MBHSP203	with PIT conductor & new X-section	to start Q3-2017	
118	MBHSP107	MBHSP107 First single aperture magnet	Coil winding schedule	
119		with RRP conductor & new X-section	IBD	
(CÉRN)				

Linear Fatigue Crack growth rate analysis and fracture assessment

- Cross check of **minimal critical fracture toughness K_{IC}** of weld metal at 4K vs. critical crack size
- Fatigue crack growth rate assessment across shell closure weld against initial embedded crack dimensions.
- Outcome of minimum acceptable embedded defect size compatible with the ISO 5817 quality level B and UT quality inspection procedure per ISO 17640 (> 5 mm²)



Where *a* is the crack size in mm, ΔK_1 the variation of stress intensity factor in MPa \sqrt{m} , *N* the number of cycles, ΔK_{th} is the threshold of stress factor intensity range





