

Energy deposition and thermo-mechanical studies for IR6 protection devices and downstream magnets/septa

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On behalf of HL-LHC WP14

6th HL-LHC Collaboration Meeting

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IR6 protection absorbers/LHC dump:

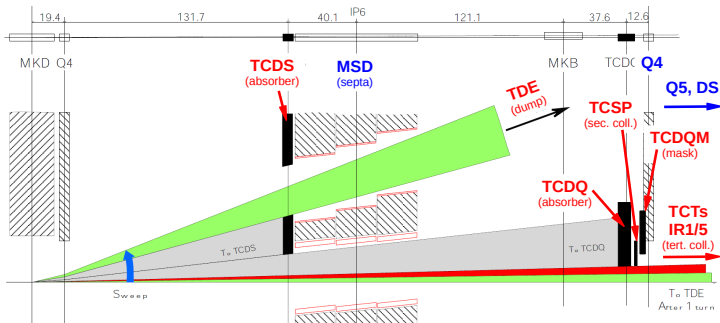
- Have been designed for **LHC ultimate beams** (1.7×10^{11} ppb, $3.5 \mu\text{m}\cdot\text{rad}$), i.e. for a smaller brightness and a smaller bunch intensity wrt HL beams

Scope of this talk:

- Assessment of the **energy deposition** in
 - IR6 protection devices
 - IR6 magnets and septafor HL beam parameters and HL optics (**HLLHCv1.2**)
- Give a first indication if we expect possible issues with
 - present absorber materials \Rightarrow **thermo-mechanical studies**
 - the protection of equipmentin case of extraction failures

Note: This presentation includes some minor updates of the thermo-mechanical studies with respect to my recent talk at the 19th HL-LHC TCC Meeting (27th Oct 2016): a longer time interval was simulated to fully assess all dynamic effects and some stresses were found a bit higher than reported in the TCC Meeting, however without any effect on the main conclusions.

Protection devices/dumps and failure scenarios



- Single MKD module prefire:

- **TCDs** → **MSDs** ⇒ *this talk*
- **TCDQ**+**TCDQM** → **Q4, Q5, DS magnets** ⇒ *this talk*
- **TCTs** → **IR1/5 triplet, D1** (studied by WP5+WP10) ⇒ *A. Tsinganis (this afternoon)*

red = need to check material robustness
blue = need to check if sufficiently protected

- Dilution (MKB) failure:

- **TDE core** and **TDE windows** ⇒ *M.I. Frankl (this session)*

(equipment in *italic* still to be studied)

Assumed beam and optics parameters

- **Beam parameters:**

- Assumed the **same normalized emittance** and **bunch intensity** as for
 - **LIU** protection/dump upgrades in **SPS/TLs** and
 - **HL-LHC WP14** protection upgrades in the **LHC injection regions**

Beam	$\epsilon_{x,y}^n$	I_b
HL Std 25 nsec	2.08 $\mu\text{m}\cdot\text{rad}$	2.3×10^{11}
LIU BCMS	1.37 $\mu\text{m}\cdot\text{rad}$	2.0×10^{11}

- This is a cautious approach, i.e. no emittance growth and no intensity loss in ramp

- **Optics:**

- All studies carried out for optics version **HLLHCv1.2**
- For each device, **selected the worst case** from flat/flat HV/round optics (*M. Fraser*)

TCDQ → Q4, Q5

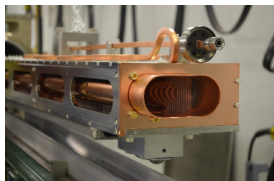
TCDS → MSDs

Conclusions

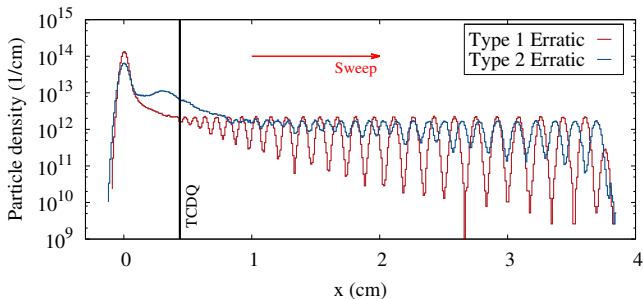
Backup

Some remarks on the TCDQ

- Was **upgraded in LS1** (2→3 modules, Gr→CfC)
- Upgrade studies (FLUKA+ANSYS) considered HL beam parameters
- However, **“new” MKD erratics observed in 2015**: particle density on TCDQ can be $2\times$ higher than assumed for LS1 upgrade studies → needed to be cross-checked

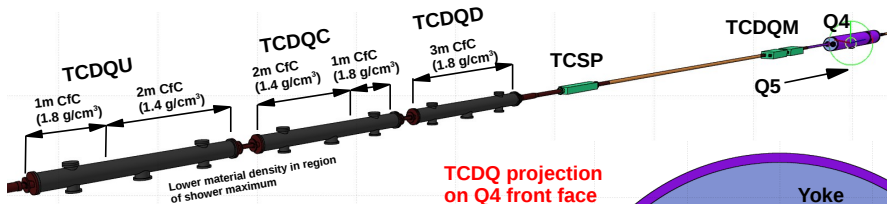


Particle distribution by M. Fraser



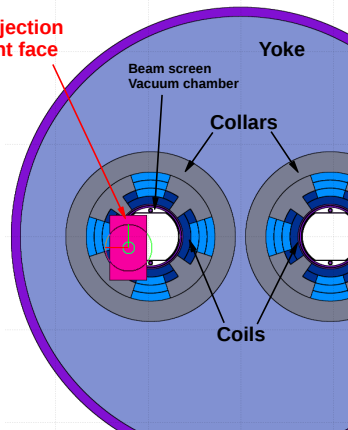
- all studies were carried out for a Type 2 erratic (worst case)
- assumed TCDQ half gap = 8.1σ (includes 0.5σ misalignment)

TCDQ+Q4/Q5 model for energy deposition simulations



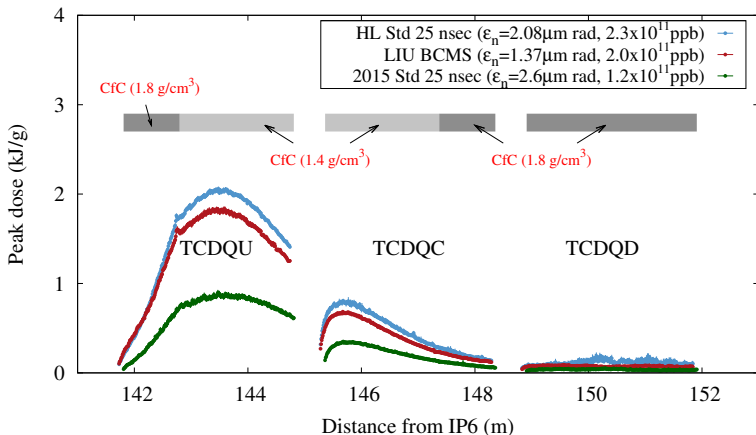
- TCDQ:

- **three modules**, each 3 m absorber length
- made of **2D CfC** blocks of different density
- **single-sided** protection element



Peak dose in TCDQ for a Type 2 MKD erratic

M. Frankl

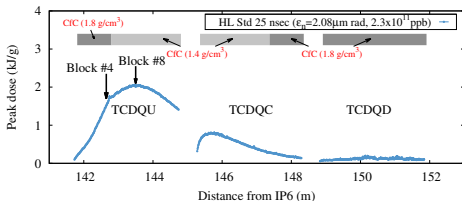


- HL-LHC std: peak dose in low-density blocks: **2.1 kJ/g**
- LIU BCMS: peak dose in low-density blocks: **1.8 kJ/g**

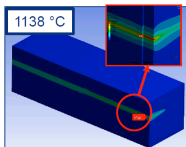
Peak temp. and stresses in TCDQ (HL-LHC std 25 ns)

C. Di Paolo

- Thermal and structural analysis for blocks with the **highest peak load** (for both CfC grades)

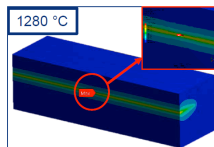


BLOCK 4 CfC 1.75 g/cm³



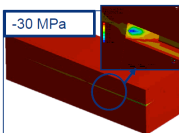
Linear elastic material model
Temperatures profiles at the peak after one pulse

BLOCK 8 CfC 1.4 g/cm³

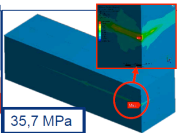


Linear elastic material model
Temperatures profiles at the peak after one pulse

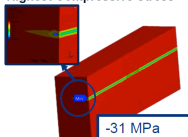
Highest Compressive Stress



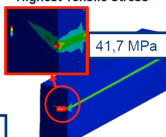
Highest Tensile Stress



Highest Compressive Stress



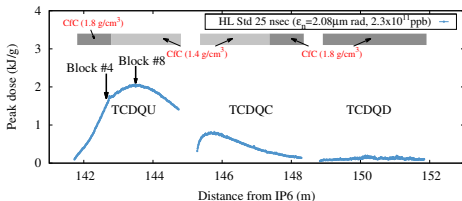
Highest Tensile Stress



Peak temp. and stresses in TCDQ (HL-LHC std 25 ns)

C. Di Paolo

- Thermal and structural analysis for blocks with the **highest peak load** (for both CfC grades)

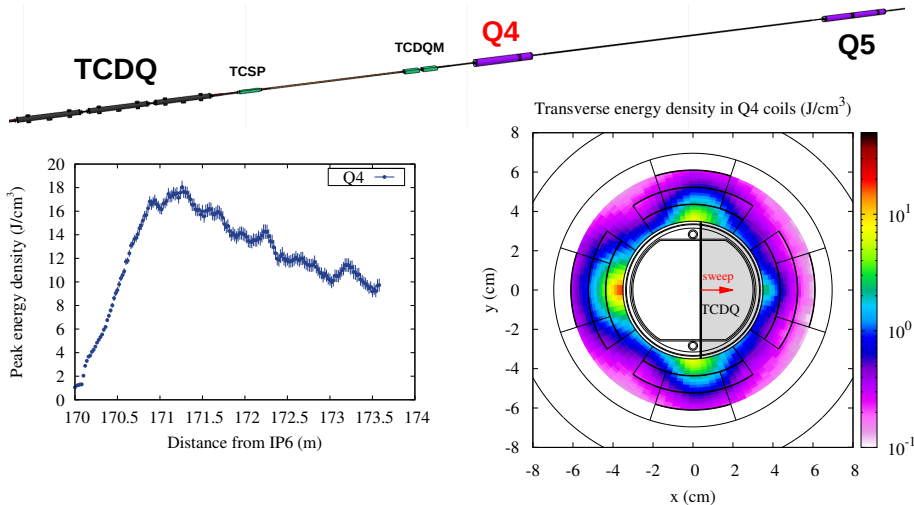


Material	C-C 1.75	C-C 1.4
Max. Temp. [°C]	1138	1280
Min. Princ. [MPa]	-30	-31
Compr. Strength	69.6	69.6
Max. Princ. [MPa]	36	42
Tensile Strength	61	61

→ *Tensile and compressive principal stresses are below the strength limits*

→ *A reduction of TCDQ half gap would require a revalidation of the block robustness*

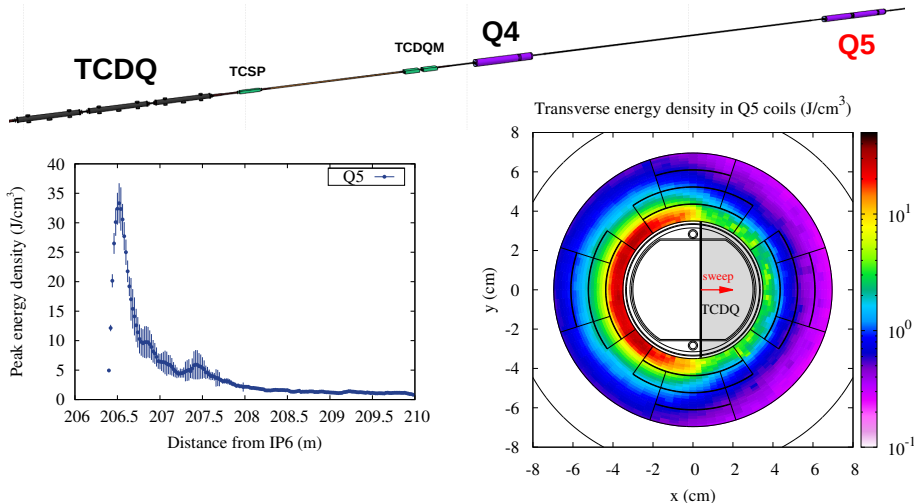
Peak energy density in Q4 coils (HL-LHC std 25 ns)



- Predicted peak energy density in Q4 coils: $\sim 17 \text{ J/cm}^3$

M. Frankl

Peak energy density in Q5 coils (HL-LHC std 25 ns)



- Predicted peak energy density in Q5 coils: $\sim 30\text{--}35 \text{ J/cm}^3$
(statistics still to be improved)

M. Frankl

Remarks on the energy density in superconducting coils

- **Model calculations:**

- **Should account for a sufficient margin** (at least a factor 3 below damage limit)

- **Main issue: the damage limit of NbTi coils for ultra-fast losses is not exactly known**

- During the design of LHC protection devices a value of $\sim 87 \text{ J/cm}^3$ was assumed, which however has to be revised

- **HiRadMat test** on SC cables carried out by colleagues from TE/MPE in Sep 2016 (at room temperature), another test planned at cryogenic temperatures

- *talk of D. Wollmann et al. this afternoon*

- *Depending on HiRadMat outcome, an improved protection might need to be considered also for the Q5 in IR6*

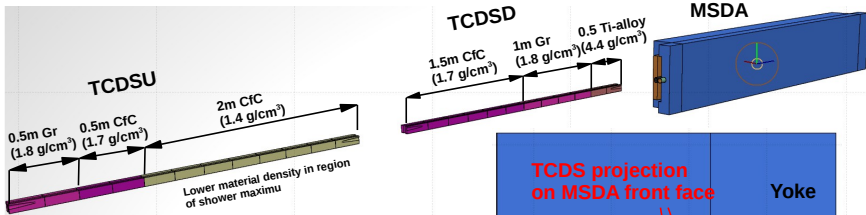
TCDQ → Q4, Q5

TCDS → MSDs

Conclusions

Backup

TCDS+MSD model for energy deposition simulations

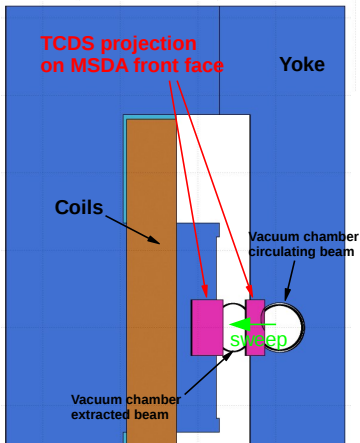


- Existing TCDS:

- **2 modules**, each with 3 m absorber length
- made of **Graphite/2D CfC blocks** of different density + **Ti-alloy block** at the downstream end
- each module has two jaws (one directly impacted in case of an asynch. beam dump)

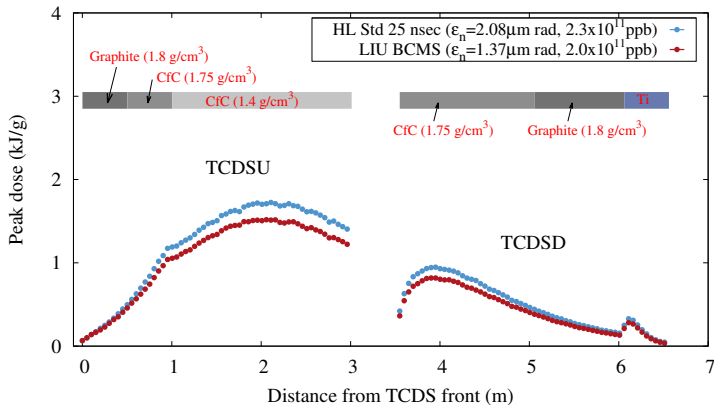
- HL upgrade (baseline):

- 2 → 3 modules (a la TCDQ)



Peak dose in TCDS for a Type 2 MKD erratic

M. Frankl

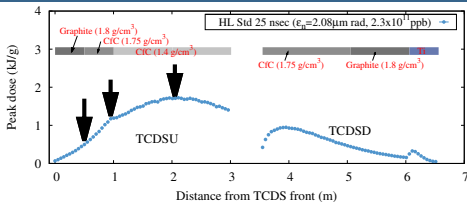


- HL-LHC std: max. energy density in low-density blocks: **1.7 kJ/g**
- LIU BCMS: max. energy density in low-density blocks: **1.5 kJ/g**

Peak temp. and stresses in TCDS (HL-LHC std 25 ns)

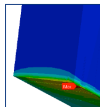
C. Di Paolo

- Thermal and structural analysis for blocks with the **highest peak load** (for all materials)



BLOCK 2 Graphite C2020

Linear elastic material model



Temperatures profiles at the peak after one pulse

397°C

Highest Compressive Stress



-20 MPa

Highest Tensile Stress



27 MPa

BLOCK 2 CfC 1.75 g/cm³

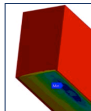
Linear elastic material model



Temperatures profiles at the peak after one pulse

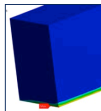
798°C

Highest Compressive Stress



-23 MPa

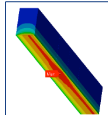
Highest Tensile Stress



18 MPa

BLOCK 5 CfC 1.4 g/cm³

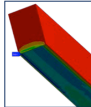
Linear elastic material model



Temperatures profiles at the peak after one pulse

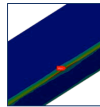
1141°C

Highest Compressive Stress



-27 MPa

Highest Tensile Stress



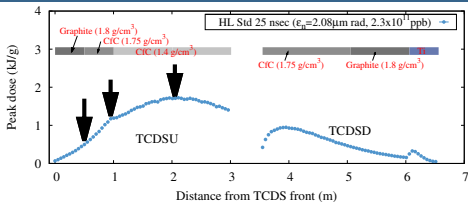
51 MPa

The maximum tensile stress is in the y direction

Peak temp. and stresses in TCDS (HL-LHC std 25 ns)

C. Di Paolo

- Thermal and structural analysis for blocks with the **highest peak load** (for all materials)



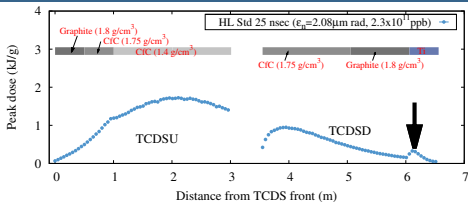
Material	C-C 1.75	C-C 1.4	Graphite
Max. Temp. [°C]	798	1141	396
Min. Princ. [MPa]	-23	-27	-20
Compr. Strength	69.6	69.6	35
Max. Princ. [MPa]	18	51	27
Tensile Strength	61	84 (y)	35

→ Tensile and compressive principal stresses are below the strength limits

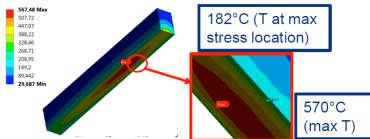
Peak temp. and stresses in TCDS (HL-LHC std 25 ns)

C. Di Paolo

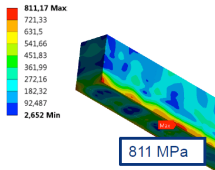
- Thermal and structural analysis for blocks with the **highest peak load** (for all materials)



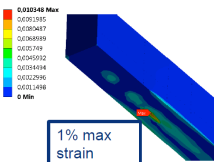
Temperature profiles at the peak after one pulse [°C]




Equivalent stress (Von Mises) [MPa]



Equivalent plastic strain [m/m]

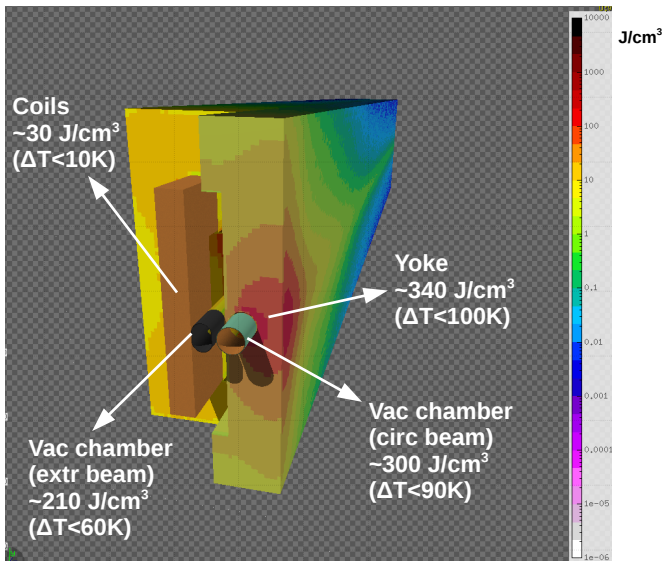


	Area at Max T	Area at Max stress
Temp. [°C]	568	182
Eq. Stress [MPa]	413	811
Yield Strength	409	670
Tensile Strength	520	830



- *Ti block expected to plastify*
- *However, plastic strain is only 1% (no risk to fracture)*

Energy deposition in first MSD for a Type 2 MKD erratic



TCDQ → Q4, Q5

TCDS → MSDs

Conclusions

Backup

Conclusions

- **TCDQ** → **Q4, Q5, DS**
 - **CfC in TCDQ sufficiently robust** for HL beams even for the worst known MKD erratic
 - **Improved protection of Q5** might be necessary - pending outcome of TE/MPE HiRadMat test
 - Assumed TCDQ half gap = 8.6σ (-0.5σ margin) → change in settings or optics **needs reevaluation** of the material robustness and magnet protection
 - Next steps: energy deposition studies for **DS magnets**
- **TCDS** → **MSDs**
 - **Graphite/CfCs in TCDS sufficiently robust** for HL beams, but **Ti-alloy** expected to **plastify** (a priori acceptable)
 - HL baseline is to **add one more TCDS module** to enhance the MSD protection → this will also relax the load on the Ti block
 - Next steps: study in more detail the load on the MSDs, in particular extend energy deposition studies for downstream **MSDs**

TCDQ → Q4, Q5

TCDS → MSDs

Conclusions

Backup

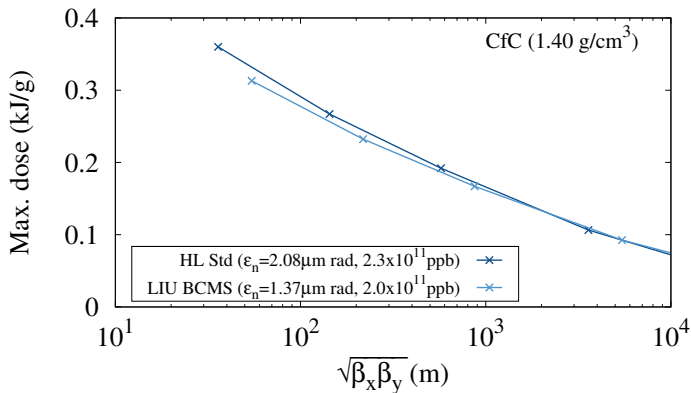
Considered optics and β -functions

- All studies presented here were carried out for **HLLHCV1.2**
- Selected the worst case for each device from flat/flat HV/round optics

Device	Optics	β_x	β_y	$\sqrt{\beta_x\beta_y}$	Remark
TCDQ	HLLHCV1.2	497 m	167 m	288 m	flat, end of squeeze, B1
	Run 2 (2015)	484 m	161 m	279 m	collision, B1
TCDS	HLLHCV1.2	168 m	174 m	171 m	flat HV, squeeze step 20, B2
	Run 2 (2015)	155 m	231 m	189 m	collision, B1
TDE	HLLHCV1.2	5052 m	3714 m	4331 m	round, end of squeeze, B2
	Run 2 (2015)	5076 m	3713 m	4341 m	collision, B2

M. Fraser

Single 7 TeV bunch: max energy density in CfC vs $\sqrt{\beta_x\beta_y}$



- A certain change of β and hence of the transverse bunch size might be digestable (yet there are other constraints for β)
- Note: the beam is swept across the TCDS/TCDQ/TDE front face
 - the peak energy density also strongly depends on the distance between neighbouring bunches in the sweep