

# KEK R&D for LHC

Plan of 800MHz Cavity

Calculation of 400MHz Cavity

16<sup>th</sup> September 2009 , LHC-CC09 at CERN

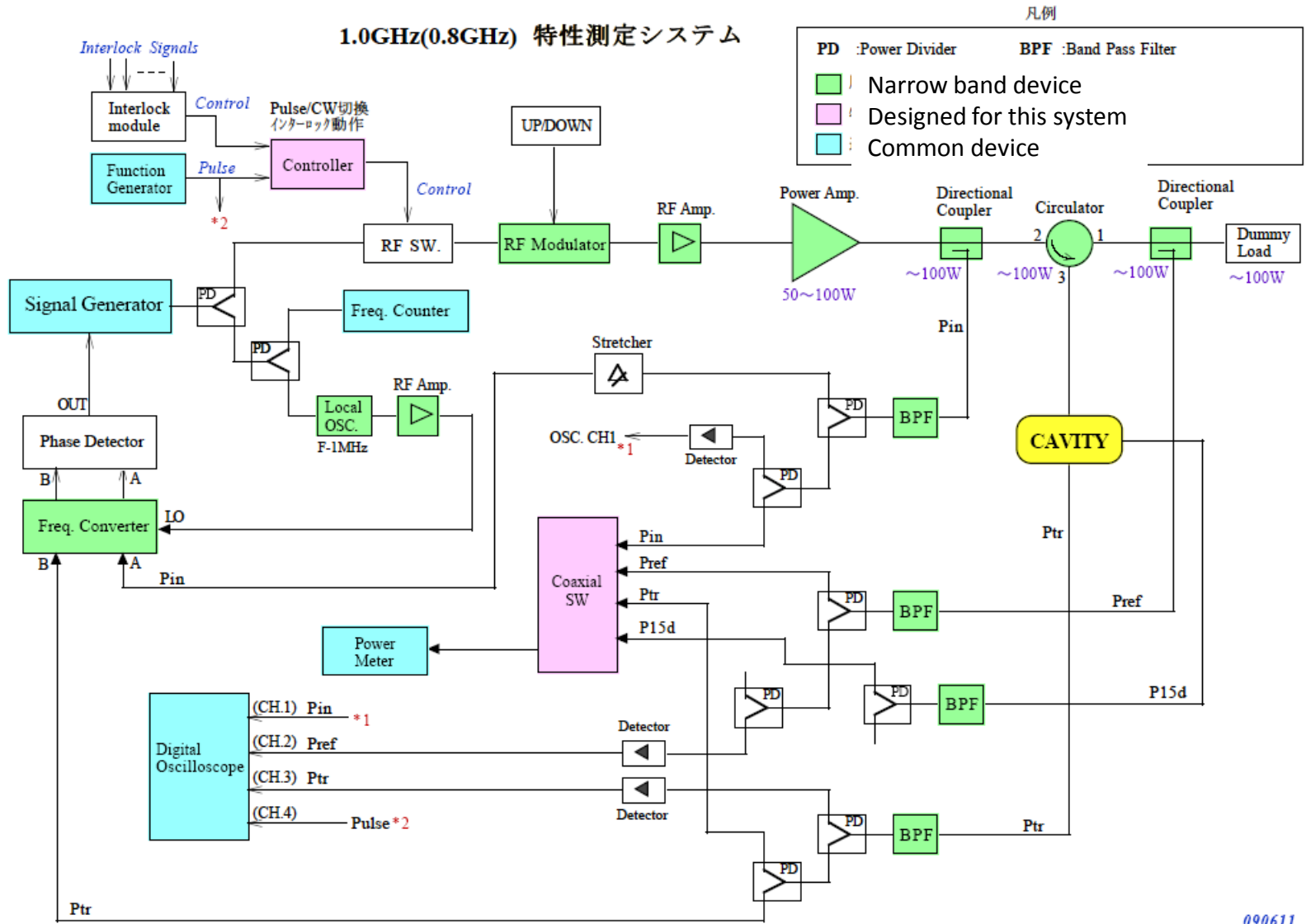
K.Nakanishi

# KEK activities (800MHz)

- Oide-san continuously supports our activities.
- New EP system
  - Construction will be completed in January 2010.
  - We will test this EP system for 509 MHz cavities.
  - We can modify this system for LHC CC.
  - HPR system will be also available.
- Vertical cold test for LHC CC
  - Our cryostat is applicable for LHC CC cold test.
  - We are planning to make a new RF system for 800 MHz (next slide).
    - Many 509 MHz components are convertible.
- Aluminum model cavity
  - We will make a aluminum model cavity.
    - To check fittings for new EP system and vertical cold tests.

# RF system for vertical cold test

## 1.0GHz(0.8GHz) 特性測定システム



# Multipacting simulations

- Multipacting simulation was done for 2-cell S-KEKB type cavity by Solyak-san.
- We thank LARP people.
- Multipactings at the opening of the coaxial coupler were found.
- This type of multipacting should be two-side, 1/2th-order multipacting.
- We have to increase coaxial gap to avoid the lowest order ( $n=1/2$ ) multipacting.
  - Increase of gap length gives enough energy to emitted electrons to avoid secondary emission.
- We observed the same type of multipacting in our 509 MHz KEKB crab cavity at the coaxial coupler at low fields.
  - Gap length was large enough to avoid the lowest order.
  - We could process in one hour.

# Multipacting on an iris

- Liling-san simulated multipacting for the baseline cavity.
- He found several multipacting levels.
- It is understood that a type of multipacting is a two-side, n-th order one. (n=1/2,3/2,5/2, etc.)
- We observed this type of multipacting in our KEKB crab cavity.
- Multipacting level exists where

$$B_{peak} \approx \frac{1}{n} \frac{m\omega}{e}, n = 1/2$$

This type of multipacting was not severe in our KEKB crab cavity.

# Concept of KEK compact crab cavity (e-crab)

- Use lowest mode.

Techniques for single mode cavities are well developed.

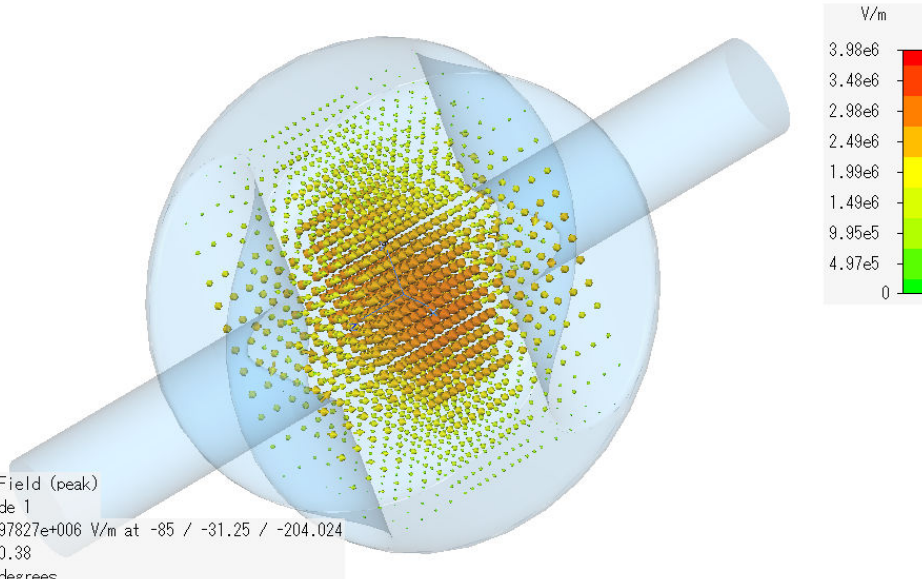
- Use the electric field.

In pillbox cavity, both of electric and magnetic field can kick the beam. The directions are opposite.

- Simple shape

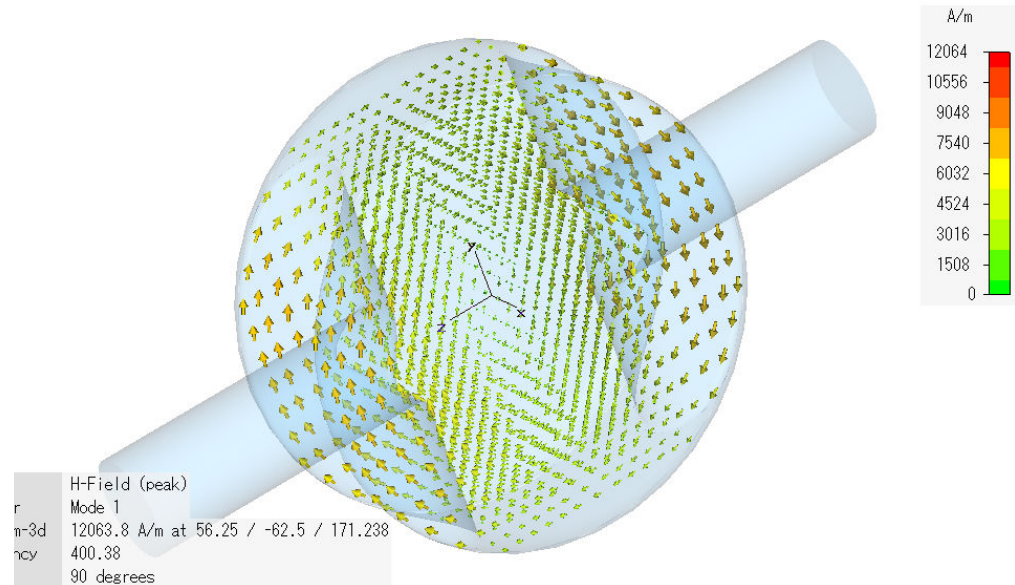
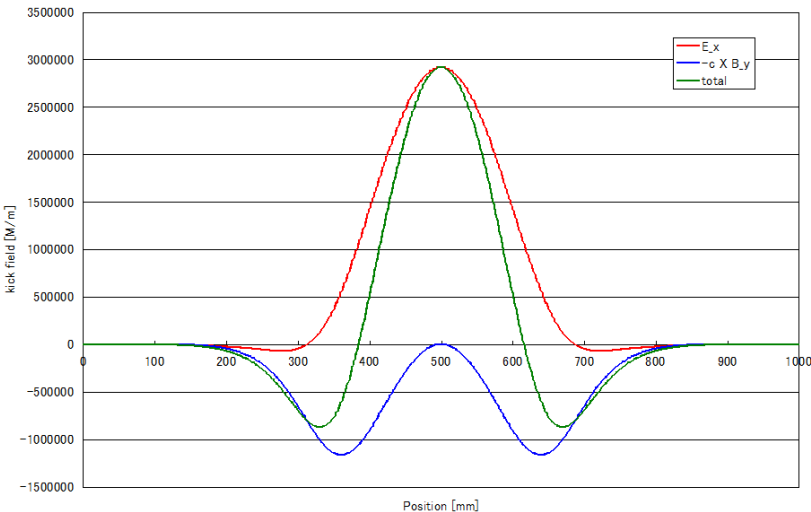
Simple shape is helpful to make clean surface.

# Field distribution



Electric and magnetic field kick the beam opposite directory.

Gap length have to be adjusted to make effective kick voltage.

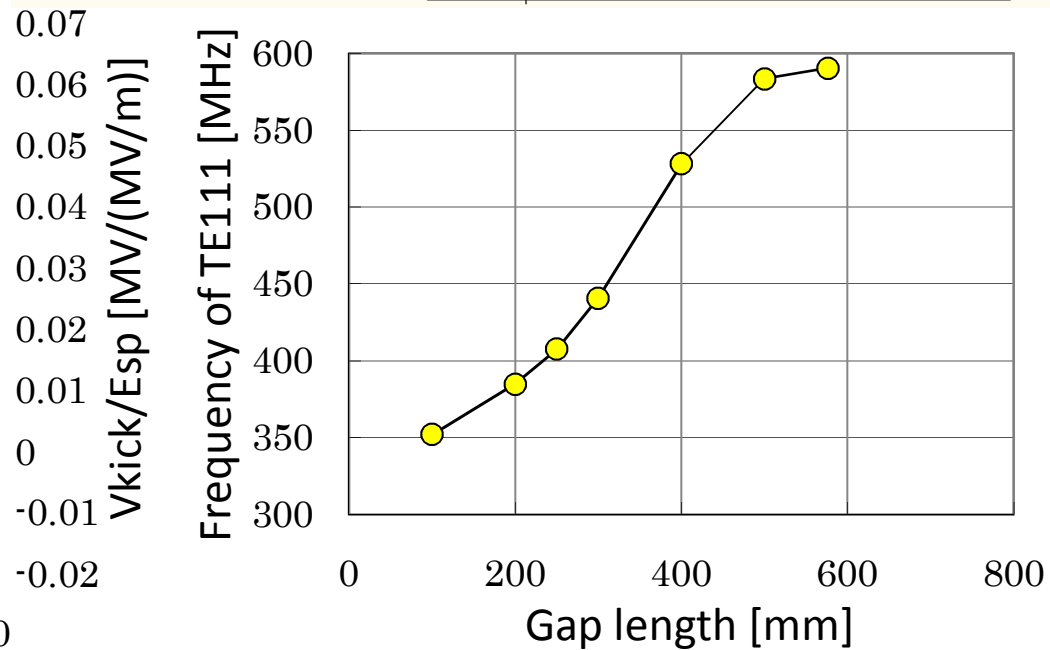
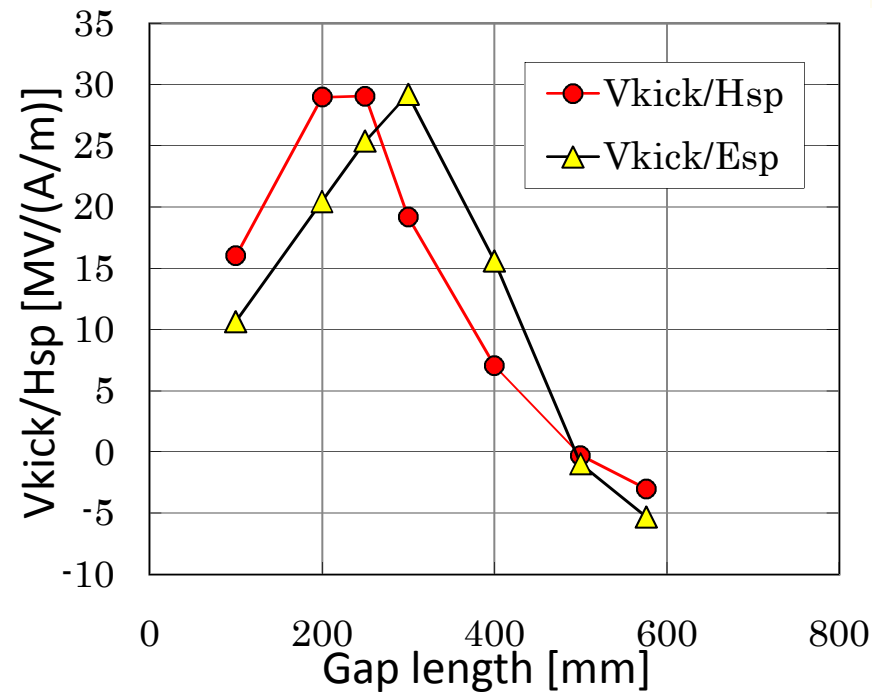
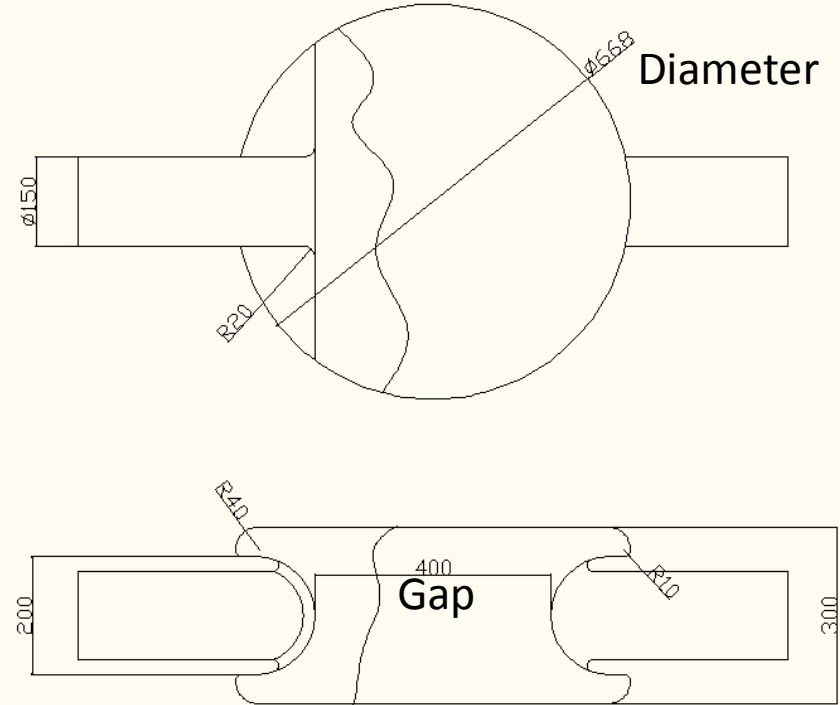


# Gap length

- Gap length was chosen to make maximum kick voltage.
- Crab mode (TM010) should be lowest mode.



Gap length -> 300mm





# HOM distribution

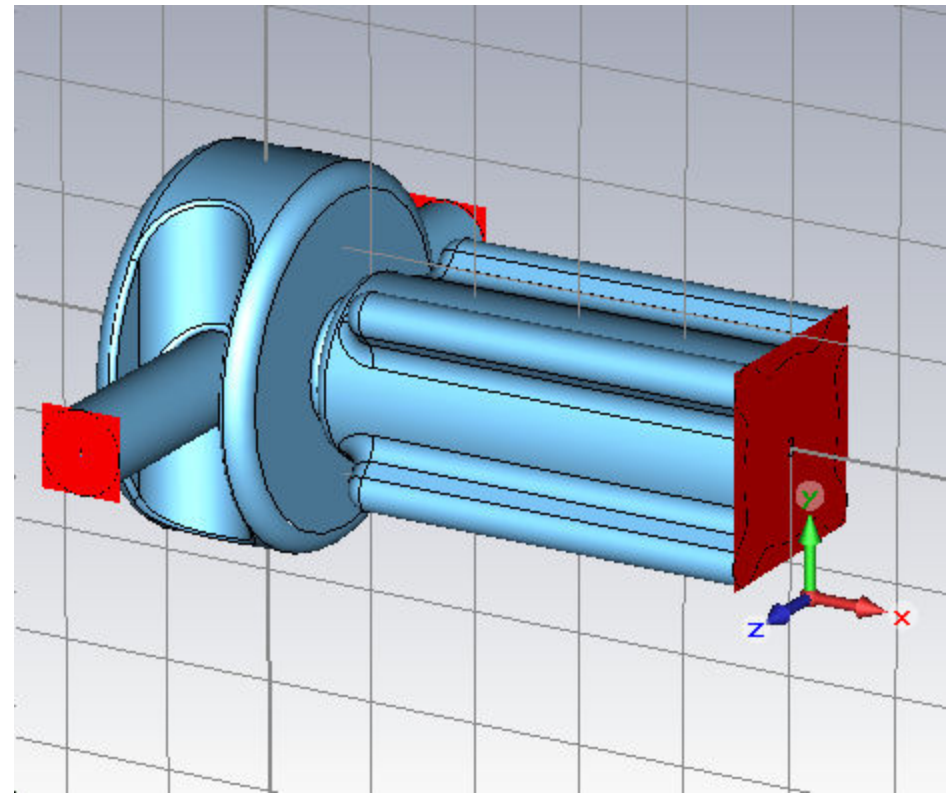
mode	Frequency [MHz]	V_kick [V/J <sup>1/2</sup> ]	Vz [V/J <sup>1/2</sup> ]	R_z/Q [Ohm]	E_sp [MV/m/J <sup>1/2</sup> ]	H_sp [Oe/J <sup>1/2</sup> ]
TM010*	400.389	238192	0.290838	0	4.08	156
TE111	440.813	0.296713	464509	78	9.27	107
TM011	471.037	0.089472	453144	69	7.74	127
TM110	574.368	40614.4	0.290216	0	8.44	152
TE211	576.627	0.633024	0.123273	0	10.1	484
TM110	587.357	0.131659	0.005841	0	3.26	175
TE211	600.556	0.593295	0.344733	0	10.4	589
TM111	678.981	0.43519	313611	23	7.03	135
TE111	681.778	0.058524	0.05005	0	3.75	130
(TM310)**	700.339	253646	0.466292	0	9.28	229

\*:Crab mode

\*\* :mode identification by cartesian coordinates.

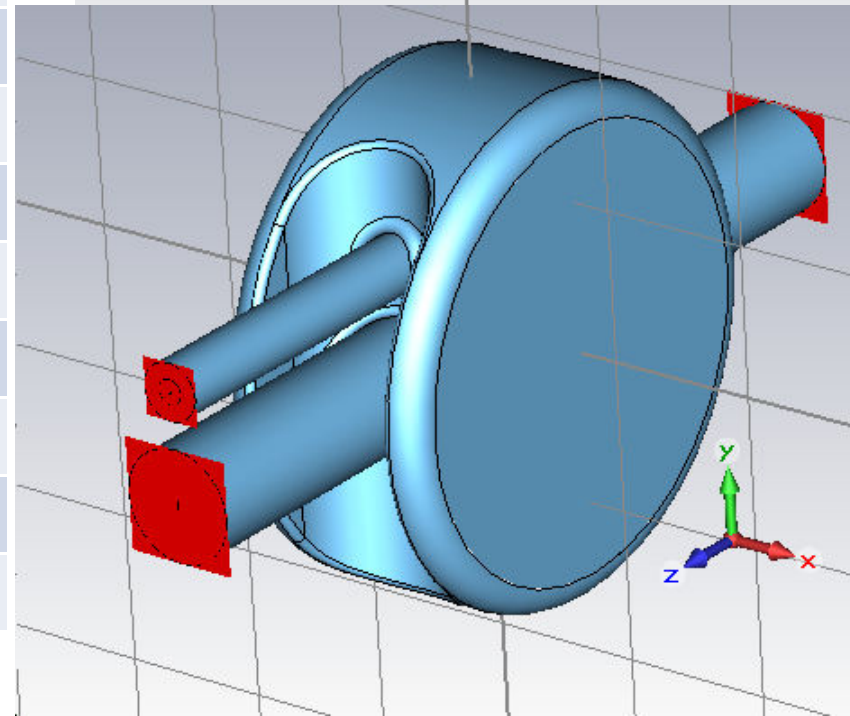
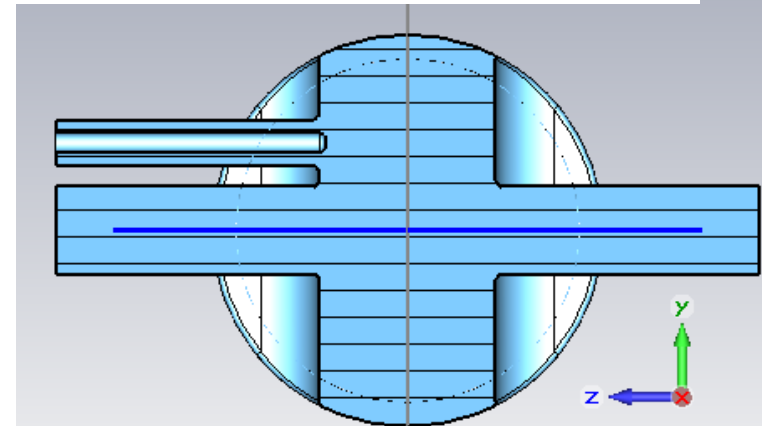
# HOM dumping (fluted pipe)

Mode	Frequency [MHz]	$Q_L$
TM010	403	1.7e10
TE111	436	1260
TM011	473	1.3e10
TM110	568	430
TM110	572	150
TE211	575	1.4e6
TE111	598	4240
TM111	647	650
TM210	699	1500



# HOM dumping (coaxial antenna)

Mode	Frequency [MHz]	$Q_L$
TM010	400	2e10
TE111	440	4700
TM011	471	6700
TM110	574	2e12
TE211	577	2100
TE111	587	1e12
-	601	2800
-	679	1480
-	699	1.23e9
-	741	6410
-	793	2.52e8
-	801	2590



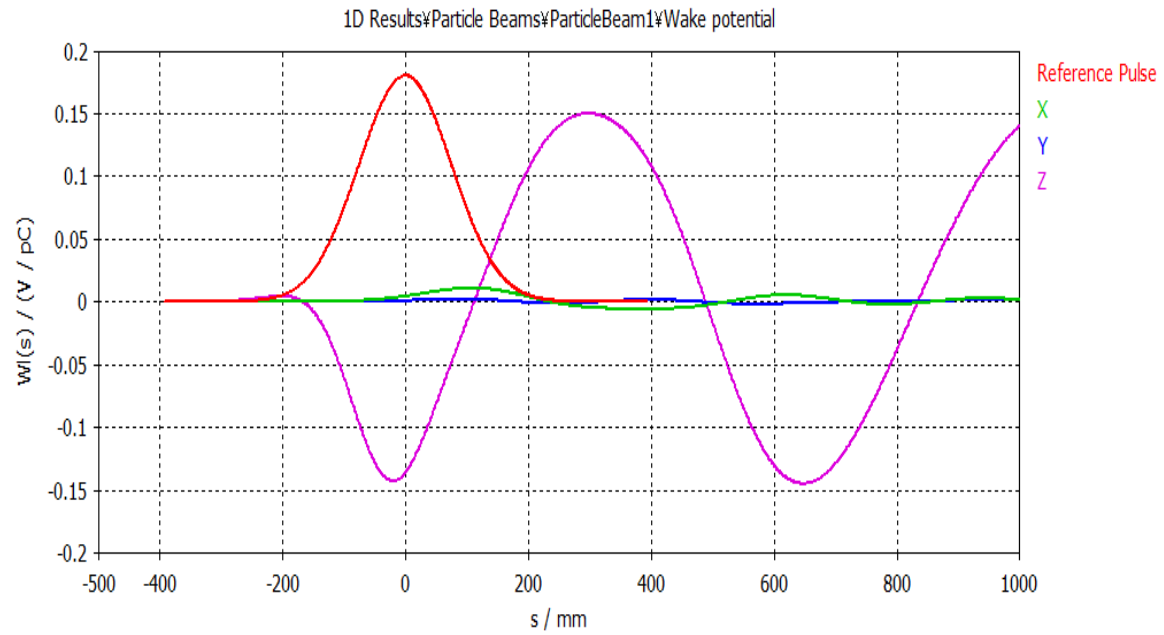


# Loss factor

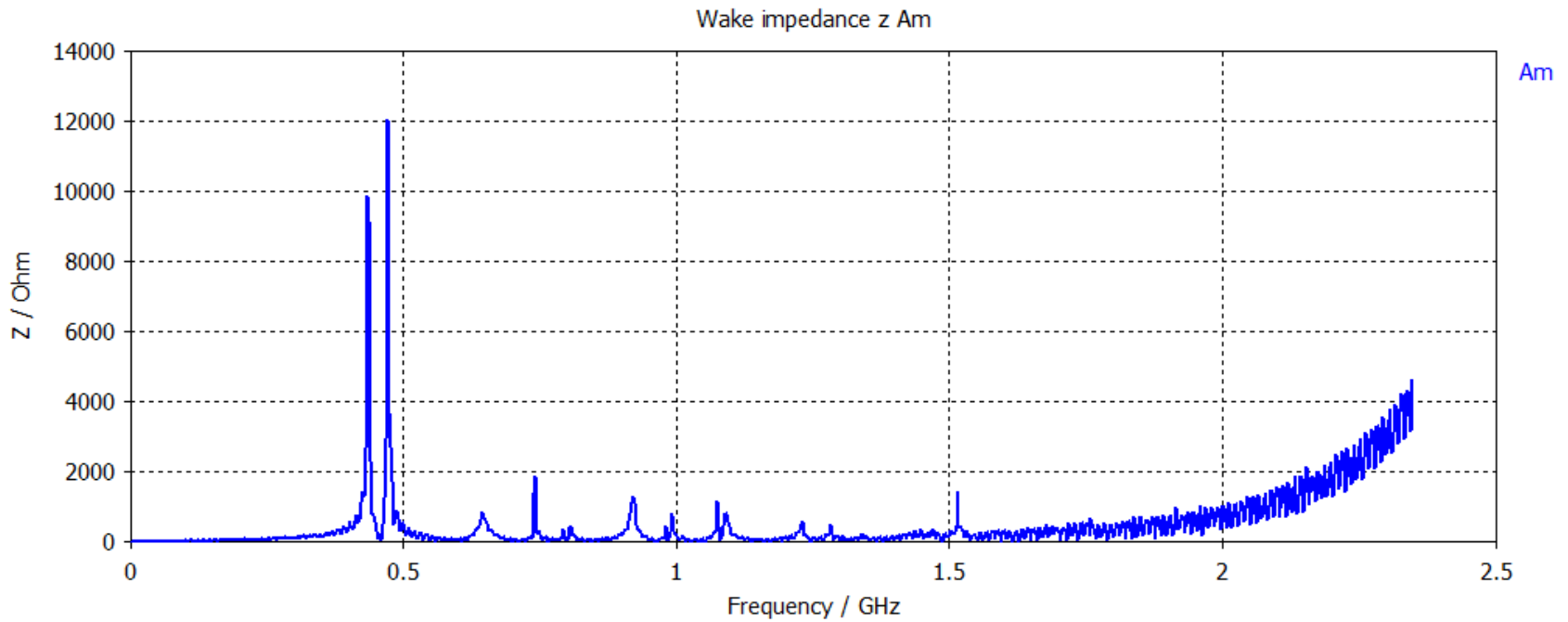
	Loss factor [ $\times 10^{-2}$ V/pC]
Cavity	8.00
With fluted pipe	8.53
With coaxial antenna	8.11
With fluted pipe and coax	8.58

~2.2kV

Sigma	Q
75.5mm	$2.72 \times 10^{-8}$ C



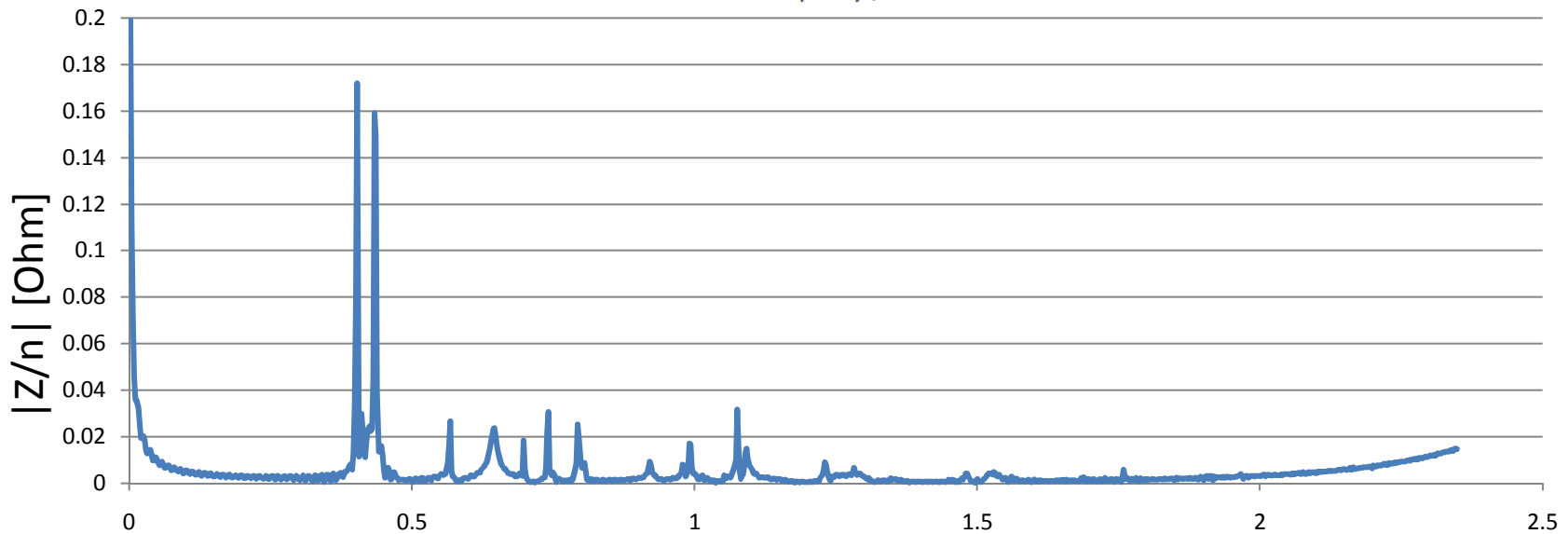
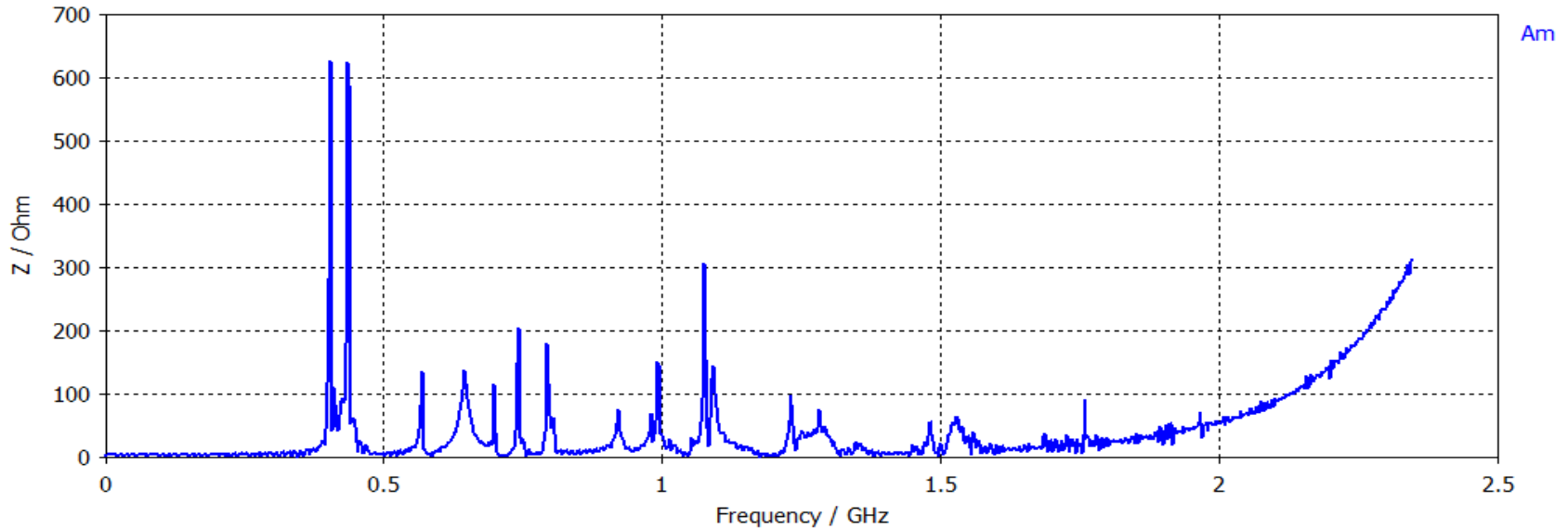
# Longitudinal impedance



Required impedance  $< 2\text{k}\Omega$

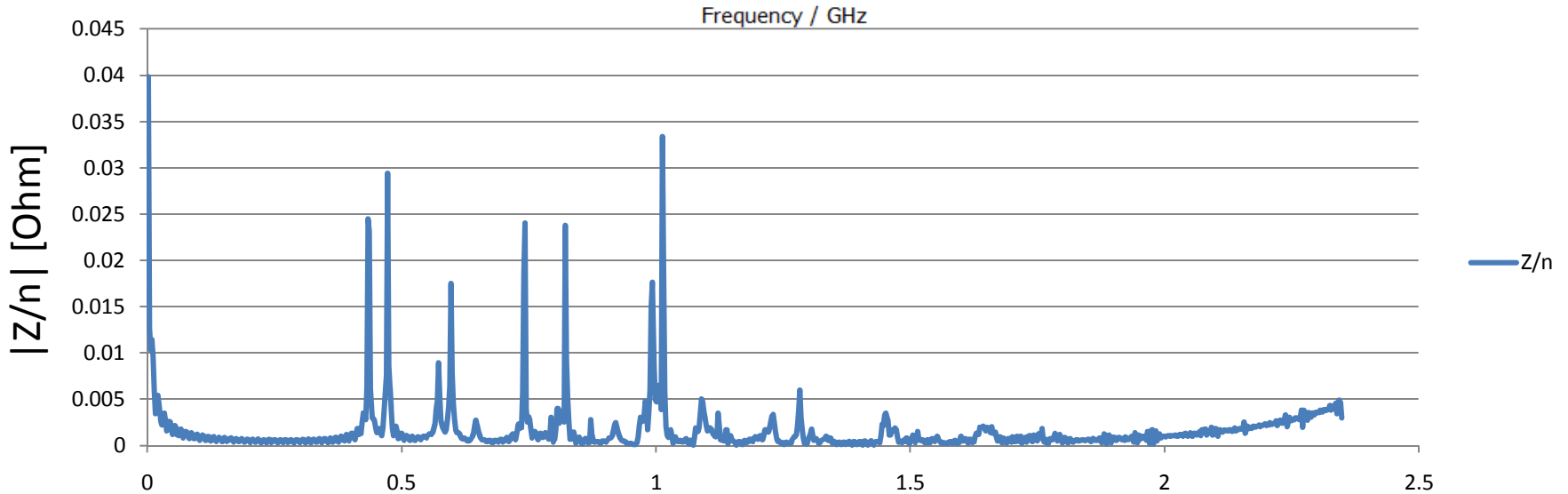
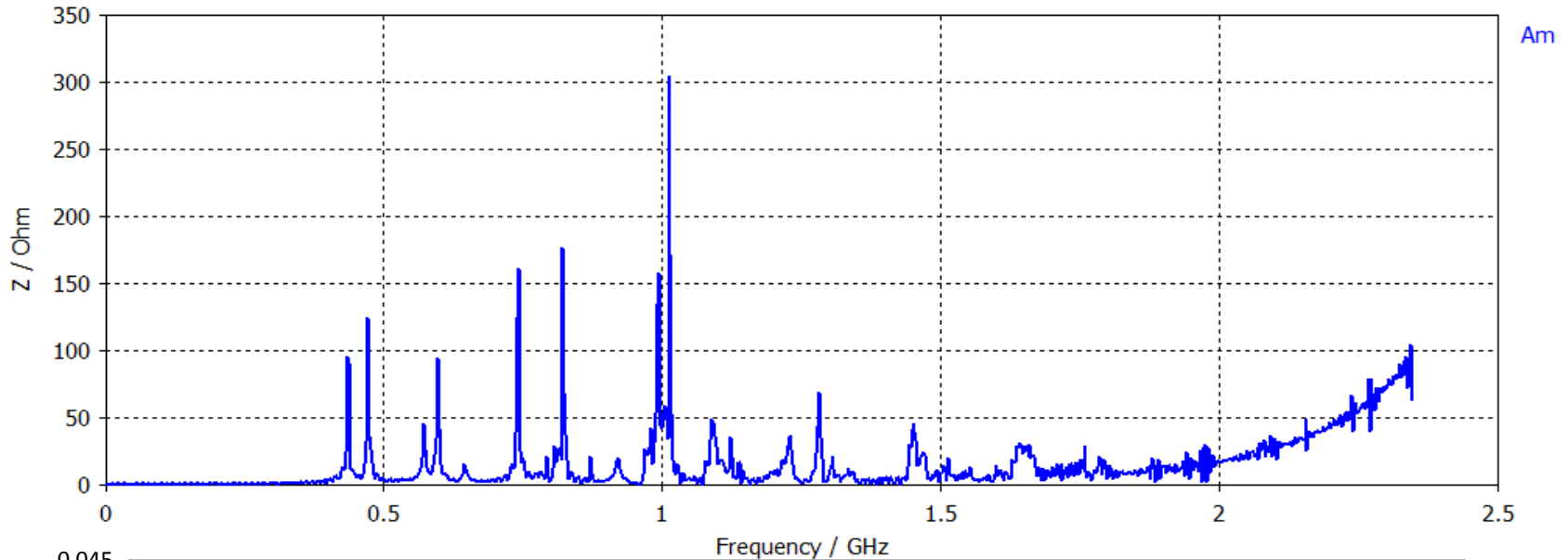
# Transverse impedance (Horizontal)

Wake impedance x  $A_m$



# Transverse impedance (vertical)

Wake impedance  $y$  Am





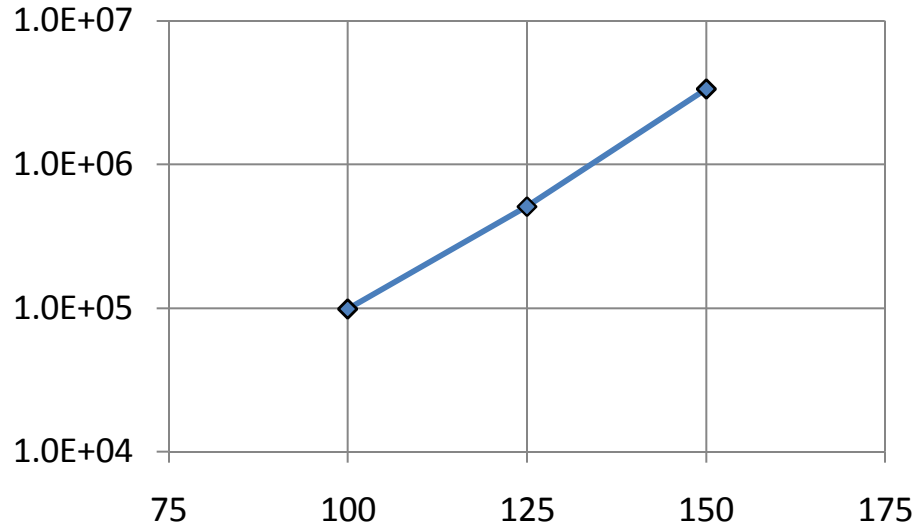
# Heat load (just for crab mode)

- In KEKB ,  $R_s$  of crab cavity was 140n $\Omega$ .
- Maximum  $E_{sp}$  is 25MV/m.

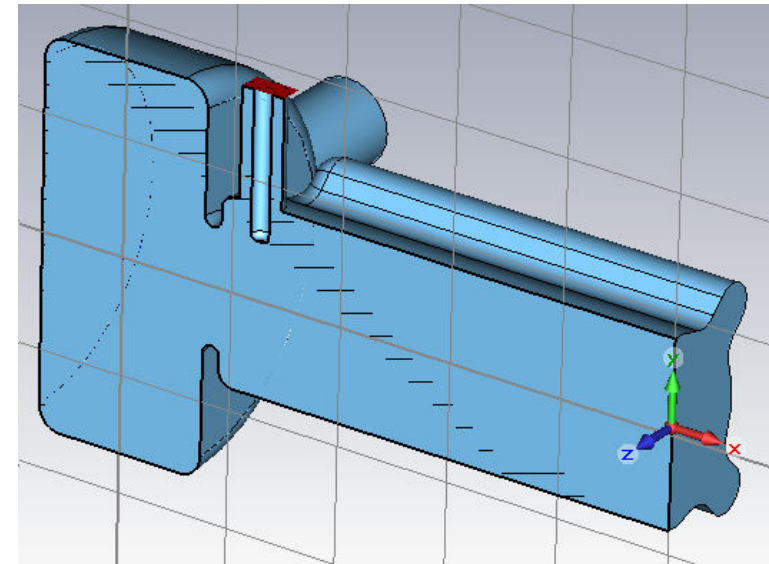


$R_s$ [n $\Omega$ ]	100~140	} assumed
$E_{sp}$ [MV/m]	25	
$H_{sp}$ [Oe]	843	
$V_{kick}$ [MV]	1.13	
Stored energy [J]	27.8	
$Q_0$	$9.1 \times 10^8 \sim 1.3 \times 10^9$	
Heat load [W]	54~77	

# Input coupler



Distance between the input coupler port and beam is assumed as 250mm. 77D standard coaxial component is applied as an input coupler.



Antenna position [mm]	Qext	RF power* [kW]
100	9.8e4	144
125	5.1e5	28
150	3.4e6	4.2

It is required RF power to make 25MV/m Esp.