Beam Current Monitors

Jean-Claude Denard
(Synchrotron SOLEIL)

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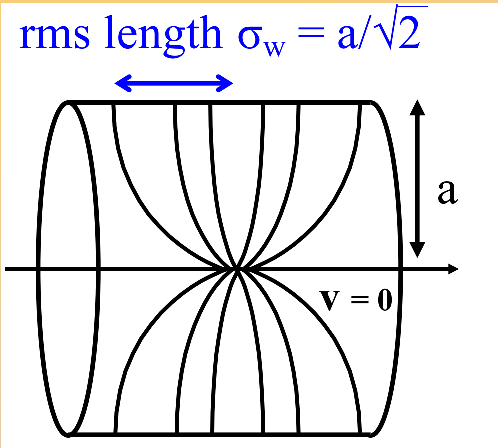
Summary

- ☼ Electromagnetic field associated to charged particle beams
- ☼ Destructive monitors: faraday cup ….
- ☼ Non destructive monitors; electromagnetic interaction
  - ➢ Wall current monitors
  - ➢ Current transformers
  - ➢ Cavity monitors, SQUID
- ☼ References

Longitudinal E Field Distribution of a Point Charge in a Conducting Tube

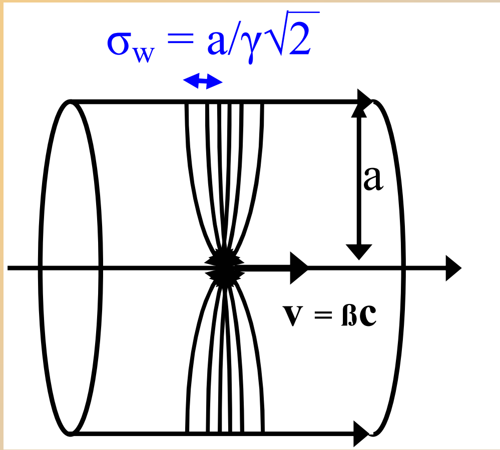
Static charge



- Charge produces E field
- E field induces image charges of opposite sign on the wall

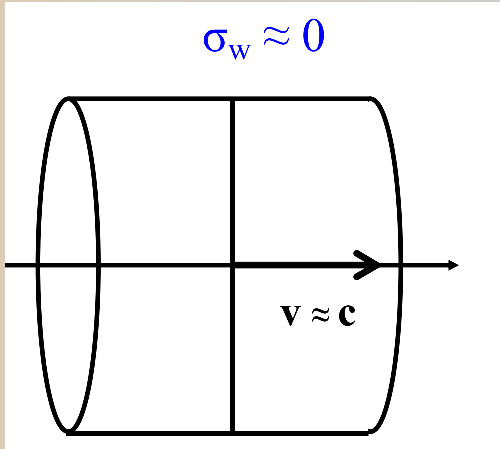
Note: <u>there is no E field outside the tube</u>

Moving charge



- Moving E field creates H field inside the tube
- The image charges move along with the inner charge.
- Wall current + beam current = 0. Then, Ampère's law, $\oint(H\, dl) = i$ indicates that <u>H = 0 outside</u> the tube (except for DC field).

Ultra-relativistic charge



- The Wall Current distribution is the image of the beam distribution but of opposite sign and without DC component

Example of Wall Current Longitudinal Distribution for a Point-like Moving Charge

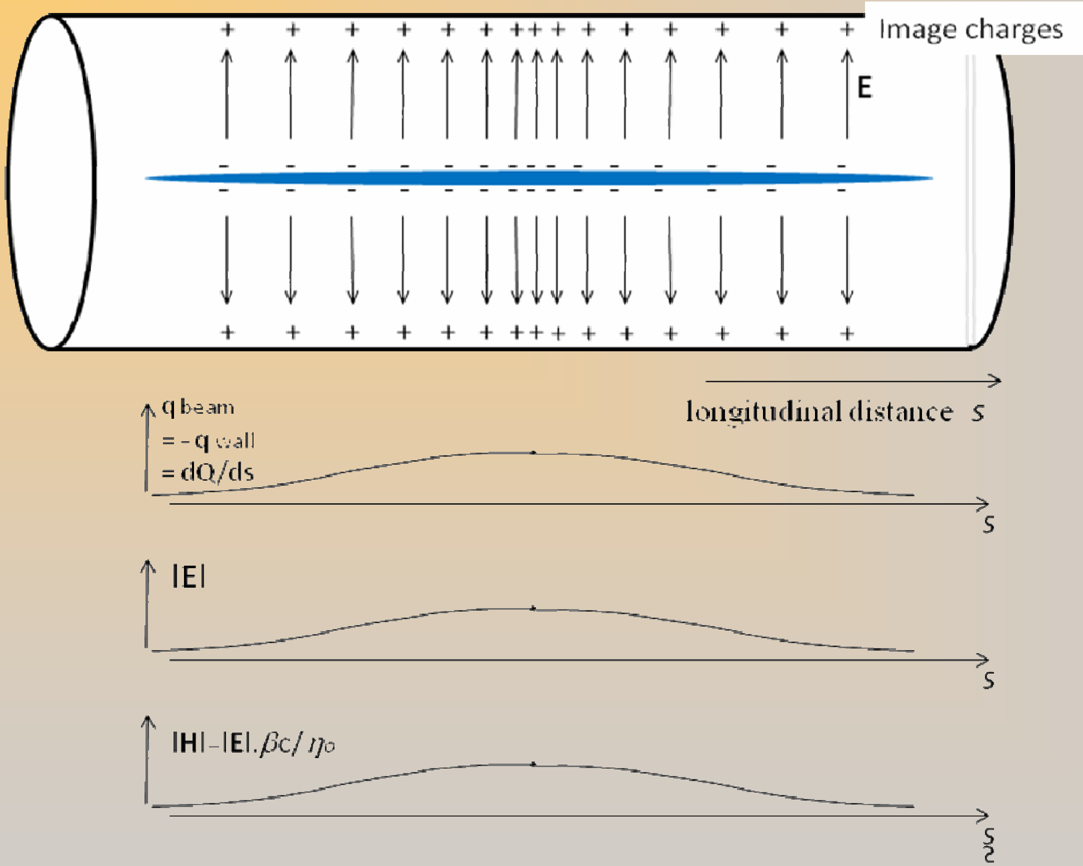
Numerical Examples with a Tube Diam. 2a = 50 mm

kinetic energy E for electrons for protons	0 0	100 keV 184 MeV	1 MeV 1.8 GeV	10 MeV 18 GeV
Lorentz factor γ	1	1.2	3	20.6
$\beta = (1-1/\gamma^2)^{1/2}$	0	0.55	0.94	0.999
$\sigma_w = a/(\gamma\sqrt{2})$	18 mm	15 mm	6 mm	0.9 mm
rms length (ps) = $a/(\beta\gamma c\sqrt{2})$	∞	90 ps	21 ps	2.9 ps
Wall current BW limitation (*)	0	1.8 GHz	7.5 GHz	55 GHz

(*) The actual distribution is not gaussian, but for the sake of simplicity, its Bandwidth has been approximated to that of a gaussian distribution of same rms length

If $\sigma_l >> a / \gamma\sqrt{2}$, wall current distribution = beam distribution σ_l

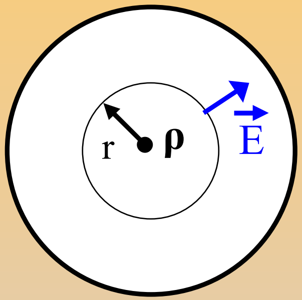
Fields associated to a charged particle beam for a beam length $\sigma_l >> a / \gamma\sqrt{2}$



Transverse Field Distribution

Static charge

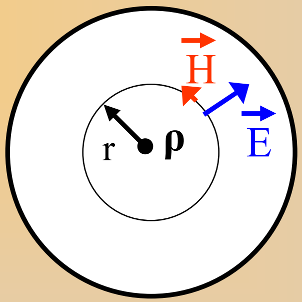
v = 0



no magnetic field inside

Moving charge

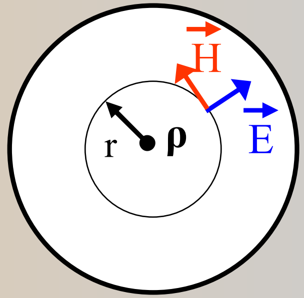
v < c



magnetic field appears

Ultra relativistic charge

v ≈ c



Ampère's Law : $\oint \vec{H}.\vec{dl} = i$

at radius r $\rightarrow H(r) = i / 2\pi r$

TEM wave : $\dfrac{|\vec{E}|}{|\vec{H}|} = \eta_o$

With $\eta_o = \sqrt{\mu_o / \varepsilon_o} = 377\ \Omega$ = vacuum impedance

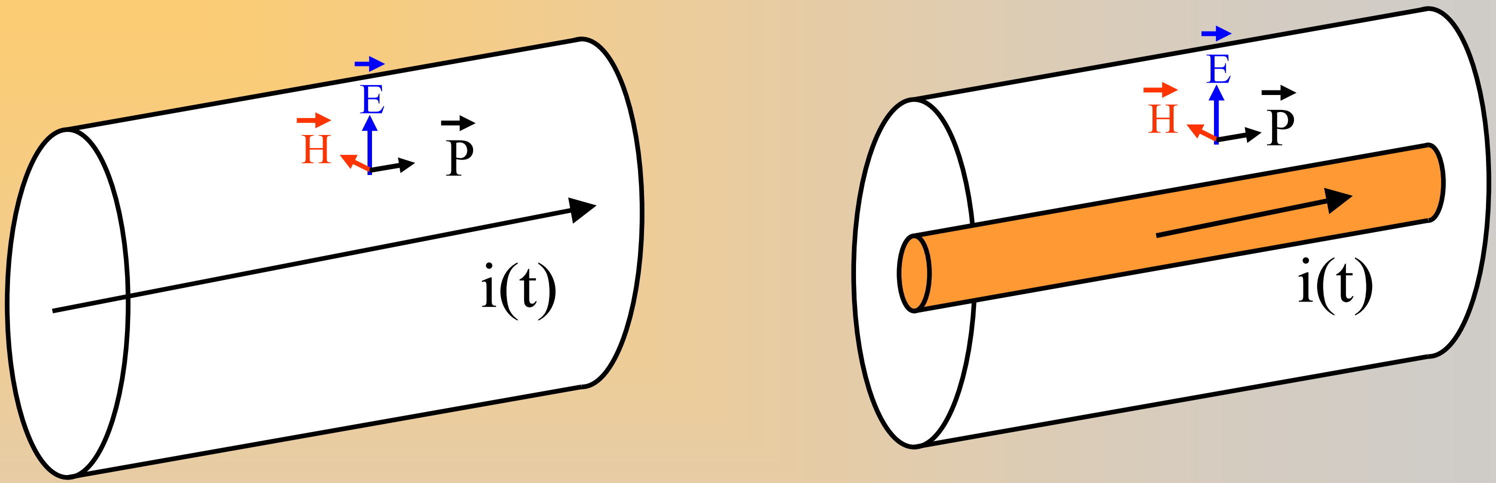
ε_o = vacuum electric permittivity

μ_o = vacuum magnetic permeability

outside the pipe: no E field

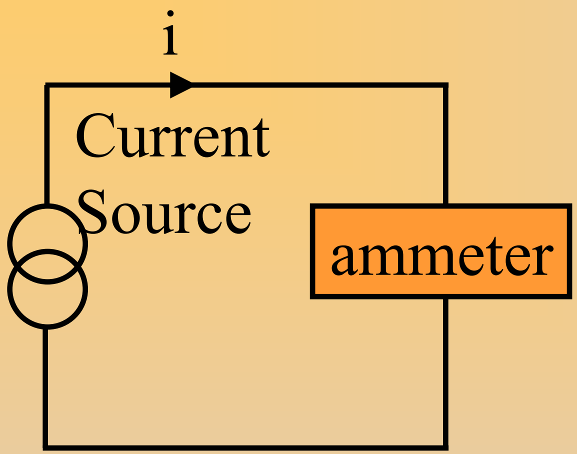
no magnetic field (except DC)

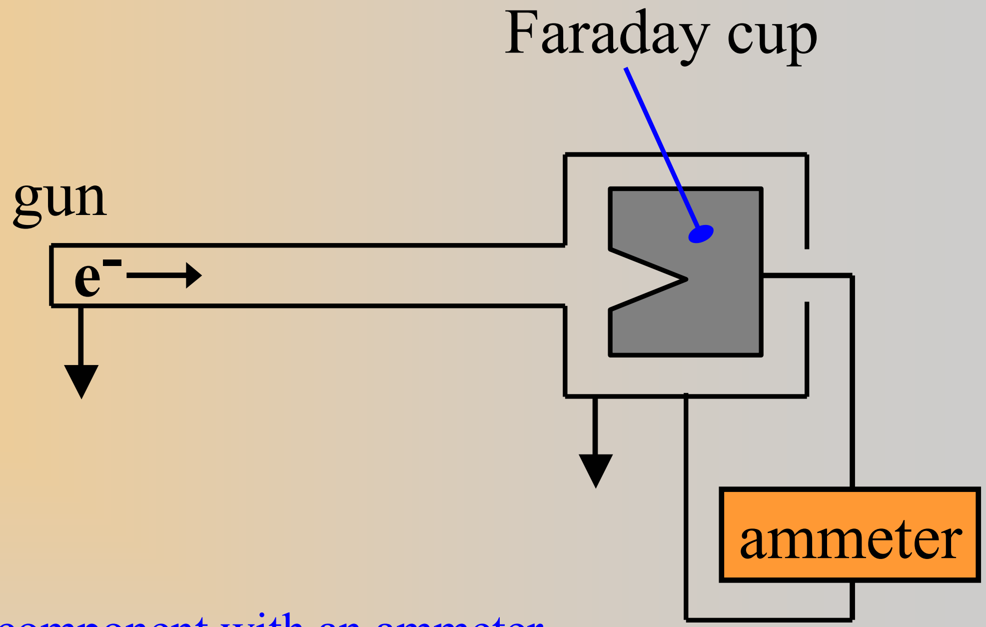
TEM Wave in Vacuum Chamber is Like in an Air Filled Coaxial Transmission Line



- **Similarities**: TEM wave carries the same EM energy (Pointing vector $\vec{P} = \vec{E} \times \vec{H}$):
- a monitor can be realistically tested in a coaxial line structure.
- **Some differences**:
  - At High frequencies (cutoff frequencies are different in the two cases)

Faraday Cup



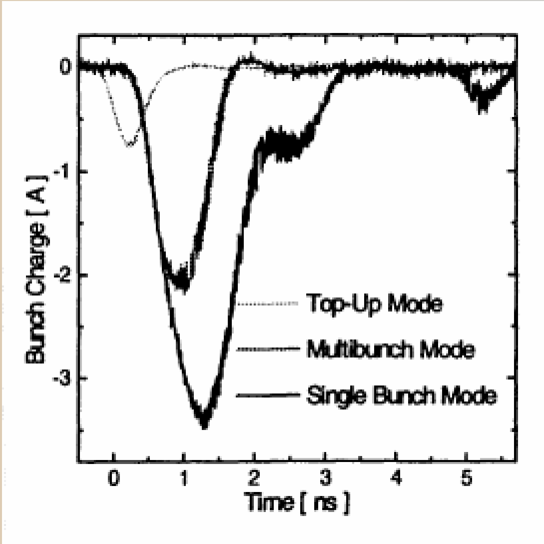


- Destructive
- Absolute measurement of DC component with an ammeter
- An oscilloscope or Sample & Hold measures the peak current in case of pulsed beam.
- Can be used for the calibration of non destructive monitors that provide relative measurements. For example FC calibrates an RF cavity current monitor on CEBAF injector (CW superconducting Linac).

Faraday Cup; Design Issues

- Absolute accuracy is usually around 1%, it is difficult to reach 0.1%.
- Needs to absorb all the beam: block with large entrance size and thickness >> radiation length. A FC built at DESY and presently used on a low current 6 GeV beam at JLAb uses 1 m^3 of lead (12 tons).
- Backscattered particles (mostly e^-): narrow entrance channel, bias voltage or magnetic field redirect the backscattered e^- on the FC. Accuracy evaluation requires Monte Carlo simulations (EGGS from SLAC; GEANT from CERN).
- Power (W) = E in MeV × I in μA.
  Example: 5 MeV FC in CEBAF injector with 200 μA CW beam → 1000 W.
  A cooling circuit takes the power out. The isolation is done with de-ionized water and insulating rubber tubes.
- <u>Safety issues</u>: FC needs to be always terminated by a DC circuit to avoid arcing and a potentially dangerous high voltage that would develop at cable end. A pair of high impedance diodes can be connected in parallel on the FC output.

SLS Wide Bandwidth Coaxial Faraday Cup (0-4 GHz)



M. Dach et al. (SLS) ;
BIW2000

Calorimeter

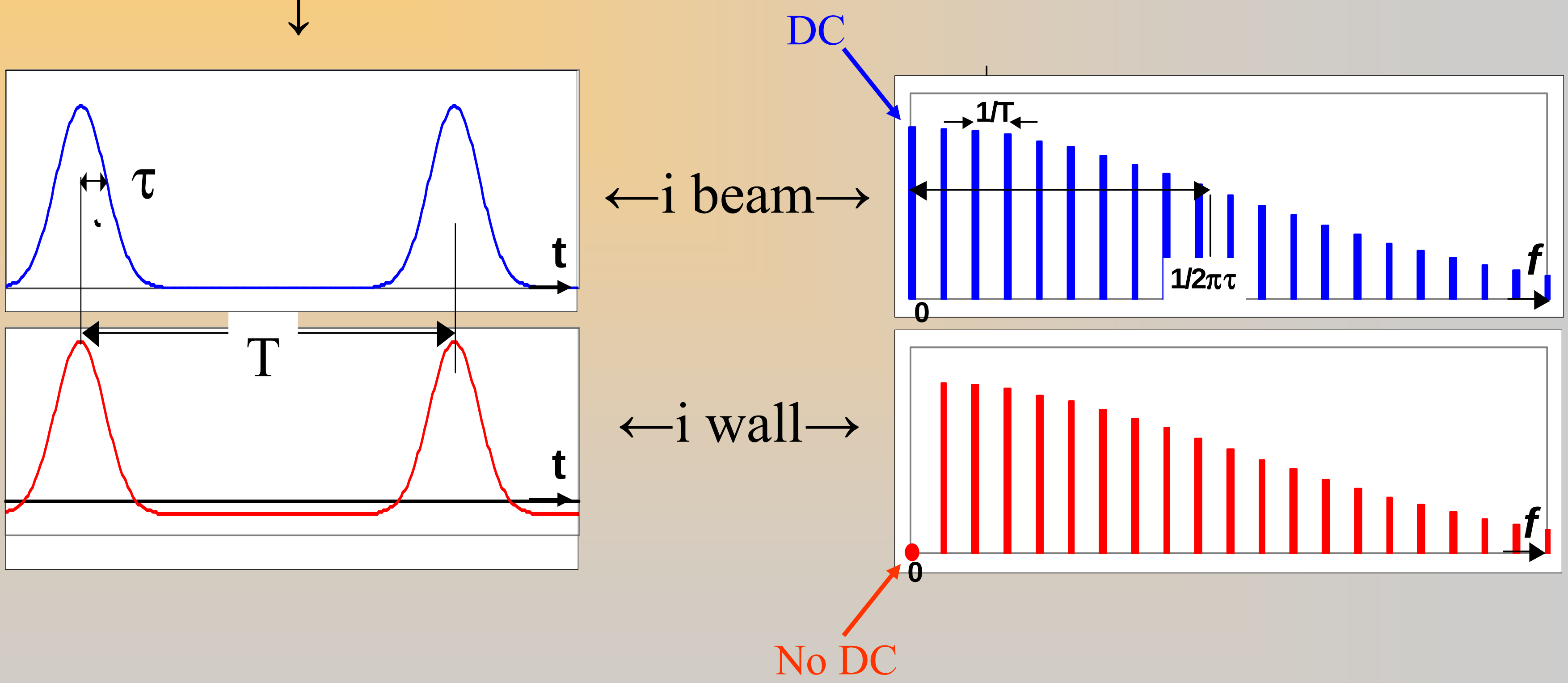
- Calorimetry refers to a direct measurement of the total energy delivered to a massive block of metal (silver or tungsten) over a period of time.
- Total energy is determined by measuring the temperature rise of the object if:
  - The average beam energy is precisely known
  - Any energy losses can be accounted for by reliable calculation or direct measurement.

- A calorimeter has been developed for CEBAF CW beam (A. Freyberger, to be published)

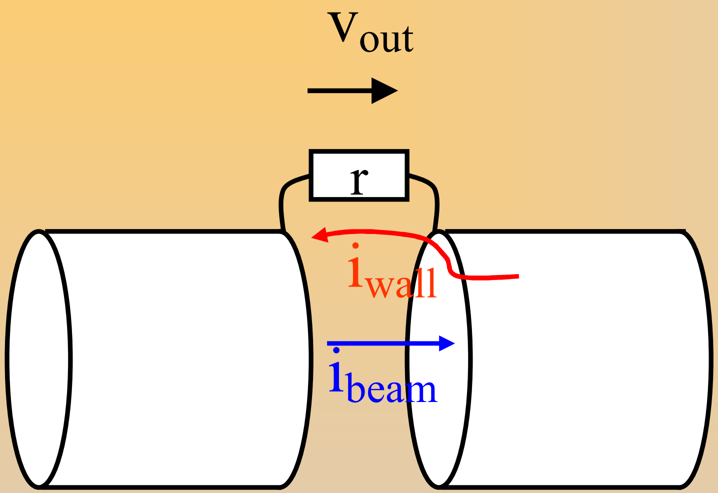
Wall Current Monitor:
Beam and Wall Current Spectra for Ultra Relativistic Beams

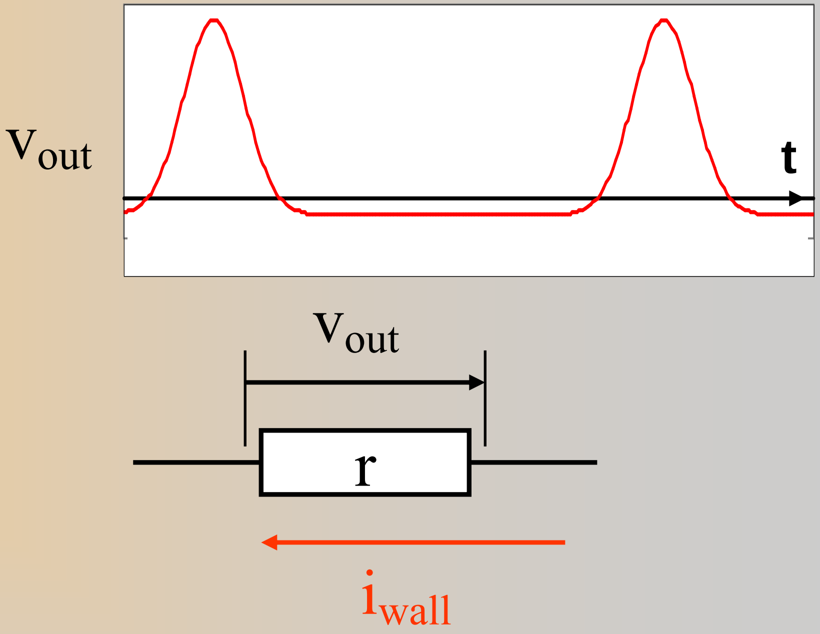
Time domain ↓

Frequency domain



Wall Current Monitor: Concept

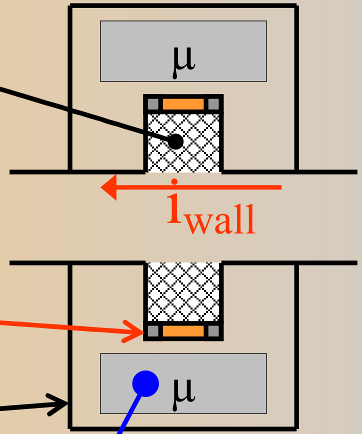


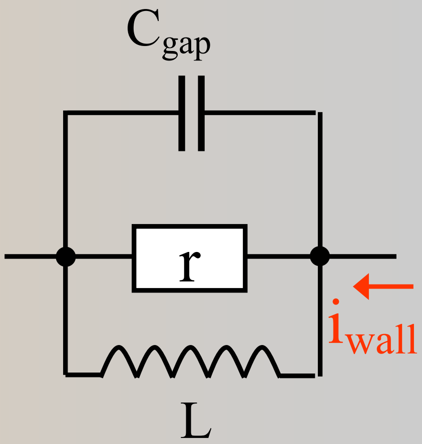


$$v_{out} = i_{wall} * r$$

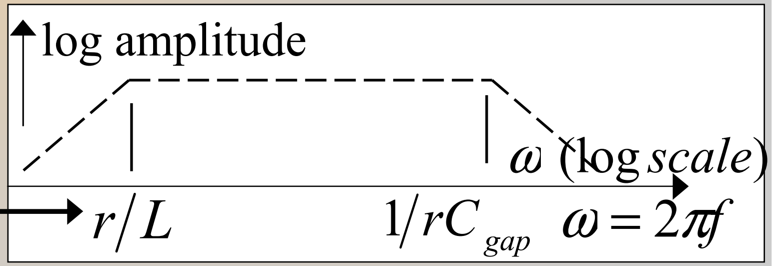
WCM: From Concept to Actual Implementation

- For vacuum quality: ceramic gap
- r is made of several resistors in parallel, distributed around the gap. Special chip resistors still behave as resistors in the GHz frequency range.
- Electrical shield: avoids parasitic external currents flowing through r, and prevents the beam EM field from radiating outside the monitor.
- High μ material fills the space between gap and shielding for low frequency response.



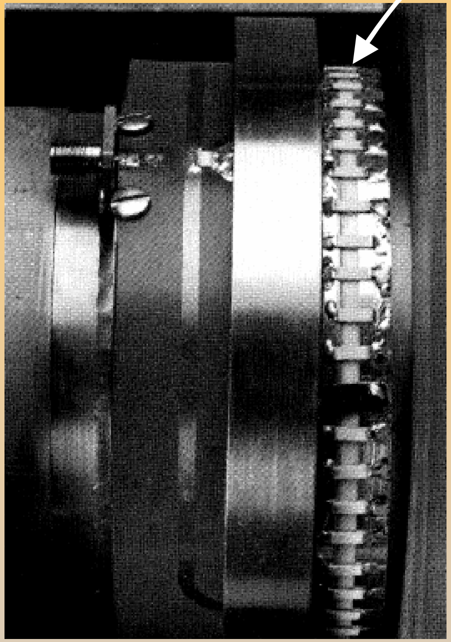


WCM response



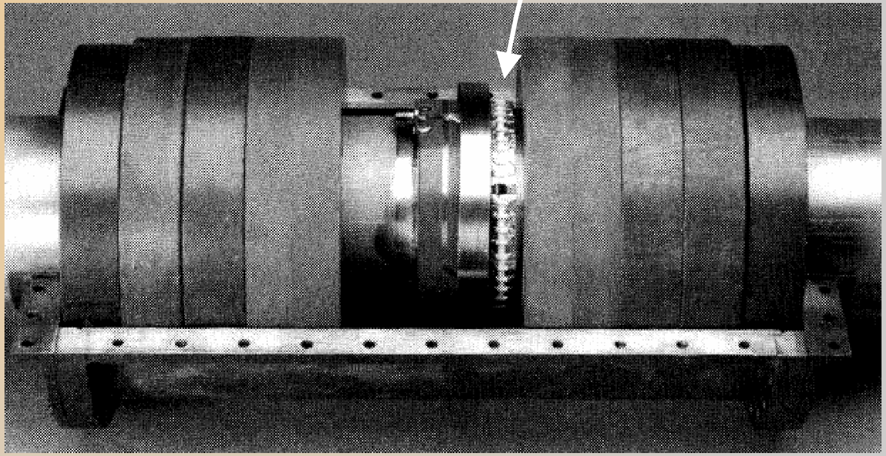
$$L = \frac{\mu_o \, \mu_r}{2\pi} h \; Ln\,(b/a)$$

Implementation Example: 6 kHz to 6 GHz WCM : (R. Weber BIW93)



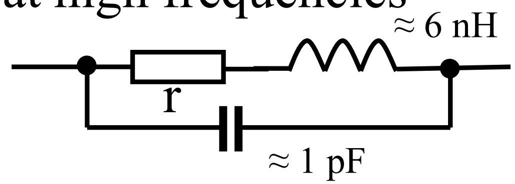
Ceramic gap and surface mounted resistors

ferrites ferrites



Resistors are not pure resistors at high frequencies

≡



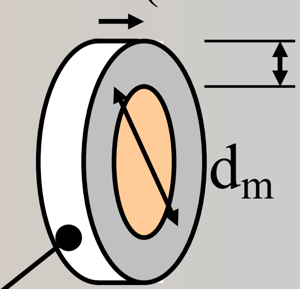
Resistor with 5 mm wire connections

In the GHz range, standard resistors are replaced by Surface Mounted Resistors that have smaller inductance and capacitance.

6 kHz to 6 GHz WCM : (R. Weber)

- r = 1.4 ohm (80 resistors in parallel).

- ***rC$_{gap}$ circuit at high frequencies***
  - Ceramic gap considered as a lump capacitor:
    d_m= 90 mm; t = 3.2 mm; and w = 4.5mm
    => C_{gap} = 33 pF
    and $f_h = 1/2\pi r C_{gap} = 3.4\,\text{GHz}$
  - Ceramic gap behaves as a radial transmission line matched to its 1.4Ω characteristic impedance: f_h > 6 GHz (measured)

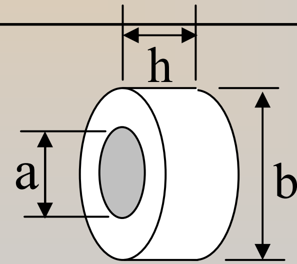


$$C_{gap} = \varepsilon_0 \varepsilon_r \frac{S}{t}$$

$$S \cong w * 2\pi d_m$$

- ***rL circuit at low frequencies***

$$f_{low} = r/2\pi L = 5.6\,\text{kHz with } L = 40\mu\text{H}$$

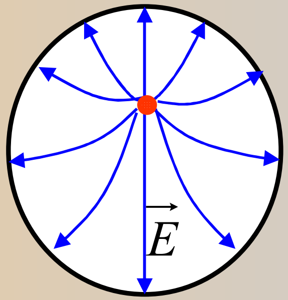


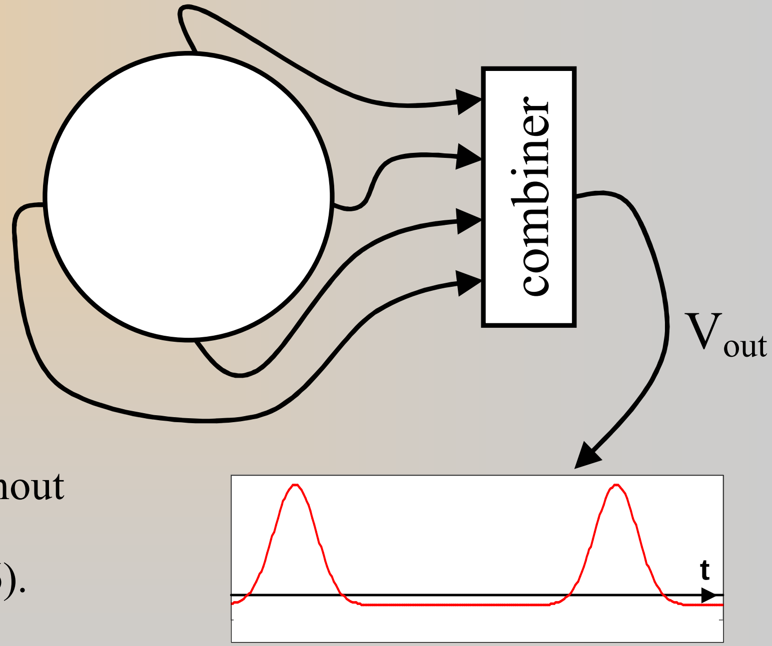
Shield = 1 turn

$$L = \frac{\mu_o \mu_r}{2\pi} h \; Ln(b/a)$$

WCM: Output Connection; Beam Position Dependence

- Off-center beam yields higher wall currents near the beam.
- There is a difference signal ($i_{\text{wall top}} - i_{\text{wall bottom}}$) that propagates around the gap. The wave velocity is reduced by a factor $\sqrt{\varepsilon_r} = 3$ with alumina.
- With our example, propagation time is 2.8 ns. Position dependence starts around f >>300 MHz. We want no position dependence up to several GHz!
- A practical solution is to combine signals from four quadrants.

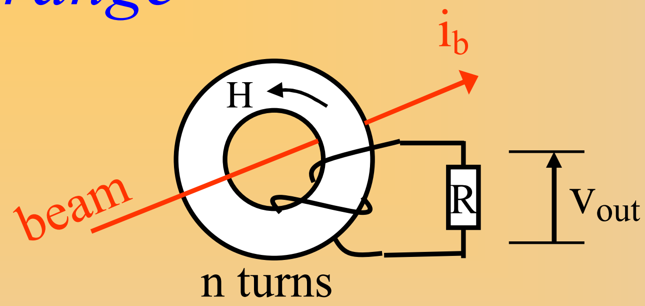




- A 20 GHz WCMs is in development at CERN.

  3D electromagnetic simulation codes (MAFIA, GDFIDL, HFSS) are necessary for damping the high frequency components of the wake fields without loading significantly the useful signal (L. Soby et al., EUROTeV-Report-2006-104, 2006).

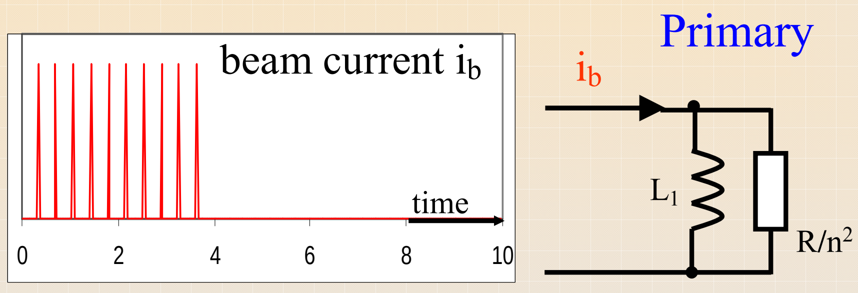
Beam Current Transformer in low and mid frequency range

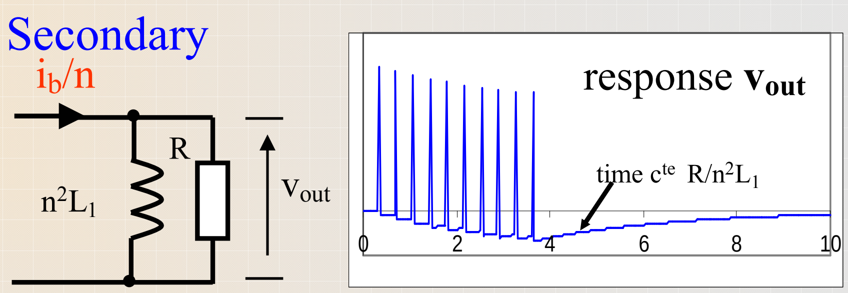


- Beam is a 1-turn primary winding

The magnetic field is :

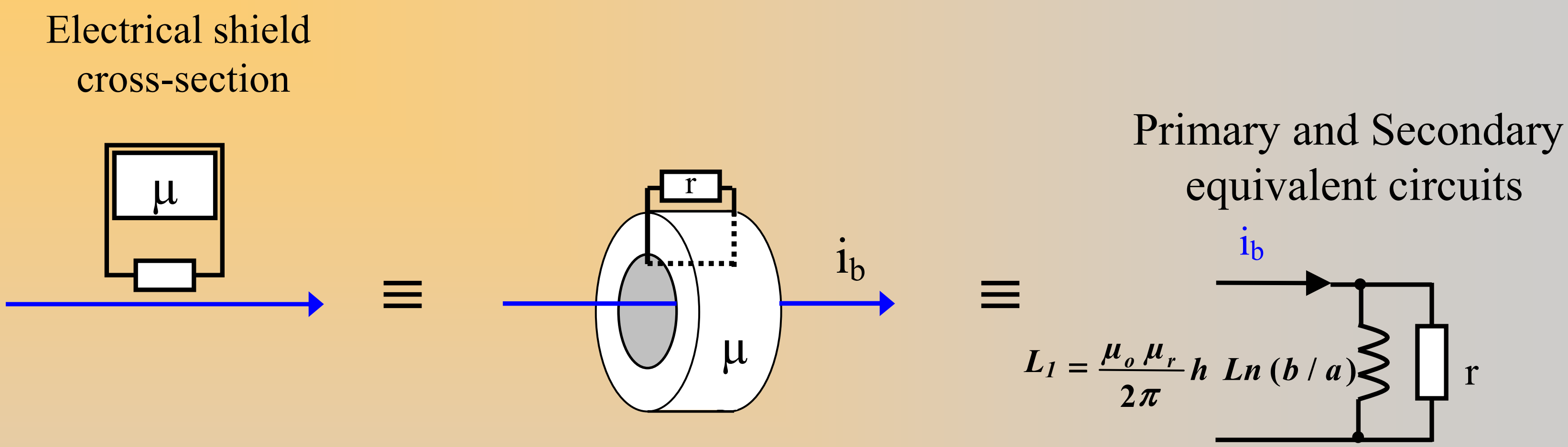
H ≈ beam current / toroid circumference





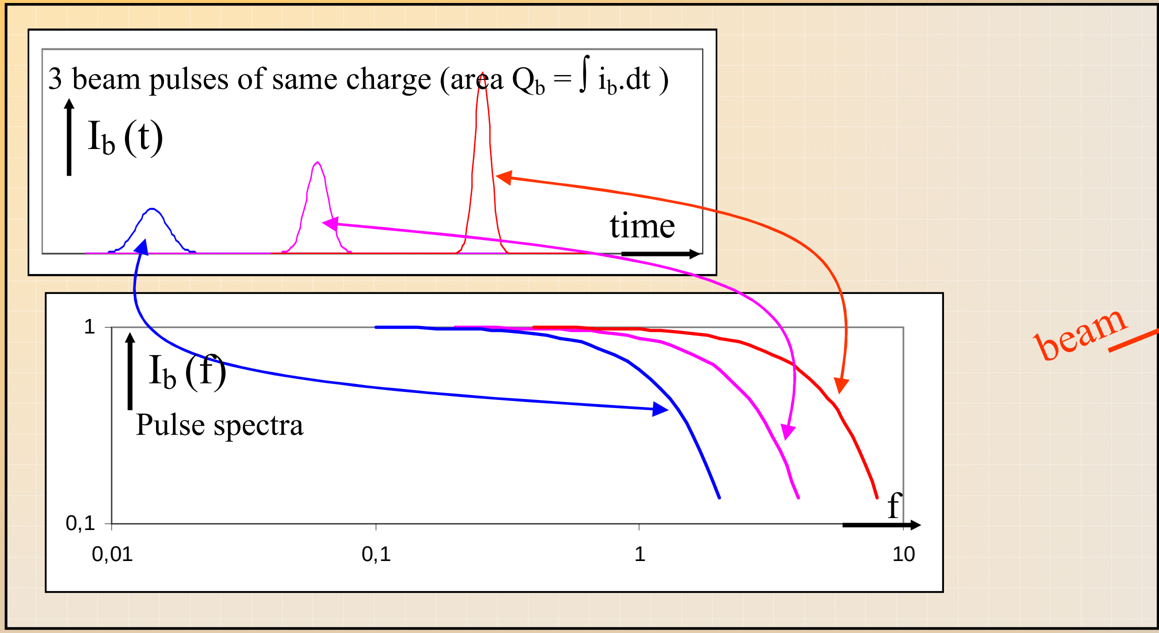
- Beam current i_b is « transformed » into i_b/n on the secondary winding. n = 10 or 20 are common values.
- $V_{out} = i_b/n * [R / (1 + R / jn^2L_1\omega)]$; with L1 = one-turn self inductance
- In mid range frequencies, $L_1\omega >> R$, and $V_{out} \approx R\, i_b / n$
- All beam current transformers need an insulating gap in order to leave the magnetic field reach the toroid.

WCM = Current Transformer with n=1

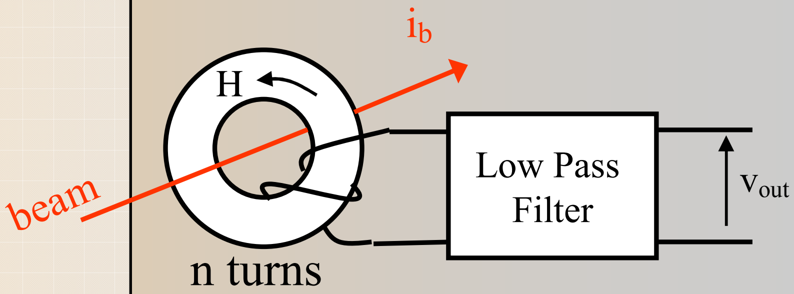


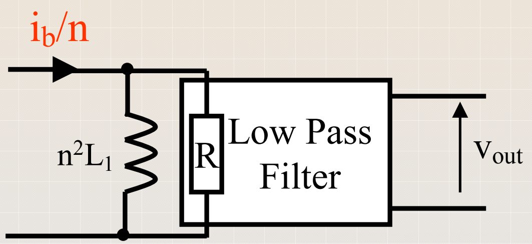
The electrical shield is equivalent to a 1-turn winding
But the high frequency analysis is better done using the WCM concept

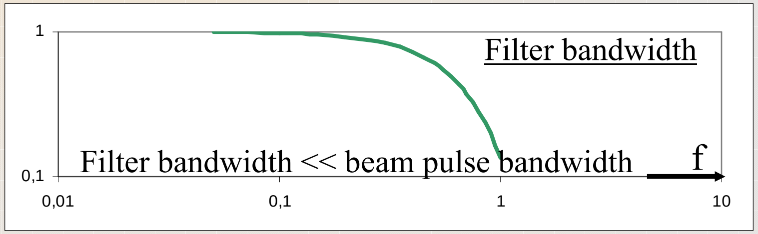
Integrating Current Transformer (ICT) = Beam Charge Monitor

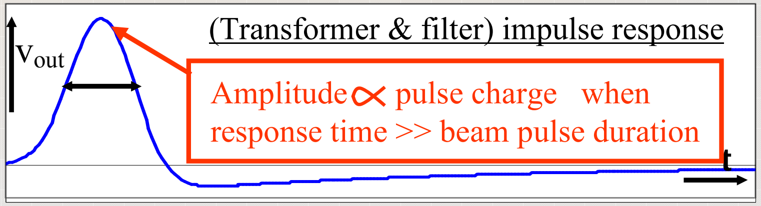


for short pulses long rep. rate:
warm Linacs & transfer lines

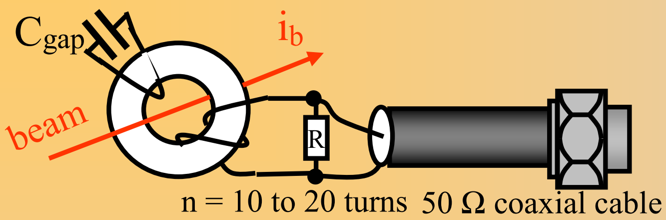


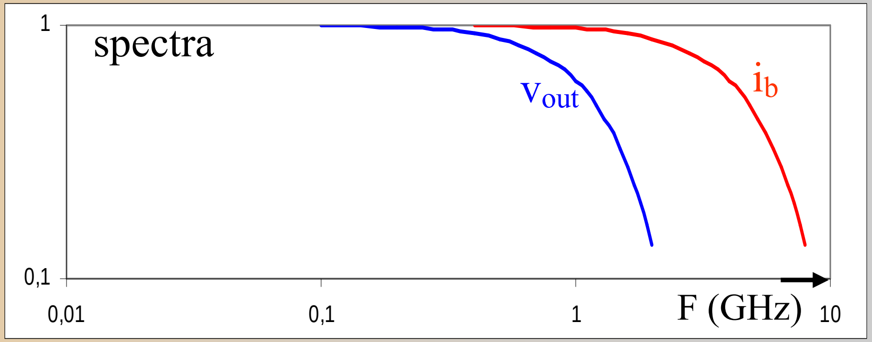




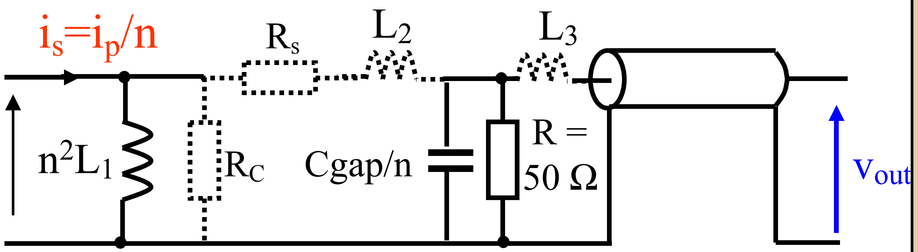


Fast Current Transformer (FCT)





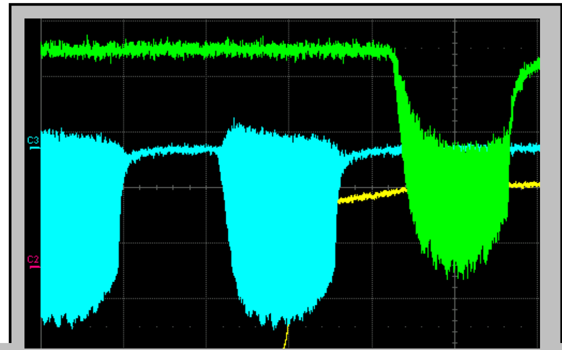
High frequency equivalent circuit



- The gap capacity usually sets a high frequency limit.
- **R_C represents transformer core losses, it depends on frequency and field amplitude**
- **R_s is the series resistance of the secondary winding**
- **L2 is the leakage inductance**
- **C is the addition of stray capacities and Cgap/n^2; a gap made of Al2O3, a few mm thick is usual (C_{gap}≈30pF).**
- **L3 is the inductance of the coaxial cable connection**
- **Coaxial cable has increasing losses with frequency**
- **Very high frequency losses occur into the shield cavity where the beam excites many modes.**
- **The high frequency equivalent circuit does not take into account the cavity mode losses. Wake field loss evaluation possible with 3D simulation codes (GDFIDL…)**

<u>Example</u>: Soleil Booster and Tranfer Line

- **Transformer bandwidth is narrower than beam spectra.**
- **Part of the signal power is lost at high frequencies into the magnetic core.**
- **There is little power taken from the beam; then beam stability or magnetic core heating are no issues.**

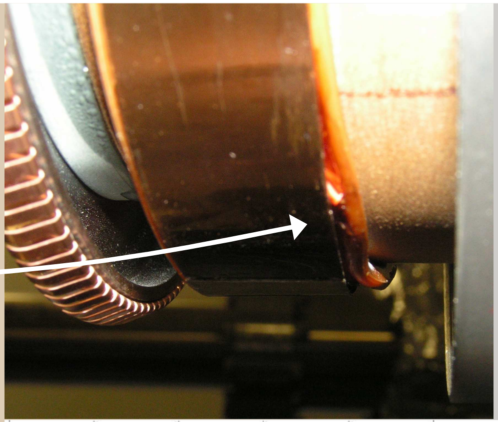


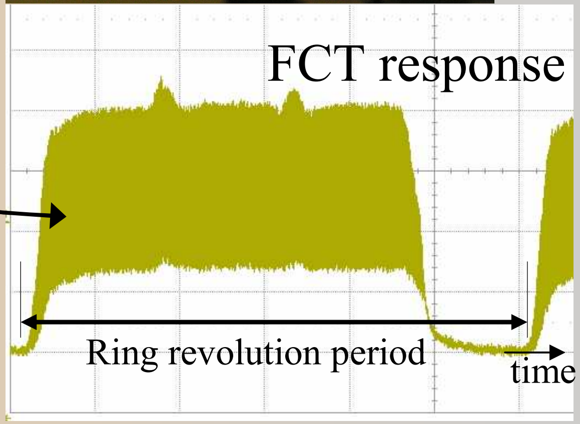
Last 2 turns in Soleil Booster and first turn in Storage Ring seen on FCTs

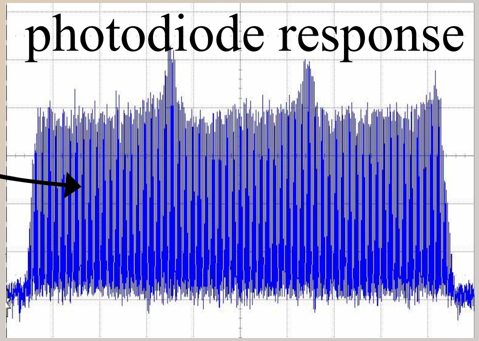
FCT Issues on high current Storage Rings

Example: Soleil Storage Ring FCT

- Magnetic core heated over 110°C with a 300 mA beam (¾ Ring filling)
- The heating problem has been solved by installing additional capacitors in parallel on the gap and improving the air cooling of the toroid.
- But the reduced bandwidth affects the information: the signal does not return to zero between bunches at 2.8 ns intervals
- Resistors around the gap (like in a WCM) can reduces the power entering the cavity.
- Another solution is to fill the cavity space with microwave absorbing material.
- A thorough study of these solutions would need GDFIDL and HFSS simulations and plenty of time.
- A good and cheap solution seems to use a photo-diode illuminated by the synchrotron radiation easily available in the diagnostic hut.
- Then, the gap could be removed which will reduce the high order mode losses on the beam.





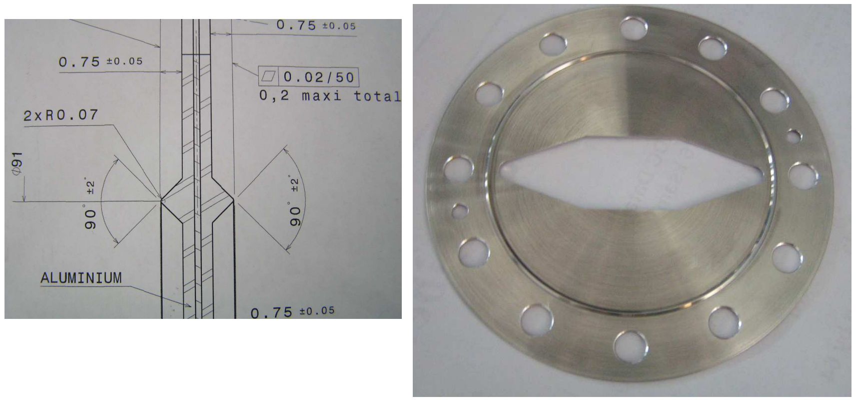


DC current Monitors: DCCTs, also called PCTs

- DCCTs are important monitors for Storage Rings. The 1 µA resolution is usually less than 1E-5 of the beam current. With a CW superconducting Linac beam of 200 µA (CEBAF), the 1 µA resolution is only 0.5 %.
- A DCCT is a zero magnetic flux sensor. It feeds back a DC current in the beam current opposite direction in order to cancel the magnetic flux in a set of toroids. A precision resistor in the feedback current path yields the output voltage.
- The DC magnetic flux induced by the beam into the magnetic circuits does not depend on the beam position (Ampère's law).
- DCCTs are commercially available.

Issues to address before installing a DCCT

- The zero flux sensing is affected by external magnetic fields: magnetic shieldings are necessary
- The zero current drifts with temperature: power losses, especially through the gap must be prevented.
- Isolation gap can be very narrow and gap capacitor high (a few nF).
- Gap Example: Elettra and Soleil have custom made isolation gap. It is a capton foil sandwiched between two aluminum half gaskets.



N. Rouvière vacuum gasket design

Other Non Destructive DC Monitors

- Cryogenic Current Comparator (A. Peters, GSI). Used for low current ion beams. A CCC uses a SQUID as null detector for the magnetic field (SQUID = **S**uperconducting **Qu**antum **I**nterference **D**evice). The SQUID detects extremely small changes of the magnetic field. A fraction of nA resolution for 100 nA beams has been obtained. It performs an absolute measurement. Like with all transformers, Ampere's law makes it independent of beam position. But it a very delicate instrument to implement.

- Cavity current monitor for CW beam measurement. It is a passive cavity in fundamental mode like an accelerating cavity. The output pick up voltage is proportional to the beam current. Like in a linac where the beam energy does not depend on beam position, the output power of a passive cavity does not depend on beam position in a rather large central area. It is sensitive to nA beams but needs an external calibration.
  Example: CEBAF, stainless steel low-Q cavities ($Q \leq 8000$) for low currents, calibrated against a DCCT at ≈ 100 µA.

References

- Much of the content of this lecture has been extracted from the following:

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