

“Transverse beam profiles”

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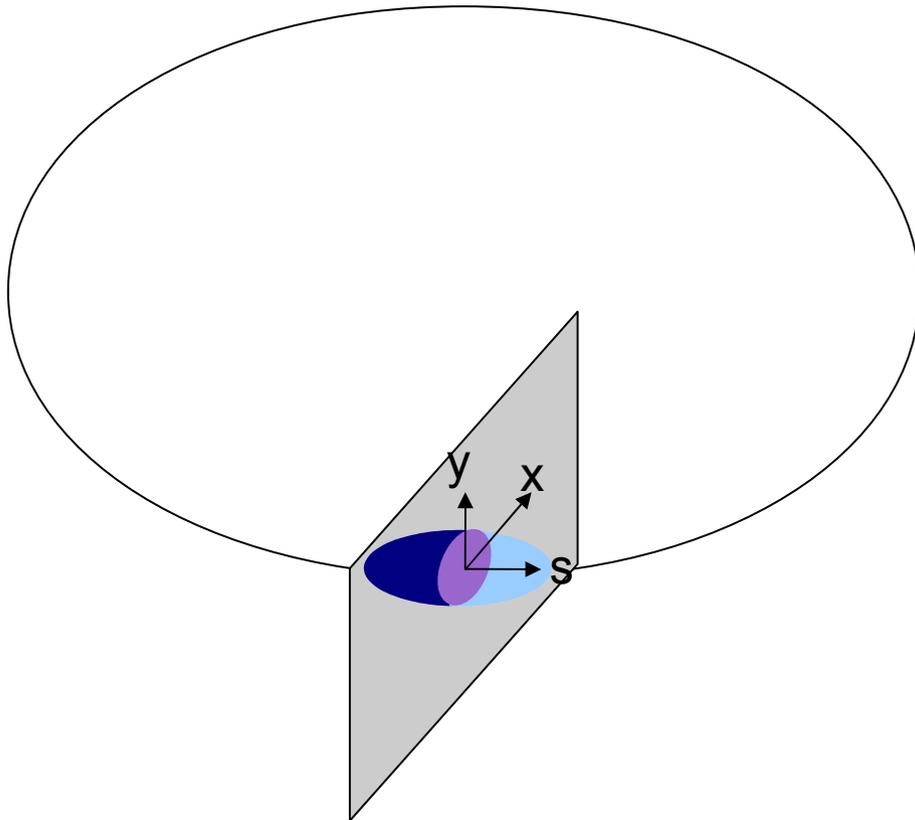
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Content

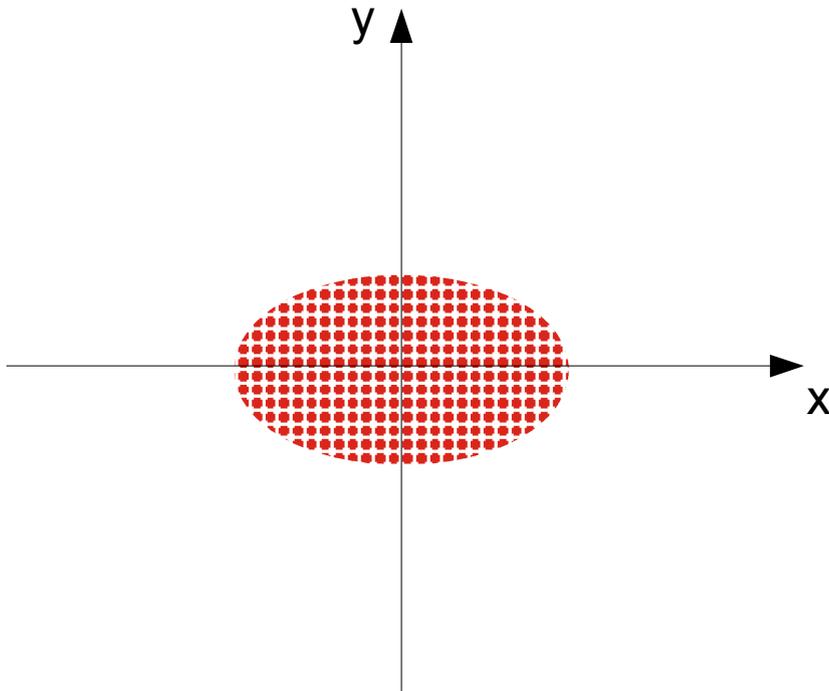
- Coordinate system
- Transverse space
- Transverse phase space
- Phase space dynamics
- Interaction of particles with matter
- Radiation emission by charged particles
- Sampling of distributions in 2D space

Coordinate System



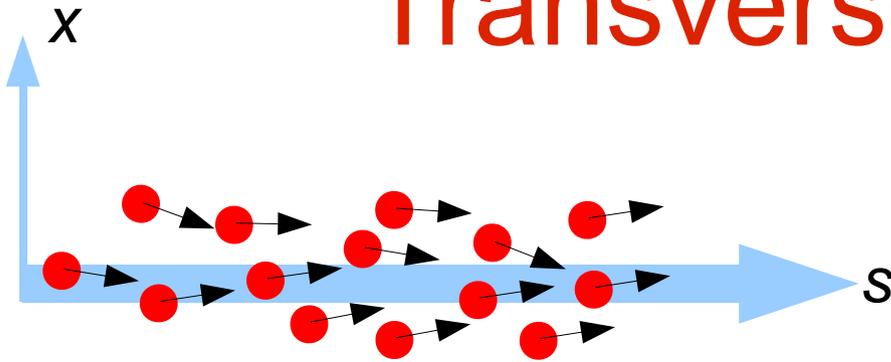
- Longitudinal coordinate
 - defined by the direction of motion of the beam
 - Axis indicated with s
- Transverse Plane
 - Plane orthogonal to the close orbit
 - Axes usually indicated with x and y and referred as *HORIZONTAL* and *VERTICAL*

Transverse x,y space

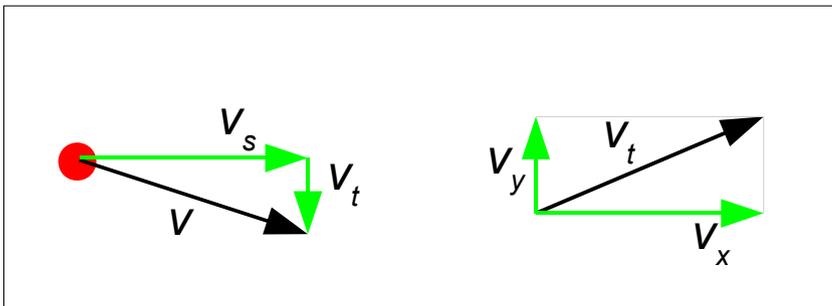
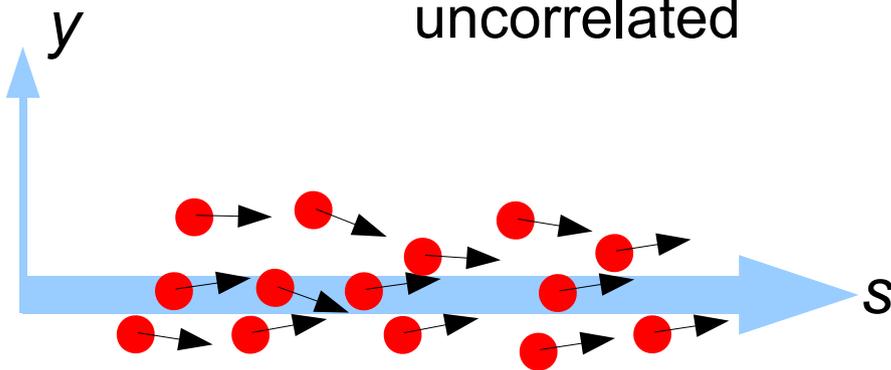


- Define a plane orthogonal to the beam trajectory at a given s
- Record the x,y coordinates of each particle crossing this plane
- Plot on a 2D chart (x, y) each particle

Transverse phase space

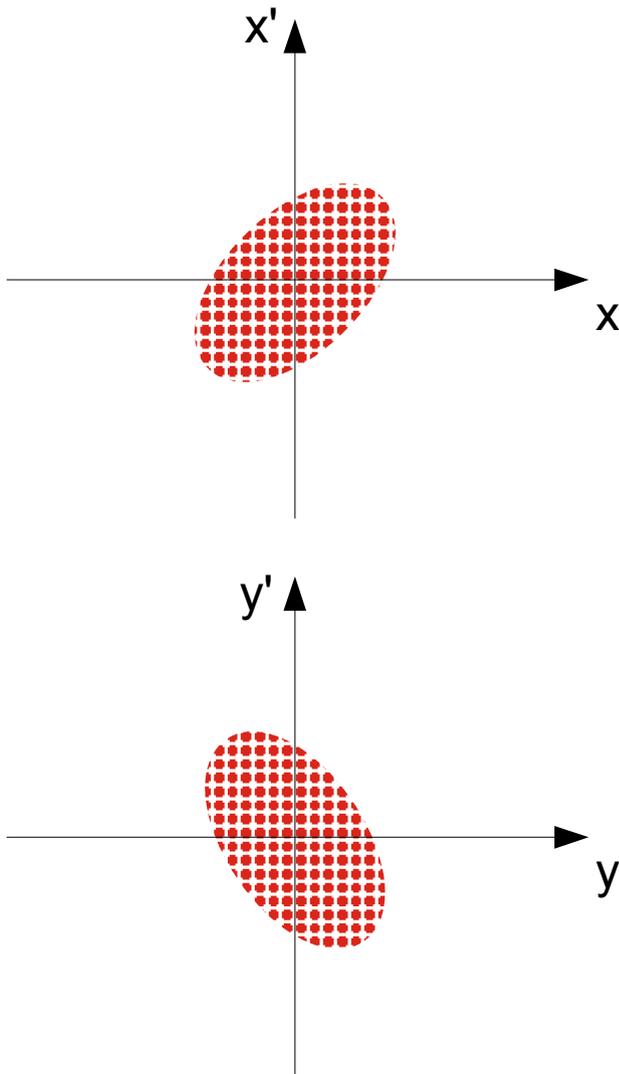


v_x , v_y and v_s are normally uncorrelated



- Beam moves along s
- Each particle moves in a different direction
- Velocity has 2 components
 - *Transverse* $v_t = v_x \hat{x} + v_y \hat{y}$
 - *Longitudinal* v_s
- Transverse components also called x' and y'

Transverse phase space (2)

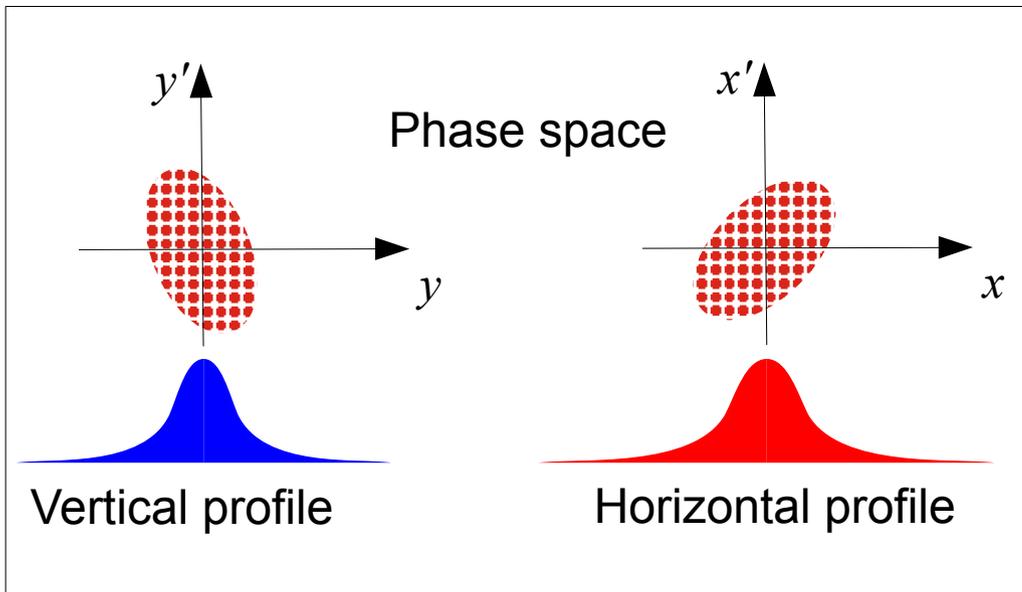
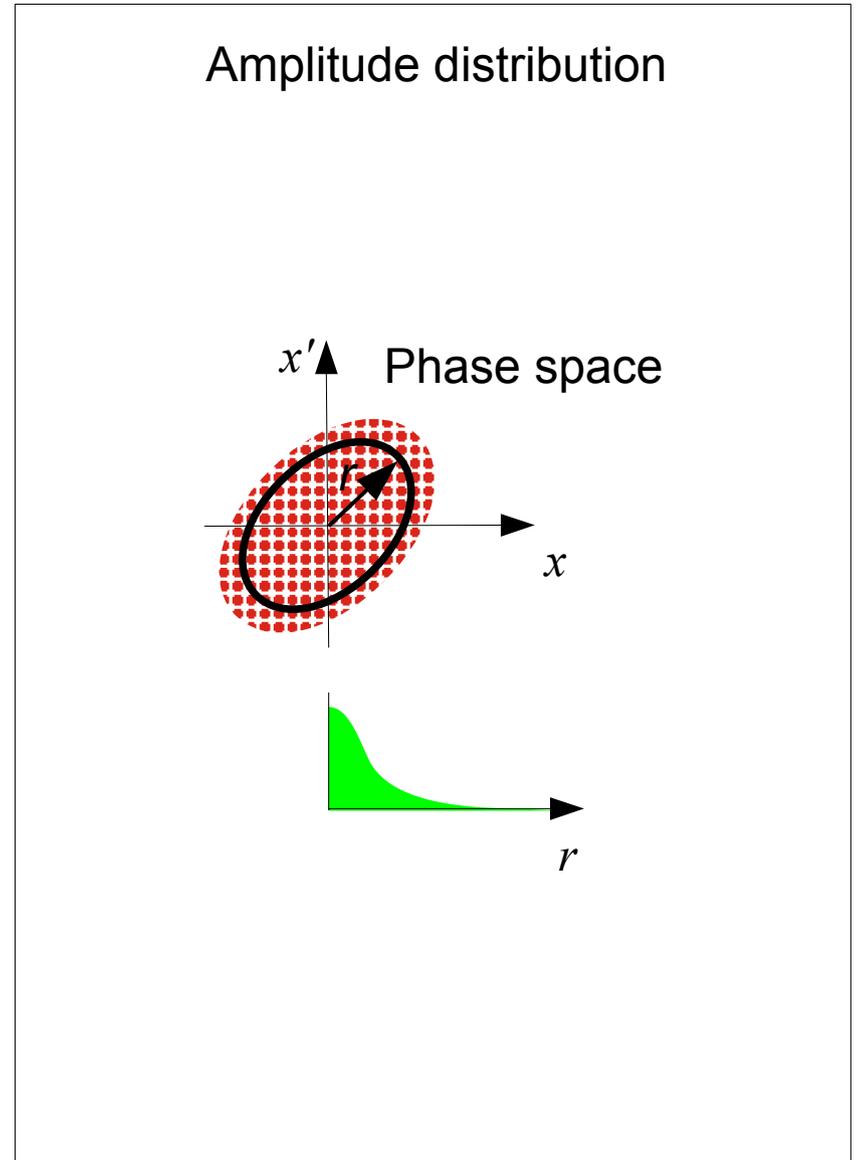
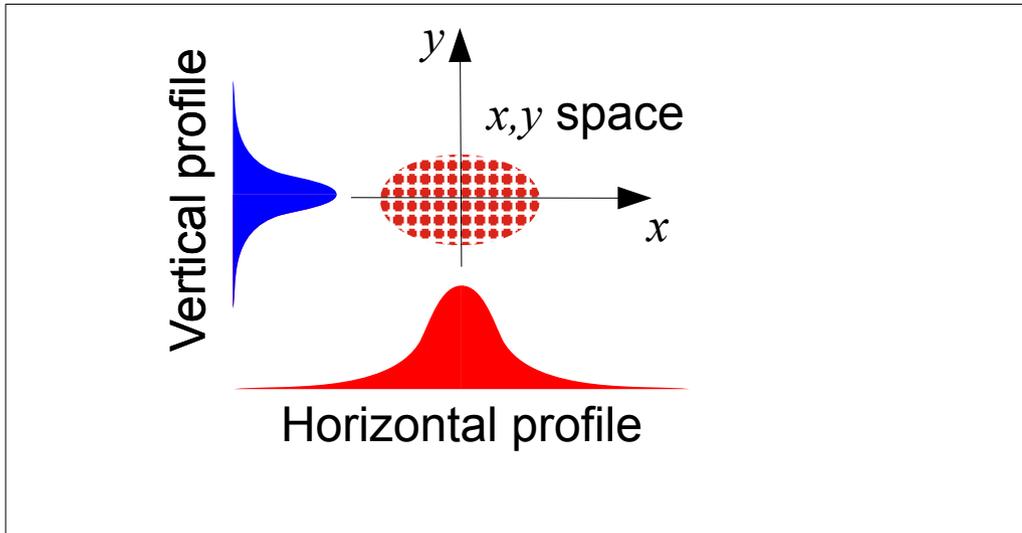


- Take the same plane as before
- Note x, v_x and y, v_y for each particle crossing the plane
- Plot on a 2D chart (x, v_x OR y, v_y) of each particle
- Rename $v_x \rightarrow x', v_y \rightarrow y'$
- Area of the ellipse is an invariant and is called transverse emittance $\varepsilon_{x'}$, $\varepsilon_{y'}$

Transverse spaces

- The x,y space and the phase space are different things
- Their projections along x or y are however the same thing
- Phase spaces contain the information needed for beam dynamic calculations
- x,y space is easier to sample
- Perform measurement in x,y and use optics parameters and beam dynamic theories to calculate the phase space

Beam Profiles



Beam Profiles (2)

Particles distribution:

$$i(x, y)$$

Profiles:

$$\left\{ \begin{array}{l} Prof_H(x) = \int_{-\infty}^{+\infty} i(x, y) dy \\ Prof_V(y) = \int_{-\infty}^{+\infty} i(x, y) dx \end{array} \right.$$

Typically $i(x, y)$ is Gaussian:
 N_0 = total number of particles

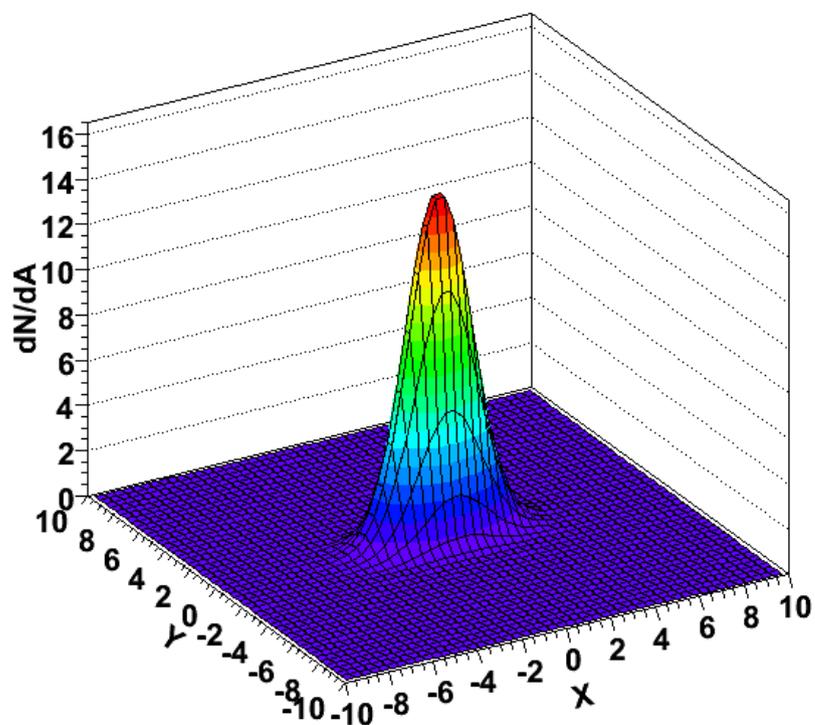
$$i(x, y) = \frac{N_0}{2\pi\sigma_x\sigma_y} e^{-\left(\frac{x^2}{2\sigma_x^2} + \frac{y^2}{2\sigma_y^2}\right)}$$

⇒

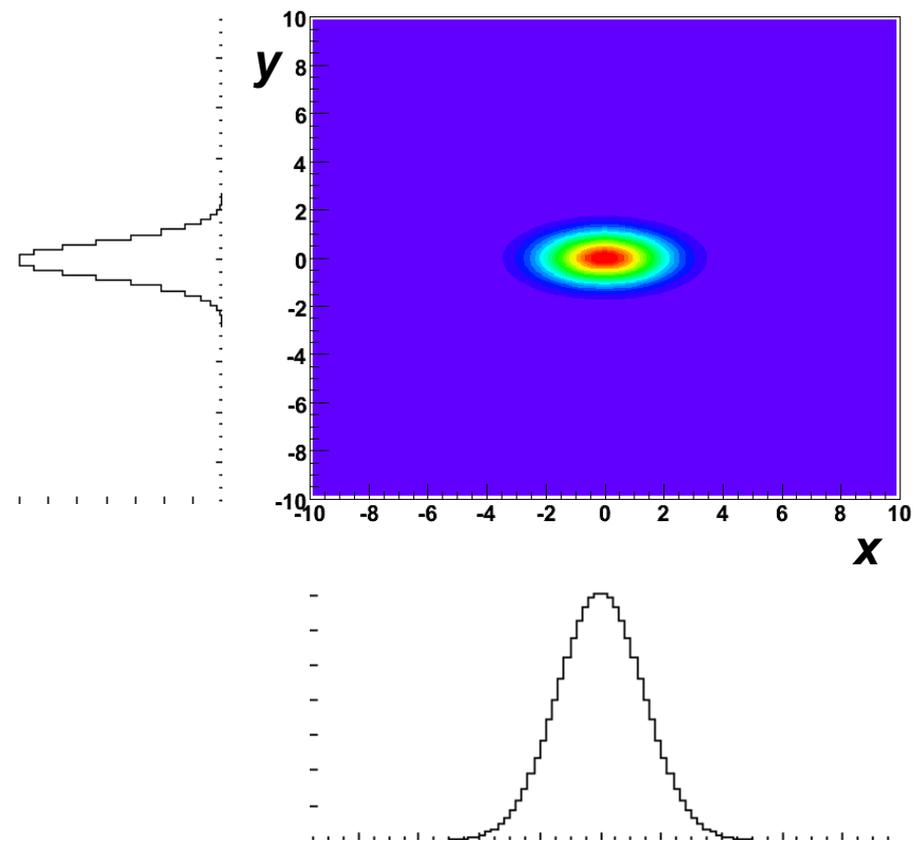
$$\left\{ \begin{array}{l} Prof_H(x) = \frac{N_0}{\sqrt{2\pi}\sigma_x} e^{-\frac{x^2}{2\sigma_x^2}} \\ Prof_V(y) = \frac{N_0}{\sqrt{2\pi}\sigma_y} e^{-\frac{y^2}{2\sigma_y^2}} \end{array} \right.$$

Beam Profiles (3)

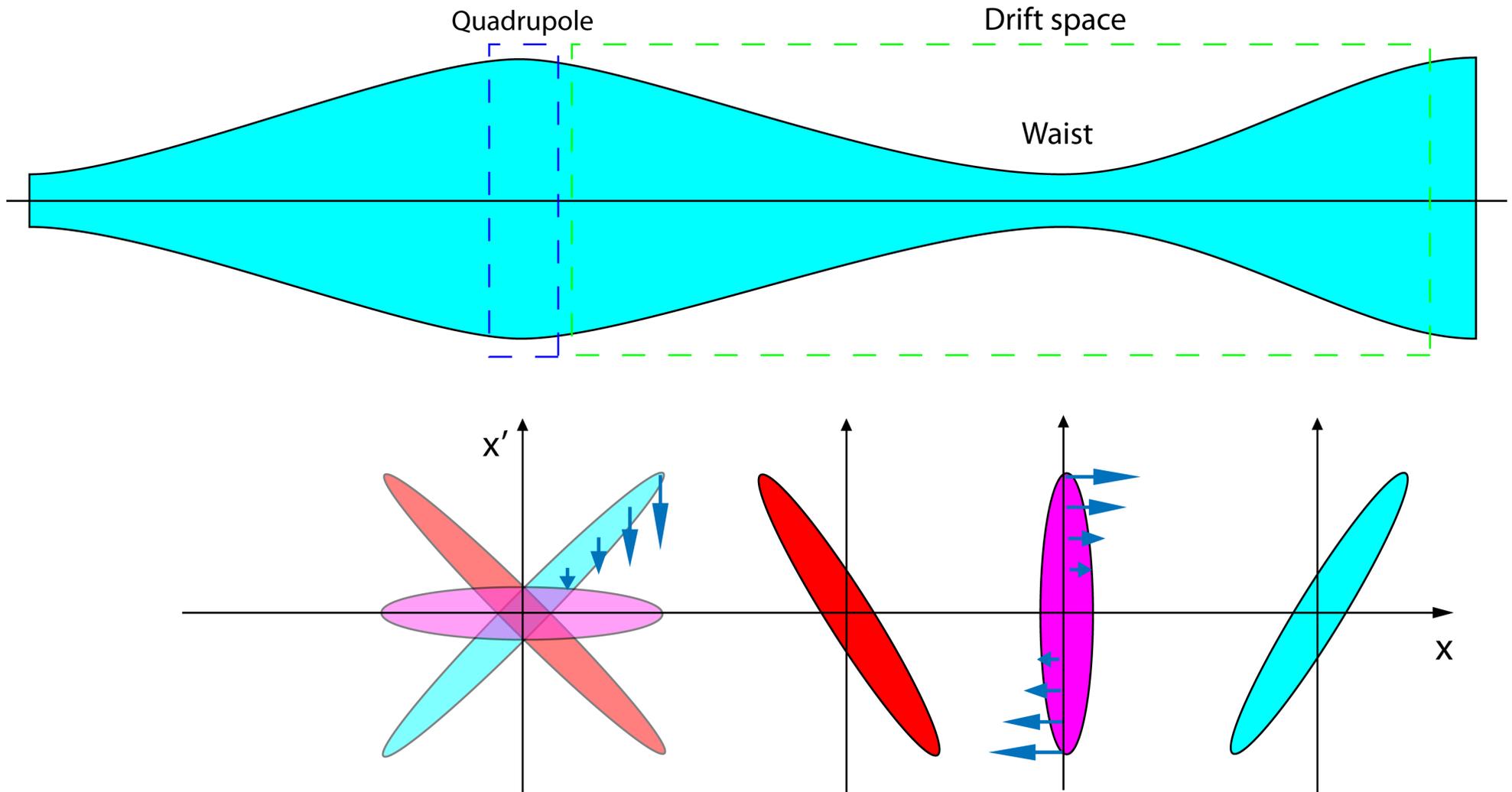
Particles Distribution



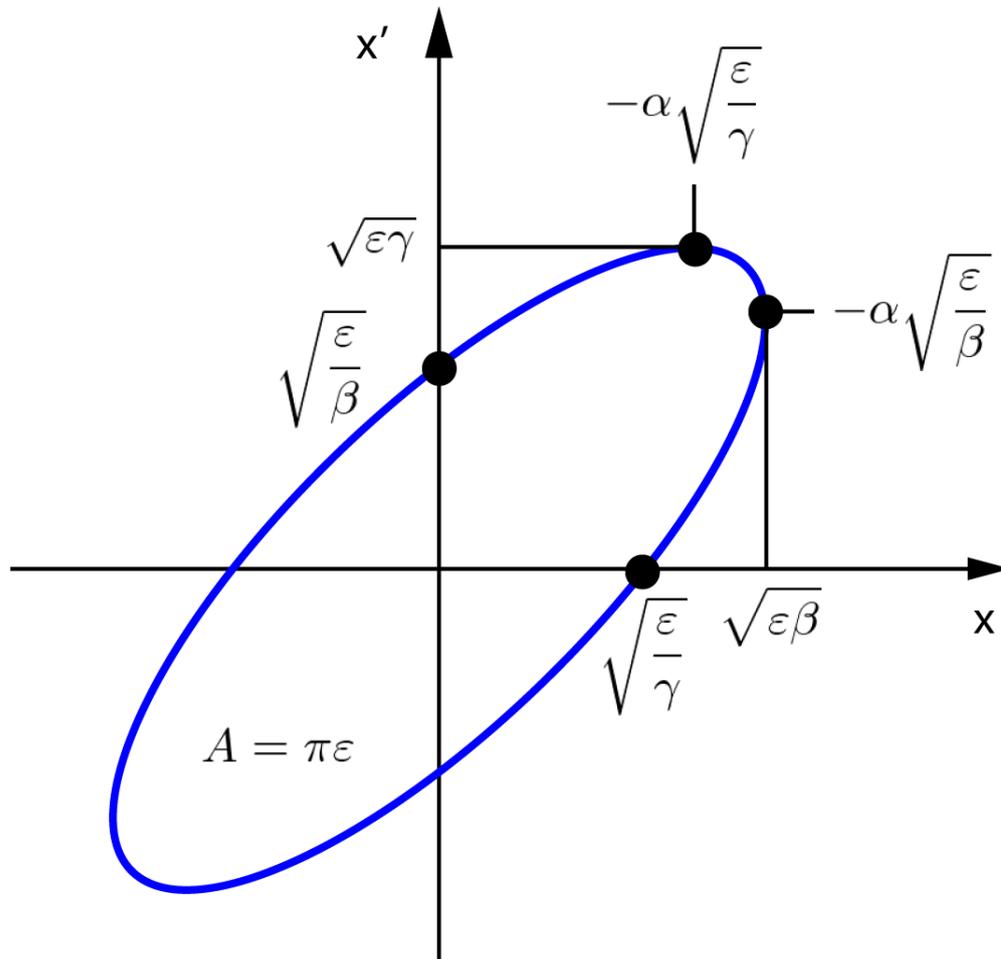
Profiles



Phase space dynamics



Courant-Snyder parameters



The phase space ellipse can be defined by 4 parameters: ε , β , α and γ , with the relation

$$\gamma = \frac{1 + \alpha^2}{\beta}$$

The equation of the ellipse is

$$\varepsilon = \gamma x^2 + 2\alpha x x' + \beta x'^2$$

Particles transport

In a linear system, like a system composed of drift space and quadrupoles, the coordinates of a particle in phase space can be transported using a simple matrix notation

$$\begin{bmatrix} x_1 \\ x_1' \end{bmatrix} = M_1 \begin{bmatrix} x_0 \\ x_0' \end{bmatrix} \quad \begin{bmatrix} x_2 \\ x_2' \end{bmatrix} = M_2 \begin{bmatrix} x_1 \\ x_1' \end{bmatrix} \quad \begin{bmatrix} x_3 \\ x_3' \end{bmatrix} = M_3 \begin{bmatrix} x_2 \\ x_2' \end{bmatrix}$$

$$\begin{bmatrix} x_3 \\ x_3' \end{bmatrix} = M_3 M_2 M_1 \begin{bmatrix} x_0 \\ x_0' \end{bmatrix} = M_{0 \Rightarrow 3} \begin{bmatrix} x_0 \\ x_0' \end{bmatrix}$$

$$M_{Drift} = \begin{bmatrix} 1 & L \\ 0 & 1 \end{bmatrix}$$

$$M_{Quad} = \begin{bmatrix} \cos(\sqrt{k} L_Q) & 1/\sqrt{k} \sin(\sqrt{k} L_Q) \\ -\sqrt{k} \sin(\sqrt{k} L_Q) & \cos(\sqrt{k} L_Q) \end{bmatrix}$$

Twiss parameters transport

If one can transport each point of the phase space one can also transport the ellipse and thus the Courant-Snyder, a.k.a. Twiss, parameters

$$\begin{bmatrix} x_1 \\ x_1' \end{bmatrix} = \begin{bmatrix} c & s \\ c' & s' \end{bmatrix} \begin{bmatrix} x_0 \\ x_0' \end{bmatrix} \quad \Rightarrow \quad \begin{bmatrix} \beta_1 \\ \alpha_1 \\ \gamma_1 \end{bmatrix} = \begin{bmatrix} c^2 & 2cs & s^2 \\ -cc' & cs' + c's & -ss' \\ c'^2 & -2c's' & s'^2 \end{bmatrix} \begin{bmatrix} \beta_0 \\ \alpha_0 \\ \gamma_0 \end{bmatrix}$$

From the measurement of the beam profiles one obtains $\sigma^2 = \varepsilon \beta$

$$\beta_1 = \begin{bmatrix} c_1^2 & 2c_1s_1 & s_1^2 \end{bmatrix} \begin{bmatrix} \beta_0 \\ \alpha_0 \\ \gamma_0 \end{bmatrix} \quad \begin{bmatrix} \varepsilon \beta_1 \\ \varepsilon \beta_2 \\ \varepsilon \beta_3 \end{bmatrix} = \varepsilon \begin{bmatrix} c_1^2 & 2c_1s_1 & s_1^2 \\ c_2^2 & 2c_2s_2 & s_2^2 \\ c_3^2 & 2c_3s_3 & s_3^2 \end{bmatrix} \begin{bmatrix} \beta_0 \\ \alpha_0 \\ \gamma_0 \end{bmatrix}$$

Twiss parameters measurement

$$\begin{bmatrix} \varepsilon \beta_1 \\ \varepsilon \beta_2 \\ \varepsilon \beta_3 \end{bmatrix} = \varepsilon M \begin{bmatrix} \beta_0 \\ \alpha_0 \\ \gamma_0 \end{bmatrix} \quad \Rightarrow \quad M^{-1} \begin{bmatrix} \varepsilon \beta_1 \\ \varepsilon \beta_2 \\ \varepsilon \beta_3 \end{bmatrix} = \begin{bmatrix} a \\ b \\ c \end{bmatrix} = \varepsilon \begin{bmatrix} \beta_0 \\ \alpha_0 \\ \gamma_0 \end{bmatrix}$$

$$\begin{cases} a = \varepsilon \beta_0 \\ b = \varepsilon \alpha_0 \\ c = \varepsilon \gamma_0 \\ \gamma_0 = \frac{1 + \alpha_0^2}{\beta_0} \end{cases} \quad \Rightarrow \quad \begin{cases} \beta_0 = \frac{a}{\sqrt{ac - b^2}} \\ \alpha_0 = \frac{b}{\sqrt{ac - b^2}} \\ \gamma_0 = \frac{c}{\sqrt{ac - b^2}} \\ \varepsilon = \sqrt{ac - b^2} \end{cases}$$

Sampling of distributions

- Intercepting methods
 - Scanning wires
 - Wire grids (Harps)
 - Radiative screens
- Non intercepting methods
 - Synchrotron light
 - Rest gas ionization
 - (Inverse Compton scattering / photo dissociation)

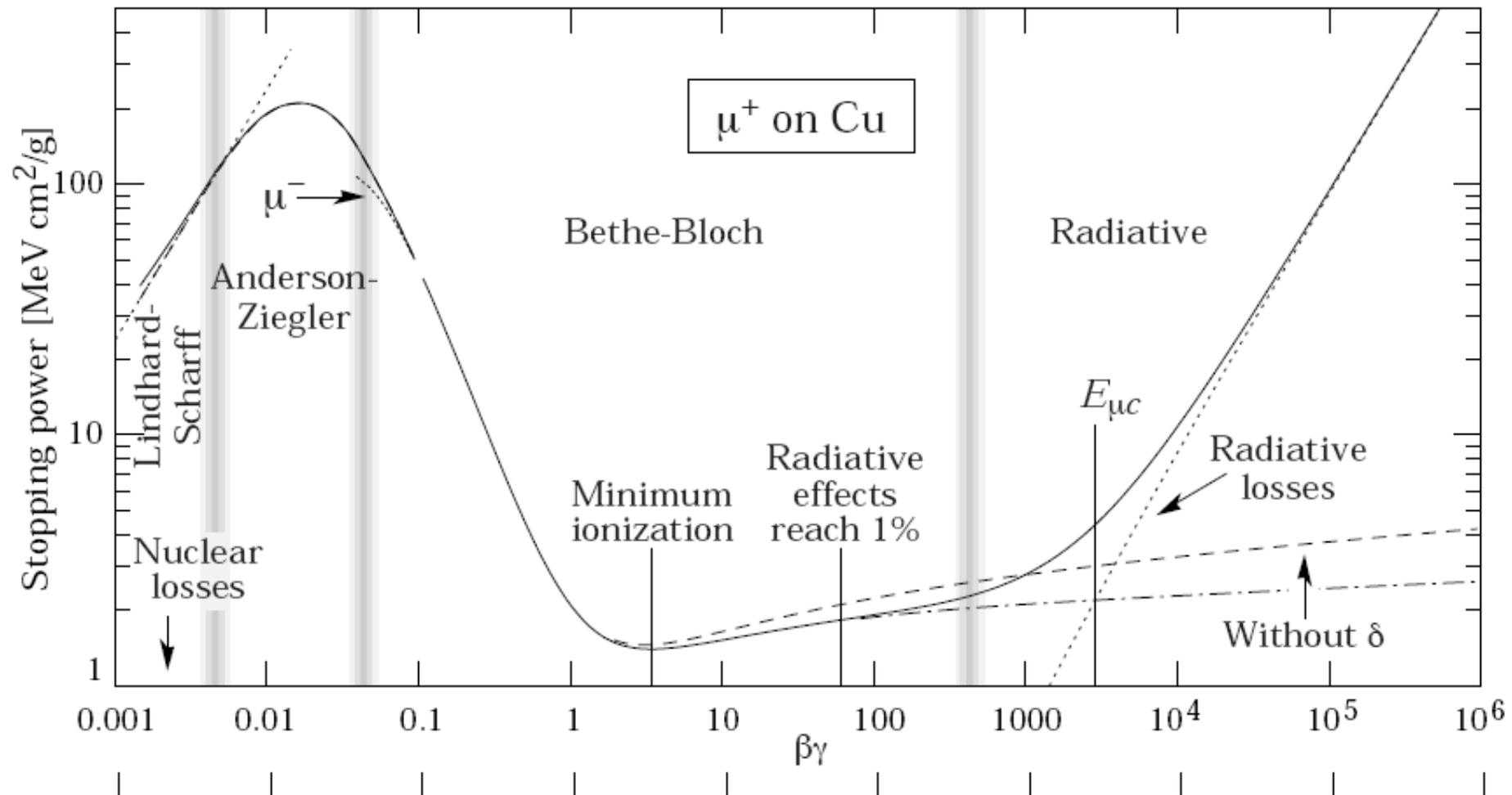
Interaction of particles with matter

- Ionization
 - Creation of electrons/ions pairs
 - Secondary electrons emission (low energy electrons)
 - Emission of photons (decay of excited states)
- Elastic and inelastic scattering
 - Dislocations
 - Production of secondary particles (high energy particles)
- Čerenkov radiation
- Bremsstrahlung
- Optical transition radiation

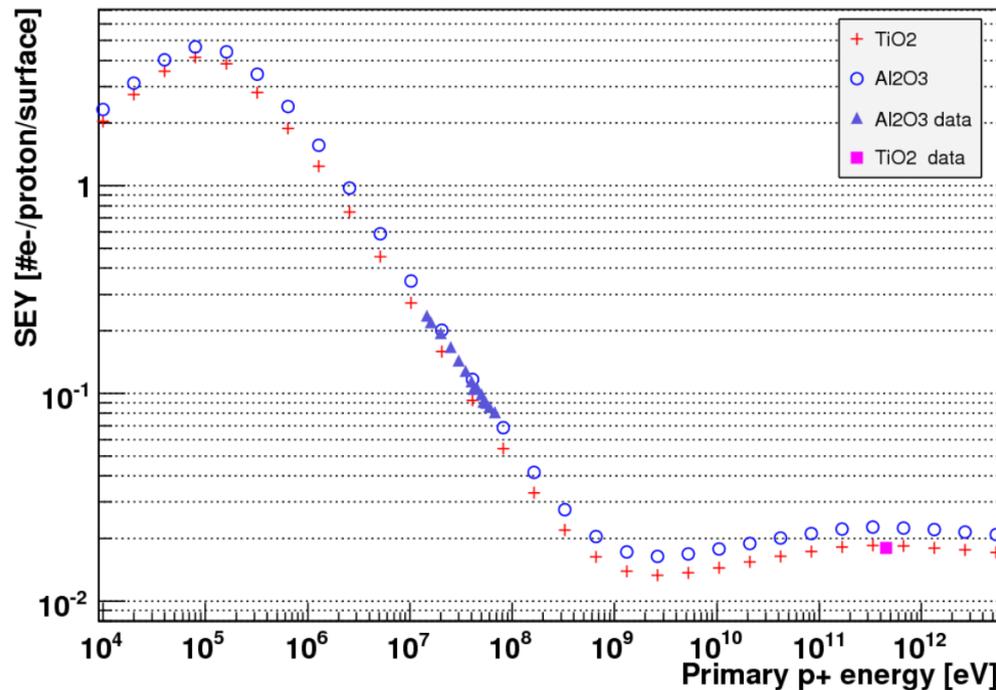
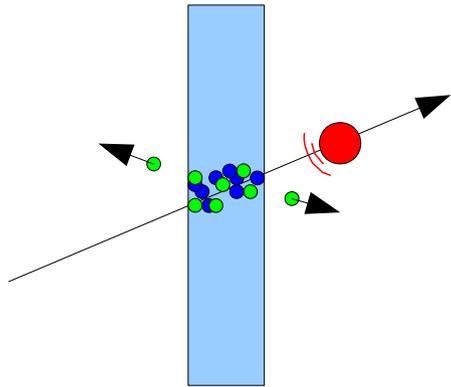
Energy deposition

- Energy deposition is probably the most important aspect for all intercepting devices
 - Signals are often proportional to the deposited energy
 - Energy deposition can cause damage to the instrument
- The Bethe-Bloch formula describes energy losses in most cases
- The energy lost by the particles is not necessarily deposited in the sensor

Energy deposition - dE/dx

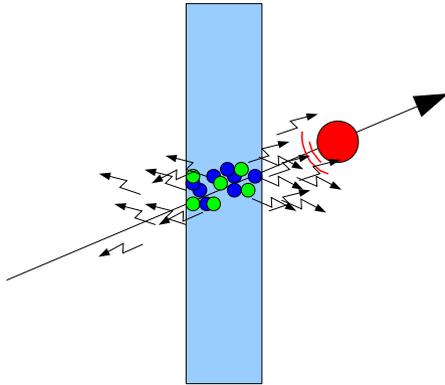


Secondary emission - SEM



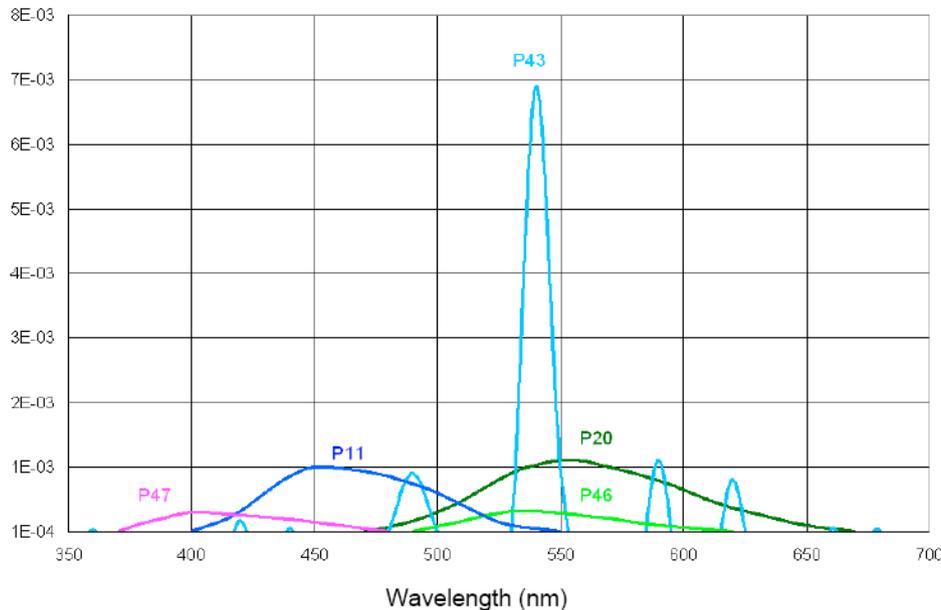
- Linked to ionization
- Surface electrons receive sufficient energy to travel to the surface and leave
- Emission yield depends on particles energy, material, surface state etc.

Scintillation



- Linked to ionization
- Photons are emitted by the de-excitation of atomic states populated by the passage of the particle
- Emission time *ns* to *hours*

Energy Conversion ((W/nm)/W)



Type	Composition	Decay Time	
		Decay of Light Intensity	
		from 90 % to 10 % in	from 10 % to 1 % in
P 43	Gd ₂ O ₂ S:Tb	1 ms	1,6 ms
P 46	Y ₃ Al ₅ O ₁₂ :Ce	300 ns	90 μs
P 47	Y ₂ SiO ₅ :Ce,Tb	100 ns	2,9 μs
P 20	(Zn,Cd)S:Ag	4 ms	55 ms
P 11	ZnS:Ag	3 ms	37 ms

1MeV *e*⁻ on 5μm P43 yields ~ 60 ph.

Scintillation (2)

- Phosphors have very high light yields, but can only be used as thin coating on a rigid support and get damaged very quickly
- Normally used only for very low intensity beams
- Ceramics, glasses and crystals are a more popular choice in high energy accelerators
- Al_2O_3 (Alumina, Aluminium Oxide) is a very common choice (eventually doped with Cr) because it is a very robust ceramic

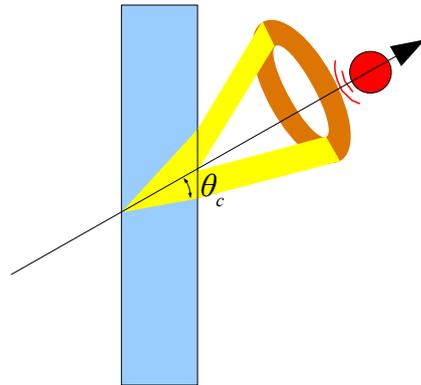
Čerenkov radiation

Index of refraction
 $n = n(\omega)$

Velocity of particle
 $v = \beta c$

Čerenkov angle

$$\cos \theta_c = \frac{1}{n(\omega) \beta}$$



Velocity Threshold

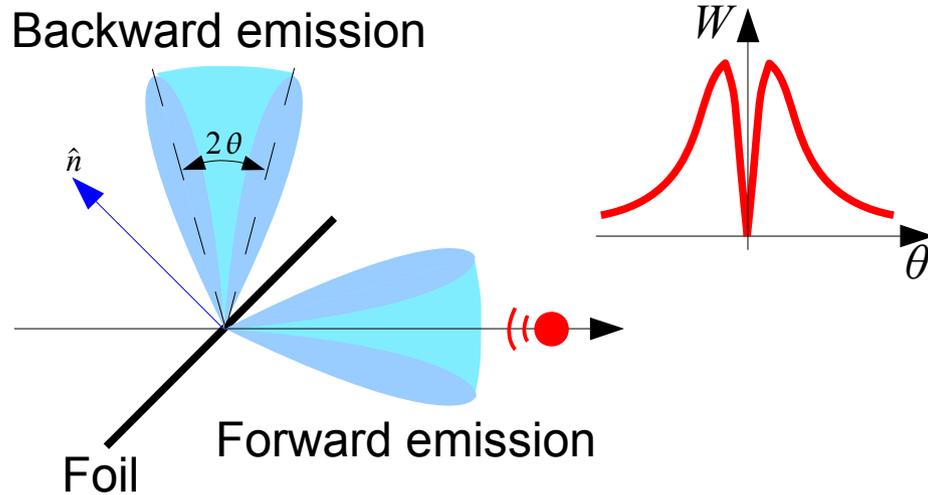
$$\beta_t = \frac{1}{n(\omega)}$$

- Linked to the polarization of the atoms in the material
- Threshold effect: particle travels faster than phase velocity of light in material
- Radiation has defined angular distribution
- Not very good resolution in imaging

$$\frac{d^2 N}{dx d\omega} = \frac{\alpha z^2}{c} \sin^2 \theta_c(\omega) = \frac{\alpha z^2}{c} \left(1 - \frac{1}{\beta^2 n^2(\omega)} \right)$$

For $\theta_c = 45^\circ$ (quartz at $\beta \approx 1$), $\lambda \in [400, 500] \text{ nm}$ and $\delta x = 1 \text{ mm} \rightarrow N \sim 10$ photons

Optical Transition Radiation (OTR)



- Radiation is emitted when a charged particle crosses the boundary of different dielectric properties
- Radiation has defined angular distribution
- Radiation is radially polarized
- Thickness of radiator not important

$$\frac{d^2 W}{d \Omega d \omega} \approx \frac{N q^2}{\pi^2 c} \left(\frac{\theta}{\gamma^{-2} + \theta^2} \right)^2$$

Maximum at $\theta = \frac{1}{\gamma}$

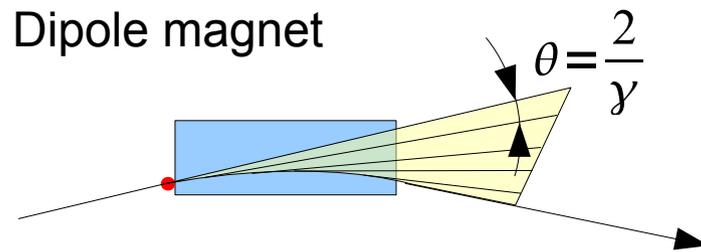
$$W \propto \left\{ \begin{array}{ll} \beta^2 & \beta \ll 1 \\ \ln(2\gamma) & \gamma \gg 1 \end{array} \right\}$$

For 50 MeV electrons ~ 0.3 ph./el.

For 100 keV electrons ~ 0.001 ph./el.

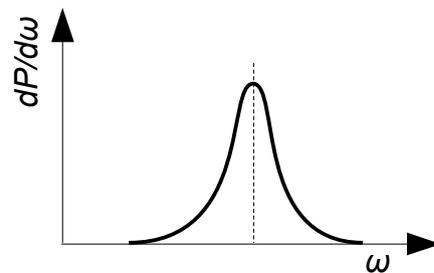
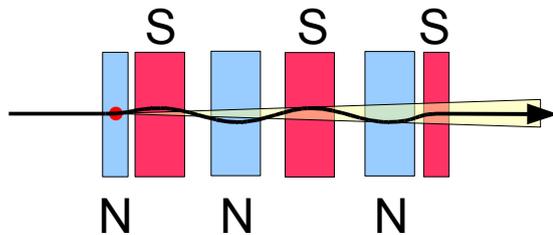
($\lambda \in [400, 600]$ nm)

Synchrotron radiation



$$P = \frac{1}{4\pi\epsilon_0} \frac{2}{3} \frac{ce^2\gamma^4}{\rho^2}$$

Wiggler / Undulator

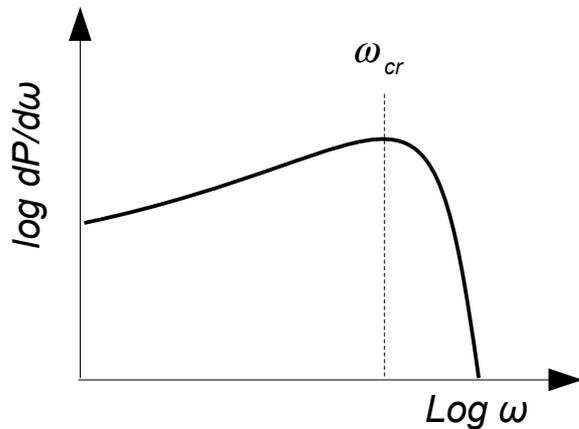


$$\lambda \propto \frac{\lambda_u}{2\gamma^2}$$

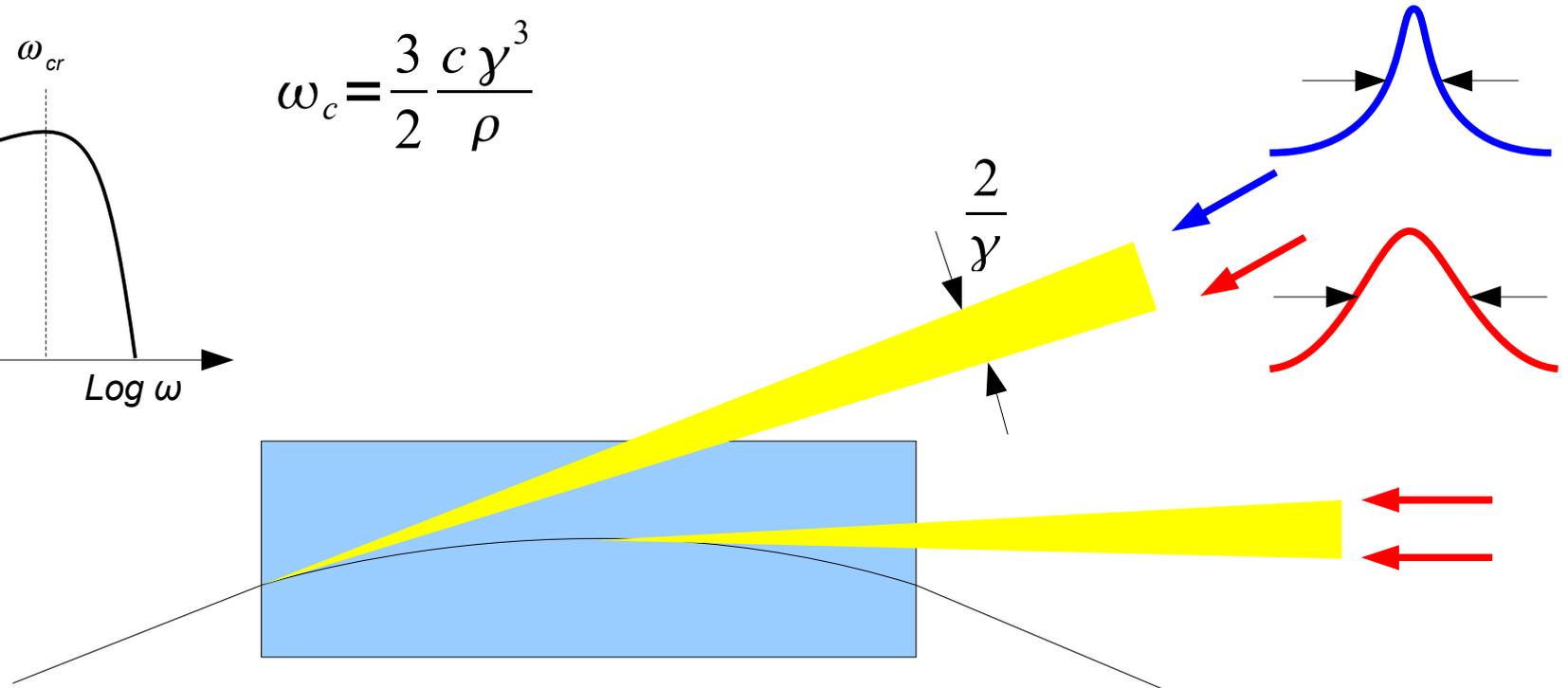
$$W \propto B_0^2 \gamma^2$$

- Charged particles emit electromagnetic radiation when accelerated
 - Bremsstrahlung: reduction of velocity
 - Synchrotron radiation: change of direction
- Synch. rad. from dipole magnet emits in a fan
- Radiation from undulator has different properties

Synchrotron radiation (2)



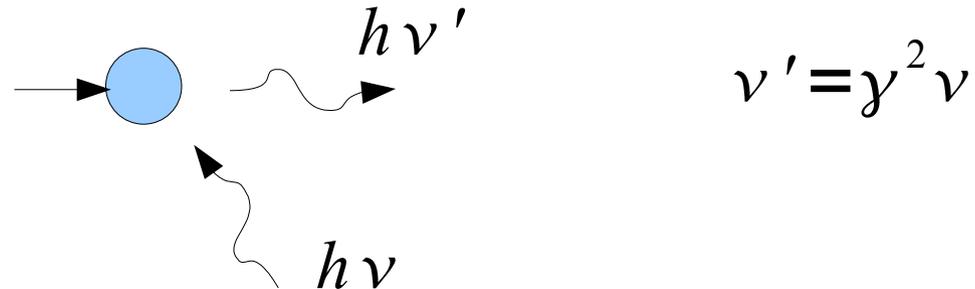
$$\omega_c = \frac{3}{2} \frac{c \gamma^3}{\rho}$$



The red observers will see a pulse which duration is equal to the time it takes to the particle to be deviated by an angle $2/\gamma$ and an emission spectrum as the one depicted above.

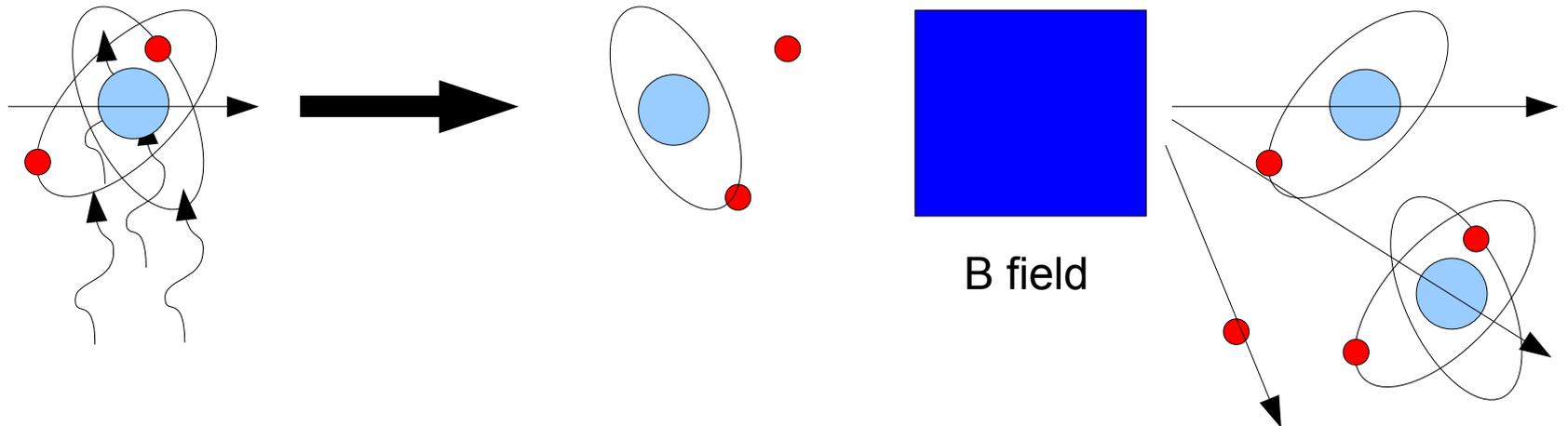
The blue observer being at the edge of the emission cone will see a shorter pulse. As a consequence the spectrum of the emission will be broadened and extend to higher frequencies (shorter wavelengths)

(Inverse) Compton scattering



- A low energy photon (few eV) interacts with a high energy charged lepton (e^- , e^+)
- The photon gets boosted and gains energy to the expense of the particles
- Cross section is small, but usable for leptons, it is however too small for hadrons (protons)

Photo dissociation (H^- beams)



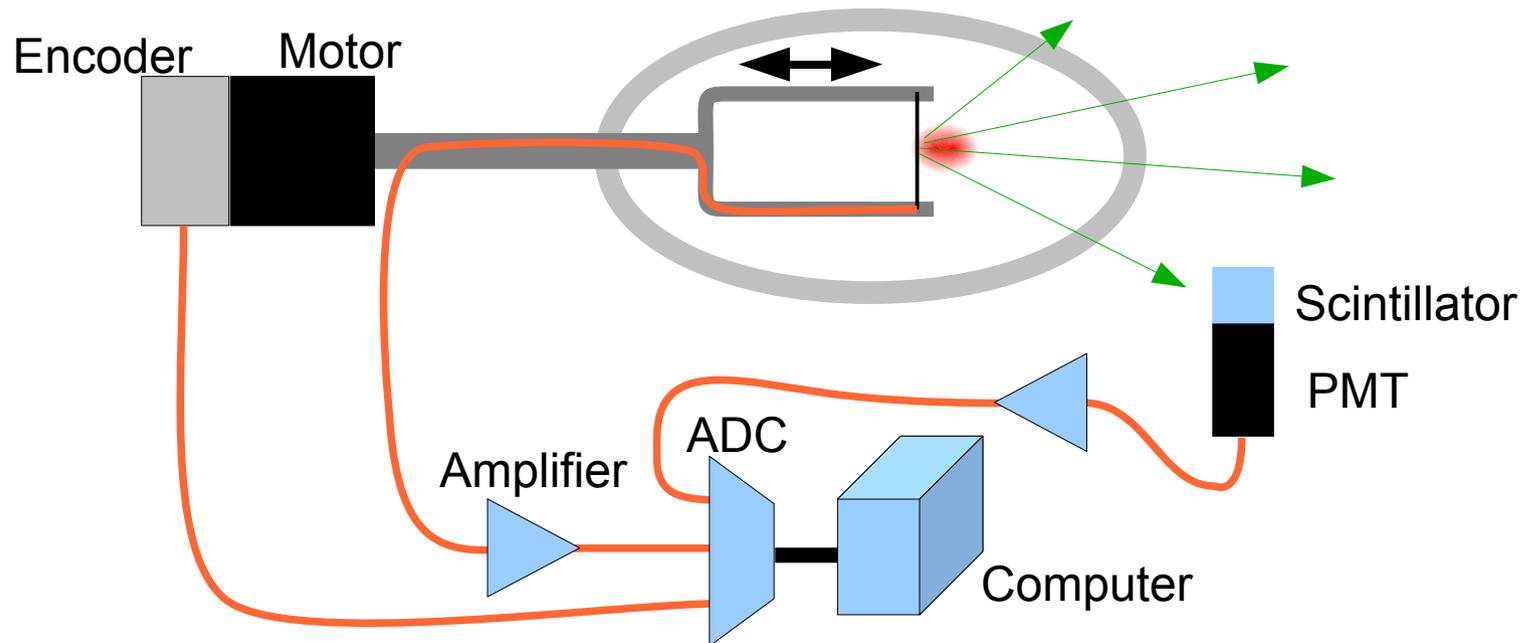
- Photons from a laser are used to separate one electron from the H^- ion. This can be facilitated by external electric or magnetic fields
- Some of the ions will lose the extra electron and become neutral H_0
- The different particles can be separated by a bending magnet

Sampling particle distributions

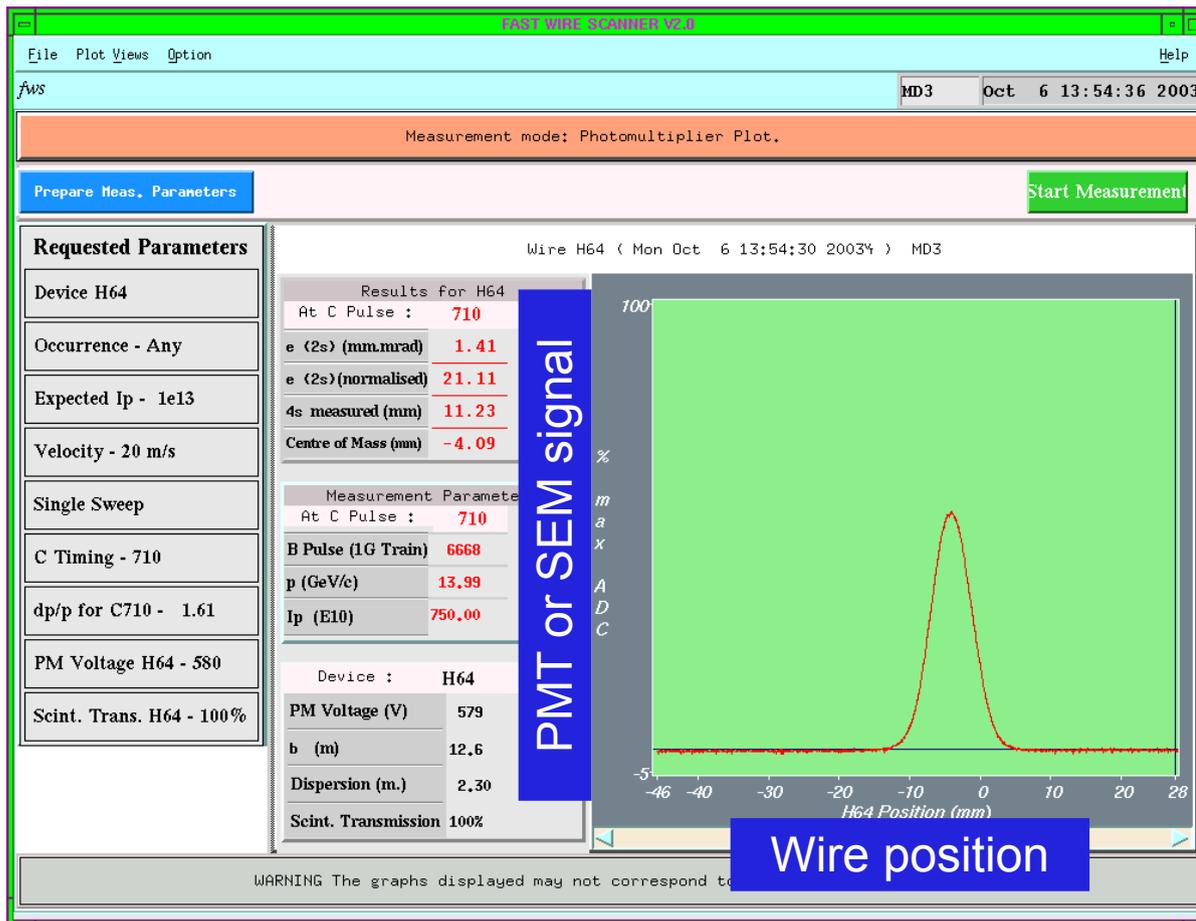
- One dimension sampling
 - Wire scanners
 - Wire grids
 - Rest gas ionization monitors
 - Laser Wire Scanner
- Two dimension sampling
 - Screens and radiators
 - Synchrotron radiation

Wire scanner

- Scans a thin wire or a needle across the beam
- Detects secondary emission current or high energy secondary particles (scintillator + PMT)



Wire scanner (2)

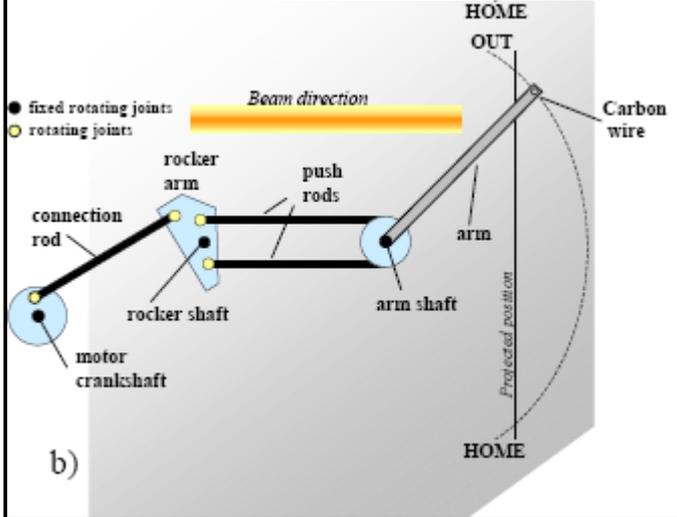
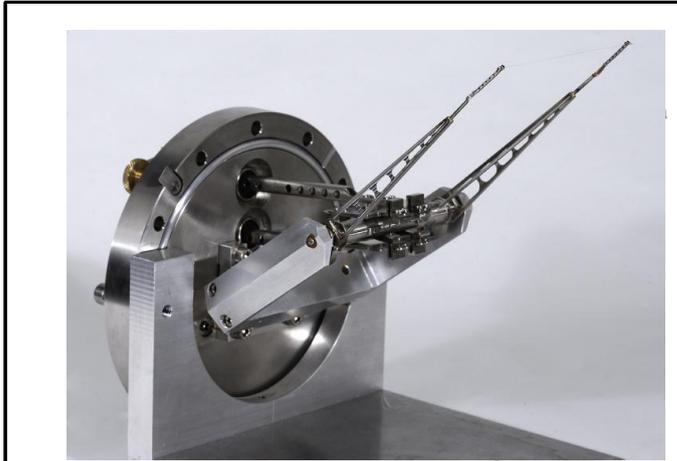


- The position of the wire is read by resolver or an encoder and sampled simultaneously with the signal
- On complex, fast mechanism the error on the position can be the largest contribution, need calibration

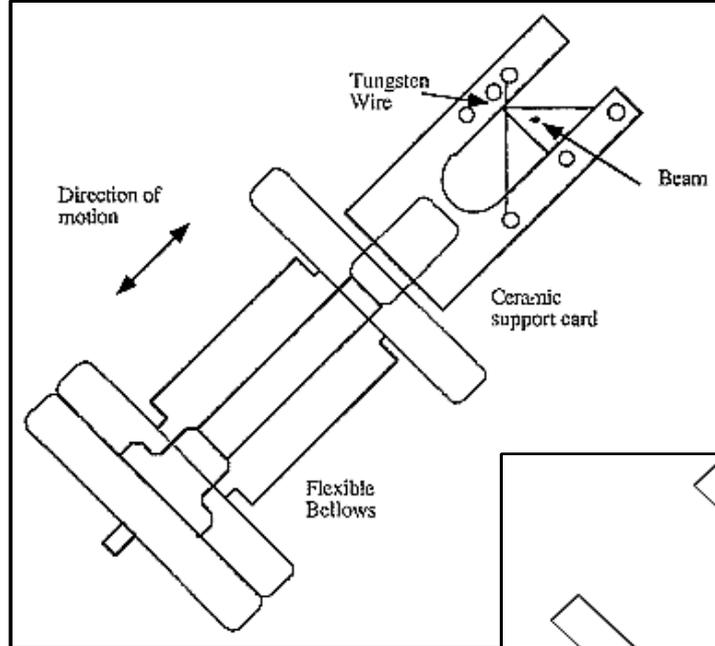
Wire scanner (3)

- Secondary emission
 - Good for low energy beams (no high energy secondary)
 - Small signal
 - If the wire becomes too hot it can start to emit thermionic electrons spoiling the measurement
- High energy secondary
 - No problem with wire heating (well...)
 - Strong signal
 - Detection may be non homogeneous leading to distorted profiles

Wire scanner (4)

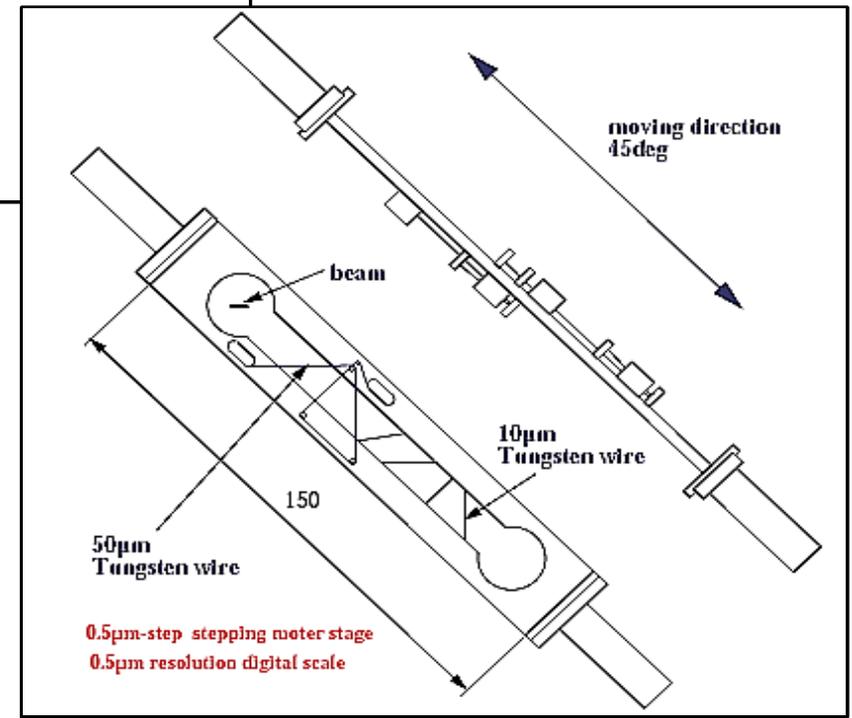


CERN "flying wires"

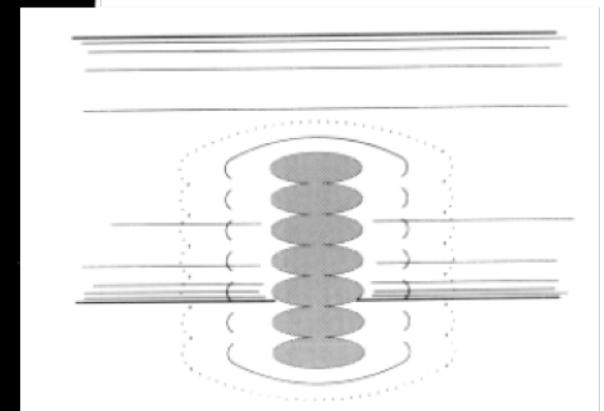
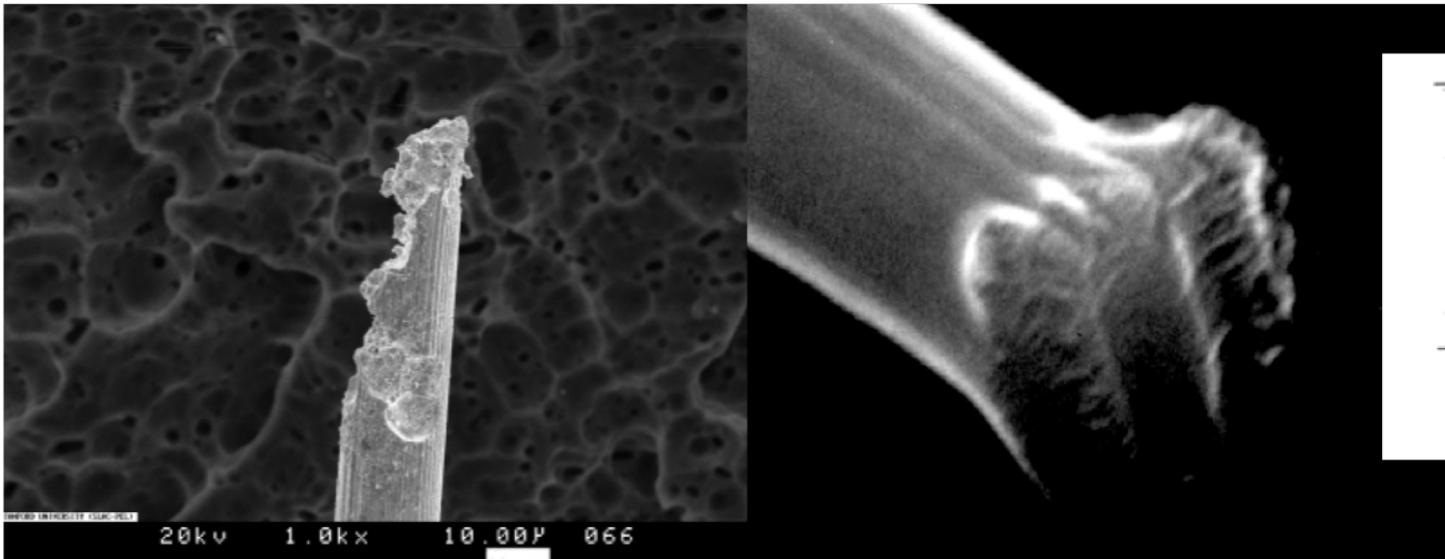
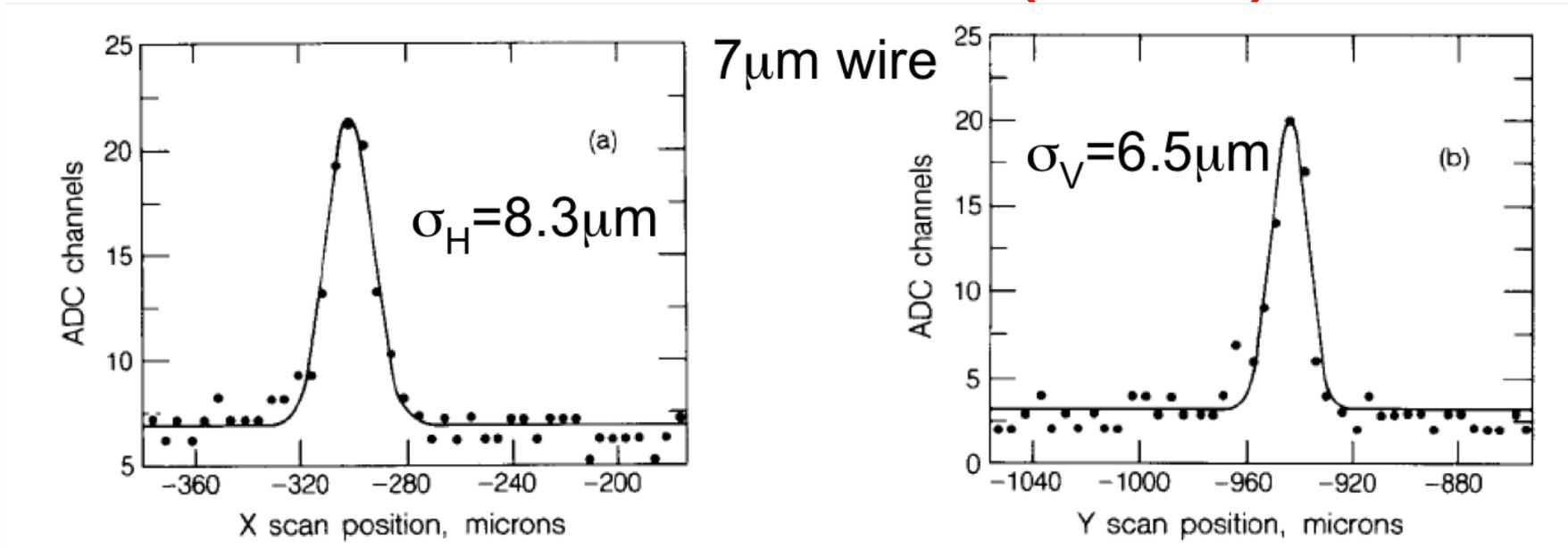


KEK ATF high resolution 3 axis scanners

SLAC SLC high resolution 3 axis scanners



Wire Scanner (SLC)

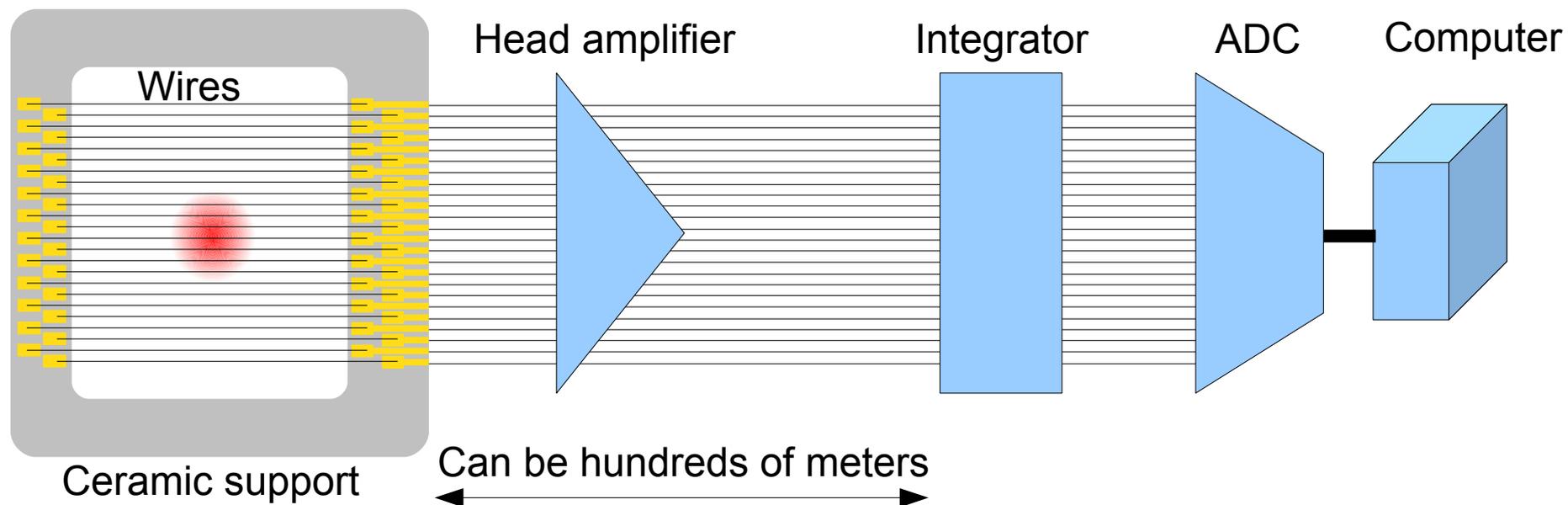


Wire scanner (5)

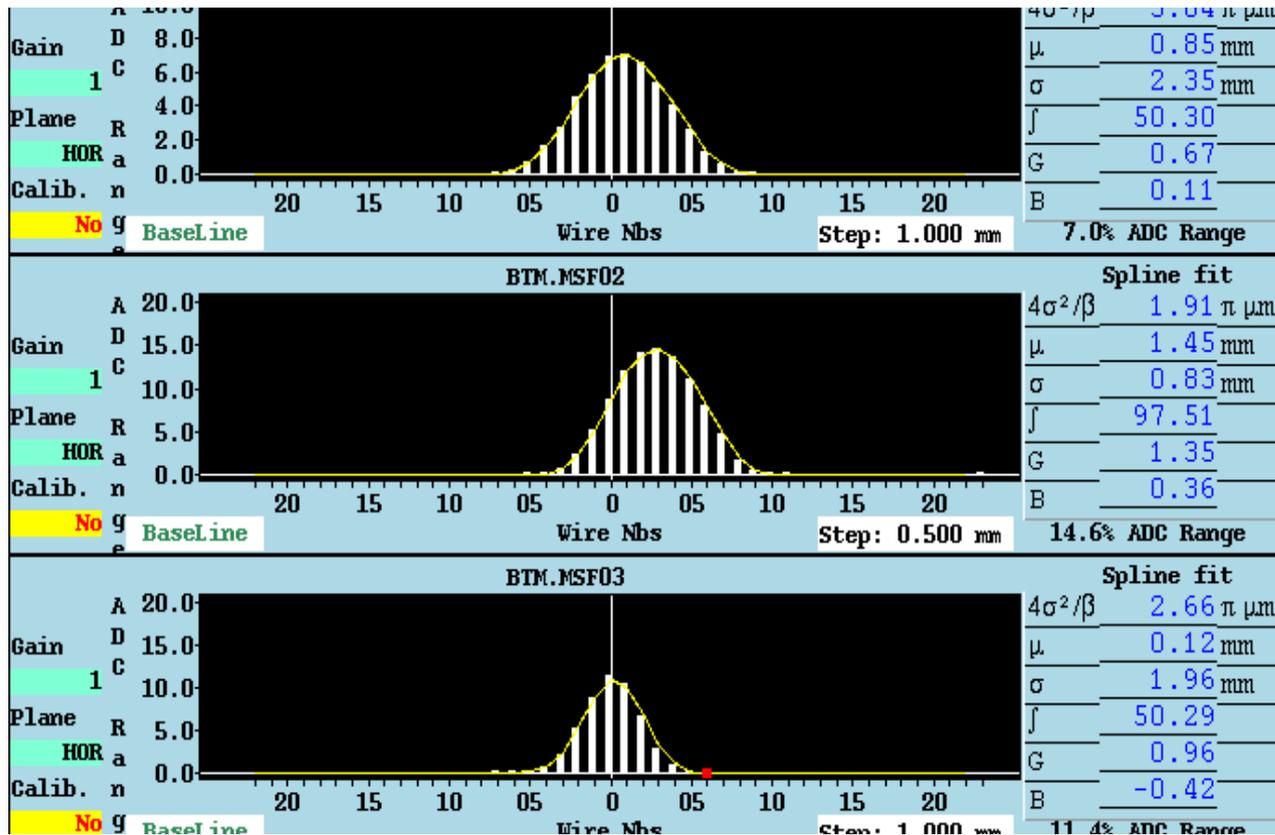
- Fast scanners
 - Present limit is around 20 m/s
 - Usually rotational mechanism
 - Acquire profile snapshots during acceleration without need of plateaus
 - Reduce wire heating (short scan time)
- Slow scanners
 - High wire position accuracy
 - Possibly thinner wires (low accelerations)
 - More reliable mechanisms
 - Long(er) measurement time
 - Tighter intensity limits

SEM Grids (Harps)

- The SEM current from each wire or strip is acquired independently
- Complex (=expensive) cabling/electronics
- Wire spacing down to a few hundreds microns

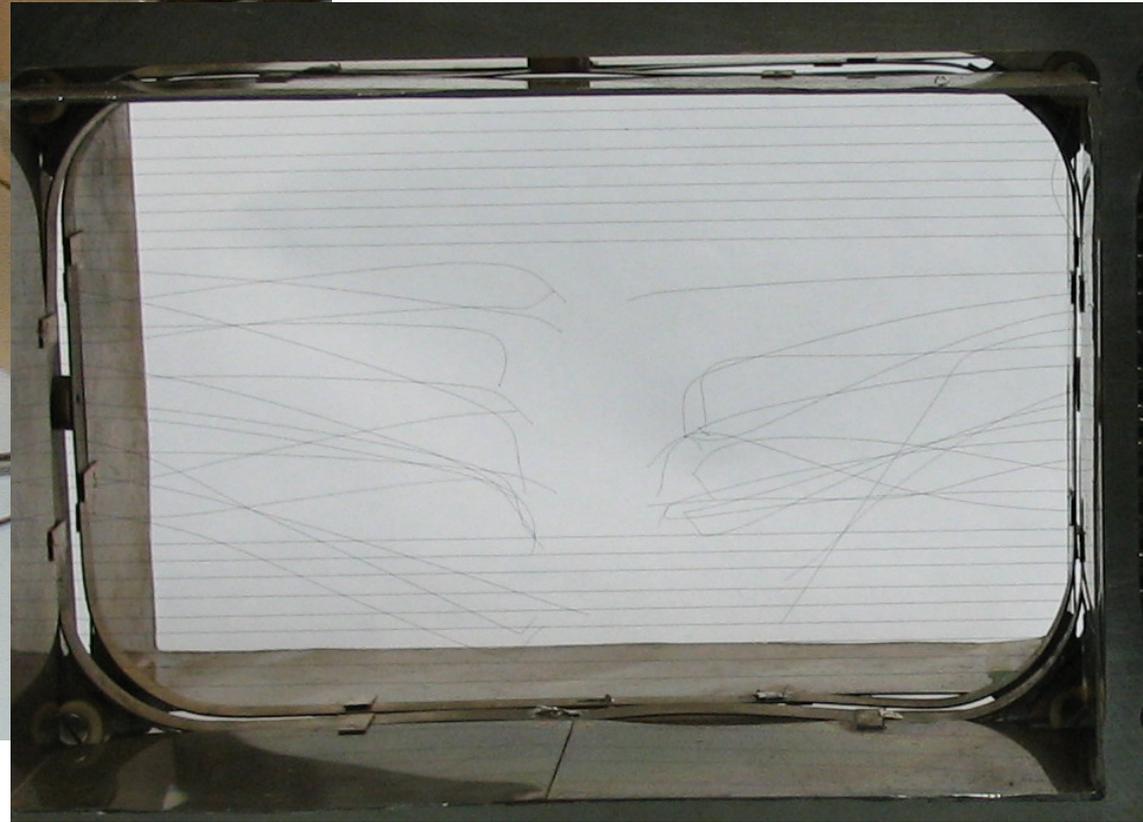
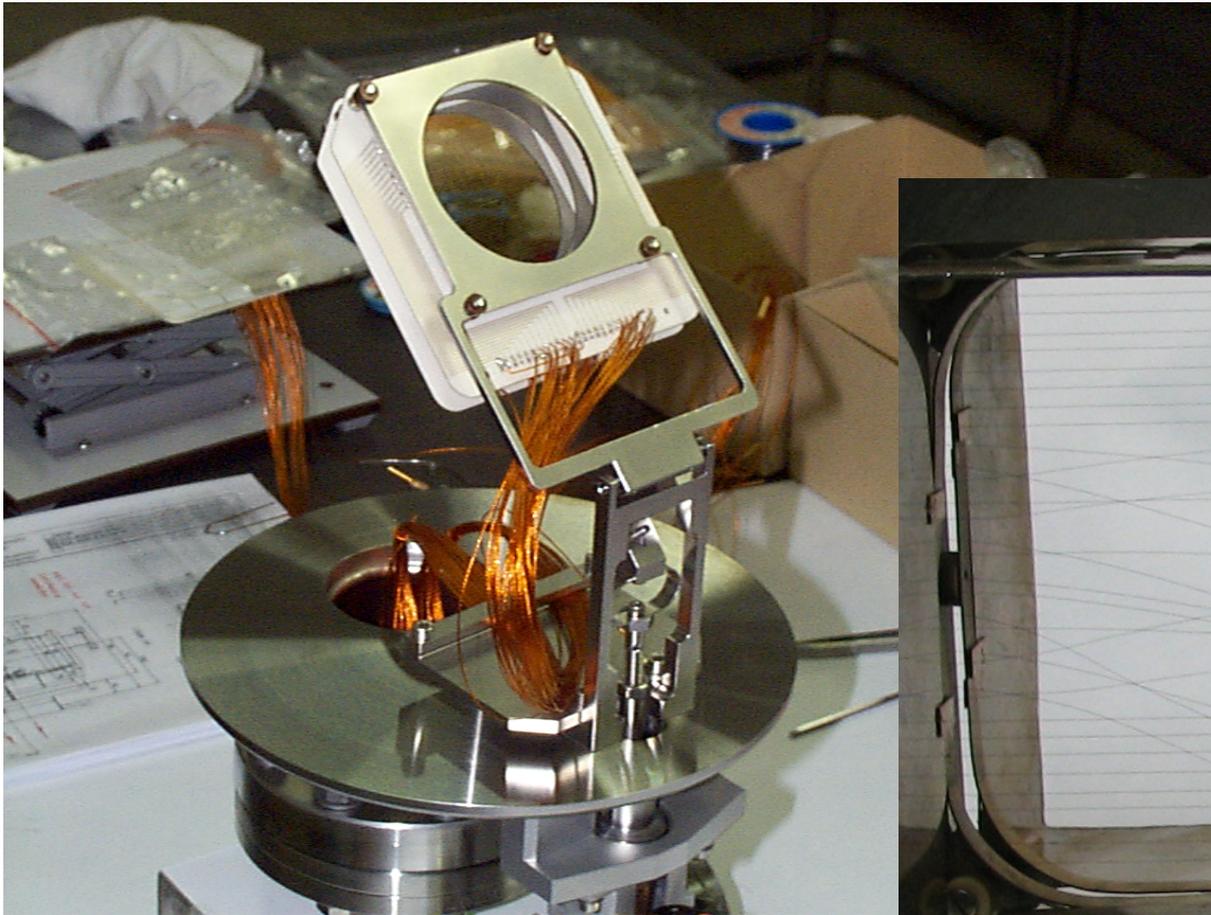


SEM Grids (2)

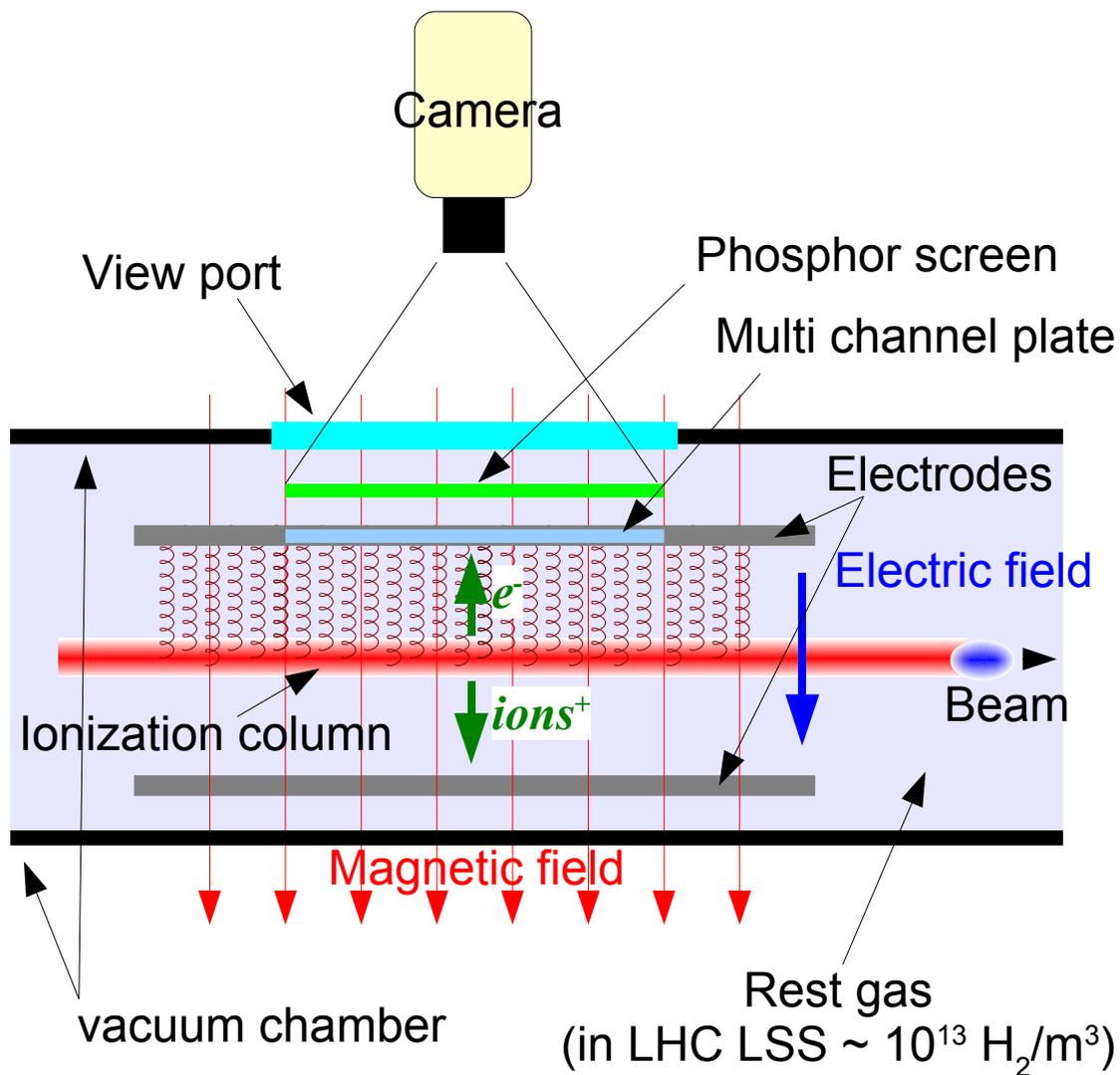


- Advantage of Grids is single shot measurement
- Time resolved measurement is possible (up to ~100 MHz)
- Damage to a single wire can make device unusable

SEM Grids (3)

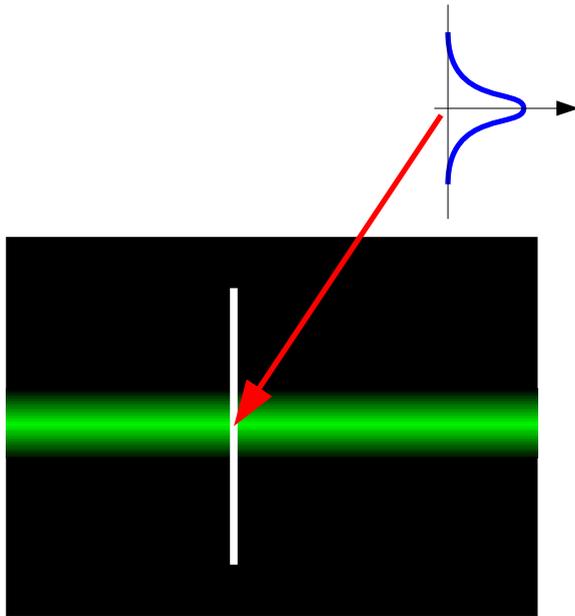


Ionization profile monitor



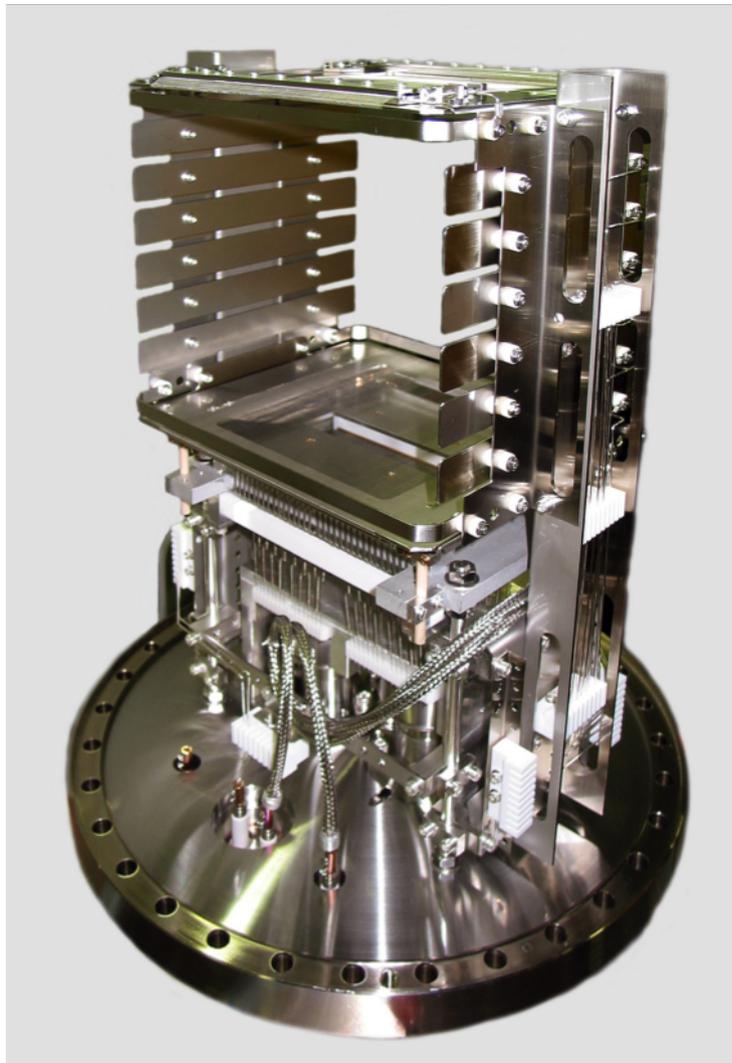
- Beam creates ionization column in rest gas
- Electric field drifts electrons toward detector
- Magnetic field guides the electron
- MCP+phosphor+CCD detects electrons
- If E is reversed ions can be detected instead of electrons (less need for B field)

Ionization profile monitor (2)

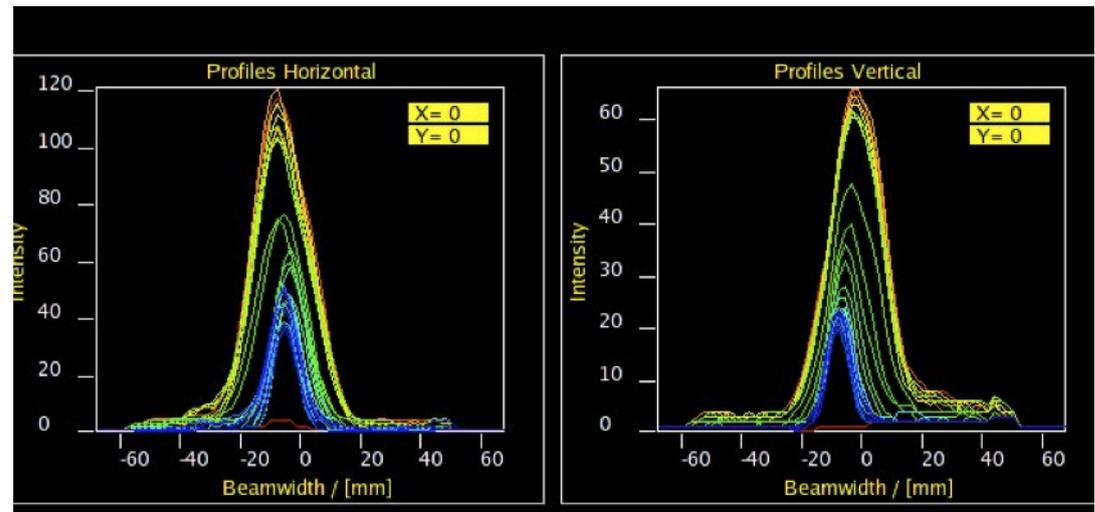


- Image shows a stripe
- Intensity profile of stripe proportional to beam profile
- Detector measures only one plane
- Transverse drift of electrons introduces broadening (need intense B field) and creates “tails”

IPM (GSI)

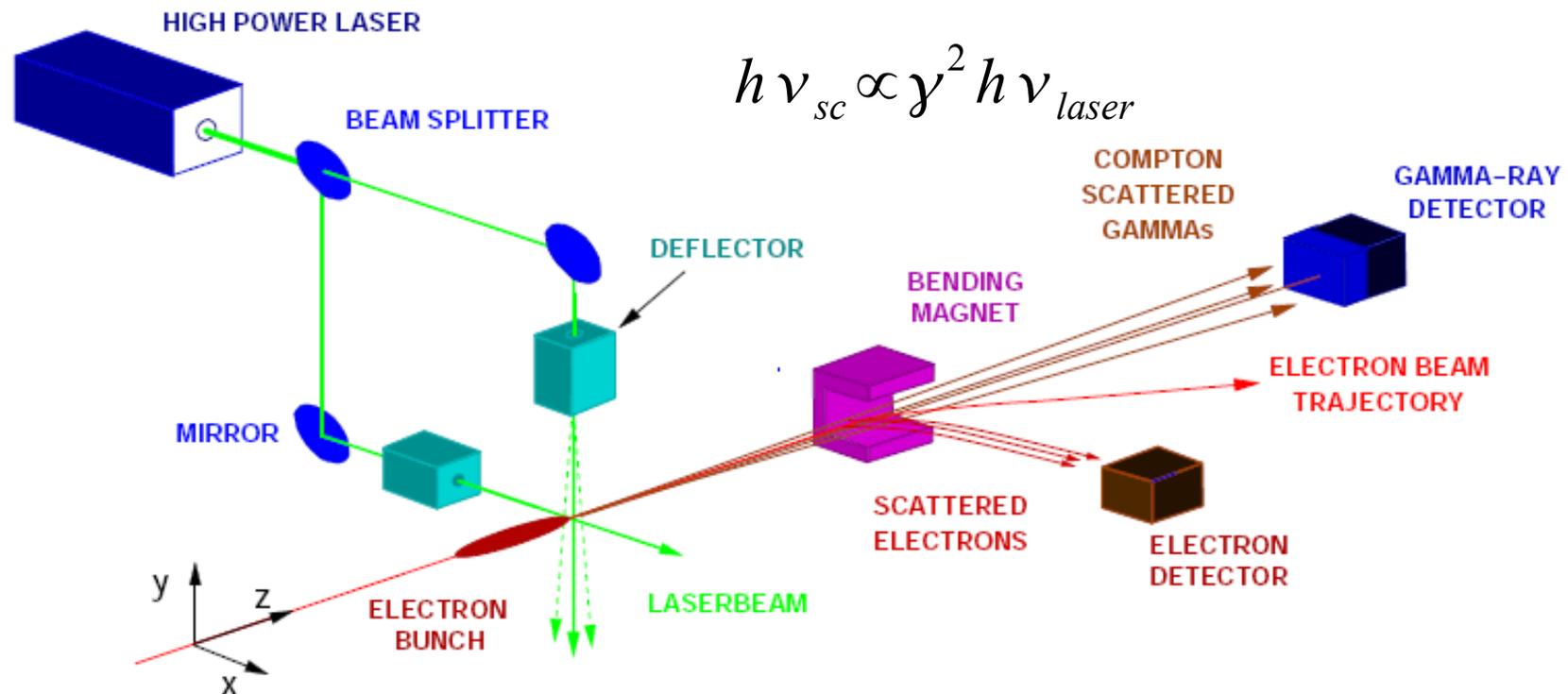


- IPMs allow the continuous monitoring of the transverse plane
- Needs a “minimum” of rest gas

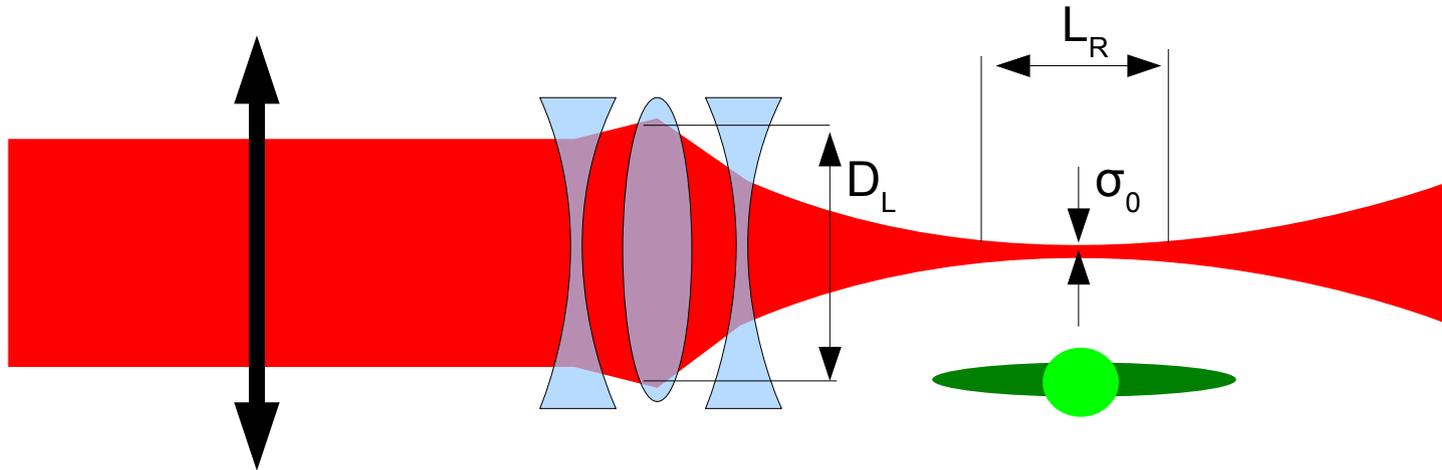


Laser Wire Scanner

- Collide a high power, focused, pulsed laser with an electron beam
- X-ray or γ -ray are produced by Inverse Compton Scattering
- Detect the x-ray / γ -ray or the degraded electrons downstream
- Can also be used on H^- beams exploiting the photo neutralization detecting either the neutral H atoms or the freed electrons



Laser Wire Scanner (2)

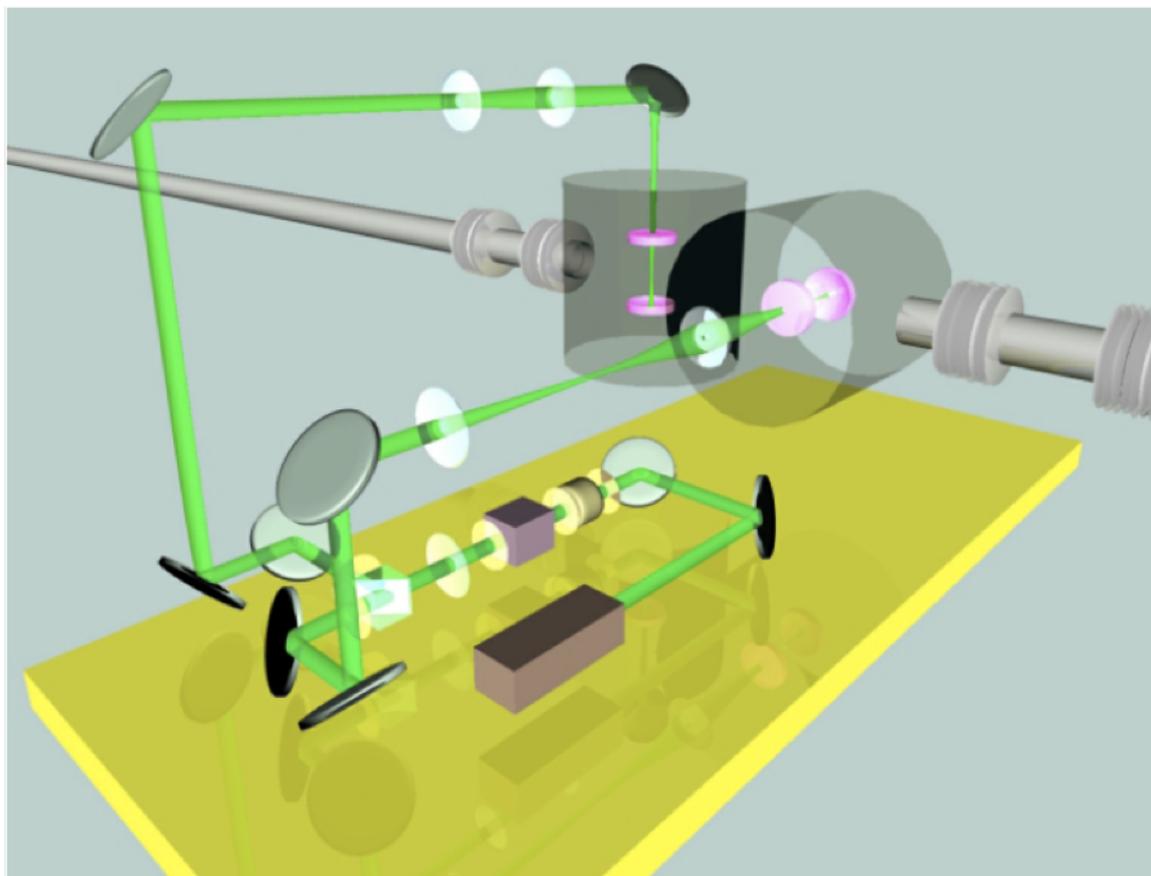


There is a physical limit on the smallest laser spot size and on the distance over which it can remain focused

$$\sigma_0 = \frac{\lambda f}{D_L} = \lambda f \#$$

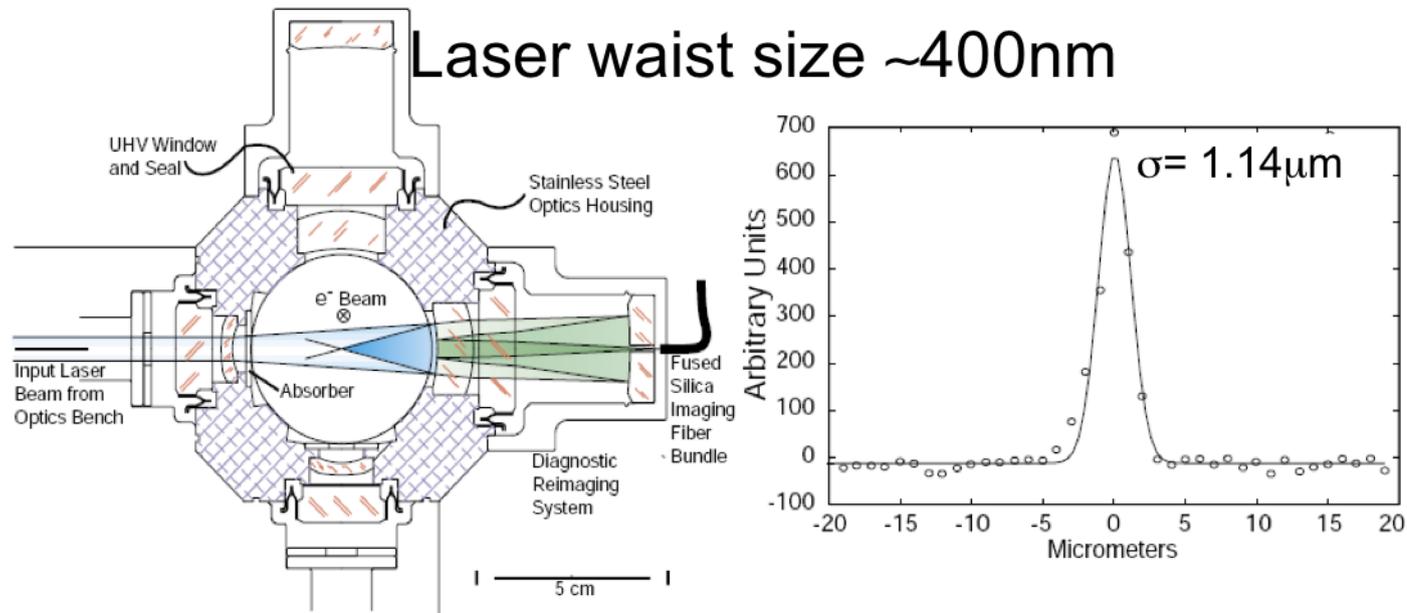
$$L_R = \frac{2\pi\sigma_0^2}{\lambda}$$

Laser Wire Scanner (3)



- At ATF original solution
- Instead of using a powerful laser an optical cavity surrounds the electrons beam
- The whole table is scanned

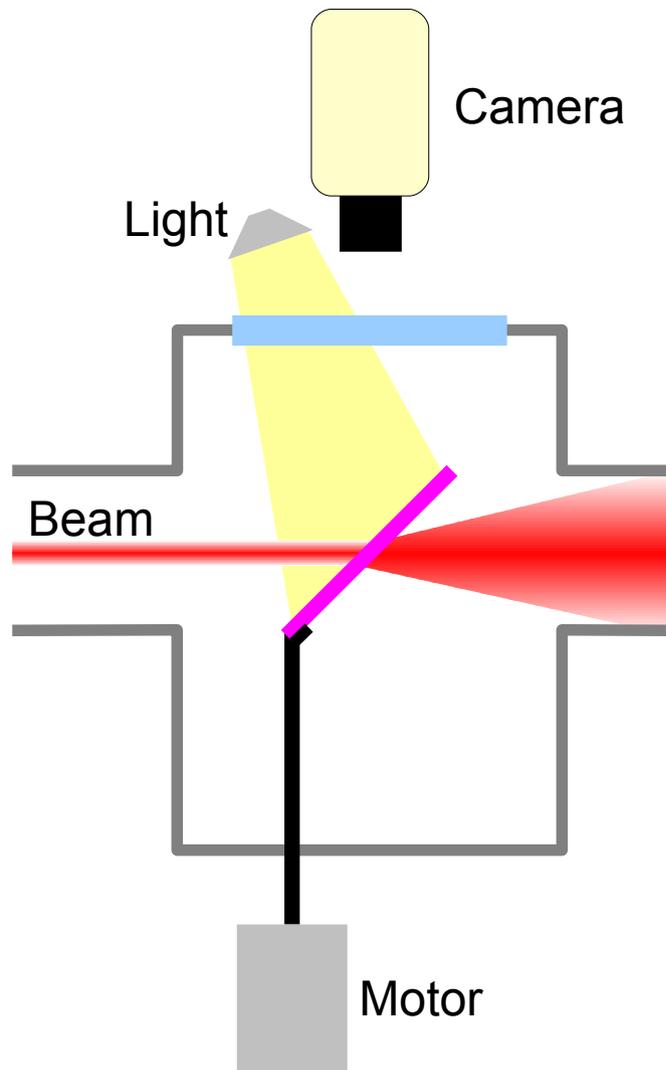
Laser Wire Scanner (SLC)



Laser Wire Scanner (4)

- High resolution LWS require
 - High power, high quality lasers (mJ, ps, $M^2 \sim 1$)
 - Complex focusing systems
 - Precise scanning systems (as an alternative the beam can be moved around)
- The resolution of the laser wire scanners is limited by the minimum waist size (of the order of the wavelength)
- A strongly focused laser beam will have a short waist length (Rayleigh length) and is not adapted for small beams with large aspect ratios
- Other limiting factors are laser stability, vibrations, x-ray detection (if low energy x-rays)

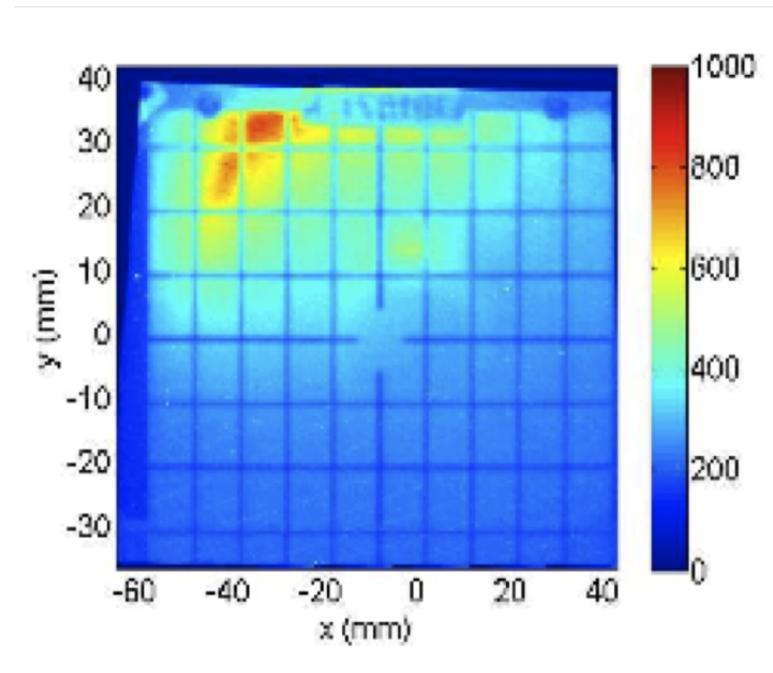
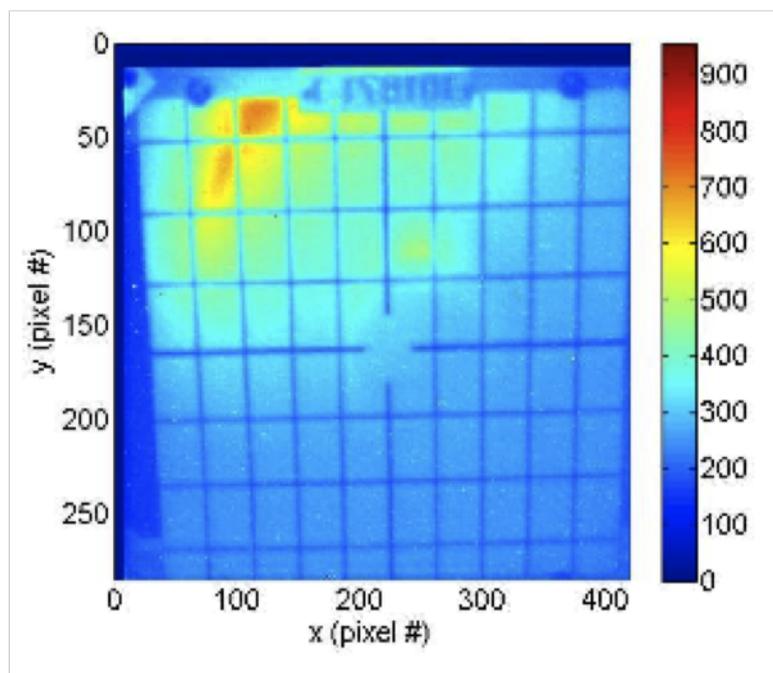
Scintillating screens



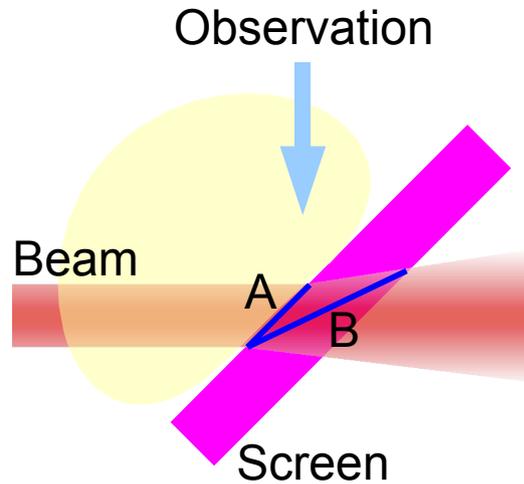
- Particles passing through the screen excite atoms and molecules
- The screen emits photons that can be observed with a TV camera (CCD)
- Multiple scattering inside screen increases beam divergence
- Typical screens are Al_2O_3 1mm thick. Robust and good for beam observation, but not for precise profile measurements.

Scintillating screens (2)

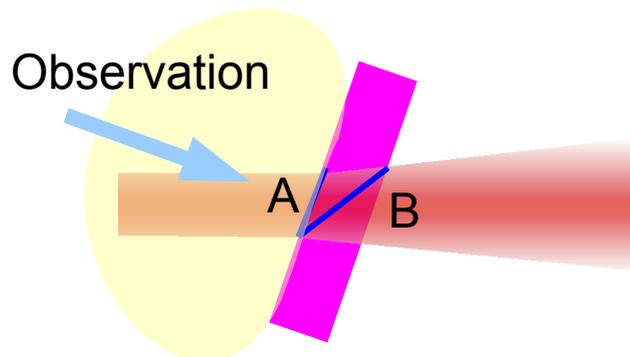
- Optical setup may introduce deformations (ex 45° screens)
- Need to perform off line corrections and calibrations



Scintillating screens (2)

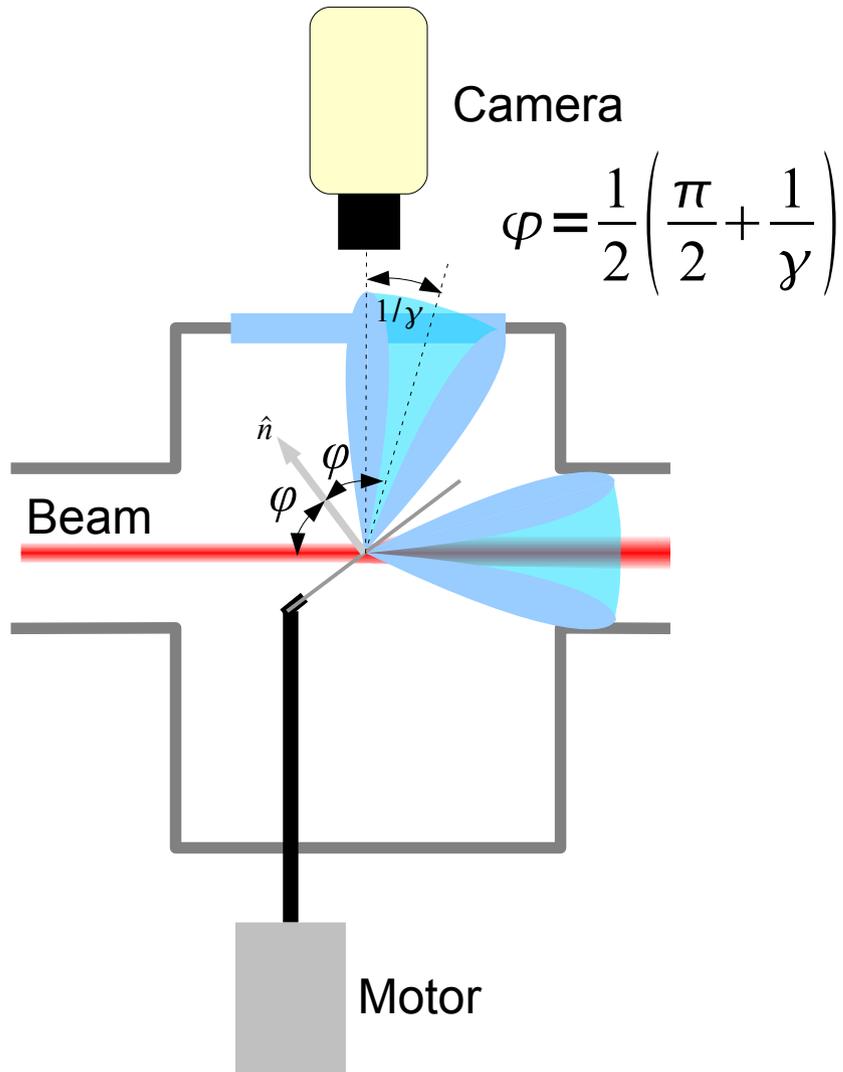


A is what we would like to observe
 B is what we really obtain



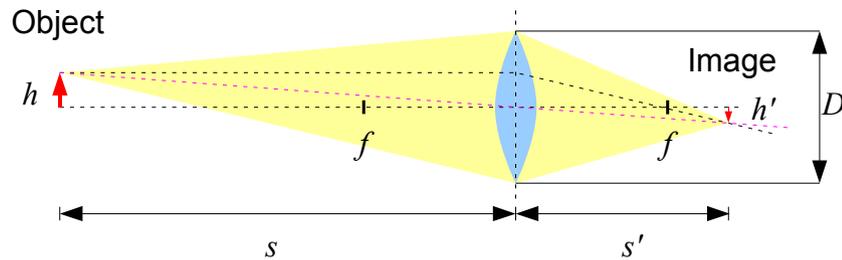
- Photons created inside the screen can escape
- The image observed is distorted
- Thickness of the screen should be small (compared to beam size)
- Observation at 90° is easy to use, but very bad for quality, also for field depth and aberrations

OTR radiators



- Use backward emission
- Reflecting properties of radiator are important (metal foil or metal coating)
- Use thin foil (few μm) or “wafers”, typically Al coated Si $\sim 300 \mu\text{m}$
- Angle of radiator depends on beam momentum
- For dense beams use carbon foils or SiC wafers

Optics primer



$$m = \frac{h'}{h} = \frac{s'}{s}$$

$$f = \frac{s m}{(m + 1)}$$

$$\frac{1}{f} = \frac{1}{s} + \frac{1}{s'}$$

$$s' = \frac{s f}{s - f}$$

Typical case: $s = 300 \text{ mm}$, $m = 0.2 \Rightarrow f = 50 \text{ mm}$, $s' = 60 \text{ mm}$

For OTR if $1/\gamma < D/(2s)$ the whole lobe can be collected and the observation angle is equal to the specular reflection. If $1/\gamma > D/(2s)$ only part of the lobe can be collected and the specular reflection differs from the observation angle

A “good” CCTV 50 mm lens has $f/\# \sim 1.4$

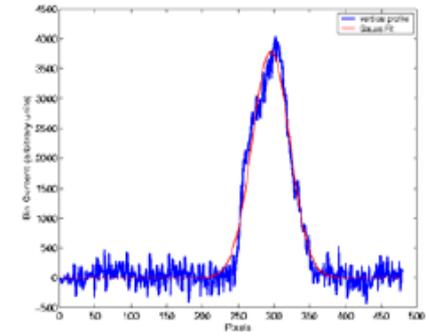
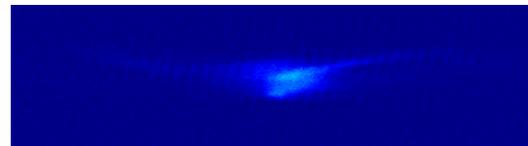
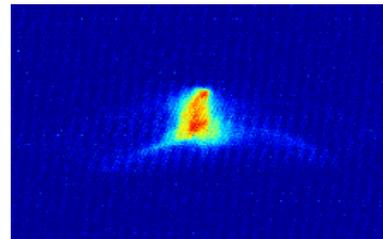
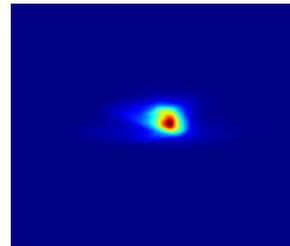
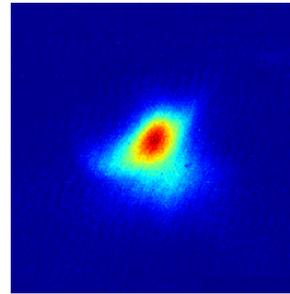
$$D = \frac{f}{f/\#} = \frac{50}{1.4} = 36 \text{ mm}$$

$$\frac{D}{2s} = \frac{36}{600} = 0.06$$

$$\gamma_{\min} = \frac{1}{0.06} = 17$$

For γ larger than γ_{\min} the whole lobe can be observed

OTR example (DESY)

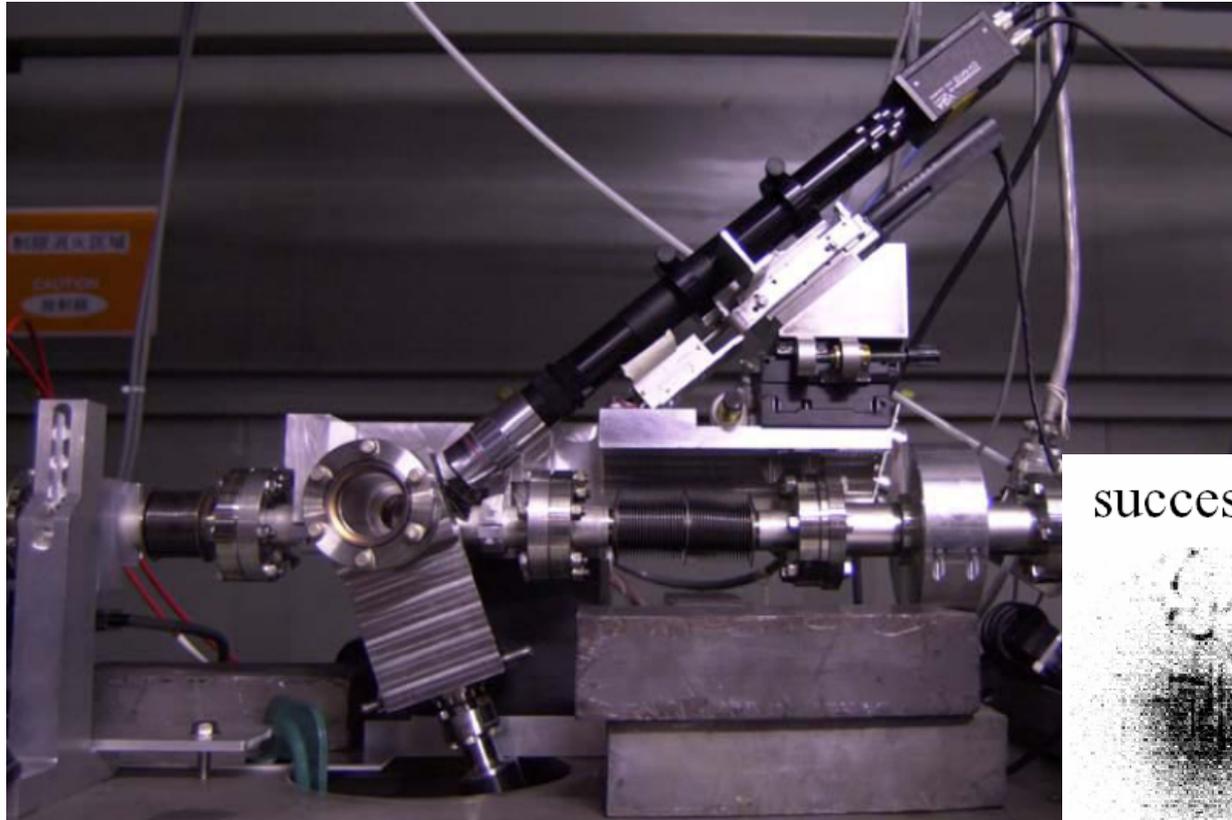


Often beams are far from Gaussian especially in linacs

Camera must be protected from radiation requiring a complex optical lines

Filters are needed to avoid saturating the camera

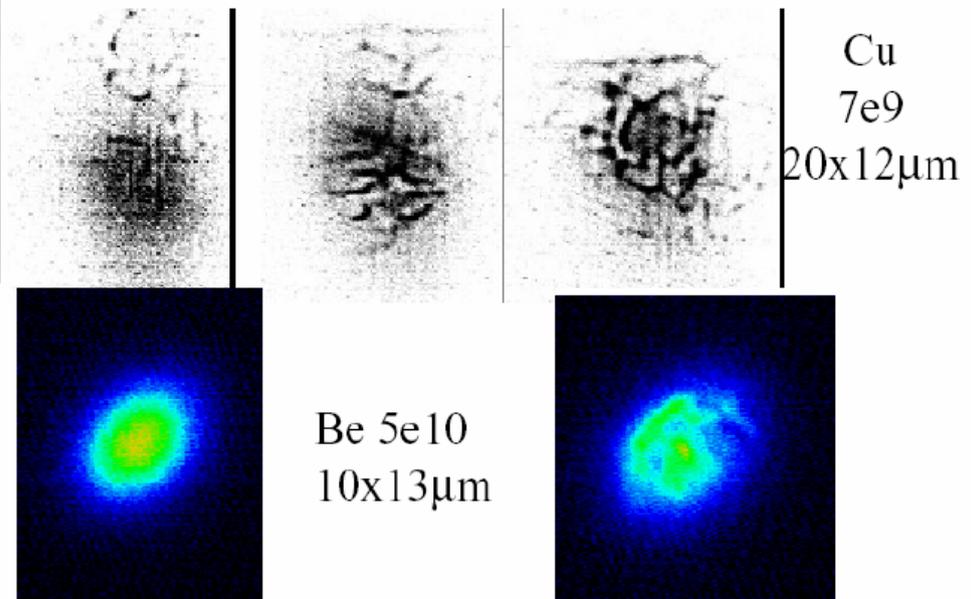
OTR example (KEK)



Small beams can be very dense posing a serious problem with radiator damage

Choosing the right material is essential

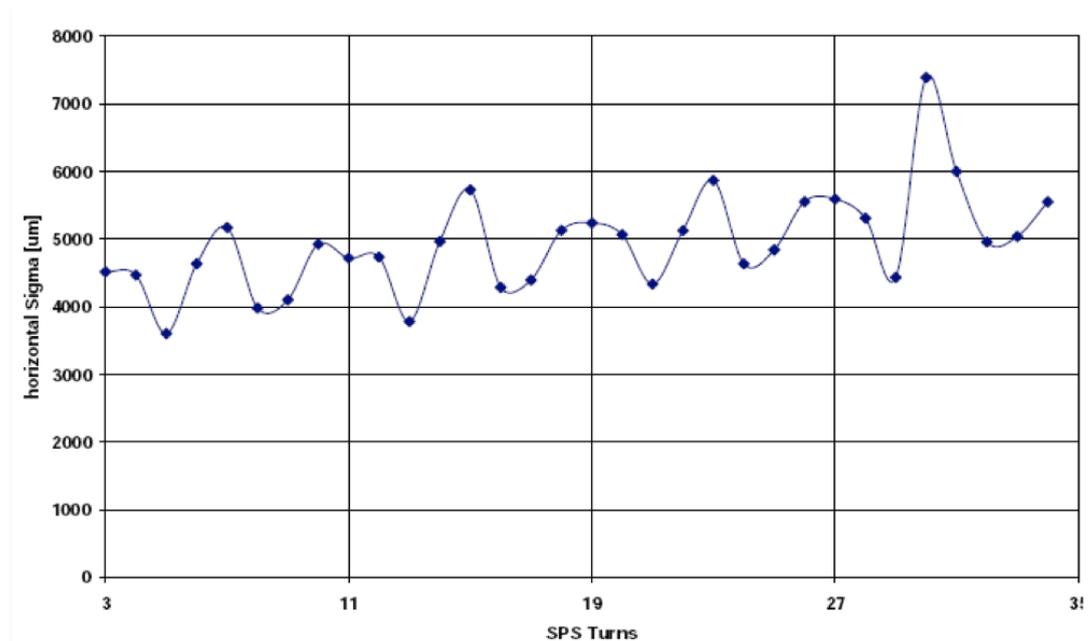
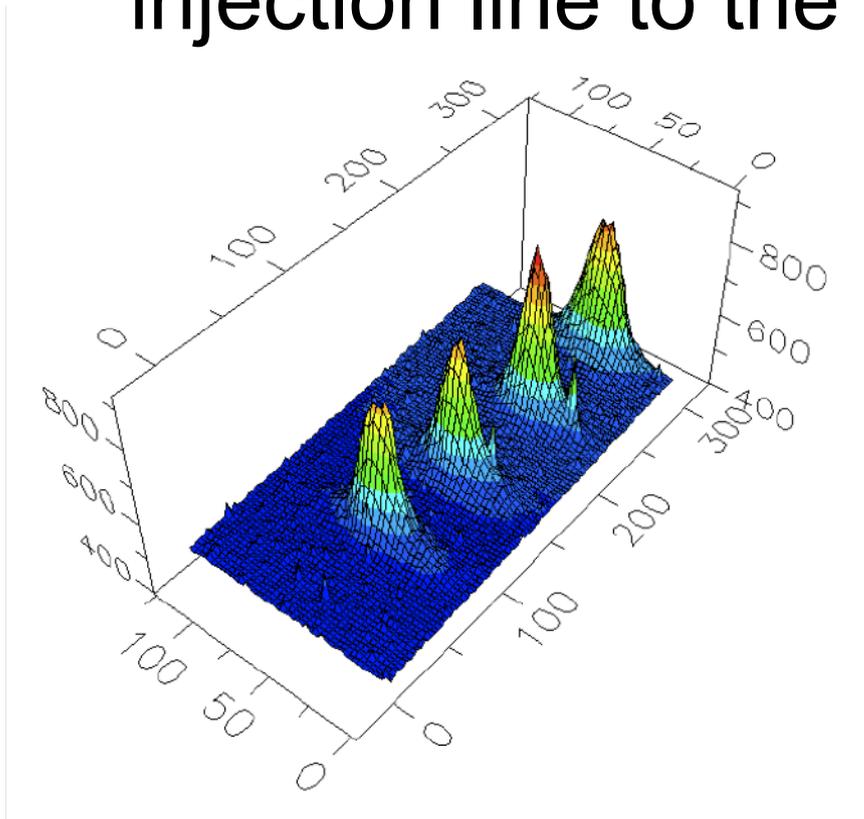
successive images illustrating damage:



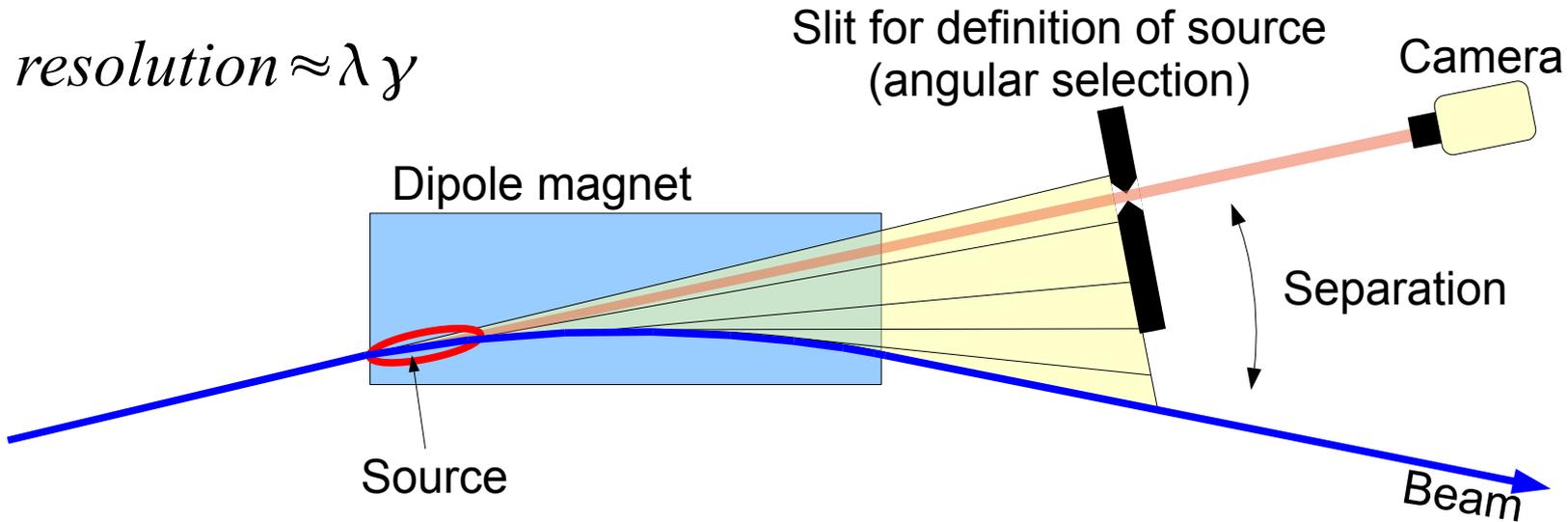
$$\Delta T(x, y) = \frac{dE}{dx} \cdot \frac{i(x, y)}{c_p}$$

OTR example (SPS)

- Consecutive images at each turn are acquired
- This can be used to tune the matching of the injection line to the ring



Synchrotron radiation



- Radiation inside magnet is constant
- Radiation at the entrance and exit edge has higher frequency components (shorter pulse) “edge radiation”
- Magnet also useful for separating photons from particles
- Source normally near entrance or even entrance edge
- Resolution limited by diffraction

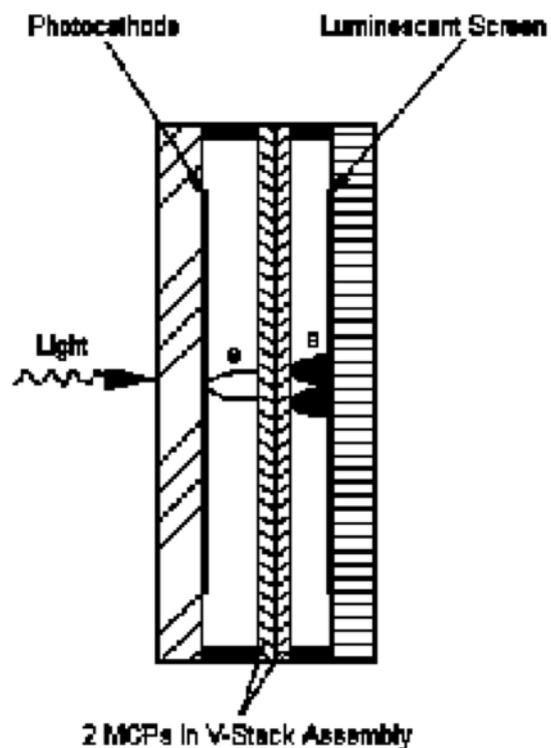
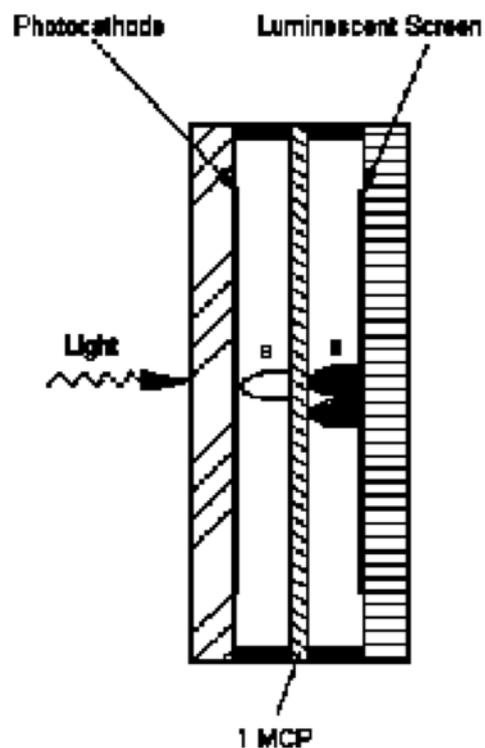
Light sensors

- 1D sensors (Can be fast up to hundreds of MHz)
 - Photo diode array
 - Linear CCD
 - Segmented photomultiplier
- 2D sensors (usually slow $\sim 50\text{Hz}$, possible up to 100 kHz)
 - image CCD
 - image CMOS
 - (Segmented photomultiplier)

Light sensors (2)

- 1D arrays (photo diodes or photo multipliers)
 - Parallel readout of each channel allows high speed, but limits resolution
- 1D CCD
 - serial readout, good resolution, but reduced speed
- 2D CCD or CMOS
 - serial readout, very good resolution, but reduced speed.
 - Special sensors with local memory and partial parallel readout allow higher acquisition speed.

Image Intensifiers

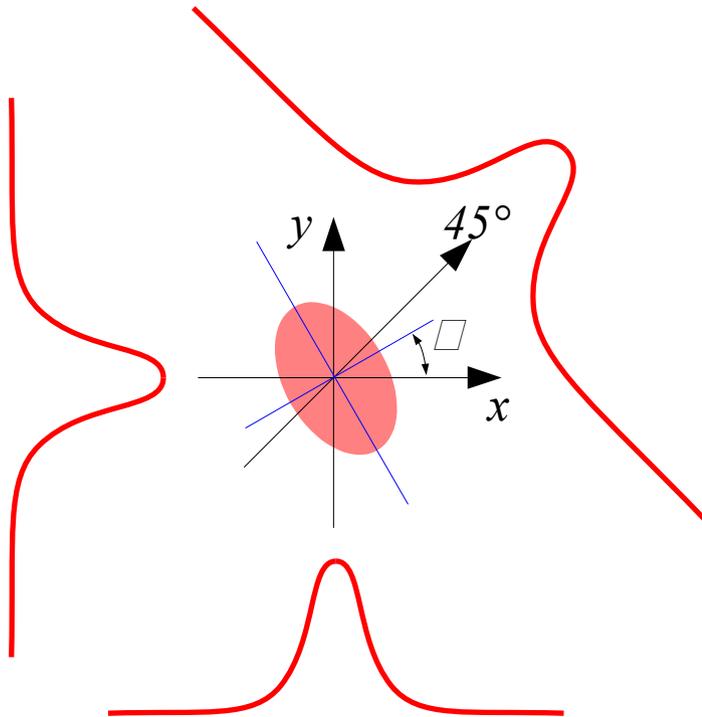


- Image intensifiers convert photons into electrons, multiply them, and then convert them back into photons, maintaining spatial information
- It is also possible to gate them and use them as shutters

Light sensors (3)

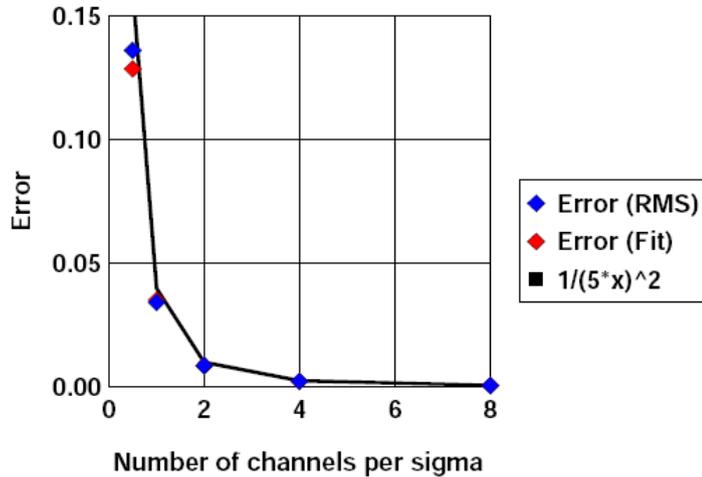
- Photomultipliers are radiation resistant (glass and metal)
- CCD and CMOS are silicon based and thus not very tolerant to radiation
- Tube cameras (ex. VIDICON) are radiation hard, but have worse resolution and sensitivity
- Special fast cameras contain loads of memory and electronics and are very sensitive to radiation (and expensive)
- Sensitivity of image sensors can be increased using image intensifiers, but usually at the expense of resolution

1D vs. 2D

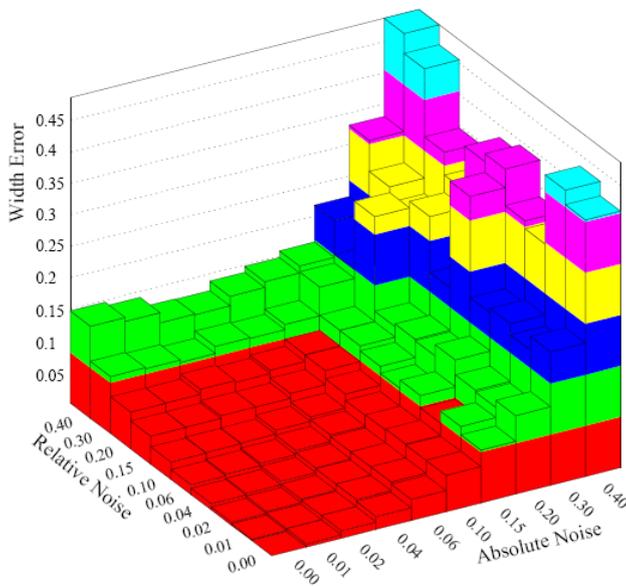


- The 2D image contains the whole spatial information
- With only 2 1D profiles (X and Y) it is impossible to see coupling (rotated ellipse in x,y) or other effects
- Need at least the profile along a third direction (45°)
- Assuming bi-Gaussian beam with tilt: σ_I , σ_{II} , θ .
- 3 D.O.F. need 3 samples

Measurement accuracy



- Accuracy of measurement depends on
 - Detector size
 - Min $\pm 3\sigma$
 - Number of points
 - Min 2 points per σ
 - Accuracy of each point
 - Both position and signal
 - Noise level
- Use fit wherever possible





**Thank you very much for your
attention**

Questions?