# HOM power in FCC-ee cavities <br> Ivan Karpov, CERN 

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## FCC-ee options

|  | Z | W | H | $t \bar{t}$ |
| :---: | :---: | :---: | :---: | :---: |
| Bunches / beam, $M$ | 71200 | 6000 | 740 | 62 |
| Bunch spacing, $t_{b b}[\mathrm{~ns}]$ | 2.5 | 50 | 400 | 4000 |
| Bunch population, $N_{b}$ | $0.4 \times 10^{11}$ | $0.5 \times 10^{11}$ | $0.8 \times 10^{11}$ | $2.1 \times 10^{11}$ |
| Bunch length, $\sigma_{t}[\mathrm{ps}]$ | 12 | 8.3 | 7.7 | 9.2 |
| Beam current, $J_{A}[\mathrm{~mA}]$ | 1399 | 147 | 29 | 6.4 |

Harmonic number, $h=130680$
Ring circumference, $C=97.75 \mathrm{~km}$

## HOM power loss in FCC cavities

Simulated cavity impedance

$f_{0}$ - revolution frequency
$J_{A}$ - average beam current
$\rightarrow$ HOM power should be extracted (max 1 kW per coupler)

## Beam power spectrum

Spectrum contains multiples of $1 / t_{b b}$ and $f_{0}$ harmonics


For Gaussian bunches $\quad\left|J_{k}\right|^{2}=e^{-\left(2 \pi k f_{0} \sigma_{t}\right)^{2}} \frac{\sin ^{2}\left(M \pi k f_{0} t_{b b}\right)}{M^{2} \sin ^{2}\left(\pi k f_{0} t_{b b}\right)}$
$M$ is number of bunches

## Example of 400 MHz cavities

Cavity options for FCC-ee (Input from R. Calaga)


Impedance calculation using ABCI
Axisymmetric structure $+$
Gaussian bunch
Loss factor
+
Impedance

## Example of 400 MHz single-cell cavity impedance



Cutoff for all trapped modes $\leq 3 \mathrm{GHz}$

## Example of 400 MHz cavities. Impedance below 3 GHz



Resonant lines are far from the beam spectrum harmonics $k \times 400 \mathrm{MHz}$ (care should also be taken in any future design) $\rightarrow$ This impedance can be excluded from power loss calculations

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## Impedance above 3 GHz


$\rightarrow$ Larger cavity impedance for larger number of cells (opposite per cell)

## Power loss for different number of cells in FCC-ee machines



Discrete impedance lines are excluded. Single-cell cavity design is feasible for $Z$ machine

## LHC-like layout of cryomodule



## Loss factor of taper-out

Analytic estimates*

$$
\begin{gathered}
c \sigma_{t} \ll b<d \\
\kappa_{\|}(\sigma)=\frac{1}{2 \pi \varepsilon_{0} c \sigma_{t} \sqrt{\pi}} \ln \left(\frac{d}{b}\right)\left[1-\frac{\tilde{\eta}}{2}\right] \\
\tilde{\eta}=\min (1, \eta) \\
\eta=\frac{L c \sigma_{t}}{(d-b)^{2}}
\end{gathered}
$$

*S. A. Heifets and S. A. Kheifets Rev. Mod. Phys. 63, 631 (1991)


Short wake potentials are used in simulations

## Loss factors of 4-cavity structure



Loss factor $\kappa_{\|}(V / p C)$
Steps Taper-out Tapers
With cavities
3.82
2.78
1.41
$\begin{array}{llll}\text { Without cavities } & 3.23 & 1.54 & 0.13\end{array}$

Loss factor of 4 cavities is $1.21 \mathrm{~V} / \mathrm{pC}$

## Optimization of transitions



## Conclusions

- Estimations of power loss for all FCC-ee machines (400 MHz cavities)
- Maximum power losses are for Z machine: ~ 2 kW for single cell cavity, main contribution is given by impedance above 3 GHz
- For higher energy machines power losses are below 1 kW
- Significant contribution to the total power loss from tapers for FCC-ee bunch length.
- For transition from 150 mm to 50 mm loss factor of taperout $\sim 1.5 \mathrm{~V} / \mathrm{pC}$ is achieved for 5 m length
- Optimization of cold-warm transitions is ongoing


## Thank you for your attention!

## Impedance of tapers: dependence on length

Taper-out



Asymptotic behavior at high frequencies

$$
f \gg \frac{c}{2 \pi b} \rightarrow Z_{0}^{\|}=\frac{Z_{0}}{\pi} \ln \frac{d}{b}
$$

## Comparison of impedances of steps and tapers




Analytical predictions
-> Reduction of loss factor due smaller impedance at frequencies below 20 GHz

## Role of gap

Example for Z1 option (2.5 ns bunch spacing) and single-cell cavity



- Scaling corresponds to the case of broadband impedance
- Only for very small $M$ one can expect that resonances can hit revolution harmonics

