

# **An ultra-light drift chamber with particle identification capabilities**

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INFN – Lecce, ITALY

WG11 Detector Design Meeting

**CERN**

**17 October 2016**

# Road to proposal

- Ancestor chamber: **KLOE** at **INFN LNF Daφne φ factory** (commissioned in 1998 and currently operating)
- **CluCou** Chamber proposed for the **4<sup>th</sup>-Concept** at **ILC** (2009)
- **I-tracker** chamber proposed for the **Mu2e experiment** at **Fermilab** (2012)
- **DCH** for the **MEG2 upgrade** at **PSI** (under construction at INFN and to be commissioned during spring 2017)

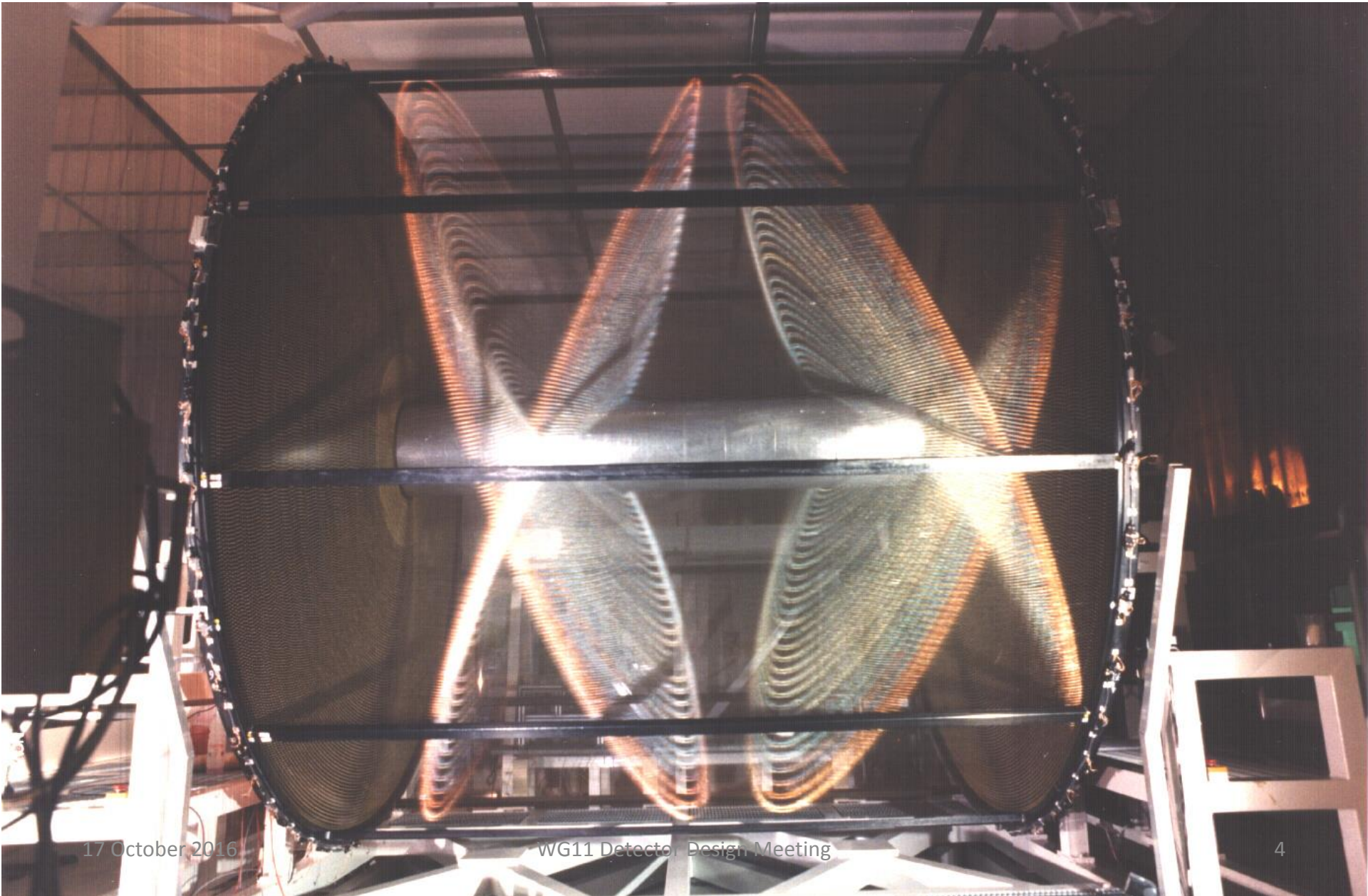
# "Traditional" Drift Chamber

A cylindrically symmetric gas volume with (para-)axial wires defining a strong electric field, strung under mechanical tension for electrostatic stability and fixed at their extremities to the end walls by means of feed-through.

## CONSTRAINTS:

- The **end walls**, holding the feed-through (which limit the chamber granularity), the FE electronics and the relative cabling, must be rigid enough to transfer the load due to the wire tension (of the order of several Tons) to the **outer cylindrical wall**, without deforming.
- The **inner cylindrical wall**, usually, does not bear any load, to minimize the multiple scattering of incoming particles.
- The **gas tightness** relies on the hermetic properties of all surfaces and of all their relative joints.

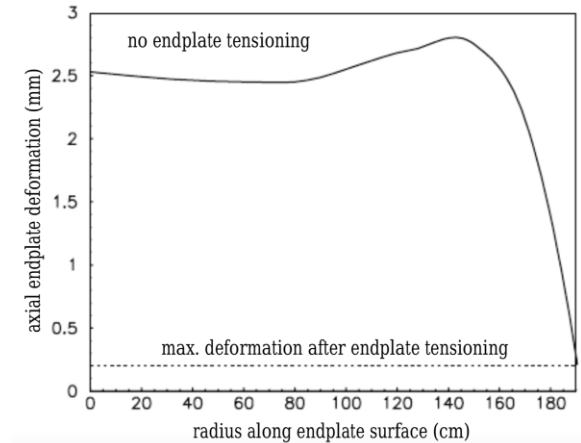
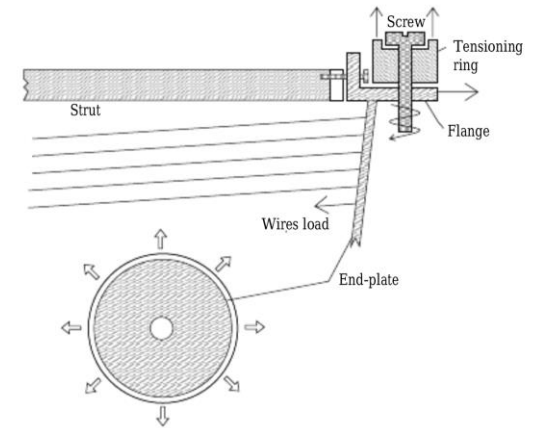
# The KLOE Drift Chamber



# The KLOE Drift Chamber

## Mechanical and construction characteristics

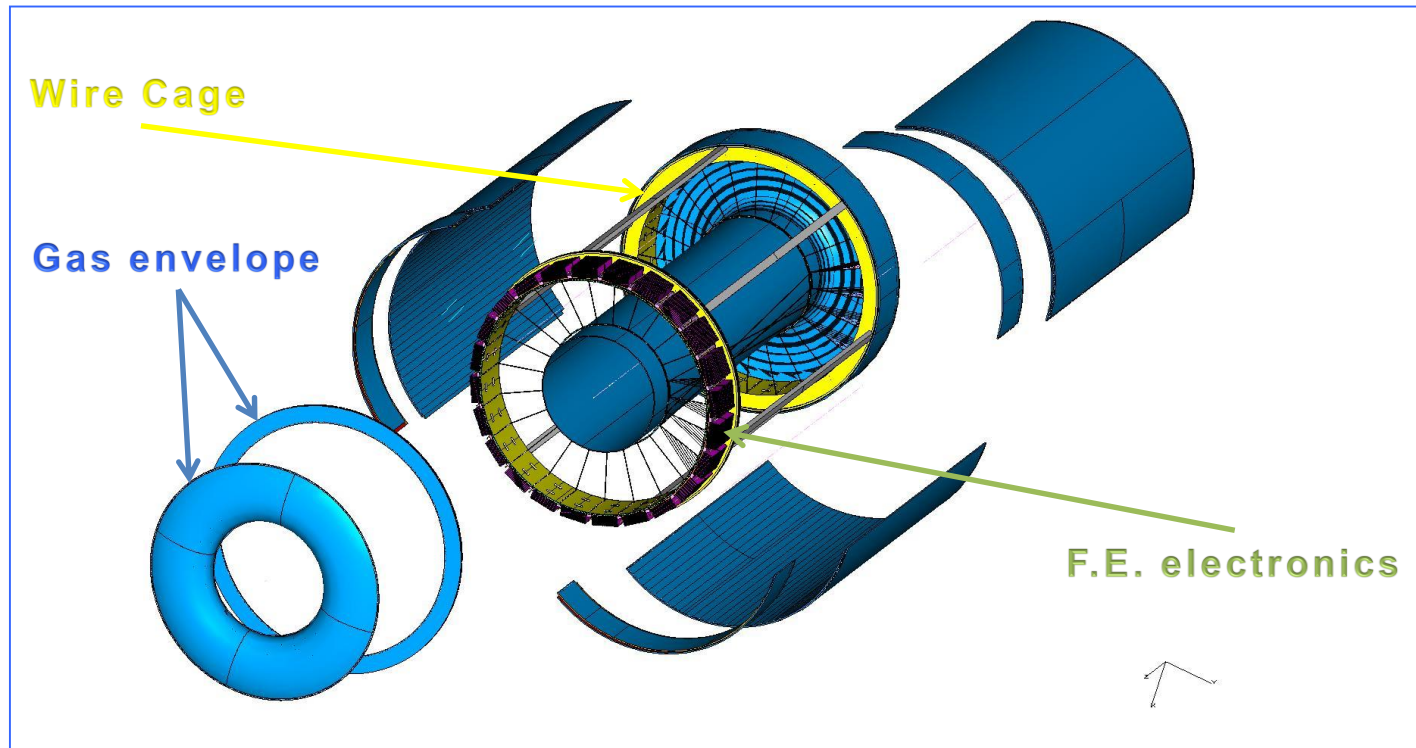
Outer radius	1980 mm
Outer panels thickness	39.0 mm
Inner cylinder radius	250 mm
Inner cylinder thickness	1.1 mm
End-plate radius of curvature	9760 mm
End-plate thickness	9 mm ( $0.03 X_0$ )
C-fiber $X_0$	26.7 cm
Maximum length	3320 mm
Minimum length	2800 mm
Number of drift cells	12,582
Number of wires	52,140
End-plate wire load	3500 kg



# Drift Chamber "Innovations"

1. Separating **gas containment** from **wire support** functions
2. Using **a larger number** of **thinner** (and **lighter** wires)
3. No **feed-through** wiring
4. Using **cluster timing** for improved spatial resolution
5. Using **cluster counting** for particle identification

# Gas containment and Wire support



**Gas containment** **Gas envelope** can freely deform without affecting the internal wire position and tension.

**Wire support** **Wire cage** structure not subject to differential pressure can be light and feed-through-less.

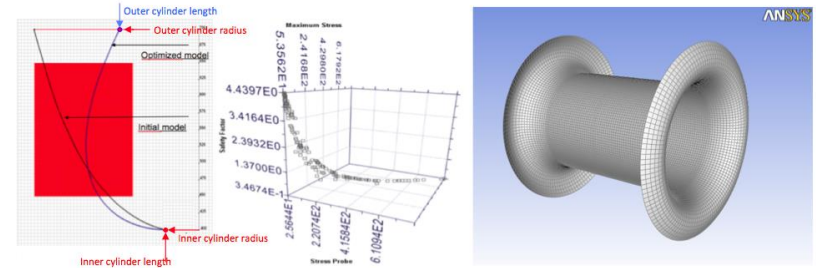
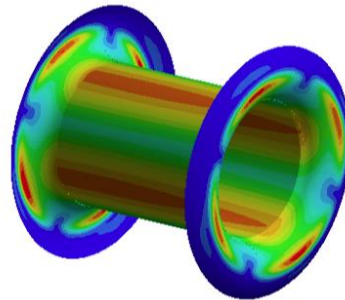
# Example: The Mu2e I-Tracker proposal

## Gas Envelope

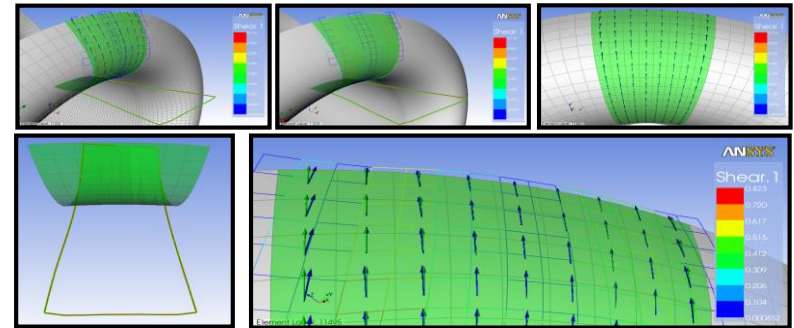
A structural multivariate analysis software (**ModeFrontier®**) has enabled to find the optimal shape for the **profile of the end plates** by minimizing maximum stress and stress on inner cylinder

**ANSYS ACP®** has chosen the proper unidirectional prepreg to form **ply**, **draping** of the laminates and **flat-wrap** of the optimized model

Solve buckling problems of inner cylinder by increasing the **moment of inertia** with use of proper light core composite sandwich



parameters	Initial model	Optimized model
Maximum stress	357.5 MPa	58.7 MPa
Stress at inner boundary	267.4 MPa	26.6 MPa
Safety factor	0.783	4.44



### End plates:

4-ply 38 $\mu$ m/ply  
orthotropic (0/90/90/0)  
**0.021 g/cm<sup>2</sup>**  
**5 × 10<sup>-4</sup> X<sub>0</sub>**

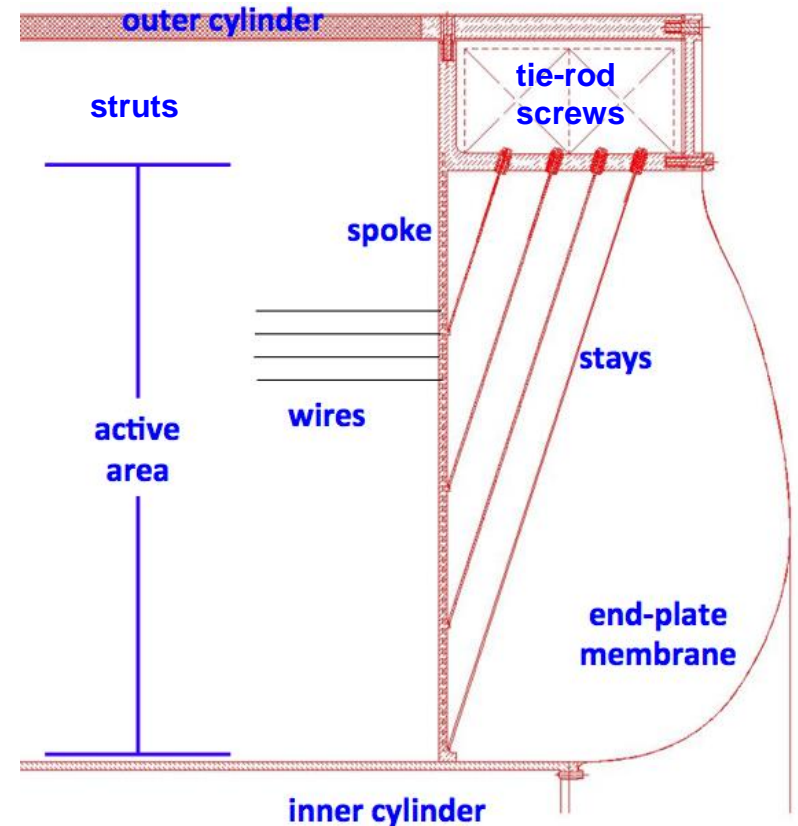
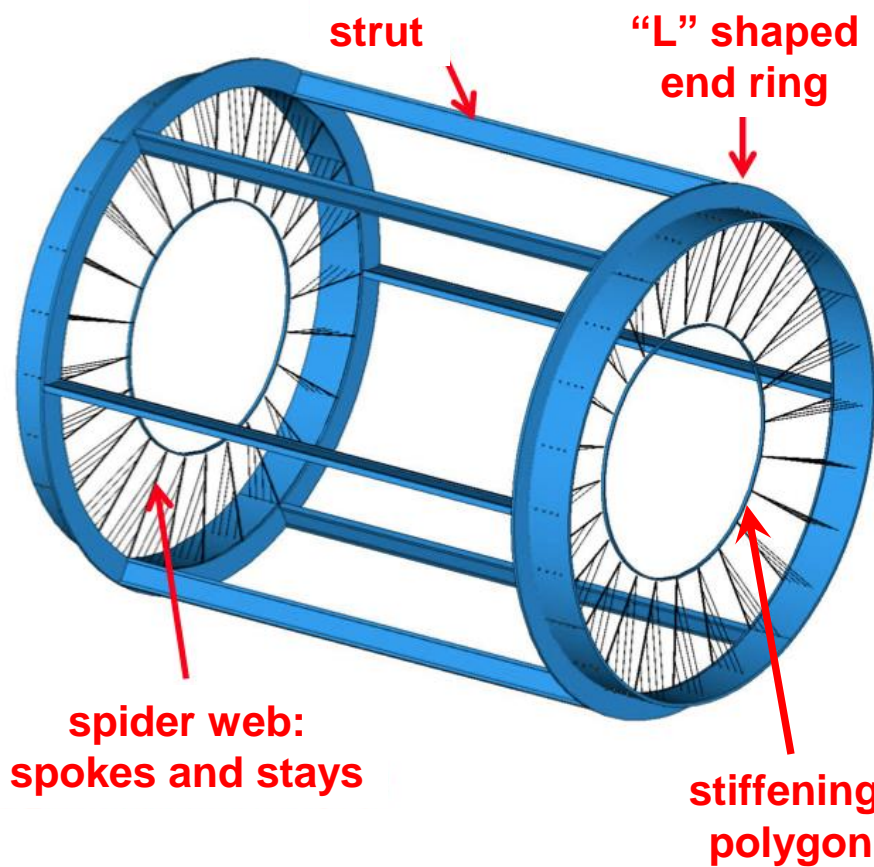
### Inner cylinder:

2 C-fiber skins, 2-ply,  
C-foam core, 5 mm  
**0.036 g/cm<sup>2</sup>**  
**9 × 10<sup>-4</sup> X<sub>0</sub>**

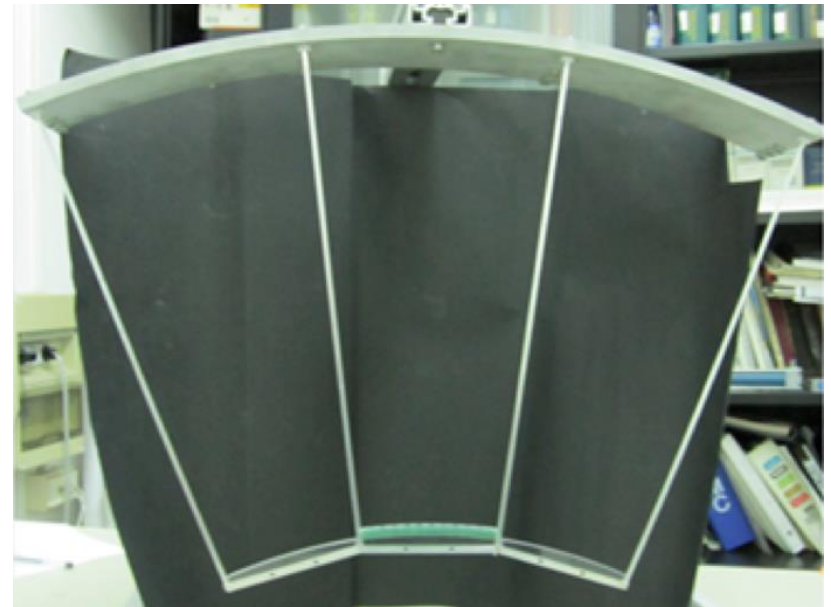
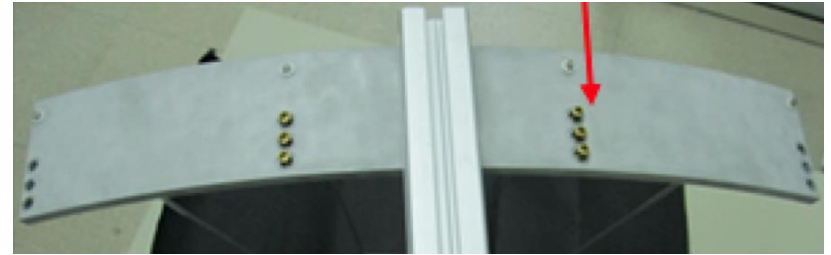
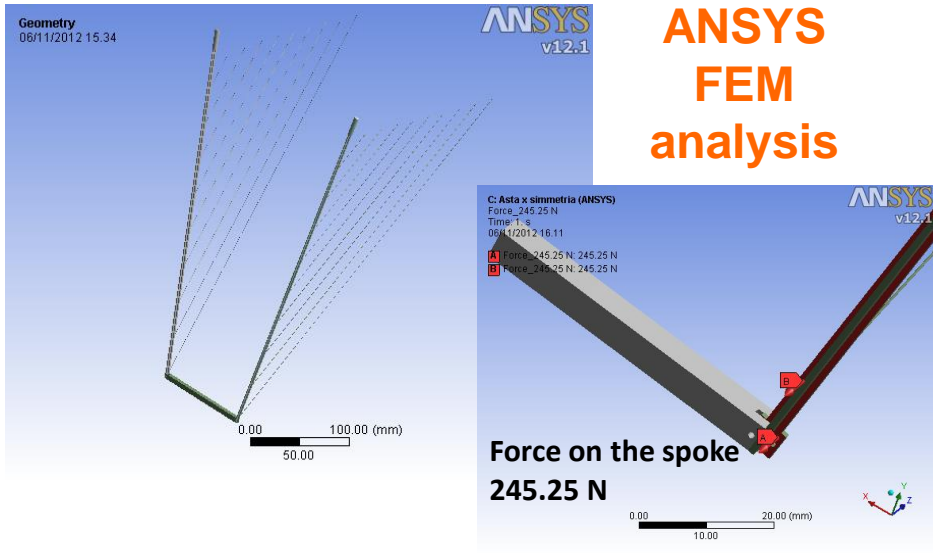


# Example: The Mu2e I-Tracker proposal

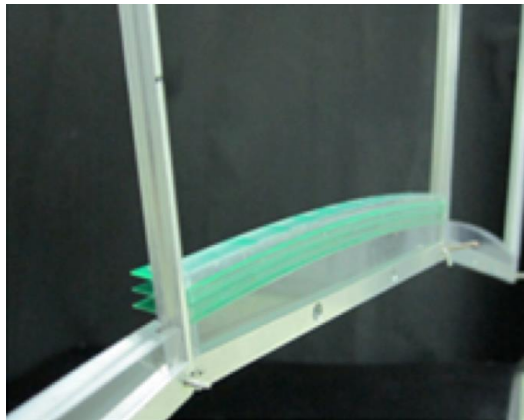
## Wire cage (conceptual)



# Verification of validity of principle



scale 1:1  
model  
to verify  
validity  
of principle

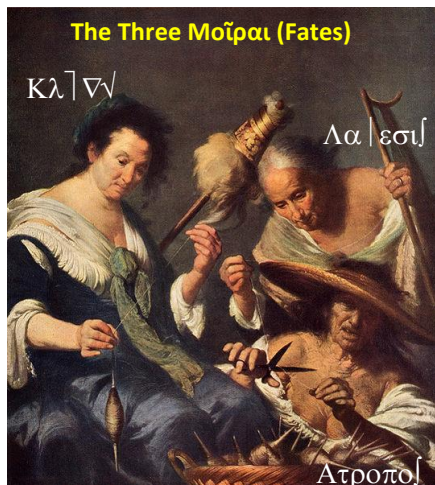


# Wire Cage

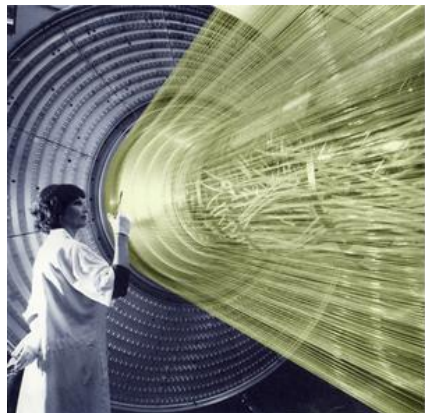
- This scheme does not require **wire feed-through** thus allowing for denser wire spacing, i.e. **smaller cells** (finer chamber granularity) and for **larger field to sense wires ratios**.
- **Larger field to sense wires ratio** and, therefore, **thinner field wires**, help reducing **multiple scattering contribution** and **total wire tension** on support structure.
- Large number of wires and small cells, however, require complex and cumbersome **assembly procedures**, which call for a **novel approach** to the wiring problem.

# DC stringing: the old way

## The Old Way



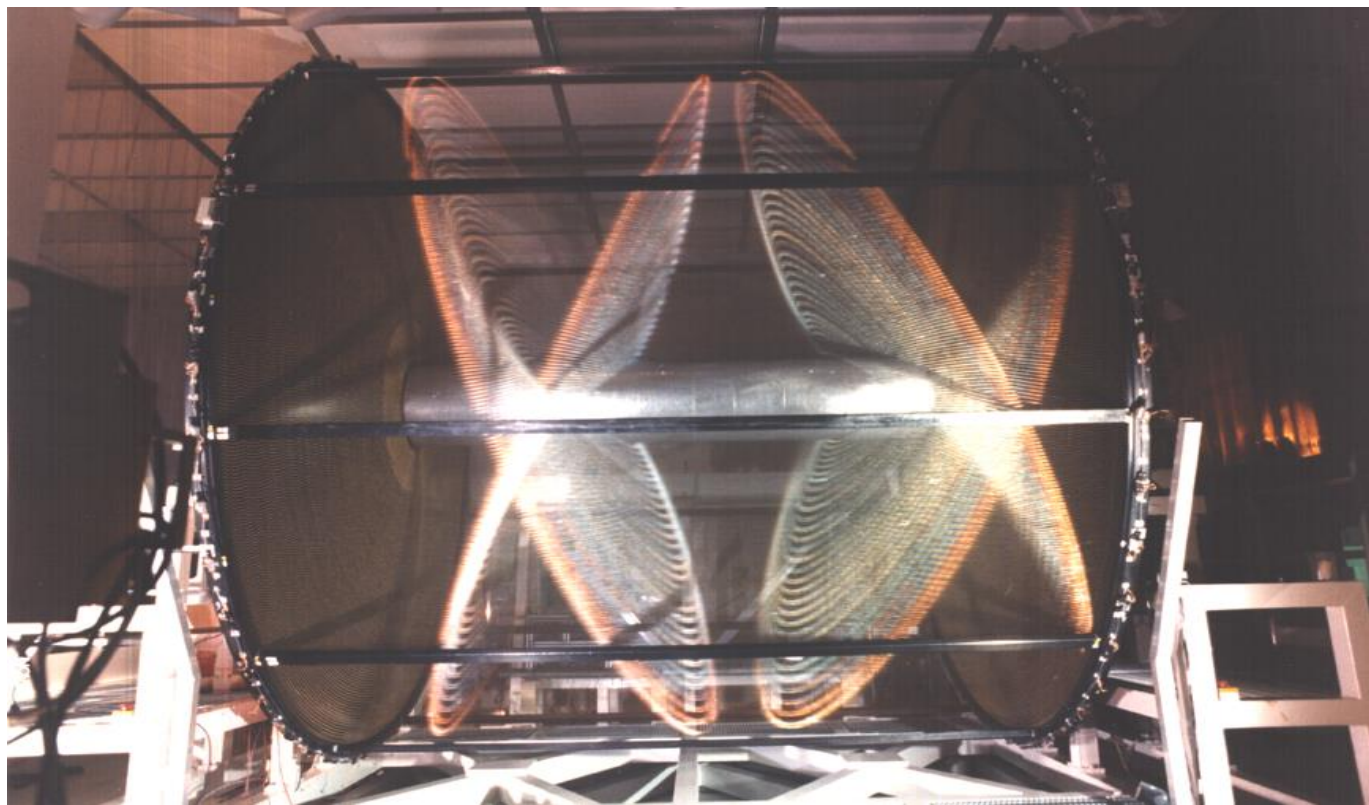
Bernardo Strozzi – Le tre Parche – Venezia, circa 1620



17 October 2016

## The KLOE Drift Chamber

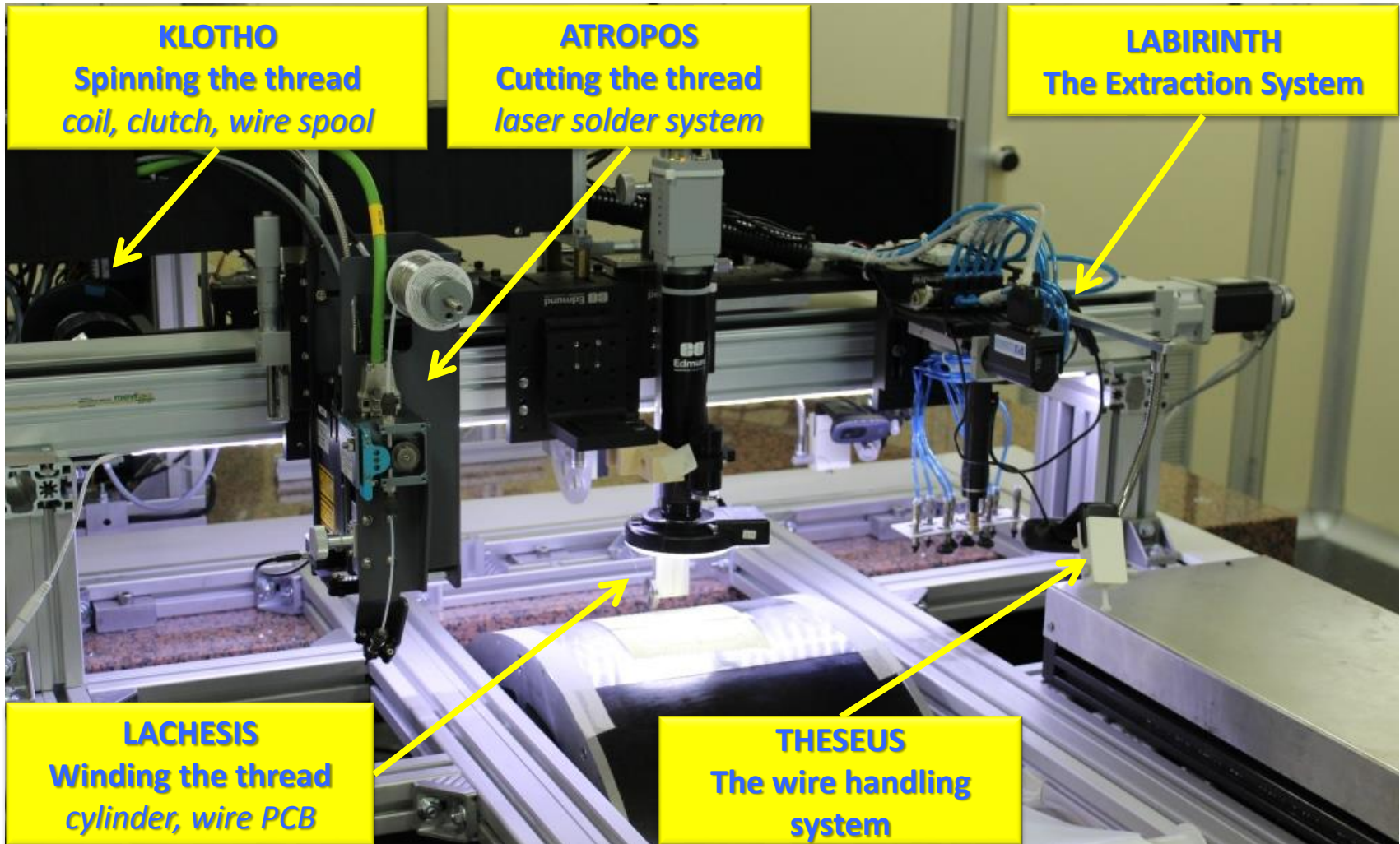
45 m<sup>3</sup> > 52,000 wires He/iC<sub>4</sub>H<sub>10</sub>



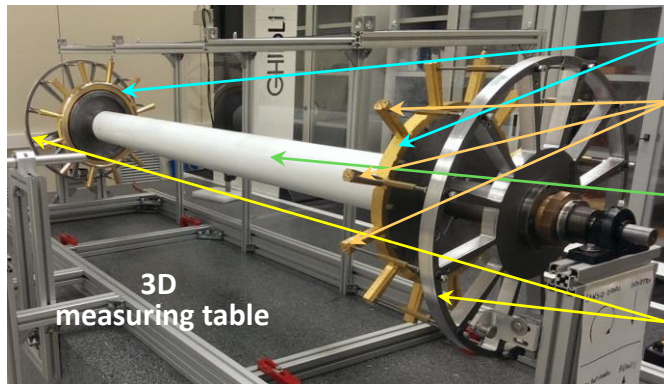
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# DC stringing: the novel way



# MEG2 DC EndPlates



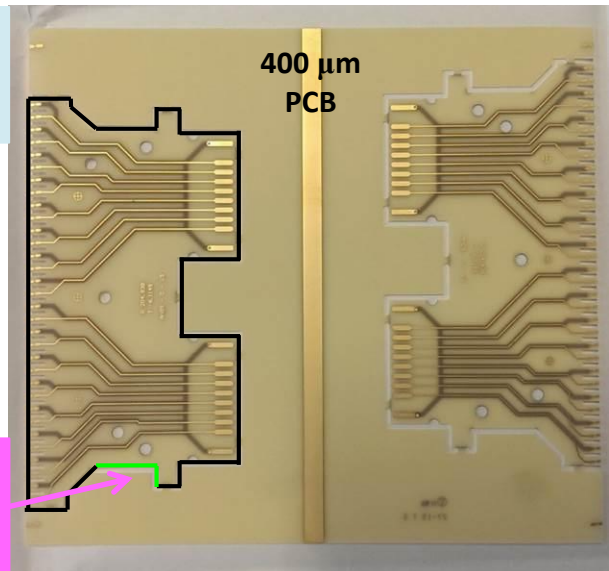
end-plates

spokes

structural  
removable  
shaft

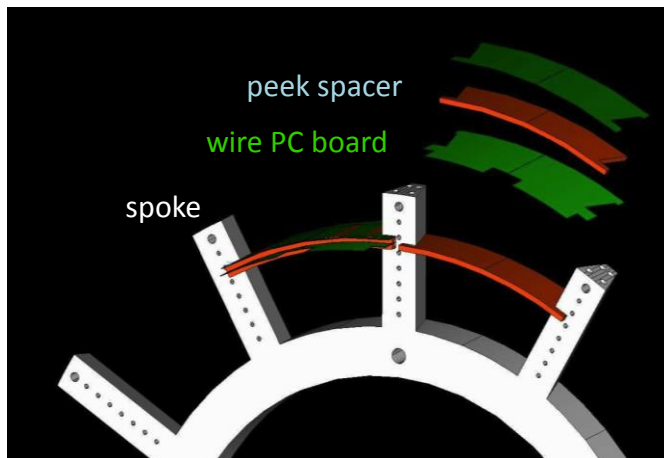
wire tension  
compensating  
wheels

sense wires  
PC boards  
(16 cells)



400 μm  
PCB

fiducial  
reference  
edge



peek spacer

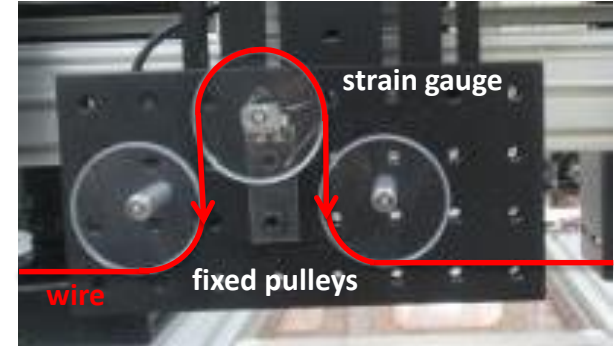
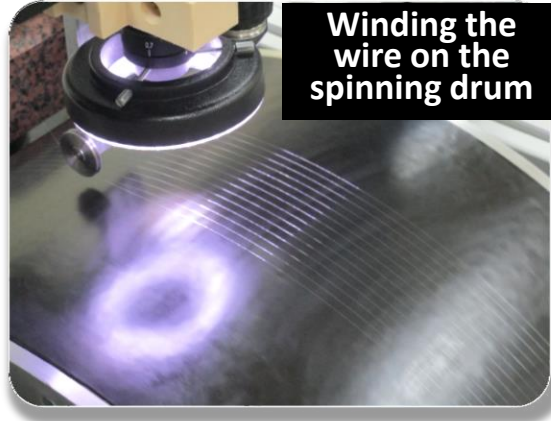
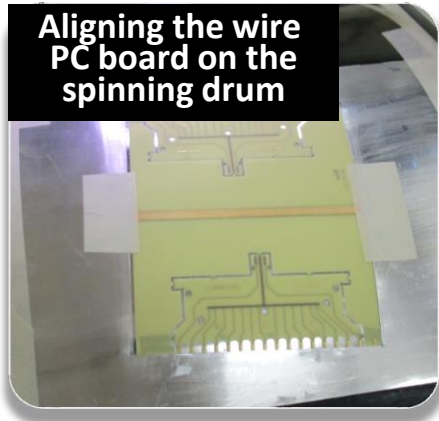
wire PC board

spoke

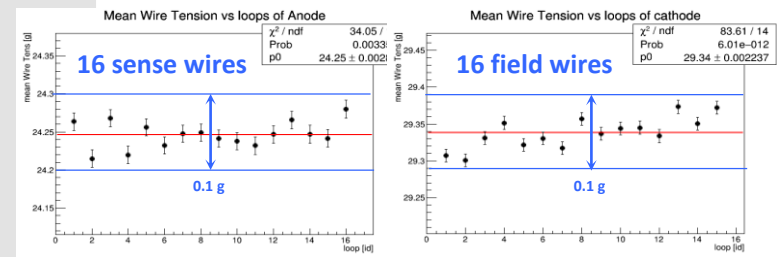
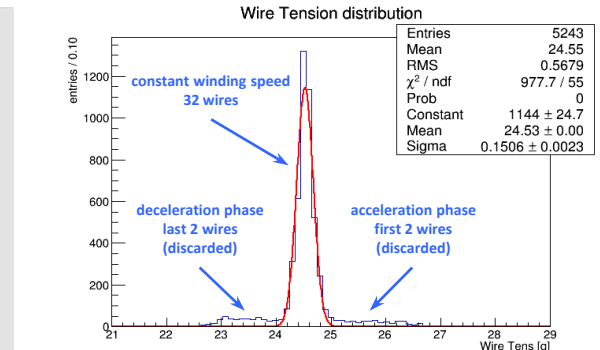
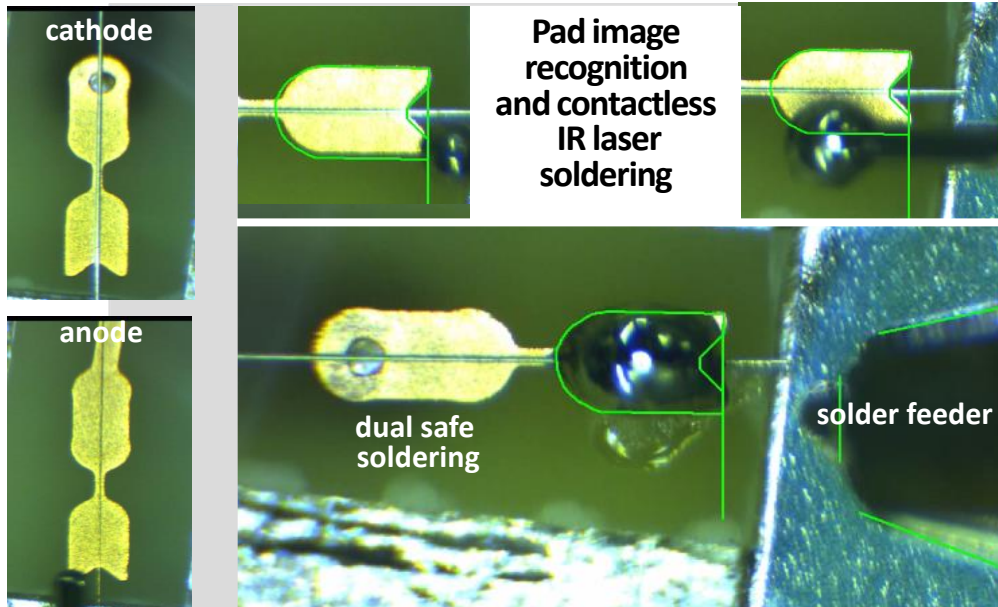
NC machined  
peek spacer  
( $\frac{1}{2}$  cell thick  
1 sector wide)



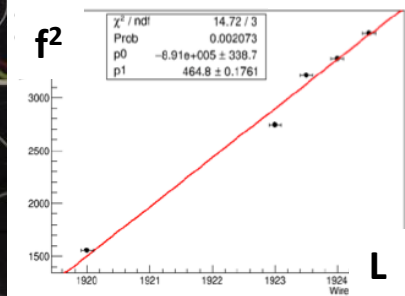
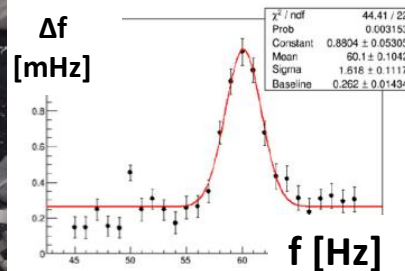
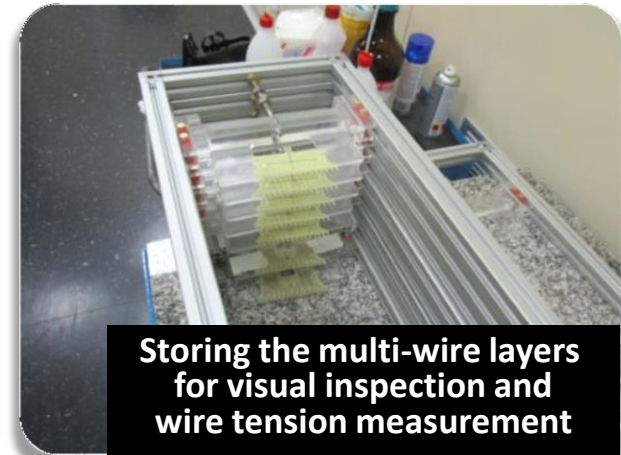
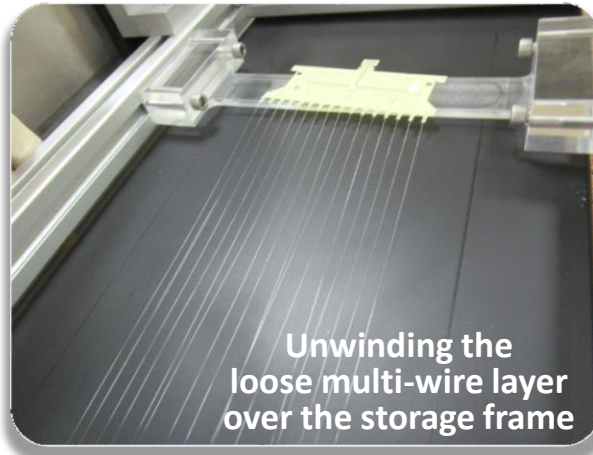
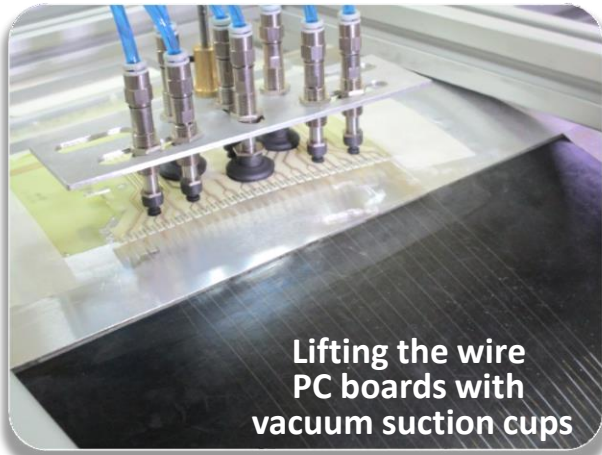
# MEG2 DC Wiring



**Wire tension set up with a real time strain gauge feedback system on the spooling el. mag. clutch**



# MEG2 DC Wiring

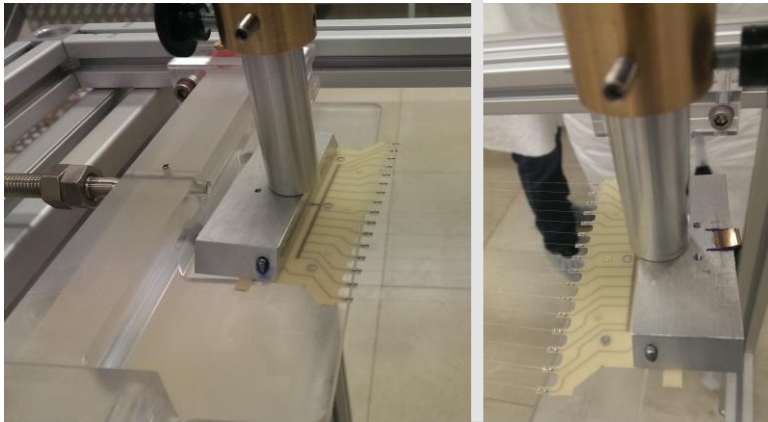


## Chamber accuracy

- stereo angle <  $35 \mu\text{rad}$
- wire position on PCB pad <  $25 \mu\text{m}$
- cell width (wire pitch) <  $1 \mu\text{m}$
- cell height (spacer) <  $50 \mu\text{m}$
- wire tension <  $0.1 \text{g}$
- PCB offset vs spoke <  $50 \mu\text{m}$
- chamber length <  $200 \mu\text{m}$

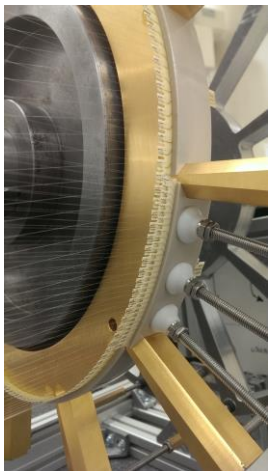
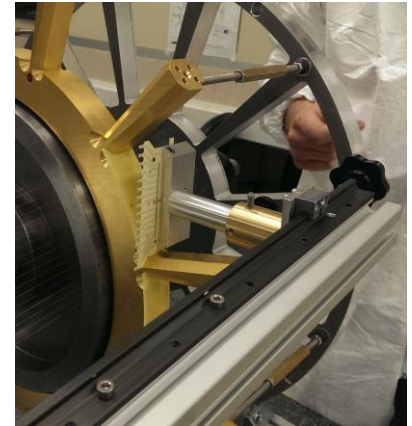


# MEG2 DC Assembly



wire PC Boards  
are lifted up by  
adjustable arm ...

... and presented to  
the end plates moved  
closer by a few mm



A pressure  
sensitive tape  
holds them in  
the correct  
position above  
the peek spacer.

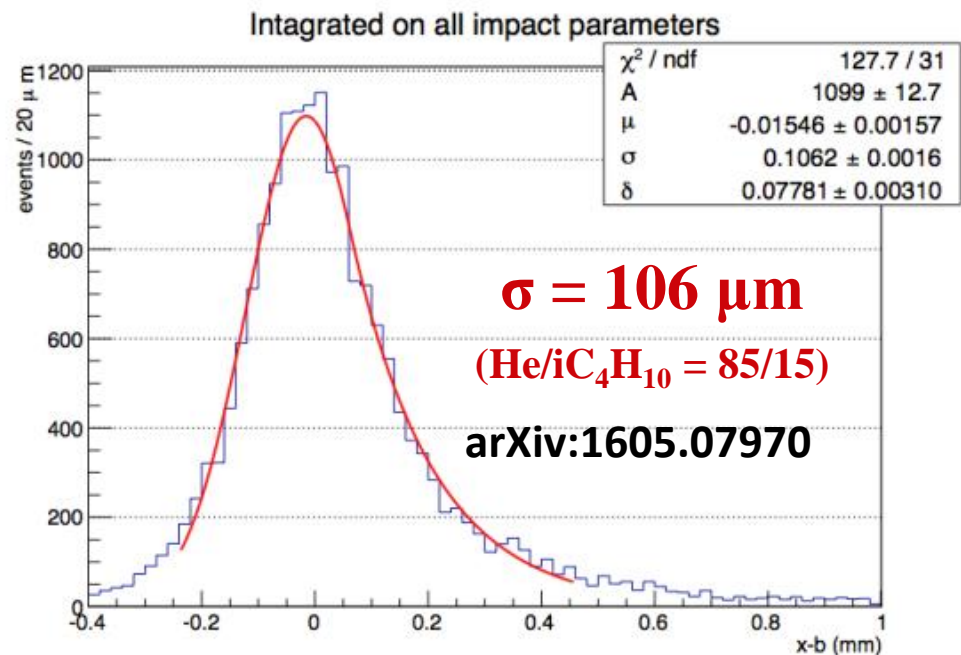
At completion of each layer (12 sectors), the end plates are moved away to the nominal length. The layer radial coordinates and the tension of all wires are then measured.

After last layer has been mounted, the outer structural carbon fiber cylindrical shell is placed and the inner shaft is removed. The end plates are sealed, the inner mylar cylinder is mounted, together with the extensions for the FEE

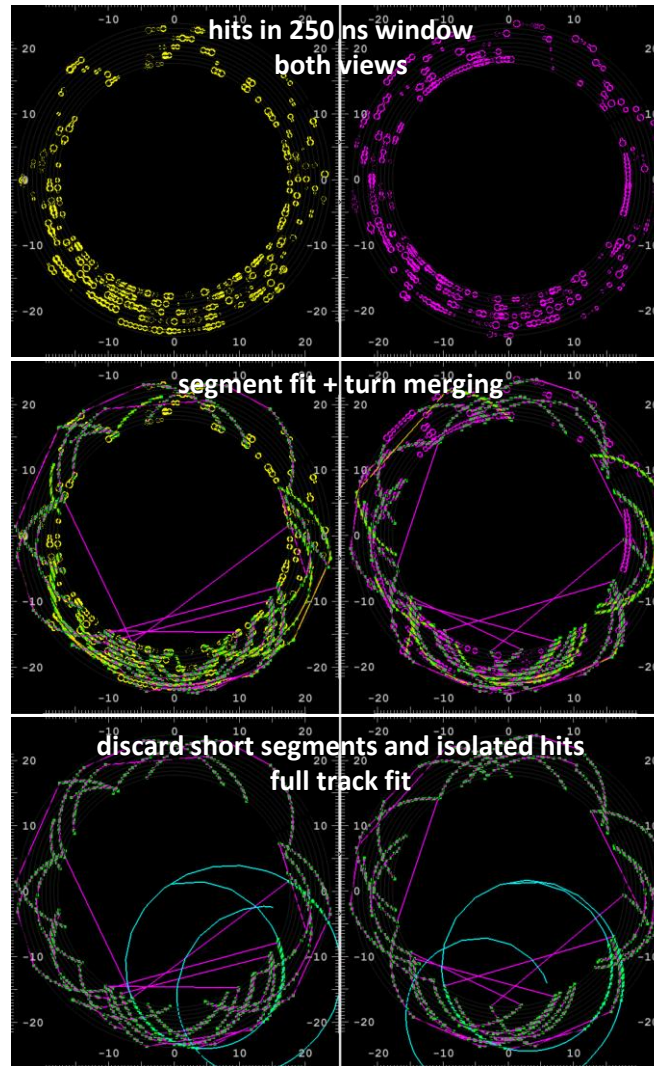
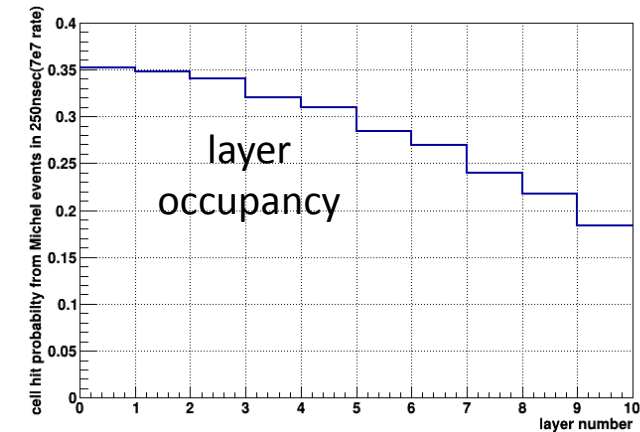
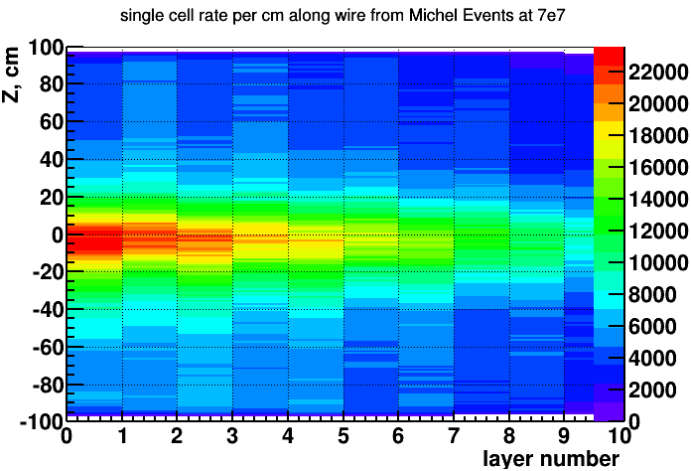
# MEG2 DC Spatial resolution

Single-hit resolution **measured** with three different prototypes. Results are all in agreement, yielding a resolution of about 110  $\mu\text{m}$  averaged throughout the cell.

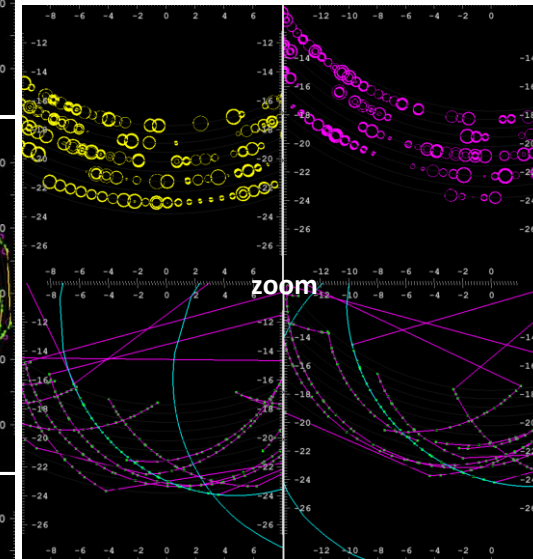
Further improvements expected thanks to the implementation of a wide bandwidth front end electronics allowing for the exploitation of the **cluster timing** technique.



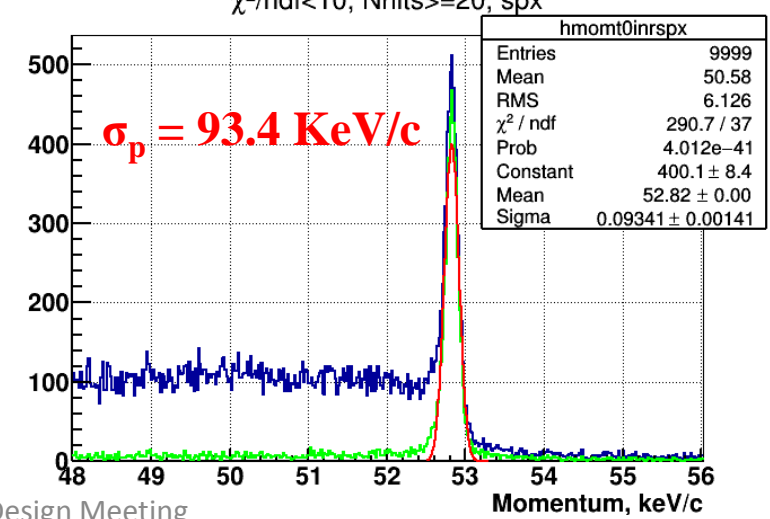
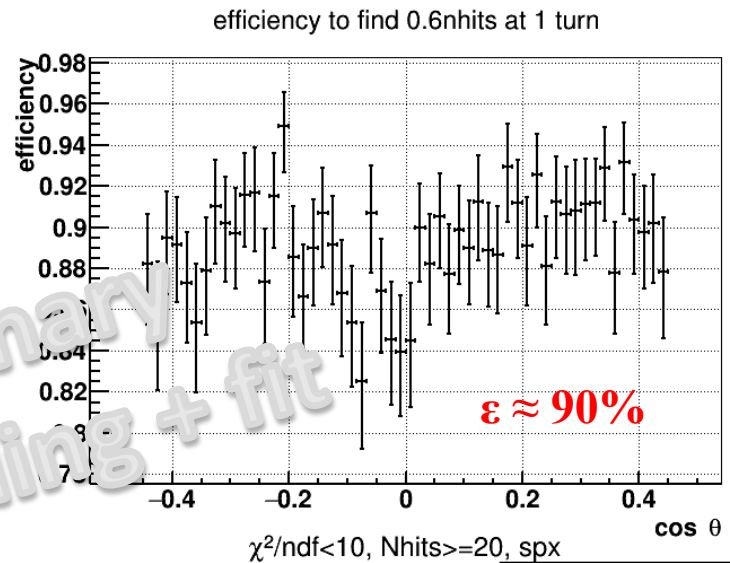
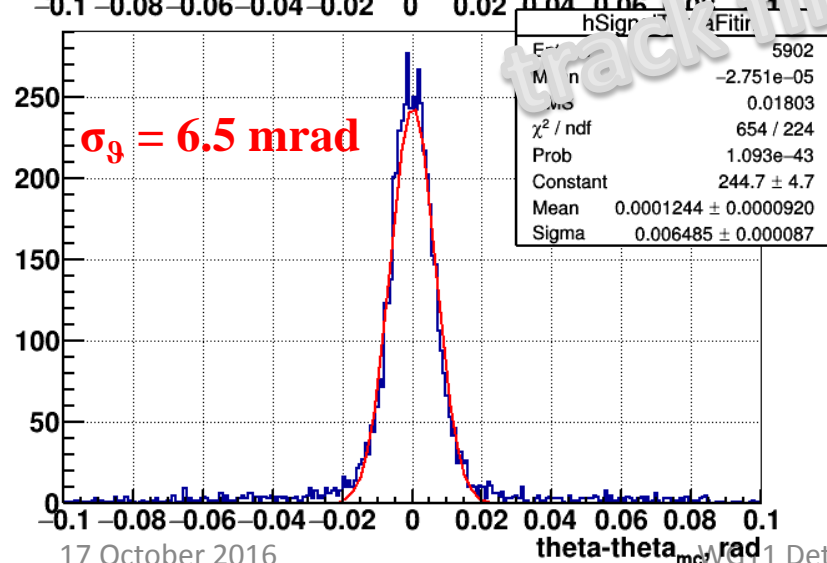
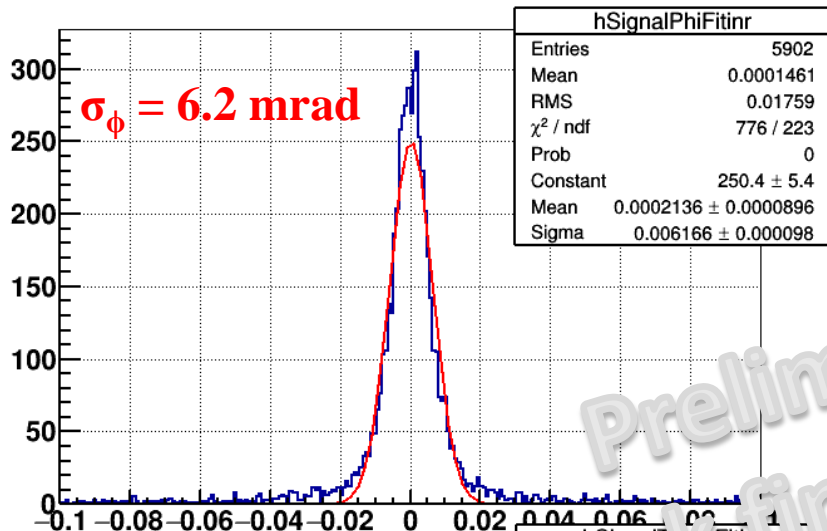
# MEG2 DC Expected Perf.



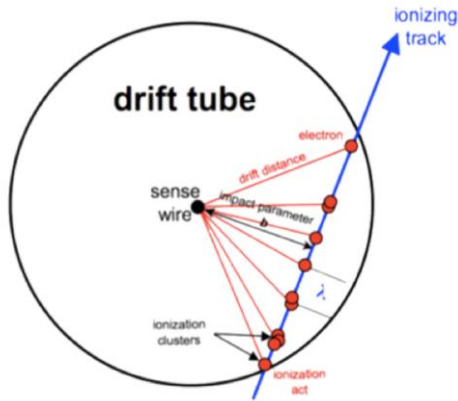
**3D**  
track finding  
and fit



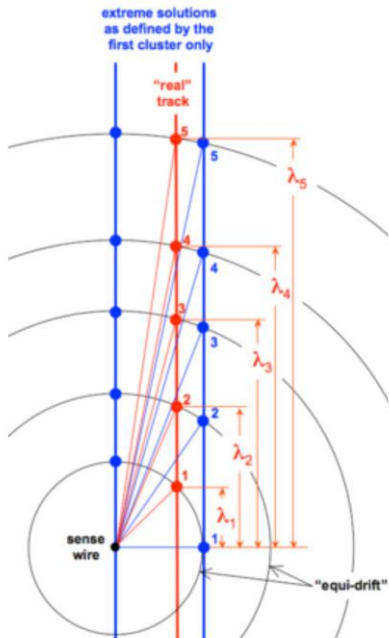
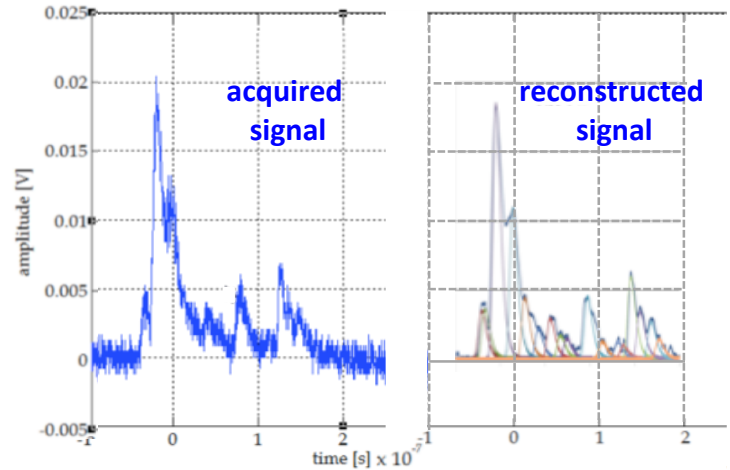
# MEG2 DC Expected Perf.



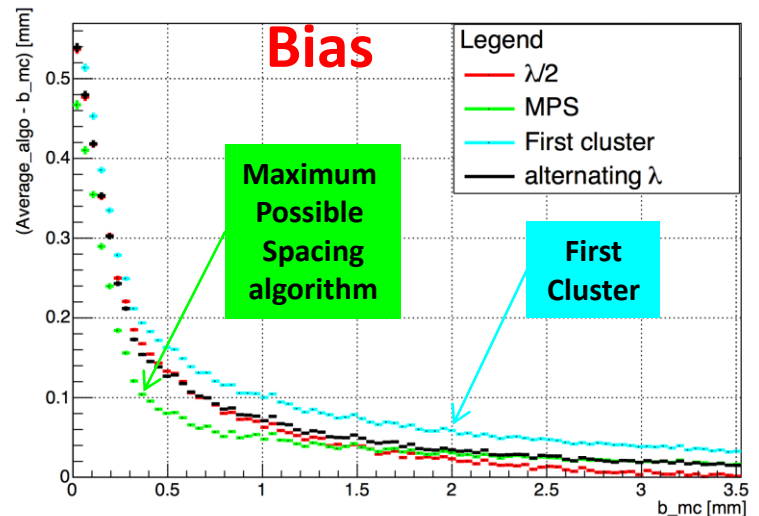
# Cluster Timing



From the **ordered sequence of the electrons arrival times**, considering the average time separation between clusters and their time spread due to diffusion, **reconstruct the most probable sequence of clusters drift times**:  $\{t_i^{cl}\} \quad i = 1, N_{cl}$

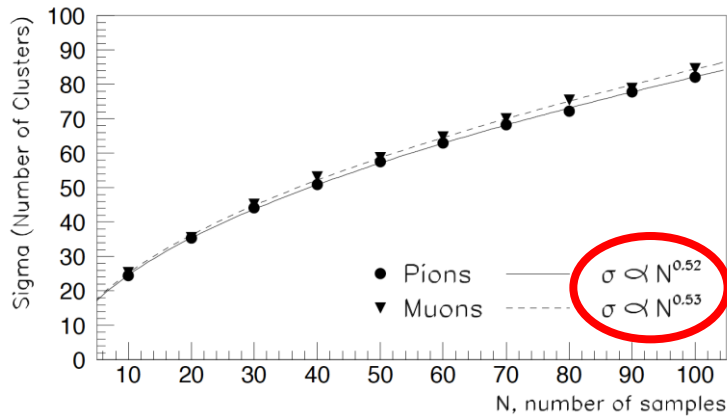


For any given first cluster (FC) drift time, the **cluster timing technique** exploits the drift time distribution of all successive clusters  $\{t_i^{cl}\}$  to determine the most probable impact parameter, thus reducing the **bias** and the average **drift distance resolution** with respect to those obtained from with the FC method alone.

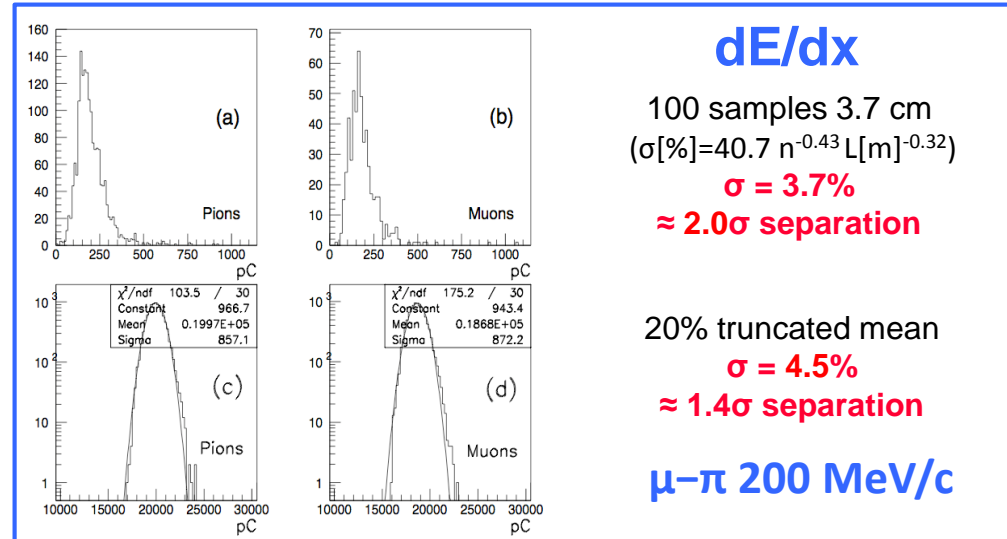


# Cluster Counting

Thanks to the **Poisson nature of the ionization process**, by counting the total number of ionization clusters  $N_{cl}$  along the trajectory of a charged track, for all the hit cells, one can reach a relative resolution of  $N_{cl}^{-1/2}$ .



The data taken with a beam of  $\mu$  and  $\pi$  at 200 MeV/c momentum at PSI, refer to a gas mixture  $He/iC_4H_{10}=95/5$ ,  $N_{cl} = 9/cm$ , 100 samples, 2.6cm each at  $45^\circ$  (to avoid space charge effects), for a total track length of 3.7 m. A 25  $\mu m$  sense wire (gas gain  $2 \times 10^5$ ), readout through a high bandwidth (1.7 GHz, gain 10) preamplifier, is digitized with a 2 GSa/s 1.1 GHz, 8 bits digital scope. (NIM A386 (1997) 458-469 and references therein)

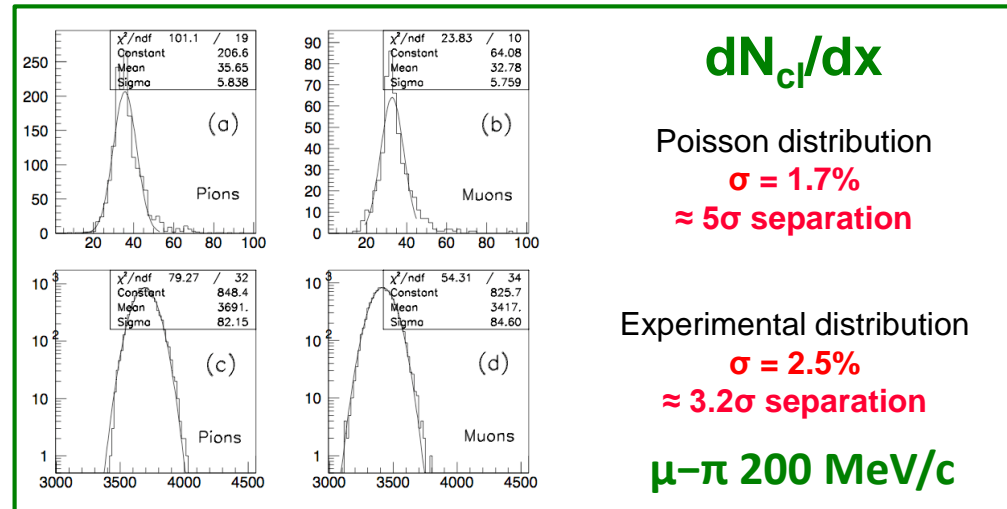


**dE/dx**

100 samples 3.7 cm  
 $(\sigma[\%]=40.7 n^{-0.43} L[m]^{-0.32})$   
 $\sigma = 3.7\%$   
 $\approx 2.0\sigma$  separation

20% truncated mean  
 $\sigma = 4.5\%$   
 $\approx 1.4\sigma$  separation

$\mu-\pi$  200 MeV/c



**dN<sub>cl</sub>/dx**

Poisson distribution  
 $\sigma = 1.7\%$   
 $\approx 5\sigma$  separation

Experimental distribution  
 $\sigma = 2.5\%$   
 $\approx 3.2\sigma$  separation

$\mu-\pi$  200 MeV/c

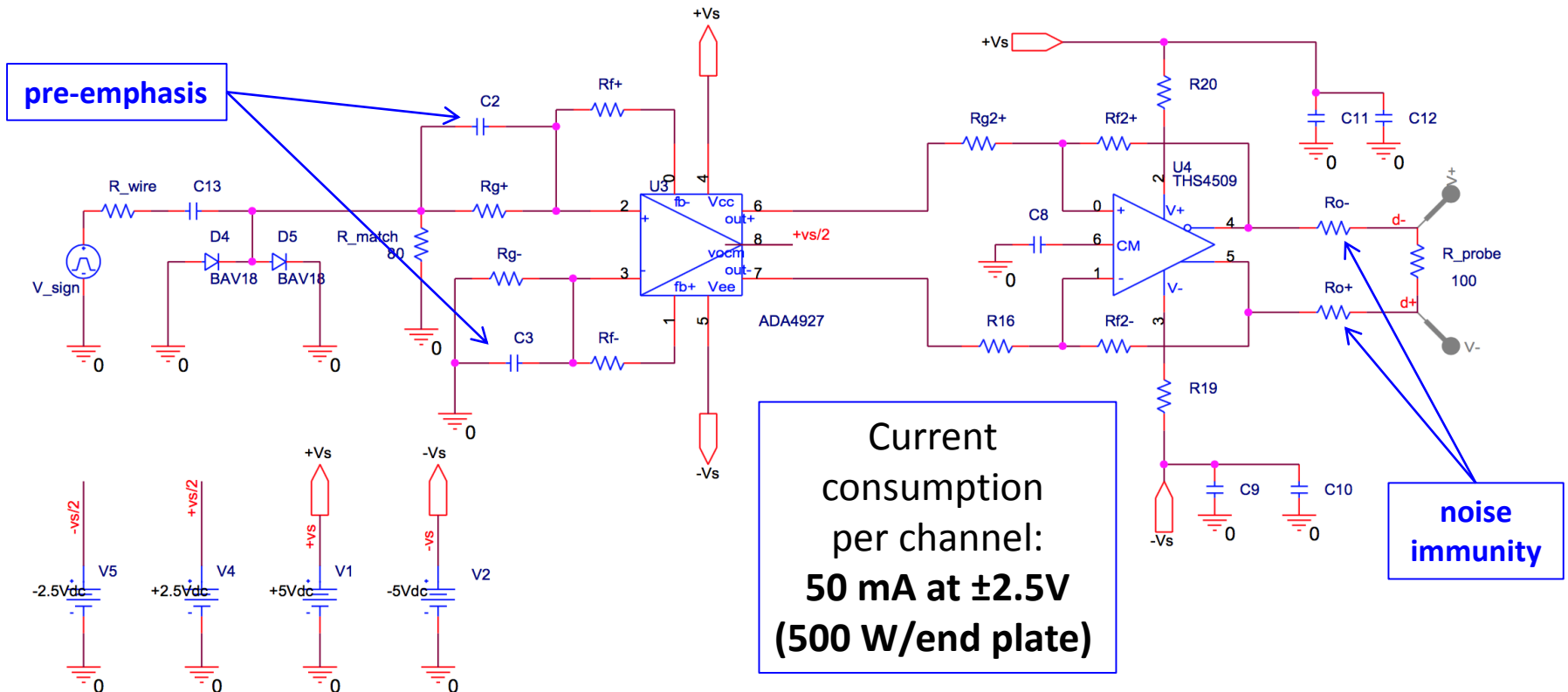
# "Innovative DC" advantages

- **Gas containment** – **wire support** separation and **feed-through-less wiring**
  - allow to reduce material to  $\approx 10^{-3} X_0$  for the inner cylinder and to a few  $\times 10^{-2} X_0$  for the end-plates, including FEE, HV supply and signal cables (Mu2e proposal design:  $1.5 \times 10^{-3} X_0$  and  $8 \times 10^{-3} X_0$ , respectively).
- **Feed-through-less wiring**
  - allows to increase **chamber granularity** and field/sense wire ratio to reduce **multiple scattering** and **total tension on end plates** due to wires
- **Cluster timing**
  - allows to reach **spatial resolution  $< 100 \mu\text{m}$**  for 8 mm drift cells in He based gas mixtures (such a technique is going to be implemented in the MEG2 drift chamber under construction)
- **Cluster counting**
  - allows to reach  **$dN_{cl}/dx$  resolution  $< 3\%$**  for particle identification (a factor 2 better than  $dE/dx$  as measured in a beam test)

**Recipe for cluster timing/counting in He based gas mixtures:**

**FEE: 1 GHz BW, x10 gain (S/N ratio  $\approx 8$ ) - digitizer: 2 GSa/s sampling rate,  $>8$  bits**

# MEG2 DC Front End El.

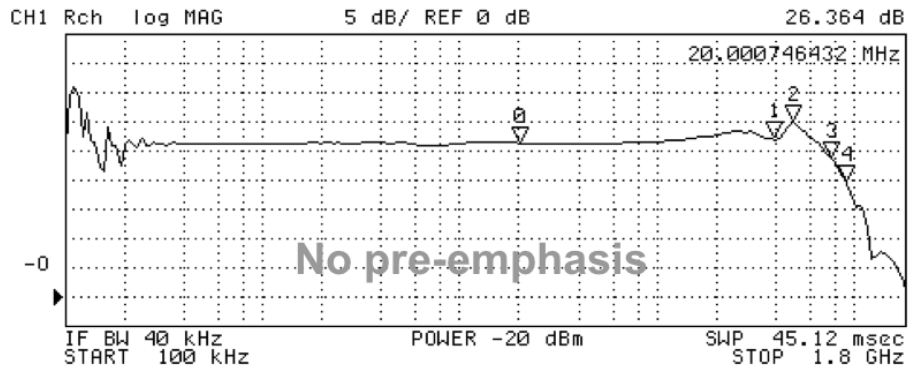


Op-amp **ADA4927** first gain stage: low noise, ultralow distortion, high speed, current feedback differential amplifier achieving wide bandwidth, low distortion, and low noise (1.3 nV/√Hz) and low power consumption.

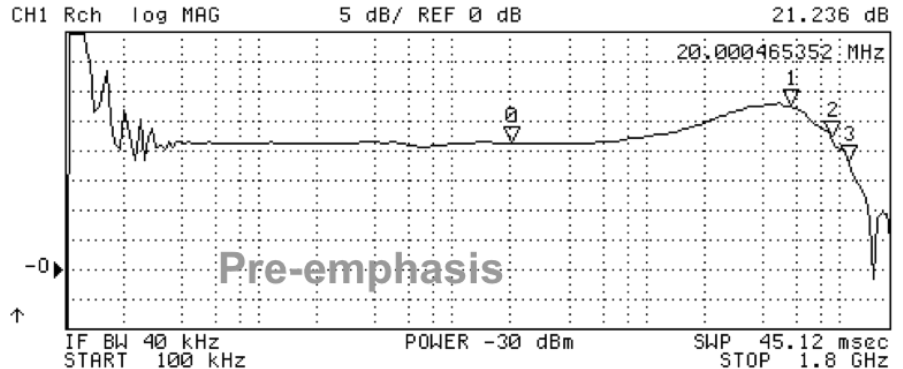
**THS4509** second gain stage and output driver: wideband, fully differential op-amp, very low noise (1.9 nV/√Hz), extremely low distortion, ideal for pulsed applications.



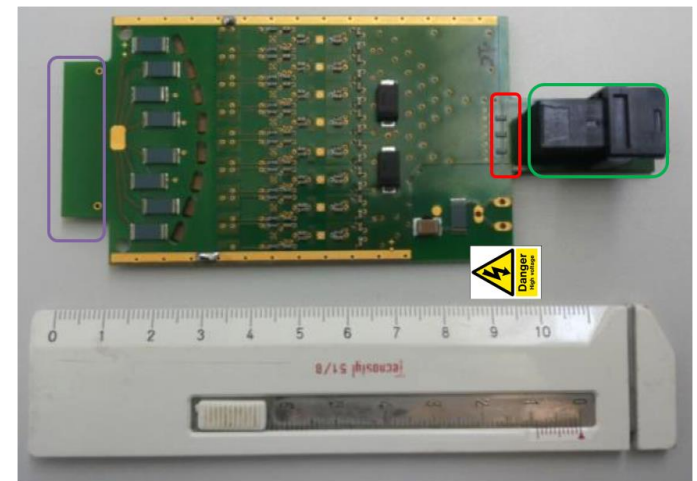
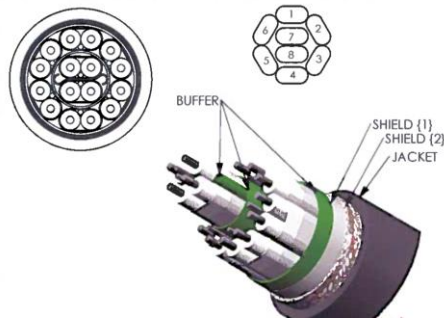
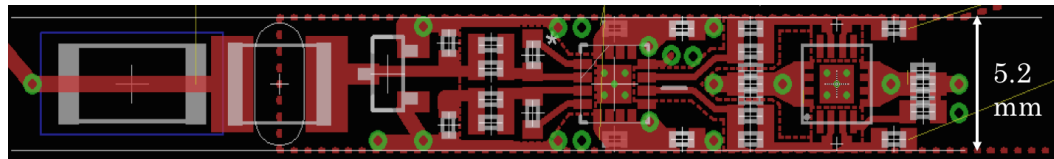
# MEG2 DC Front End El.



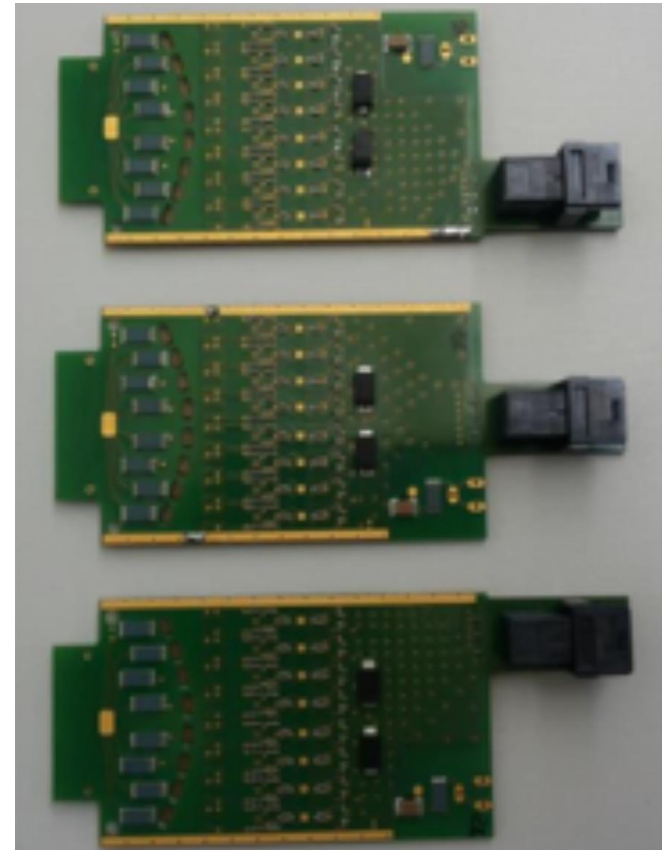
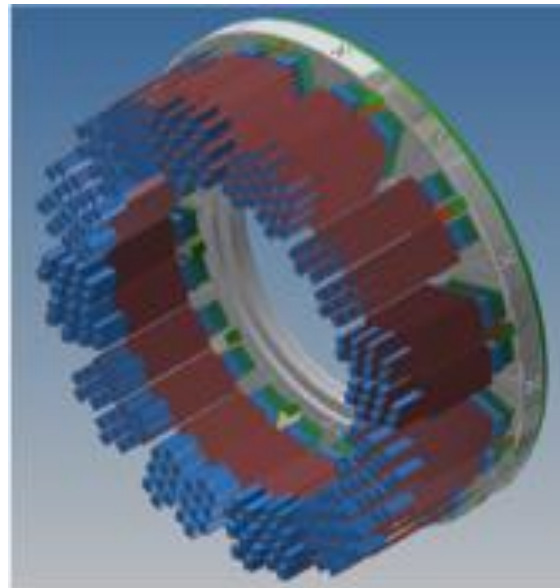
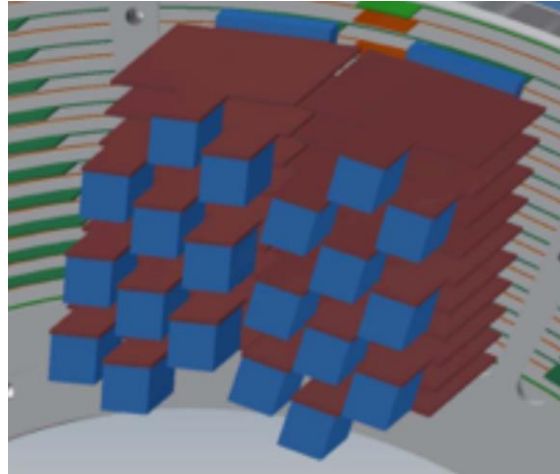
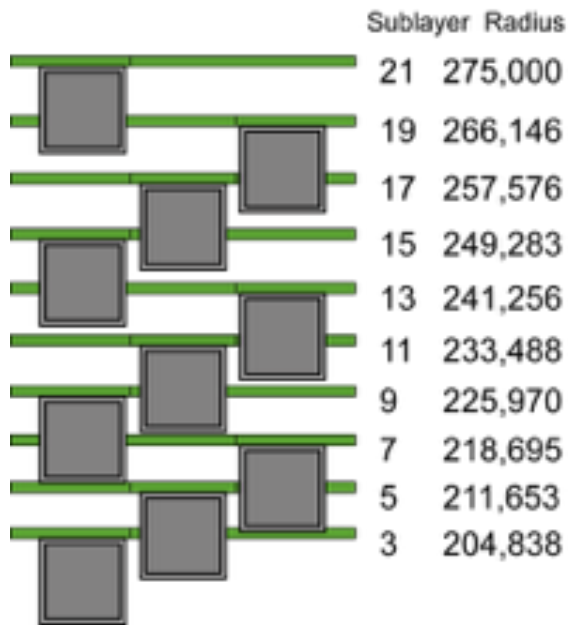
N	SWP PARAM	VAL
0	20.000746432 MHz	26.364 dB
1	387.431573185 MHz	27.042 dB
<b>Peak 2</b>	484.430980668 MHz	29.955 dB
<b>BW 3</b>	756.290673874 MHz	23.666 dB
4	899.763007493 MHz	19.788 dB



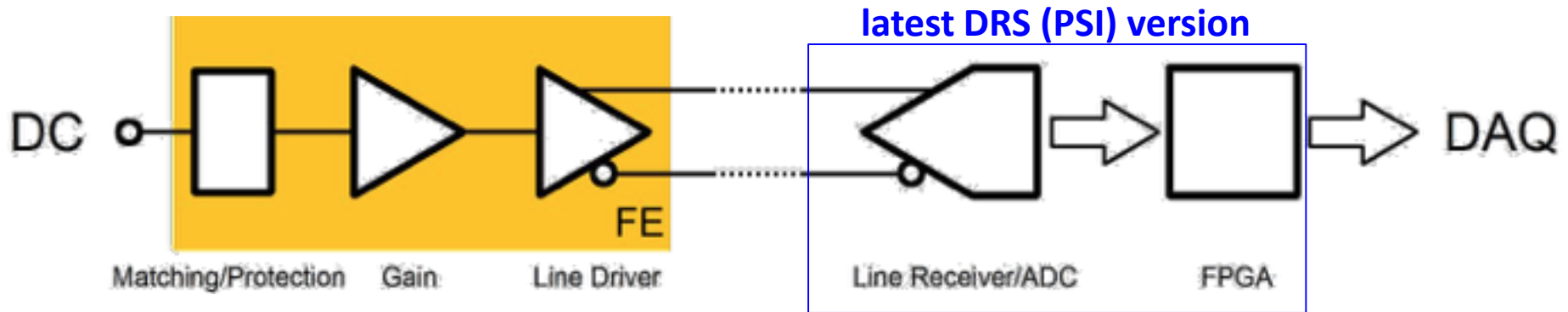
N	SWP PARAM	VAL
0	20.000465352 MHz	21.236 dB
1	554.109452707 MHz	27.458 dB
<b>Peak 2</b>	899.74895028 MHz	22.206 dB
<b>BW 3</b>	1.099455926016 GHz	18.203 dB



# MEG2 DC Front End El.

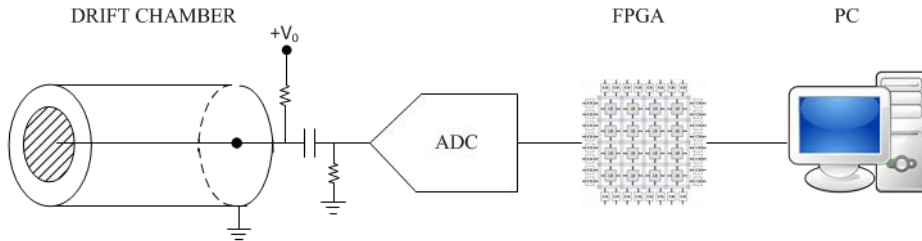


# MEG2 DC Read Out

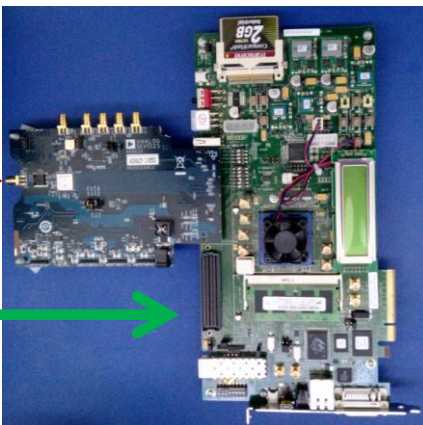


More generally, in a large DCH (60,000 channels, 30% occupancy, 1  $\mu$ s drift time, 2 GSa/s - 12 bits digitization), at a 5 kHz trigger rate, expect: **> 100 GB/s!**

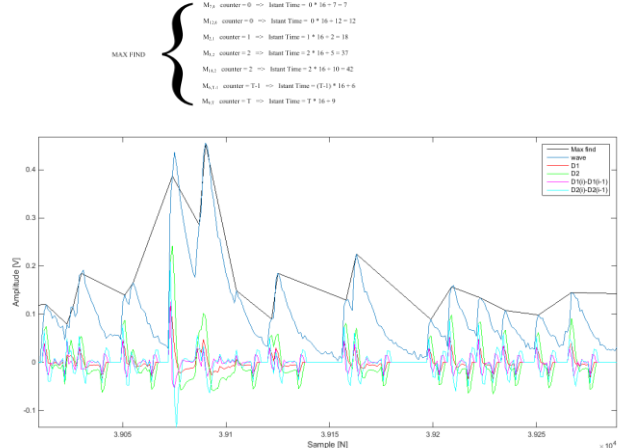
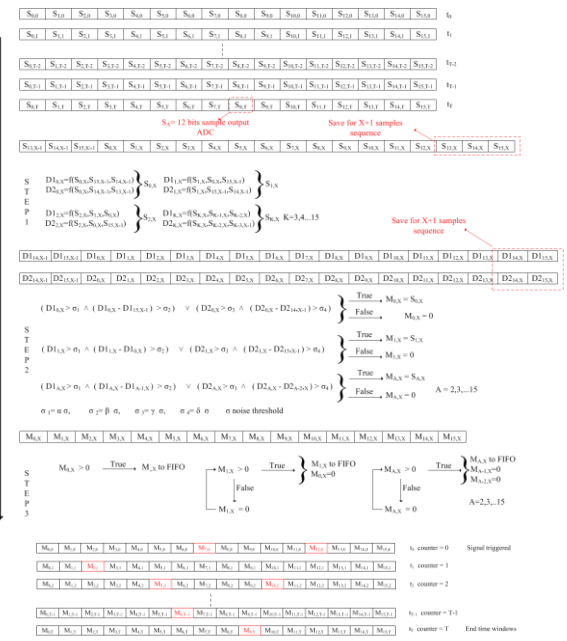
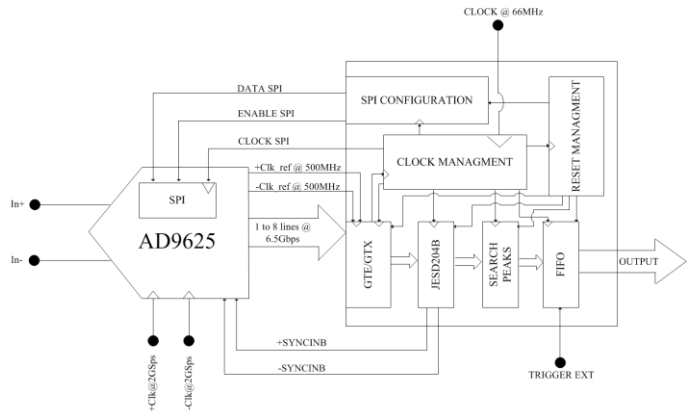
# Clu-Tim/Cou Read Out



**ANALOG DEVICES**  
AD9625-2.0EBZ



**XILINX**  
UG534 ML605



# How long a drift chamber can be?

## Gravitational sag

wire L along x-axis, f force per unit length along y, T tension of wire

$$f \times dx = T \frac{d^2 y}{dx^2} dx$$

f independent of x, parabolic solution

$$y = ax^2 \quad \text{or} \quad y = \frac{T}{2f} x^2$$

sag  $d = \frac{f}{8T} L^2$

wire radius r, volume density  $\rho$ , gravitational sag

$$f = \rho r^2 g \quad \text{or} \quad d = \frac{\rho r^2 g}{8T} L^2$$

### Example:

L=2m; sense: 20 $\mu$ m W(Au), T=27g; field: 40 $\mu$ m Al(Ag), T=17g; guard: 50 $\mu$ m Al(Ag), T=26.5g

$$d_{\text{sense}} = 110 \text{ mm}$$

$$d_{\text{field}} = 110 \text{ mm}$$

$$d_{\text{guard}} = 110 \text{ mm}$$

# How long a drift chamber can be?

## Electrostatic stability

Simplified model of a wire of radius  $R$  at voltage  $V_0$ , placed between two parallel grounded planes at distance  $W/2$  from the wire

linear charge density

$$\lambda = \frac{2peV_0}{\ln\left(\frac{2W}{2R}\right)}$$

assume a wire displacement  $\Delta$  towards one plane

$$f = \frac{2C^2V_0^2}{peW^2} D$$

cap. per unit length

$$C = \frac{2pe}{\ln\left(\frac{2W}{2R}\right)}$$

$$d = \frac{f}{8T} L^2 = \frac{C^2V_0^2L^2}{4peTW^2} D$$

perfectly symmetric geometry

$$f = 0$$

$$\frac{d}{D} < 1 \Rightarrow T > \frac{C^2V_0^2L^2}{4peW^2}$$

**stability  
condition**

# How long a drift chamber can be?

## Electrostatic stability: a numerical example MEG2

20 $\mu$ m W sense wire,  $V_0 = 1500V$ ,  $W = 7mm$ ,  $L = 2m$ ,  $T = 0.25N$

linear charge density  $\lambda = 1.3 \cdot 10^{-8} \text{Coul} / m$  assume a wire displacement  $\Delta = 50 \mu m$

cap. per unit length  $C = 8.5 pF / m$   $f = 1.2 \cdot 10^{-5} N$   $d = 24 mm$

**stability condition**  $T > 0.12 N$  or  $L < 2.8 m$

increase sense wire diameter to **50 $\mu$ m**,  $T = 1.56N$ , for the same gain (same  $\lambda$ ) need  **$V_0 = 1750V$**

$C = 9.9 pF / m$   $f = 2.2 \cdot 10^{-5} N$   $d = 7.0 mm$   $T > 0.22 N$  or  $L < 5.3 m$

**drawback:**

**multiple scattering** and **force on end plates** increase by a factor **2.5<sup>2</sup>**  
(Ti(Sn) instead of W(Au)? to regain a factor 4 in mass and 10 in  $X_0$ )

# A proposal for FCCee

- **112 para-axial layers** at alternating sign stereo angles, arranged in **16 equal azimuthal sectors**;
- **32 square, single sense wire, drift cells** per sector (512 total per layer) increasing linearly as a function of layer radius;
- **Cell sizes** ranging from **6.3 mm to 25 mm** from inner to outer radius;
- **Alternating sign stereo angles** in consecutive layers ranging from **40 to 160 mrad** (constant azimuthal angular displacement)
- **Length: 5000 mm**; fully efficient up to  **$\cos\vartheta = 0.97$**  ( $\geq 16$  hit)
- **Inner Wall**: made of 25  $\mu\text{m}$  of Kapton plus 0.1 $\mu\text{m}$  of Au ( **$1.2 \times 10^{-4} X_0$** ) at **Radius = 500 mm**;
- **Outer Wall**: Sandwich of 8-ply C-fiber (0° and 90°, total of 250  $\mu\text{m}$ ) - 2.5 mm Rohacell30 - 8-ply C-fiber ( **$8.0 \times 10^{-3} X_0$** ) at **Radius = 2060 mm** (must support **20 Tons** - check for buckling over 5 m);
- **End plates:**
  - **Wire cage** (in analogy to Mu2e I-Tracker):  
0.9 g/cm<sup>2</sup> -  **$3 \times 10^{-2} X_0$**  (incl. power distr., decoupling C's, term. resistors and signal and HV cables).
  - **Gas envelope** made of 8 ply (quasi-isotropic, 10×38  $\mu\text{m}$  = 380  $\mu\text{m}$ ) C-fiber plus 0.3  $\mu\text{m}$  Au, for a total of 0.090 g/cm<sup>2</sup> -  **$3.0 \times 10^{-3} X_0$** ;
- **Gas: 90% He - 10% iC<sub>4</sub>H<sub>10</sub>** ( $\delta = 4 \times 10^{-4}$  g/cm<sup>3</sup>,  $X_0 = 1410$  m), - 12.5 p.i./cm, gas gain:  $4 \times 10^5$  at  $V \approx 1700$  V on 50  $\mu\text{m}$  wire,  $v_{\text{drift}} \sim 2.5$  cm/ $\mu\text{s}$  -  **$0.47 \times 10^{-3} X_0/1\text{m track}$**
- **Wires:** - **57,344 sense** (50 $\mu\text{m}$  Sn coated Ti); **290,816 field and guard** (100 $\mu\text{m}$  Sn coated C); for a total equivalent thickness of  **$1.34 \times 10^{-3} X_0/1\text{m track}$**



# Expected spatial resolution

## Expected Performance: Track parameters resolutions

$n = 112$ ,  $B = 2.0$  T,  $R_{out} = 2.05$  m,  $L = 3.0$  m or  $5.43 \times 10^{-3} X_0$ ,  $\sigma_{xy} = 100$   $\mu\text{m}$ ,  $\sigma_z = 1.0$  mm

measurement

$$\frac{Dp_{\wedge}}{p_{\wedge}} = \frac{8\sqrt{5}S}{.3BL^2\sqrt{n}} p_{\wedge} = 7.1 \times 10^{-5} p_{\wedge} [\text{GeV}/c]$$

$$Df_0 = \frac{4\sqrt{3}S}{R_{out}\sqrt{n}} = 4.0 \times 10^{-5}$$

$$Dq = \frac{\sqrt{12}S_z}{R_{out}\sqrt{n}} \frac{1 + \tan^2 q}{\tan^2 q} = 2.1 \times 10^{-4} \frac{1 + \tan^2 q}{\tan^2 q}$$

multiple scattering (gas + wires)

$$\frac{Dp_{\wedge}}{p_{\wedge}} = \frac{0.0523 [\text{GeV}/c]}{bpBL \sin q} \sqrt{\frac{L}{X_0}} = \frac{5.5 \times 10^{-4} [\text{GeV}/c]}{bp \sin q}$$

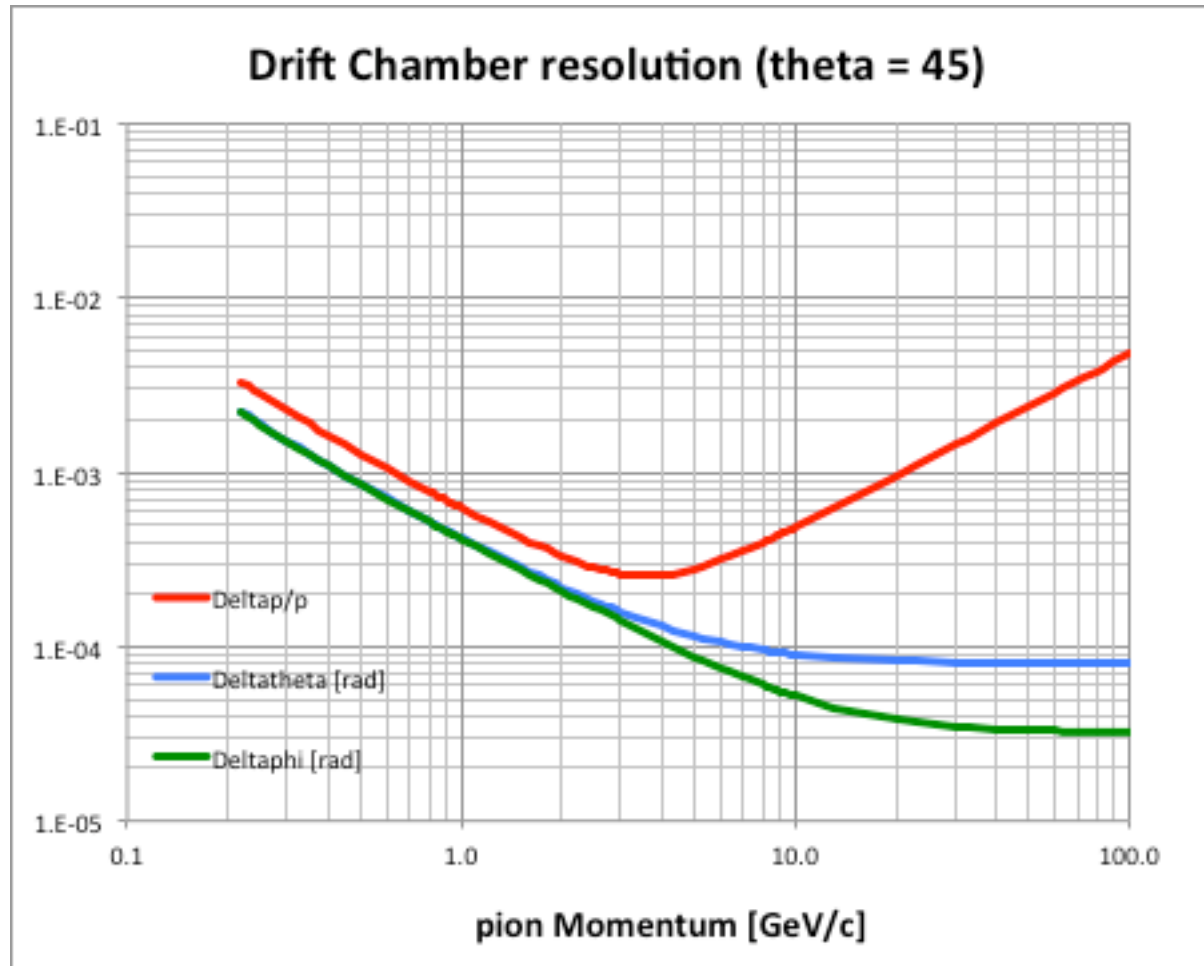
$$Df_0 = \frac{13.6 \times 10^{-3} [\text{GeV}/c]}{bp} \sqrt{\frac{L}{X_0}} = \frac{1.0 \times 10^{-3} [\text{GeV}/c]}{bp}$$

$$Dq = \frac{13.6 \times 10^{-3} [\text{GeV}/c]}{bp} \sqrt{\frac{L}{X_0}} = \frac{1.0 \times 10^{-3} [\text{GeV}/c]}{bp}$$

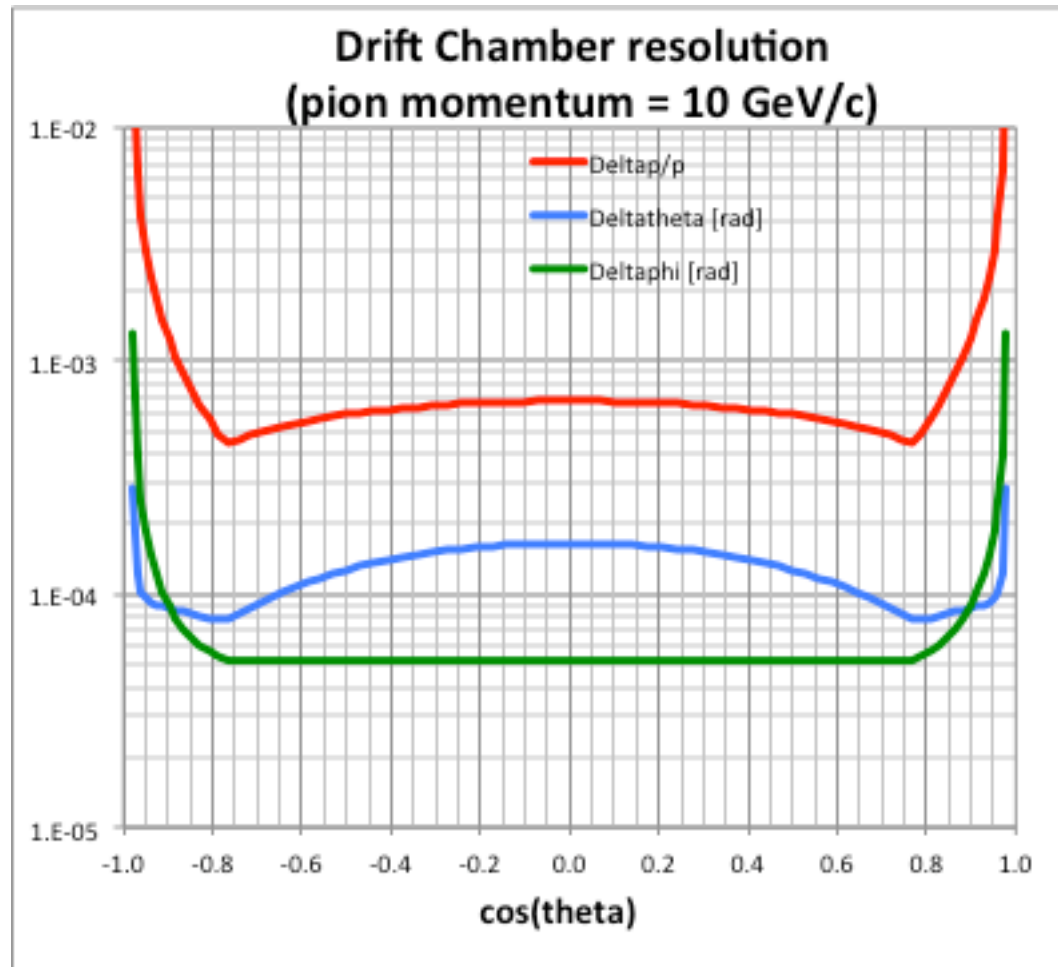
$$\frac{Dp_{\wedge}}{p_{\wedge}} = 5.8 \times 10^{-4}; \quad \frac{Dp}{p} = \frac{Dp_{\wedge}}{p_{\wedge}} \oplus \frac{Dq}{\tan q} = 6.1 \times 10^{-4}$$

for  $p = 10$  GeV/c and  $q = 45^\circ$

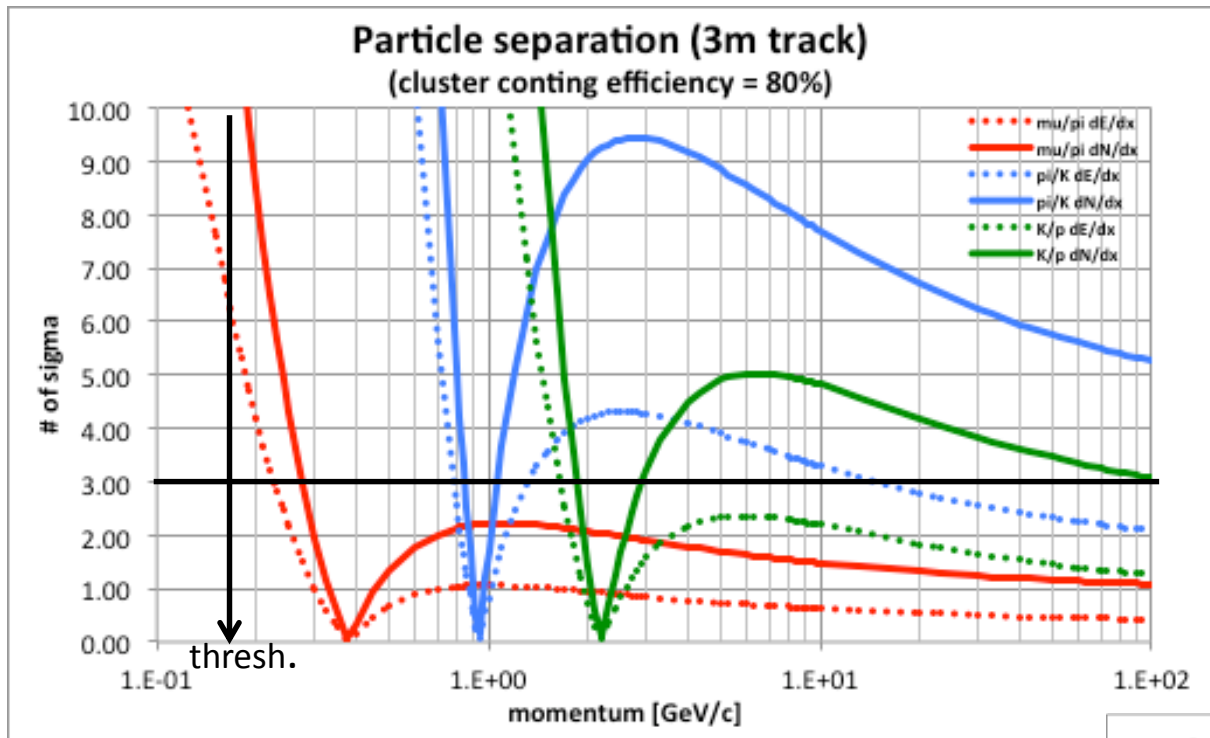
# Expected spatial resolution



# Expected spatial resolution



# Expected p. id. capabilities



$$\sigma_{dE/dx}/dE/dx =$$

$$= 5.4 L[m]^{-0.37} \%$$

(Lehraus parametrization)

$$3.6\% \text{ for } L=3m$$

cluster counting efficiency

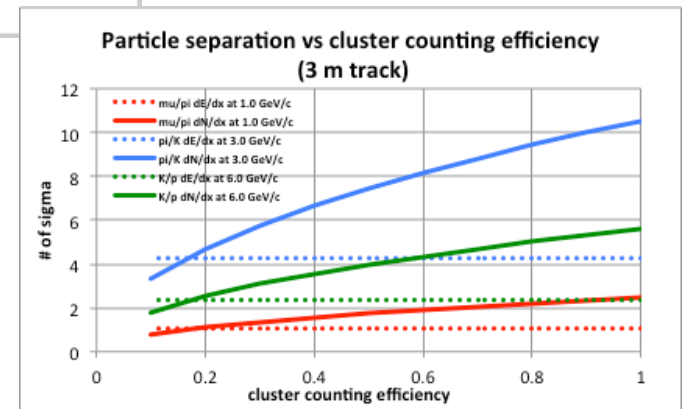
$$\varepsilon = 80\%$$

$$\sigma_{dN_{cl}/dx}/dN_{cl}/dx =$$

$$= \varepsilon \times L \times 12.5/cm =$$

$$1.8\% \text{ for } L=3m$$

Particle separation power as a function of cluster counting efficiency for 2m tracks.  
Cluster counting outperforms dE/dx for counting efficiencies as low as 20%.



# Conclusions

- We propose for FCCee an innovative tracking system based on a **"ultra-light drift chamber with peculiar particle identification capabilities"** using cluster timing/counting techniques.
- It consists of a full stereo, single sense wire, square cells:
  - $R_{in} = 50 \text{ cm}$ ;  $R_{out} = 205 \text{ cm}$ ;  $L = 500 \text{ cm}$ ; **112 layers  $\times$  (6.3 to 25.0 mm)**; **57,344 cells**;  $>16$  hits down to  **$\cos\vartheta = 0.97$** ; stereo angles ranging from **40 mrad to 160 mrad**;
  - Inner cylindrical wall:  **$1.2 \times 10^{-4} X_0$**
  - Outer cylindrical wall:  **$8.0 \times 10^{-3} X_0$**
  - End plates (fully instrumented):  **$3.3 \times 10^{-2} X_0$**
  - Gas + wires:  **$.47 \times 10^{-3} X_0/1\text{m track} + 1.34 \times 10^{-3} X_0/1\text{m track}$**
- Expected spatial resolutions:  **$\sigma_{r\varphi} < 100 \mu\text{m}$ ,  $\sigma_z < 1 \text{ mm}$**
- Expected momentum resolution:  **$\Delta p/p = 4.9 \times 10^{-4}$ ,  $\Delta\vartheta = 0.9 \times 10^{-4}$ ,  $\Delta\varphi = 0.5 \times 10^{-4}$**  for  $p = 10 \text{ GeV}/c$  and  $\vartheta = 45^\circ$
- Expected p. id.:  $\pi/k$  separation  **$> 3\sigma$  for  $p < 850 \text{ MeV}/c$  and  $p > 1070 \text{ MeV}/c$**

**At current status of the art no need for major R&D**