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Vacuum acceptance tests for particle accelerator equipment

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Vacuum for Particle Accelerators Glumslöv, Sweden, 6 - 16 June, 2017



Outline

- 1. The CERN accelerator complex
- 2. Vacuum requirements evolution: An historical example
- 3. Acceptance thresholds
- 4. Acceptance tests procedures:
 - Unbaked system
 - Example of polymeric component
 - Partially baked equipment
 - Baked system
 - Low outgassing but not conform RGA
 - Non Evaporable Getter (NEG) coating qualification
- 5. Conclusions & Advices
- 6. Additional slides: Some special needs and examples:
 - Beam induced effects: ESD & PSD cases
 - New sintered materials
 - Glues vs. NEG

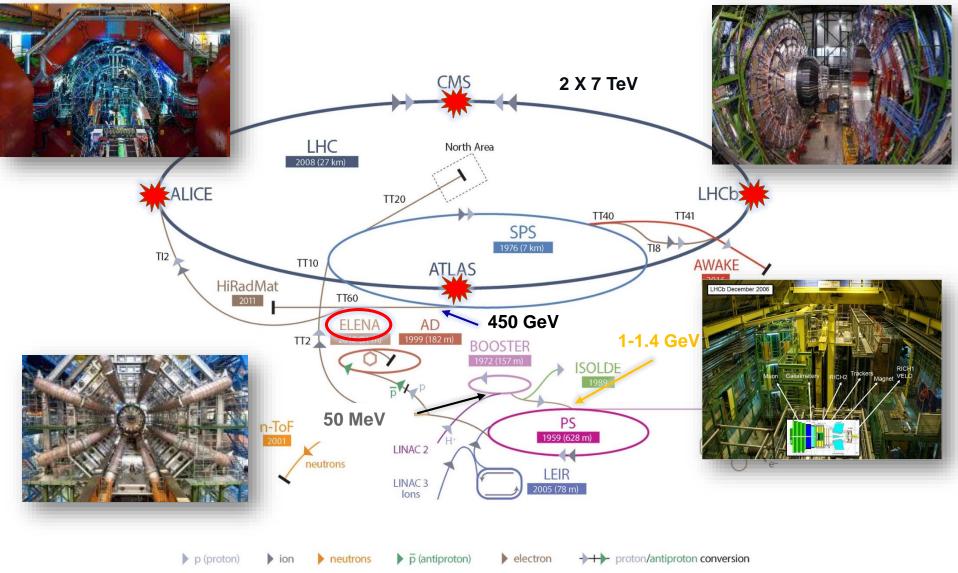


Why Vacuum Acceptance Tests?

- 1. One of the main mandates of the CERN Vacuum Surfaces Coatings group is to provide the beam operation with a required vacuum level on all the accelerator complex.
- 2. To achieve that mandate, acceptance tests are needed to assess the compatibility of all pieces of equipment to be installed in the beam vacuum system of the accelerator complex:
 - Leak tightness.
 - Detection of contamination.
 - > Measurement of outgassing rate and its time variation.
 - Measurement of virtual leaks (in leakage).



CERN accelerators chain





LINAC 2



LINAC 2 started up in 1978 when it replaced LINAC 1. It was originally built to allow higher intensity beams for the accelerators that follow it in CERN's accelerator complex. LINAC 2 will be replaced by LINAC 4 in 2020.

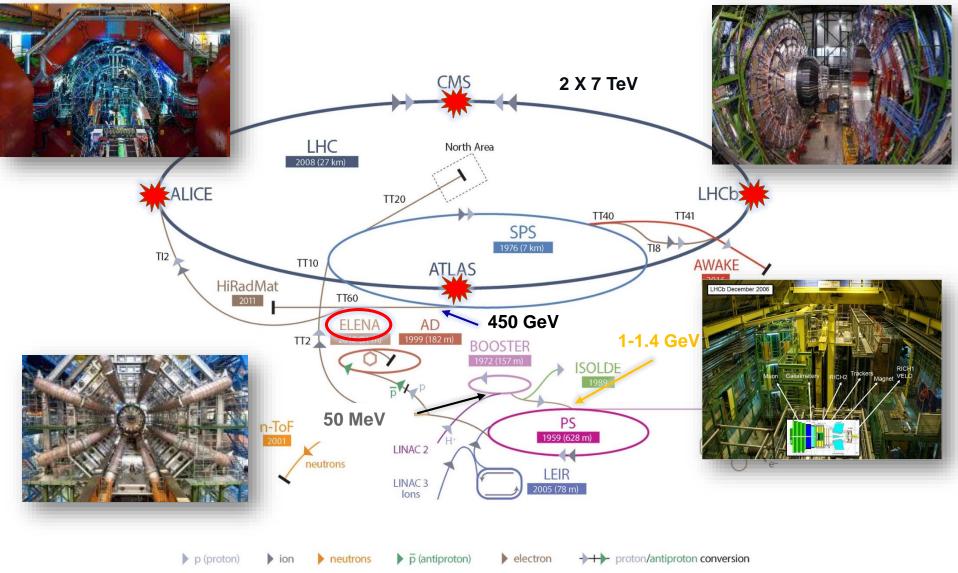
Unbaked system P_{Limit} < 2x10⁻⁶ mbar*

ENERGY: Linac 50 MeV

* After 24 h pump down



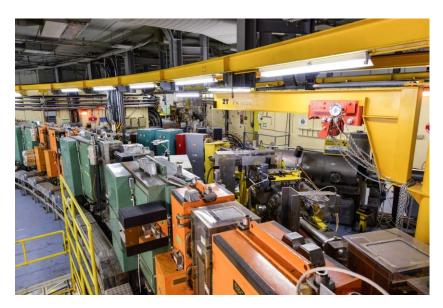
CERN accelerators chain





PS Booster

The Proton Synchrotron Booster is made up of four superimposed synchrotron rings that receive beams of protons from the linear accelerator Linac 2 at 50 MeV and accelerate them to 1.4 GeV for injection into the Proton Synchrotron (PS).





PS Booster: 45 Years old

Unbaked system $P_{\text{Limit}} < 5x10^{-8} \text{ mbar}^*$ for ions run

* After 24 h pump down



Proton Synchrotron ENERGY:

The PS first accelerated protons on 24 November 1959, becoming for a brief period the world's highest energy particle accelerator



PS 25 GeV

The Proton Synchrotron (PS) is a key component of CERN's <u>accelerator</u> <u>complex</u>, where it usually accelerates either proton delivered by the <u>Proton</u> <u>Synchrotron Booster</u> or heavy ions from the <u>Low Energy Ion Ring</u> (LEIR).

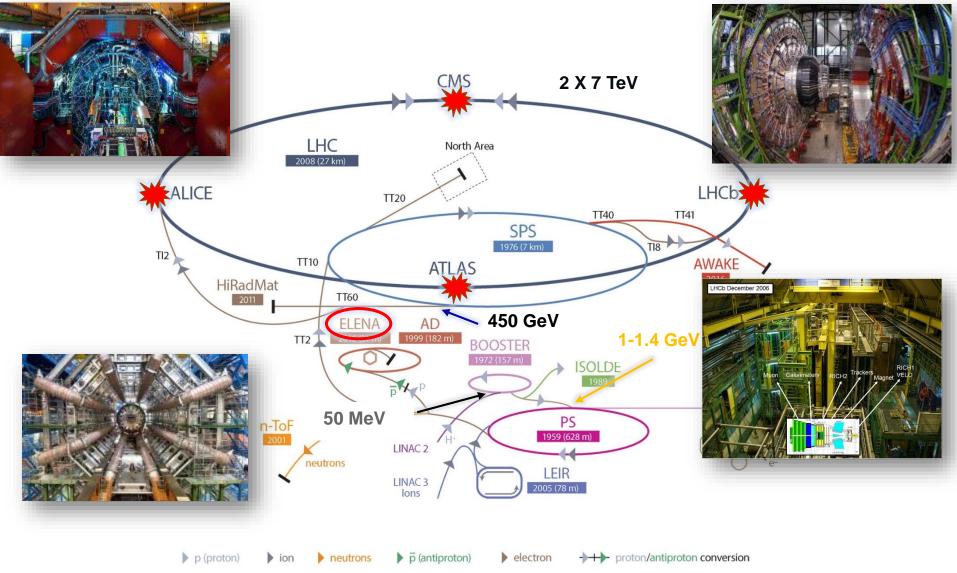
With a circumference of 628 metres, the PS has 277 conventional (room-temperature) electromagnets, including 100 dipoles to bend the beams round the ring. The accelerator operates at up to 25 GeV.

Unbaked system $P_{\text{Limit}} < 2x10^{-8} \text{ mbar}^*$ for ions run



* After 24 h pump down

CERN accelerators chain





Super Proton Synchrotron



Unbaked system P_{Limit} < 1x10⁻⁷ mbar*

ENERGY: SPS 450 GeV

Seven kilometres in circumference, the Super Proton Synchrotron (SPS) was the first of CERN's giant underground rings. It was also the first accelerator to cross the Franco–Swiss border.

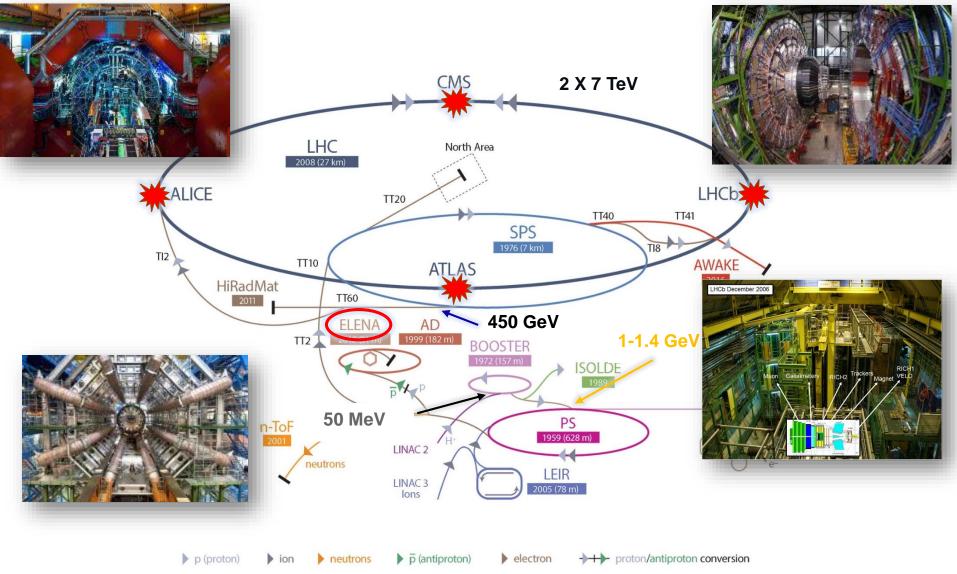
Eleven of CERN's member states approved the construction of the SPS in February 1971, and it was switched on for the first time on 17 June 1976, two years ahead of schedule.

The SPS operates at up to 450 GeV. It has 1317 conventional (roomtemperature) electromagnets, including 744 dipoles to bend the beams round the ring

* After 24 h pump down



CERN accelerators chain



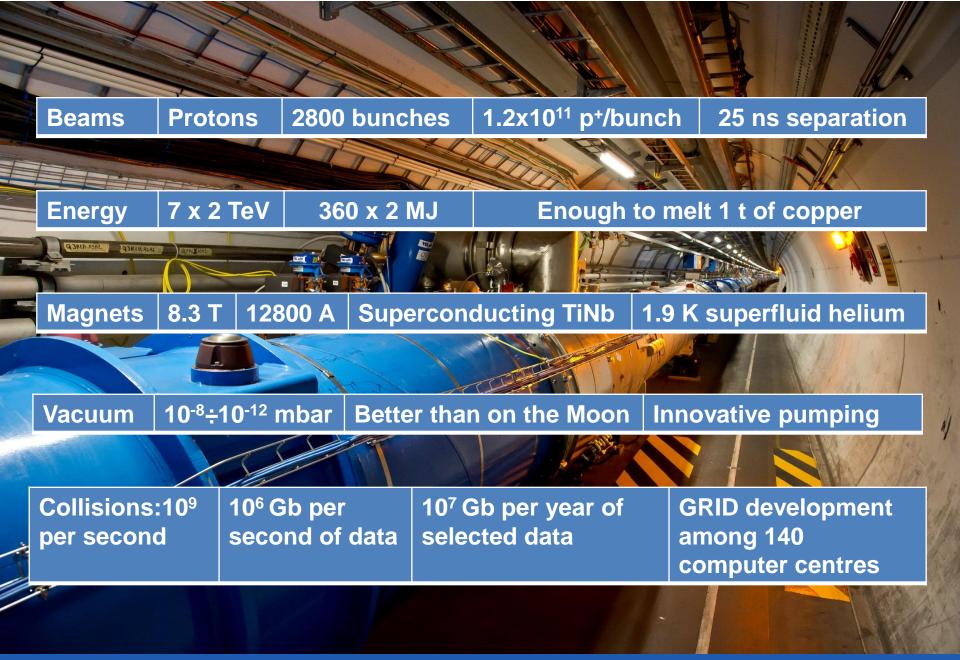


The Large Hadron Collider: LHC

At 10.28am on 10 September 2008, a beam of protons is successfully steered around the 27kilometre Large Hadron Collider (LHC) for the first time. The machine is ready to embark on a new era of discovery at the high-energy frontier.

LHC experiments address questions such as what gives matter its mass, what the invisible 96% of the universe is made of, why nature prefers matter to antimatter and how matter evolved from the first instants of the universe's existence.







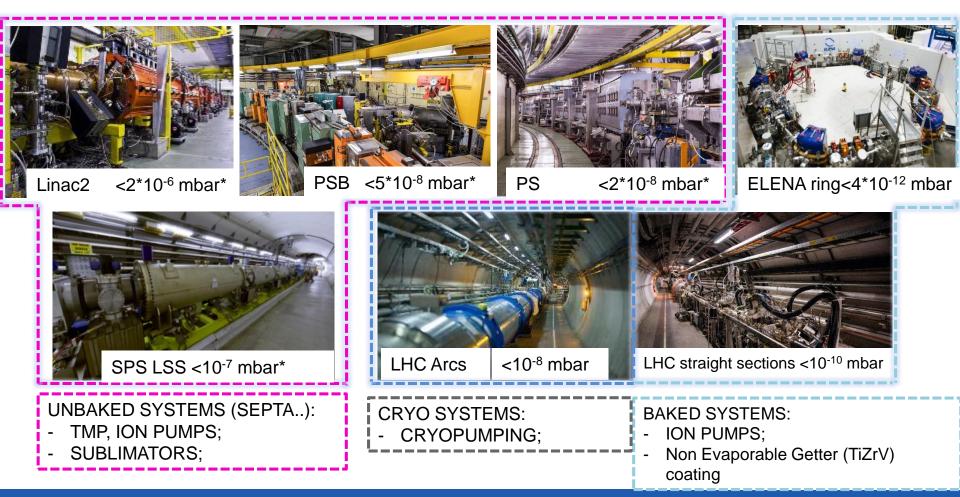
CERN accelerators chain: vacuum systems and requirements



* After 24 h pump down



CERN accelerators chain: vacuum systems and requirements





CERN's vacuum beamlines

Туре	Year	Energy	Bakeout	Pressure (Pa)	Length	Particles	
Linac, Booster, ISOLDE, PS, n-TOF and AD Complex 2.6 km !							
linac	1978	50 MeV	lon pumps	10 ⁻⁷	40 m	р	
electrostatic	1992	60 keV	-	10 ⁻⁴	150 m	ions: 700 isotopes	
linac	2001	3 Me∨/u	partly	10 ⁻⁵ - 10 ⁻¹⁰	20 m	and 70 (92) elements	
linac	1994	4.2 MeV/u	lon pumps	10 ⁻⁷	30 m	ions	
accumulator	1982/2005	72 MeV/u	complete	10 ⁻¹⁰	78 m	pbar, ions	
synchrotron	1972	1-1.4 GeV	lon pumps	10 ⁻⁷	157 m	P, ions	
synchrotron	1959	28 GeV	lon pumps	10 ⁻⁷	628 m	P, ions	
decelerator	?	100 MeV	complete	10 ⁻⁸	188 m	pbar	
linac/ring	2004-09		partly	10 ⁻⁸	300 m	e	
Transfer line	1976	26 GeV	-	10 ⁻⁶	~1.3 km	P, ions	
SPS Complex 15.7 km !							
synchrotron	1976	Extractions	10 ⁻⁷	7 km			
Transfer line	1976	450 GeV		10 ⁻⁶ - 10 ⁻⁷	~1.2 km	p, ions	
Transfer line	1976				~ 1.4 km		
Transfer line	2004/2006		-		2 x 2.7 km		
Transfer line	2005]			~730 m		
				ı	~109 km !		
			-		2 x (2 x 25 km)		
	2007	0 7 T -) (complete	< 10 ⁻⁸	2 × 3.2 km	p, ions	
collider	2007	2×7 Tev			~ 570 m		
					~ 180 m		
Transfer line	2006	7 TeV	-	10 ⁻⁶	2 × 720 m		
			High Vacuum		~20 km		
			UHV w/wo NEG		~ 57.5 km	~128 km !	
			Insulat	ion vacuum	~ 50 km		
	D Complex linac electrostatic linac accumulator synchrotron decelerator linac/ring Transfer line Synchrotron Transfer line Transfer line Transfer line Transfer line	D Complexlinac1978electrostatic1992linac2001linac1994accumulator1982/2005synchrotron1972synchrotron1979decelerator?linac/ring2004-09Transfer line1976Transfer line1976Transfer line1976Transfer line2004/2006Transfer line2005	D Complex 000000000000000000000000000000000000	D Complex Ion pumps linac 1978 50 MeV Ion pumps electrostatic 1992 60 keV - linac 2001 3 Mev/u partly linac 1994 4.2 MeV/u lon pumps accumulator 1982/2005 72 MeV/u complete synchrotron 1972 1-1.4 GeV lon pumps synchrotron 1959 28 GeV lon pumps decelerator ? 100 MeV complete linac/ring 2004-09 partly partly Transfer line 1976 26 GeV - synchrotron 1976 26 GeV - synchrotron 1976 450 GeV - Transfer line 1976 - - Transfer line 2004/2006 450 GeV - collider 2007 2 × 7 TeV complete Transfer line 2006 7 TeV - Collider 2006 7 TeV <	D Complex Ion pumps 10^{-7} electrostatic 1992 60 keV - 10^{-4} linac 2001 3 Mev/u partly $10^{-5} - 10^{-10}$ linac 1994 4.2 MeV/u lon pumps 10^{-7} accumulator 1982/2005 72 MeV/u lon pumps 10^{-7} accumulator 1982/2005 72 MeV/u complete 10^{-10} synchrotron 1972 1-1.4 GeV lon pumps 10^{-7} synchrotron 1972 1-1.4 GeV lon pumps 10^{-7} synchrotron 1979 28 GeV lon pumps 10^{-7} decelerator ? 100 MeV complete 10^{-8} linac/ring 2004-09 partly 10^{-8} 10^{-8} Transfer line 1976 26 GeV - $10^{-6} - 10^{-7}$ Transfer line 2004/2006 $ 10^{-6} - 10^{-7}$ $10^{-6} - 10^{-7}$ collider 2007 2×7 TeV complete $-$	$\begin{array}{ c c c c c c } \hline D \ Complex & 2.6 \ km \ ! \\ \hline linac & 1978 & 50 \ MeV & Ion pumps & 10^{-7} & 40 \ m \\ \hline electrostatic & 1992 & 60 \ keV & - & 10^{-4} & 150 \ m \\ \hline linac & 2001 & 3 \ Mev/u & partly & 10^{-5} \cdot 10^{-10} & 20 \ m \\ \hline linac & 1994 & 4.2 \ MeV/u & Ion pumps & 10^{-7} & 30 \ m \\ \hline accumulator & 1982/2005 & 72 \ MeV/u & complete & 10^{-10} & 78 \ m \\ \hline synchrotron & 1972 & 1-1.4 \ GeV & Ion pumps & 10^{-7} & 157 \ m \\ \hline synchrotron & 1972 & 1-1.4 \ GeV & Ion pumps & 10^{-7} & 628 \ m \\ \hline decelerator & ? & 100 \ MeV & complete & 10^{-8} & 188 \ m \\ \hline linac/ring & 2004-09 & partly & 10^{-8} & 300 \ m \\ \hline Transfer line & 1976 & 26 \ GeV & - & 10^{-6} & \sim 1.3 \ km \\ \hline Transfer line & 1976 \ Transfer line & 1976 \ Transfer line & 2005 & 450 \ GeV & - & 10^{-6} \cdot 10^{-7} & 7 \ km \\ \hline collider & 2007 & 2 \times 7 \ TeV & - & 10^{-6} - 10^{-8} & 22 \times (2 \times 25 \ km) \\ \hline Transfer line & 2006 & 7 \ TeV & - & 10^{-6} & 2 \times 720 \ m \\ \hline Transfer line & 2006 & 7 \ TeV & - & 10^{-6} & 2 \times 720 \ m \\ \hline Transfer line & 2006 & 7 \ TeV & - & 10^{-6} & 2 \times 720 \ m \\ \hline Transfer line & 2006 & 7 \ TeV & - & 10^{-6} & 2 \times 720 \ m \\ \hline Migh \ Vacuum & \sim 20 \ km \ High \ Vacuum & \sim 20 \ km \\ \hline \end{array}$	



The CERN Proton Synchrotron project (henceforth referred to as the CPS) was started in 1954, and it has now -- 1958 -- reached a sufficient stage of development for a general report to summarize the progress achieved in the design of the various components of the machine. Although a number of details still remain to be worked out, the chief parameters for the machine are finally fixed, construction is under way and assembly of the components is due to begin shortly. This seems a suitable time for a general review of the work done and of the difficulties encountered.

THE CERN PROTON SYNCHROTRON

(1st Part)

CERN 59-29

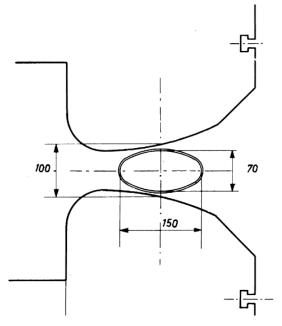
Proton Synchrotron Division 21st August 1959 by

E. Regenstreif



15. Gas scattering.

Owing to scattering by residual gas molecules, the cross-section of the beam increases during the time interval between injection and the moment when the energy of the particles becomes about double the energy at injection. The damping of the betatron oscillations due to the rise of the magnetic field subsequently leads to a gradual diminution of the scattering effect. In accordance with theoretical forecasts, for a vacuum of 10^{-5} mm Hg and an energy of 50 MeV at injection in the CPS, scattering by gas adds only a few millimetres to the beam diameter, and should cause negligible loss of beam.



CERN 59-29

Proton Synchrotron Division 21st August 1959



3. Système à vide E. Fischer

Les anneaux de stockage d'électrons et de protons exigent une pression de gaz résiduel beaucoup plus basse que les accélérateurs classiques. Alors que, par exemple, le PS du CERN fonctionne de manière satisfaisante avec une pression d'environ 10⁻⁶ torr, pour les ISR, la pression moyenne autour des anneaux doit être mille fois plus basse, c'est-à-dire de 10⁻⁹ torr. Cette pression est même encore trop forte pour les régions d'interactions où elle doit être inférieure à 10⁻¹⁰ torr et si possible d'environ 10⁻¹¹ torr.

Courrier CERN Volume 6, N° 7, Juillet 1966



1. THE VACUUM SITUATION PRIOR TO 1990

The PS was designed and build in the mid 50ties and entered service in 1959. Vacuum was realised with some 100 pumping groups each one composed of a rotary pump and an oil diffusion pump. Most of the seals were made of elastomer materials. The pressures reached at that time were in the 10^{-4} Pa region. Besides the high pressure the bad influence on the beam of the heavy hydrocarbon molecules was detected and in the late 60ties the change to Ion Getter Pumps was made. This left of course much of the vacuum containment wall contaminated. It was only after the mid 80ties that all 100 magnets received new vacuum chambers made out of vacuum fired 316L+N stainless steel. Almost all seals used were by then made in metal; lead, aluminium or copper. Most of the big equipment tanks like for septa, or kickers were equipped with rectangular covers with vacuum seals made up out of a diamond shaped aluminium extrusion bend and welded in the

- Elastomers seals: not more adequate
- Contamination problems: Heavy hydrocarbons bad influence on the beam

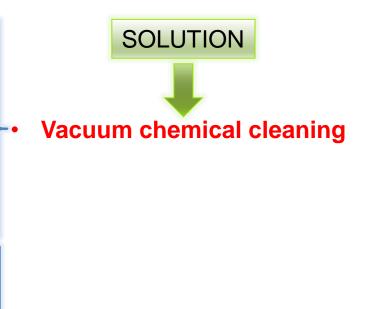
THE VACUUM UPGRADE OF THE CERN PS AND PS BOOSTER

M. van Rooij, J.-P. Bertuzzi, M. Brouet, A. Burlet, C. Burnside, R. Gavaggio, L. Petty, A. Poncet, CERN



In order to reach the required vacuum improvement, besides a general cleaning action, adding sublimation pumps and cryo pumps to the existing ion pumps was considered. There exists a CERN design of a Ti sublimation cartridge depositing Ti on the inside of a ø 200 mm pump body along a length of some 150 mm. Connected with a proper conductance that gives a pumping speed around 600 1/s for air mixture at the beam tube. That would so roughly quadruple the pumping speed there. For the PS that would not be entirely sufficient, for the PSB a factor of more than 2 would still be missing.

The choice of cryo pumping to improve pressure in high outgassing areas was not retained, but improving the vacuum quality of the beam tubes and specially of the necessary equipment in tanks was considered to be a more economic approach, certainly point of view of later exploitation cost.



 Decrease the outgassing rate more than increase pumping speed

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Intermediate Summary

From PS Experience:

1.Beam losses and beam lifetime drive the vacuum level but maximum pressure in N_2 equivalent is used as acceptance criteria.

2.Work mainly on the total outgassing more than increase the pumping speed.

3.Cleanliness important factor: consequently gas composition start to have an important role

Pressure requirements different as a function of each machine:

- Difficult to define general criteria.
- Impossible to have a detailed simulation of each machine.

So....how to define the acceptance criteria?



How to define the acceptance criteria?

1. ADMISSIBLE OUTGASSING RATE

- a) DRIVEN BY Beam-gas scattering: Beam losses and beam lifetime
 - Estimation of average pumping speed to define a total admissible outgassing rate;
 - Determine admissible molecules density;
- b) DRIVEN BY Beam downtime: Allowed time to restart the machine in case of components exchange.
- c) DRIVEN BY Equipment requirement: Maximum allowed pressure/molecules density to run devices like kickers or RF cavities.

2. NO CONTAMINATION

- Anomalous presence of hydrocarbons, most probably due to error in design and/or lack of appropriate cleaning (error in cleaning procedure or post-cleaning pollution); inappropriate choice of materials (polymers, glues, lubricants ...);
- Higher than expected CO and CO₂ outgassing indicating the presence of carbonised elements;
- Any chemical element or compound usually not present in the residual gas phase, for example, F and Cl (issue with etching and cleaning), K and Na (manipulation), P and S (issue with electrolytic treatments).



Some examples: Baked system

LHC				
Area	Equivalent gas density	Hydrogen	Effective speed (ind	pumping icative)
Arcs	≤10 ⁺¹⁵ H ₂ m ⁻³		≥100) I.s ⁻¹
Experiments	≤10 ⁺¹³ H ₂ m ⁻³			
GAS	Nuclear scattering cross section(cm ²)		ensity (m ⁻³)) hour lifetir	ne
H_2	$9.5 10^{-26}$		9.810 ¹⁴	
He	$1.26 \ 10^{-25}$		7.410^{14}	
CH_4	5.6610^{-25}		1.610^{14}	
H_2O	$5.65 10^{-25}$		1.610^{14}	
СО	8.54 10 ⁻²⁵		1.110^{14}	
CO_2	8.54 10 ⁻²⁵ 1.32 10 ⁻²⁴		7 10 ¹³	

LHC ACCEPTANCE THRESHOLDS

Ensure 100 h of circulating beams before intensity degradation due to residual gas interactions occurs and minimise the background for the experiments.

LHC Design Report CERN-2004-003 4 June 2004



In both examples, the pressure requirements are driven by **beam** requirements.



	ΕL	E	Ν	А	,
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Area	Pressure requirements	Effective pumping speed (indicative)
Ring	≤4 x10 ⁻¹² mbar	Depend upon
Transfer lines	≤10 ⁻¹⁰ mbar	position (NEG
		sticking probability)

ELENA ACCEPTANCE THRESHOLDS

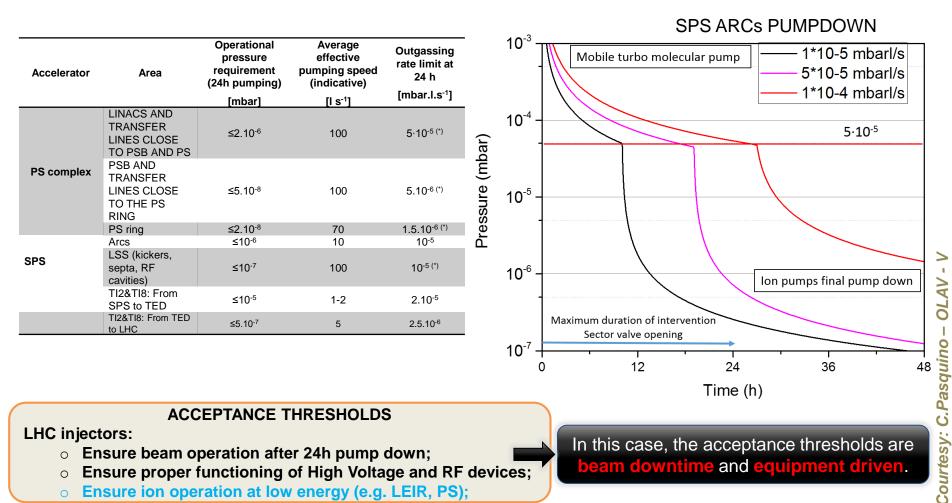
limitation of momentum and Ensures the emittance blow up induced by the interaction of 100 keV antiprotons with a beam population of 10⁷. No specification on gas composition

> Extra Low ENergy Antiproton (ELENA) ring and its Transfer Lines

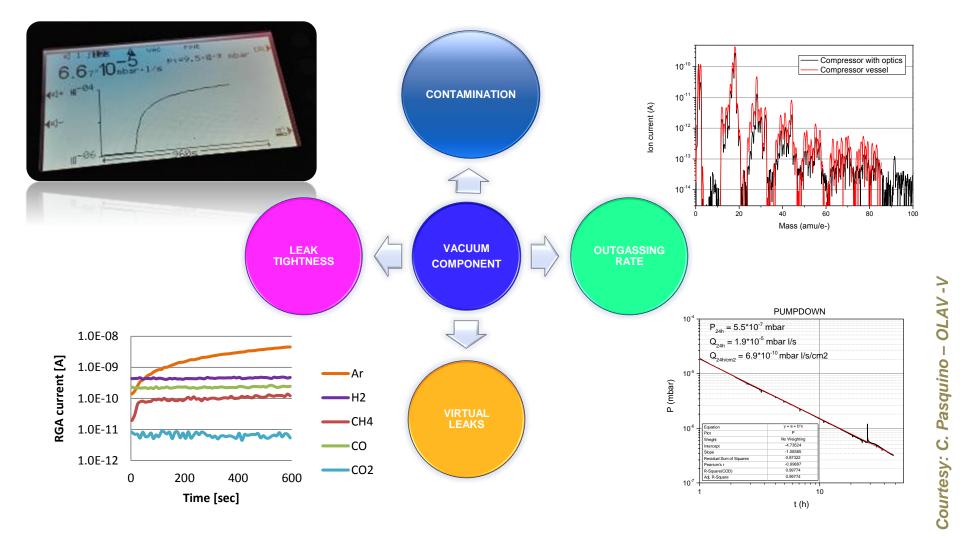
> > Design Report 3 April 2014

CERN-2014-002

Some examples: Unbaked system

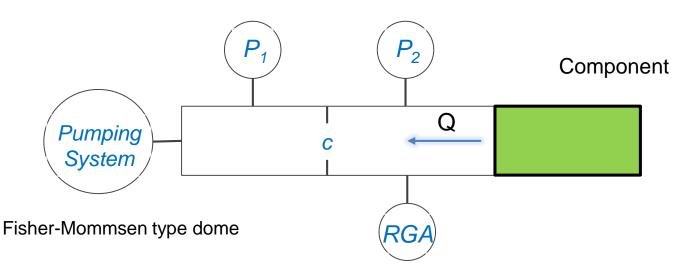


Acceptance Criteria

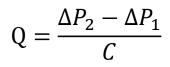




Outgassing rate measurements



• Outgassing rate:



- Pumping system:
 - I. Unbaked system:
 - II. Baked System

Turbo molecular pumps Chemical pumps



Unbaked: Vacuum validation steps

Measurement and verification of vacuum performance

- Functionality
- Leak tightness (First: high background)
- Outgassing rate after 24h of pump down
- Residual Gas Analysis
- Leak tightness (Final)



Unbaked: Acceptance Thresholds Overview

- He leak rate:
 - Q_{AIR} < 10⁻¹⁰ mbar·l/s
- Outgassing rate after 24h of pump down:
 - Q_{Out} < Depends on the machine
- Gas composition: H₂O is the dominant peak

Atomic mass units from 18 to 44

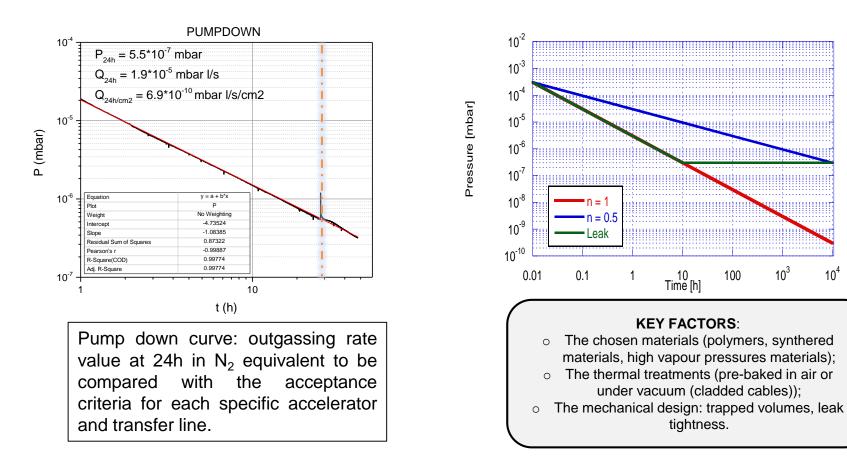
All the masses between **18 et 44** are at least **100 lower of the intensity of peak 18** (2 order of magnitude lower) except for masses 28 et 44

Atomic mass units from 44 to 100 (Indication of organic contamination)

All the masses from **44 to 100** are at least **1000 lower of the intensity of peak 18** (3 order of magnitude lower) except for mass 44



Acceptance tests for unbaked components





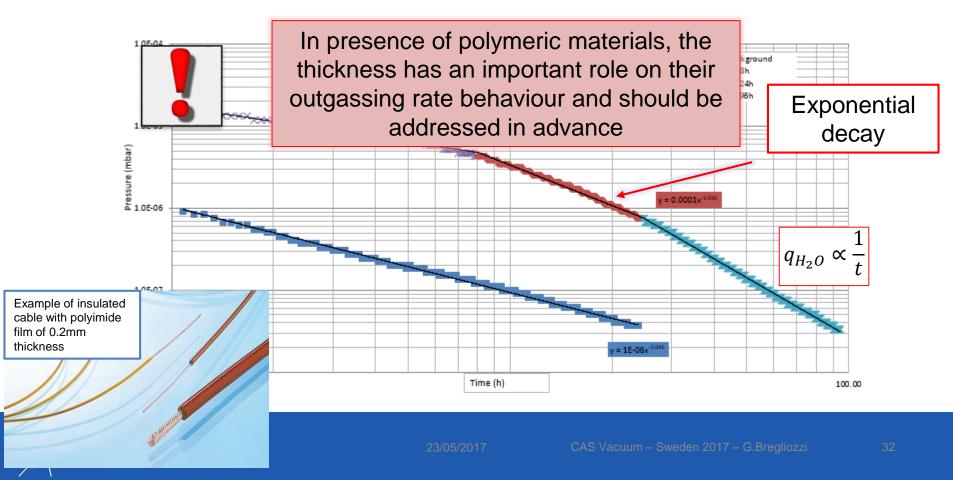
 10^{3}

100

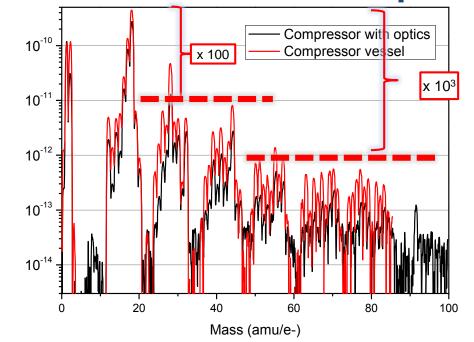
 10^{4}

Is it 24h of pump down enough?

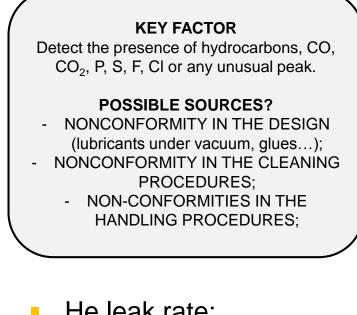
• 24h represent a good compromise that allows performing test within 1 week of time: installation, first leak detection, air venting overnight and final test. However.....



Acceptance tests for unbaked components



Residual Gas Analysis: after few hours of filament conditioning, the amplitude of the peaks is compared to the water content in the system. The component is considered accepted if the ratio between the water peak and the peaks up to mass 44 is higher than 100 and if the same ratio is higher then 1000 for peaks above mass 44.





on current (A)

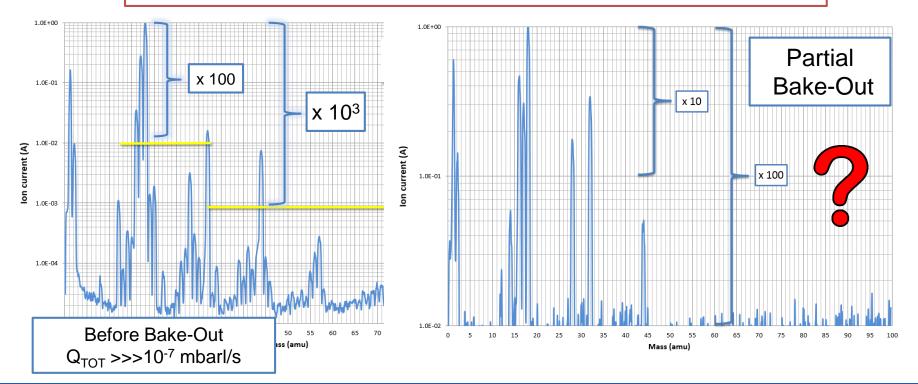
- He leak rate: Q_{AIR}< 10⁻¹⁰ mbar·l/s
- Courtesy: C. Pasquino OLAV V

Acceptance Thresholds Equipment subjected to partial bake-out

After bake In general, before bake-out, the total outgassing rate is dominated by H₂O: porous materials, polymers, etc....

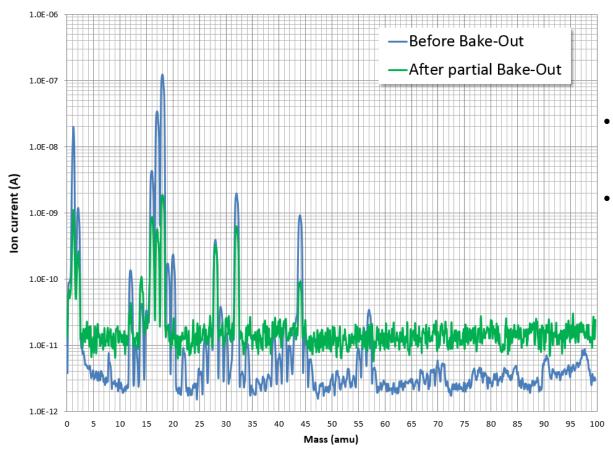


How consider the RGA Scan: Normalized? baked or unbaked?





Acceptance Thresholds Equipment subjected to partial bake-out



RGA Guideline

- H₂O intensity should decrease of ≈2 orders of magnitudes:
- No more traces of contamination: hydrocarbons, carbonised elements and any chemical elements not present in a gas phase.



Baked: Vacuum validation steps

Measurement and verification of vacuum performance





Baked: Acceptance Thresholds Overview LHC Case

- He leak rate:
 - Q_{AIR}< 10⁻¹⁰ mbar·l/s
- Internal leak rate:
 - Q_{AIR}< 5·10⁻⁹ mbar·l/s
- Outgassing rate:
 - Q_{Out} < 1.10⁻⁷ mbar·l/s
- Gas composition: H₂ is the dominant peak

Atomic mass units from 18 to 44 (Possible impact on NEG performance)

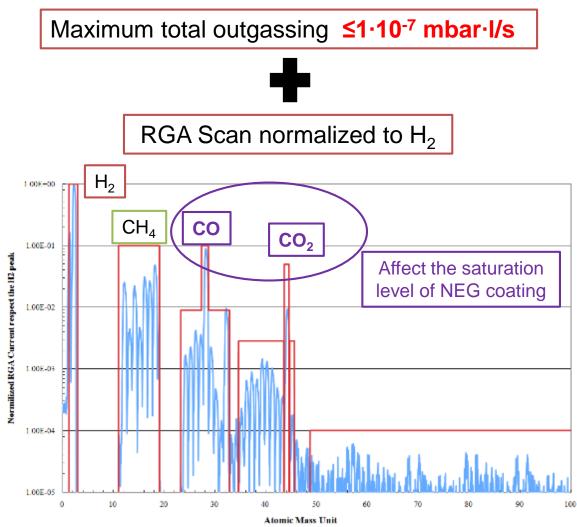
Different acceptance thresholds are selected as a function of the gas.

Atomic mass units from 44 to 100 (Indication of organic contamination)

Acceptance criterion: RGA signals for all masses higher than 44 are at least 10000 times lower than the signal of peak H_2 (mass 2).

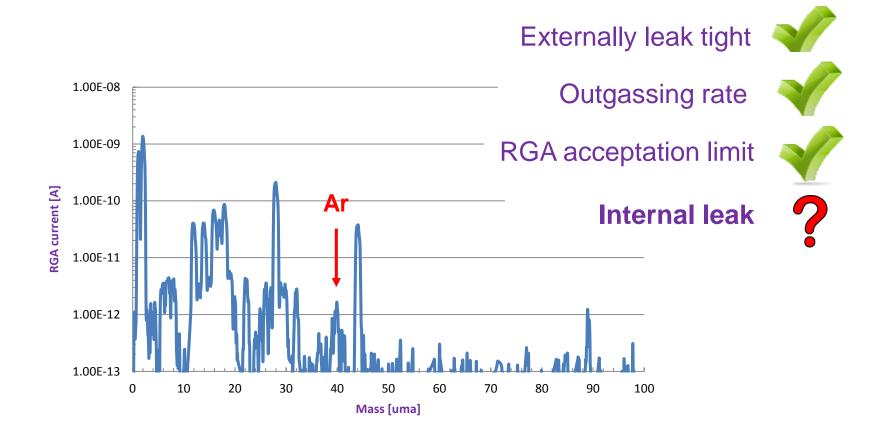


Baked: Acceptance Thresholds Overview LHC Case



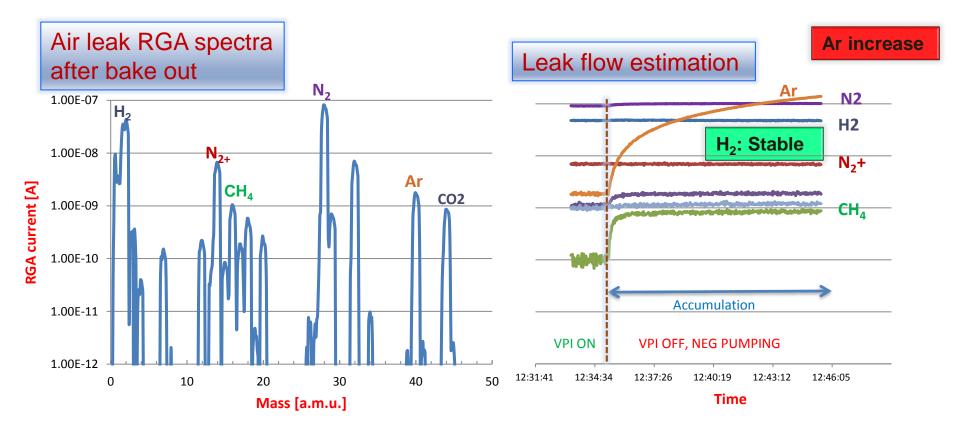


Baked: Acceptance Thresholds Overview LHC Case





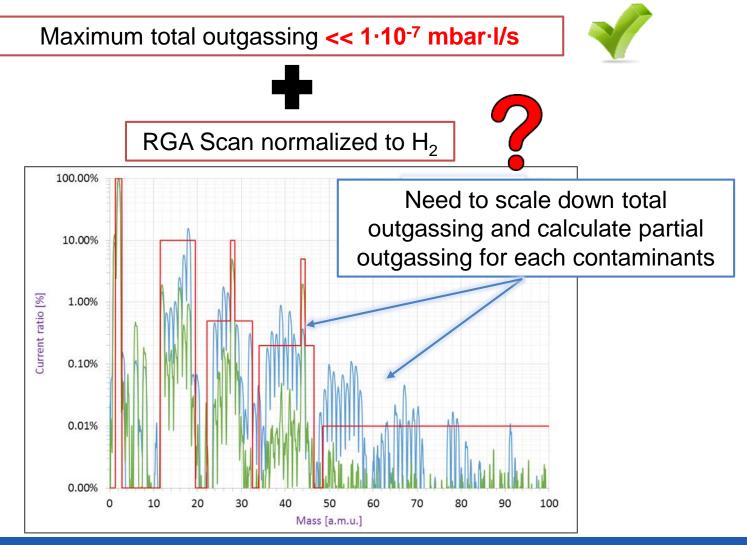
Baked: Acceptance Thresholds Overview LHC Case



 $Q_{[air_eq.]} < 5 \cdot 10^{-9}$ mbar·l/s correspond to ≈ 1 m saturated NEG (80mm ϕ) every 150 days



Acceptance thresholds: Low outgassing but not conform RGA





NEG coatings in particle accelerator

NEG coatings provide very large pumping speeds:

for $H_2 0.3 \sim 1 \text{ l/s/cm}^2$

for CO 5 ~ 10 l/s/cm²

Surface capacity of ~5 10¹⁴ molecules/cm².

EXAMPLE: chamber of 1 meter, ϕ =80 mm (LHC): S_{H2}~750 l/s; S_{C0}~10000 l/s; Capacity for CO ~1.25x10¹⁸ molecules:

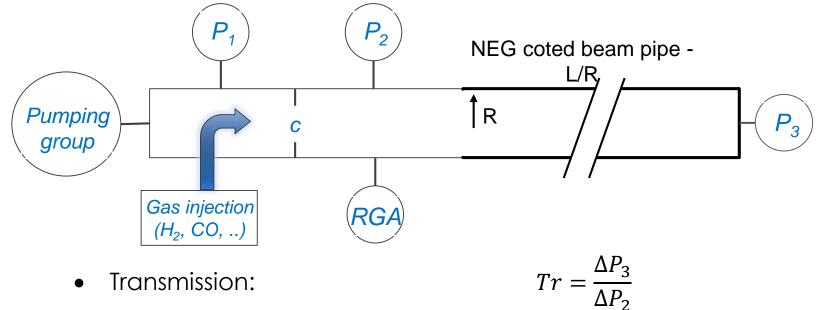
Leak rate [mbar.l/s]	Time to saturate
10 ⁻⁵	~1 hours
10 ⁻⁷	~4.5 days
10 ⁻⁹	~1.3 years
10 -11	~125 years



Zero order approach: considers homogeneous saturation.



Evaluation of NEG performance



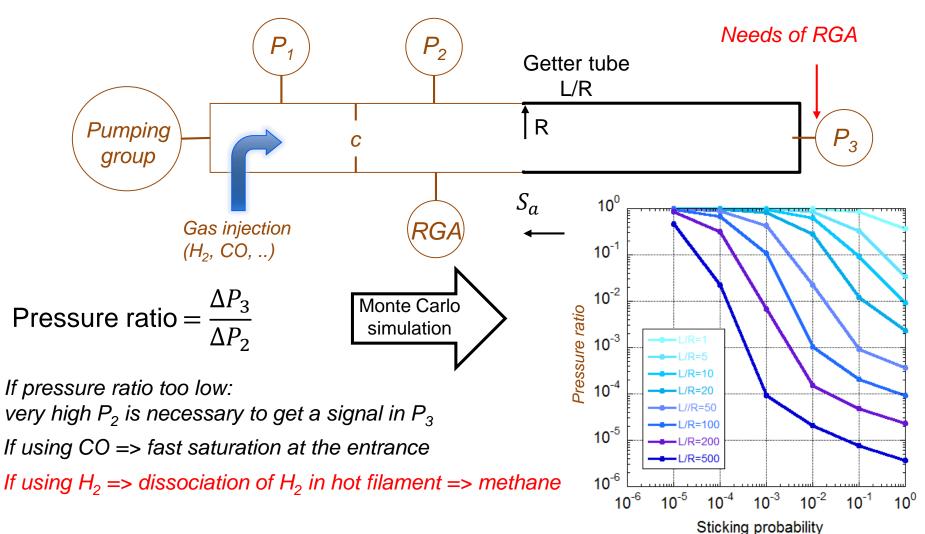
- Pumping speed: $S = \frac{Q}{\Delta P_{BEGIN}} [l/s]$
- Capture probability:

$$CP = \frac{S}{C_{AP}}$$



Practical use of NEG coatings

Measure the pumping speed of a thin film: transmission method

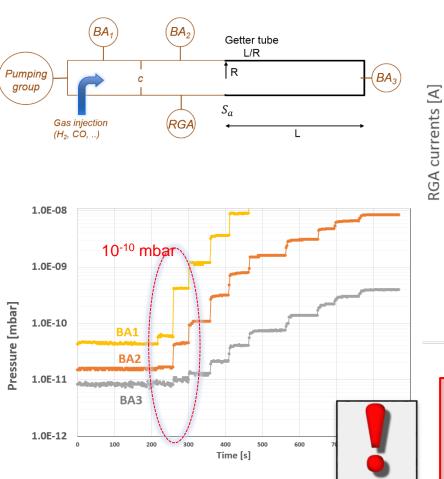


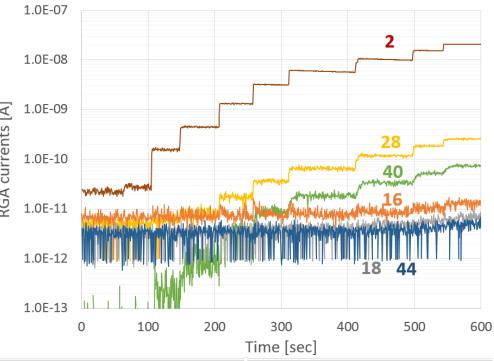


EVC13

Courtesy: P.Costa Pinto & G.Bregliozzi

NEG Transmission limitation: H₂ Injection





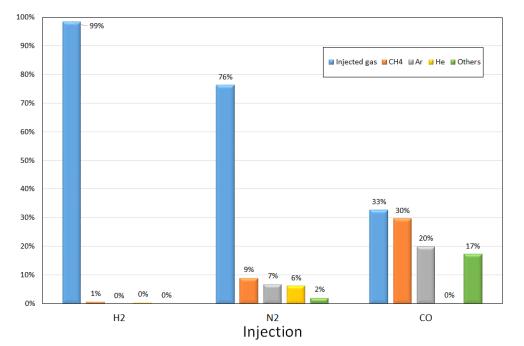
In case of long coated beam pipe need to carefully consider the cleanliness of the injection line and presence of hot filaments or selective pumping in the system.



Transmission method limitations

NEG Coated copper beam pipe - Length of 1 m – ϕ 80 mm

- H₂ injection: 99% of the total pressure is due to hydrogen, allowing to always use the ΔP_{TOTAL} transmission to evaluate the sticking factor
- N_2 injection: 26% of the total pressure is due to methane and noble gases, so the $\Delta P_{PARTIAL}$ transmission has to be used.



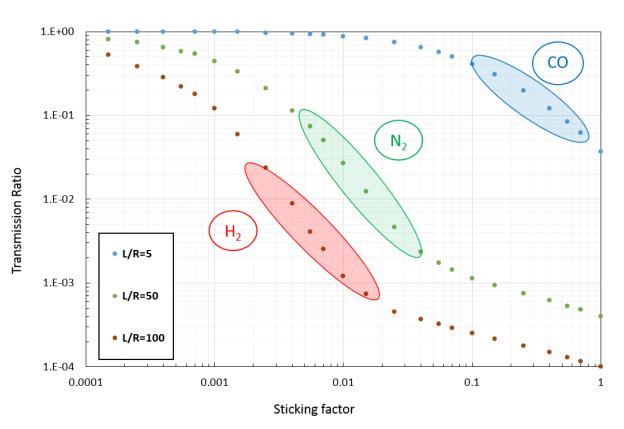
CO injection: 66% of the pressure reading is due to gases others than CO. Only using $\Delta P_{PARTIAL}$ transmission it is possible to obtain representative results.



Transmission method optimization

- The sticking factor strongly depends on the ratio L/R between the length and the radius of the chamber
- To have representative sticking factor values the transmission has to be in the range where the curve is steepest
- Different gases have different sticking factors

	Sticking factor		
H_2	$7.0 \cdot 10^{-3}$ - $7.0 \cdot 10^{-4}$		
N_2	$5.0 \cdot 10^{-2}$ - $1.2 \cdot 10^{-3}$		
CO	$7.0 \cdot 10^{-1}$ - $1.2 \cdot 10^{-2}$		





Conclusion & Advices

- Need to clearly analyze and define which is your driving parameter and then set the acceptance criteria;
- Once defined stick to the acceptance limits and try to be always coherent;
- Define gas density more than general pressure;
- Try to find a compromise: Do not be too stringent
- Be flexible on the total outgassing but do not accept any form of contaminations;
- Participate as much as possible to the design phase to eliminates problems and non conformities at the source.

You'll be able to predict much better your vacuum system, anticipate problems and malfunctioning and have fastest and simpler intervention in the accelerators.



.....thank you very much for your attention





Vacuum for Particle Accelerators Glumslöv, Sweden, 6 - 16 June, 2017



Additional Slides:

Some special needs and examples



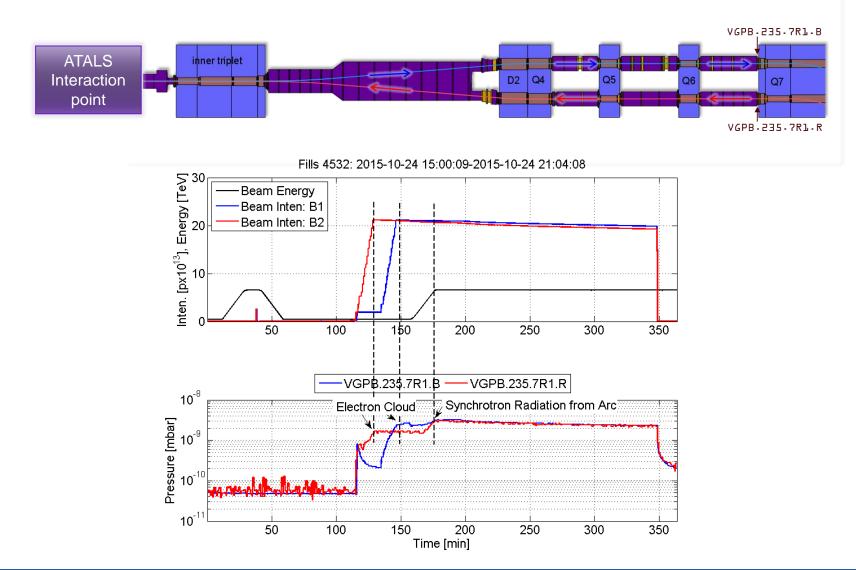
What about beam induced pressure increase?

How to deal with it?

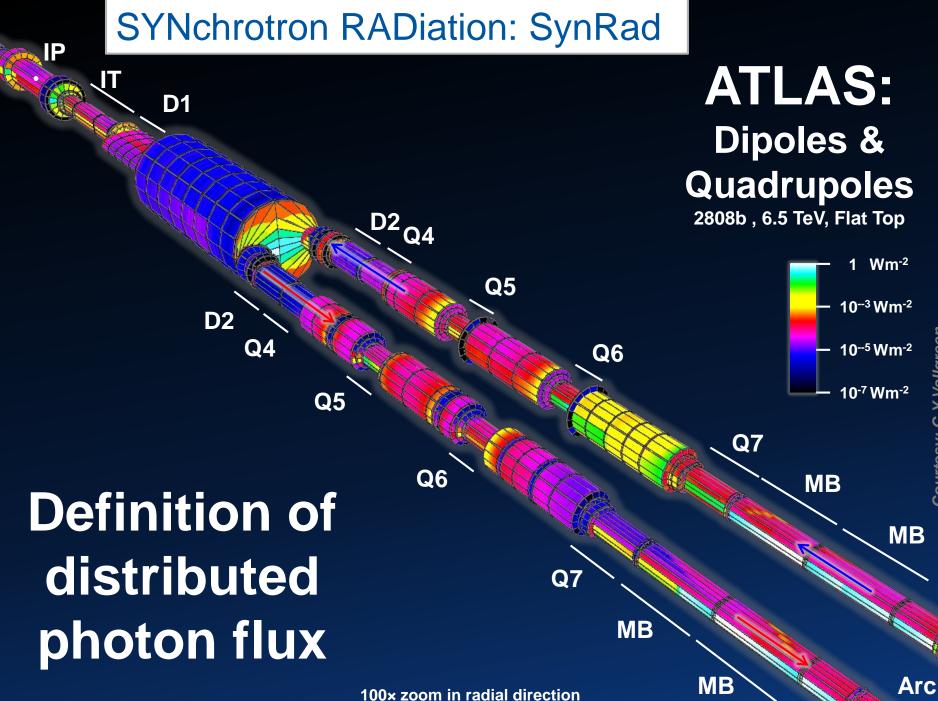
An example in case of electron and photon flux



Beam induced pressure increase



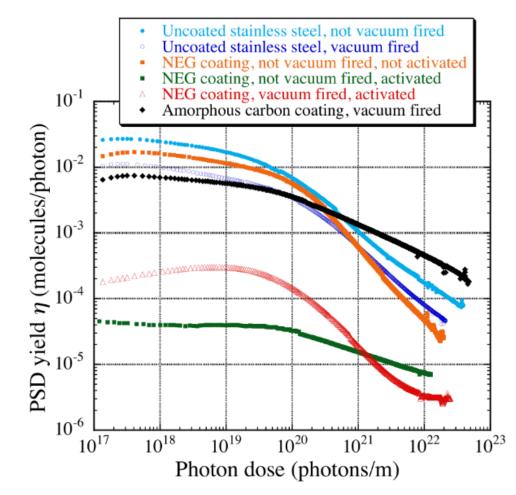




Material characterization: η_{ph}

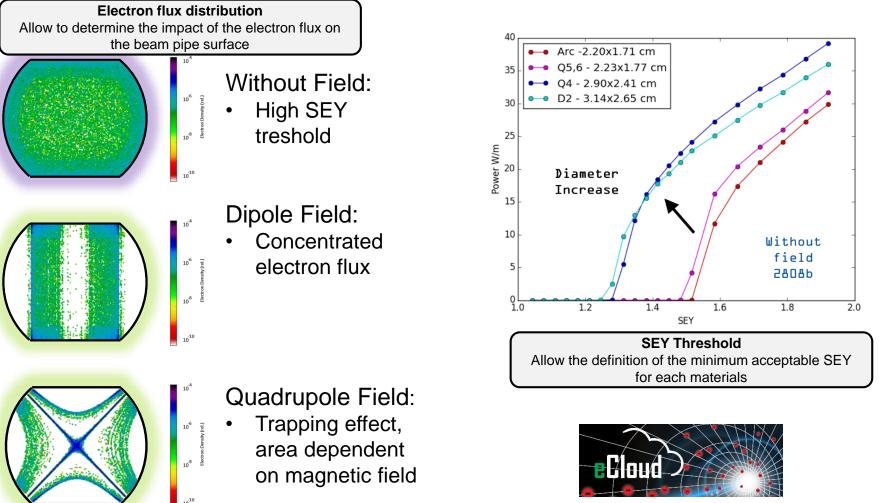
Sample Treatment and coating

- 1 Reference stainless steel sample basic treatment only
- 2 Stainless steel sample vacuum fired
- 3 TiZrV NEG coating not activated
- 4 TiZrV NEG coating, activated prior to the experiment
- 5 TiZrV NEG coating vacuum fired, activated
- 6 Amorphous carbon coating vacuum fired





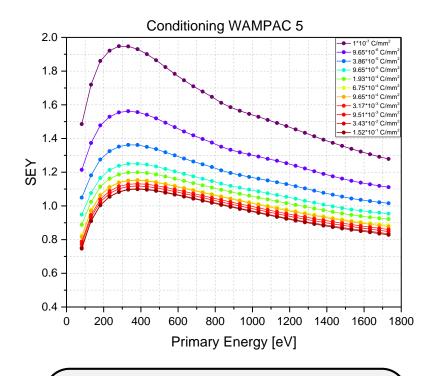
Definition of the SEY Threshold & Electron Flux





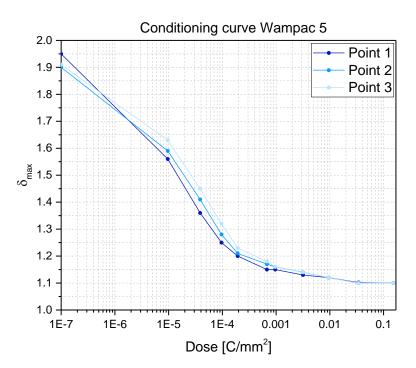
Example of LHC Beam Screen

Material characterization





- The SEY scan allow determining the secondary electron evolution function of primary energy;
- Accumulating electron dose bombardment it reduces the SEY and allow to create the 'conditioning' curve;



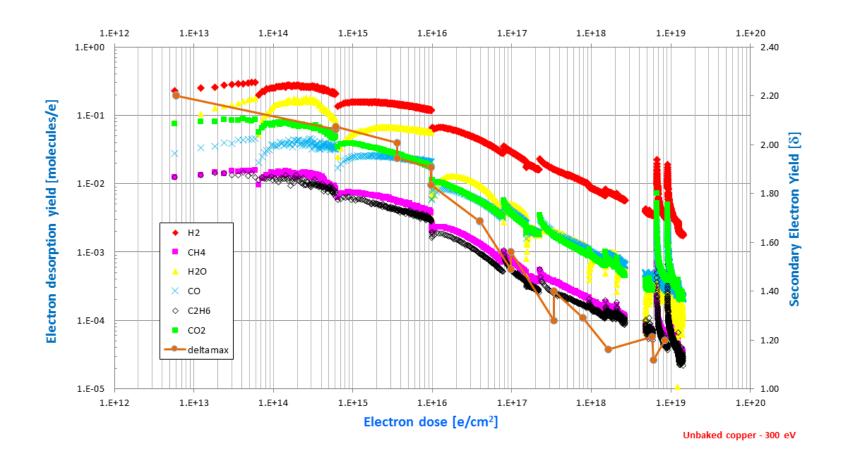
Conditioning Curve:

 Allow determining and the SEY evolution and study its impact function of the simulated SEY threshold and electron flux.



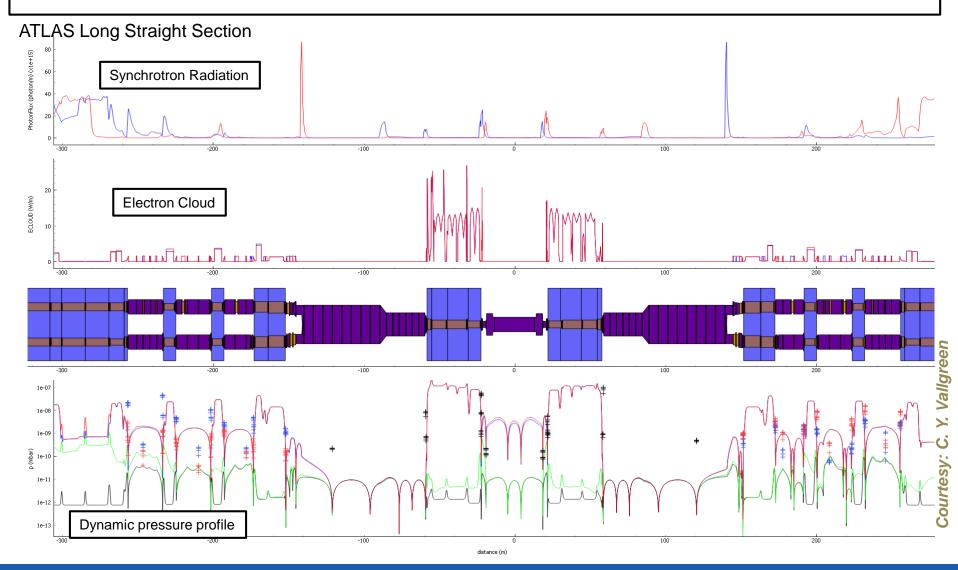
Courtesy: R.Salemme & M.Taborelli

Material characterization: η_{el}





Synchrotron Radiation & Electron Cloud Dynamic Pressure Profile: VAcuum Stability COde (VASCO)





New Sintered Materials

new materials characterisation, MoGr

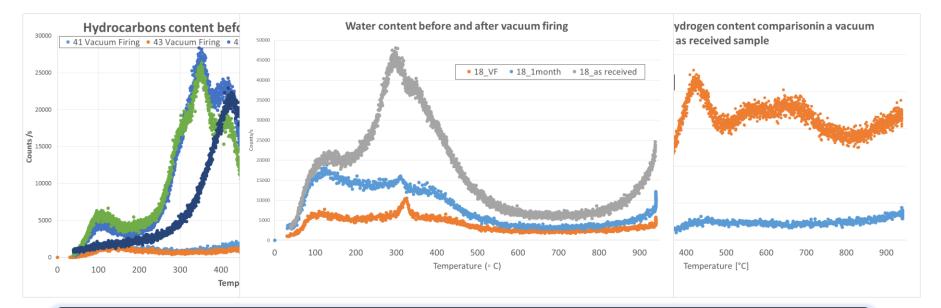
Two aradas have h Two aradas have h					
far, with same initial composition			Atmosphere: air	T=250°C Atmosphere: vacuum	
but different atmospheres during the production process.	* %vol Mo=4.5	Sintering	T=2300°C Duration= 2400s Atmosphere: vacuum Venting gas: air	T=2300°C Duration= 2400s Atmosphere: vacuum Venting gas: Ar	
	%vol Graphite=95.3 %vol Ti=0.2	Post sintering	T=2400°C Duration= 3000s	T=2400°C Duration= 3000s	



Venting gas: air

Venting gas: Ar

New Sintered Materials Thermal Desorption Spectroscopy of MoGr

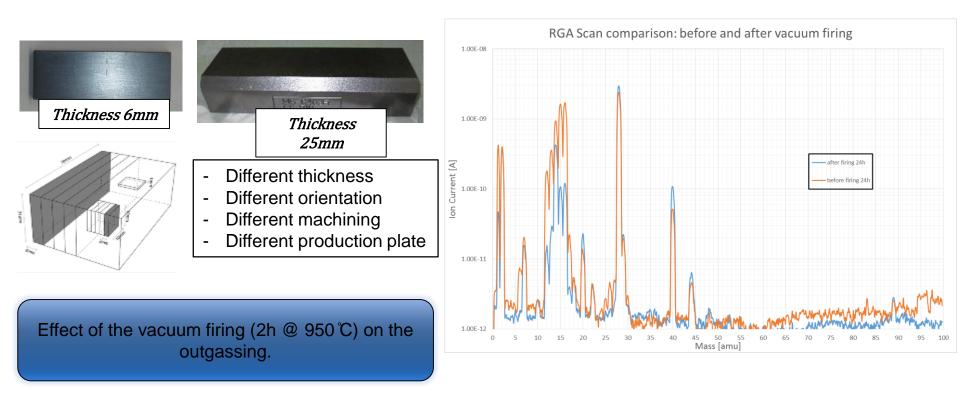


TDS (Thermal desorption spectroscopy) is used to study gases evolution from the material under different conditions (before and after vacuum firing, air time exposure..).



New Sintered Materials

new materials characterisation, MoGr

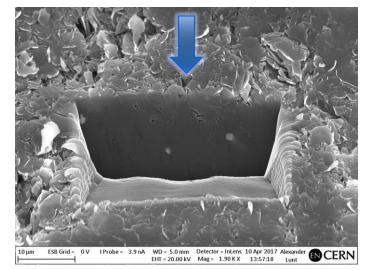


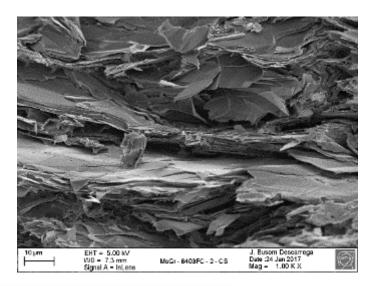


New Sintered Materials

new materials characterisation, MoGr

Ion beam





Focus Ion Beam and SEM analysis to evaluate the presence of voids, pores and surface damages induced by machining.



Glue or "strange materials" v.s. NEG

 Few tests done to validate the use of small not conventional components with NEG: Finally validated by XPS*



	Chamber 1	Chamber 2
Step 1 – Temp for 24h	250°C	120°C
Step 2 - Temp for 24h	150°C	180-250°C
		*\/



XPS on NEG coated sample

