

Nb-coated copper crab cavity alternative for FCC

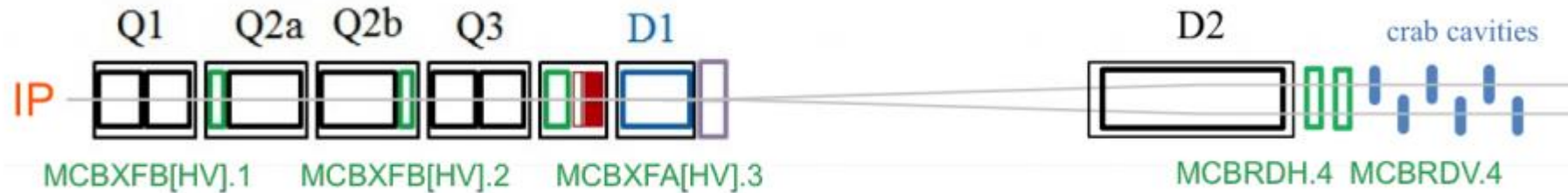
Alexej Grudiev

17.05.2017

Outline

- Crab cavity system for FCC-hh
- Motivation for Nb-coated crab cavity
- Cavity design and parameters
- Budget and time line

Crab cavity system for FCC-hh (april 2017)



Schematic layout:
E. Cruz-Alaniz,
Nov. 2016, Barcelona

	FCC-hh		HL-LHC (R. Calaga, Chamonix 2012)
RF frequency [MHz]	400		400
Total voltage V [MV]	18 (uncertainty $\pm 20\%$)		6 \div 10
Available length [m]	20		
Beam separation [mm]	250 (maybe 204 soon)		194
Average beta in the ring [m]	$(339+67)/2 = 203$		200
Beta* [m]	0.3	0.1	15 \div 25
Crossing angle [urad]	89	154	235 \div 290
Beta at CC location [m]	10100 \div 10900	30300 \div 32700	4000

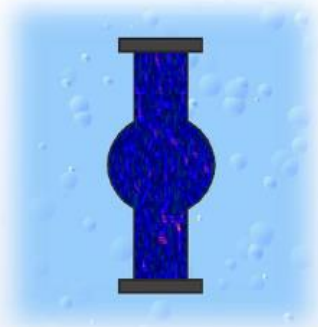
Information for FCC-hh provided by FCC-hh general design WG: D. Schulte, E. Cruz-Alaniz, A. Seryi, R. Martin, R. T. Garcia

Comparing CC pars for FCC-hh to the HL-LHC

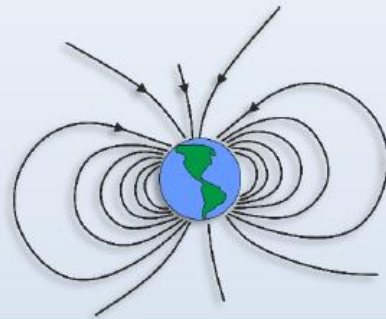
- MORE CCs: Total voltage is 3 (2) times higher => **6** cavities per beam/side/IP
- Available length: $20\text{m}/(6 \times 2) = 1.7$ m per cavity is sufficient even for longer alternatives (WOWCC)
- Larger beam separation 250 vs 194 may give some advantages in case of redesign
- EFFECTIVE TRANSVERSE IMPEDANCE IS MUCH (up to $3 \times 8 = \mathbf{24}$ times) HIGHER than for HL-LHC:
 - Beta function at the CC location is 2.5 -> **8** times higher for the same $\langle \beta \rangle$
 - Number of cavities per beam 2-**3** times higher
- Low impedance CC are desirable
- In Conclusion: larger number of cavities, larger beam coupling impedance and different beam separation justifies looking into new alternatives for FCC-hh CC system

Motivation

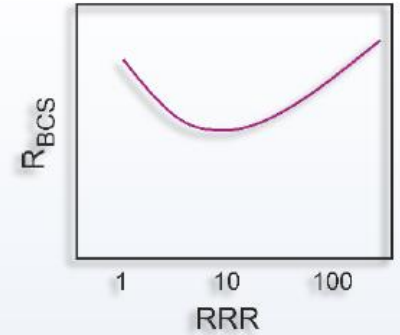
S. Aull, SRF2015



No thermal runaway



No magnetic shielding



Minimize BCS losses

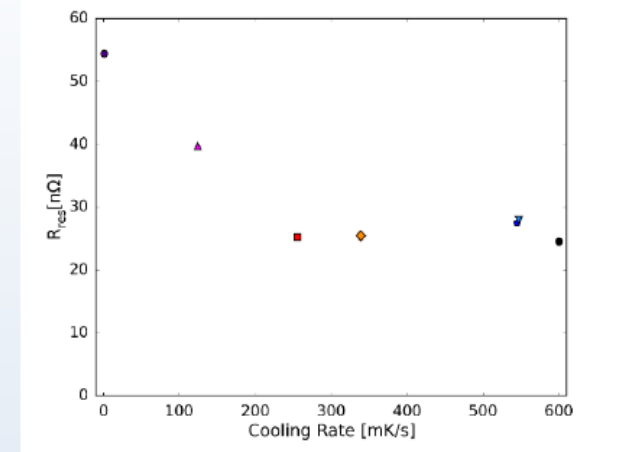
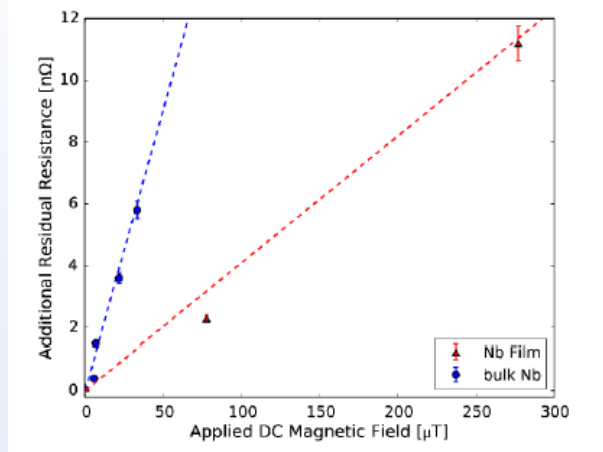
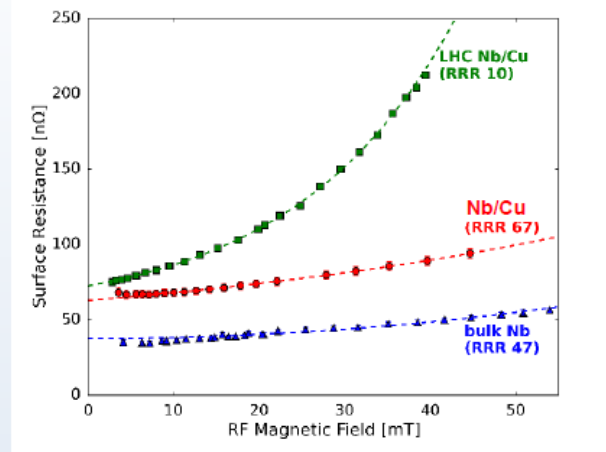


Save on raw material



Can we apply the state of the art coating technique to 400 MHz crab cavity?

We have a bulk-like Nb/Cu film...



with a Q-Slope comparable to bulk niobium at 4 K

still less sensitive to trapped flux

severely affected by thermal currents?

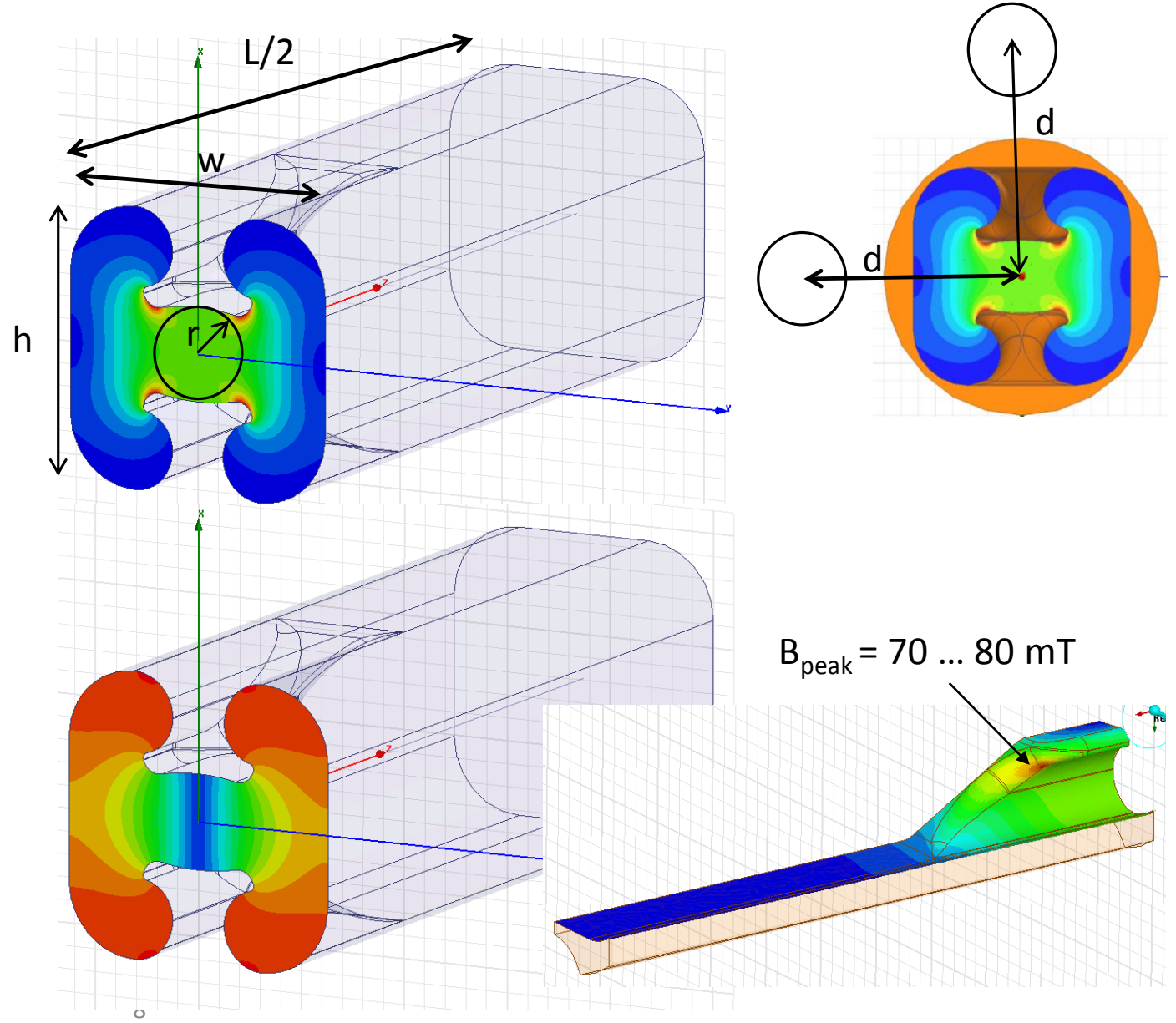
Introduction

- This work package covers design, construction and testing of 2 prototypes of a compact superconducting crab-cavity for LHC using Nb-on-Cu-coating technique.
- The cavity shape is based on the ridged waveguide resonator with wide open apertures to provide access to the inner surface of the cavity for coating.
- It also provides natural damping for HOMs and rather low longitudinal and transverse impedances.
- **The final goal is to validate the fabrication and coating of the cavity prototypes and to characterize its high gradient performance in a vertical test at 4K**

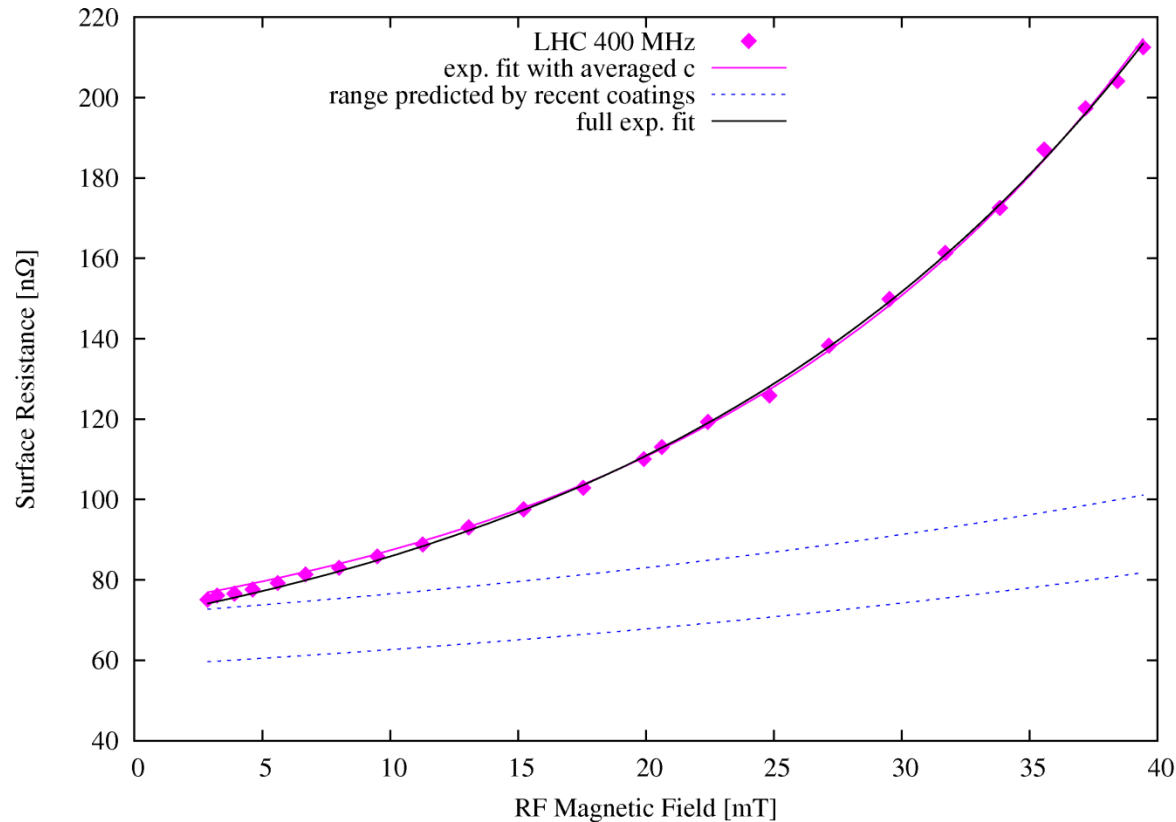
Main Parameter

w [mm]	251.70
h [mm]	251.70
r [mm]	42.00
L [mm]	1400.00
d [mm]	192.00

Frequency [MHz]	400.000
G [Ω]	109
Vx [MV]	3.0
Total Energy [J]	10.4
Rx/Q [Ω]	343.5
E _{peak} [MV]	50
B _{peak} [mT]	78



Non-linear behaviour of surface resistance (S. Calatroni, S. Aull)

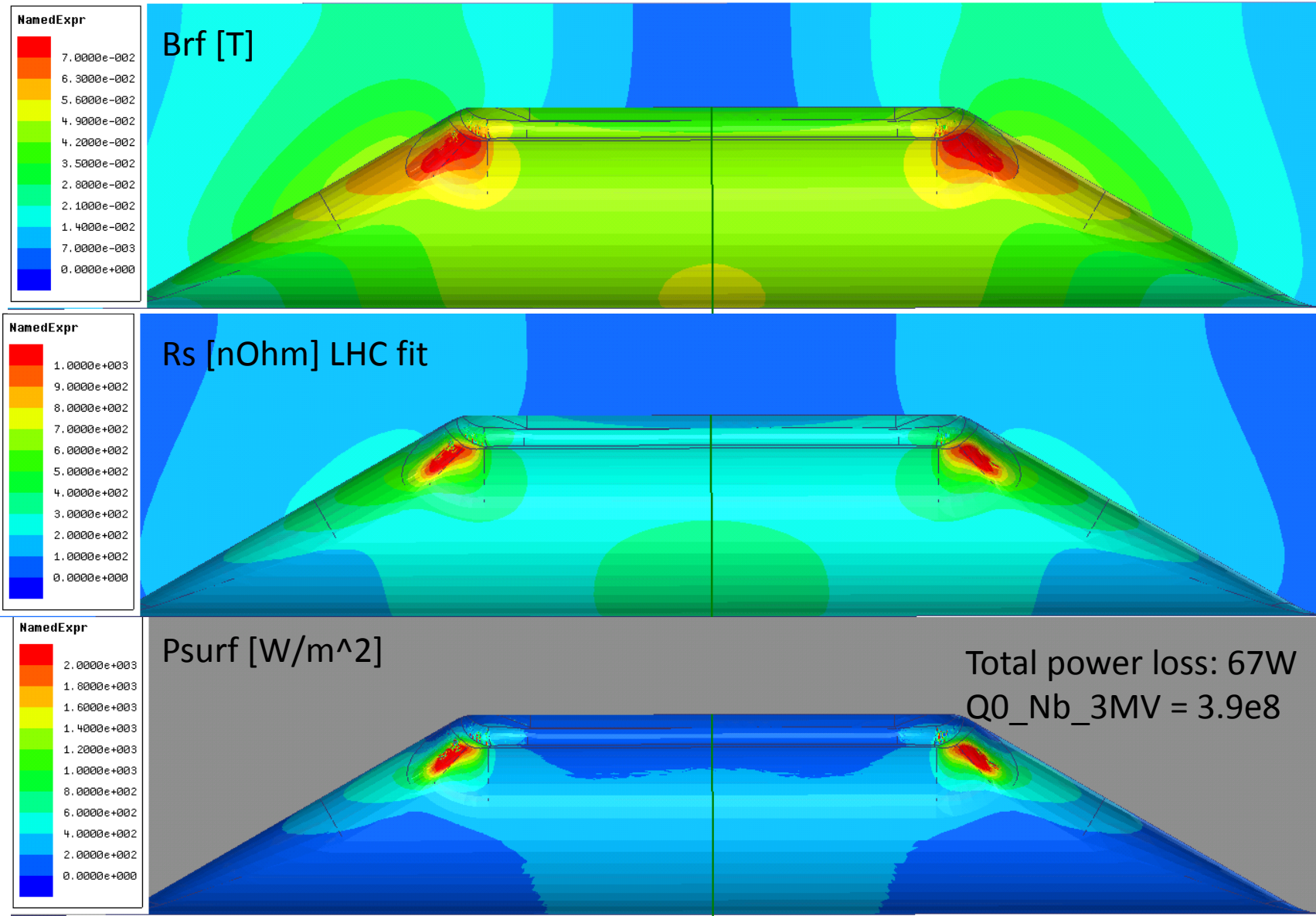


$$\text{LHC: } R_s(\text{Brf})[\text{nOhm}] = 54.7 + 19.0 \cdot \exp(0.054 \cdot \text{Brf}[\text{mT}])$$

$$\text{ECR: } R_s(\text{Brf})[\text{nOhm}] = 46.9 + 17.1 \cdot \exp(0.023 \cdot \text{Brf}[\text{mT}])$$

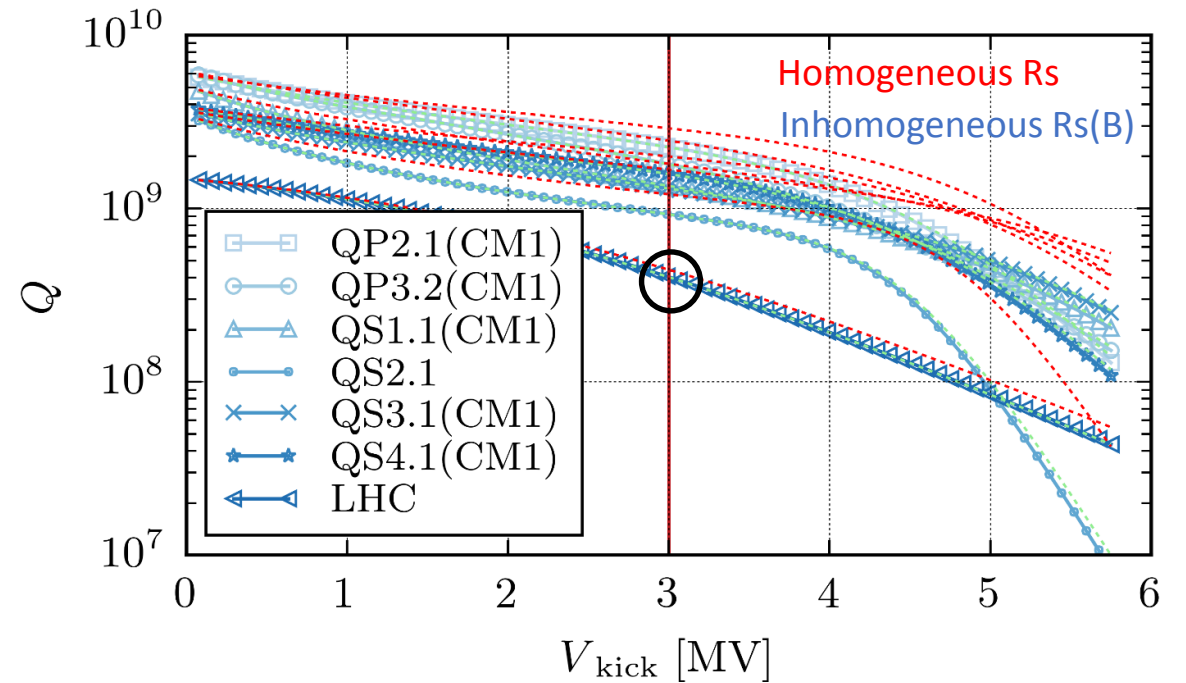
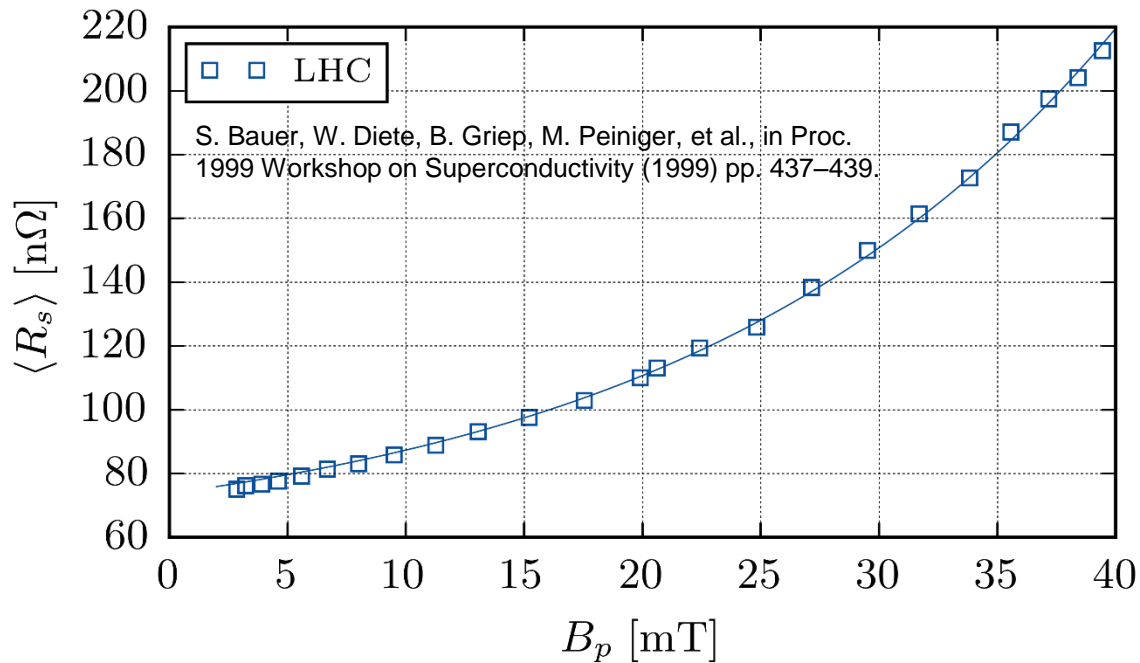
There is a big potential in the new coatings but let's be conservative and take LHC cavity data.

Power loss distribution on the surface for 30 degree taper at 3 MV



Q₀ calculation

- Nominal kick voltage 3 MV → B_{peak} up to 80 mT
- Results above 40mT for LHC uncertain due to lack of measurement data
- Q based on extrapolation of R_s from the LHC data
- Q₀ (R_s=const.) = 4.45e8
- Q₀ (R_s=R_s(B)) = 4.05e8



Wake Field and Impedance Calculation

Monopole

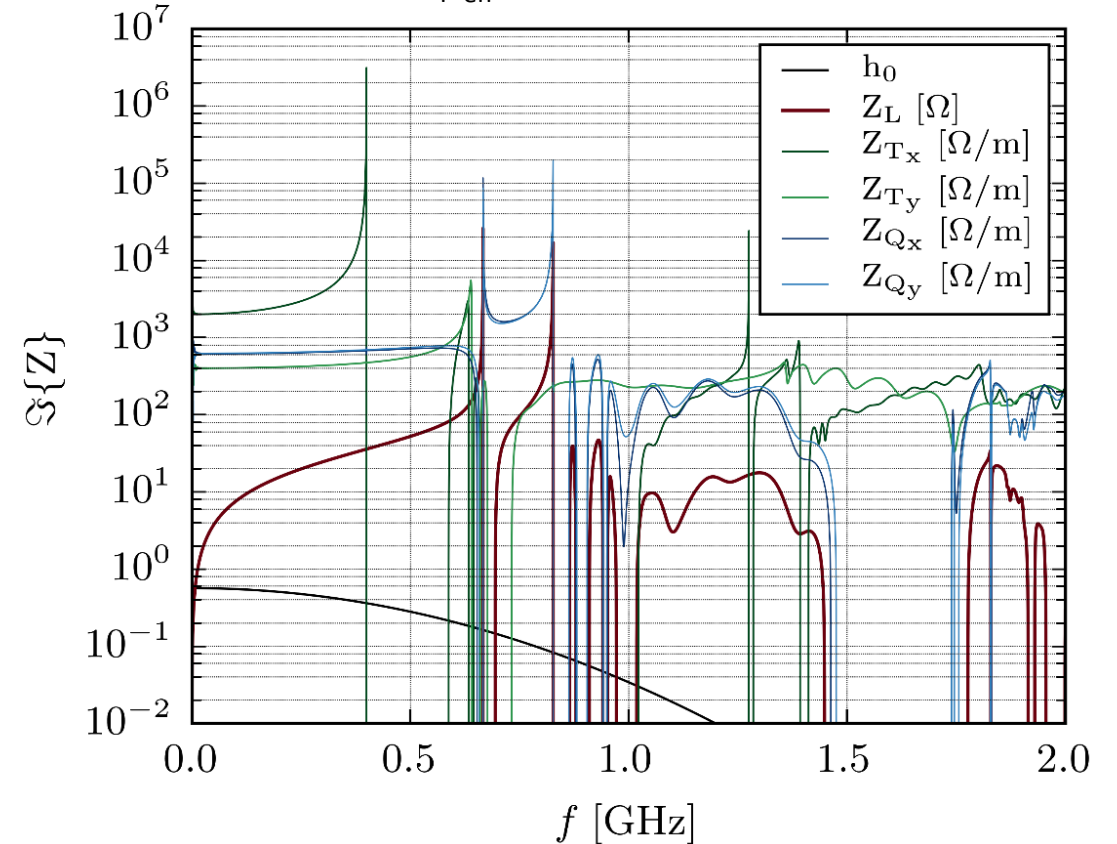
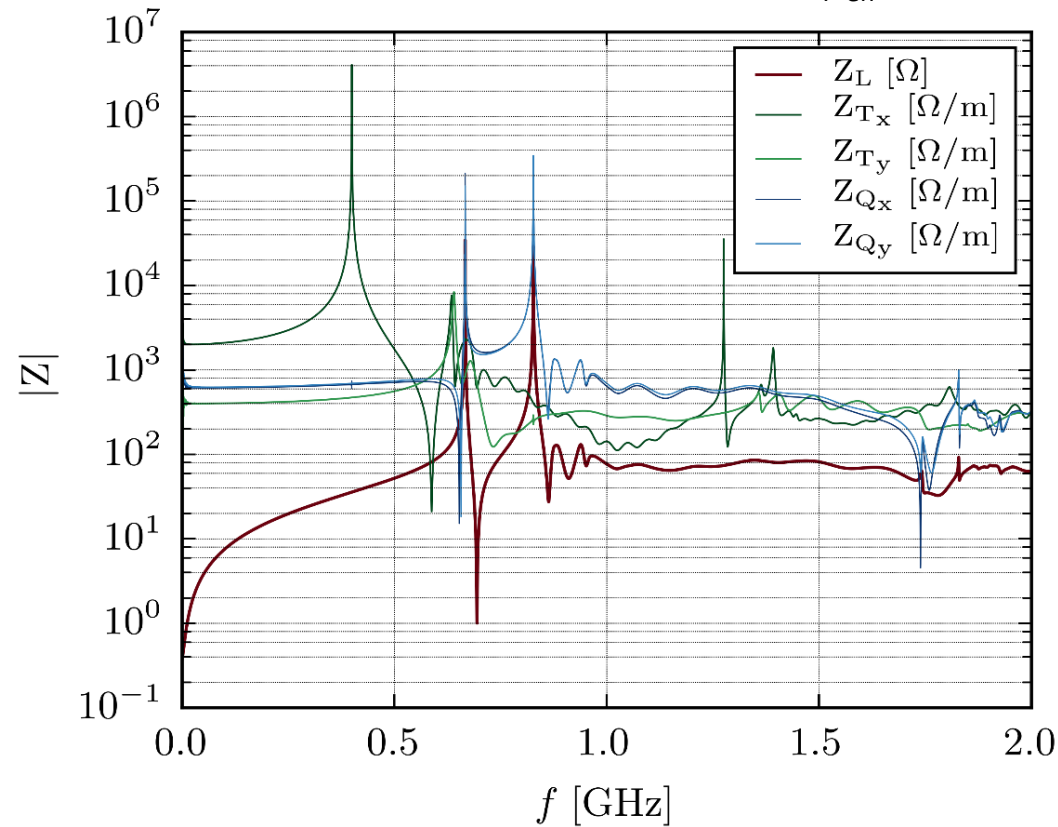
Loss factor [V/pC]	0.012
$(Z_L/N)_{\text{eff}}$ [m Ω]	0.974

Dipole

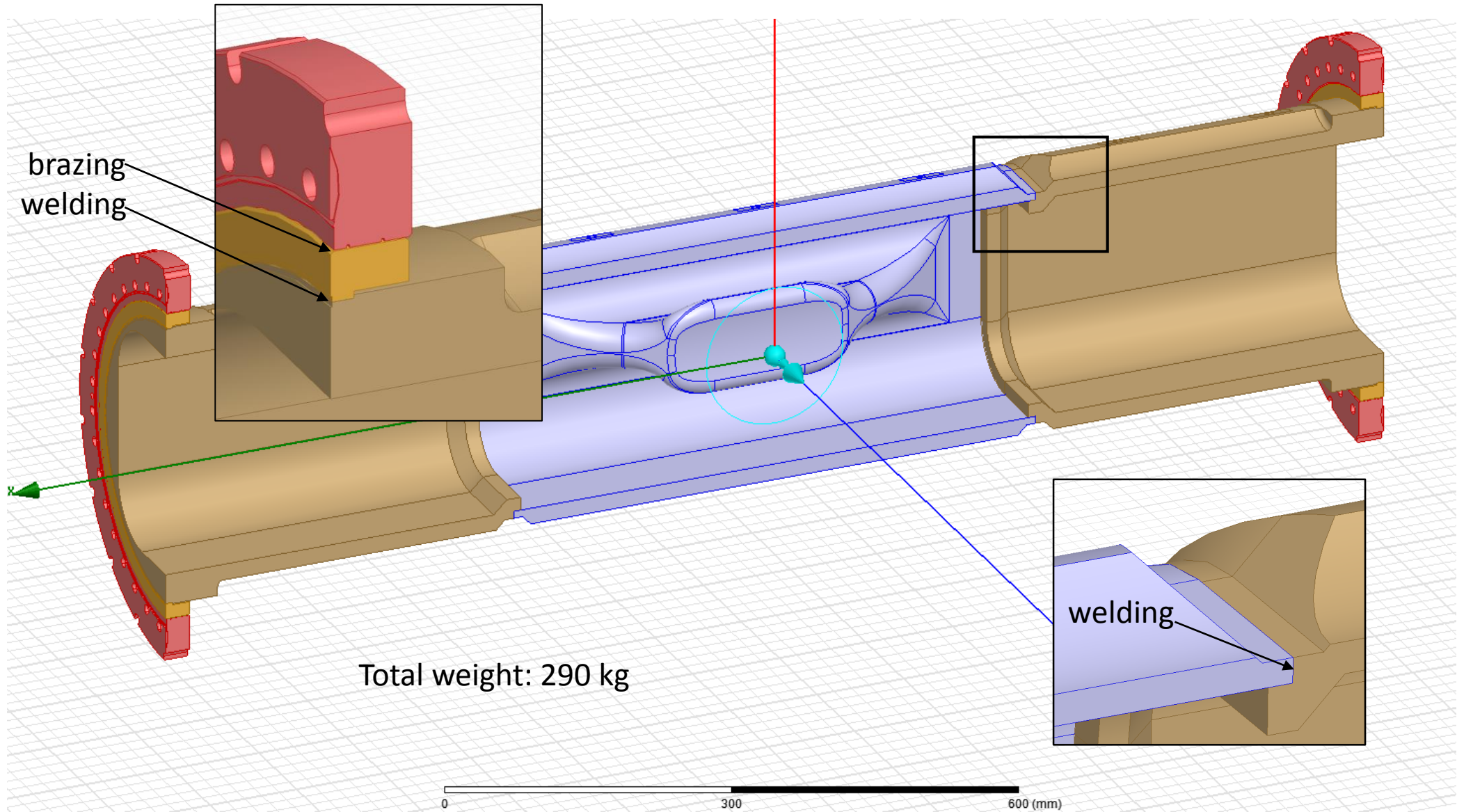
Kick factor x [V/pC/m]	1.673
Kick factor y [V/pC/m]	0.460
$(Z_T)_{\text{eff}}$ x [Ω /m]	1562.8
$(Z_T)_{\text{eff}}$ y [Ω /m]	437.6

Quadrupole

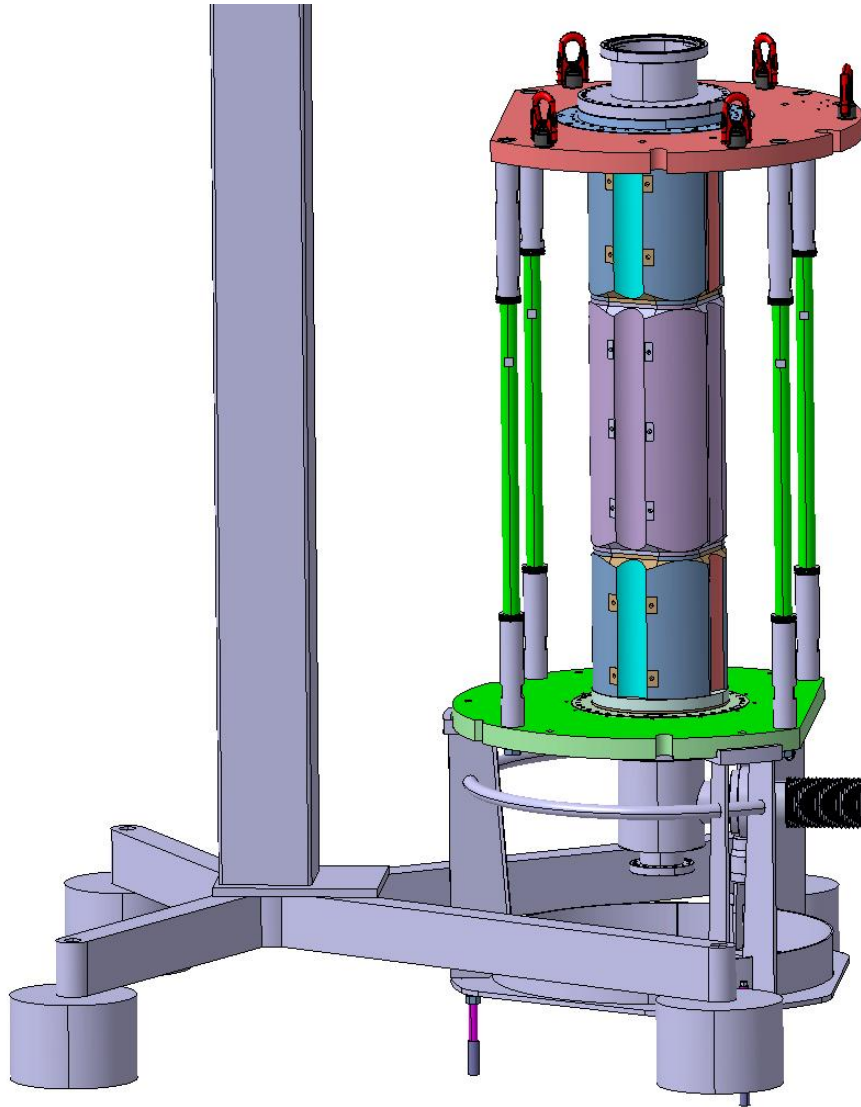
Kick factor x [V/pC/m]	0.733
Kick factor y [V/pC/m]	0.769
$(Z_T)_{\text{eff}}$ x [Ω /m]	631.9
$(Z_T)_{\text{eff}}$ y [Ω /m]	791.9



Assembly concept of the WOWCC copper substrate

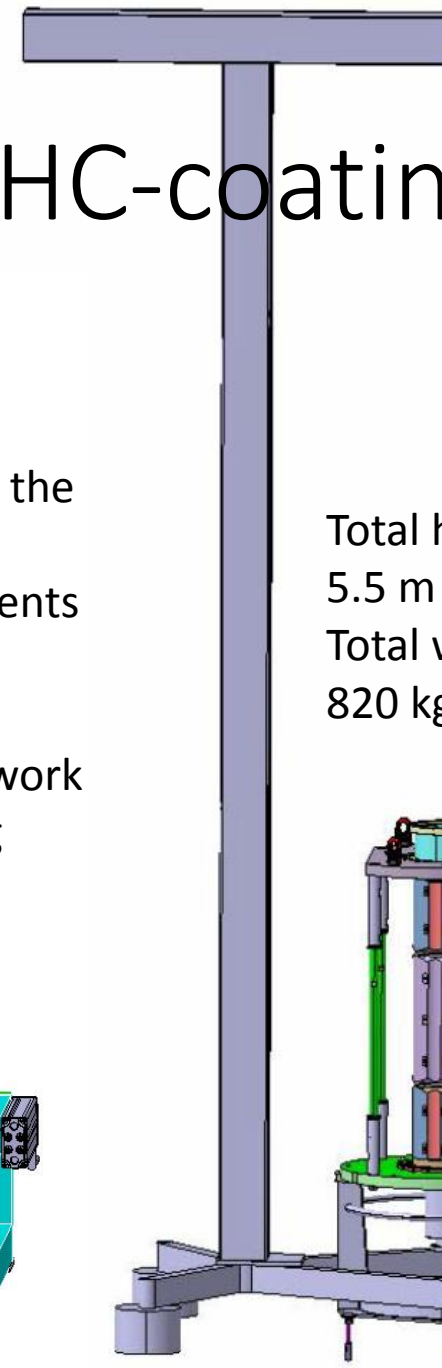
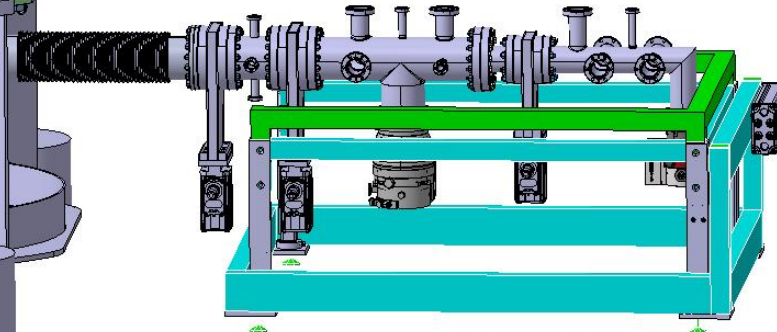


Integration of WOWCC into LHC-coating setup



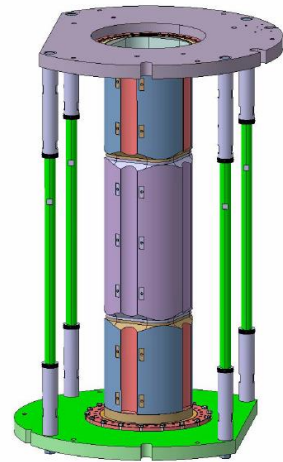
Aim of the integration study:

- Get overall dimensions and weight of the setup
- Formulate requirements for the infrastructure in the B252
- Communicate the requirements to the responsible for the infrastructure in B252
- Pave the way to the future work on the design of the coating setup



Total height:
5.5 m
Total weight:
820 kg

WOWCC +
frame
weight:
517 kg




Work package structure:

- Task 1: RF design (Alexej Grudiev (RF))
- Task 2: Mech. Design of the prototype and tooling (Ofelia Capatina (MME))
- Task 3: Fabrication of the “substrates” (Pierre Naisson (MME))
- Task 4: Surface treatment (Leonel Ferreira (VSC))
- Task 5: Coating system and coating (Alban Sublet (VSC))
- Task 6: Rinsing and clean room assembly of the prototypes for testing (Mikko Karppinen (RF))
- Task 7: Cold Testing in cryostat (Mikko Karppinen (RF))

Budget and manpower profile (end of 2016)

		2016	2017	2018	Total
Budget [kCHF]	Design	20	20	?	
	Material	80	~0	?	
	Fabrication	0	150	50	
	Chemistry	0	100	50	
	Coating	0	150	50	
	RF infrastructure	?	?	?	
	Total	100	420	150	670
Manpower [FTE]					
	Engineer (ENG)	0.33	0.85	0.5	1.7
	Technician (TEC)	0	1.5	1.5	3.0
	Fell/PJAS (FEL)	0.45	0.25	0.25	1.0

 20% less cost for coating system
 Reduction of manpower for coating
 2PM-ENG
 3PM-FEL
 3PM-TEC

The resources for SRF infrastructure modification in order to accommodate the WOWCC prototypes are not included

Summary

why would we do coated crab

- No thermal run-away (operation, machine protection)
- Potential to reach 5 MV per cavity if coating is (2-3 times) better than for LHC 400 MHz main RF cavities (cost, impedance)
- Lower impedance (x2, Z/n ; x3 $Z_{x,y}$)
- No magnetic shielding (cost)
- Material (cost)