

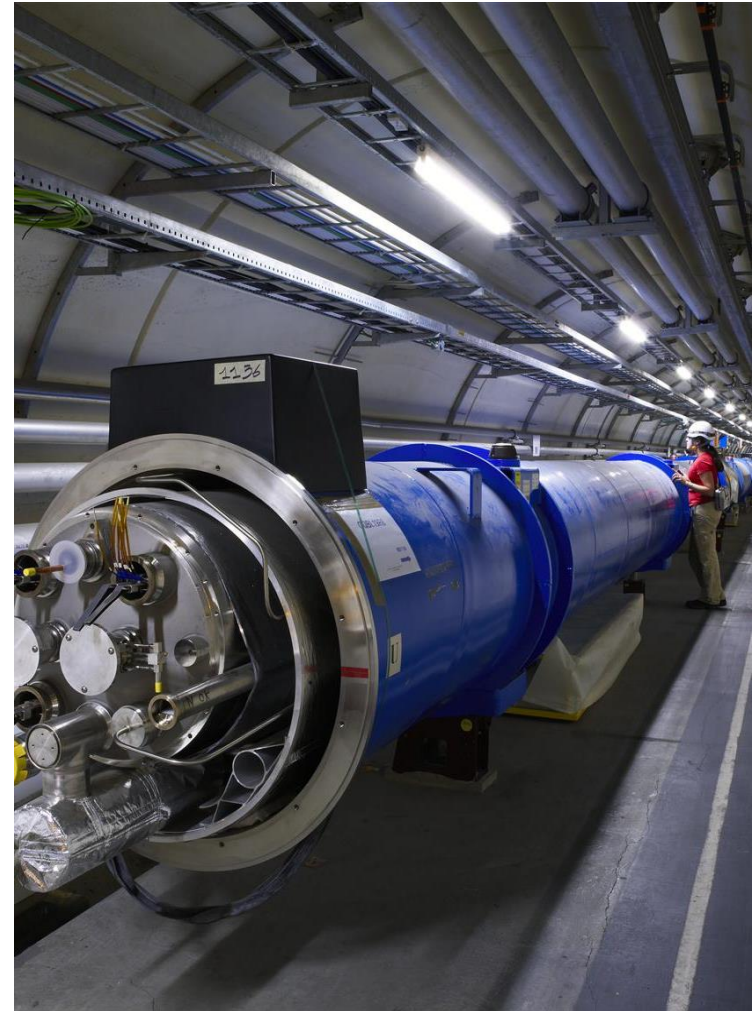
# Superconductivity for accelerators - why bother?

## Abolish Ohm's Law

- no power consumption  
(although do need refrigeration power)
- high current density  $\Rightarrow$  compact windings, high gradients
- ampere turns are cheap, so don't need iron  $\Rightarrow$  high fields  
(although often use it for shielding)

## Consequences

- lower power bills
- higher magnetic fields mean reduced bend radius
  - $\Rightarrow$  smaller rings
  - $\Rightarrow$  reduced capital cost
  - $\Rightarrow$  new technical possibilities (eg muon collider)
- higher quadrupole gradients
  - $\Rightarrow$  higher luminosity (eg CERN HiLumi)



# *Superconducting Magnets: plan*

## **1 Introduction to Superconductors**

- critical field, temperature & current
- superconductors for magnets
- manufacture of superconducting wires
- high temperature superconductors HTS
- where to find more

## **2 Magnetization, Cables & AC losses**

- superconductors in changing fields, critical state model
- filamentary superconductors & magnetization
- coupling between filaments  
⇒ magnetization
- flux jumping
- why cables, coupling in cables
- mini tutorial
- AC losses in changing fields

## **3 Magnetic and mechanical design**

*Paolo Ferracin*

## **4 Magnet fabrication and assembly**

*Paolo Ferracin*

## **5 Cryogenics and cryostat design**

*Philippe Lebrun*

## **6 Quench, quench protection & training**

*Paolo Ferracin*

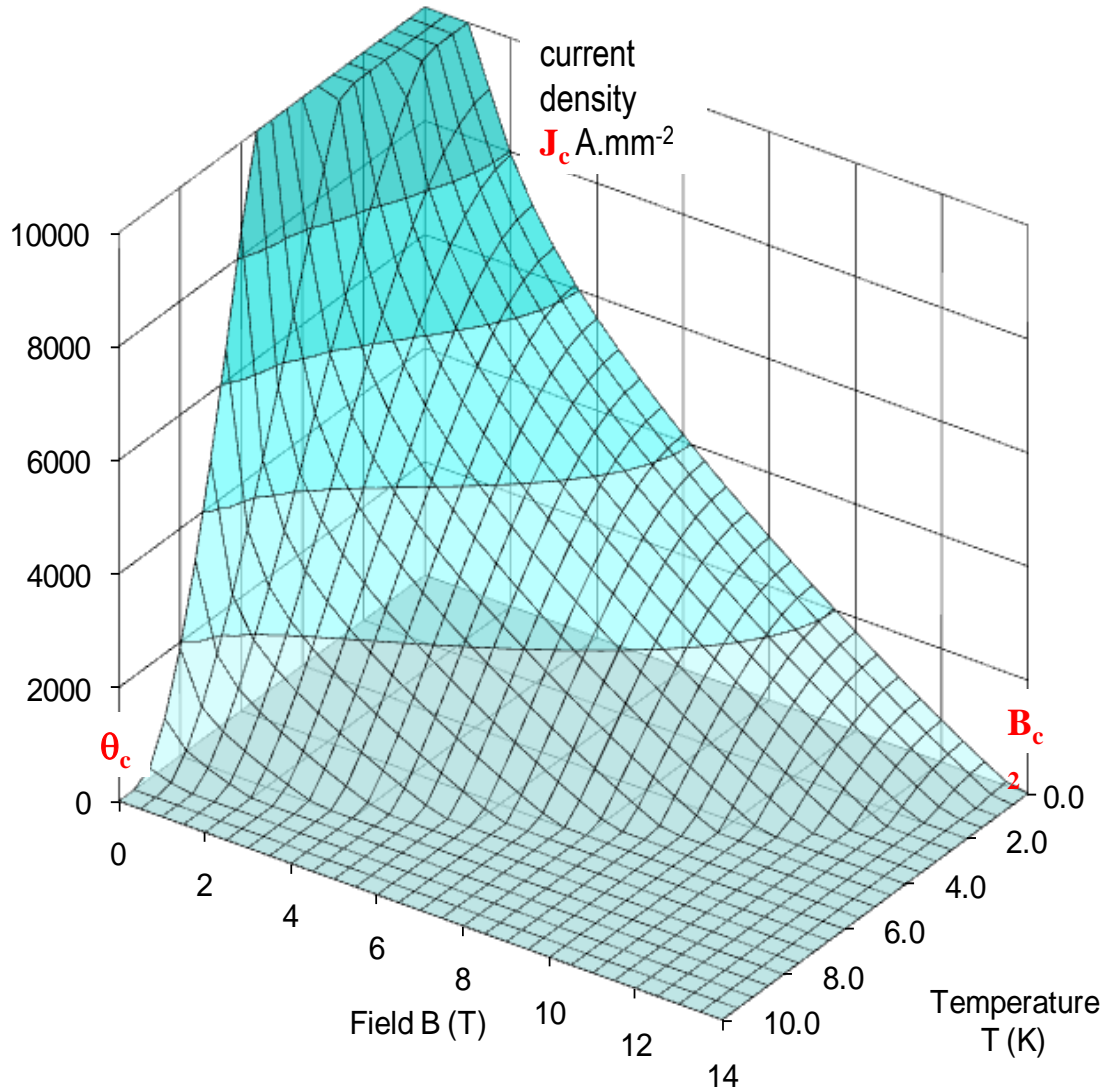
## **Mini workshop Superconducting Magnets**

*Daniel Schoerling Paolo Ferracin*

*Martin Wilson*

# The critical surface of niobium titanium

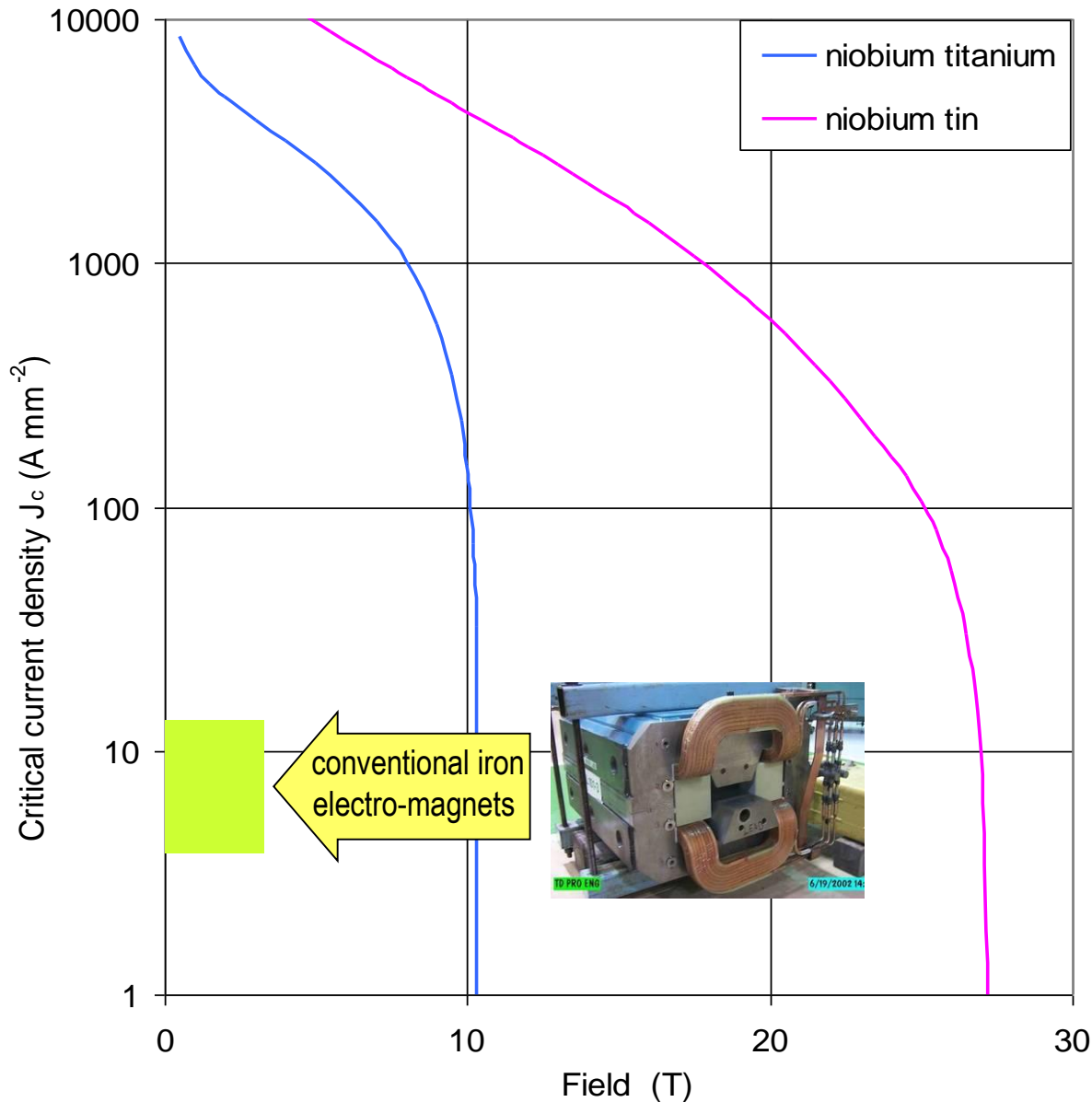
- **NbTi** is the standard commercial ‘work horse’ of the superconducting magnet business



- **critical surface** is the boundary between superconductivity and normal resistivity in  $J, B, \theta$  space
- superconductivity prevails everywhere below the surface, resistance everywhere above it
- upper critical field  $B_{c2}$  (at zero temperature and current)
- critical temperature  $\theta_c$  (at zero field and current)
- $B_{c2}$  and  $\theta_c$  are characteristic of the alloy composition
- critical current density  $J_c$  depends on processing

• keep it cold!

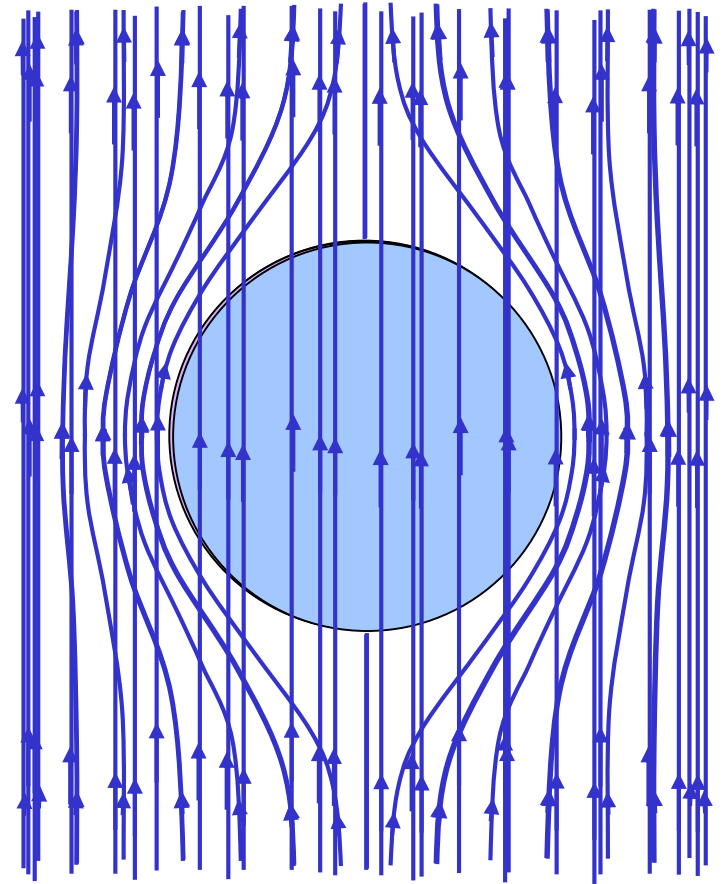
# The critical line at 4.2K



- magnets usually work in boiling liquid helium, so the critical surface is often represented by a curve of current versus field at 4.2K
- niobium tin Nb<sub>3</sub>Sn has a much higher performance than NbTi
- **but** Nb<sub>3</sub>Sn is a brittle intermetallic compound with poor mechanical properties
- both the field and current density of both superconductors are way above the capability of conventional electromagnets

# Two kinds of superconductor: type 1

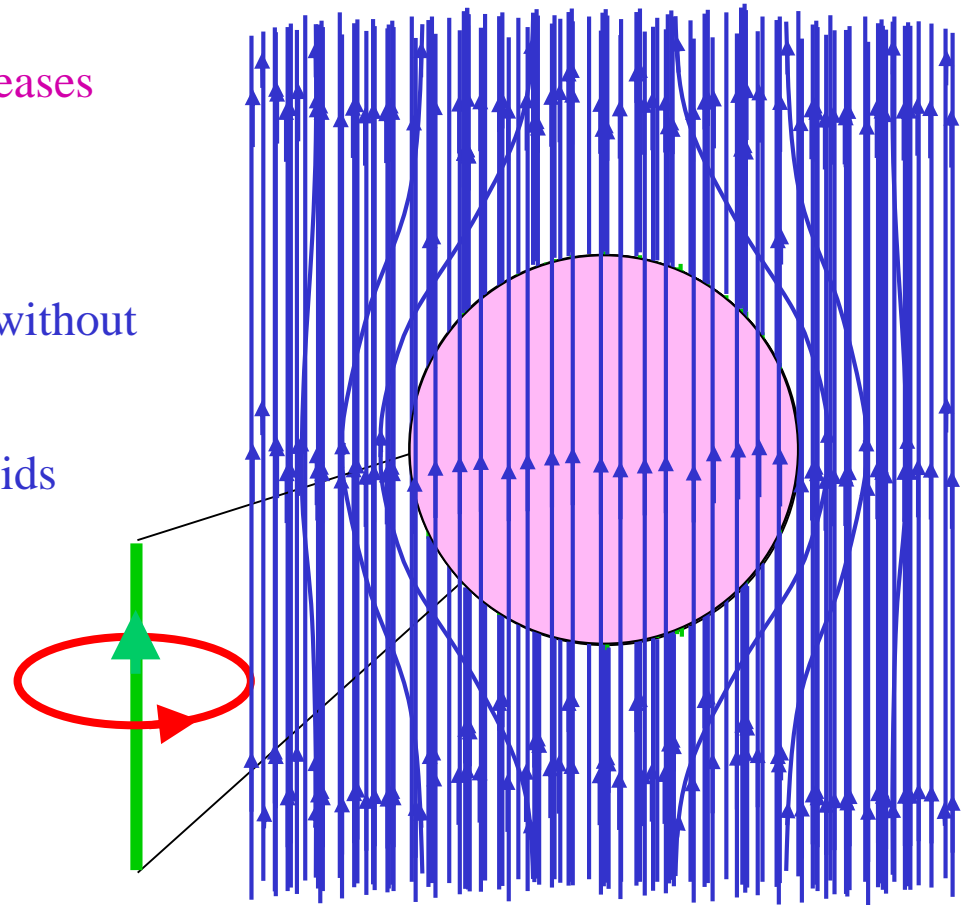
- the materials first discovered by Kammerlingh Onnes in 1911 - soft metals like lead, tin mercury
- sphere of metal at room temperature
- **apply magnetic field**
- **reduce the temperature - resistance decreases**
- **reduce the temperature some more - resistance decreases some more**
- at the critical temperature  $\theta_c$  the field is pushed out - the **Meissner effect** - superconductivity!
- increase the field - field is kept out
- increase the field some more - superconductivity is extinguished and the field jumps in
- thermodynamic critical field  $B_c$  is trade off between **reducing** energy via condensation to superconductivity and **increasing** energy by pushing out field  $\sim 0.1T$



  
*useless for magnets!*

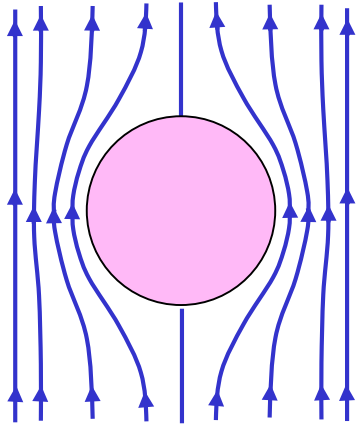
# Two kinds of superconductor: type 2

- apply magnetic field
- reduce the temperature - resistance decreases
- at the critical temperature  $\theta_c$  the field is pushed out
- increase the field - field jumps back in without quenching superconductivity
- it does so in the form of quantized fluxoids
- lower critical field  $B_{c1}$
- supercurrents encircle the resistive core of the fluxoid thereby screening field from the bulk material
- higher field  $\Rightarrow$  closer vortex spacing
- superconductivity is extinguished at the (much higher) upper critical field  $B_{c2}$

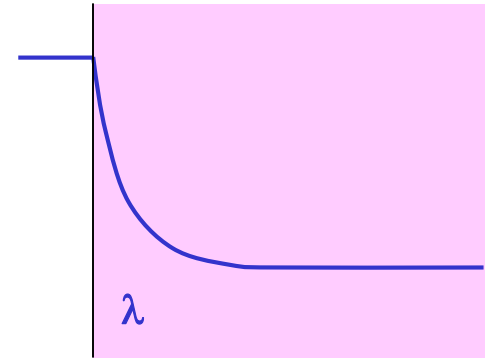




# Type 1 and type 2 superconductors

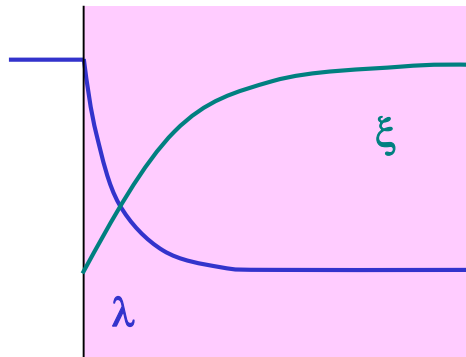


- Meissner effect is not total
- magnetic field penetrates a small distance  $\lambda$
- the **London Penetration Depth**.

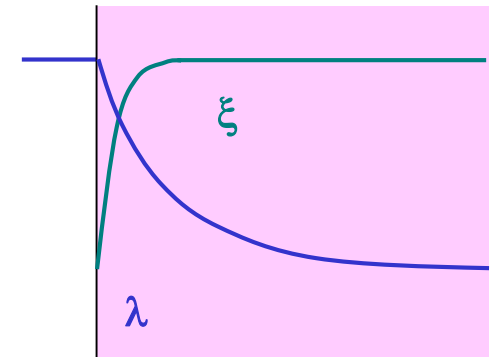


- another characteristic distance is the **coherence length**  $\zeta$  - the minimum distance over which the electronic state can change from superconducting to normal
- theory of Ginsburg, Landau, Abrikosov and Gorkov **GLAG** defines the ratio  $\kappa = \lambda / \zeta$

if  $\kappa < 1/\sqrt{2}$   
material is  
**Type 1**



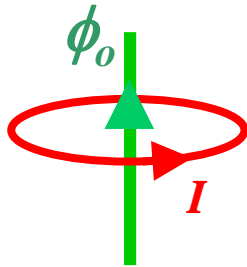
if  $k > 1/\sqrt{2}$   
material is  
**Type 2**



# Critical fields of type 2 superconductors

- recap thermodynamic critical field  $B_c$
- lower critical field  $B_{c1} = B_c / \kappa$
- above  $B_{c1}$  magnetic field penetrates as discrete quantized **fluxoids**

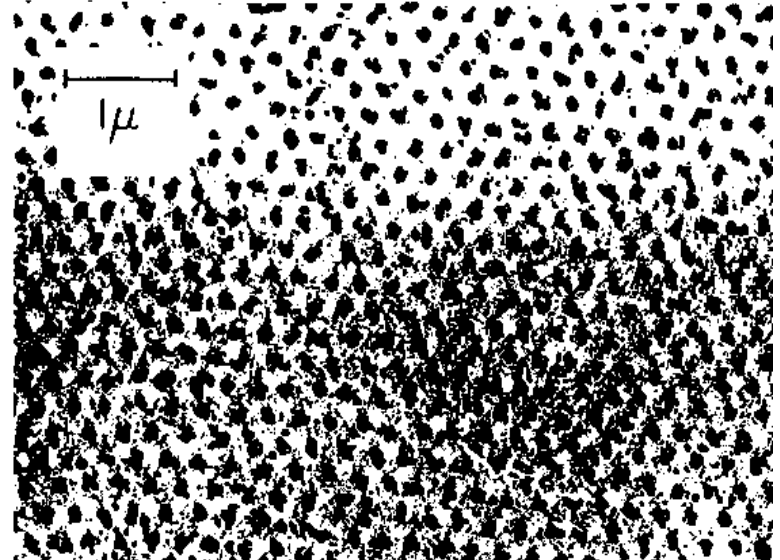
human hair  
in earth's  
magnetic  
field  $\sim 50\phi_0$



a fluxoid encloses flux

$$\phi_0 = \frac{h}{2e} = 2 \times 10^{-15} \text{ Wb}$$

$h$  = Planck's constant  
 $e$  = electronic charge



**upper  
critical field**

$$B_{c2} = \sqrt{2} \kappa B_c$$

in the  
'dirty limit'  $\kappa \approx 2.4 \times 10^6 \gamma^{\frac{1}{2}} \rho_n$

where  $\rho_n$  is the  
normal state resistivity  
**- best superconductors  
are best resistors!**

thus the upper critical field

$$B_{c2} = 3.1 \times 10^3 \gamma \rho_n \theta_c$$

for NbTi:  $\gamma \sim 900 \text{ J m}^{-3} \text{ K}^{-2}$      $\rho_n \sim 65 \times 10^{-8} \text{ W m}$      $\theta_c = 9.3 \text{ K}$     hence  **$B_{c2} \sim 18.5 \text{ T}$**

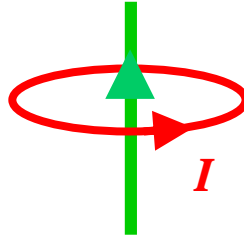
*Sommerfeld coefficient of electronic specific heat*  $C_e = \gamma \theta$



# Critical current density: type 2 superconductors

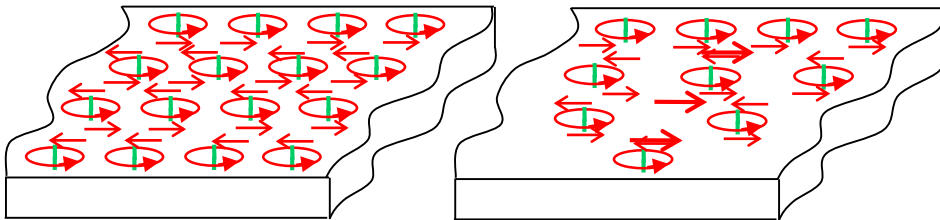
- a single fluxoid encloses flux

$$\phi_o = \frac{h}{2e} = 2 \times 10^{-15} \text{ Webers}$$

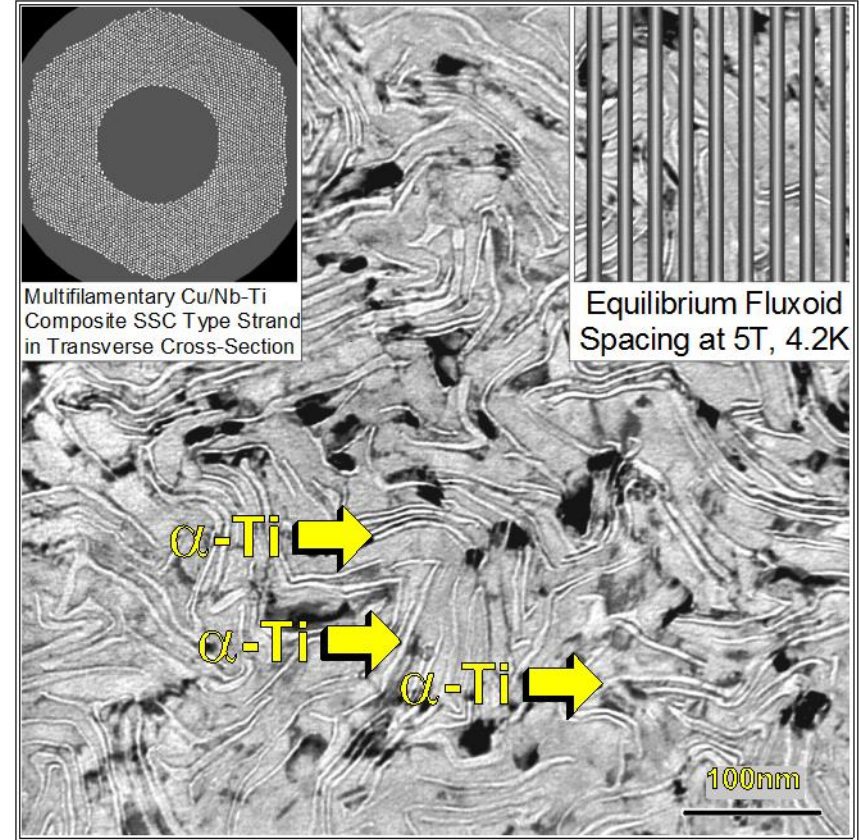


$h$  = Planck's constant,  $e$  = electronic charge

- so density of fluxoids  $\sim$  average field  
uniform density  $\Rightarrow$  uniform field  
 $\Rightarrow$  zero  $J$  (because  $\text{Curl } B = \mu_o J$ )
- to get a current density we must produce a **gradient** in the density of fluxoids



- fluxoids like to distribute uniformly
- must impose a gradient by inhomogeneities in the material, eg dislocations or precipitates

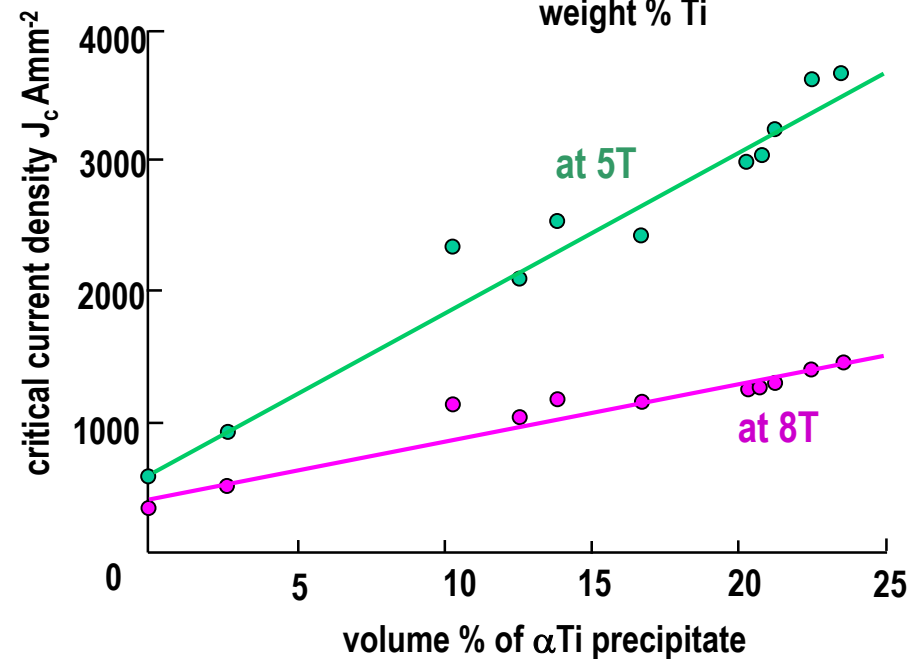
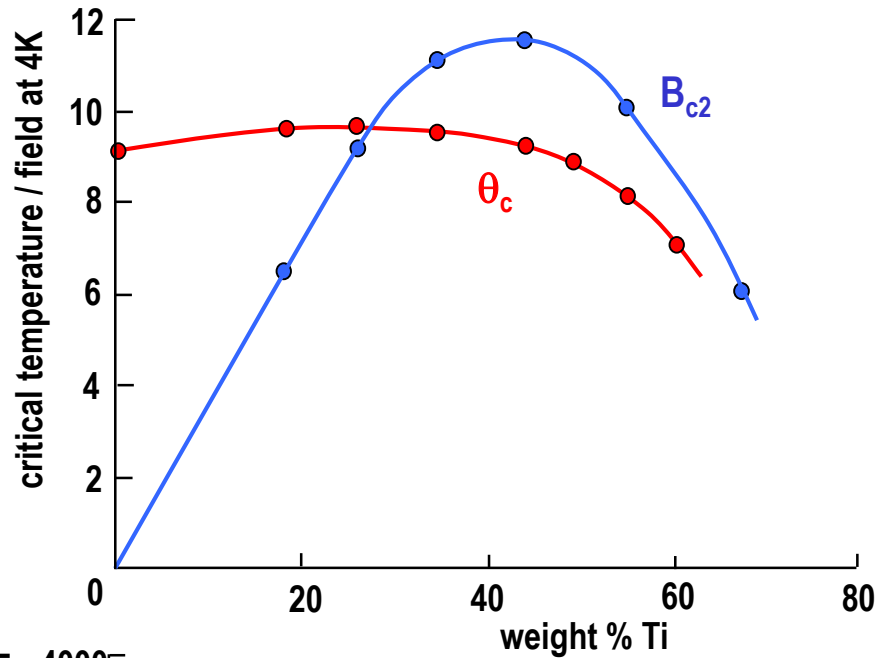


**precipitates of  $\alpha$  Ti in Nb Ti**

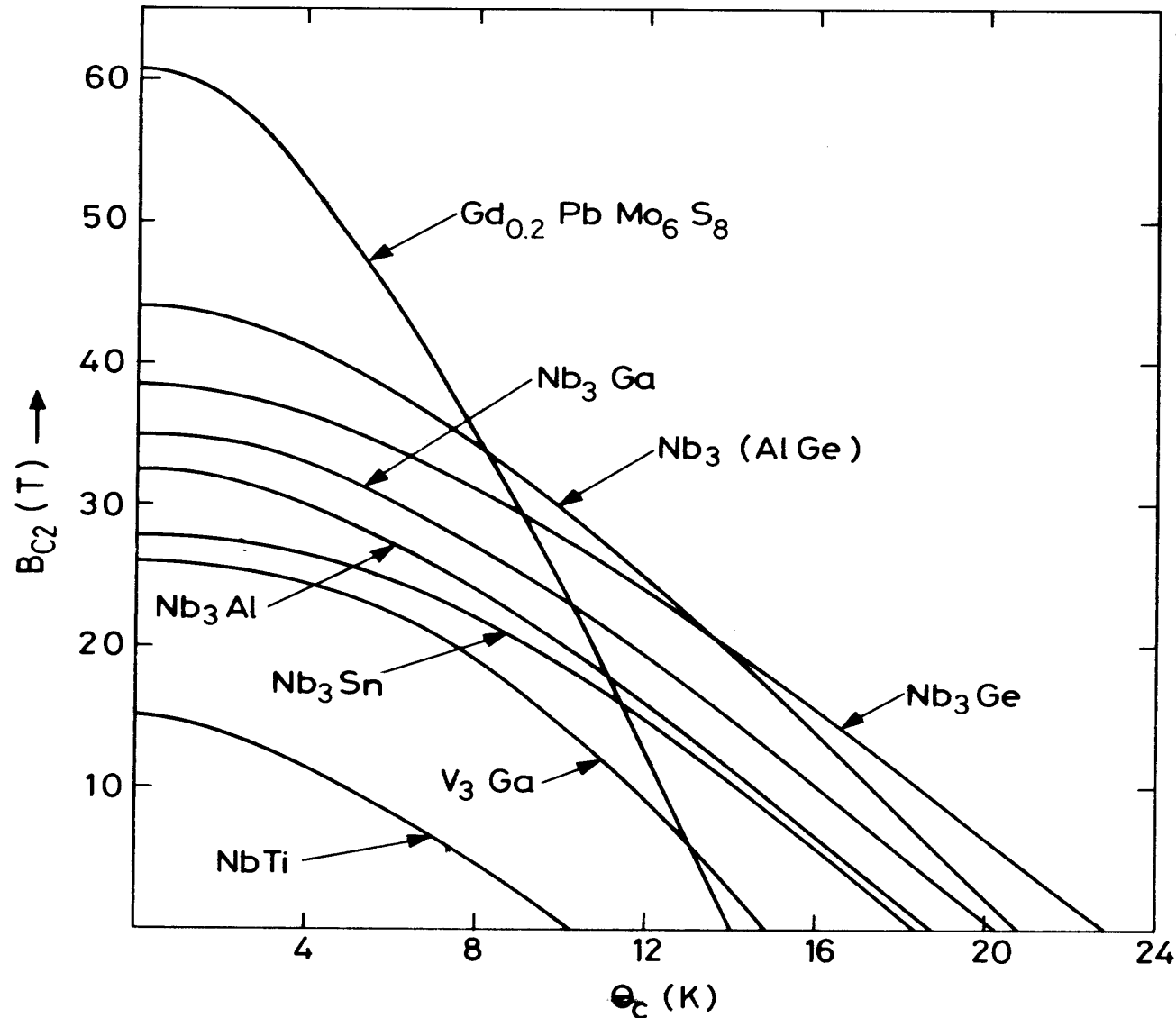
Meingast, P Lee and DC Larbalestier: *J. Appl. Phys.* 66, 5971

# Critical properties

- **Critical temperature  $\theta_c$** : choose the right material to have a large energy gap or 'depairing energy'  
*property of the material*
- **Upper Critical field  $B_{c2}$** : choose a Type 2 superconductor with a high critical temperature and a high normal state resistivity  
*property of the material*
- **Critical current density  $J_c$** : mess up the microstructure by cold working and precipitation heat treatments  
*hard work by the producer*



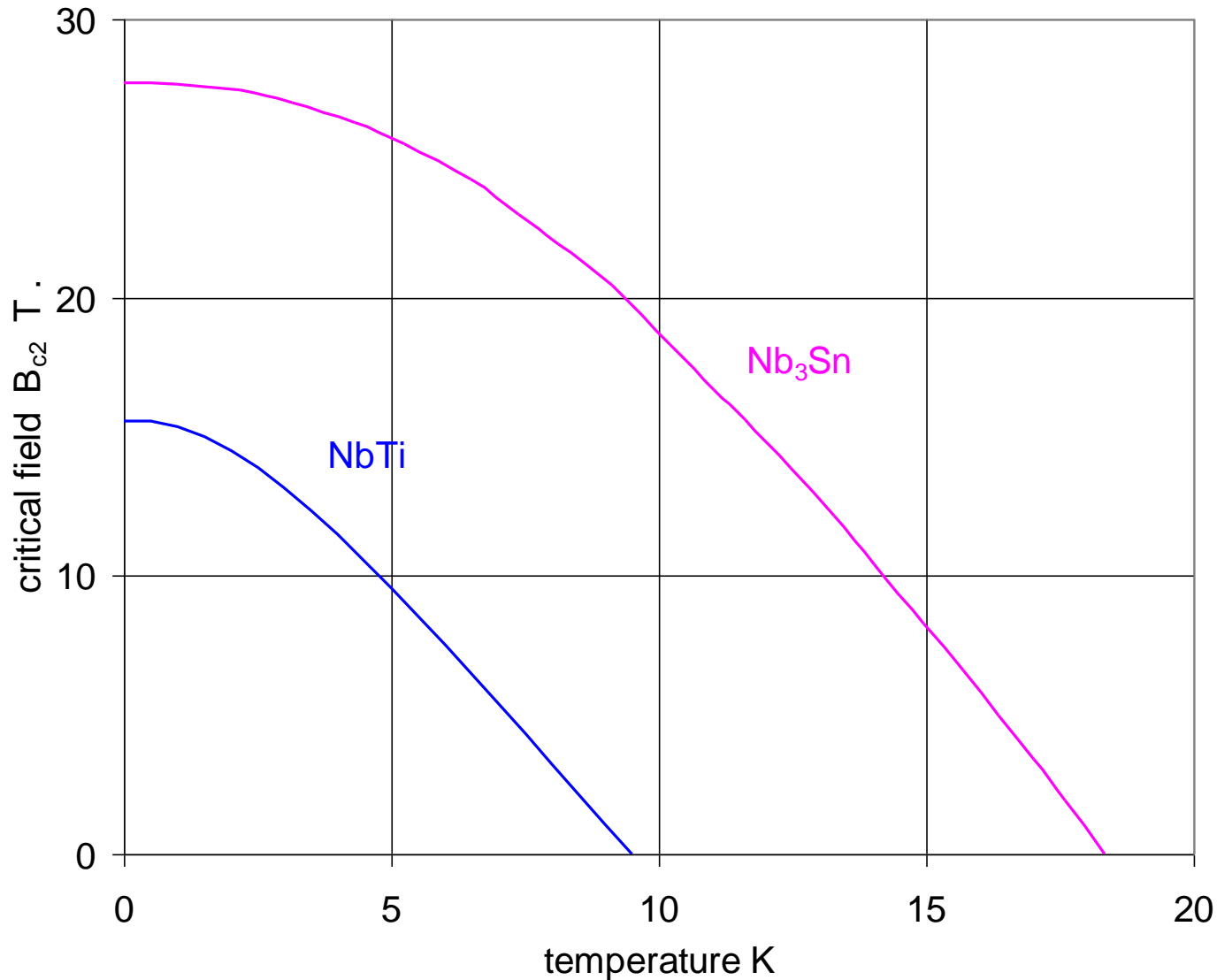
# Critical field & temperature of metallic superconductors



Note: of all the metallic superconductors, only NbTi is ductile.

All the rest are brittle intermetallic compounds

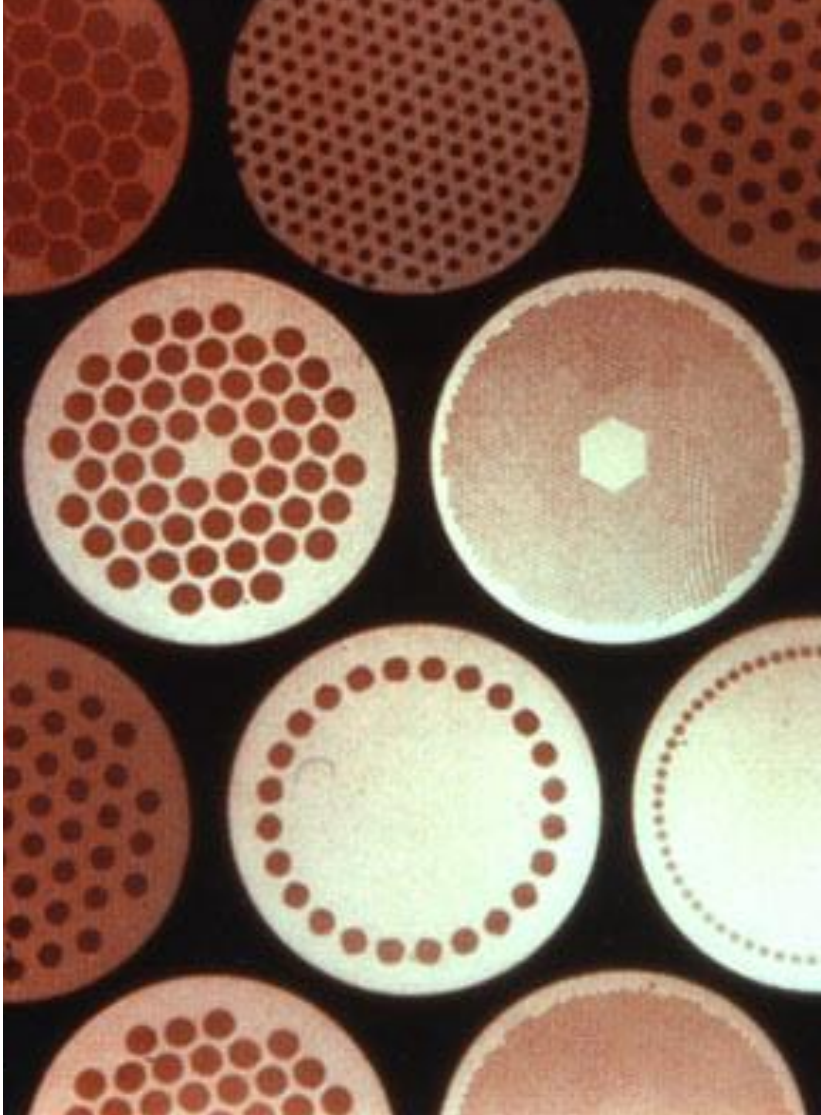
# Critical field & temperature of metallic superconductors



To date, all superconducting accelerators have used NbTi.

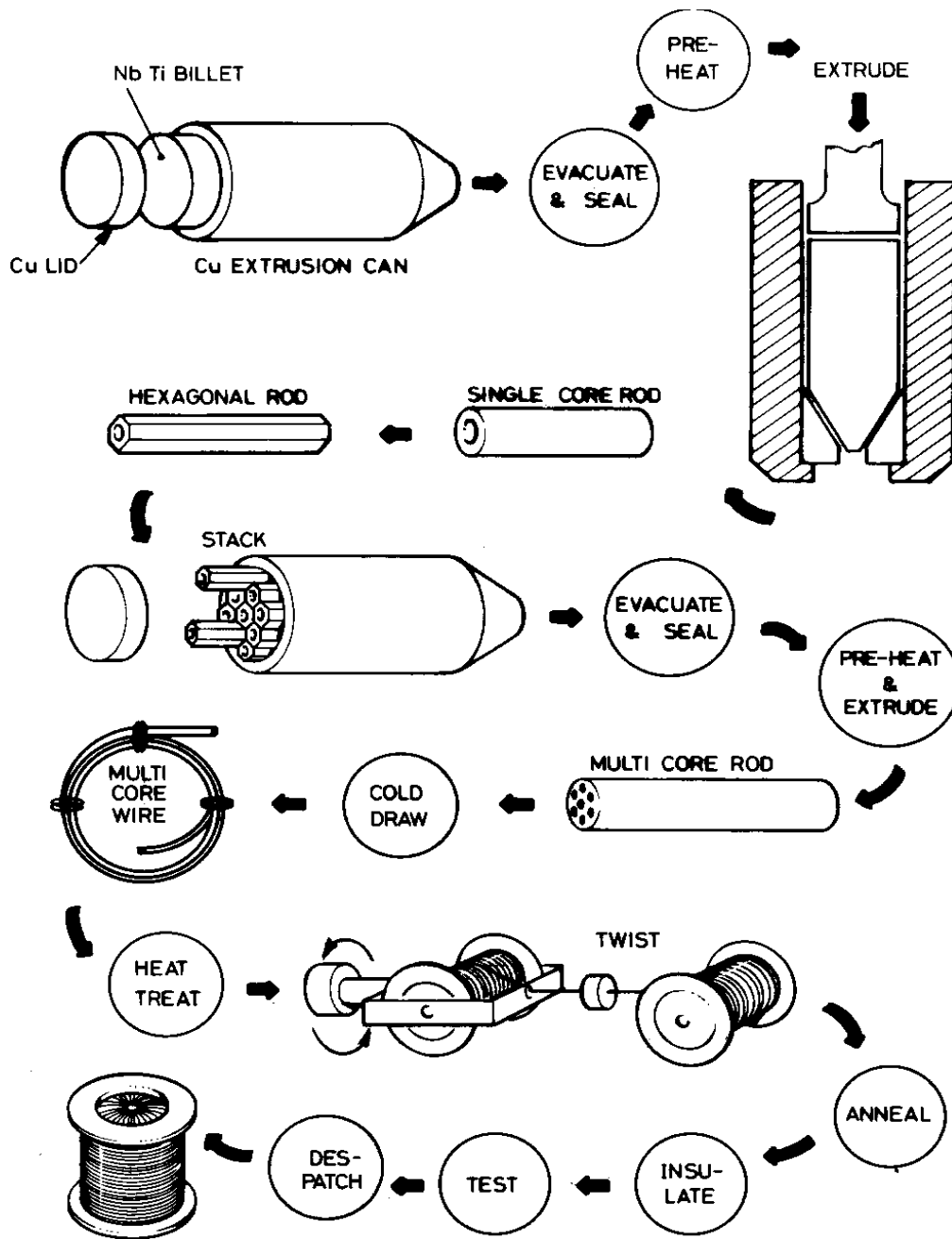
Of the intermetallics, only Nb<sub>3</sub>Sn has found significant use in magnets

# Practical wires for magnets



- some 40 years after its development, NbTi is still the most popular magnet conductor, with Nb<sub>3</sub>Sn being used for special high field magnets and HTS for some developmental prototypes.
- for reasons that will be described later, superconducting materials are always used in combination with a good normal conductor such as copper
- to ensure intimate mixing between the two, the superconductor is made in the form of fine filaments embedded in a matrix of copper
- typical dimensions are:
  - wire diameter = 0.3 - 1.0mm
  - filament diameter = 5 - 50μm
- for electromagnetic reasons, the composite wires are twisted so that the filaments look like a rope (see Lecture 2)

# NbTi manufacture



- vacuum melting of NbTi billets
- hot extrusion of the copper NbTi composite
- sequence of cold drawing and intermediate heat treatments to precipitate  $\alpha$ Ti phases as flux pinning centres
- for very fine filaments, must avoid the formation of brittle CuTi intermetallic compounds during heat treatment
  - usually done by enclosing the NbTi in a thin Nb shell
- twisting to avoid coupling - see lecture 2

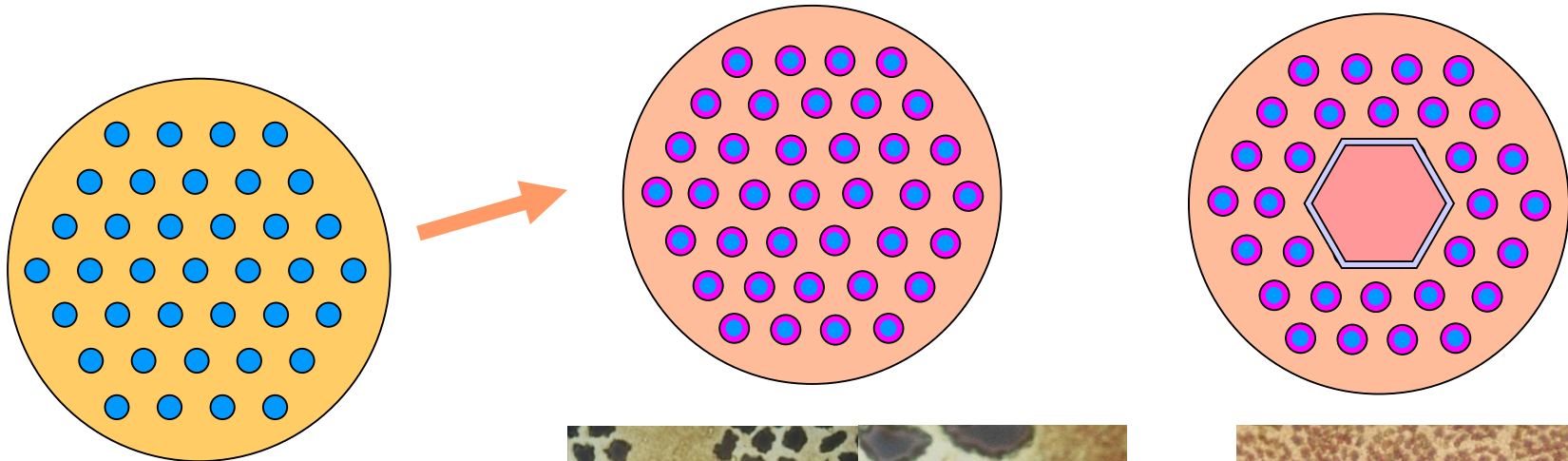


# Filamentary $Nb_3Sn$ wire via the bronze route

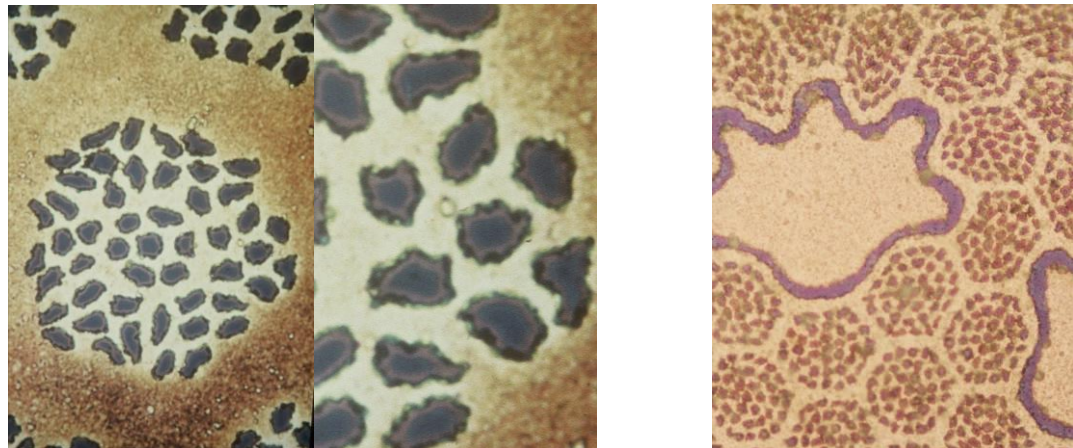
$Nb_3Sn$  is a brittle material and cannot be drawn down. Instead must draw down pure niobium in a matrix of bronze (copper tin)

At final size the wire is heated ( $\sim 700^\circ\text{C}$  for some days) tin diffuses through the Cu and reacts with the Nb to form  $Nb_3Sn$

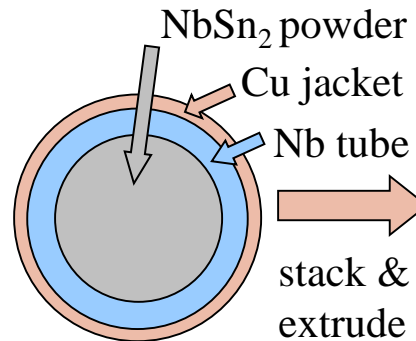
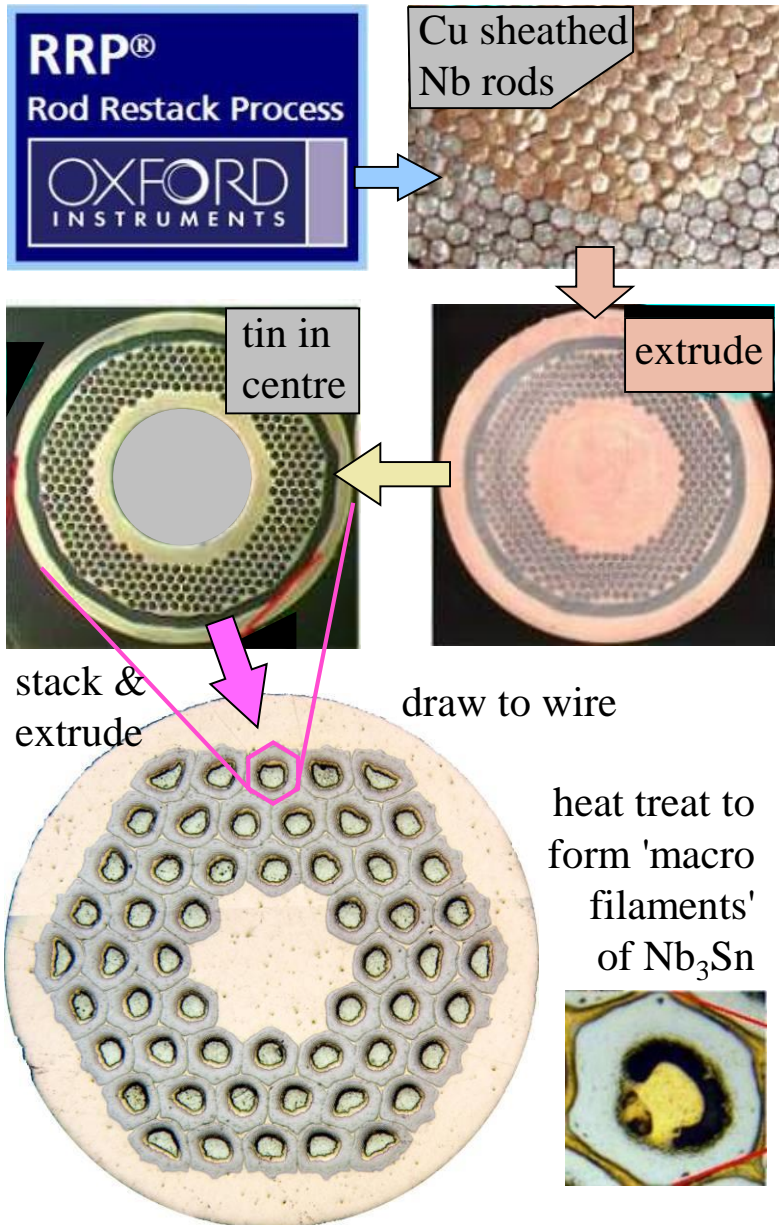
The remaining copper still contains  $\sim 3\text{wt}\%$  tin and has a high resistivity  $\sim 6 \times 10^{-8} \Omega\text{m}$ . So include 'islands' of pure copper surrounded by a diffusion barrier



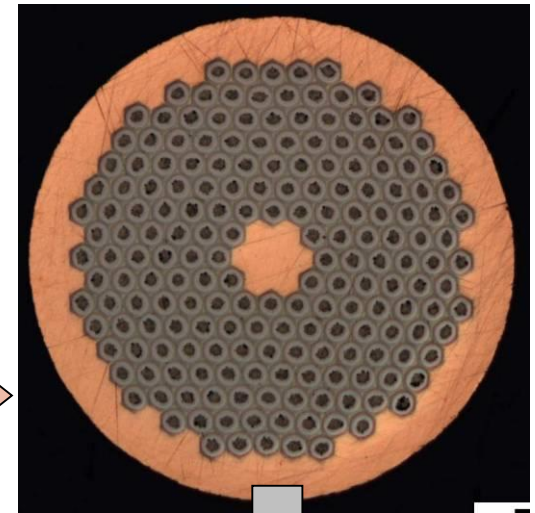
- *BUT maximum ductile bronze is  $\sim 13\text{wt}\%$  tin,*
- *reaction slows at  $\sim 3\text{wt}\%$*
- *so low engineering  $J_c$*



# $Nb_3Sn$ with higher engineering $J_c$



Powder in tube PIT

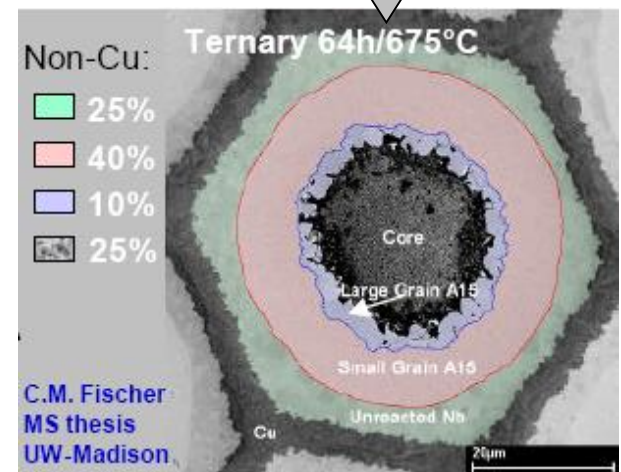


draw to wire

heat treat

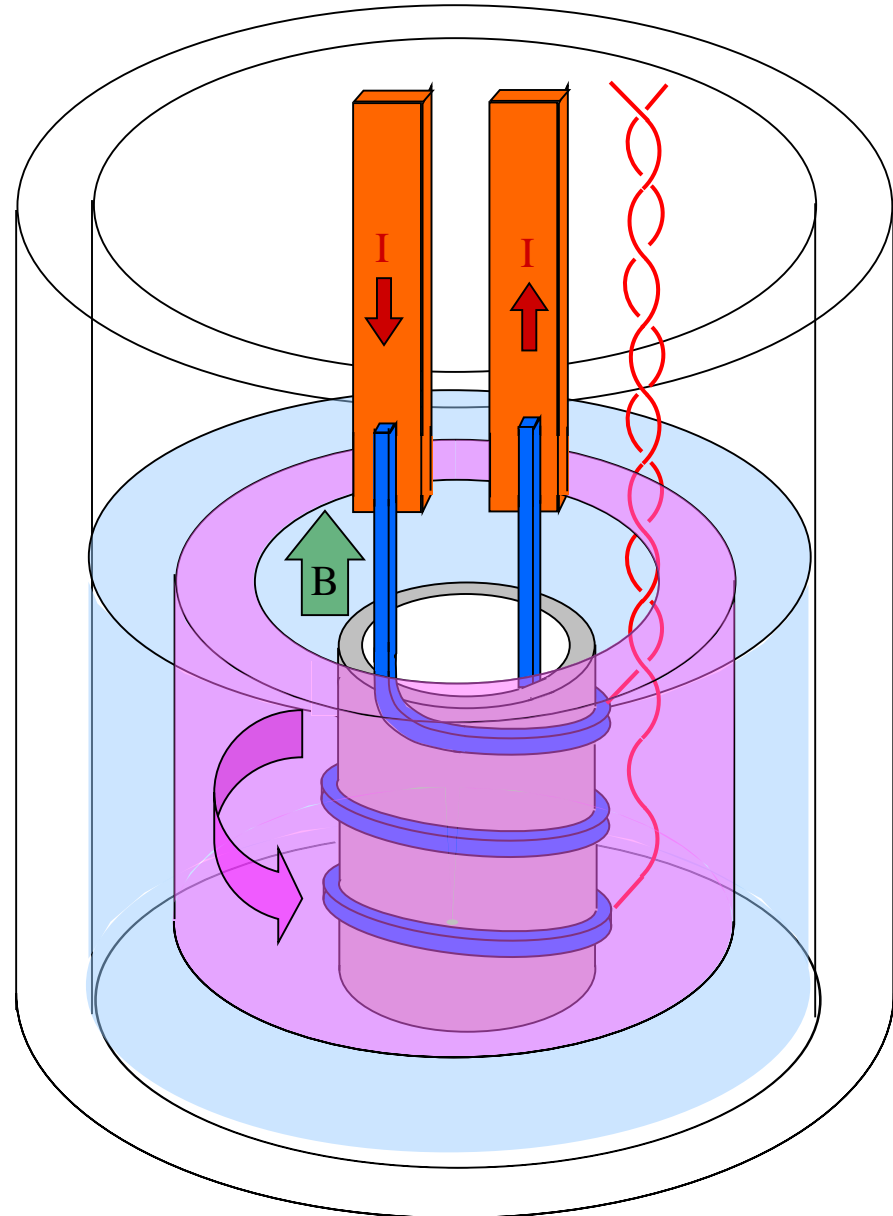
both make high  $J_{eng}$  (RRP is the highest)

but large filaments



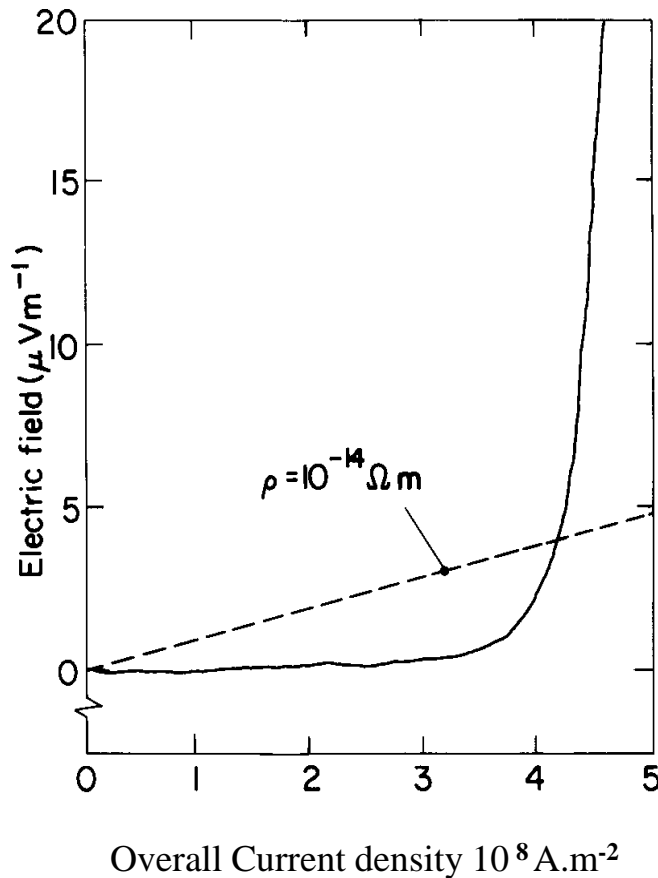
# Measurement of critical current

- spiral sample with current leads and voltage taps
- place in the bore of a superconducting solenoid
- put in cryostat
- immerse in liquid helium
- at each field level slowly increase the current and measure the voltage across the test section

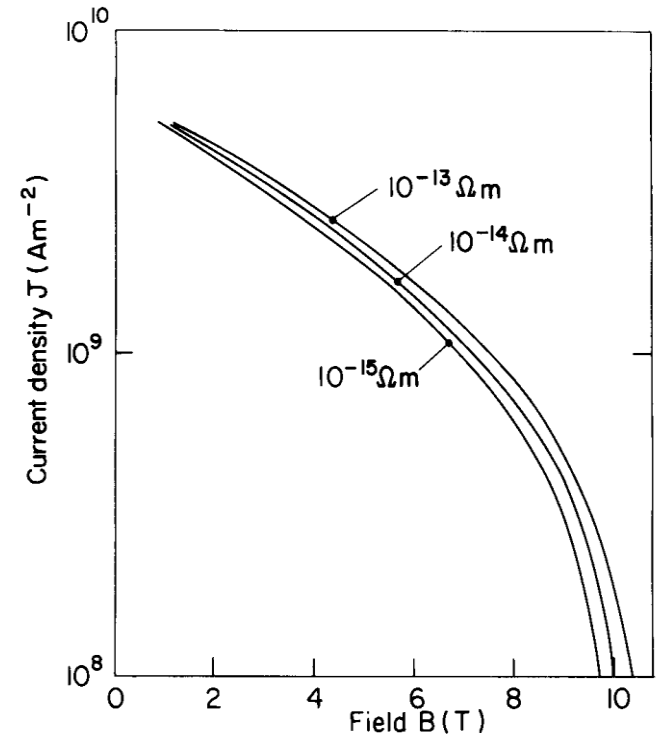


# Resistive transition 1

- in practical magnet conductors, the boundary between superconducting and resistive states is not sharp, but slightly blurred.



- measure  $J_c$  with voltage taps across sample  
 $\Rightarrow$  gradual voltage rise
- must define  $J_c$  at a given measurement sensitivity
  - electric field
  - effective resistivity.



- usual definitions are  $\rho = 10^{-14} \Omega\text{m}$  or  $E = 1 \mu\text{V.m}^{-1}$
- critical current defined at this level is about what you would expect the conductor in a resin impregnated solenoid to achieve. At higher resistivity, self heating would start to raise the internal temperature and reduce the critical current



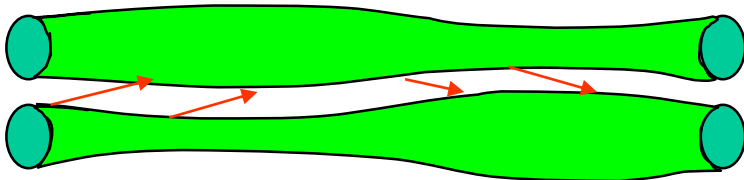
# Resistive transition 2

- find empirically that the resistive transition may be represented by a power law

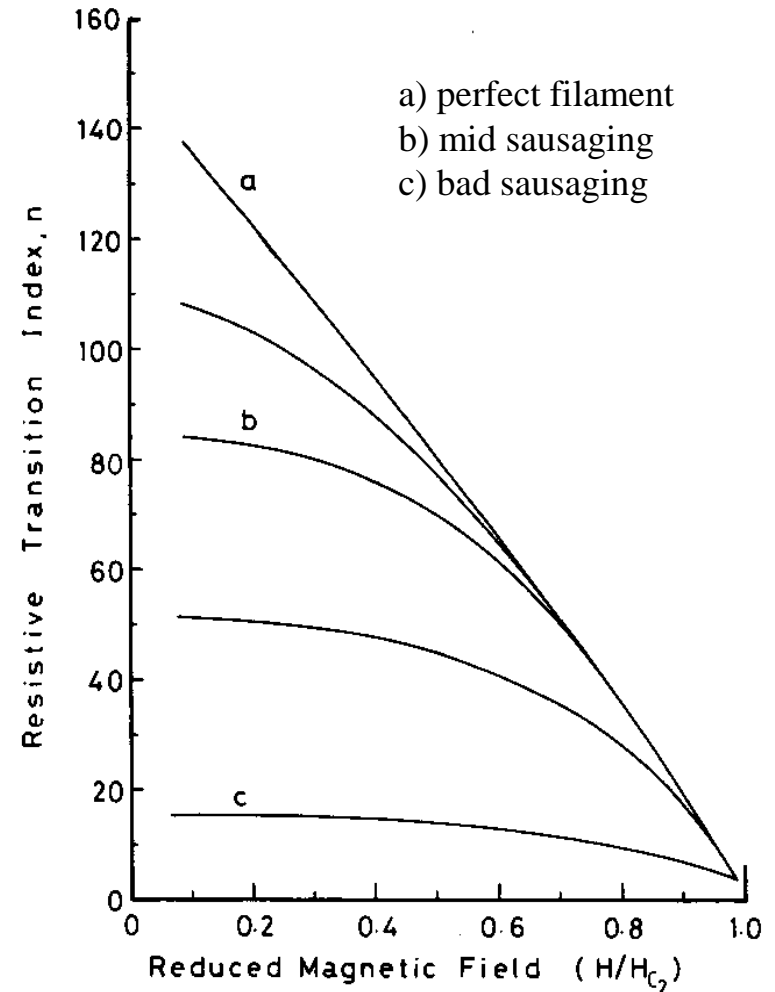
$$\rho(J) = \rho_o \left\{ \frac{J}{J_o} \right\}^n$$

where  $n$  is called the resistive transition index.

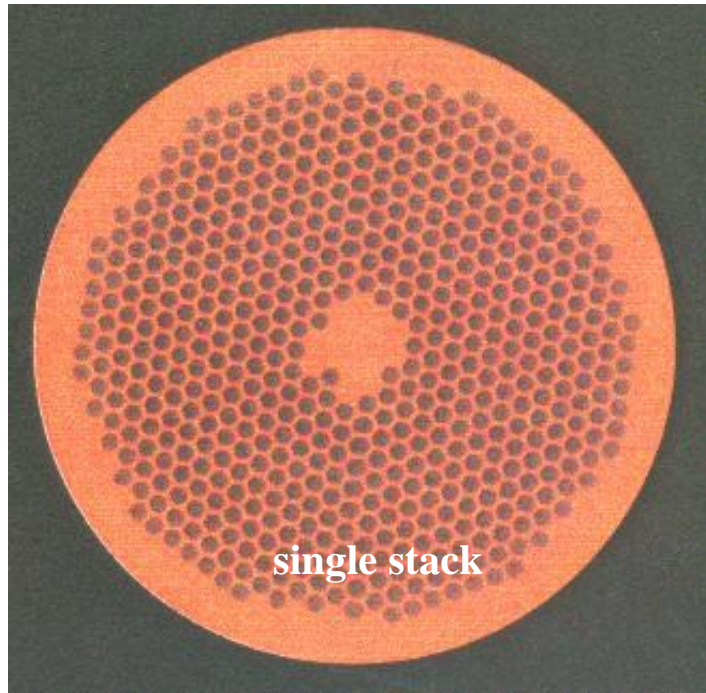
- the effect is partly within the filaments (flux flow) and partly between the filaments
- 'sausaging of the filaments, forces current to cross the copper matrix as critical current is approached.



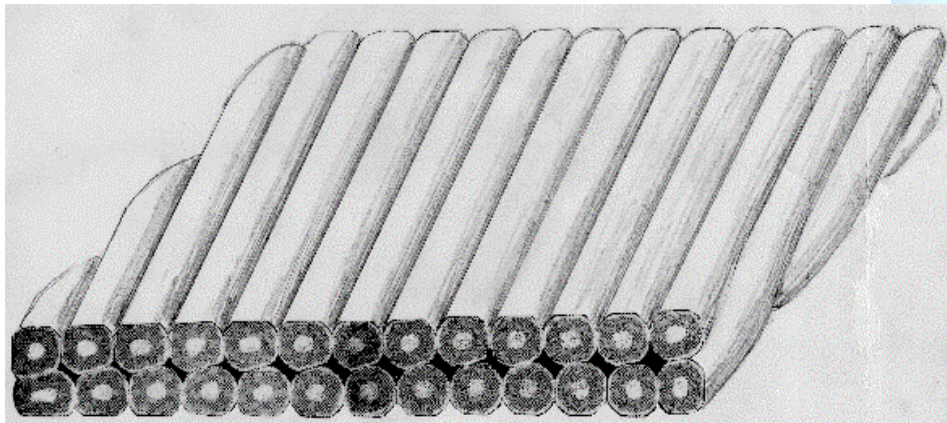
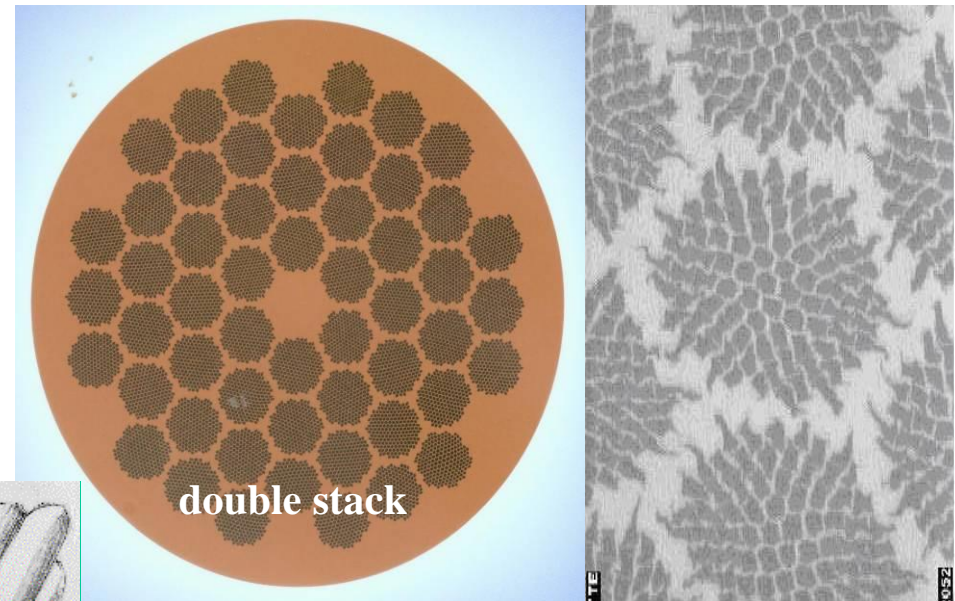
- resistive transition can be the main source of decay in persistent magnets
- 'n' is often taken as a measure of quality - look for  $n > 50$
- HTS conductors so far have low  $n \sim 5 - 10$



# Conductors for accelerator magnets



- to date, all superconducting accelerators have used NbTi superconductor.
- to control field errors and ac losses, the filaments must be  $< 10\mu\text{m}$  diameter (lectures 2 & 3)



- to get the necessary high operating currents, many wires must be cabled together.



# Engineering current density and filling factors

In magnet design, what really matters is the overall 'engineering' current density  $J_{eng}$

$$J_{eng} = \text{current} / \text{unit cell area} = J_{sup} \times \lambda_{su}$$

where  $\lambda_{su}$  = filling factor of superconductor in unit cell

filling factor superconductor in the wire  $\lambda_{sw} = 1 / (1 + mat)$

where  $mat$  = matrix : superconductor ratio

typically:

for NbTi  $mat = 1.2$  to  $3.0$  ie  $\lambda_{sw} = 0.45$  to  $0.25$

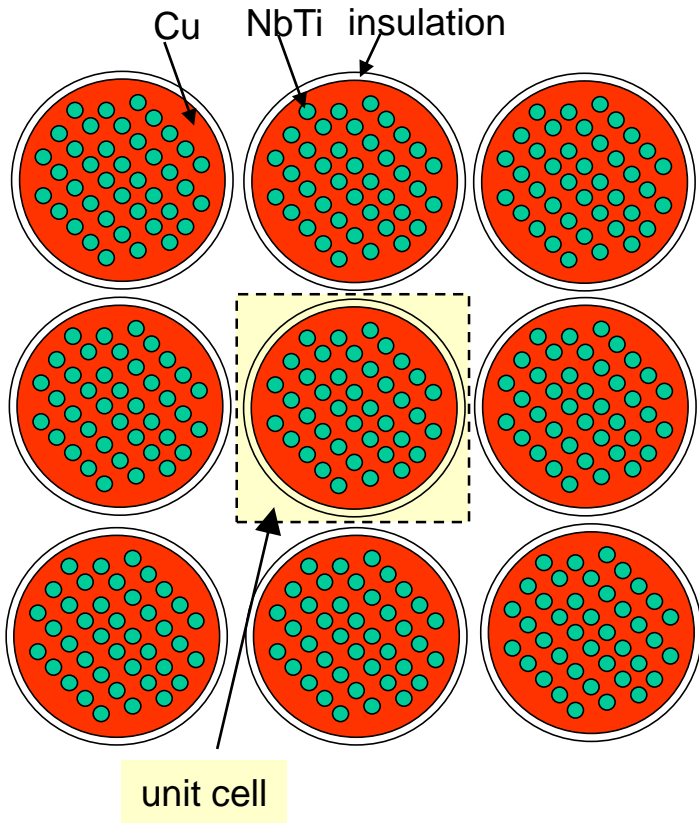
for Nb<sub>3</sub>Sn  $mat = 2.0$  to  $4.0$  ie  $\lambda_{sw} = 0.33$  to  $0.2$

for B2212  $mat = 3.0$  to  $4.0$  ie  $\lambda_{sw} = 0.25$  to  $0.2$

For Nb<sub>3</sub>Sn and B2212 the area of superconductor is not well defined, so often define  $J_{sup}$  over 'non matrix' or 'non Cu' area, which is greater than superconductor area.

$\lambda_{wu}$  fraction of wire in unit cell taking account of space occupied by insulation, cooling channels, reinforcement etc: typically  $\lambda_{wu} \sim 0.7$  to  $0.8$

filling factor of superconductor in unit cell  $\lambda_{su} = \lambda_{sw} \times \lambda_{wu}$



So typically  $J_{eng}$  is only 15% to 30% of  $J_{supercon}$

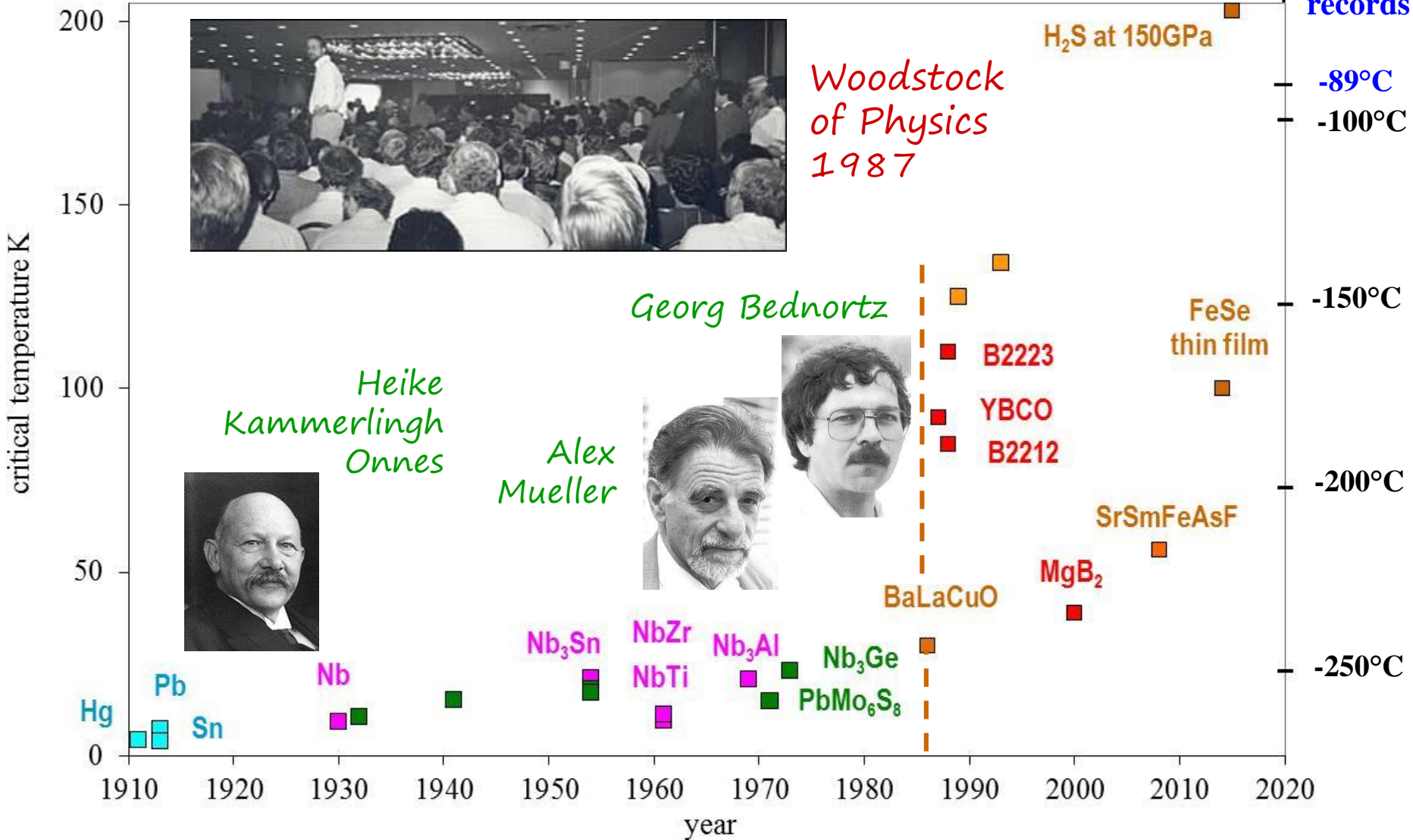
# Critical temperatures



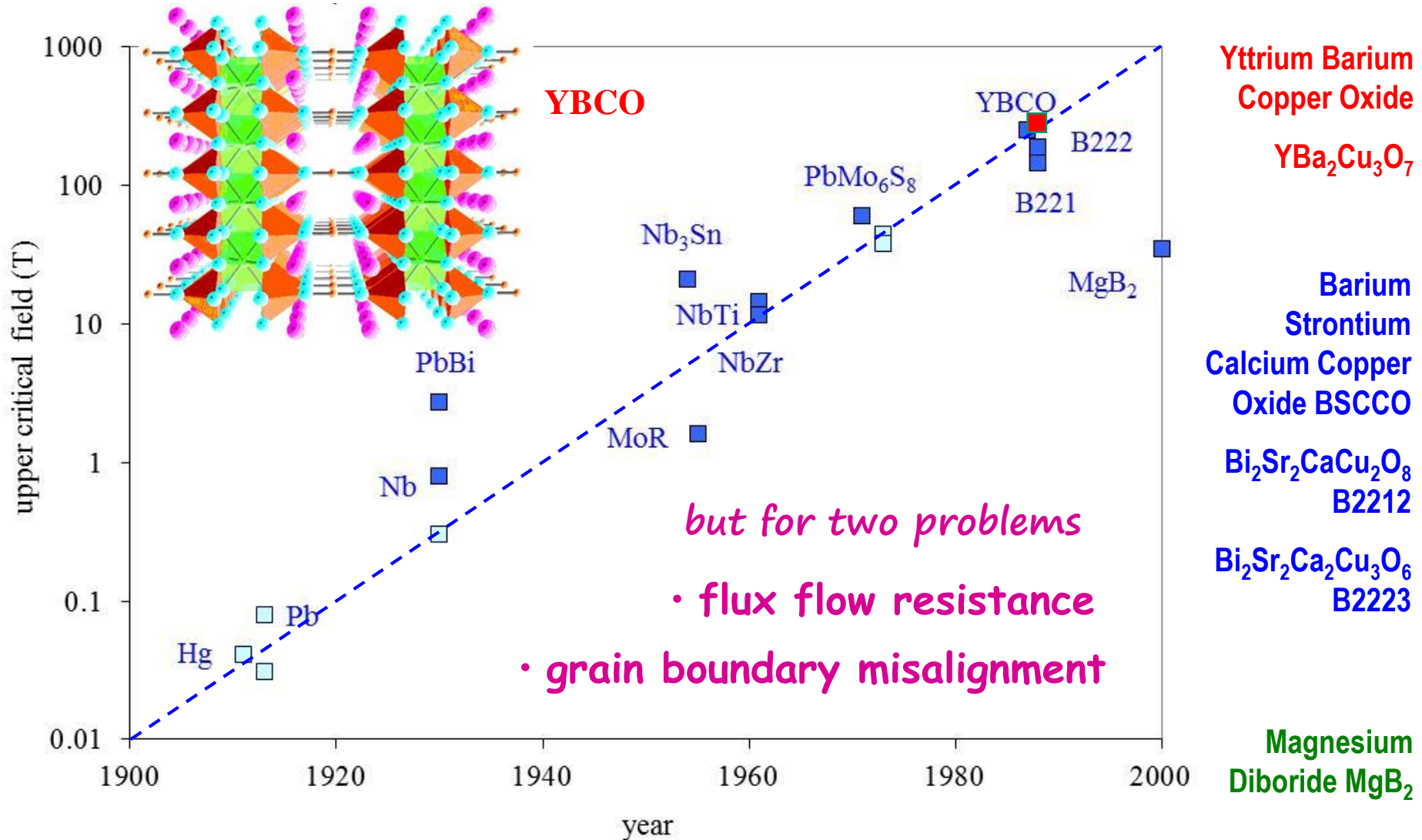
-20°C  
in 1983  
Vostok  
records



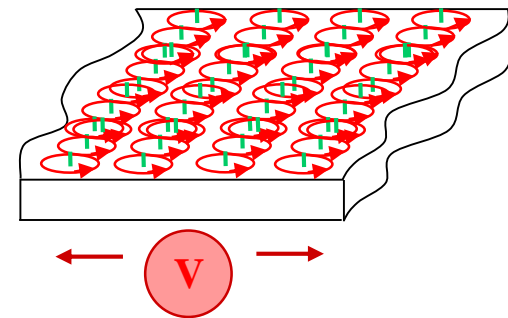
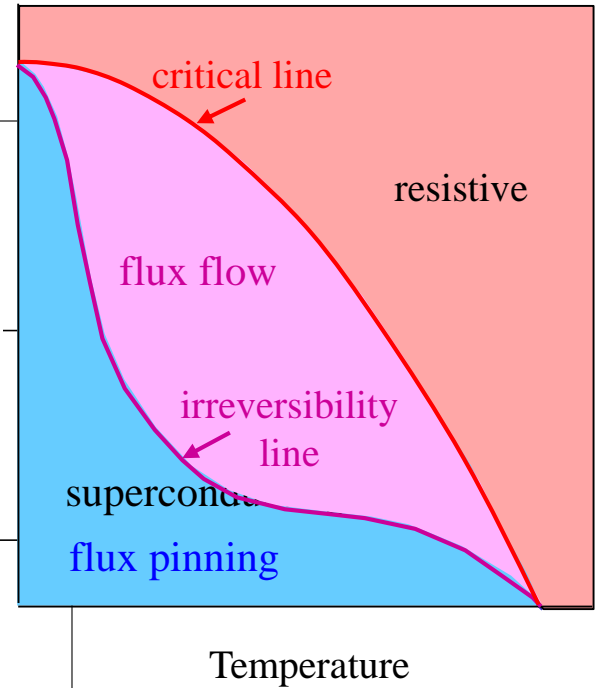
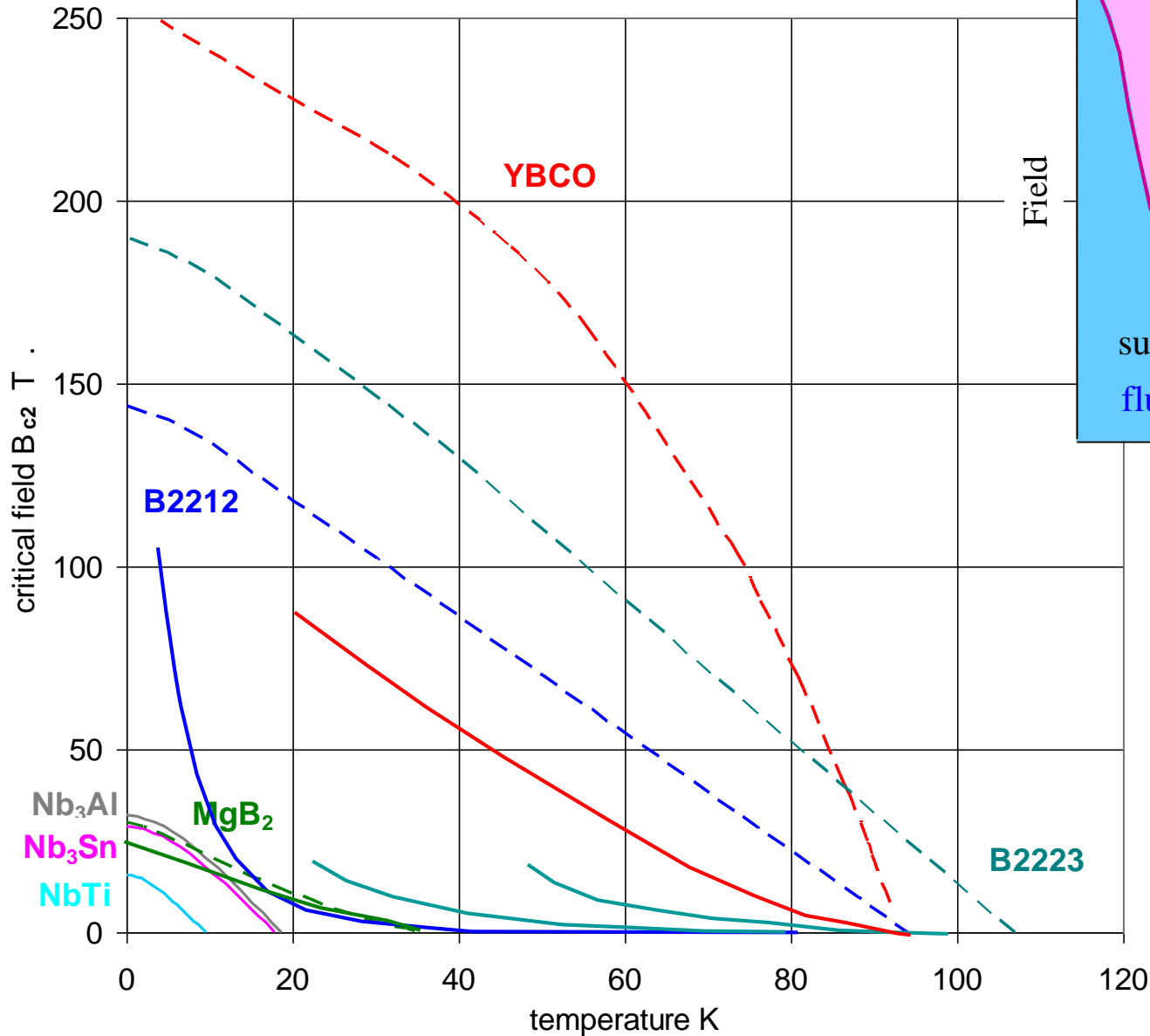
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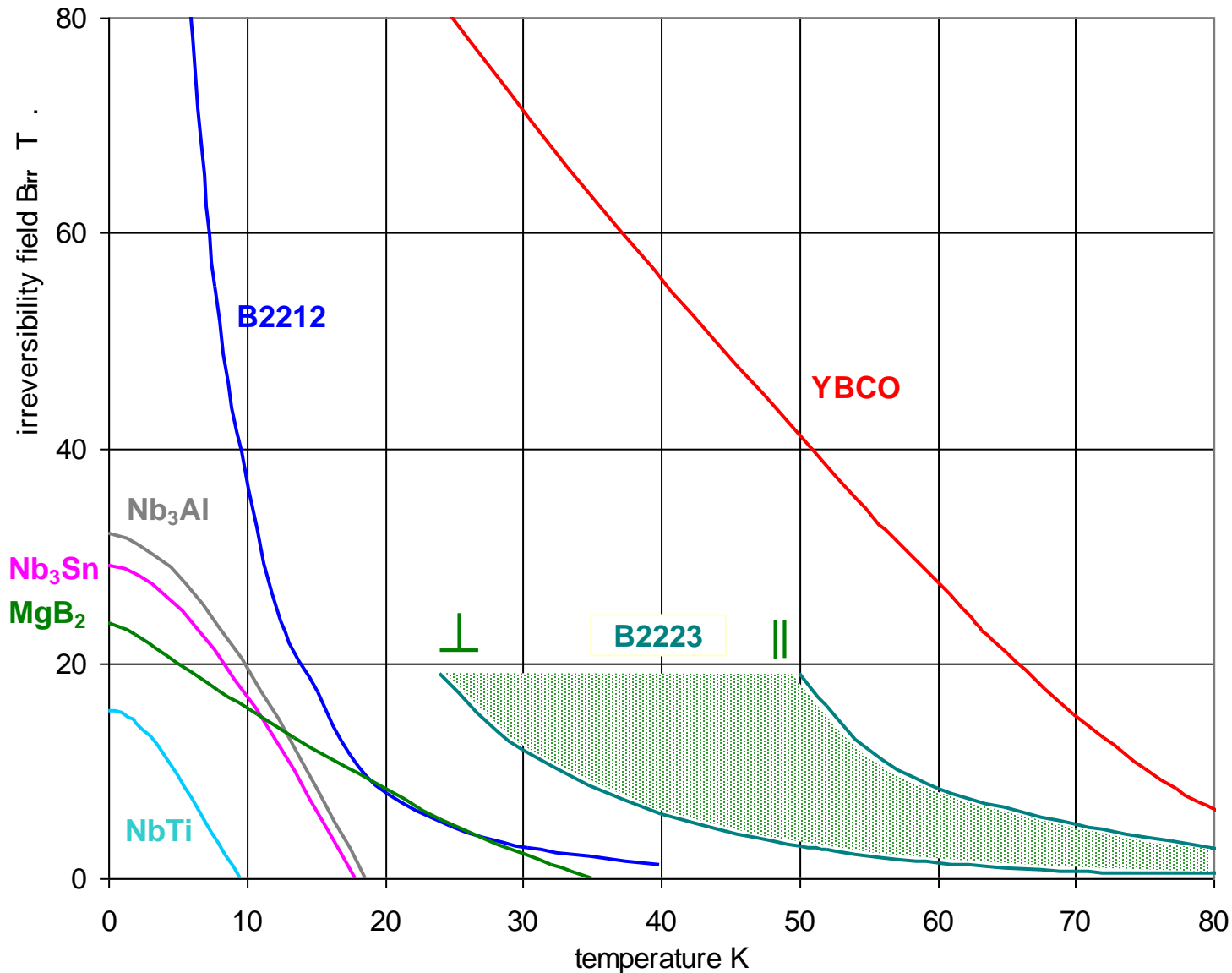
# Wonderful materials for magnets



# 1) Flux flow resistance



# Accessible fields for magnets



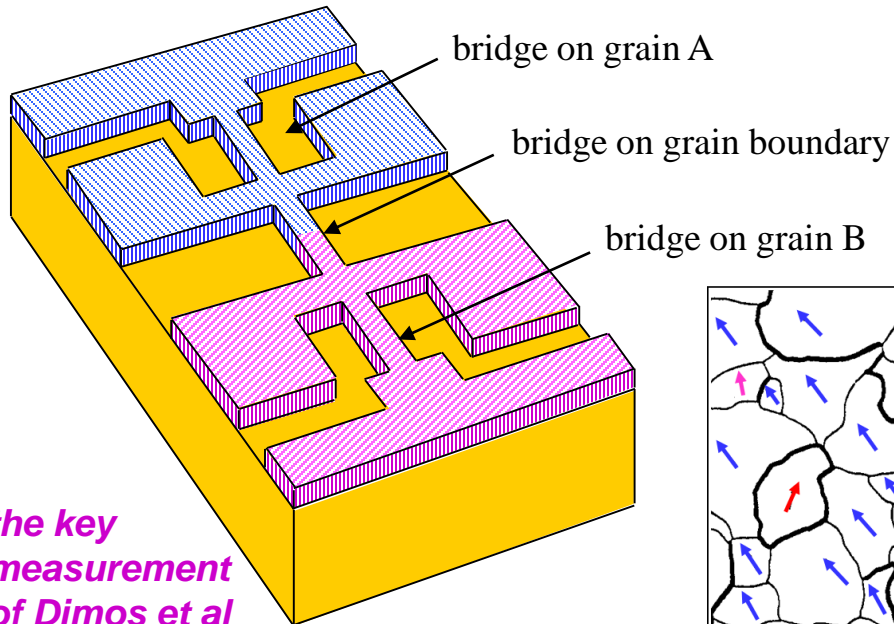
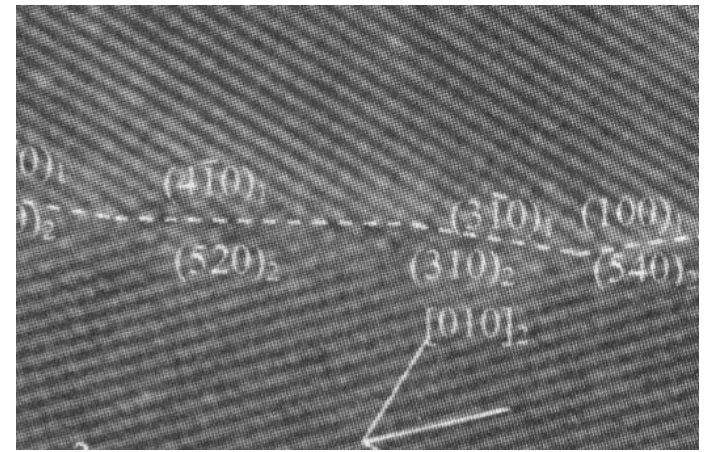
so here's the parameter space for future magnets

and we still need to work on the current density

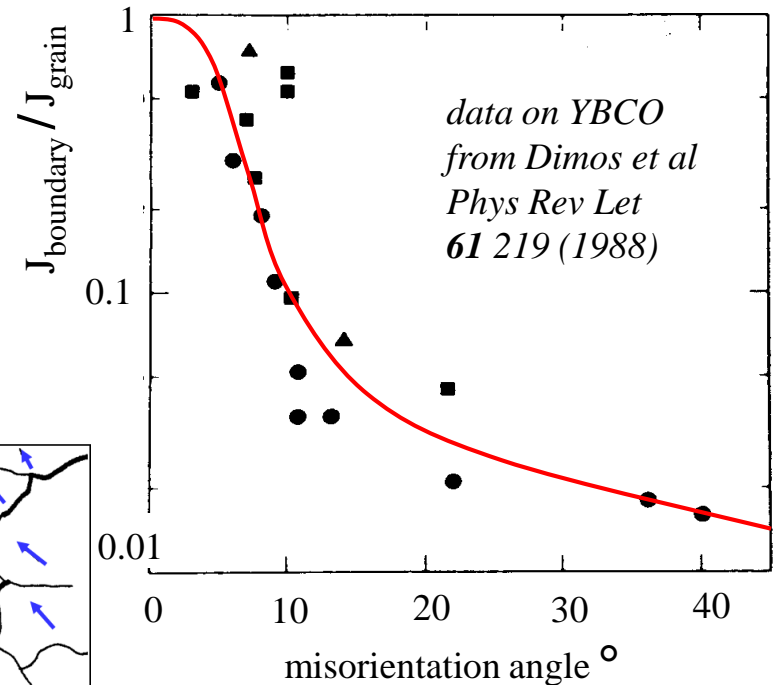
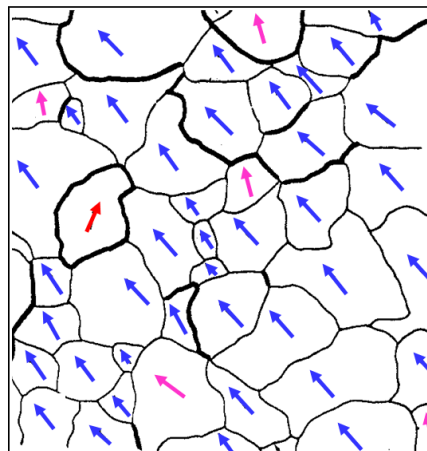


## 2) Grain boundary mismatch

- crystal planes in grains point in different directions
- critical currents are high within the grains
- $J_c$  across the grain boundary depends on the misorientation angle
- for good  $J_c$  must align grains to within a few degrees



the key measurement of Dimos et al

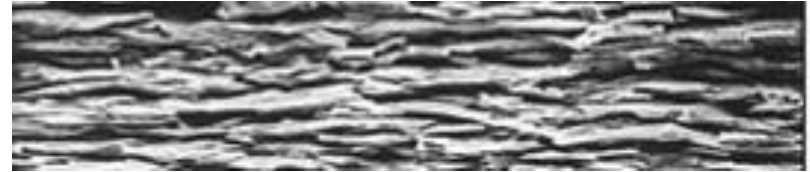
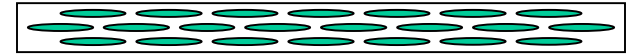
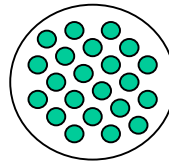
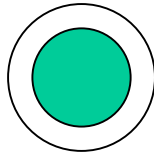


must align (almost) all the grains



# BSCCO conductors

- BSCCO powder in silver matrix
- silver is transparent to oxygen
- grains tend to line up during processing in contact with silver
- but low irreversibility field



## $\text{Bi}_2\text{Sr}_2\text{Ca}_2\text{Cu}_3\text{O}_6$ B2223

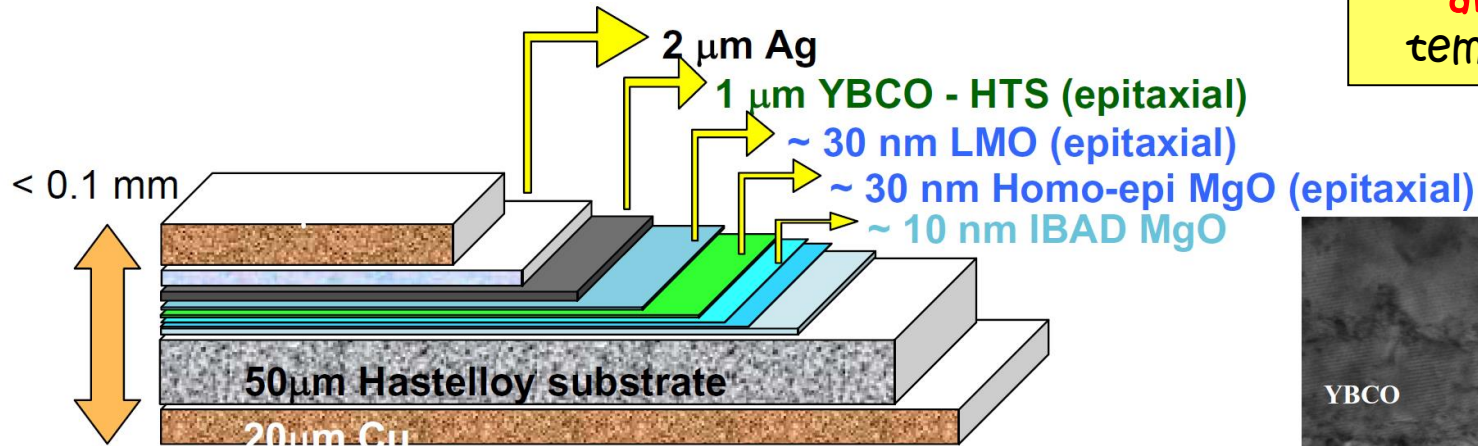
- $\theta_c \sim 110 \text{ K} \Rightarrow 77 \text{ K use}$
- complex thermo-mechanical fabrication route to produce uniaxial texture
- reaction of 2212 + stuff to 2223 occurs primarily in the solid state at  $\sim 840^\circ\text{C}$
- texture requires pressing to a large aspect ratio tape (4 x 0.2 mm)
- anisotropic  $J_c$
- mature conductor – semi commercial production for > 10 years

## $\text{Bi}_2\text{Sr}_2\text{CaCu}_2\text{O}_8$ B2212

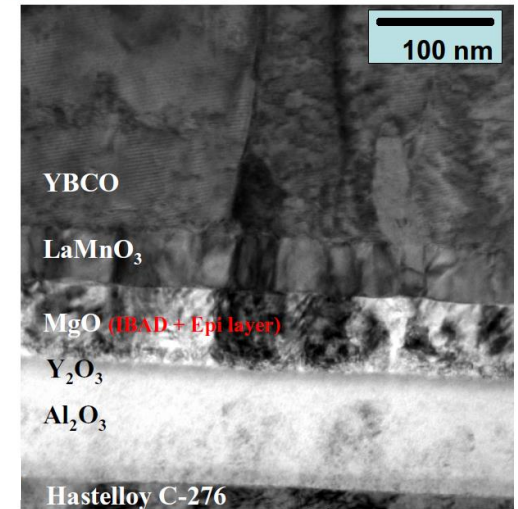
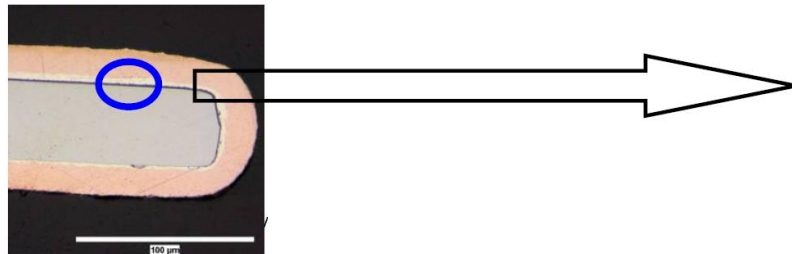
- $\theta_c \sim 85 \text{ K}$
- produced by melting B2212 powder inside silver matrix
- round filaments in round wires
- isotropic  $J_c$
- high  $J_c$  but used to be only in short samples
- recently achieved high  $J_c$  in long lengths
- engineers like round wire
- can make Rutherford cables

# Coated YBCO tape

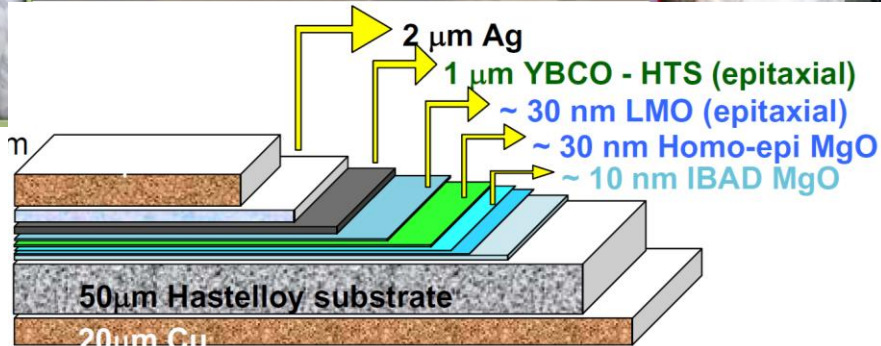
- YBCO has the best irreversibility field, but it is very sensitive to grain boundary misalignment
- the grains do not line up naturally - they must be persuaded
- deposit YBCO on a substrate where the grains are aligned and the lattice roughly matches YBCO



OK high field  
and high  
temperature



# YBCO coated tape at



# Lecture 1: concluding remarks

- superconductors allow us to build magnets which burn no power (except refrigeration)
- ampere turns are cheap, so don't need iron
  - ⇒ fields higher than iron saturation (but still use iron for shielding)
- performance of all superconductors described by the critical surface in  $B J \theta$  space,
- three kinds of superconductor
  - **type 1**: low temperature, unsuitable for high field
  - **type 2**: low temperature, good for high field - but must create flux pinning to get current density
  - **HTS**: high temperature, high field - but current density is a difficult problem
- NbTi is the most common commercial superconductor - standard production process
- Nb<sub>3</sub>Sn has higher critical field & temperature - specialized commercial production
- BSCO high temperature **or** high field, but not both - prototype commercial production
- YBCO high temperature **and** high field, but must align the grains - prototype commercial production
- measure  $I_c$  to check specification, the index  $n$  indicates quality
- for accelerators, so far it's only been NbTi, usually in Rutherford cables



# Some useful references

## Superconducting Magnets

- Superconducting Accelerator Magnets: KH Mess, P Schmuser, S Wolf., pub World Scientific, (1996) ISBN 981-02-2790-6
- Case Studies in Superconducting Magnets, Second edition: Y Iwasa, pub Springer (2009), ISBN 978-0-387-09799-2.
- High Field Superconducting Magnets: FM Asner, pub Oxford University Press (1999) ISBN 0 19 851764 5
- Superconducting Magnets: MN Wilson, pub Oxford University Press (1983) ISBN 0-019-854805-2
- Proc Applied Superconductivity Conference: pub as IEEE Trans Applied Superconductivity, Mar 93 to 99, and as IEEE Trans Magnetics Mar 75 to 91
- Handbook of Applied Superconductivity ed B Seeber, pub UK Institute Physics 1998

## Cryogenics

- Experimental Techniques for Low-temperature Measurements: J. W. Ekin Pub. Oxford University Press, ISBN 978-0-19-857054-7
- Helium Cryogenics Van Sciver SW, pub Plenum 86 ISBN 0-0306-42335-9
- Cryogenic Engineering, Hands BA, pub Academic Press 86 ISBN 0-012-322991-X
- Cryogenics: published monthly by Butterworths
- Cryogenie: Ses Applications en Supraconductivite, pub IIR 177 Boulevard Maiesherbes F5017 Paris France

## Materials Mechanical

- Materials at Low Temperature: Ed RP Reed & AF Clark, pub Am. Soc. Metals 1983. ISBN 0-87170-146-4
- Handbook on Materials for Superconducting Machinery pub Batelle Columbus Laboratories 1977.
- Nonmetallic materials and composites at low temperatures: Ed AF Clark, RP Reed, G Hartwig pub Plenum
- Nonmetallic materials and composites at low temperatures 2, Ed G Hartwig, D Evans, pub Plenum 1982
- Austenitic Steels at low temperatures Editors R.P.Reed and T.Horiuchi, pub Plenum 1983

## Superconducting Materials

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- Superconductivity of metals and Cuprates, JR Waldram, Institute of Physics Publishing (1996) ISBN 0 85274 337 8
- High Temperature Superconductors: Processing and Science, A Bourdillon and NX Tan Bourdillon, Academic Press, ISBN 0 12 117680 0
- Superconductivity: A Very Short Introduction by Stephen J. Blundell: Oxford University Press (2009) ISBN 978-0-19-954090-7

# on the Web

- **Lectures on Superconductivity** <http://www.msm.cam.ac.uk/ascg/lectures>.  
A series of lectures produced for SCENET by Cambridge University: fundamentals, materials, electronics, applications. Also available as a DVD
- **Superconducting Accelerator Magnets** <http://www.mjb-plus.com>.  
A course developed from SSC experience, available from website for \$20
- [www.superconductors.org](http://www.superconductors.org) website run by an enthusiast; gives some basic info and links
- **Superconductivity Course** at the (UK) Open University.  
<http://openlearn.open.ac.uk/course/view.php?id=2397> Good coverage of basics.
- **Wikipedia** on Superconductivity <http://en.wikipedia.org/wiki/Superconductivity>  
Good on basics with lots of references and links.
- **European Society for Applied Superconductivity** <http://www.esas.org/>  
News, events and people in the area of applied superconductivity
- **CONNECTUS** Consortium of European Companies determined to use Superconductivity  
<http://www.conectus.org/>
- **IEEE Council on Superconductivity** <http://www.ewh.ieee.org/tc/csc/>  
News, events and people in the area of applied superconductivity (US based)



# Materials data on the Web

- Cryogenic properties (1-300 K) of many solids, including thermal conductivity, specific heat, and thermal expansion, have been empirically fitted and the equation parameters are available free on the web at [www.cryogenics.nist.gov](http://www.cryogenics.nist.gov)
- Thermodynamic properties of gases (and liquids) available free as a programme which you can interrogate for your own temperature interval etc.  
<http://webbook.nist.gov/chemistry/fluid/>
- Plots and automated data-look-up using the NIST equations are available on the web for a fee from [www.cpia.jhu.edu](http://www.cpia.jhu.edu)
- Other fee web sites that use their own fitting equations for a number of cryogenic material properties include: [www.cryodata.com](http://www.cryodata.com) (cryogenic properties of about 100 materials), and [www.jahm.com](http://www.jahm.com) (temperature dependent properties of about 1000 materials, many at cryogenic temperatures).
- Commercially supplied room-temperature data are available free online for about 10 to 20 properties of about 24,000 materials at [www.matweb.com](http://www.matweb.com)

## *Cryodata Software Products*

### GASPAK

properties of pure fluids from the triple point to high temperatures.

### HEPAK

properties of helium including superfluid above 0.8 K, up to 1500 K.

### STEAMPAK

properties of water from the triple point to 2000 K and 200 MPa.

### METALPAK, CPPACK, EXPAK

reference properties of metals and other solids, 1 - 300 K.

### CRYOCOMP

properties and thermal design calculations for solid materials, 1 - 300 K.

### SUPERMAGNET

four unique engineering design codes for superconducting magnet systems.

### KRYOM

numerical modelling calculations on radiation-shielded cryogenic enclosures.

*thanks to Jack Ekin of NIST and Charles Monroe for this information*