

# RF Cavity Design - an introduction -



Oxford – John Adams Institute

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Ciprian Plostinar

# Overview

## Part 1:

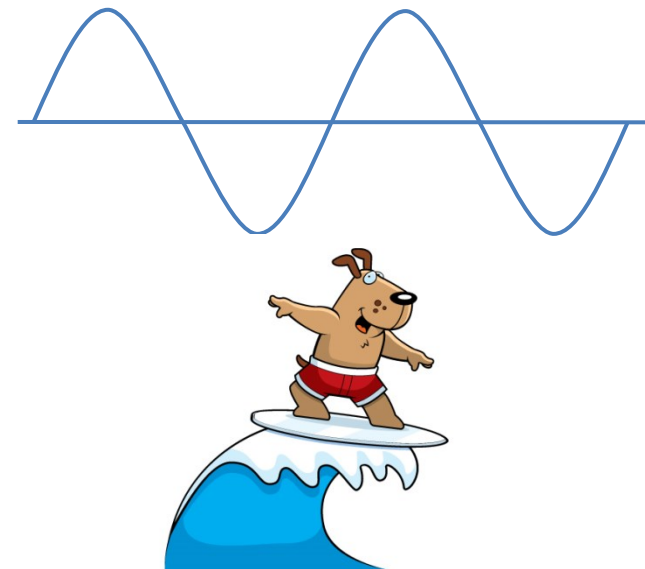
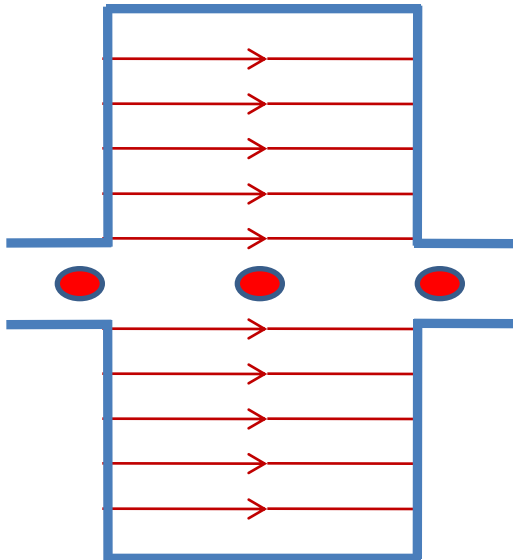
- RF Cavity Design
  - Design Criteria
  - Figures of Merit
- Introduction to Superfish (2D)
- Examples:
  - Pill-box type cavity
  - DTL type cavity
  - Elliptical cavity
  - A ferrite loaded cavity

## Part 2:

- CST MicroWave Studio Demo (3D)
- Surprise Cavity Model
- A Simple Measurement

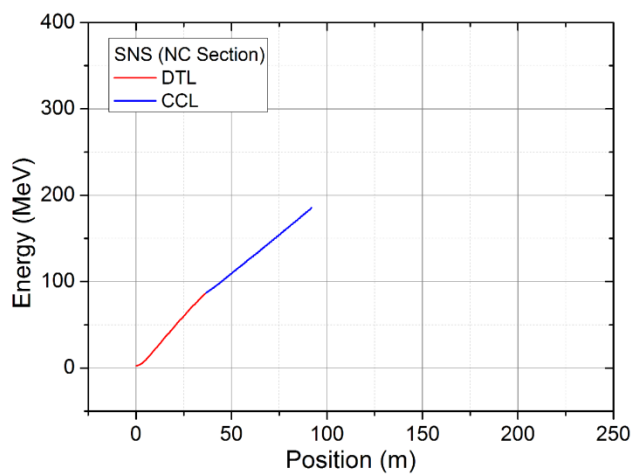
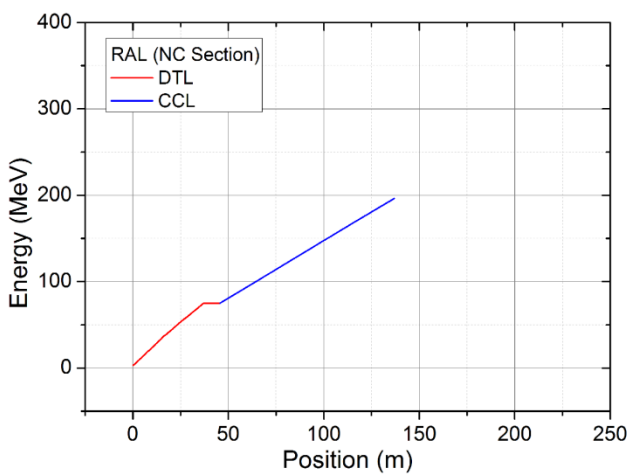
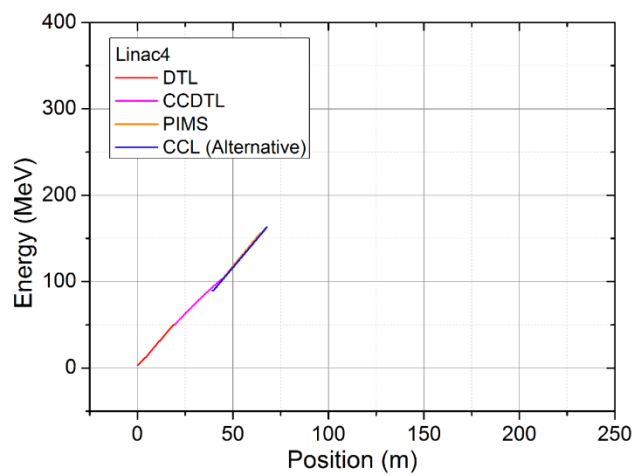
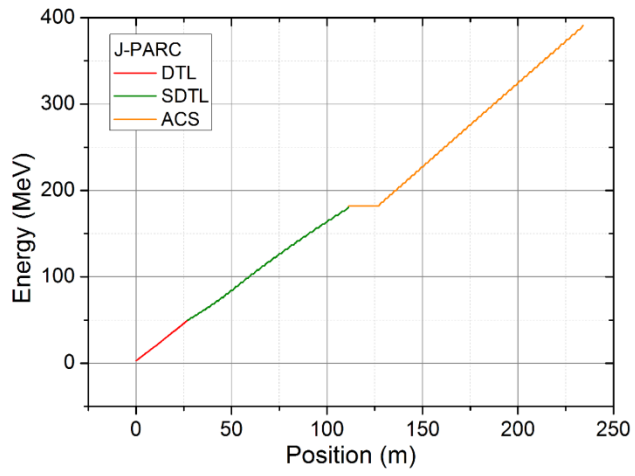
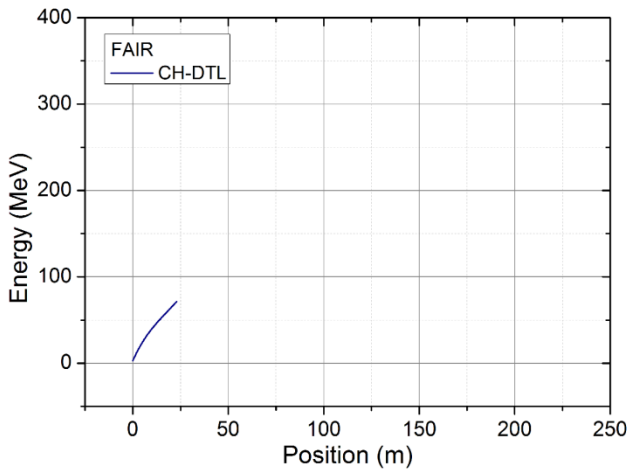
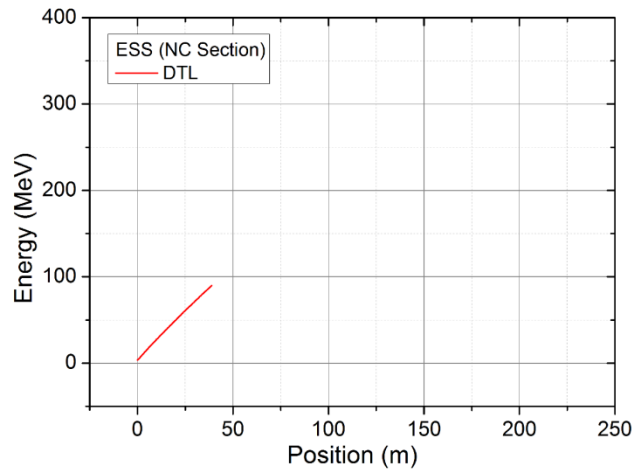
# RF Cavity Design

- In most particle accelerators, the energy is delivered to the particle by means of a large variety of devices, normally known as **cavity resonators**.
- The ideal cavity: volume of perfect dielectric limited by infinitely conducting walls.
- Hollow cylindrical resonator excited by a radio transmitter -> standing wave -> accelerating fields (the pillbox cavity).



# Why Cavity Design Is Important?

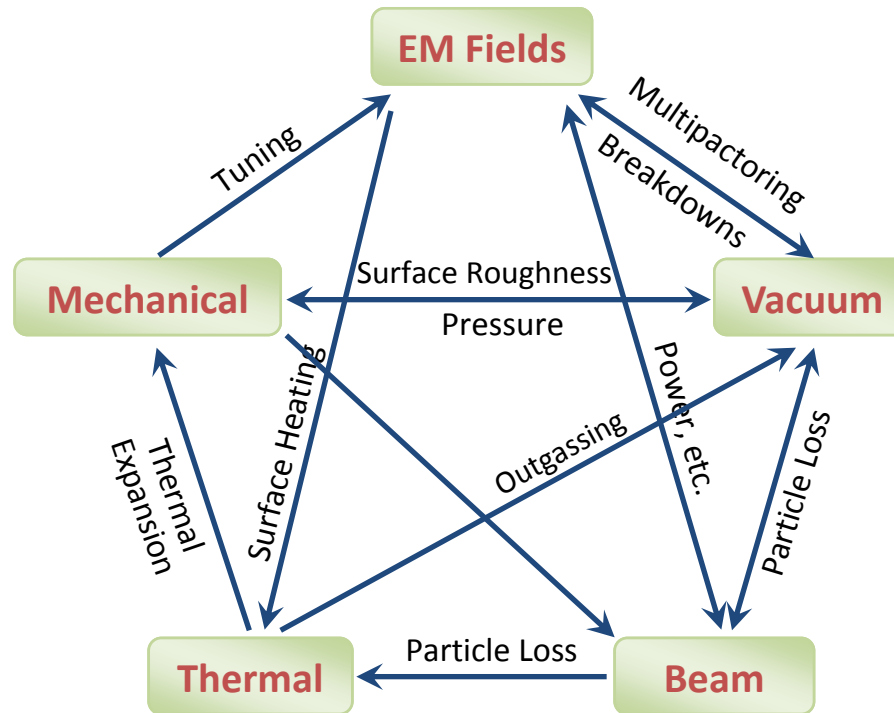
## Acceleration Profile in Several Linacs



# Design Criteria

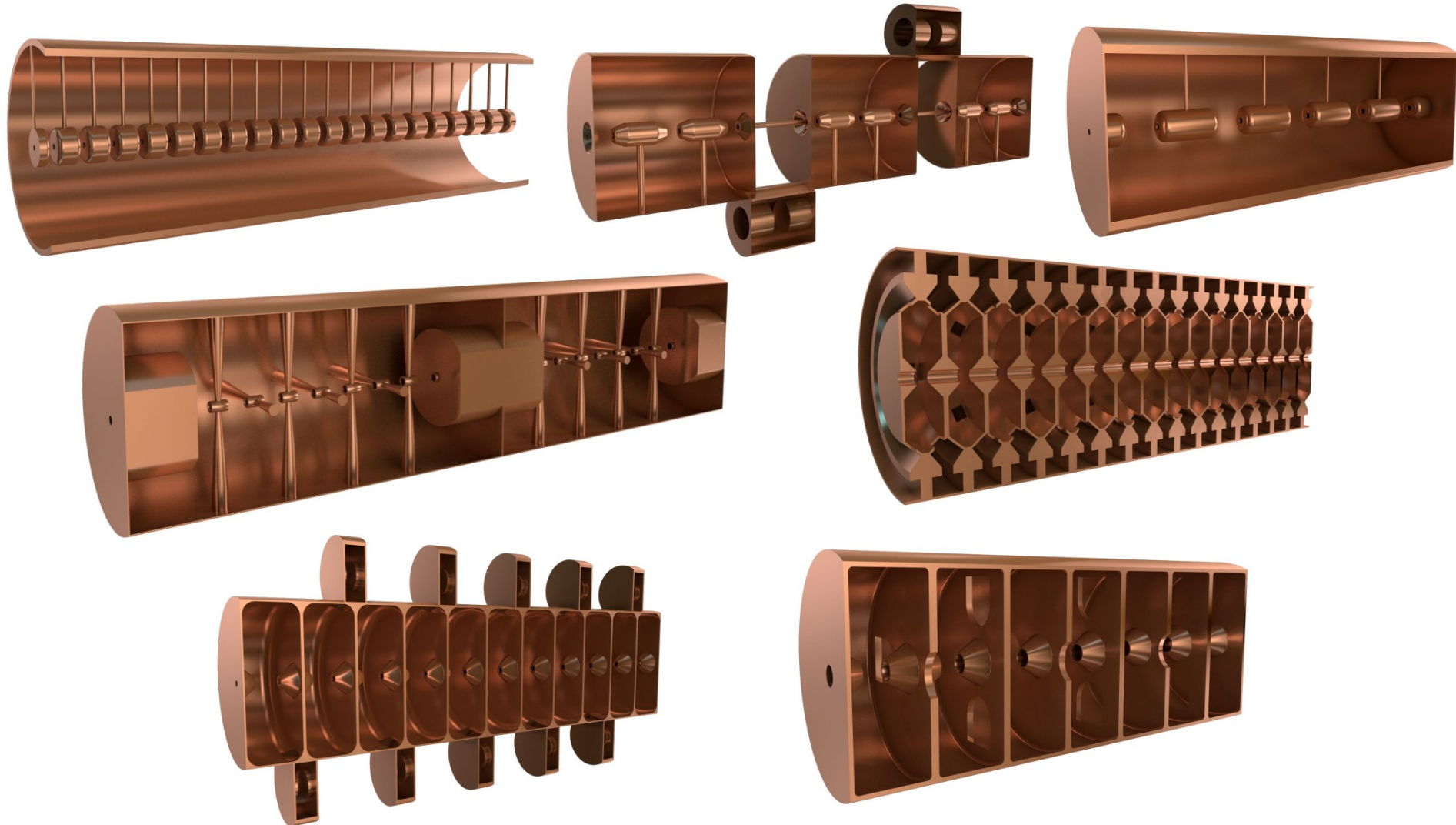
- Define the requirements (intended application), RF frequency, NC/SC, voltage, tuning, etc.
- General design criteria:
  - Power Efficiency & RF Properties
  - Beam Dynamics considerations (control of loss and emittance growth, etc.) – especially true for linacs
  - Technologies and precisions involved
  - Tuning procedures (frequency, field profile, stability against perturbations)
  - Sensitivity to RF errors (phase and amplitude)
  - Etc.

# The “Magic Pentagon” of Cavity Design



- The pentagon shows the importance of each design and manufacturing choice
- Technologies are interdependent

# Cavity Zoo

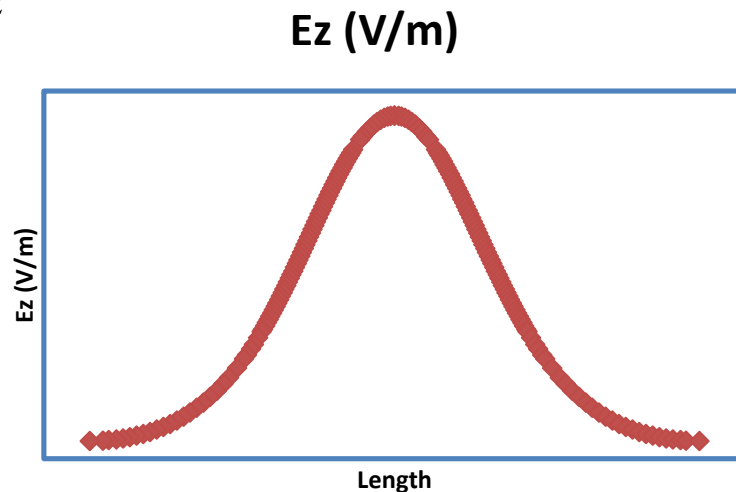
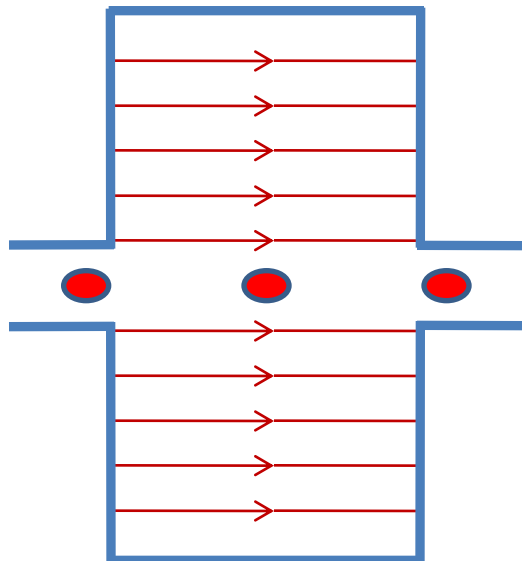


# Figures of Merit

## The Transit Time Factor, T

- While the particle crosses the cavity, the field is also varying -> less acceleration -> the particle sees only a **fraction** of the peak voltage -> T is a measure of the reduction in energy gain cause by the sinusoidal time variation of the field in the cavity.

$$T = \frac{\int_{-L/2}^{L/2} E(0, z) \cdot \cos \frac{2\pi z}{\beta\lambda} dz}{\int_{-L/2}^{L/2} E(0, z) dz}$$





# Figures of Merit

## The Quality Factor, Q

$$Q_0 = \frac{2\pi \cdot \text{stored energy}}{\text{energy consumed per period}} = \frac{2\pi W}{TP_0} = \omega \frac{U}{P_0}$$

- To first order, the Q-value will depend on the conductivity of the wall material only
- High Q -> narrower bandwidth -> higher amplitudes
- But, more difficult to tune, more sensitive to mechanical tolerances (even a slight temperature variation can shift the resonance)
- Q is dimensionless and gives only the ratios of energies, and not the real amount of power needed to maintain a certain resonant mode
- For resonant frequencies in the range 100 to 1000 MHz, typical values are 10,000 to 50,000 for normal conducting copper cavities;  $10^8$  to  $10^{10}$  for superconducting cavities.

# Figures of Merit

## Shunt Impedance

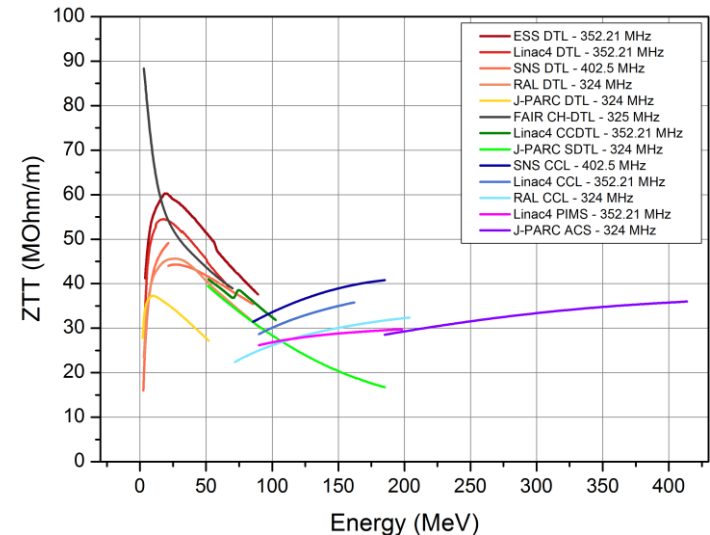
- A measure of the effectiveness of producing an axial voltage  $V_0$  for a given power dissipated

$$r_s = \frac{V_0^2}{P_0}$$

- Effective Shunt Impedance per unit length

$$ZT^2 = \frac{r}{L} = \frac{(E_0 T)^2}{P_0 / L}$$

- Typical values of  $ZT^2$  for normal conducting linacs is 30 to 50  $M\Omega/m$ . The shunt impedance is not relevant for superconducting cavities.



# Figures of Merit

**r/Q**

- measures the efficiency of acceleration per unit of stored energy at a given frequency

$$\frac{r}{Q} = \frac{(V_0 T)^2}{\omega U}$$

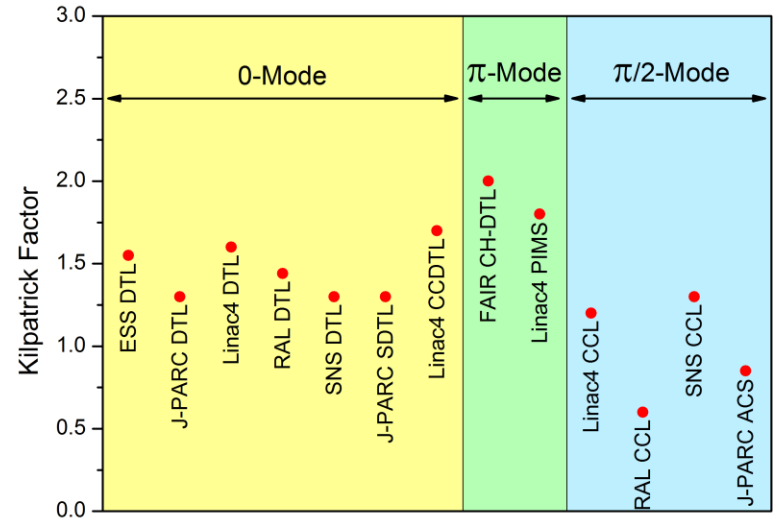
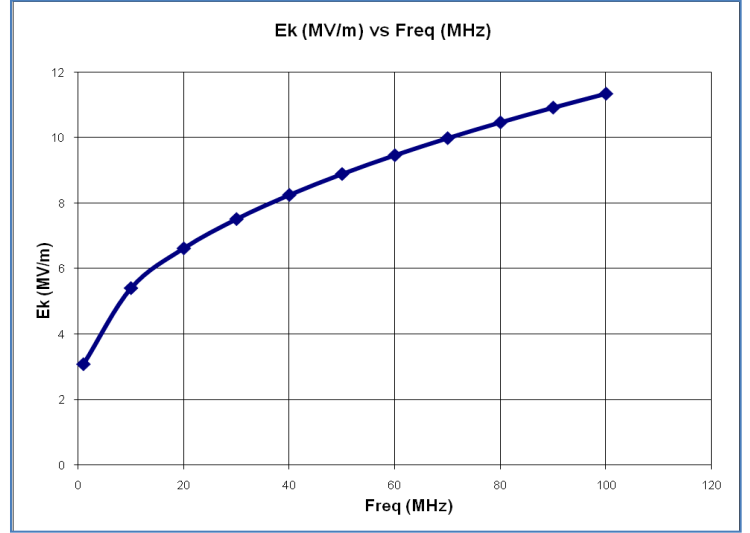
- It is a function only of the cavity geometry and is independent of the surface properties that determine the power losses.

# Figures of Merit

## The Kilpatrick limit

- High Field -> Electric breakdown
- Maximum achievable field is limited

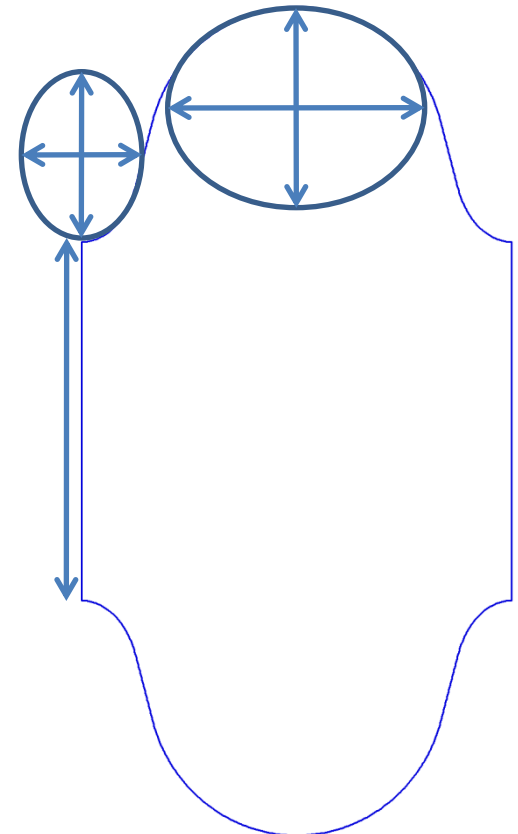
$$f = 1.64 E_k^2 e^{-8.5/E_k}$$



# Figures of Merit

## Superconducting Cavities (Slightly different story for ):

- $r/Q$  (characteristic impedance)
- $G$  (Geometric Factor - the measure of energy loss in the metal wall for a given surface resistance)
- $E_{\text{peak}}/E_{\text{acc}}$  - field emissions limit (Eacc limit)
- $B_{\text{peak}}/E_{\text{acc}}$  – quench limit (sc breakdown)
- Higher Order Modes – manage and suppress HOM (e.g.: dipole modes can degrade the beam  $\rightarrow$  suppression scheme using HOM couplers)
- $K_{\text{cc}}$  – Cell to cell coupling
- Multicell cavities: Field Flatness
- Optimise geometry to increase both  $r/Q$  and  $G$  resulting in less stored energy and less wall loss at a given gradient (low cryogenic losses)
- Optimise geometry to reduce  $E_{\text{peak}}/E_{\text{acc}}$  and  $B_{\text{peak}}/E_{\text{acc}}$
- Find optimum  $K_{\text{cc}}$ . (e.g.: a small aperture increases  $r/Q$  and  $G$  (!), but reduces  $K_{\text{cc}}$ . A small  $K_{\text{cc}}$  increases the sensitivity of the field profile to cell frequency errors.)



# Introduction to Poisson Superfish

- You will need a laptop running Windows. If you have Linux/MacOS install VMWare/Wine.
- Please download and install Poisson Superfish. To do this go to the following address and follow the instructions:  
[http://laacg1.lanl.gov/laacg/services/download\\_sf.phtml](http://laacg1.lanl.gov/laacg/services/download_sf.phtml)
- Please download the example files to your computer from the JAI website.
- An extensive documentation can be found in the Superfish home directory (usually C:/LANL).
  - Have a look at the SFCODES.DOC file. Table VI-4 explains how the object geometry is defined in Superfish (page 157).
  - For a list of Superfish variables, see SFINTRO.doc, Table III-3 (page 76)
- For any questions, email Emmanuel ([emmanuel.tsesmelis@cern.ch](mailto:emmanuel.tsesmelis@cern.ch)) or Ciprian ([ciprian.plostinar@stfc.ac.uk](mailto:ciprian.plostinar@stfc.ac.uk)). Good luck!

# Introduction to Poisson Superfish

- Poisson and Superfish are the main solver programs in a collection of programs from LANL for calculating static magnetic and electric fields and radio-frequency electromagnetic fields in either 2-D Cartesian coordinates or axially symmetric cylindrical coordinates.
- Finite Element Method

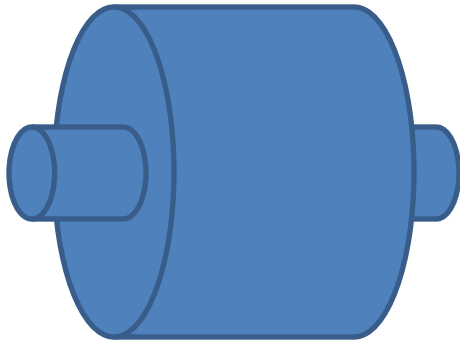
## Solvers:

- **Automesh** – generates the mesh (always the first program to run)
- **Fish** – RF solver
- **Cfish** – version of Fish that uses complex variables for the rf fields, permittivity, and permeability.
- **Poisson** – magnetostatic and electrostatic field solver
- **Pandira** – another static field solver (can handle permanent magnets)
- **SFO, SF7** – postprocessing
- **Autofish** – combines Automesh, Fish and SFO
- **DTLfish, DTLCells, CCLfish, CCLcells, CDTfish, ELLfish, ELLCAV, MDTfish, RFQfish, SCCfish** – for tuning specific cavity types.
- **Kilpat, Force, WSFPlot**, etc.



# A Pillbox Cavity

- The simplest RF cavity



For the accelerating mode ( $TM_{010}$ ), the resonant wavelength is:

$$\lambda = \frac{\pi D}{x_1}$$

$$x_1 = 2.40483$$

$x_1$  - first root of the zero-th order Bessel function  $J_0(x)$

- > Resonant frequency independent of the cell length
- > Example: a 40 MHz cavity (PS2) would have a diameter of  $\sim 5.7$  m
- > In the picture, CERN 88 MHz





# A Pillbox Cavity

## Superfish input file

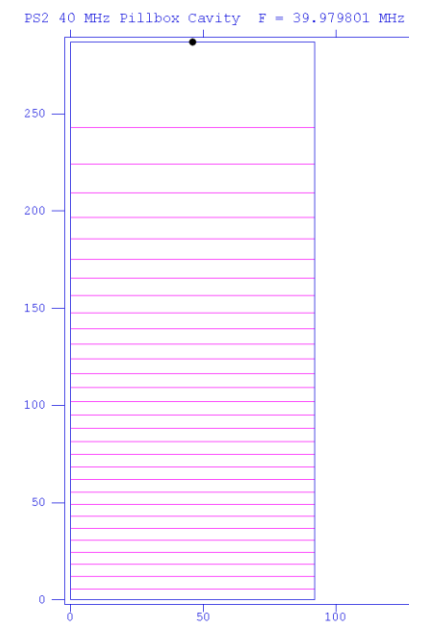
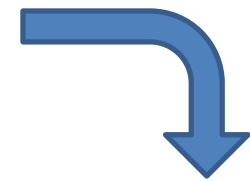
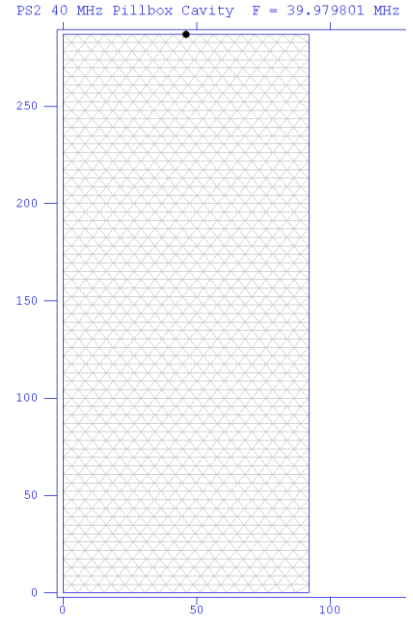
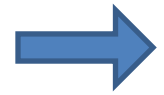
```

PS2 40 MHz Pillbox Cavity

PARTICLE H-,
$reg kprob=1,           ; Superfish problem
dx=5,                  ; X mesh spacing
freq=40.,              ; Starting frequency in MHz
icylin=1

xdri=46.,ydri=287 $    ; Drive point location

$po x=0.0,y=0.0 $      ; Start of the boundary points
$po x=0.0,y=287 $
$po x=92,y=287 $
$po x=92,y=0.0 $
$po x=0.0,y=0.0 $
  
```



```

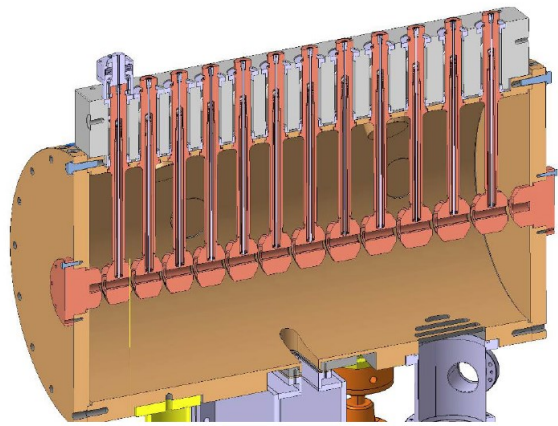
Lister - [c:\_Current Projects\Superfish Course Oxford\Example 1\PILLBOX.SFO]
File Edit Options Help 100 %

-----
All calculated values below refer to the mesh geometry only.
Field normalization (NORM = 0):  EZERO = 1.00000 MV/m
Frequency = 39.97980 MHz
Particle rest mass energy = 938.272029 MeV
Beta = 0.2453792 Kinetic energy = 29.590 MeV
Normalization factor for E0 = 1.000 MV/m = 5187.056
Transit-time factor = 0.0001158
Stored energy = 28.3520963 Joules
Using standard room-temperature copper.
Surface resistance = 1.64961 milliohm
Normal-conductor resistivity = 1.72410 microhm-cm
Operating temperature = 20.0000 C
Power dissipation = 25.9402 kW
Q = 274557. Shunt impedance = 35.466 Mohm/m
Rs*Q = 452.911 Ohm 2*T*I = 0.000 Mohm/m
r/Q = 0.000 Ohm Wake loss parameter = 0.00000 U/pC
Average magnetic field on the outer wall = 1376.86 A/m, 156.361 mW/cm^2
Maximum H (at Z,R = 74.1111,287) = 1376.86 A/m, 156.361 mW/cm^2
Maximum E (at Z,R = 89.4404,287) = 1.00783E-04 MV/m, 1.22091E-05 K1lp.
Ratio of peak fields Bmax/Emax = 17167.7287 mT/(MV/m)
Peak-to-average ratio Emax/E0 = 0.0001

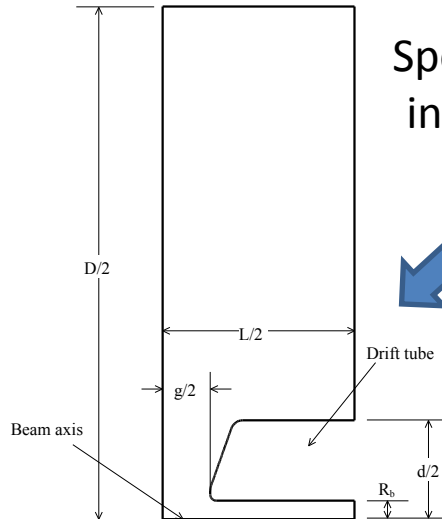
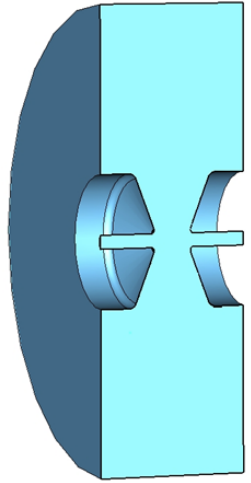
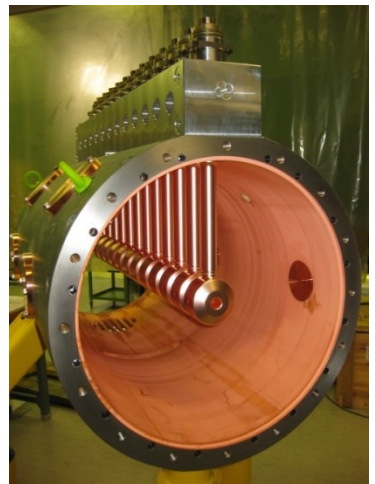
Wall segments:
Segment Zend Rend Enax Power P/R dF/dZ dF/dR
(cm) (cm) (MW/m) (kW) (mW/cm^2) (MHz/mm) (MHz/mm)
-----
0.0000 287.00
2 92.000 287.00 1.2258E-04 25.94 156.4 0.000 -1.3933E-02
-----
Total 25.94
  
```

# A DTL-type Cavity

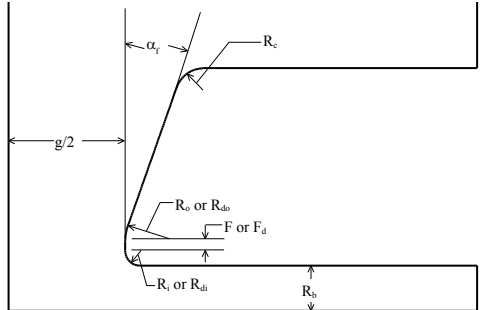
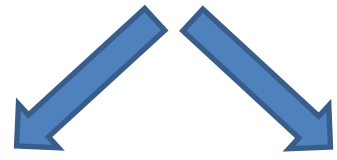
- Drift Tube Linac Cavity



← CERN Linac4 DTL prototype →



Special Superfish input geometry



# A DTL-type Cavity

Superfish input file

```

File Edit Options Help 100 %
Title
DTL-type cavity
Resonant Frequency = 324 MHz
ENDTitle

PARTICLE          H-
InitialEnergy      3      ; Energies used in program DTLCells

FILENAME_prefix   DTL
SEQUENCE_number   1
FREQUENCY         324
BETA              0.079732
LENGTH           7.37748526582
DIAMETER         55.81982579555
G_OVER_Beta_lambda 0.2
GAP_Length       1.475497853164
E0_Normalization 2.5
E0T_Normalization 1.65138369868
CORNER_radius    0.5
INNER_nose_radius 0.15
OUTER_nose_radius 0.3
FLAT_length      0.2
FACE_angle       18
DRIFT_TUBE_Diameter 18
GAP_Change       0.0
STEIN_Diameter   3
STEIN_Count      1
BORE_radius      1.4
PHASE_length     180
DELTA_Frequency  0.01
MESH_Size        0.02
INCREMENT        2
START            4

; Start codes for DTLfish:
; 1 No tuning
; 2 Adjust tank diameter
; 3 Adjust drift tube diameter (not recommended)
; 4 Adjust gap
; 5 Adjust Face angle

EndFile
  
```

Geometry file

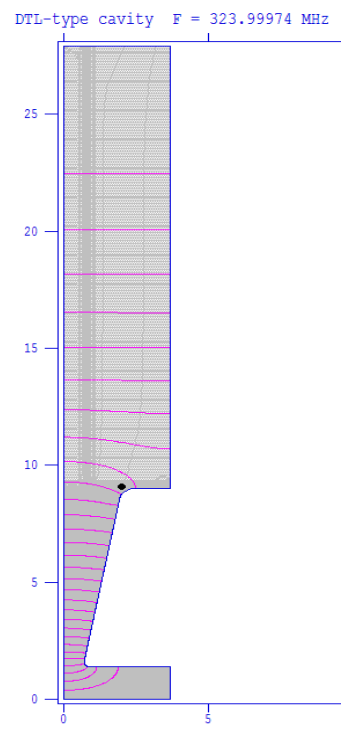
```

File Edit Options Help 100 %
DTL-type cavity
Resonant Frequency = 324 MHz
Adjusting gap, currently = 1.4754971, g/bl = 0.2000000

$REG KPROB=1      ; Superfish problem
MFI=1            ; Material air or empty space
FREQ=323.9997439729 ; Mode Frequency, starting Frequency in Fish solv
FREQ0=324        ; Design Frequency, used (with BPH1) to compute w
BETA=0.079732    ; Particle velocity, used to compute wave number
KNETH00=1       ; SFD will use BETA to compute wave number
DPHI=180        ; Phase length of the half cavity, used (with FRE
NBSUP=1,NBSLO=0,NBSRT=1,NBSLF=1 ; Boundary conditions
LINES=1         ; Fix internal points on line regions
ICVLIH=1       ; X>2,Y>R, cylindrical coordinates
NBMH=0         ; Normalize to EZERO
EZERO=2500000   ; Accelerating field
DIL=1          ; Cavity is drift-tube linac
RMSS=3         ; Best mesh value or indicator
EPS0=1.0E-6    ; Mesh optimization convergence parameter
IRIYPE=0       ; RS method: Normal conductor formula
XDRI=1.098814697996 ; Drive point X coordinate
VDRI=9.09621635729 ; Drive point Y coordinate
DLSUPE=1      ; Allow convergence in 1 iteration
; X line-region physical locations:
XREG=0.557748526582,0.677748526582,0.947748526582,1.067748526582,
; X line-region logical locations:
XREG=1,0,11,25,28,
KMX=62         ; Column number for X = XMX
; V line-region physical locations:
VREG=0.0282842712475,1.357573593129,3.698196086483,9.084852813742,
9.36769526217,
; V line-region logical locations:
VREG=1,3,51,219,418,415,
LMAX=580 &    ; Row number for V = VMX

; Start of boundary points
BPO X=0,V=0 & ; 1
BPO X=0,V=27.98991289778 & ; 2
BPO X=3.68874263291,V=27.98991289778 & ; 3
BPO X=3.68874263291,V=9 & ; 4
BPO X=2.431048968741,V=9 & ; 5
BPO NT=2,X=2.431048968741,V=8.5, ; 6
X= -0.4924838765861,V=0.084824888835 & ; 7
BPO X=0.742302086783,V=-1.820948533 & ; 8
BPO NT=2,X=-1.837748526582,V=0-1.75, ; 9
X= -0.3,V=0 & ; 10
BPO X=0.737748526582,V=1.55 & ; 11
BPO NT=2,X=0.887748526582,V=0-1.55, ; 12
X=0,V=-8.15 & ; 13
BPO X=3.68874263291,V=-1.4 & ; 14
BPO X=3.68874263291,V=0 & ; 15
BPO X=0,V=0 & ; 16
  
```

Solution

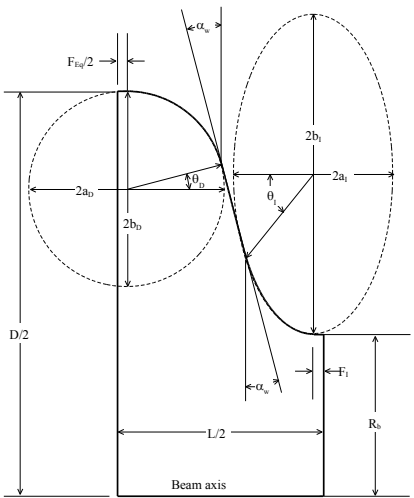


# An Elliptical Cavity

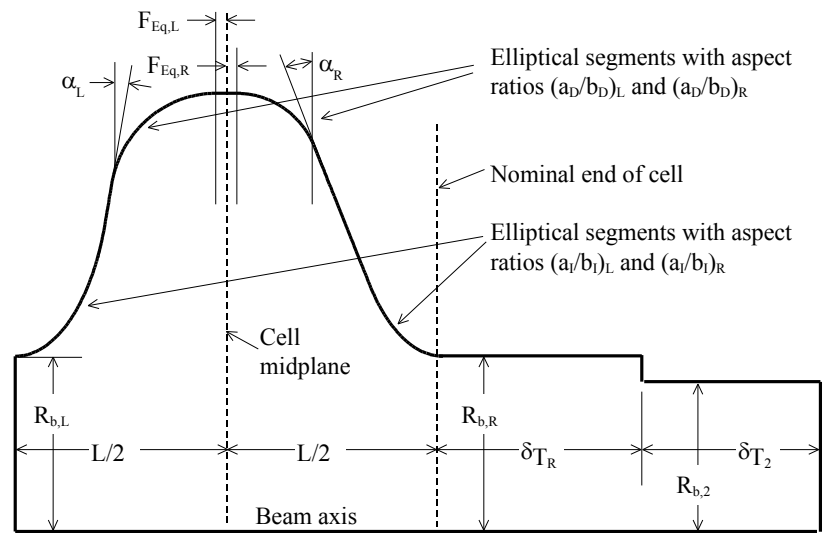
- Often used in superconducting applications



INFN & CEA 704 MHz elliptical SC cavities



Special Superfish input geometry



# An Elliptical Cavity

Superfish input file

Geometry file

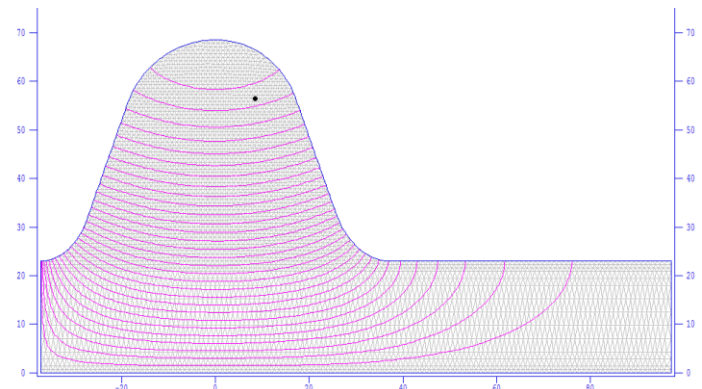
```

Elliptical Cavity - Notepad
File Edit Format View Help
Title
Tuning elliptical cavity NF muon linac
Design beta = 1
Resonant frequency = 201.49 MHz, Bore radius = 23.00 cm
ENDTITLE
REST_mass          105.658369
SUPERCONDUCTOR    2 9.2 1.0E-08
numberofcells      10 ; used by the ELLCAV code
FULL_cavity
FILENAME_prefix    elliptical
SEQUENCE_number    1
FREQUENCY          201.249
BETA               1
LENGTH            74.48296836258
DIAMETER          137.091519298
EO_Normalization  14.81357443775
LOI_Normalization 20
DOME_B           18.16662400282
LEFT_DOME_B      1
RIGHT_DOME_B     1
DOME_A/B         1
LEFT_DOME_A/B   1
RIGHT_DOME_A/B  1
WALL_angle      20
LEFT_WALL_angle 20
RIGHT_WALL_angle 20
EQUATOR_flat    0.0
LEFT_EQUATOR_flat 0.0
RIGHT_EQUATOR_flat 0.0
IRIS_flat       0.0
LEFT_IRIS_flat  0.0
RIGHT_IRIS_flat 0.0
RIGHT_BEAM_tube 60
IRIS_A/B        0.7
LEFT_IRIS_A/B   0.7
RIGHT_IRIS_A/B  0.7
BETASTART       0.0
BETASTOP        0.0
BETASTEP        0.0
BETATABLE       0.0
BORE_radius     23
LEFT_BORE_radius 23
RIGHT_BORE_radius 23
SECOND_BEAM_tube 0.0
SECOND_TUBE_radius 0.0
DELTA_Frequency 0.01
MESH_size      1
INCREMENT      1
START          1
; Start codes for ELLfish:
; 1 No tuning
; 2 Adjust diameter
; 3 Adjust dome ellipse size
; 4 Adjust wall slope
; 5 Adjust wall slope with fixed iris ellipse size
; (Right side only in full cavities for 3, 4, and 5.)
EndFile
    
```

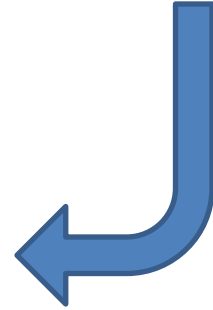
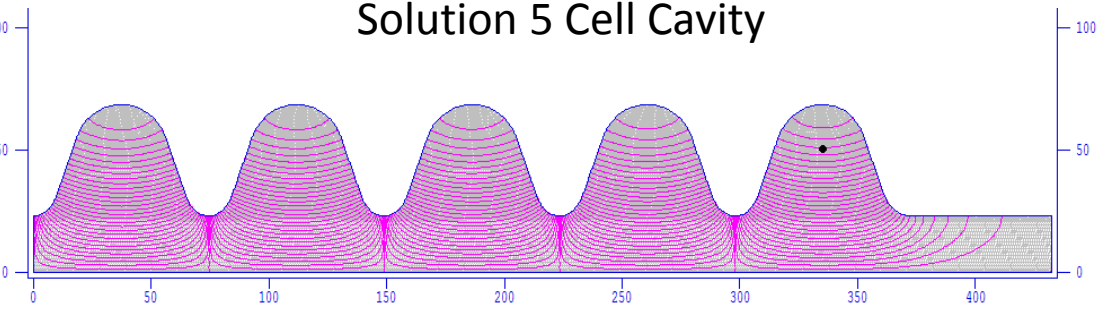
```

Litor [c:\Current Projects\Superfish Course\Oxford\Example 3\ELLIPTICAL1...
File Edit Options Help
Tuning elliptical cavity NF muon linac
Design beta = 1
Resonant frequency = 201.49 MHz, Bore radius = 23.00 cm
No tuning on this cavity.
; Superfish problem
; Material air or empty space
; Mode frequency, starting frequency in
; FREQ=201.249
; Design frequency, used (with DPW1) to
; BETA=1
; Particle velocity, used to compute w
; RHEI=0.0
; SF0 will use BETA to compute wave num
; DPW1=100
; NBSUP=1,NBSLO=0,NBSRT=0,NBSLF=0
; Boundary conditions
; Fix internal points on line regions
; LINES=1
; SCYZ,V=0, cylindrical coordinates
; Normalize to EZEROT
; MORRH=1
; Accelerating field times 1
; EZEROT=-1.E+07
; SUPERCONDUCTING elliptical cavity
; REST mass value or indicator
; RMSS=105.658369
; Mesh optimization convergence paramet
; EPSD=1.E-6
; RS method: Superconductor formula
; IRVFK=1
; SUPERCONDUCTOR temperature, degrees K
; TD=0.2
; RESIDR=1.E-08
; XDR1=8.531253899282
; Drive point X coordinate
; YDR1=54.5916824044
; Drive point Y coordinate
; ALLOW convergence in 1 iteration
; DSLOPE=-1
; Mesh spacing in X direction
; DX=1
; V line-region physical locations:
; VREQ=1.414213562373,4.242640687119,18.05825253169,20.87867965644,
; V line-region logical locations:
; LREQ=1,3,5,10,12,
; Row number for V = VMOX
; Start of boundary points
; EPD X=0.0,V=0.0 & ; 1
; EPD X=-37.24148418129,V=0.0 & ; 2
; EPD X=-37.24148418129,V=23 & ; 3
; EPD NI=2,X0=-37.24148418129,V0=30.66951733241, ; 4
; R=10.96866213269,ROURB=0.7,
; X=9.724175078025,V=-7.228789358454 & ; 5
; EPD X=-18.79385241572,V=55.38749436551 & ; 6
; EPD NI=2,X0=0.0,V0=48.547891499,
; R=20,ROURB=1,
; X=0.0,V=20 & ; 7
; EPD NI=2,X0=0.0,V0=58.38866789618,
; R=18.16662400282,ROURB=1,
; X=17.87189252888,V=6.212351945188 & ; 8
; EPD X=55.63276925568,V=53.86792864119 & ; 9
; EPD NI=2,X0=-37.24148418129,V0=-41.61088937394,
; R=13.88386256176,ROURB=0.7,
; X=8.8,V=-18.49088937394 & ; 10
; EPD X=97.24148418129,V=23 & ; 11
; EPD X=97.24148418129,V=0.0 & ; 11
; EPD X=0.0,V=0.0 & ; 12
    
```

Solution 1 Cell

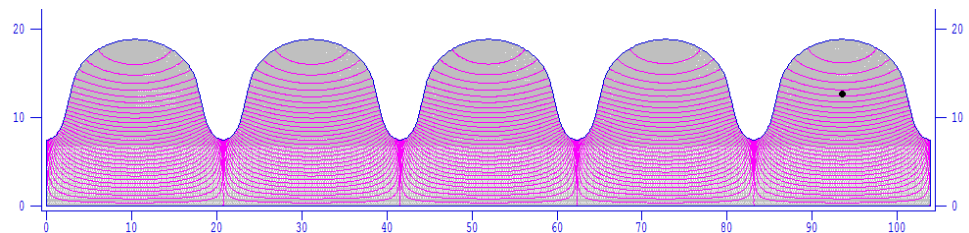
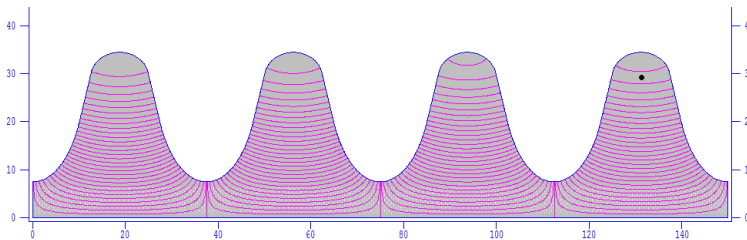
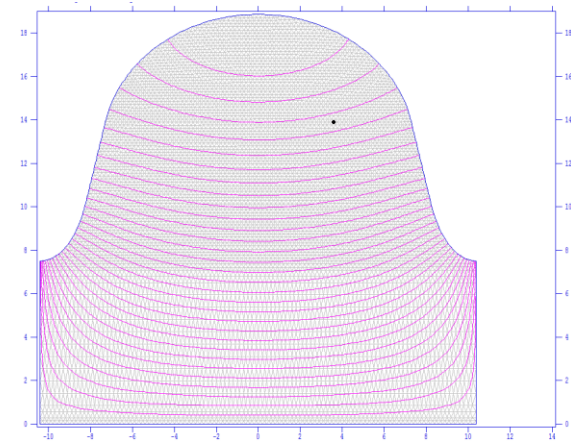
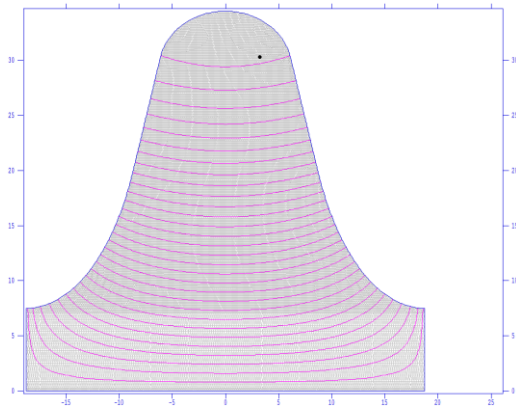


Solution 5 Cell Cavity



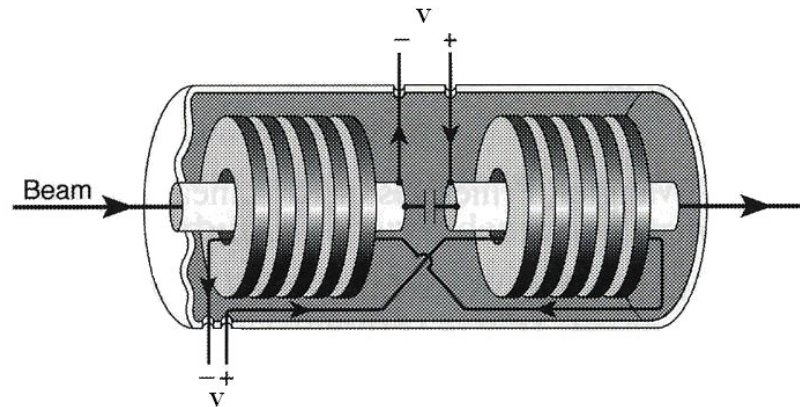
# An Elliptical Cavity

- Example 1: 400 MHz
  - Like the LHC 400 MHz RF
  - 4-cell cavity, 4 cavities/Cryomodule
- Example 2: 721.4 MHz
  - SPL-like cavities
  - 5-cell cavity



# Ferrite Loaded Cavities

- Used when variable resonance is needed
- The torus of the ferrite encircles the beam path
- Ferrite properties are important (limit the cavity capabilities)
- Bias current  $\rightarrow$  Variable magnetic field  $\rightarrow$  Variable magnetic permeability of the ferrite  $\rightarrow$  Frequency change
- The structure can be thought of as a resonant transformer in which the beam constitutes a one-turn secondary winding.
- Frequencies domain: 100 kHz and 60 MHz
- Typical gap voltage of up tens of kV
- Different requirements (large frequency ranges, rapid swings, space, etc)  $\rightarrow$  various designs.



# Ferrite Loaded Cavities

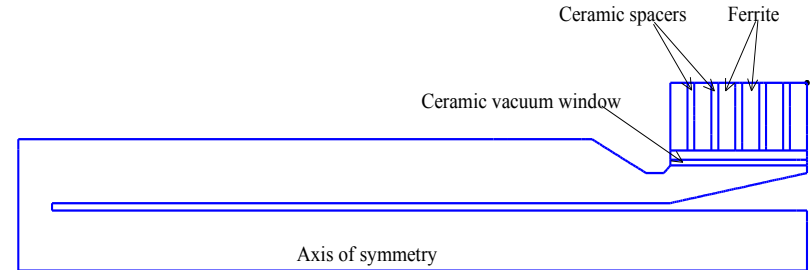
**Six ferrite blocks:** Epsilon = 14.5, Mu = 1.5

**Five ceramic-spacers:** Epsilon = 10.0, Mu = 1.0

**Ceramic vacuum window:** Epsilon = 9.0, Mu = 1.0

Cavity length: 116 cm

Number of gaps: 1



```

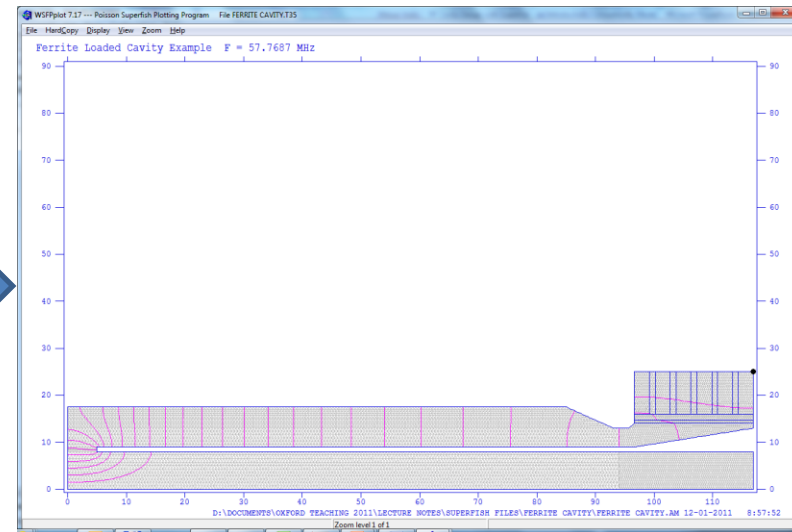
Lister - [D:\Documents\Oxford Teaching 2011\Lecture Notes\Superfish Files\Ferrite Cavity\Ferrite Cavity.am]
File Edit Options Encoding Help
Ferrite Loaded Cavity Example
Six ferrite blocks: Material 2, Epsilon = 14.5, Mu = 1.5
Five ceramic-spacers: Material 4, Epsilon = 10.0, Mu = 1.0
Ceramic vacuum window: Material 3, Epsilon = 9.0, Mu = 1.0
Initialize one large ferrite block, then superimpose ceramic spacers
[Originally appeared in 1987 Reference Manual C.12.2]

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kreg kprob=1,          ! Superfish problem
icilin=1              ! Cylindrical symmetry
Freq=57.76775,       ! Starting frequency
dslope=-1,           ! Allow convergence after one iteration
xreg1=94.0,          ! X line region
kreg1=188,           ! Logical coordinate for XREG1
yreg1=8,yreg2=9,     ! Y line regions
yreg3=13,yreg4=17.5
lreg1=12,lreg2=15,   ! Logical coordinates for YREGS
lreg3=21,lreg4=31,
kmax=260,lmax=43 &

! Maximum X and Y logical coordinates

!po x=0.0,y=0.0 &
!po x=116.88,y=0.0 &
!po x=116.88,y=0.0 &
!po x=5.0,y=0.0 &
!po x=5.0,y=9.0 &
!po x=96.64,y=9.0 &
!po x=116.88,y=13.0 &
!po x=116.88,y=25.0 &
!po x=96.64,y=25.0 &
!po x=96.64,y=14.0 &
!po x=95.64,y=13.0 &
!po x=93.0,y=13.0 &
!po x=85.0,y=17.5 &
!po x=0.0,y=17.5 &
!rn  v=0.0 u=0.0 &
  
```





Now, use your imagination!