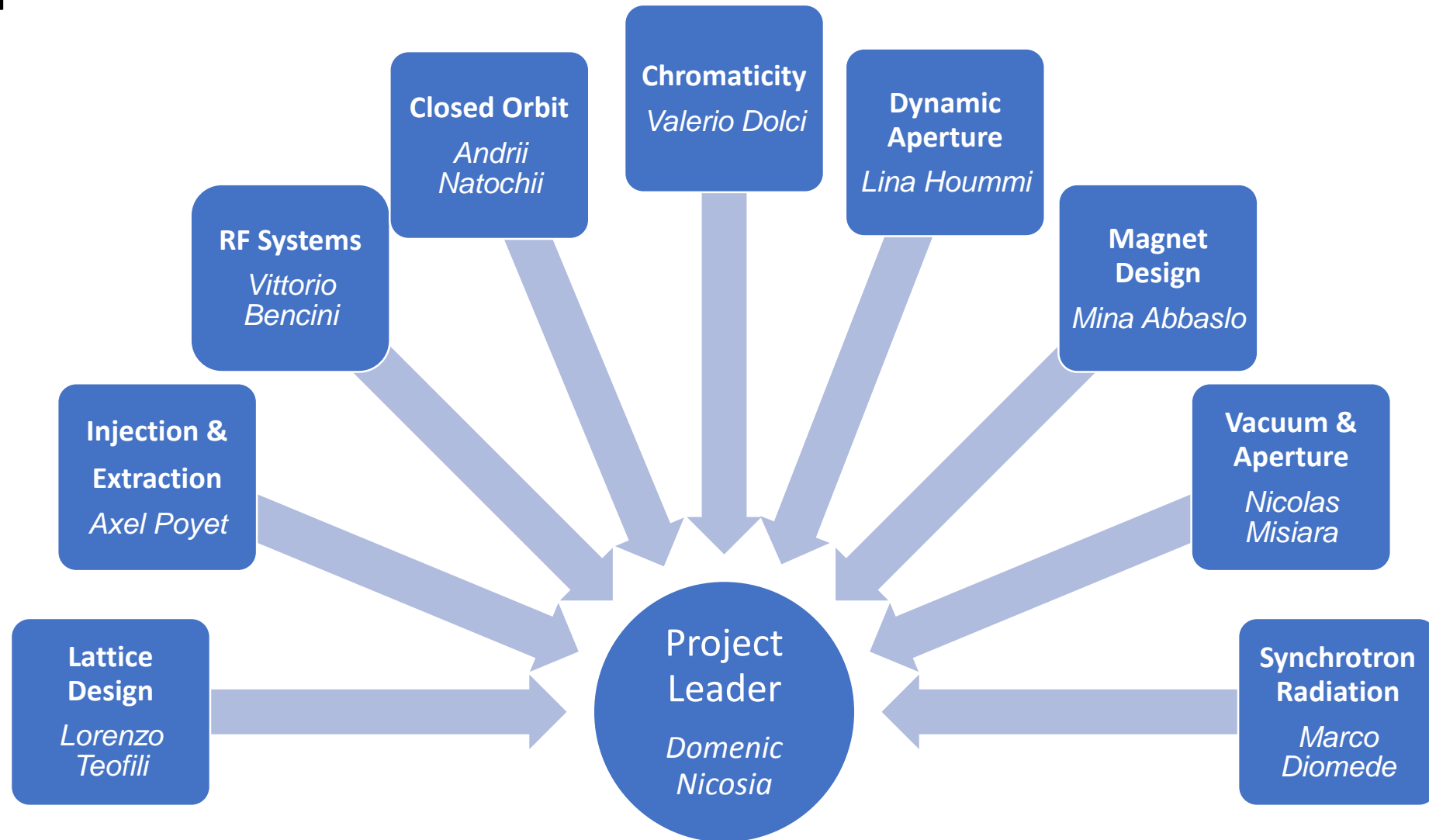




Synchrotron Light Source Project

JUAS 2017

Group Structure



Content

- Introduction
- Lattice design
- Injection/Extraction
- RF
- Closed orbit
- Chromaticity
- Dynamic Aperture & Resonances
- Magnet considerations
- Aperture & Vacuum considerations
- Synchrotron radiation

Aim

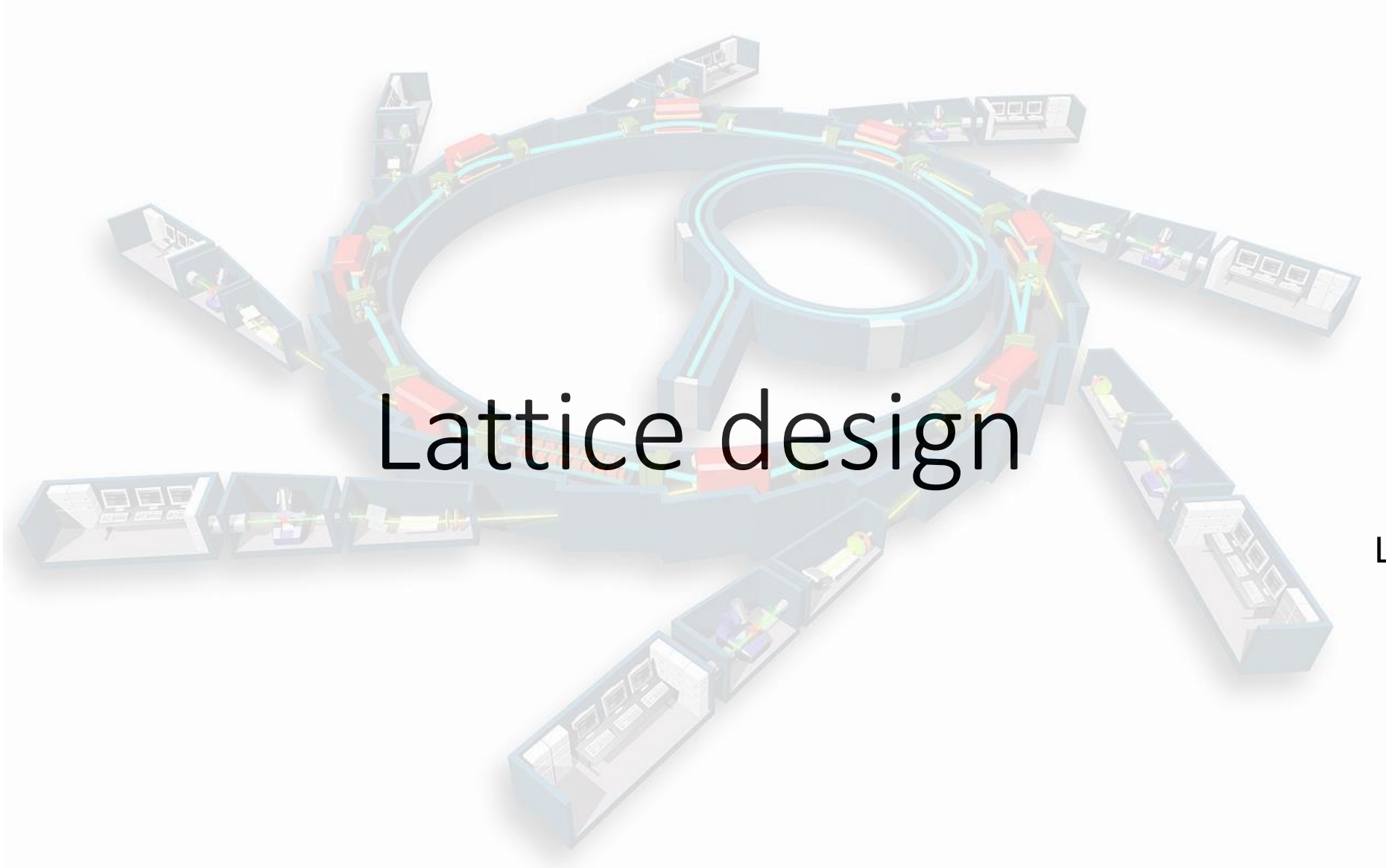
- To upgrade a synchrotron light facility with a new 3 GeV high-brightness ring, whilst keeping the existing 2GeV injector.

Requirements

- Maximum permitted circumference: 700m
- Lattice: 2 super periods connected by 2 dispersion-free regions
- Super period contains DBA 12 bending cells
- 500MHz RF system, 2GeV to 3GeV whilst compensating for radiative losses
- Smallest possible equilibrium horizontal emittance

Existing injector parameters

- Existing injector operates at 500MHz
- Single injector pulse contains 225 bunches, duty cycle of 5s
- Bunch length of 40ps (12mm)
- Bunch intensity of 4×10^{10} electrons per bunch
- 1- σ emittances of 0.15π mm mrad for both in both H & V planes, $\frac{\Delta p}{p} = 10^{-3}$



Lattice design

Lorenzo Teofili,
Heidi
Giacomo
Riccardo
Antonia
Paul
Ángel
Ezgy
Antonio
Pang

The lattice group



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Antonia Morabito
Riccardo Mirabelli
Ezgi Ergenlik
Heidi Ayse Rösch
Ángel Ferran Pousa
Paul Thrane
Antonio Paladino
Giacomo Mazzacano
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And Riccardo

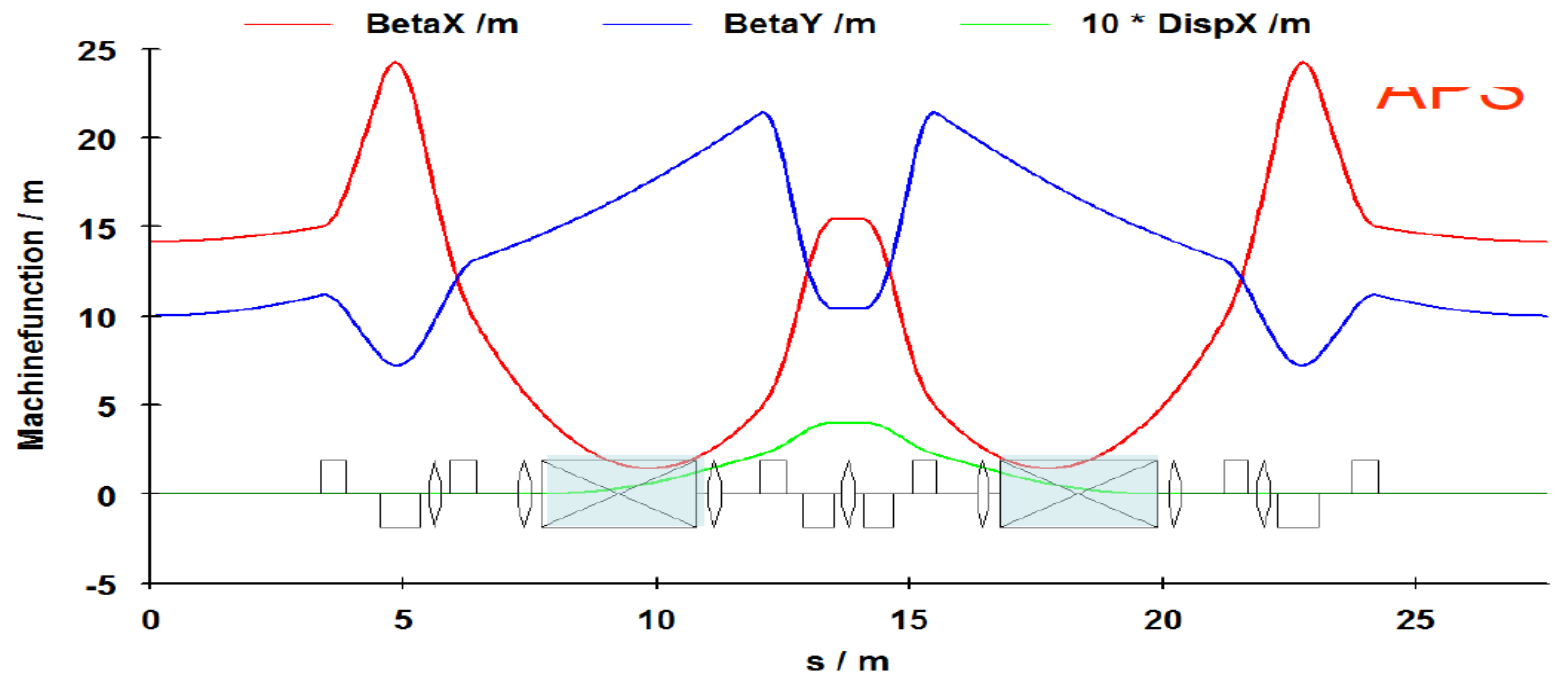
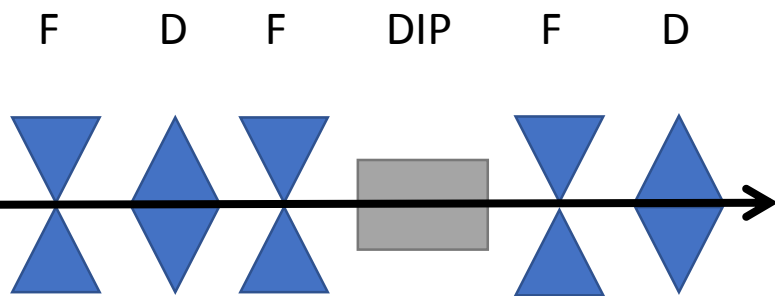


The main task

Improving the lattice of a 2^o generation synchrotron light source lattice into a 3^o generation one

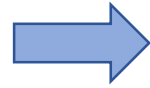
The key parameter to do that is the emittance! Indeed, the performance of such a machine are optimized if the lattice keep the equilibrium **emittance as lower as possible**, however, having a **reasonable cost!**

Standard Cell Double Bend Achromat (DBA)



Cell optimization (Numerical)

Here it is our main Guest
The Equilibrium Emittance



$$E_{x,eq} = A \left[\frac{\int_{Dipole} H(s) ds}{L\rho_0 + 2\rho_0^2 k \int_{Dipole} D_x(s) ds} \right]$$

- **First Optimization:**
Chasman-Green

$$\beta_x(0) = 1.549L$$

$$\alpha_x(0) = 3.873$$

- **"Super" Optimization**
Including the gradient

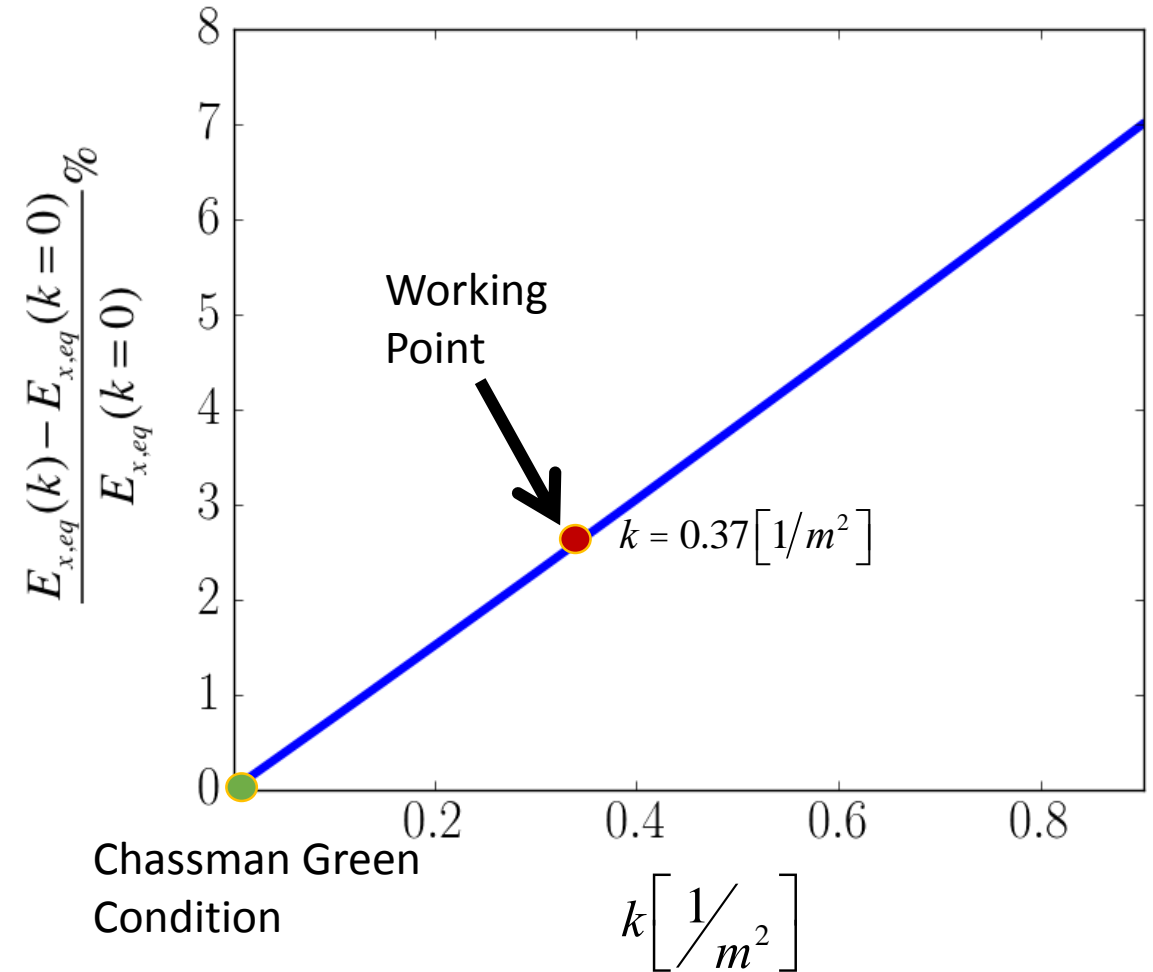
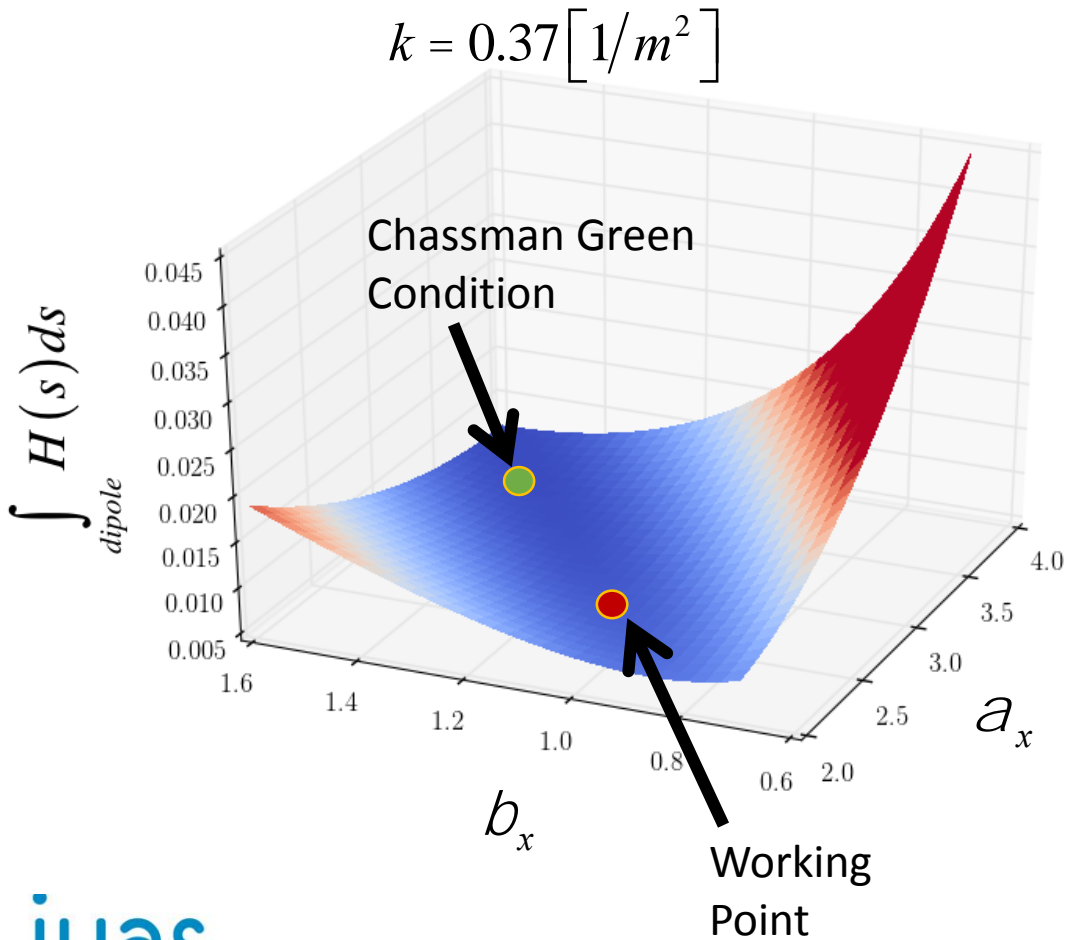
$$\beta_x(0) = ?$$

$$\alpha_x(0) = ?$$

$$H(s) = \gamma_x D_x^2 + 2\alpha_x D_x D_x' + \beta_x D_x'^2$$

$$\begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_s = \begin{pmatrix} t_{11}^2 & -2t_{11}t_{12} & t_{12}^2 \\ -t_{11}t_{21} & t_{11}t_{22} + t_{12}t_{21} & -t_{12}t_{22} \\ t_{21}^2 & -2t_{21}t_{22} & t_{22}^2 \end{pmatrix} \begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_0$$

Cell optimization (Numerical)

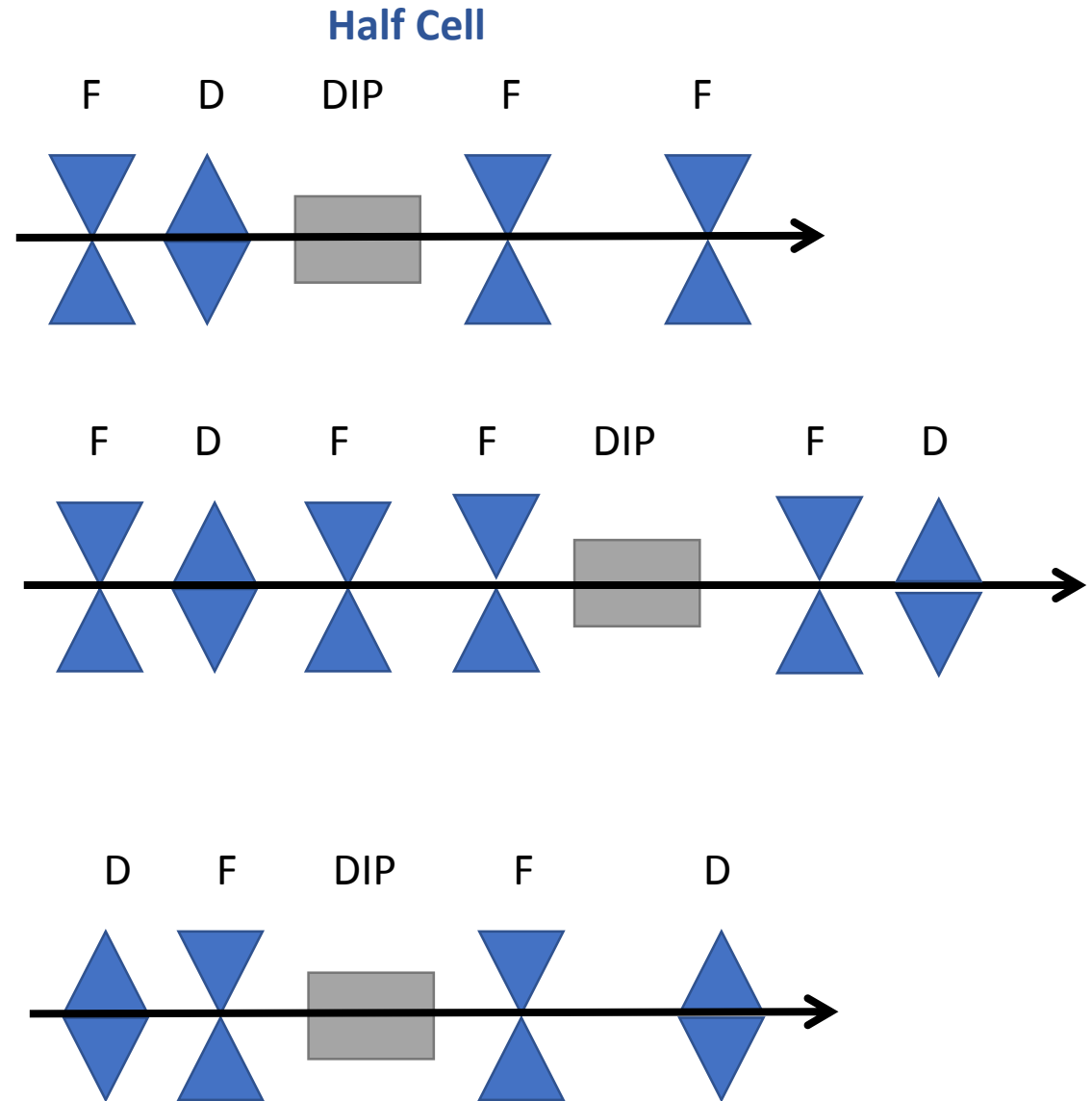


Three different cell designs

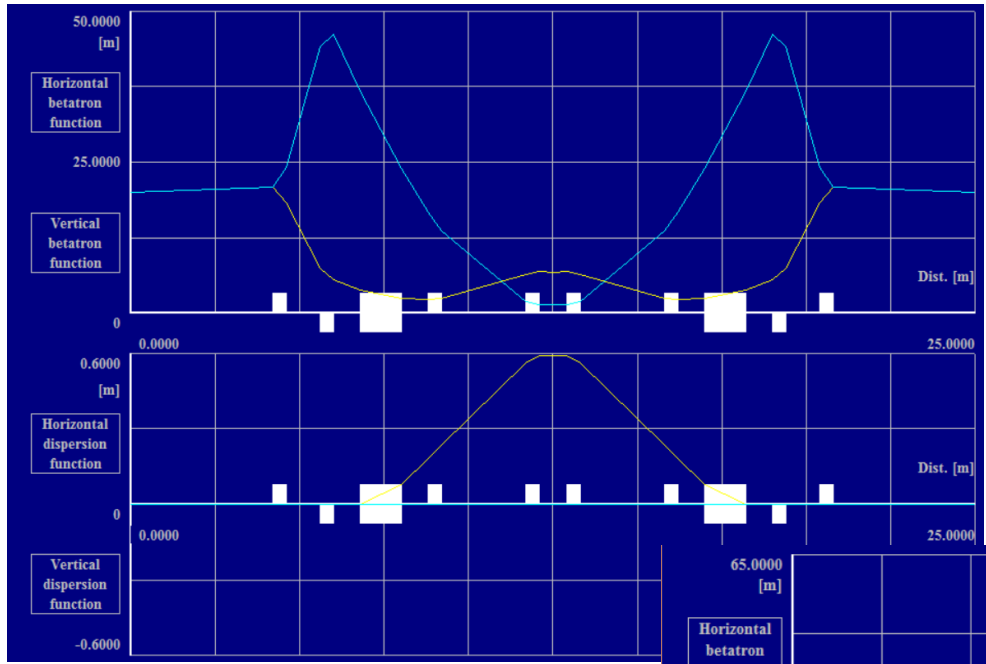
	Cell Values
Beam size (hor.) (mm)	1.28
Beam size (vert.) (mm)	1.90
Eq. Emittance (mm mrad)	0.026π
Beta max horizontal (m)	20.08
Beta max vertical (m)	44.25
Maximum Disp. (vert.) (m)	0.59

Beam size (hor.) (mm)	1.7
Beam size (vert.) (mm)	3.9
Eq. Emittance (mm mrad)	0.0014π
Beta max horizontal (m)	33.65
Beta max vertical (m)	64.8
Maximum Disp. (vert.) (m)	0.23

Beam size (hor.) (mm)	0.52
Beam size (vert.) (mm)	0.53
Eq. Emittance (mm mrad)	0.0026π
Beta max horizontal (m)	25.08
Beta max vertical (m)	62.67
Maximum Disp. (vert.) (m)	0.3607

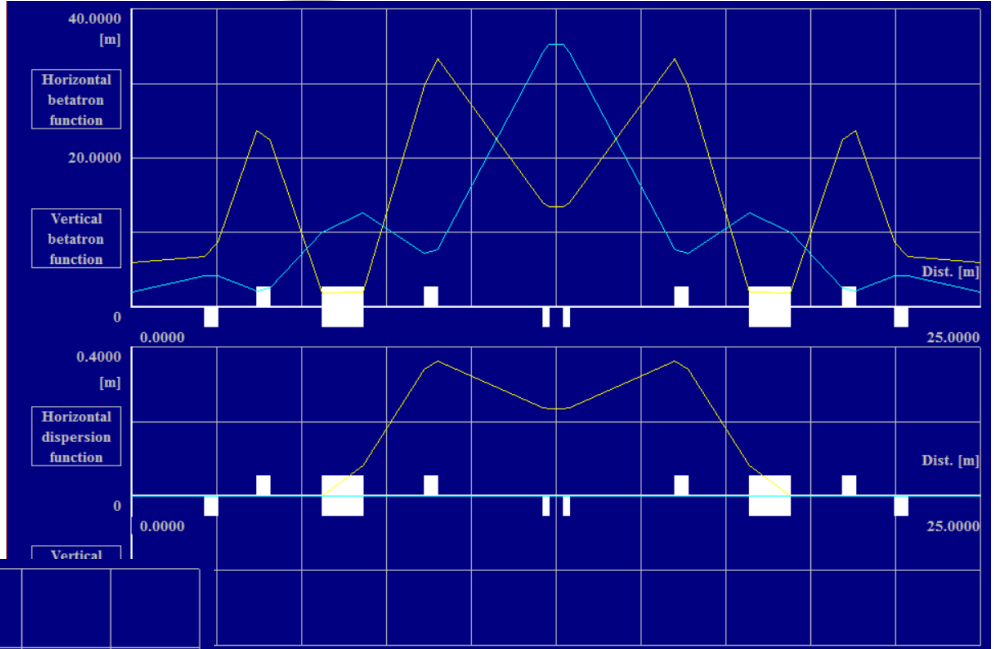


Three Different Cell Designs

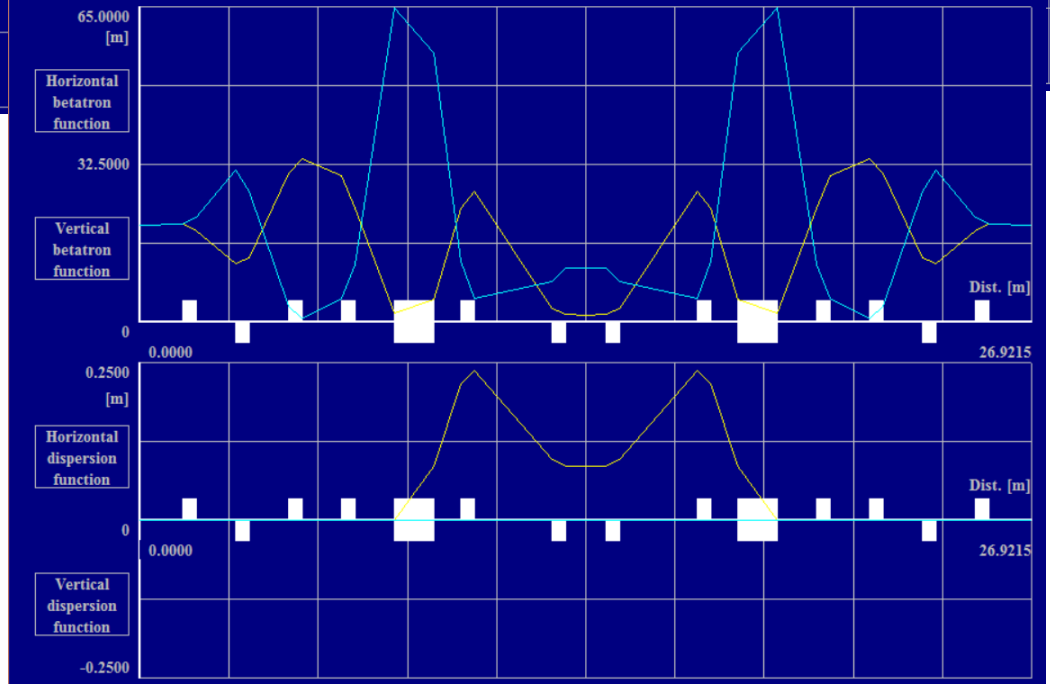


Basic Cell

1° Optimized Cell

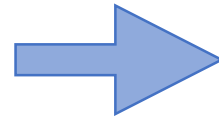


2° Optimized Cell



Cost estimation

“Rough” estimation
of components cost



Quadrupole ~ 15K\$
Dipole ~ 20K\$

- Basic Cell

Element	Number	Length [m]
Dipole	2	1.2
Quadrupole	8	0.4

Total Cost:3840 K\$

$\epsilon=0.0260 \pi \text{ mm mrad}$

$\epsilon C=99.84 \pi \text{ mm mrad K\$}$

- 1° Optimized Cell:

Element	Number	Length [m]
Dipole	2	1.2
Quadrupole	12	0.4

Total Cost:5280 K\$

$\epsilon=0.0014 \pi \text{ mm mrad}$

$\epsilon C=7.795 \pi \text{ mm mrad K\$}$

- 2° Optimized Cell:

Element	Number	Length [m]
Dipole	2	1.2
Quadrupole	6 (+2)	0.4 (0.2)

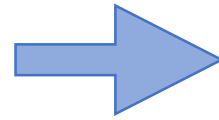
Total Cost:3840 K\$

$\epsilon=0.0026 \pi \text{ mm mrad}$

$\epsilon C=9.98 \pi \text{ mm mrad K\$}$

Cost estimation

“Rough” estimation
of components cost



Quadrupole ~ 15K\$
Dipole ~ 20K\$

• Basic Cell

Element	Number	Length [m]
Dipole	2	1.2
Quadrupole	8	0.4

Total Cost:3840 K\$

$\epsilon=0.0260 \pi \text{ mm mrad}$

$\epsilon C=99.84 \pi \text{ mm mrad K\$}$

• 1° Optimized Cell:

NOT STABLE

Element	Number	Length [m]
Dipole	2	1.2
Quadrupole	12	0.4

Total Cost:5280 K\$

$\epsilon=0.0014 \pi \text{ mm mrad}$

$\epsilon C=7.795 \pi \text{ mm mrad K\$}$

• 2° Optimized Cell:

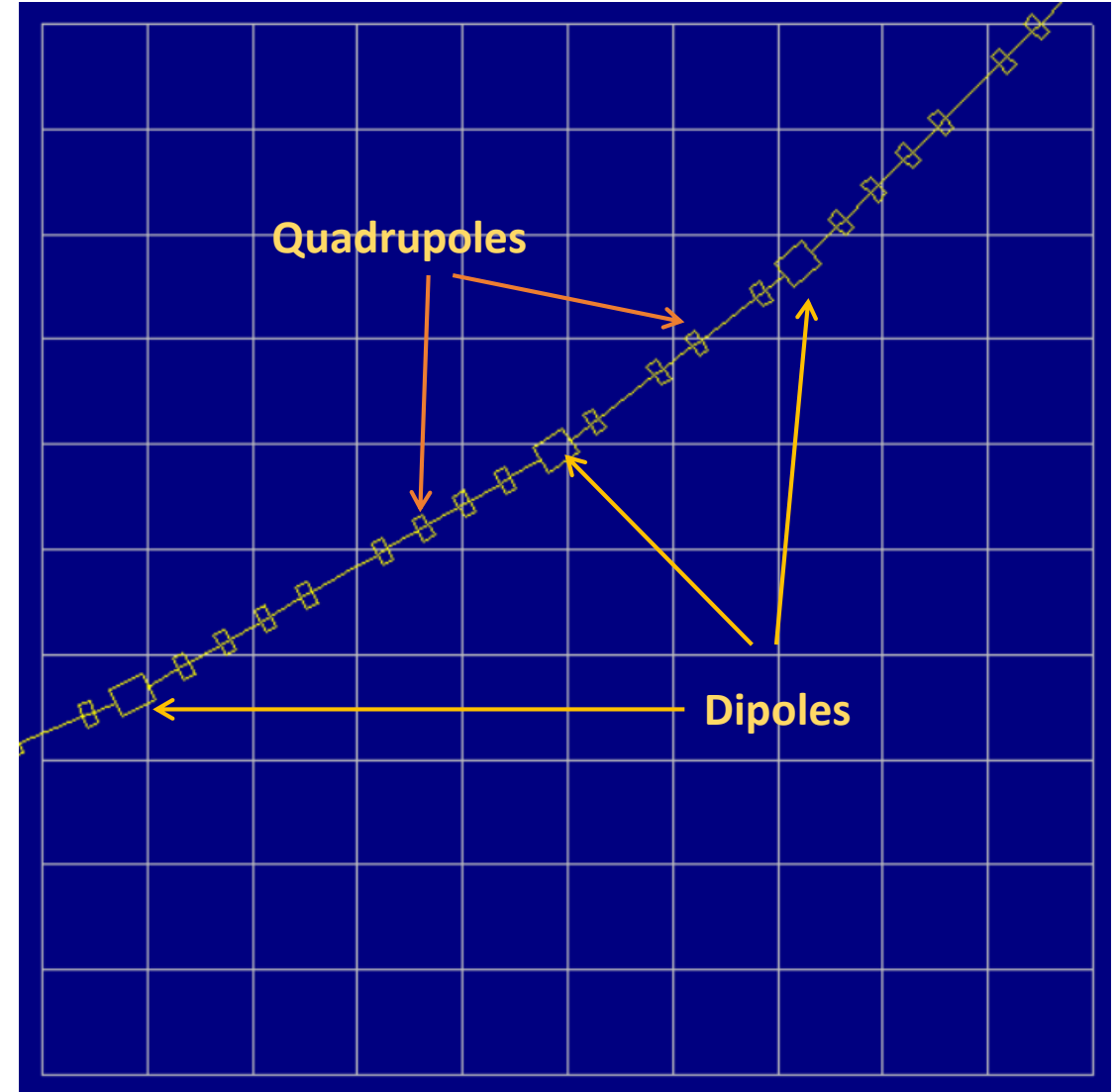
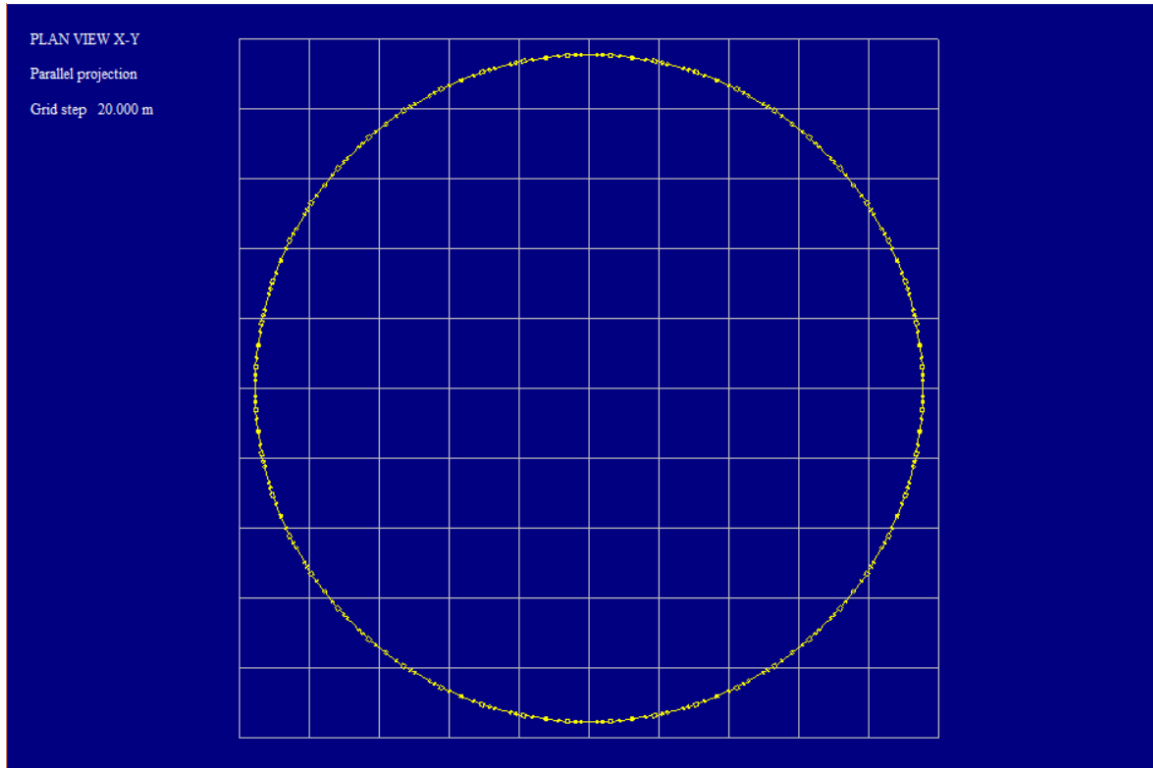
Element	Number	Length [m]
Dipole	2	1.2
Quadrupole	6(+2)	0.4 (0.2)

Total Cost:3840 K\$

$\epsilon=0.0026 \pi \text{ mm mrad}$

$\epsilon C=9.98 \pi \text{ mm mrad K\$}$

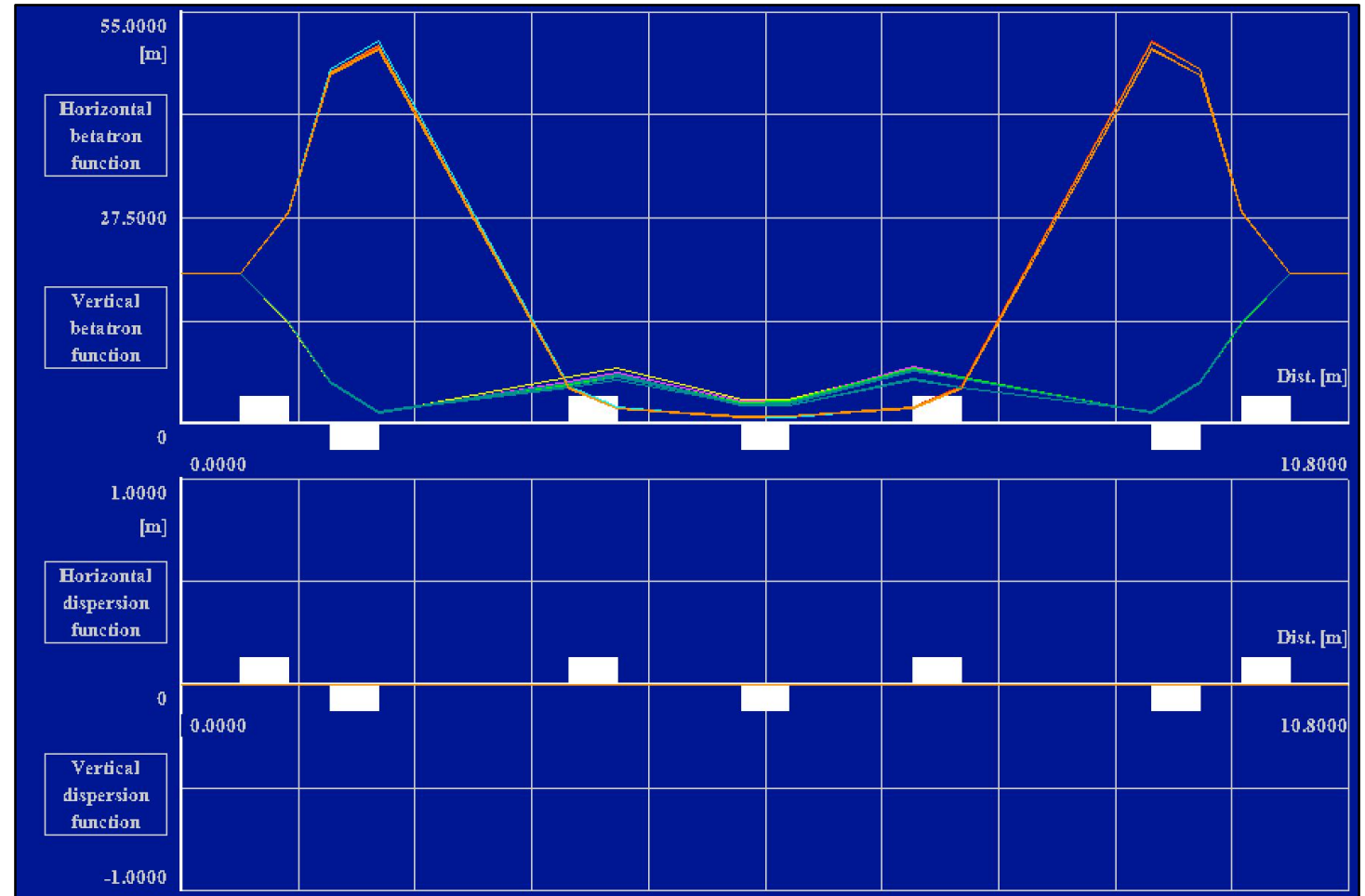
Lattice design geometry



CENTRAL ORBIT			
Circular machine			
Circumference	[m] =		599.9993
Horizontal tune	$Q_x =$		27.113570
Vertical tune	$Q_z =$		17.747357
Horizontal chromaticity	$dQ_x/dp/p =$		-111.972
Vertical chromaticity	$dQ_z/dp/p =$		-33.531
Gamma transition	gamma tr =		59.61421

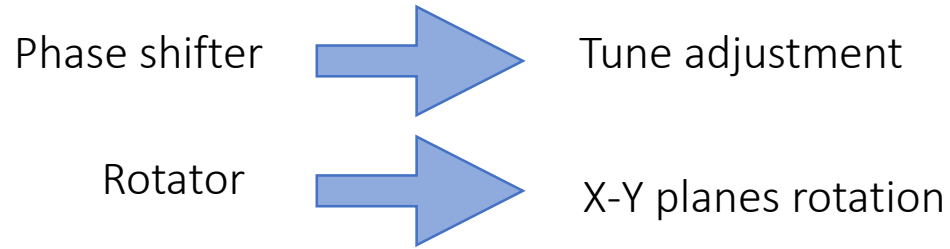
Phase shifter

- Change phase advance to find the best working point.
- Phase advance of the shifter changed from $\Delta\mu = 6.2832$ to $\Delta\mu = 6.40$ to explore a big range of phase shifts.
- 6 steps of phase shifts from $\Delta\mu = 6.30$ to $\Delta\mu = 6.40$
- To find the matching, 6 conditions were set, with 7 quadrupole gradients used as variables.

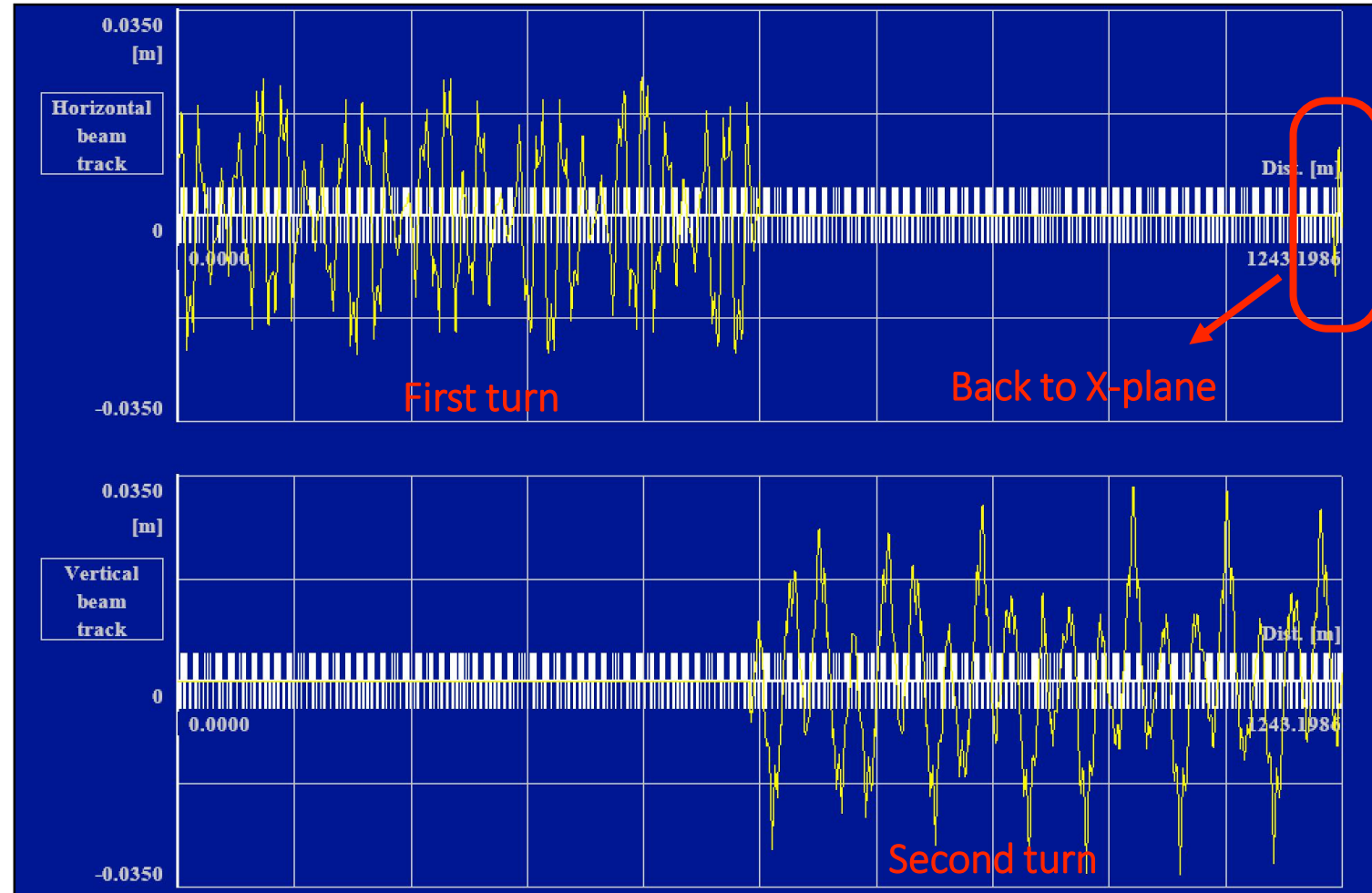


Möbius Ring

- Phase shifter and rotator added to the ring.



- Ring lattice replicated two times and run as a transfer line.
- Using single particle tracking:
 - during first turn the particle oscillates in X-plane;
 - during second turn the particle oscillates in Y-plane;
- Successful exchange of X-Y planes.





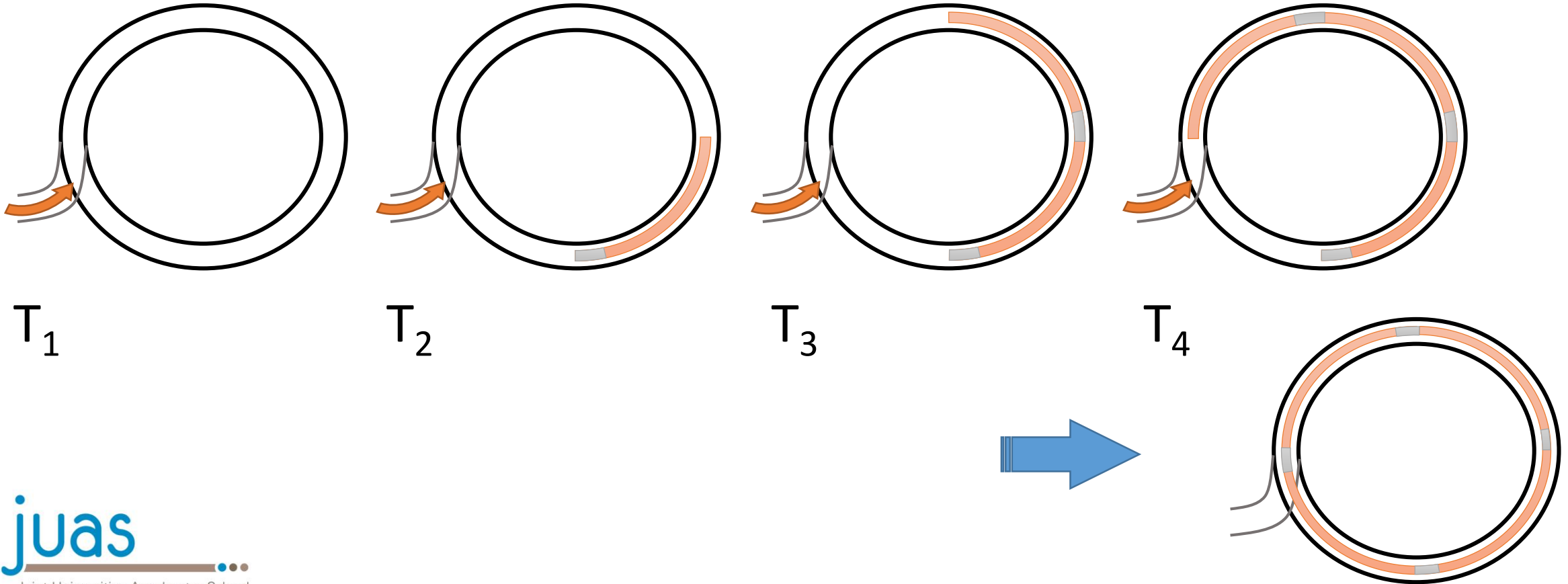
Injection/Extraction

Axel Poyet
Edgar
Jérémy
Félix,
Doru
Alexandru
Adrian
Volker Schramm

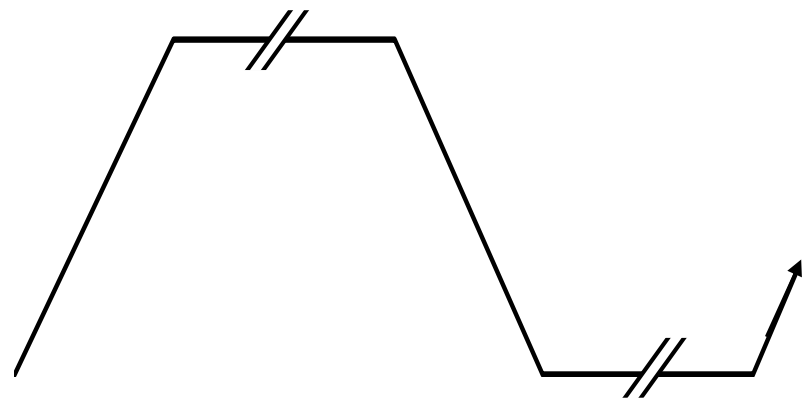
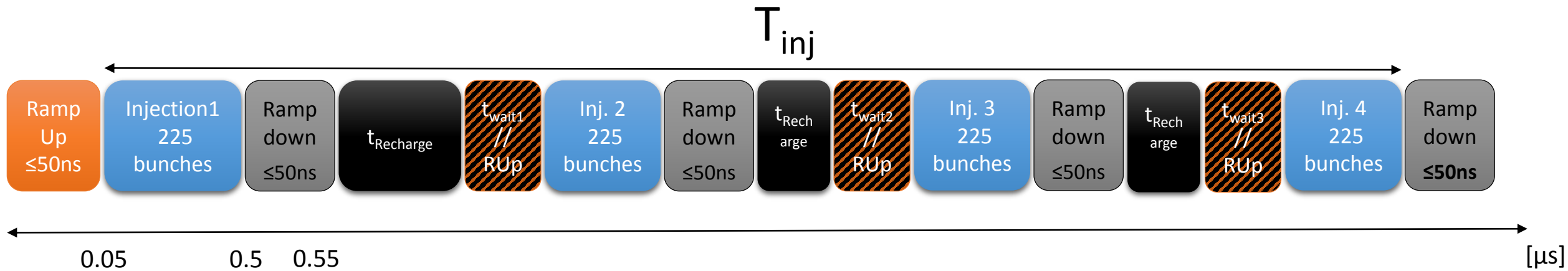
Injection Process

1st approach (tricky solution):

- Injection of 4 pulses (225 bunches) in 4 separate periods



Injection Process



- Flat top for 450ns to inject a pulse of 225 bunches
- Ramp up/down $\leq 50\text{ns}$ to keep a gap of 25 bunches

$t_{\text{Ramp Up/Down}}$

Available time to ramp the magnet

t_{Recharge}

Needed time to recharge capacitors (PS)

t_{wait}

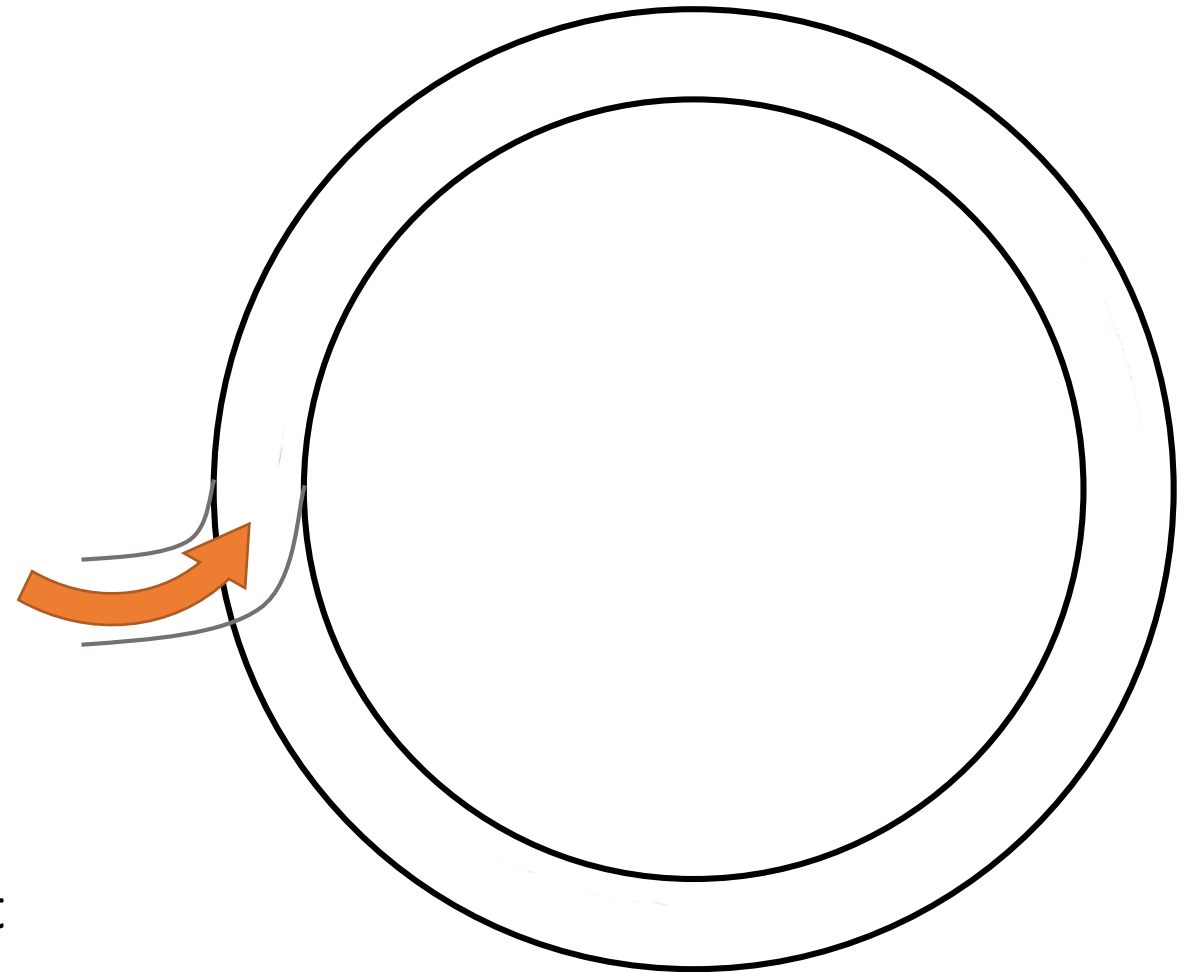
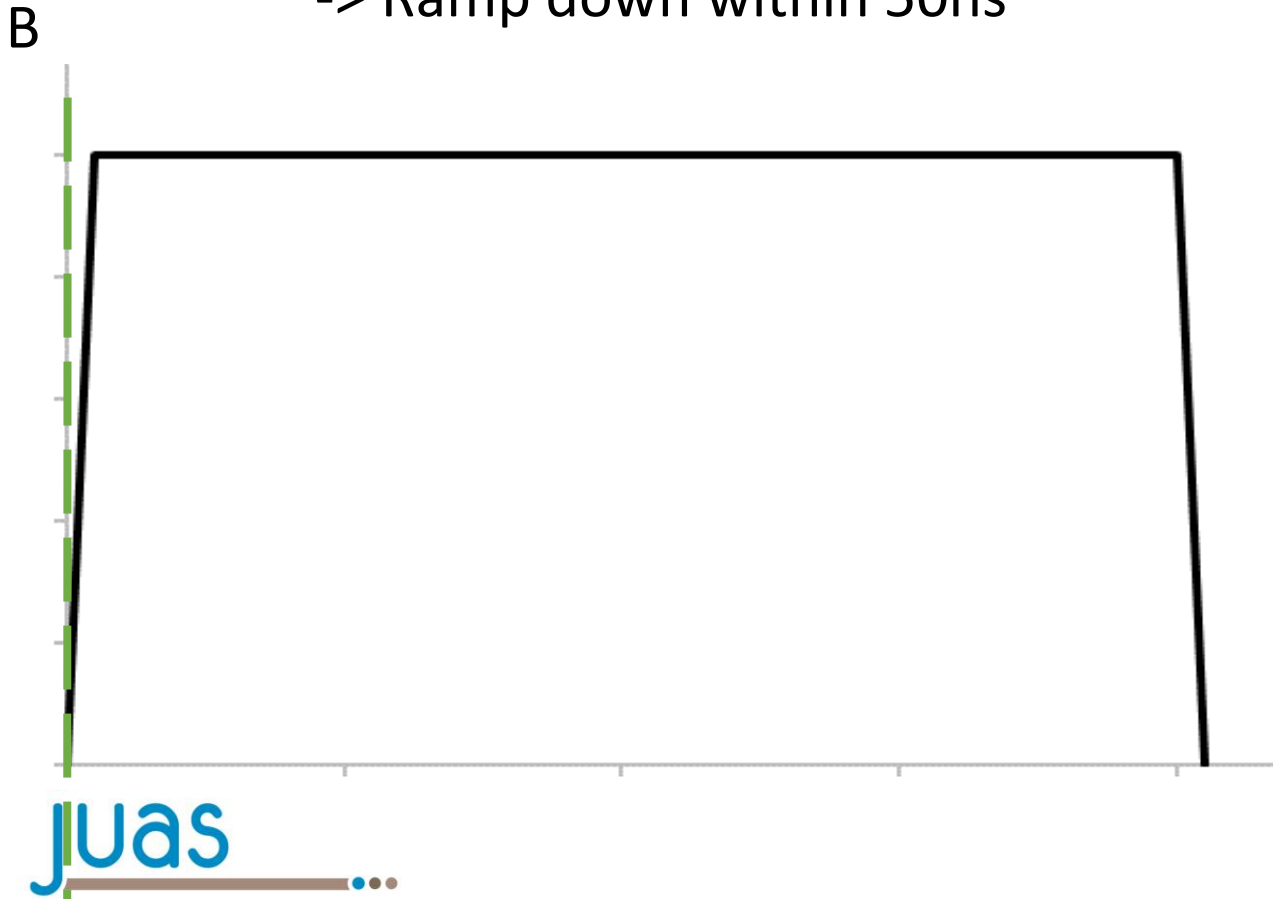
Waiting time to place next pulse

Injection Process

Simple solution:

-> Ramp up and inject all 4 pulses at once

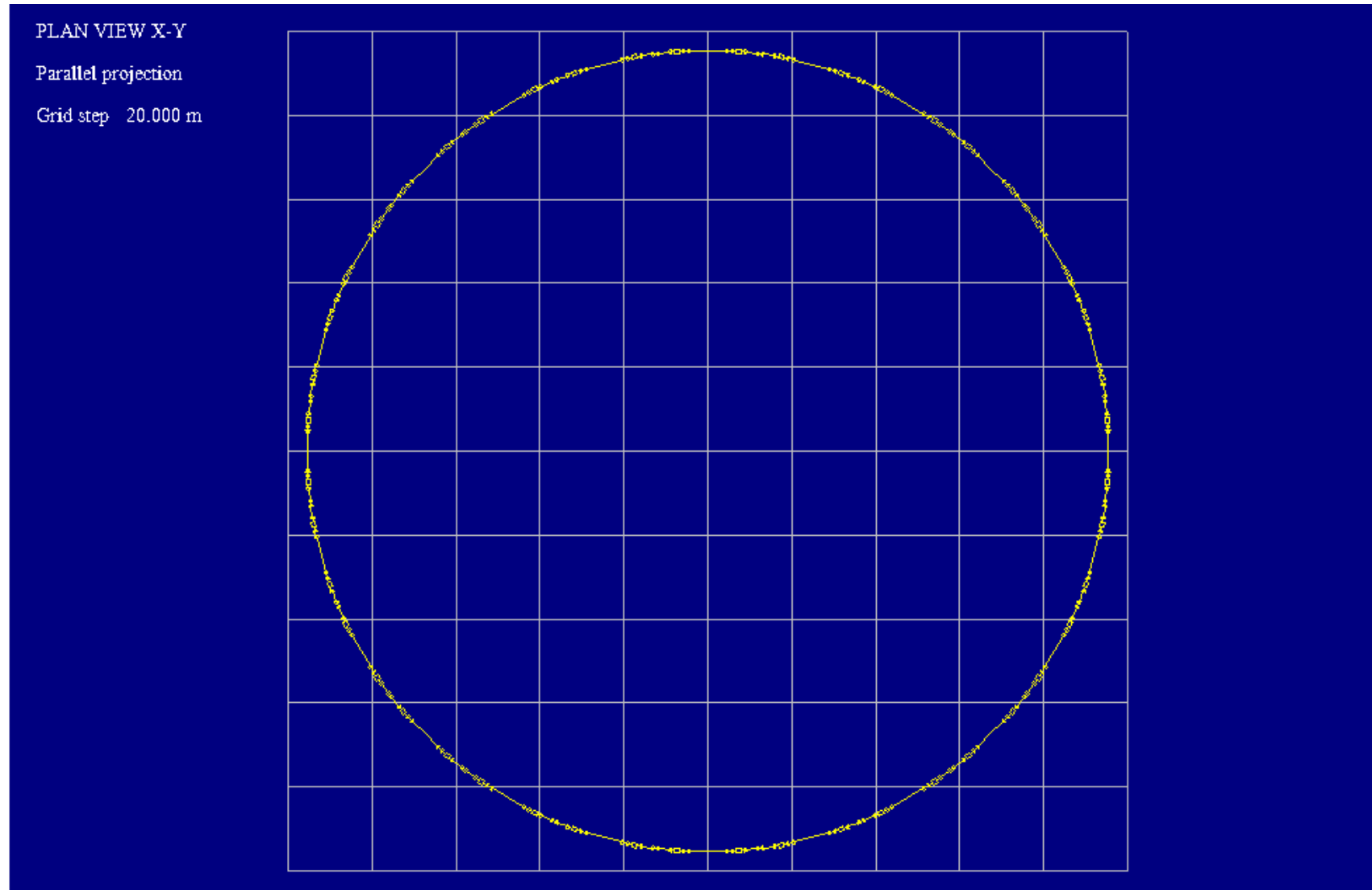
-> Ramp down within 50ns



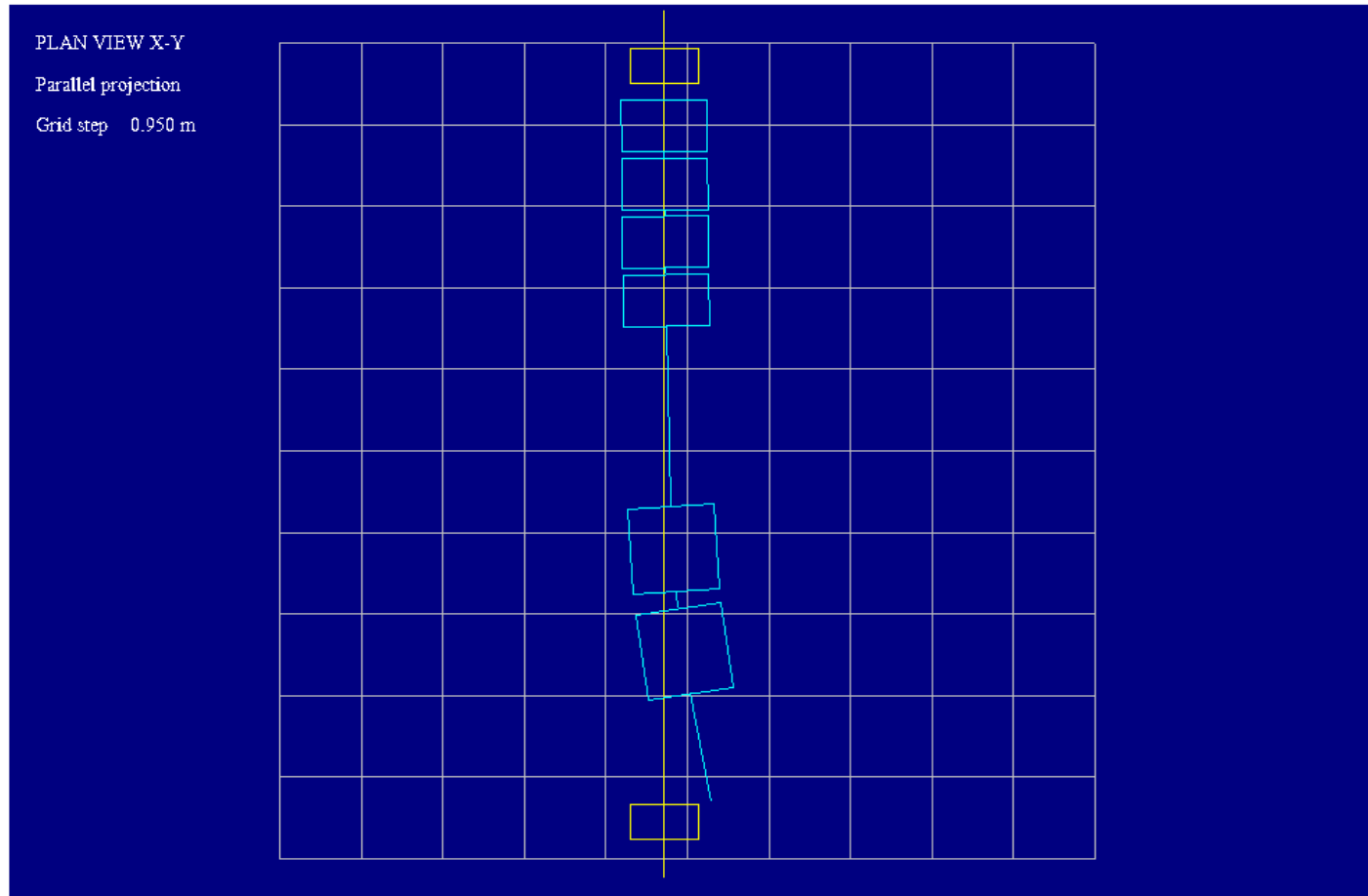
Extraction Process

- Ramp up extraction kicker within 50ns in the gap
- Complete extraction in one turn
- Dumping in a secure structure (steel)

Injection & Extraction – Basic Design



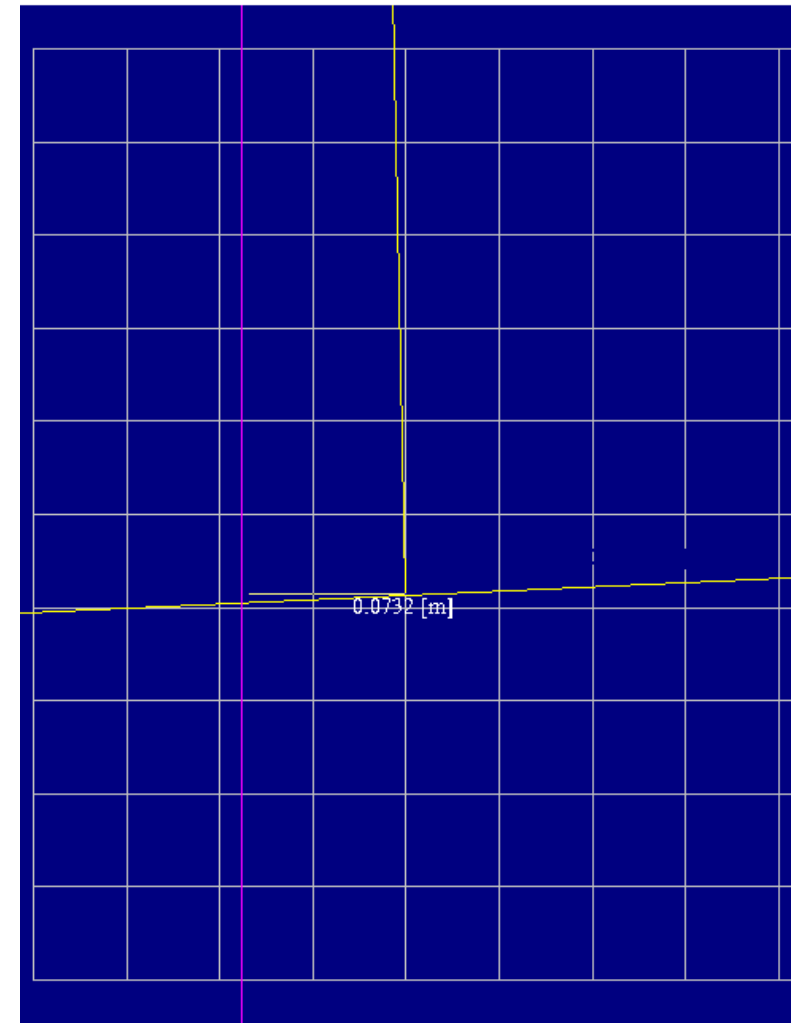
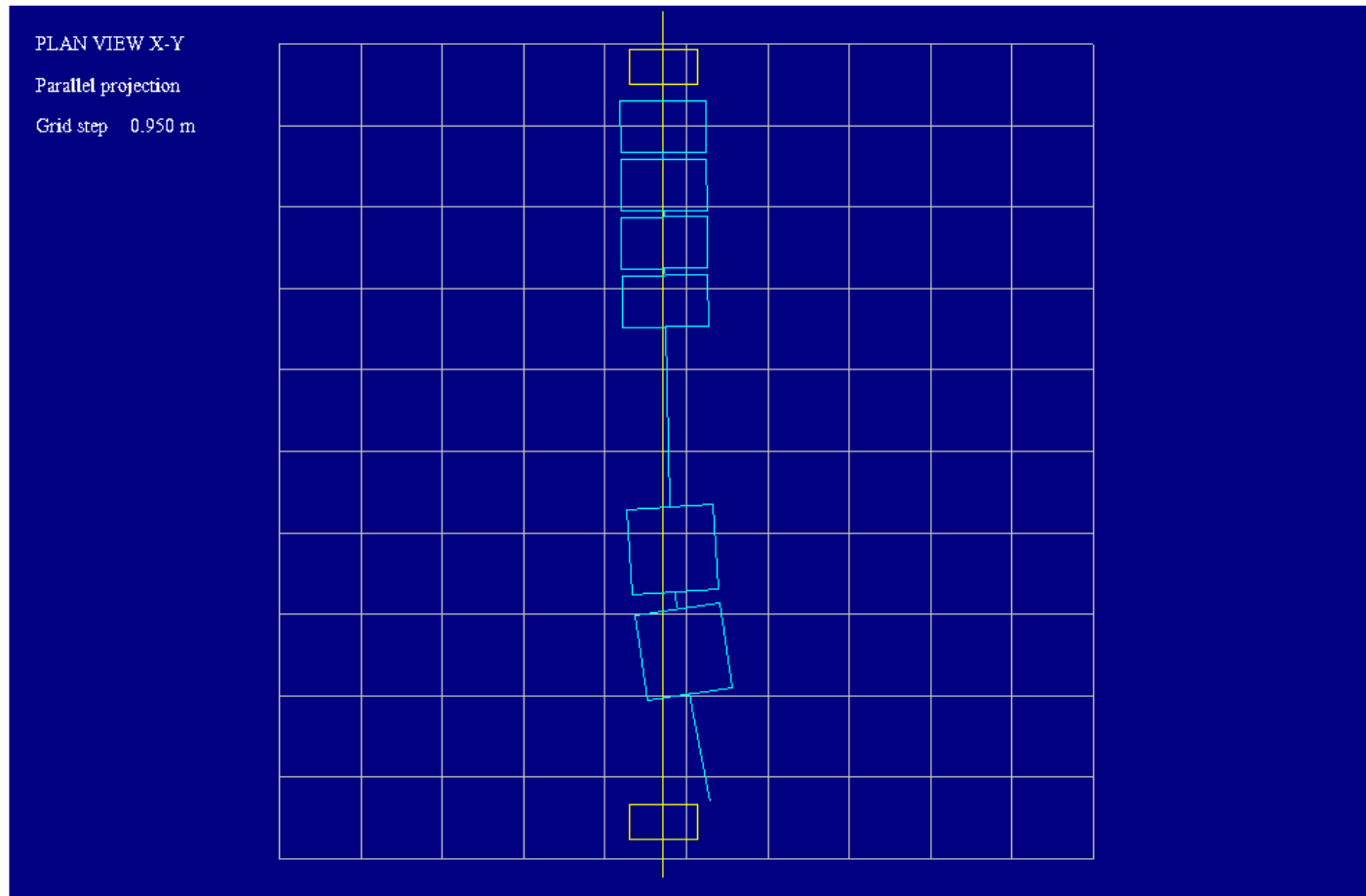
Injection – Basic Design



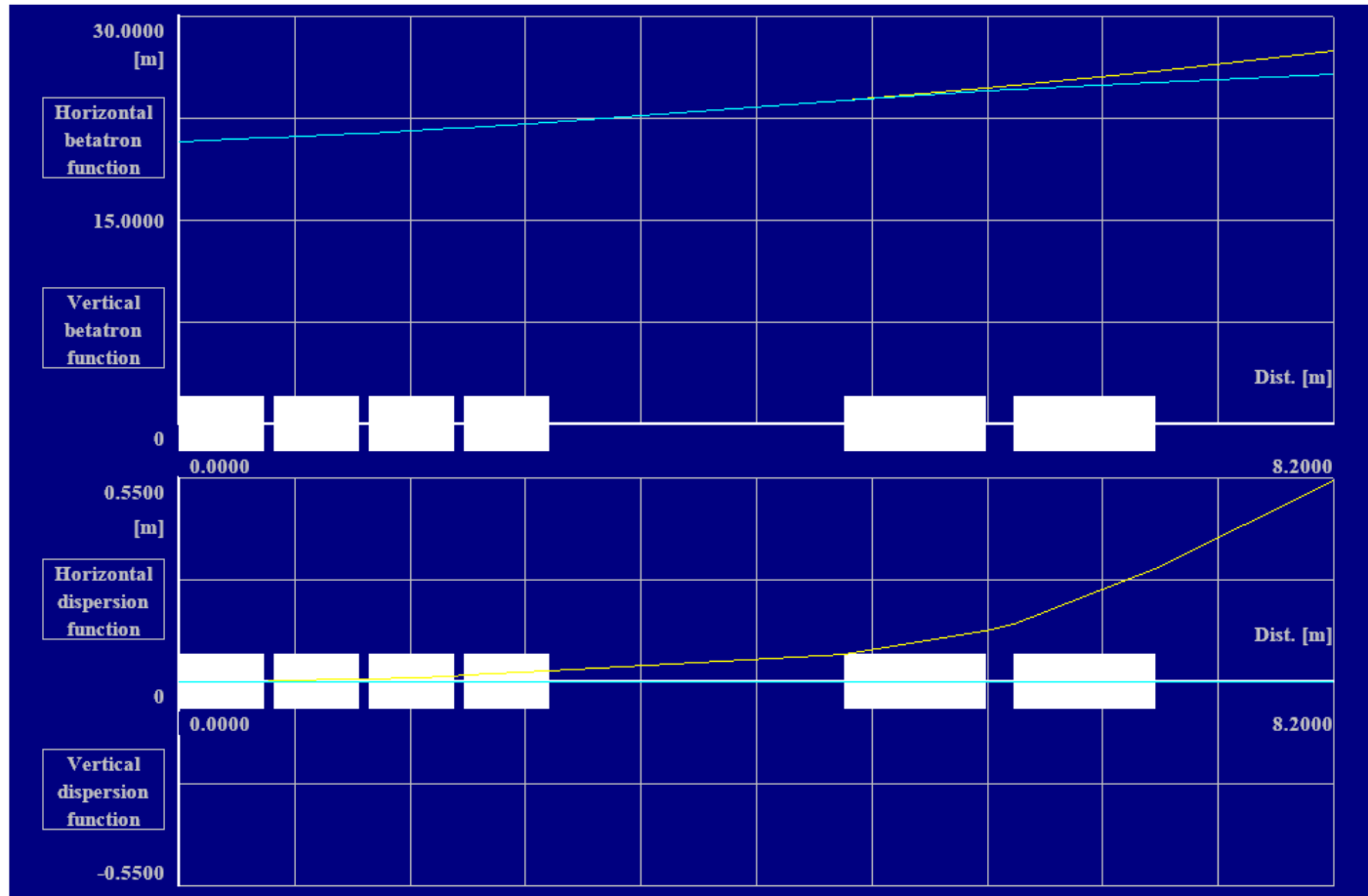
Parameters

- Particles at 2 GeV, 8.2 meters long.
- 2 septa at $B = 0.55$ T.
- 4 kickers at 0.06 T $\rightarrow \theta = 5.4$ mrad.
- Large space margin at the second septum exit (7.32 cm).
- Matching parameters at insertion point.
 - $\beta_x = \beta_z = 20.8\text{m}$; $\alpha_x = \alpha_z = -0.2$
 - $\epsilon_x = \epsilon_z = 0.1500$ pi.mm.mrad

Injection – Basic Design



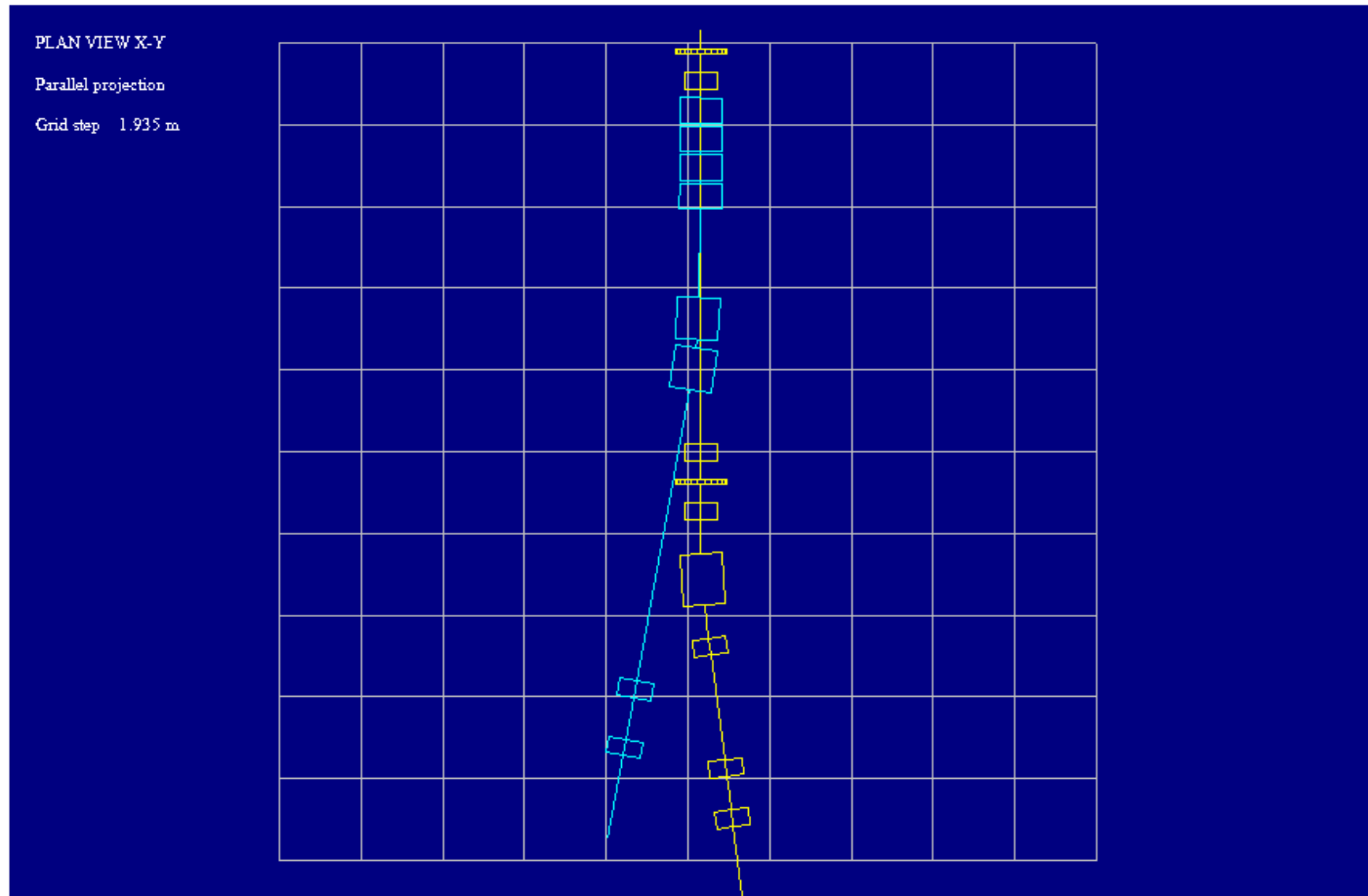
Injection – Basic Design



Main functions in the line

- Required conditions are matched.
- Prior to injection line, there will be :
 - 1 RF cavity
 - 6 quadrupoles ($\beta_x, \beta_z, \alpha_x, \alpha_z, D_x, D_z$)
- Functions don't get out of hand :
 - Dispersion is ok since we're out of an RF
 - Beta function will be easy to match
- No need for more elements. Keep cost as low as possible.

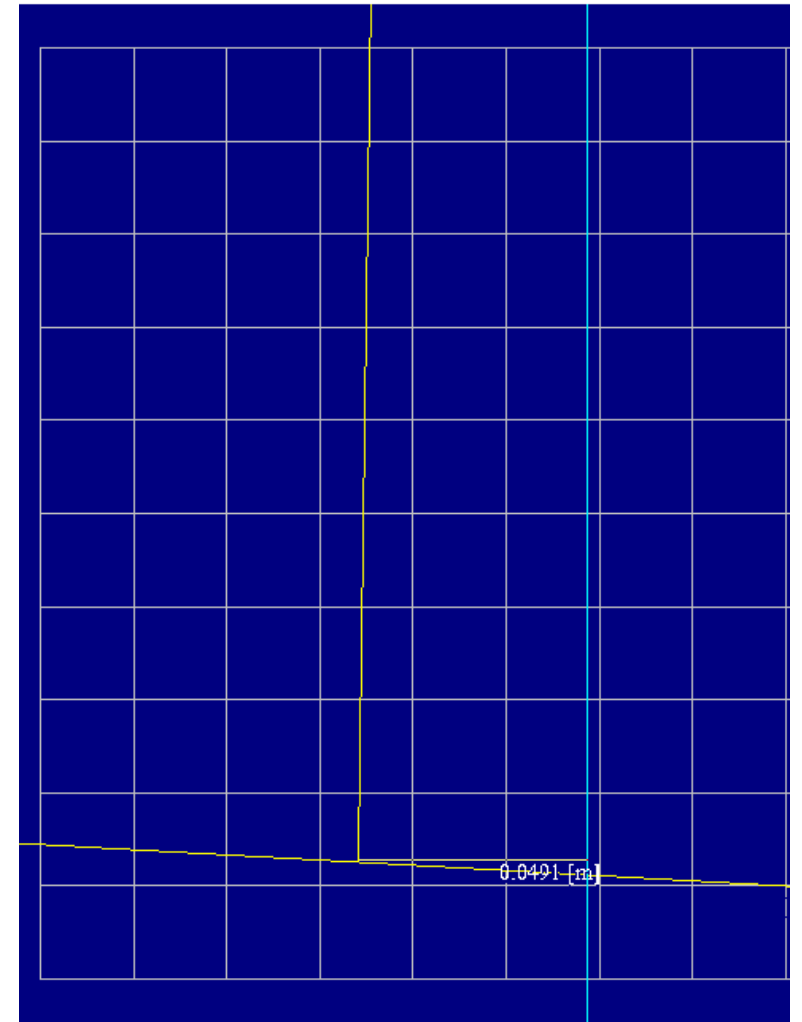
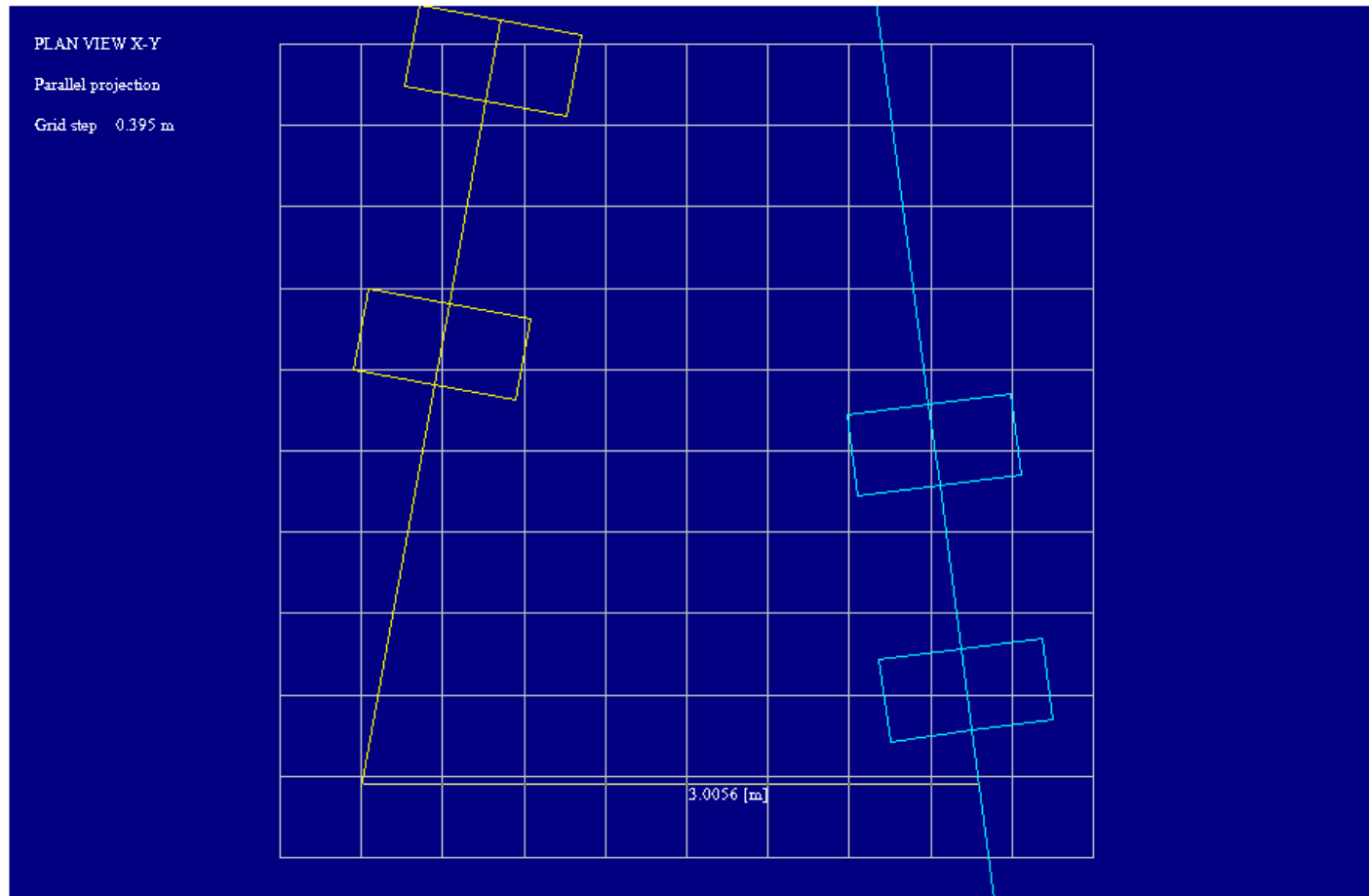
Extraction & Dump – Basic Design



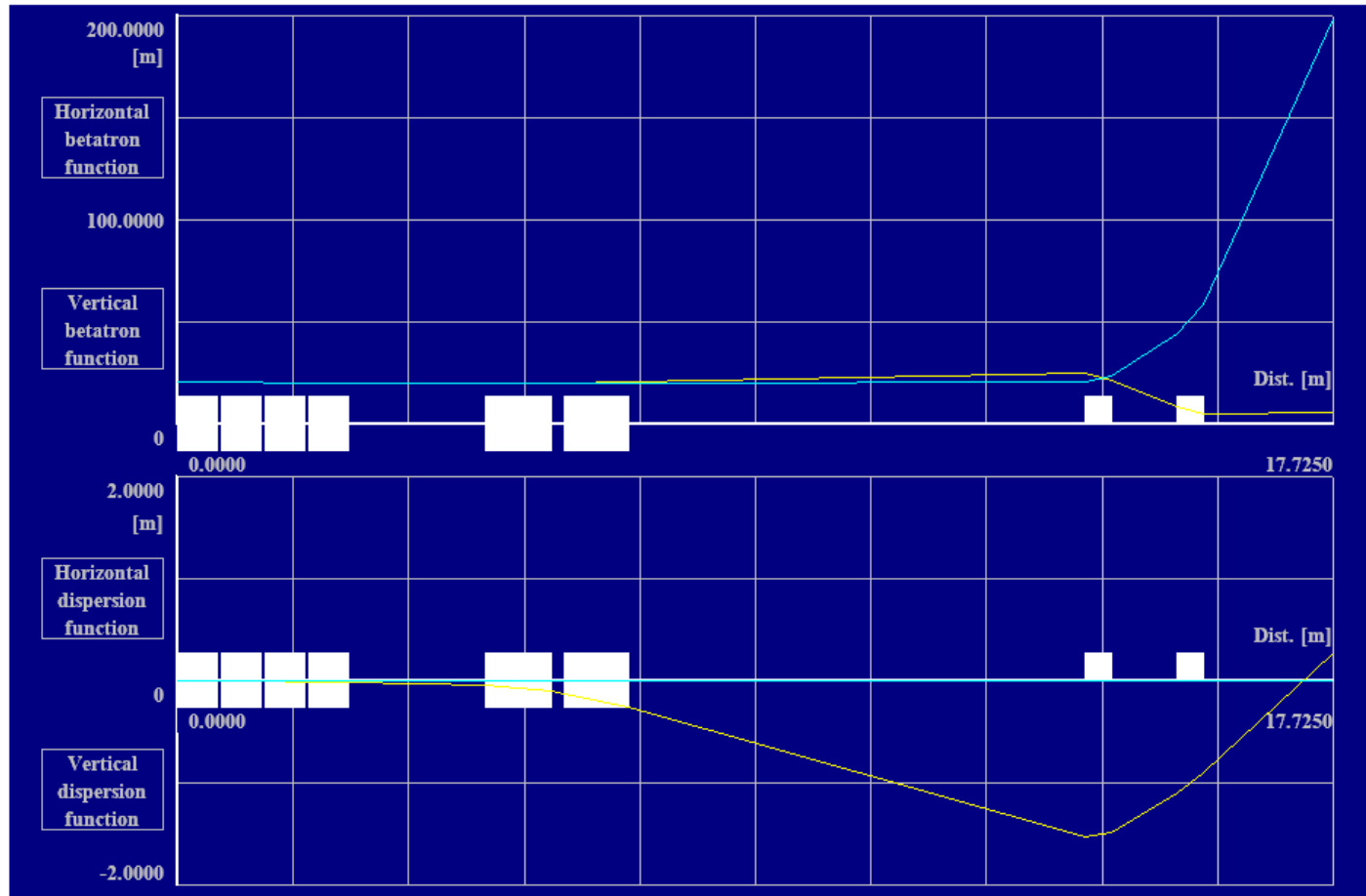
Parameters

- Particles at 3 GeV, 17.725 meters long.
- 2 septa at $B = 0.83$ T
- 4 kickers at 0.06 T $\rightarrow \theta = 3.6$ mrad
- 2 defocusing quads spread the beam for dumping.
- Minimal space margin at the first septum entrance (4.91 cm).
- Dump structure is 3 meters away from ring.
- Matching parameters at insertion point
 - $\beta_x = \beta_z = 20.8$ m; $\alpha_x = \alpha_z = 0.2$
 - $\epsilon_x = \epsilon_z = 0.1500$ pi.mm.mrad

Extraction & Dump – Basic Design



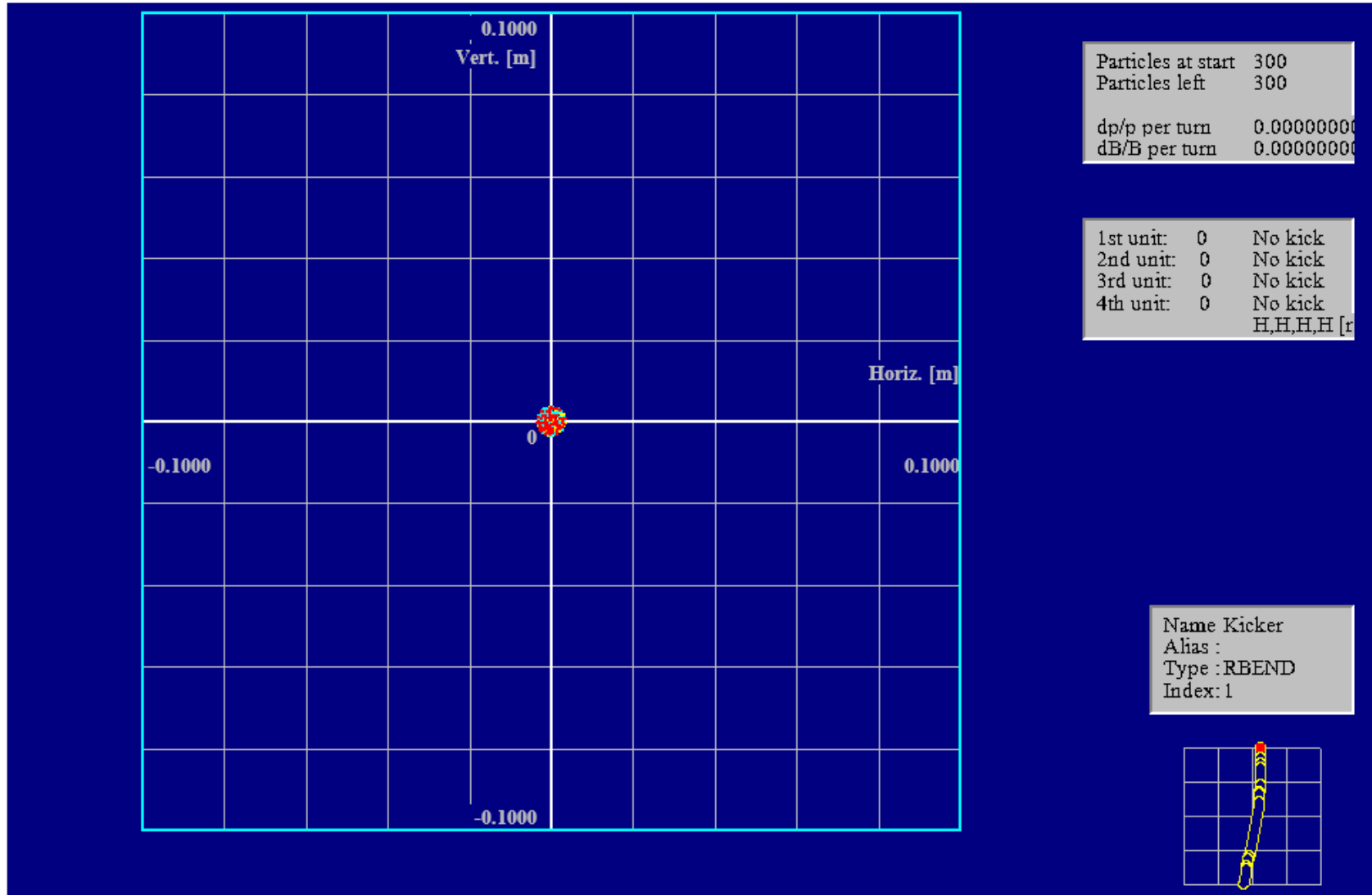
Extraction & Dump – Basic Design



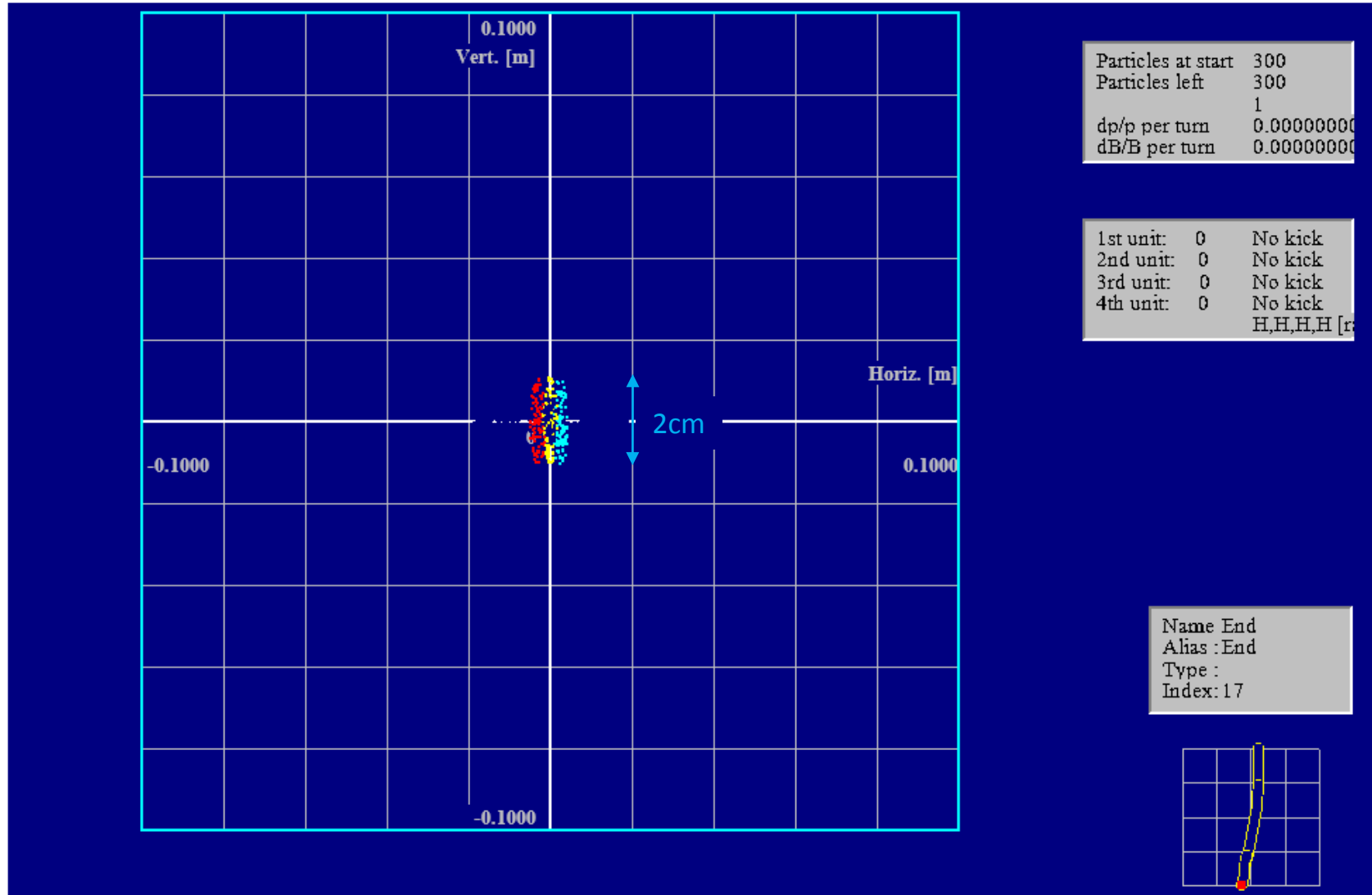
Main functions in the line

- Required conditions are matched.
- The quadrupoles are the same as the ring's ones :
 - Reduces cost and assembly complexity.
 - Can be plugged in series and left passive (no powering problem).
- Functions have a satisfying behavior :
 - Dispersion does not matter that much.
 - One very high beta is enough for dumping.

Extraction & Dump – Basic Design



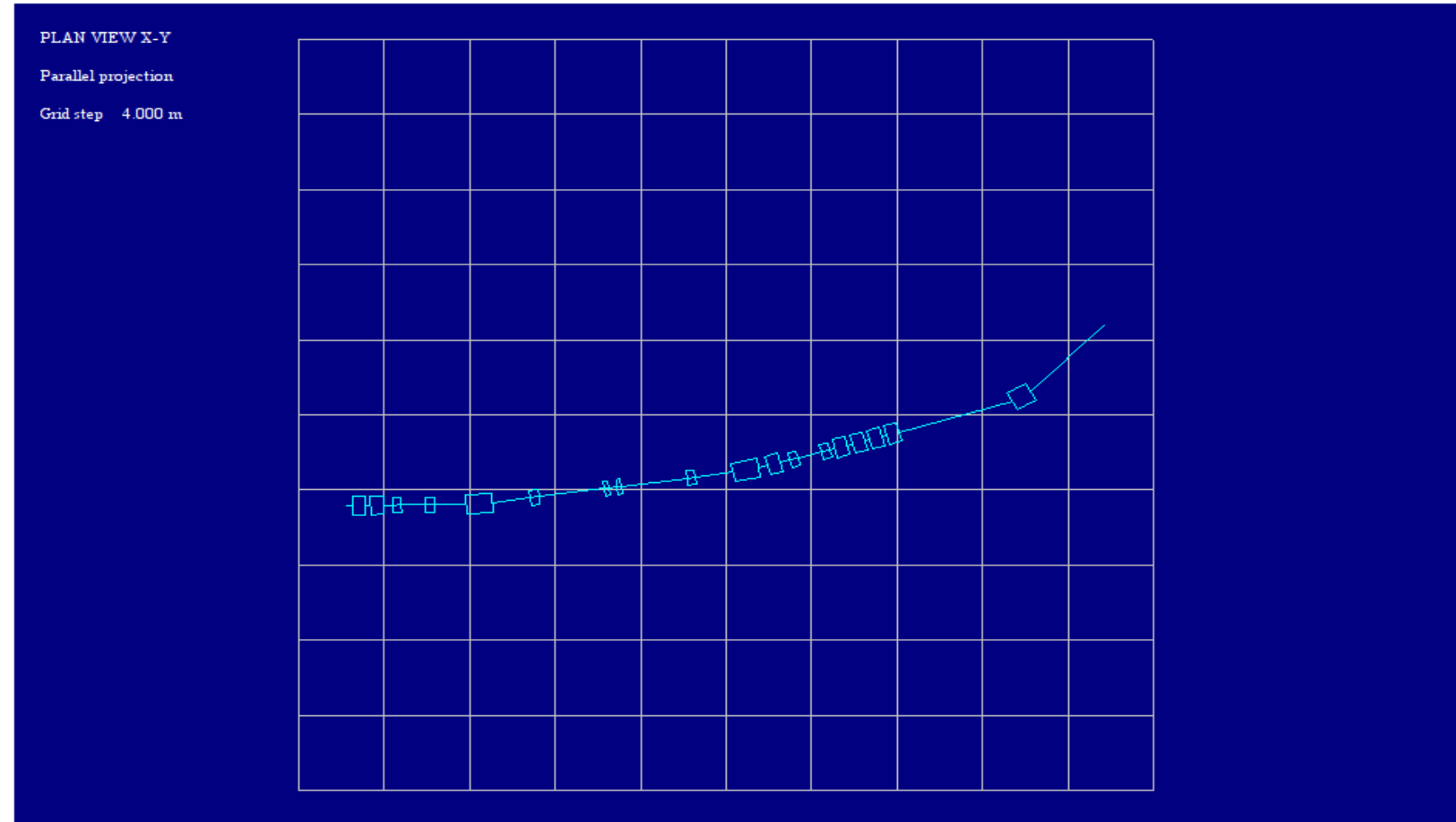
Extraction & Dump – Basic Design



Extraction Process

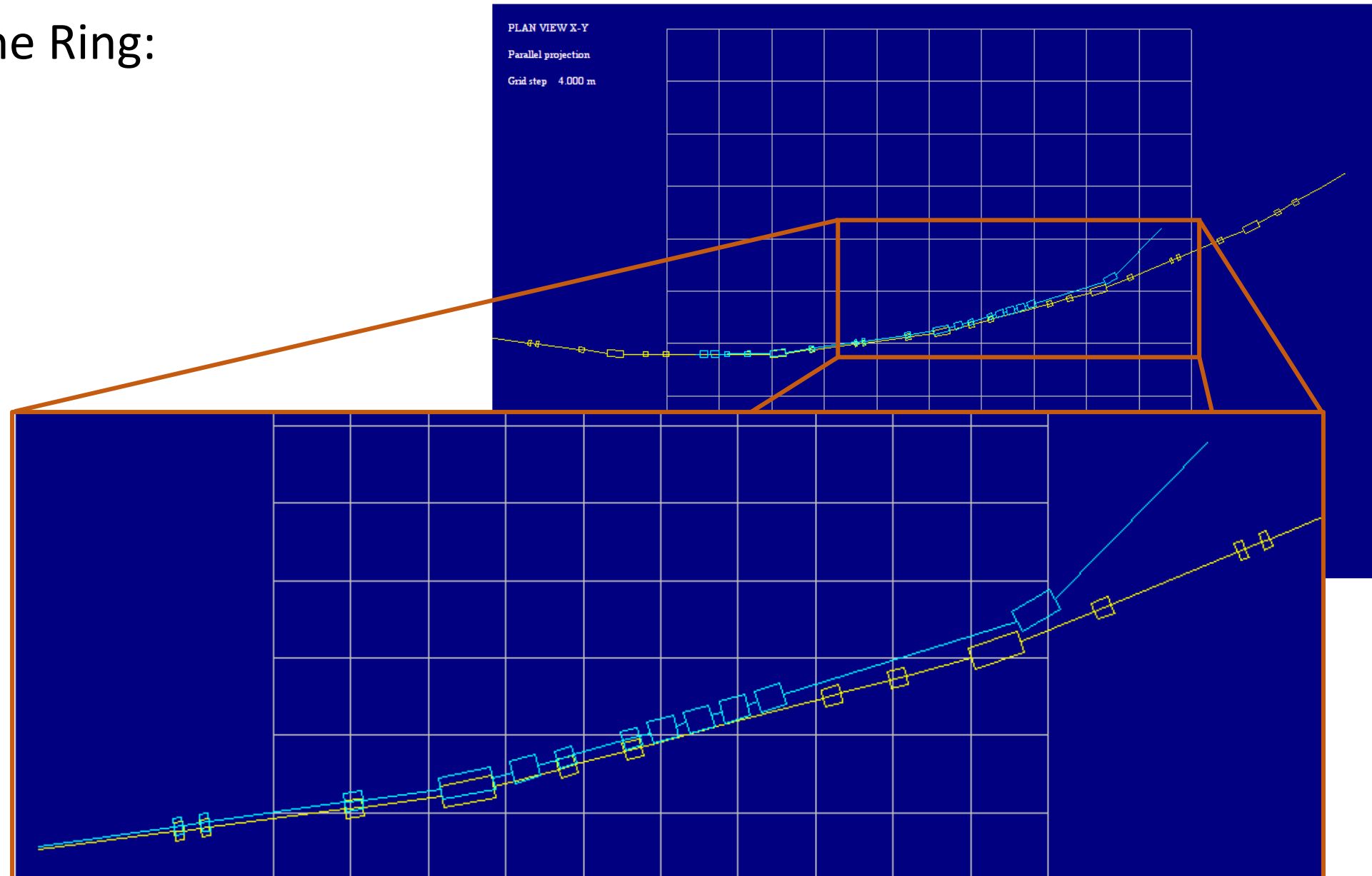
- Ramp up extraction kicker within 50ns in the gap
- Complete extraction in one turn

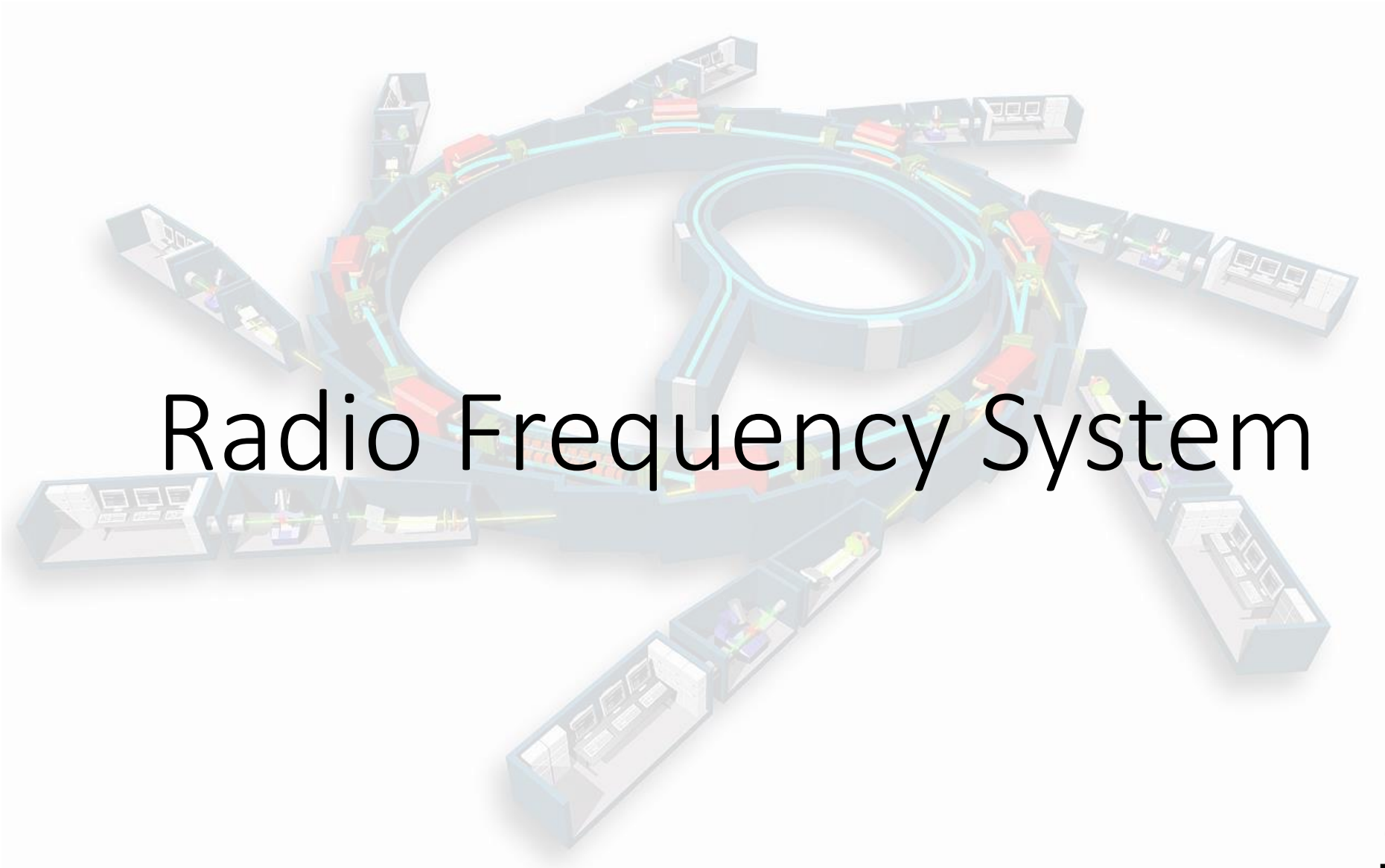
Extraction Line:



Extraction Process

Extraction Line Ring:





Radio Frequency System

Vittorio Bencini
Anna Pugelise
Marco Diomede
Gabriel Tutturcia
Mostafa Behtoei
Thomas Coldfix

Requirements and design parameters

- Requirements
- Compensate losses due to synchrotron radiation
 - Provide constant acceleration to the electrons to follow up the magnets ramp

Design parameter	Value
C ring [m]	600
R [m]	95.49
ρ [m]	9.17
σ_z bunch [m]	0.012
σ_e bunch [m]	0.001
$E_{injection}$ [GeV]	2
E_{final} [GeV]	3

RF modulation

In order to compute the V_{RF} needed to compensate the losses and accelerate the particle we have to consider

$$\frac{dB}{dt} = const \quad \longrightarrow \quad \Delta E_{ACC,turn} = \frac{dB}{dt} \times 2\pi R\rho = 1.084KeV$$

So, taking into account the losses due to synchrotron radiation, it becomes

$$\Delta E_{RF,turn} = \Delta E_{ACC,turn} + \Delta E_{L,turn}$$

$$\Delta E_{L,turn}[KeV] = 88.46 \times \frac{E[GeV]^4}{\rho}$$

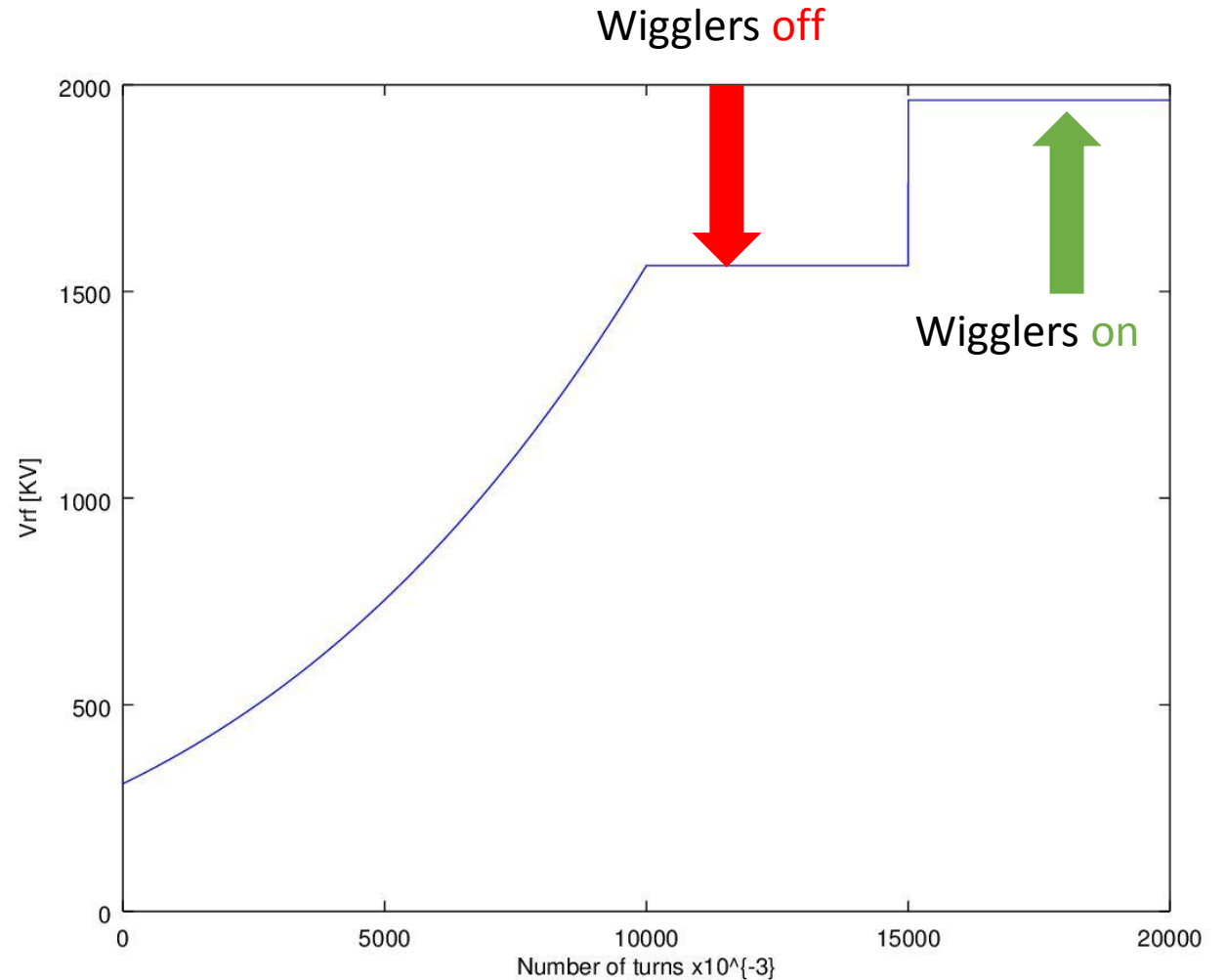
RF modulation

The energy gain is followed by modulating V_{RF} \longrightarrow $\sin\varphi_s = 30^\circ = \text{const}$

$$V_{RF,2\text{ GeV}} = 308.7\text{ KV}$$

$$V_{RF,3\text{ GeV}} = 1562.8\text{ KV}$$

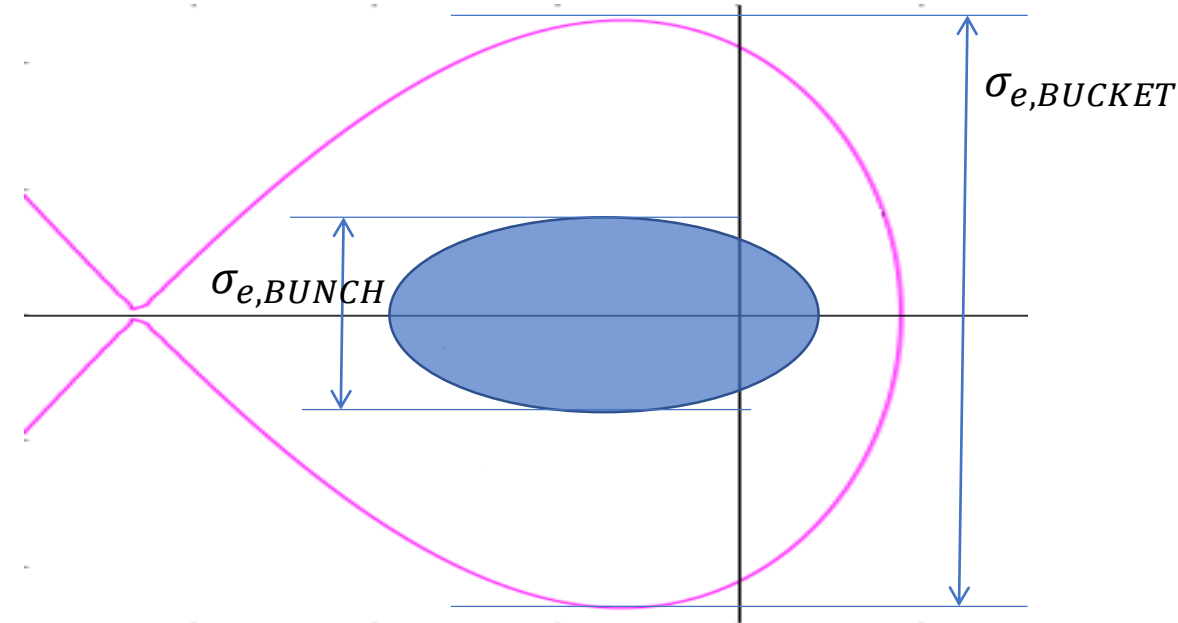
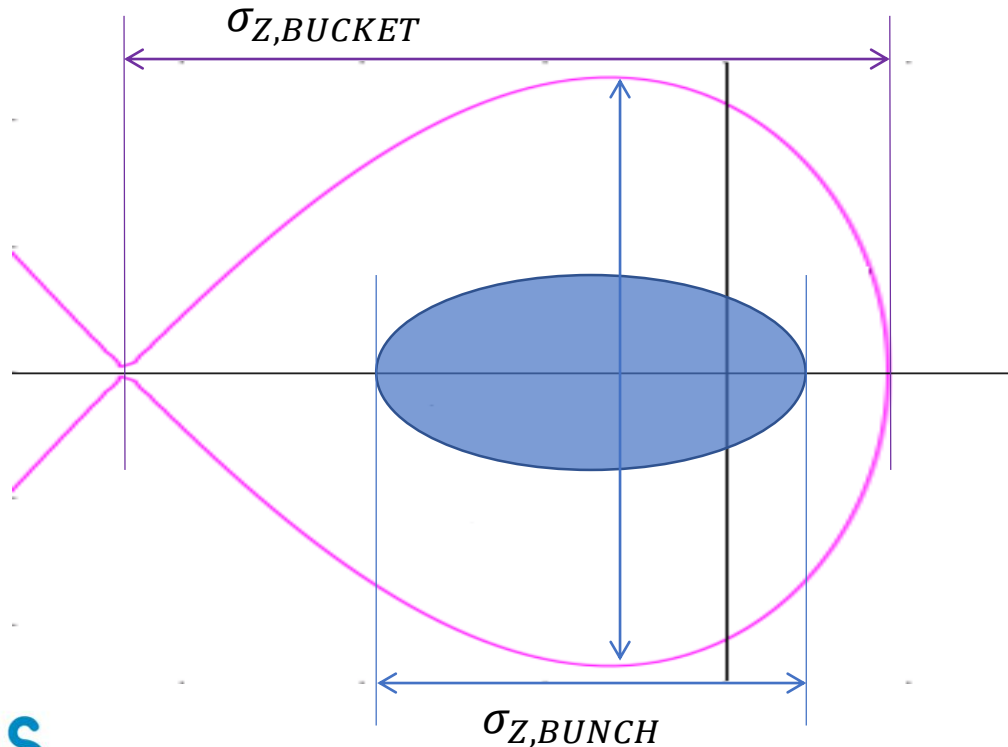
$$V_{RF,3\text{ GeV},W} = 1962.8\text{ KV}$$



Matching at injection

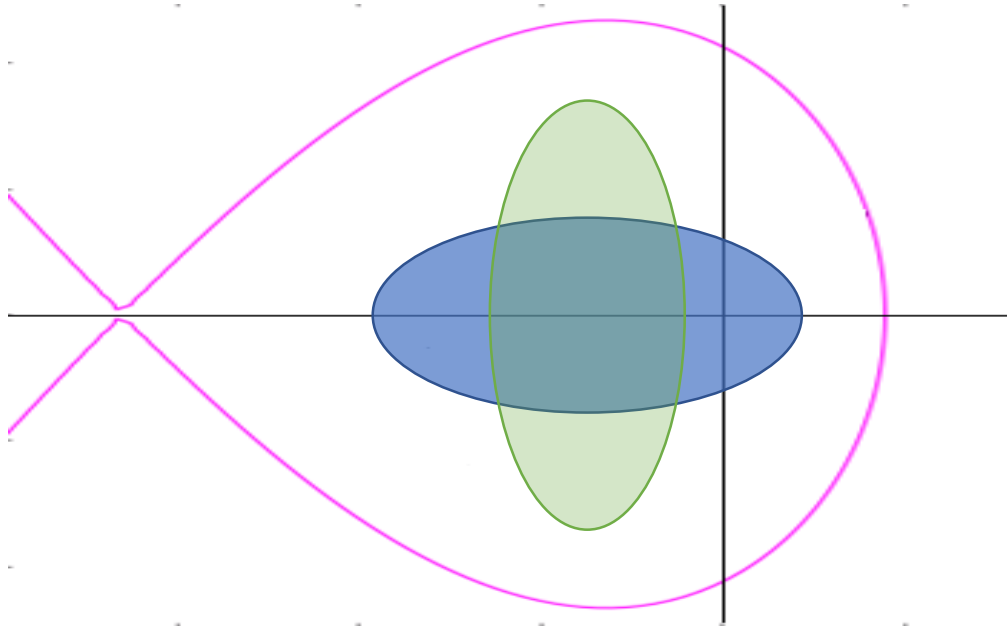
The matching condition is respected if the ratio between the axis of the bunch ellipse is similar to those of the bucket.

$$\left| \frac{\sigma_z}{\sigma_\varepsilon} \right|_{bunch} \approx \left| \frac{\sigma_z}{\sigma_\varepsilon} \right|_{bucket}$$



Matching at injection

Another condition is that, in case the first is not respected, the rotated ellipse still completely fits into the bucket



$$\left| \frac{\sigma_z}{\sigma_\varepsilon} \right|_{bunch} = 12$$

$$\left| \frac{\sigma_z}{\sigma_\varepsilon} \right|_{bucket} = 14$$



OK!

RF cavity design

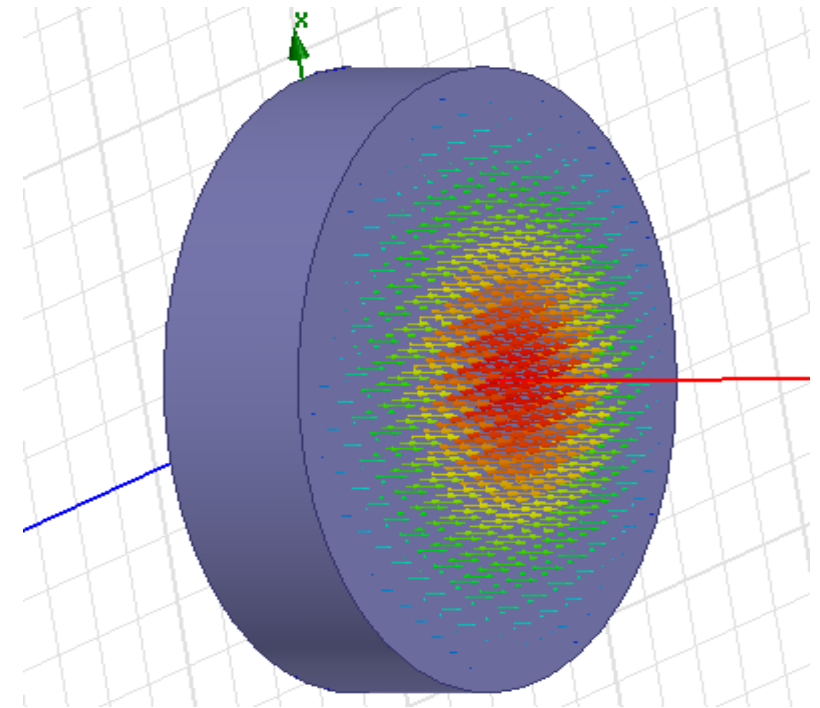
Cavity parameter	Value
$V_{RF,peak}$ [KV]	750 KV
φ_s (above transition) [deg]	150
Gap [mm]	100
R_0 [M Ω]	3.5
f_{res} [MHz]	500

Using HFSS and CST simulation it was possible to confirm the radius and to compute the shunt impedance of the cavity

$$R = 23.08 \text{ cm}$$

From EM theory we know that the relationship between radius and frequency in TM_{01} mode is given by

$$R = \frac{2.405}{f_{res}} = 22.95 \text{ cm}$$



RF power and cooling

At 3 GeV (wigglers on) the cavities have to be powered with

$$P = \frac{(V_{RF})^2}{R_0} = 1.1 \text{ MW}$$

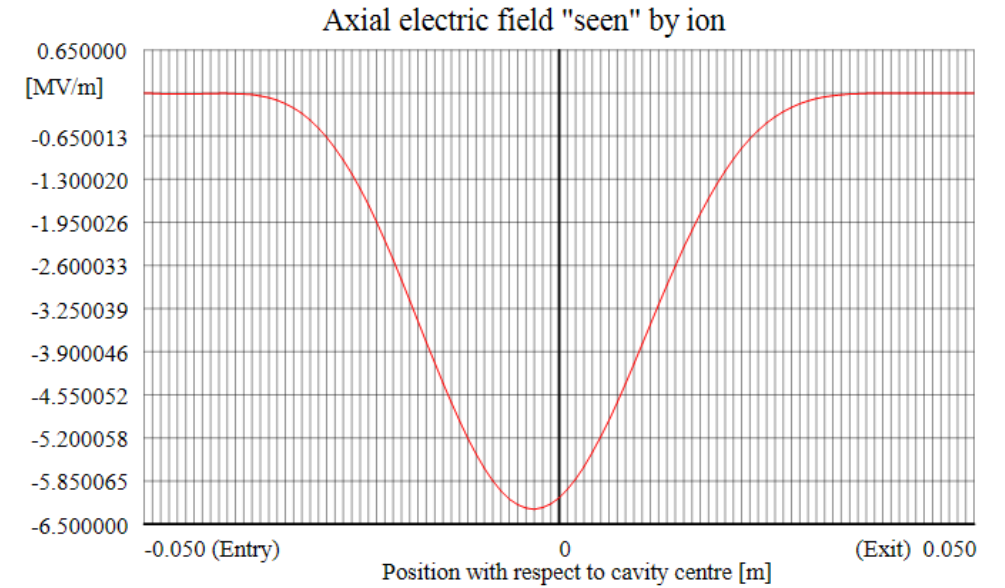
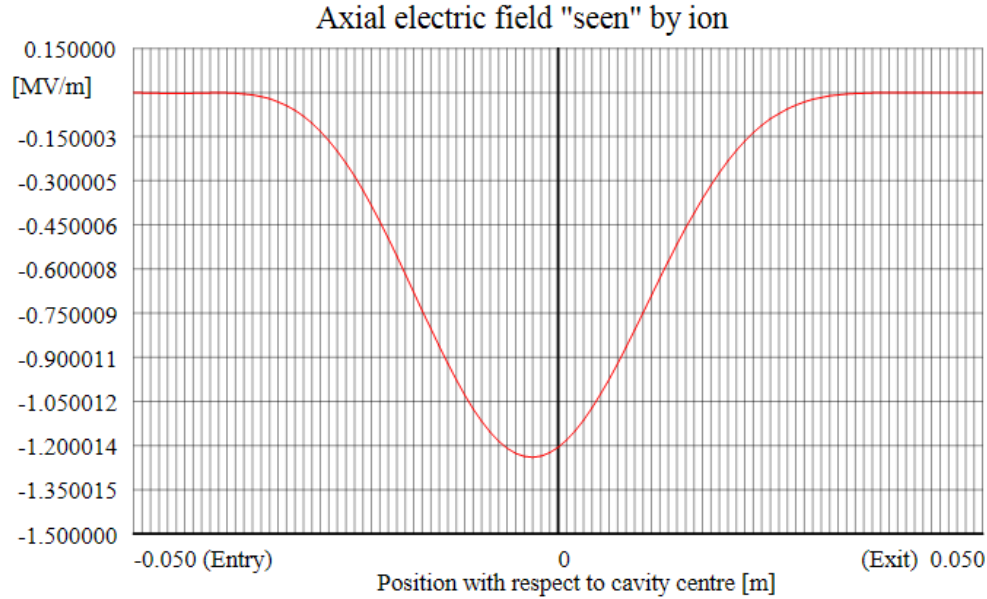
The efficiency between klystron and cavity is usually in the order of $\varepsilon = 0.85$

$$P_{tot} = P \times (2 - \varepsilon) = 1.27 \text{ MW}$$

Cooling:

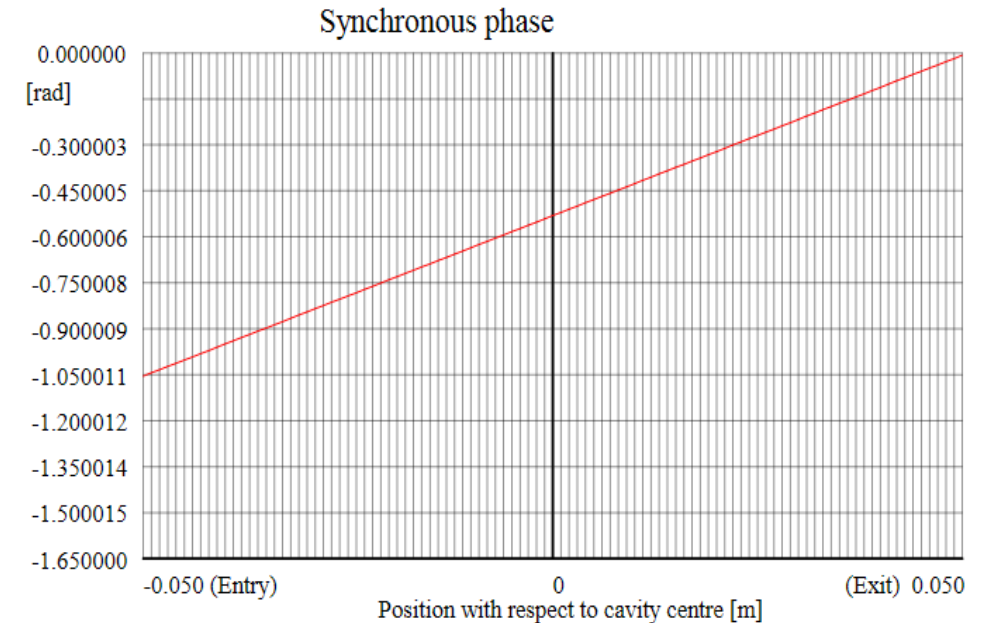
- The power dissipated in the cavity walls induce a ΔT that could affect the performances of the cavities (resonance frequency shift, mechanical stress)
- Colling system is needed

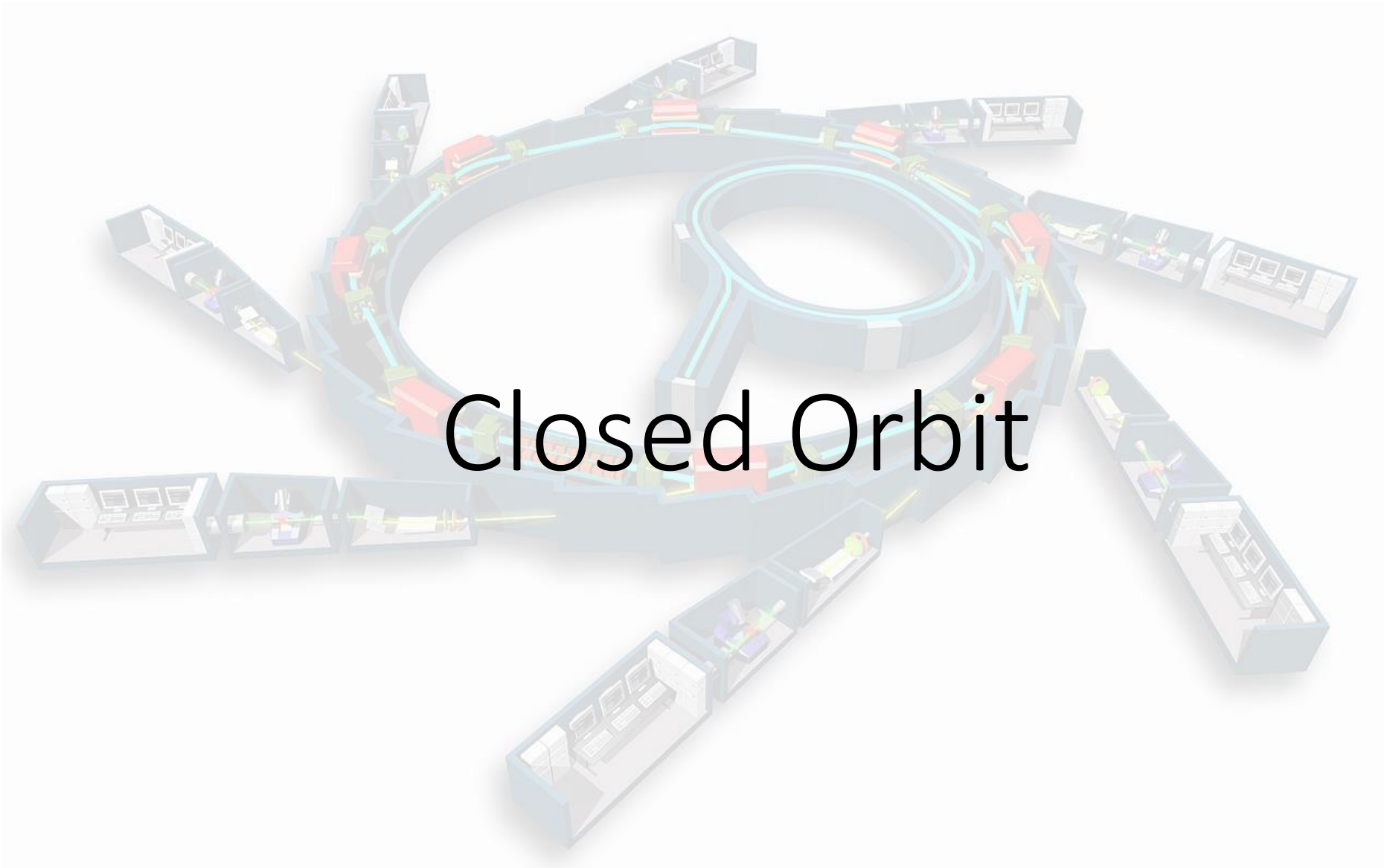
WinAGILE results



Putting the computed V_{RF} values at 2 and 3 GeV (wigglers off) we can see that

- The phase at the center of the cavity is exactly 150 deg (in the figure different reference system and negative phase)
- The E field has different amplitudes but the right shape





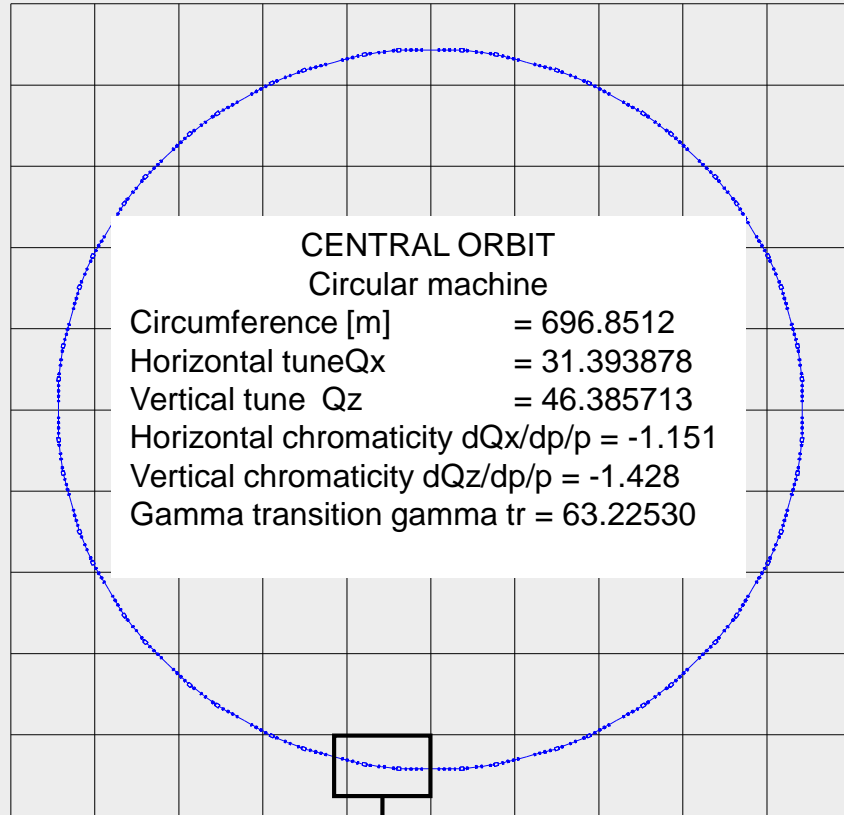
Closed Orbit

Andrii Natochii
Mirza Sajjad Hussain

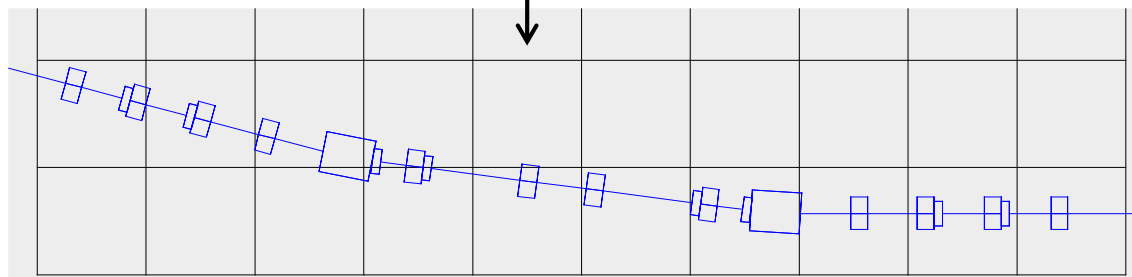
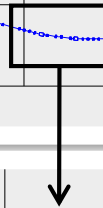
Closed Orbit

“Optimized ring SEXTU.lat” 3 GeV electrons

Horizontal plan view [X-Y plane]



Grid size 25.0000 [m]

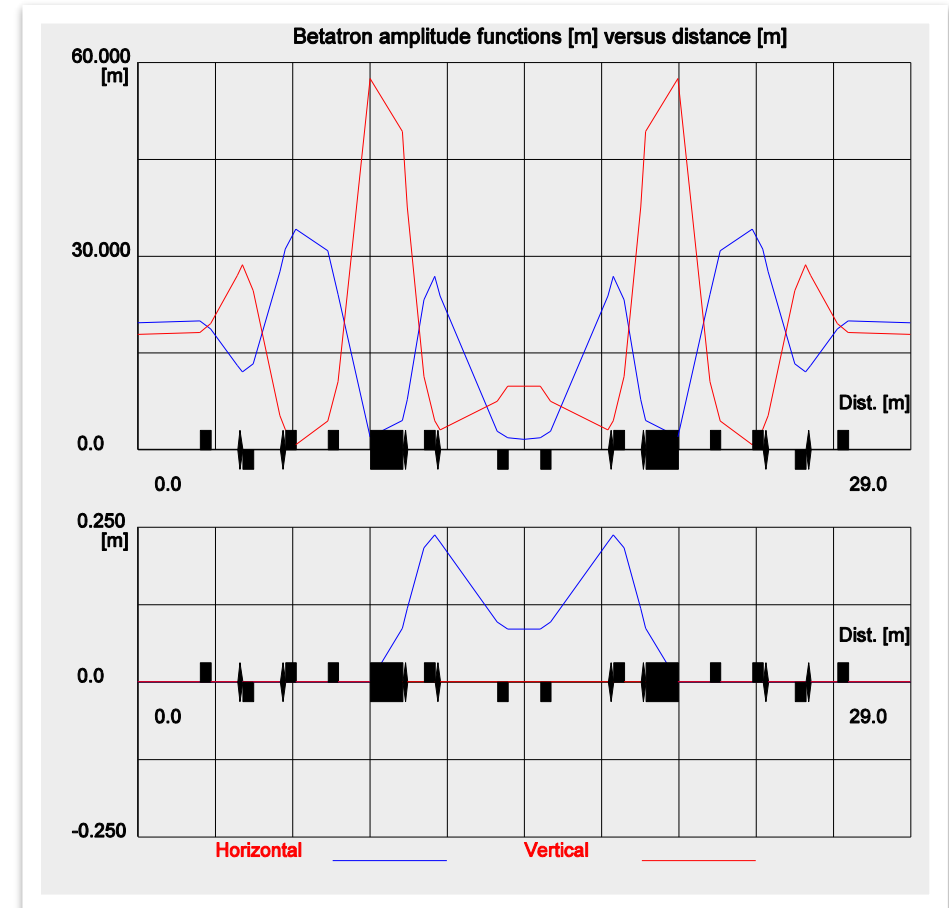


Grid size 2.6108 [m]

Closed-orbit correction is a compromise. The orbit is measured at only a finite number of positions and there is only a finite number of correctors.

Our goals:

- Generate errors inside the machine
- Choose correctors and monitors
- Try to correct the orbit of the particle in closed orbit case



Machine errors

Random generated errors:

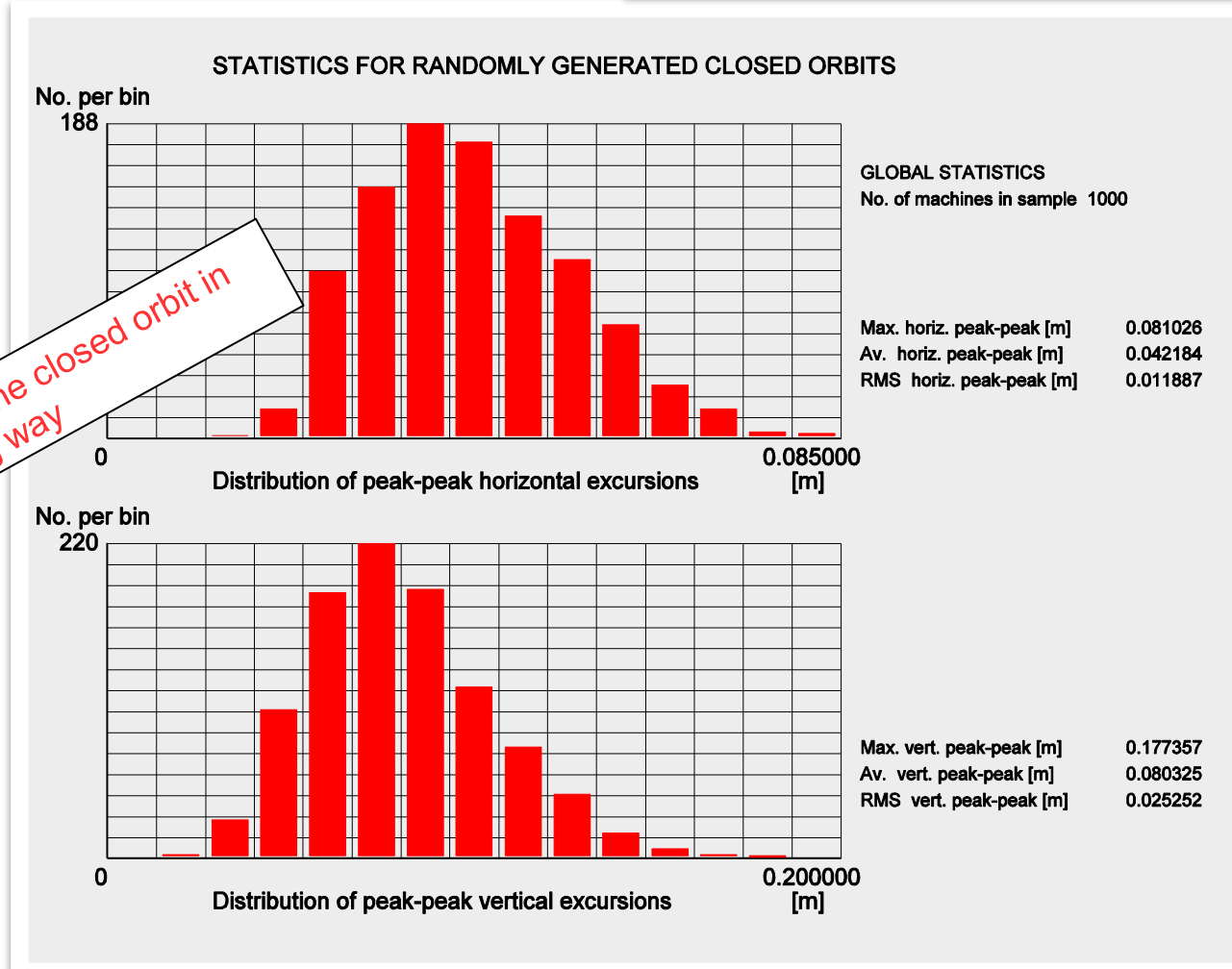
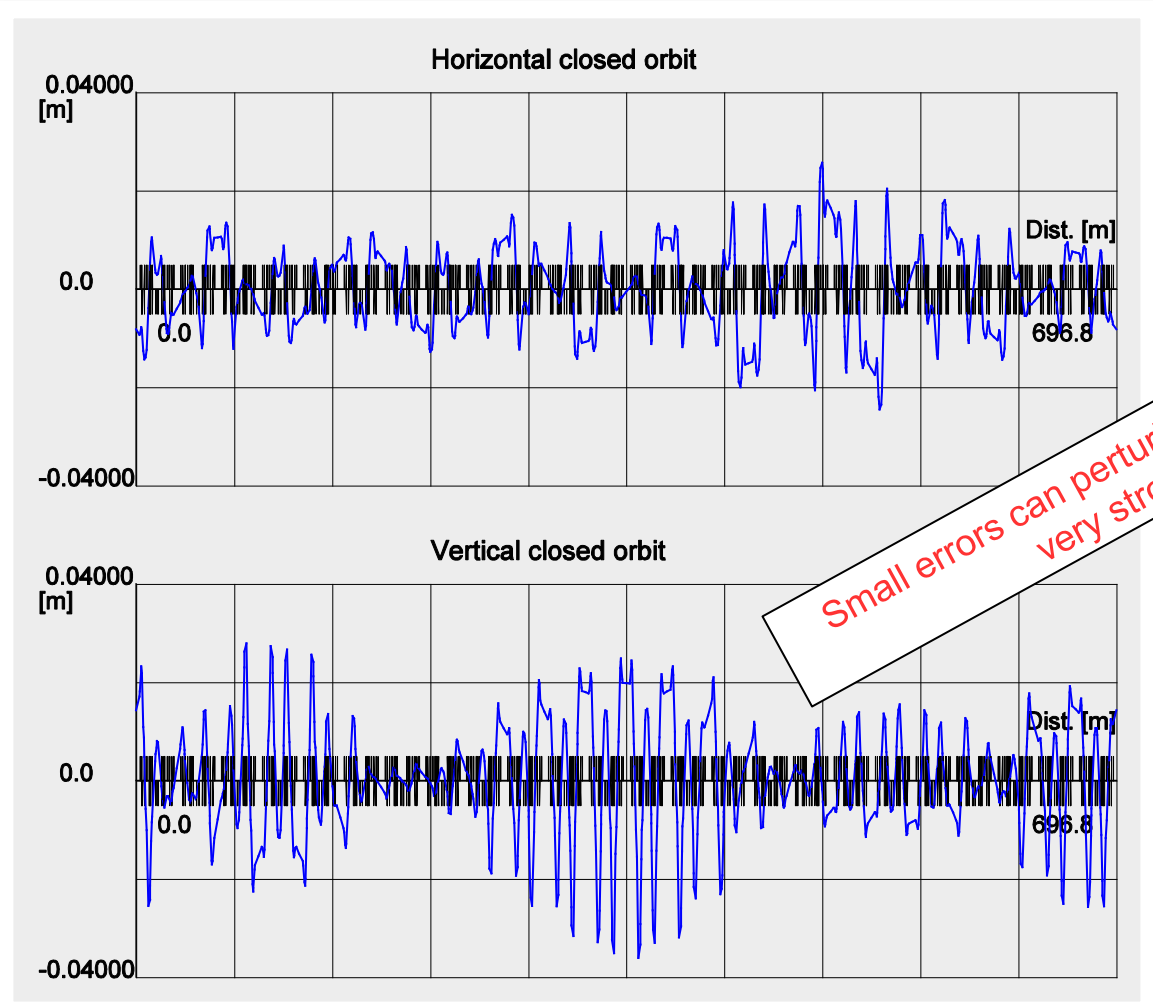
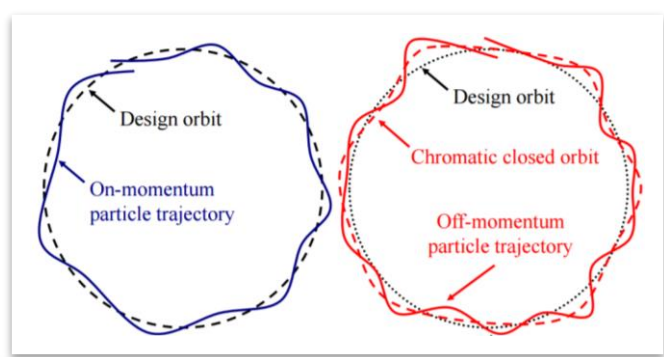
Distribution: Truncated gaussian (4.5 sigmas)

Axial shift of all dipoles [m] = 0.001

Tilts of all dipoles [rad] = 0.001

Trans. shifts of all quads. [m] = 0.0001 (H&V)

No. of machines in sample: 1000



Small errors can perturb the closed orbit in very strong way

Correctors/Monitors of the orbit

# corr	Pk-Pk [m]	Mean [m]	RMS [m]
0	0.050201	-0.000036	0.008351
1	0.034230	-0.000152	0.004511
2	0.033369	-0.000166	0.004433
3	0.028876	-0.000184	0.004055
4	0.028863	-0.000171	0.004047
5	0.028869	-0.000167	0.004047
6	0.028859	-0.000170	0.004046
7	0.028921	-0.000181	0.004043
8	0.028974	-0.000189	0.004041
9	0.028984	-0.000192	0.004041
10	0.028978	-0.000191	0.004041
11	0.028899	-0.000179	0.004033
12	0.028816	-0.000165	0.004022
13	0.028557	-0.000141	0.003991
14	0.028347	-0.000119	0.003973
15	0.028218	-0.000142	0.003957
16	0.028200	-0.000149	0.003954
17	0.028180	-0.000158	0.003946
18	0.028099	-0.000205	0.003905
19	0.027895	-0.000171	0.003852
20	0.027693	-0.000134	0.003791
21	0.027624	-0.000110	0.003765
22	0.027534	-0.000082	0.003730
23	0.027509	-0.000054	0.003701
24	0.027508	-0.000032	0.003681

Initial values



# corr	Pk-Pk [m]	Mean [m]	RMS [m]
0	0.064047	0.000189	0.011008
1	0.049571	0.000310	0.007059
2	0.051840	0.000321	0.007338
3	0.035442	0.000233	0.005486
4	0.035533	0.000224	0.005491
5	0.035597	0.000217	0.005496
6	0.035700	0.000238	0.005494
7	0.035736	0.000246	0.005496
8	0.035774	0.000242	0.005499
9	0.036114	0.000229	0.005523
10	0.036367	0.000220	0.005540
11	0.036565	0.000210	0.005552
12	0.036796	0.000198	0.005567
13	0.036798	0.000197	0.005567
14	0.036939	0.000215	0.005569
15	0.036990	0.000228	0.005570
16	0.037156	0.000219	0.005581
17	0.037299	0.000212	0.005590
18	0.037522	0.000236	0.005593
19	0.037600	0.000244	0.005597
20	0.037681	0.000239	0.005601
21	0.038402	0.000224	0.005643
22	0.038853	0.000214	0.005671
23	0.039191	0.000205	0.005693
24	0.039577	0.000195	0.005720

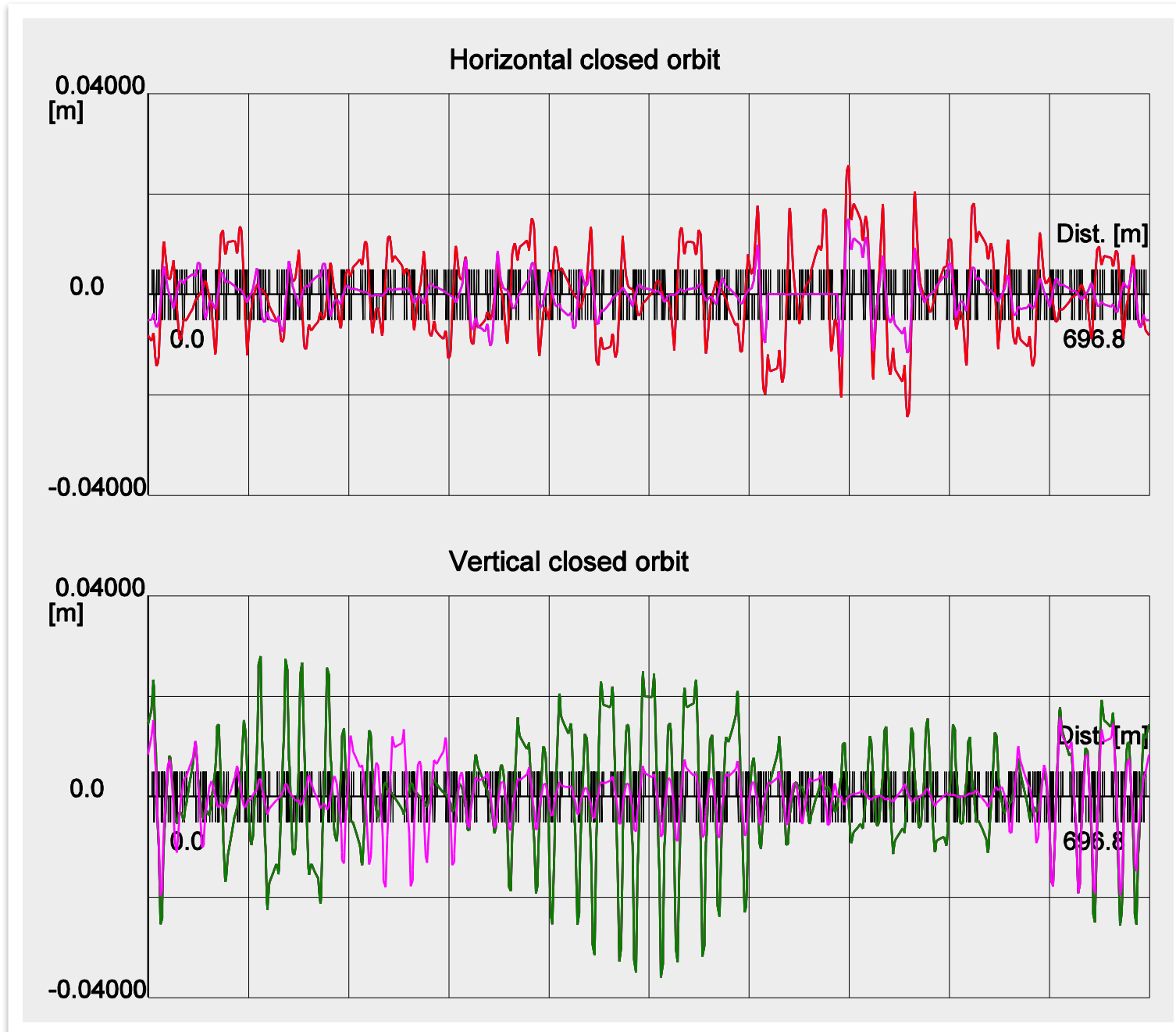


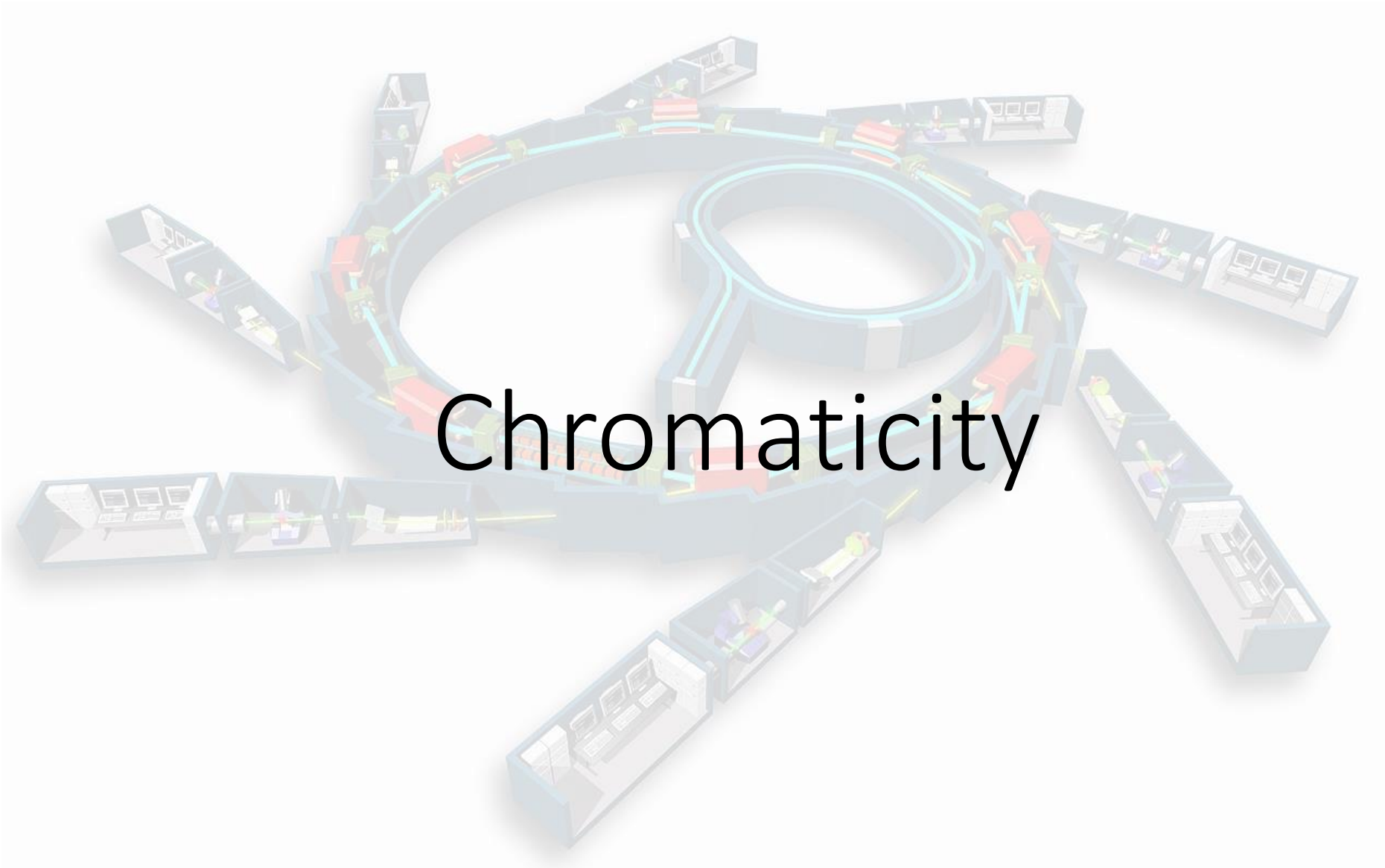
Horizontal plane

Vertical plane



Closed orbit (corrected)





Chromaticity

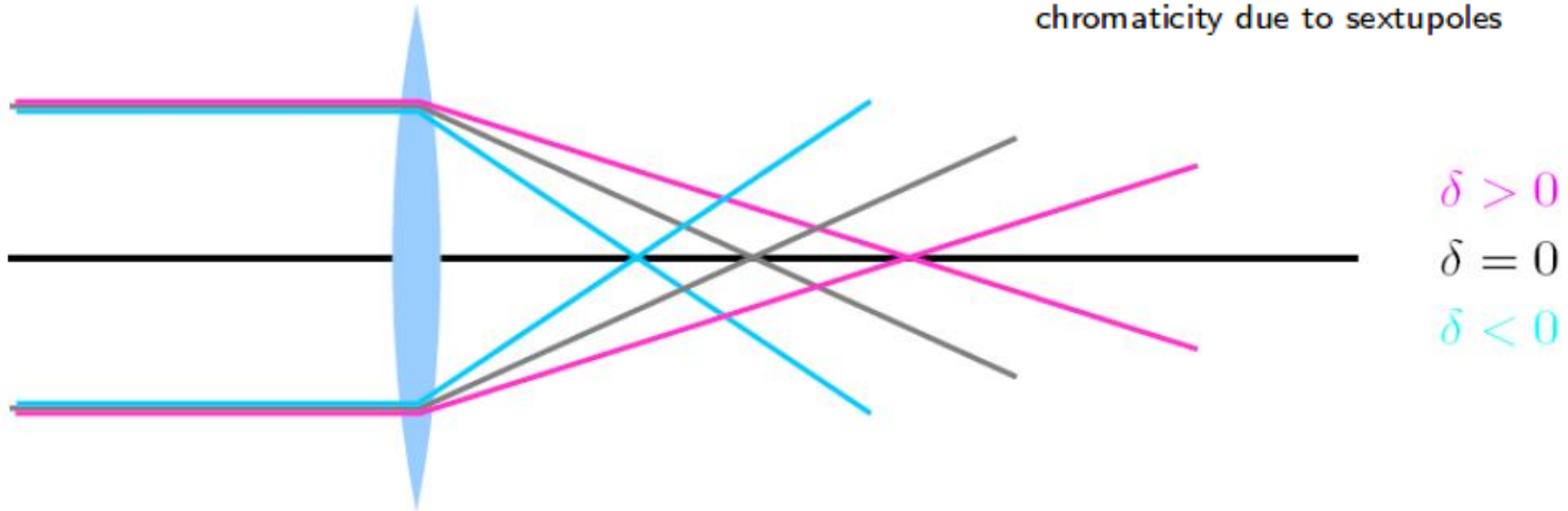
Valerio Dolci

Theory of chromaticity

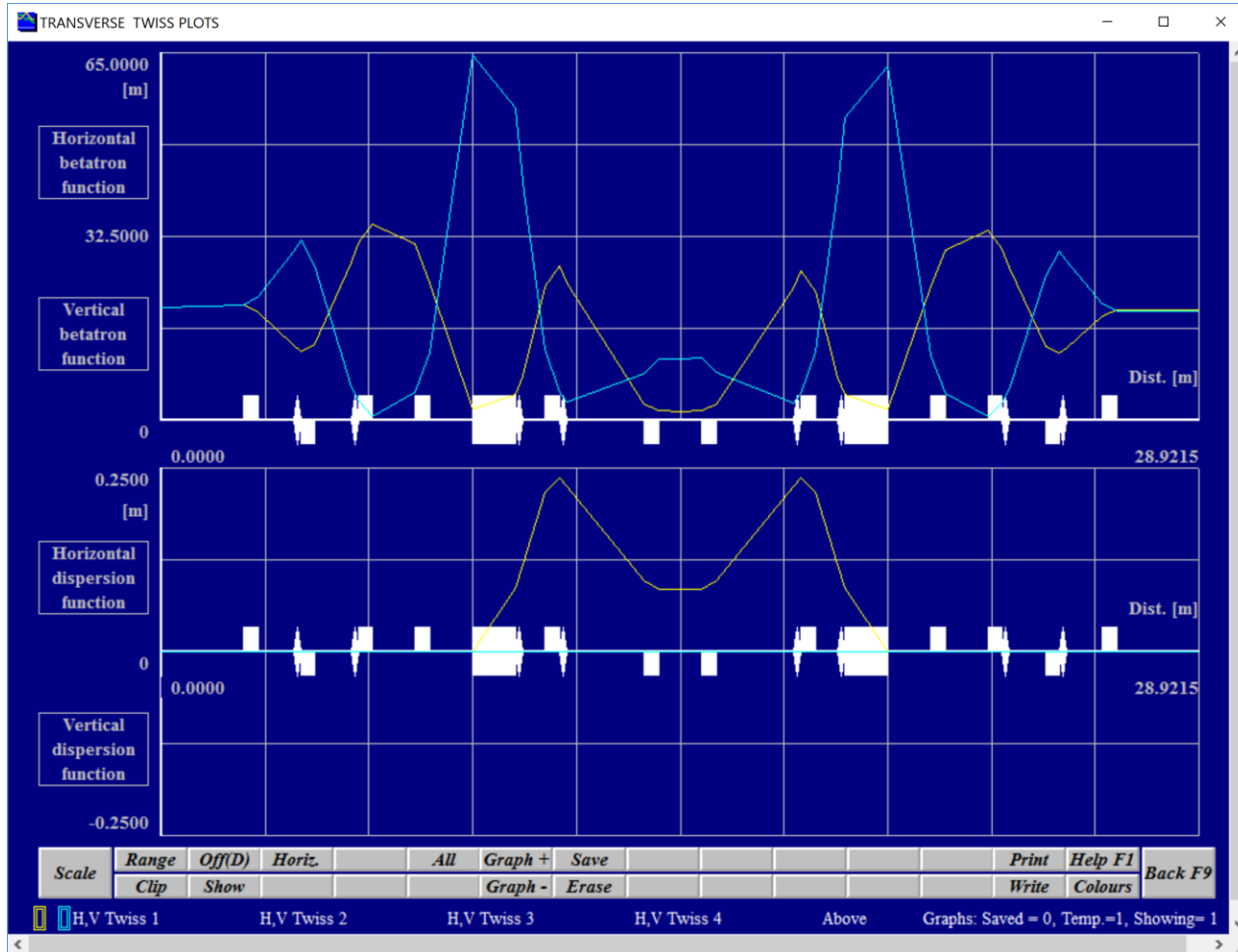
$$\xi_{x,y} = \frac{\delta Q x_y}{\frac{\delta P'}{P}}$$

$$\xi = \underbrace{-\frac{1}{4\pi} \oint k(s) \beta(s) ds}_{\text{chromaticity due to quadrupoles}} +$$

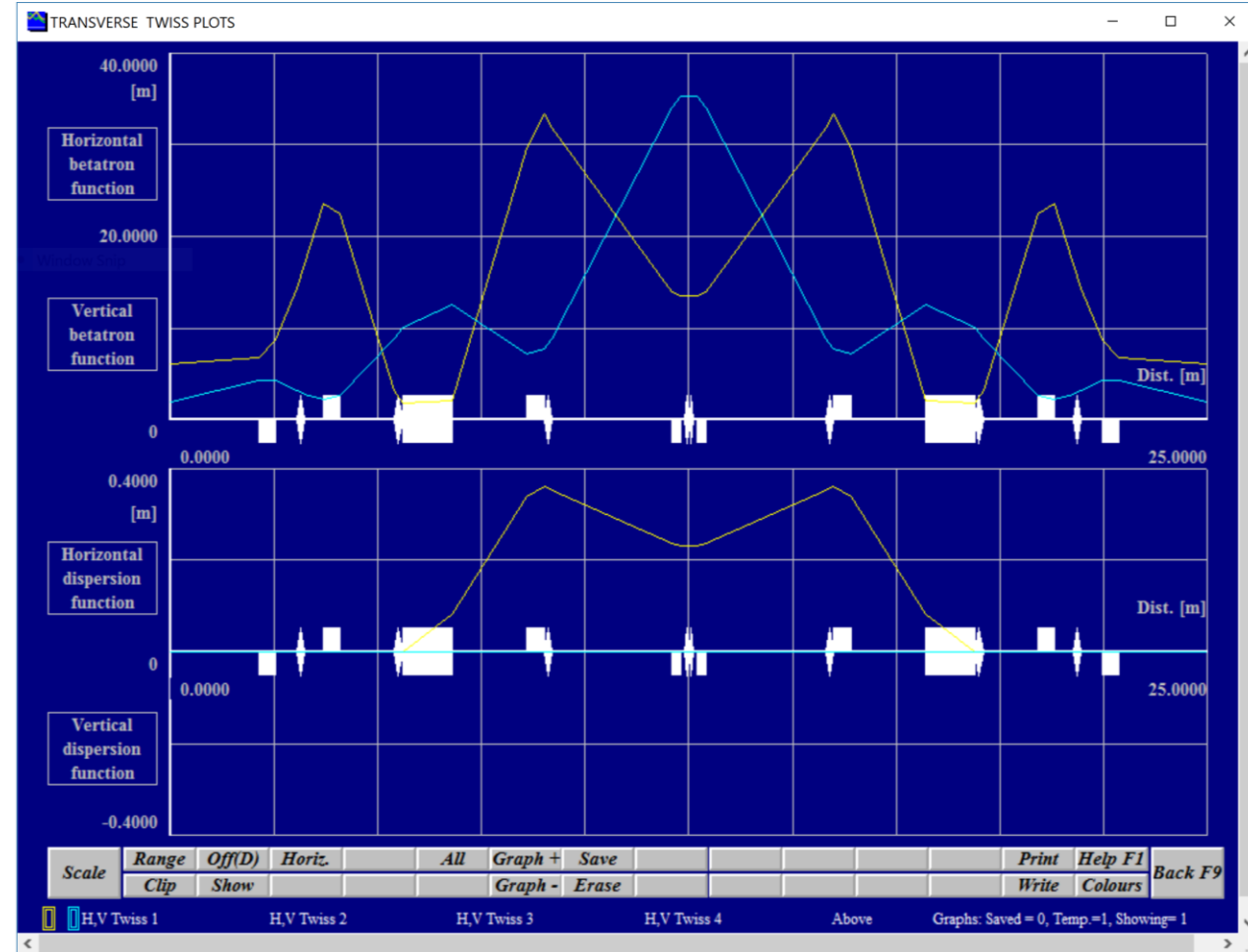
$$\underbrace{\frac{1}{4\pi} \oint k_2(s) D\beta(s) ds}_{\text{chromaticity due to sextupoles}}$$



Global chromaticity correction



$K_2(\text{sext1})=95,68861$
 $K_2(\text{sext2})=-46,42698$



$K_2(\text{sext1})= 15,5725$
 $K_2(\text{sext2})= 21, 9066$

W-vector local correction

$$B = \frac{(\beta_1 - \beta_0)}{(\beta_0 \beta_1)^{1/2}} \quad \text{and} \quad A = \frac{(\alpha_1 \beta_0 - \alpha_0 \beta_1)}{(\beta_0 \beta_1)^{1/2}}$$

$$\psi = \frac{1}{2}(\mu_0 + \mu_1) \quad \text{and} \quad \Delta K = (K_1 - K_0)$$

$$a = \underbrace{\text{Limit}}_{\Delta p/p \rightarrow 0} \frac{A}{\Delta p/p} \quad \text{and} \quad b = \underbrace{\text{Limit}}_{\Delta p/p \rightarrow 0} \frac{B}{\Delta p/p}$$

$$\frac{\delta P}{P} = 0.001\%$$

$$\Delta K = \underbrace{\text{Limit}}_{\Delta p/p \rightarrow 0} \frac{-\Delta K}{\Delta p/p} \quad \text{and} \quad \psi \rightarrow \mu$$

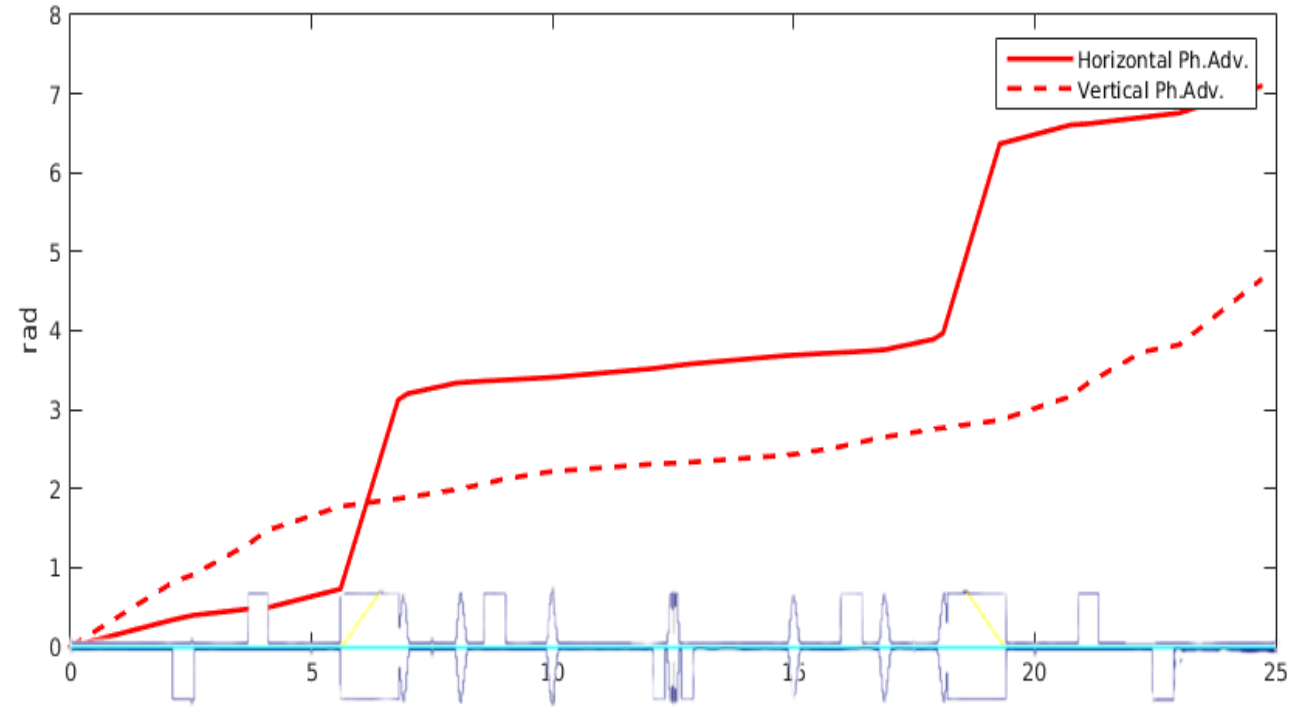
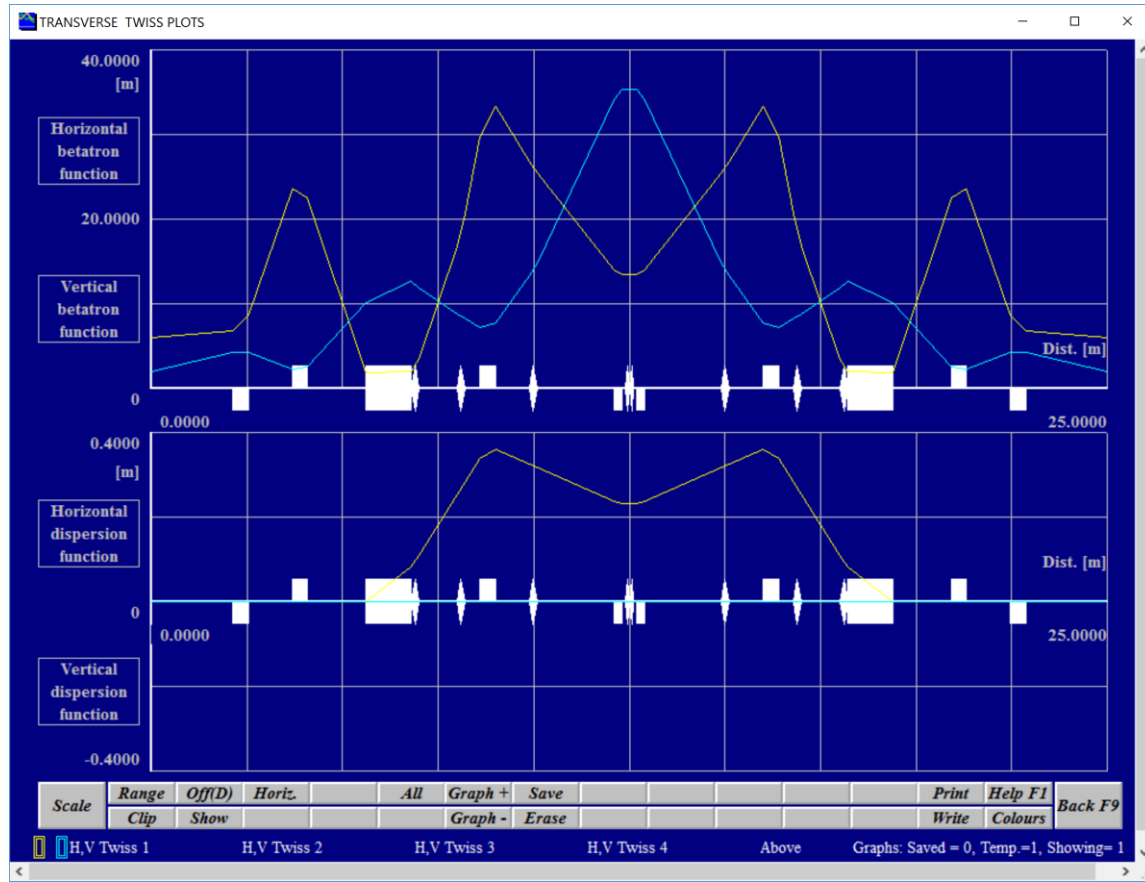
$$w = (b + ja)$$

Thin lens
approximation

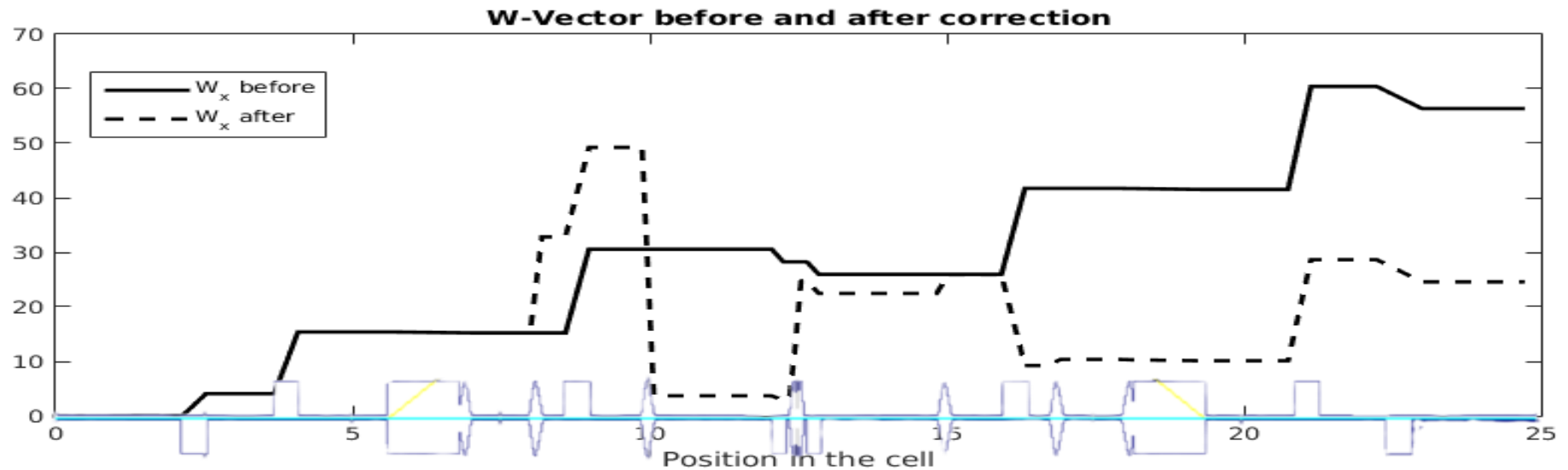
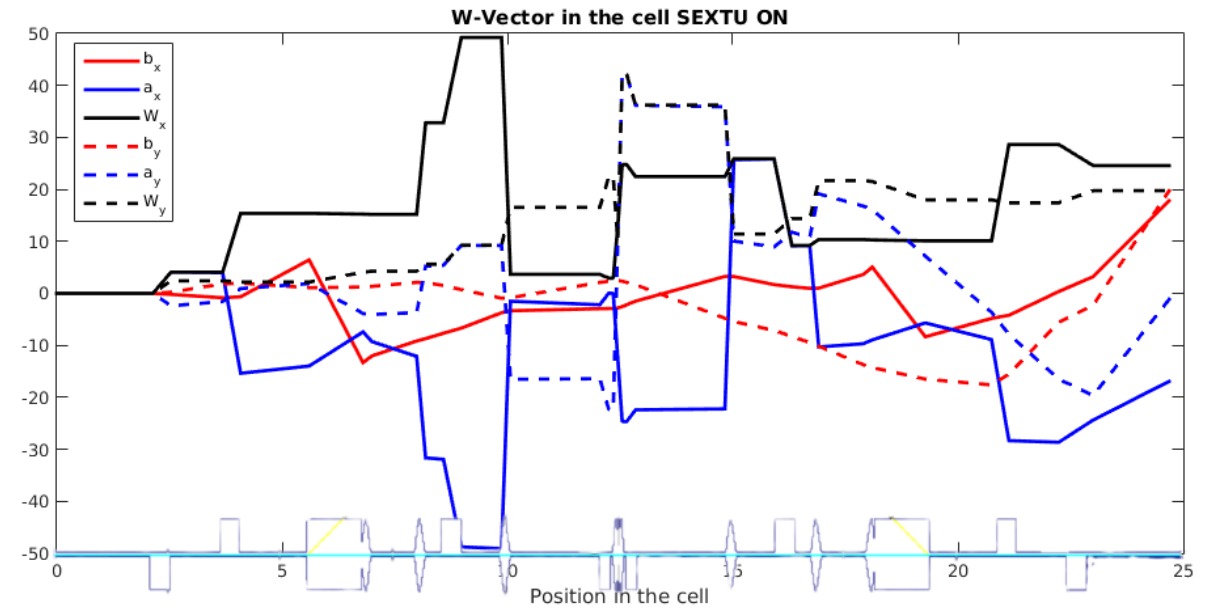
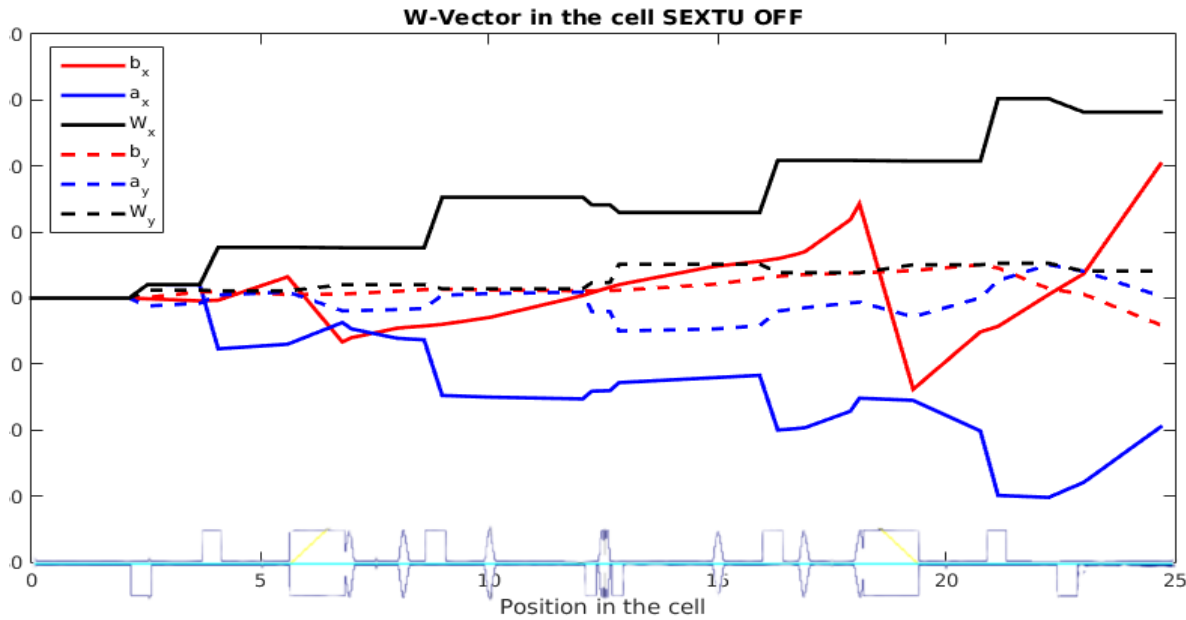
$$\text{Quadrupole: } \Delta a(0) = -(\beta_0 \beta_1)^{1/2} \Delta k \Delta s \approx \beta_0 k_0 \ell_q$$

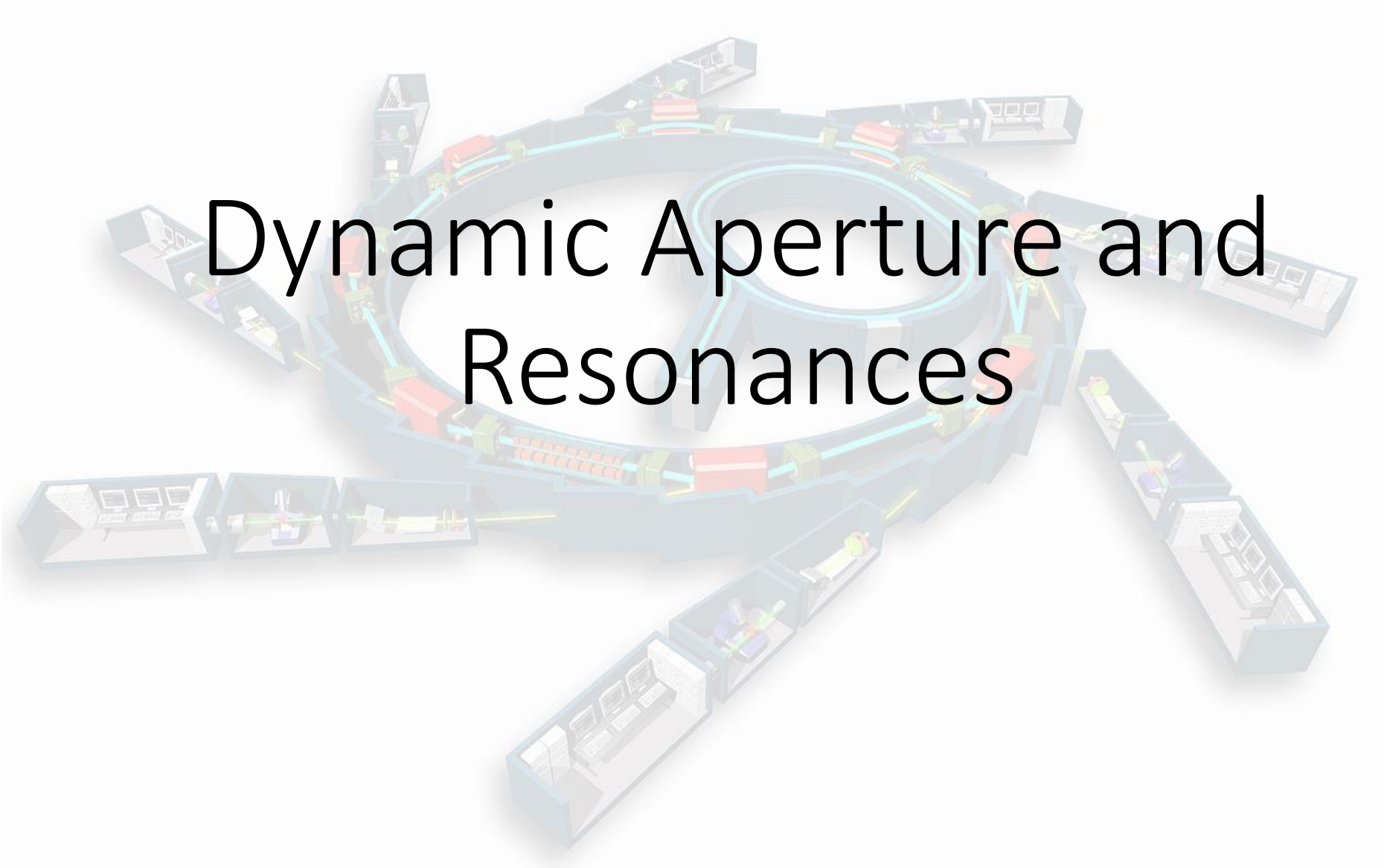
$$\text{Sextupole: } \Delta a(0) = -(\beta_0 \beta_1)^{1/2} \Delta k \Delta s \approx -\beta_0 D_x k_n^1 \ell_s$$

Local correction in optimized cell



Result of local correction on W-vector





Dynamic Aperture and Resonances

Summary

- 1) Introduction to dynamic aperture
 - 2) Resonances
 - 3) Dynamic aperture : First lattice cell.
 - 4) Dynamic Aperture : New lattice.
 - 5) Dynamic Aperture : Improvement.
- Conclusion

Introduction to dynamic aperture

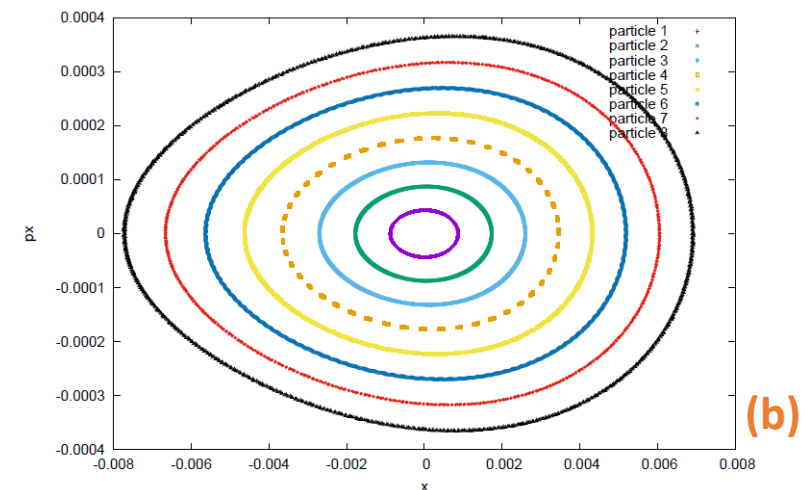
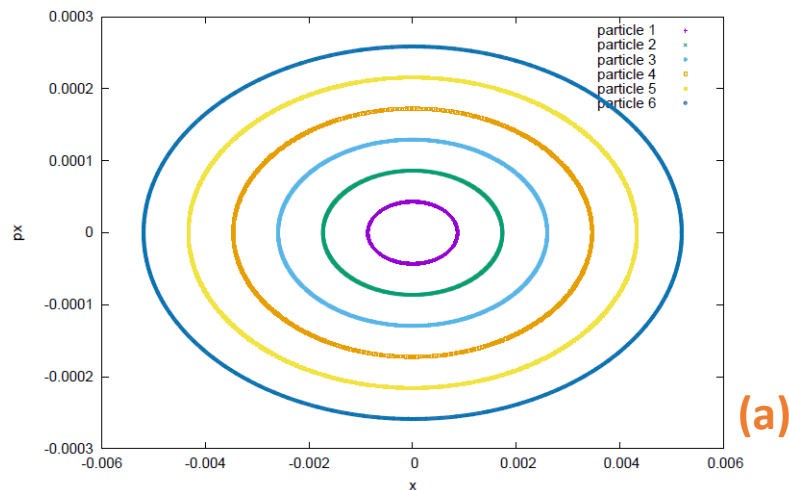
Sextupoles create 2nd order magnetic fields:

- => **non-linear** deformation of the field.
- => non-linear deformation of the **phase space**.
- => modes of **resonance**.



Resonances can dispel the beam in few turns.

Example: *transverse phase space for the ring with sextupoles switched off (a) and on (b).*

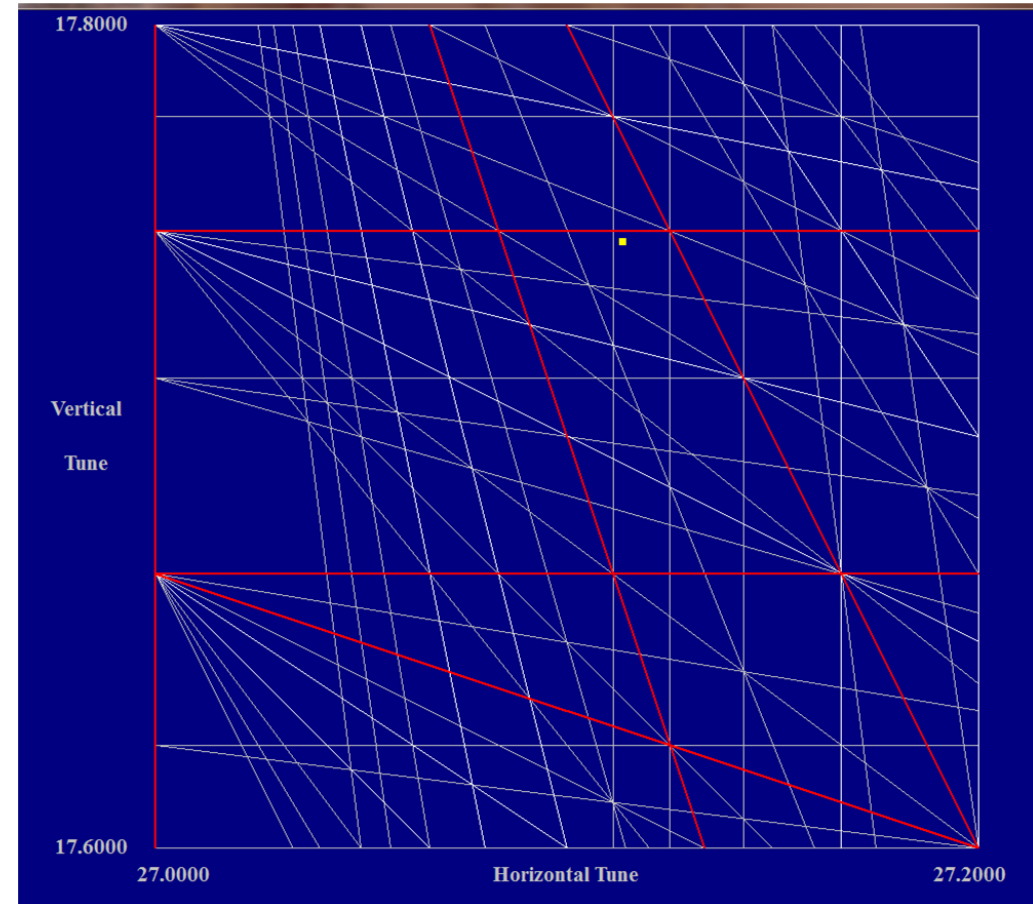


2) Resonances

Sextupoles:

- Correct the chromaticity.
- Do not change the **tune** BUT add resonance modes.
- Problem of **beam stability**.

*Tune diagram showing resonance modes for the optimized ring, from **WinAgile**.*



3) Dynamic aperture: First lattice cell

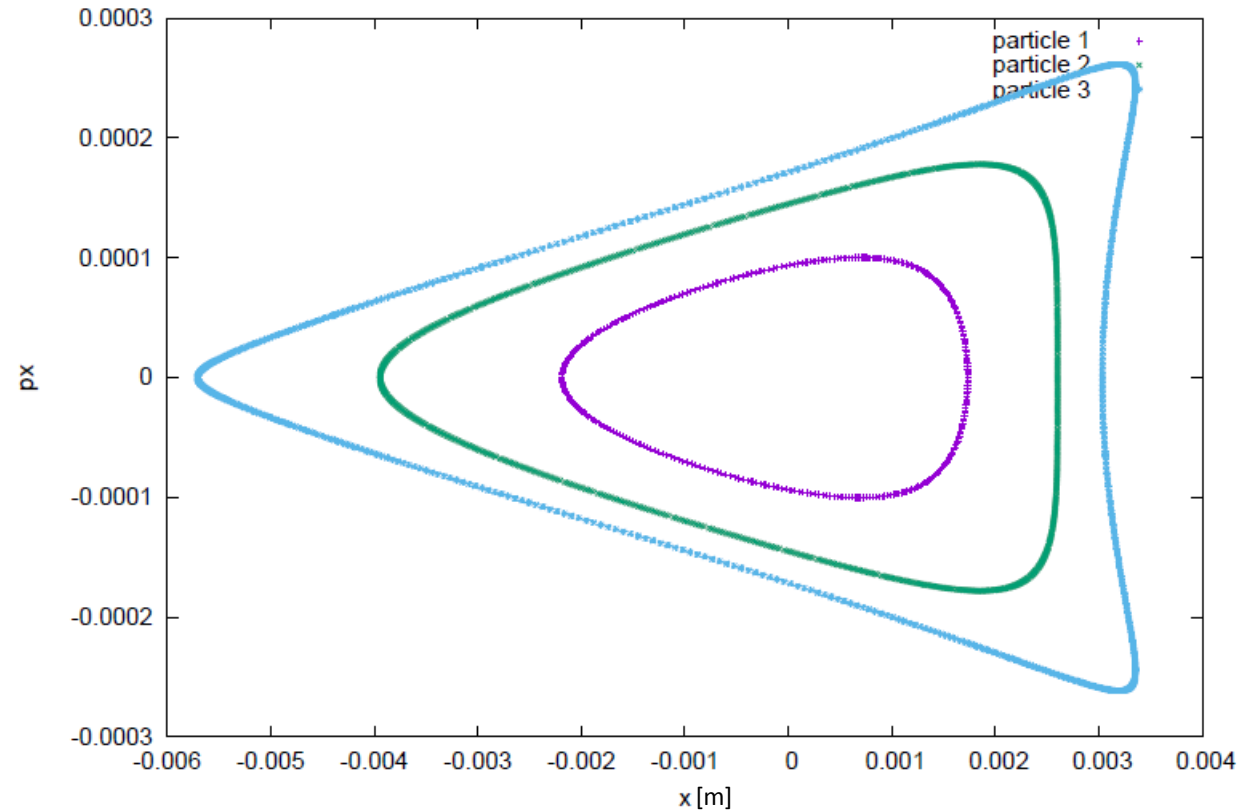
Tracking done with **MAD-X**.

Problems:

- High chromaticity => high **sextupoles strength**.
- => Particles lost after **1,75 σ** only.

With:

$$\sigma_i = \sqrt{\beta_i \cdot \varepsilon_G} = 1,7 \text{ mm}$$



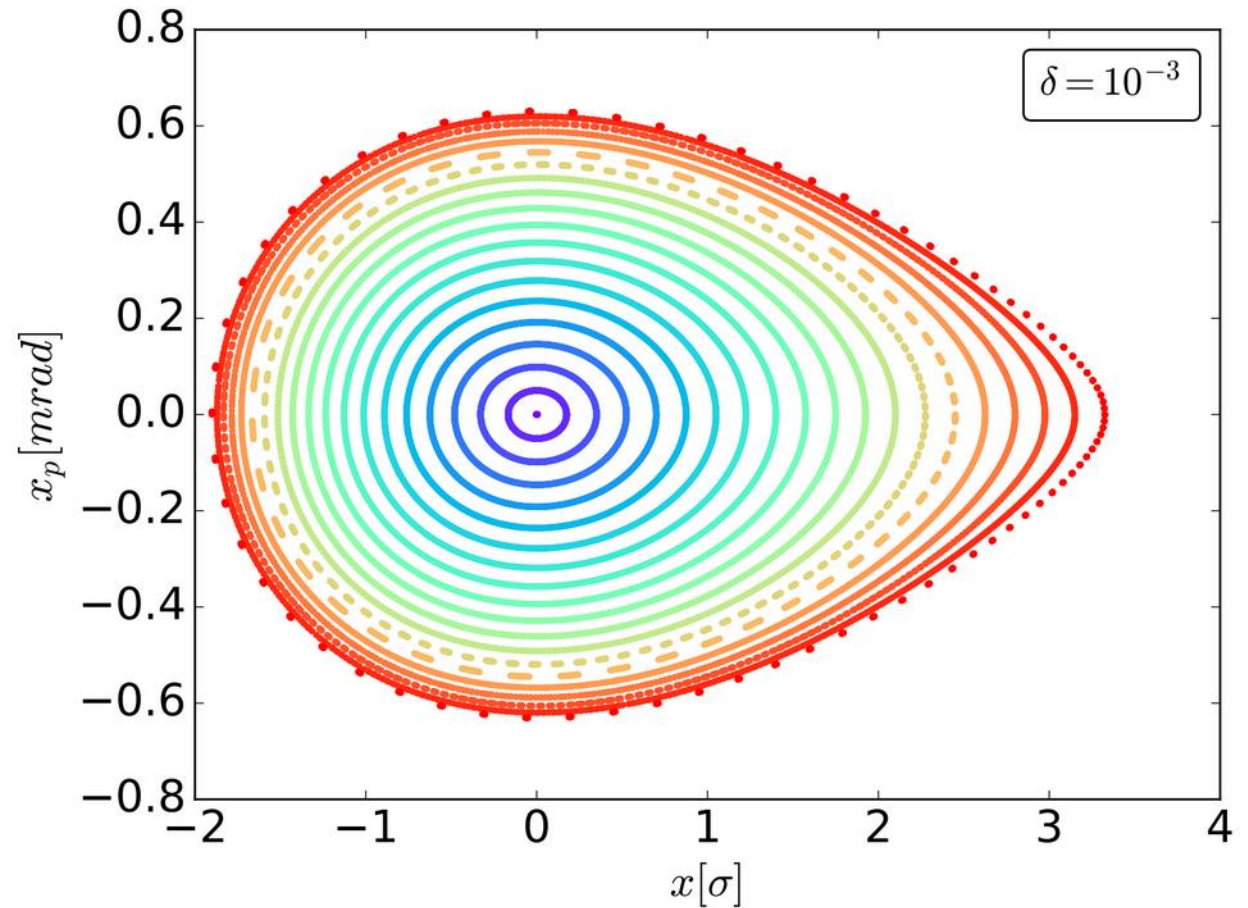
3) Dynamic aperture: New lattice cell

Natural chromaticity is lower than before:

- => lower sextupoles strength
- => Particles now lost after **3,65 σ** .

Note:

All focusing and defocusing sextupoles have respectively the **same strength**.



3) Dynamic aperture: Improvement

Correction sextupoles are in:

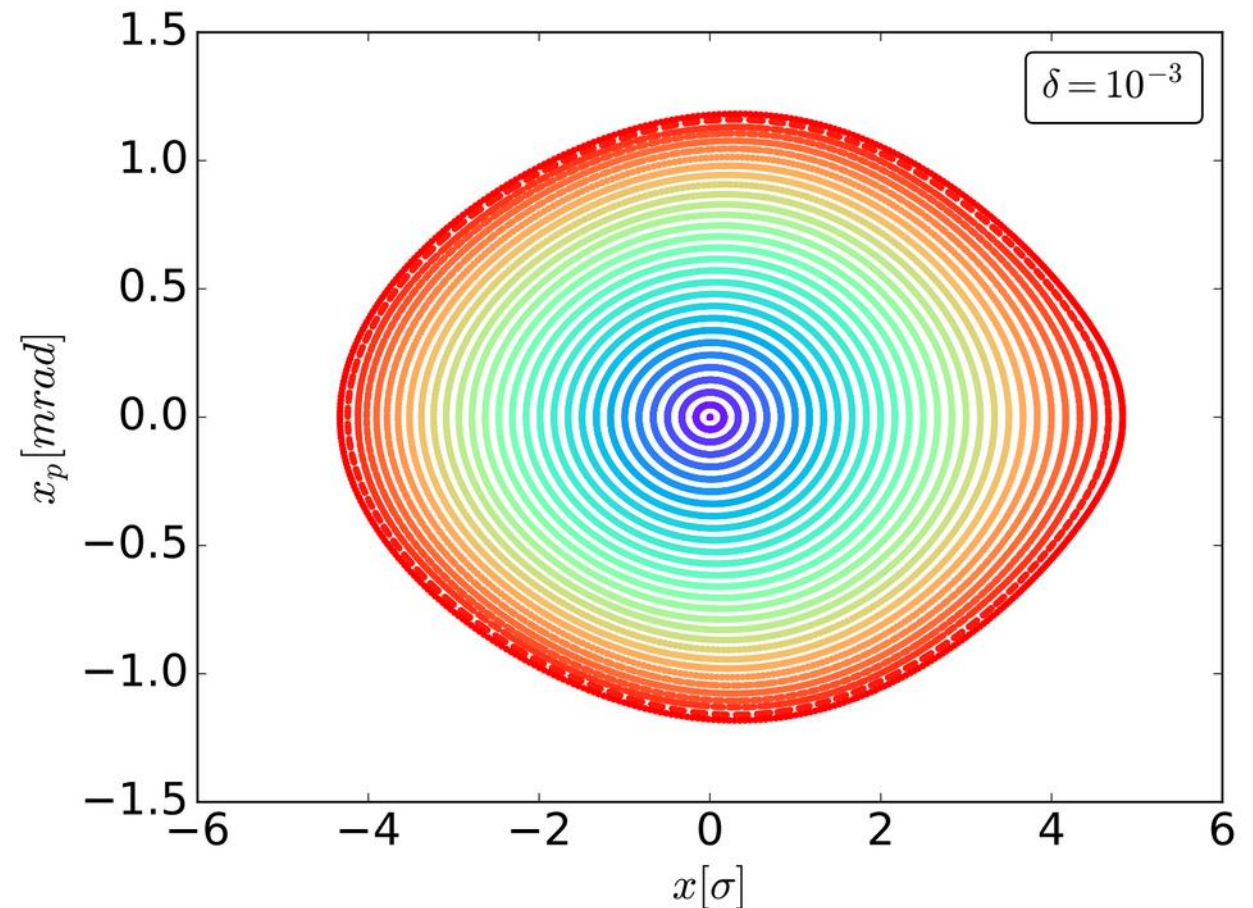
- Zero-dispersion zone.
- => do not affect chromaticity.
- => only compensate other sextupoles strength.

- Low- β zone.
- => need **more strength** to do the compensation.

With:

$$K_{corrector} = 2,5 \cdot K_{sextupole}$$

=> Reach **5 σ** .



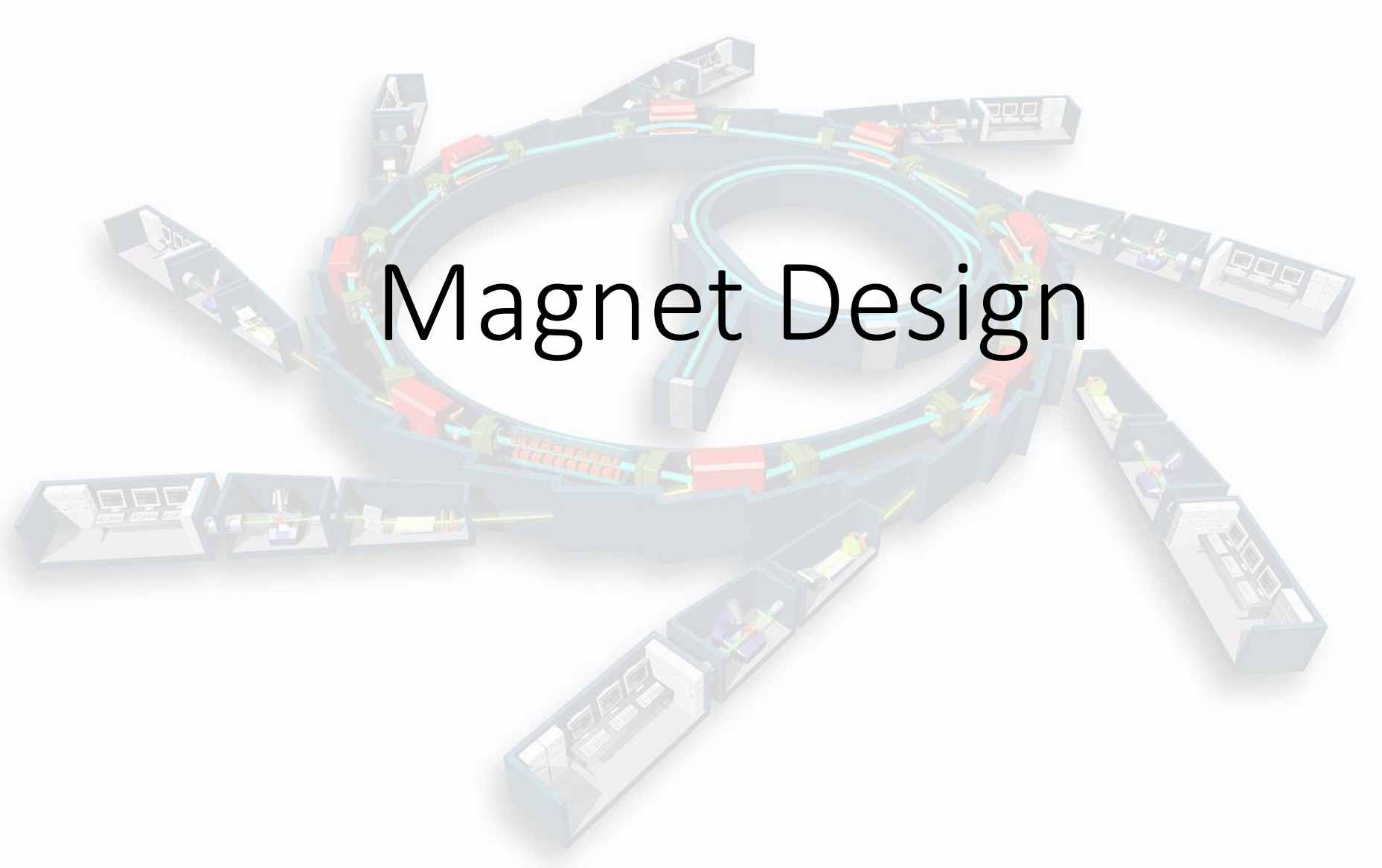
Conclusion

Dynamic aperture high enough to have a **stable beam**: 5σ (at least 3σ are required).

Due to:

- Lower natural chromaticity (lattice design, quadrupoles).
- So lower sextupoles strength to correct it.
- So less magnetic field **deformations**.

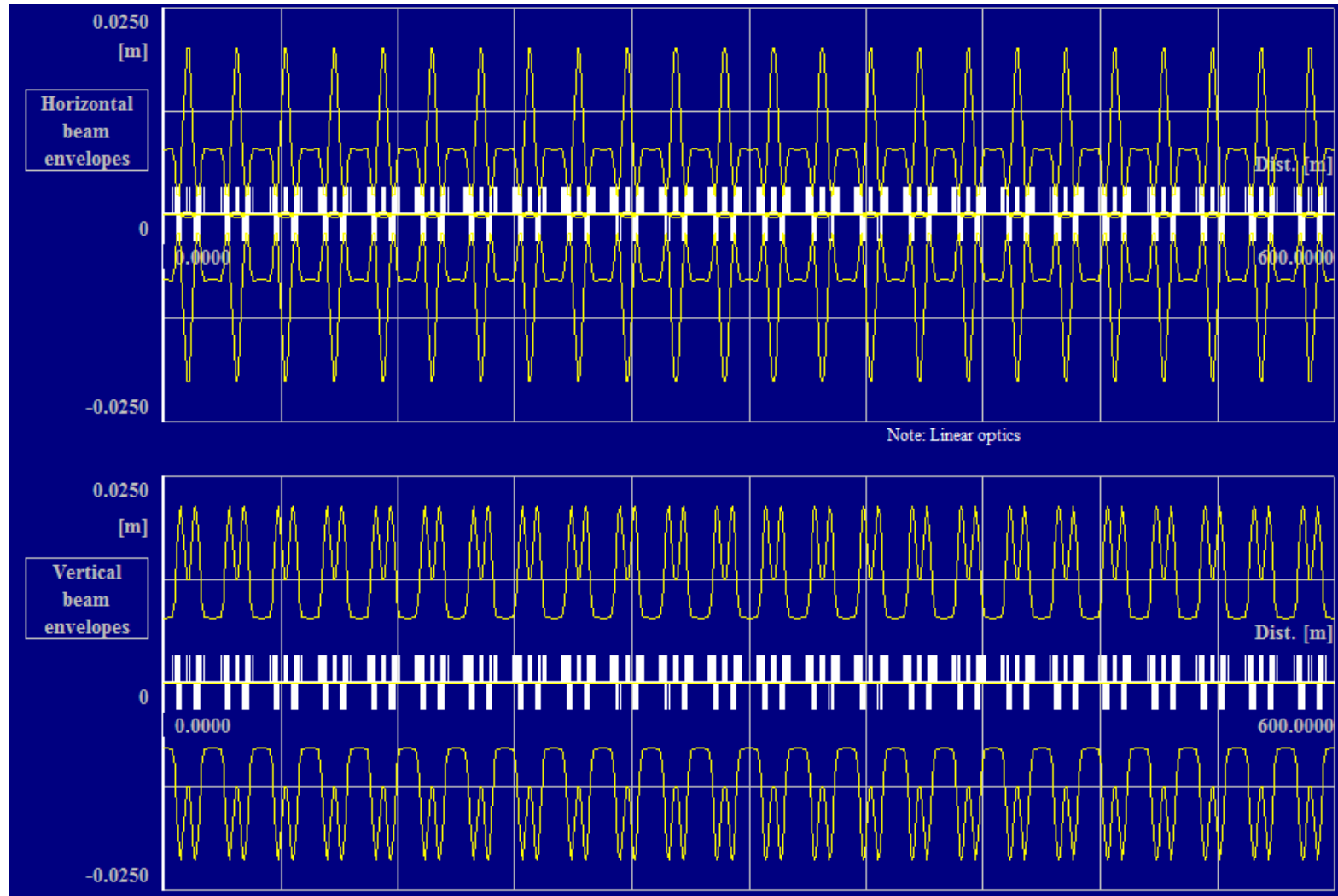
Close to resonances, but can be corrected by a **tune shifter**.



Magnet Design

Mina Abbaslo
Elham Salehi

Magnet Design



Main Specifications For Dipole

$B_{max}, [T]=1.0918$

Bending Radius, [mm]=9160

Bending Angle, [°]=0.1309

Magnet Length, [mm]=1200

Iron Yoke Specifications

Overall Length, [mm]=10*gap=560

$L_{iron}, [mm]=1166.9$

Pole width, [mm]=5*56=280

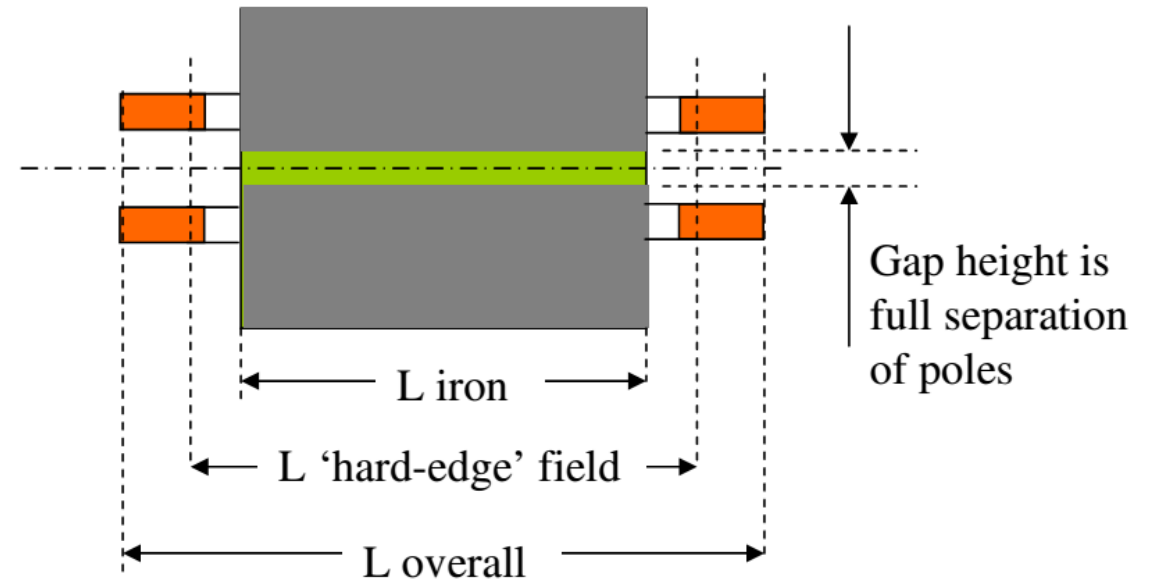
Overall width, [mm]=13*56=728

Overall height, [mm]=10*56=560

Coil Specifications

$NI, [A]=24326.5245$

Conductor dimensions, [mm]=12*12



Gap height= 56mm (External beam pipe Diameter + Geometric alignment tolerance + Thermal insulation)

Dipole Eddy Current

Selected unit=10. Dipole1

Dipole half gap [m]= 0.028000

Left/lower wall [m]= -0.02850

Right/upper wall [m]= 0.02850

Wall thickness [m] =0.00150000

Resistivity [ohm m] =0.0000007200

Laminated yoke

Pole width [m] = 0.210000

Lamination thickness [m] =0.00100000

End plate thickness [m] =0.05000000

Lamination resistivity [ohm m] =0.0000001000

End plate resistivity [ohm m] =0.0000001000

Path length in iron [m] = 1.120000

Lamination: principal mode, T 1,1 = 0.00002496

End plate: principal mode, T 1,1 = 0.05906533

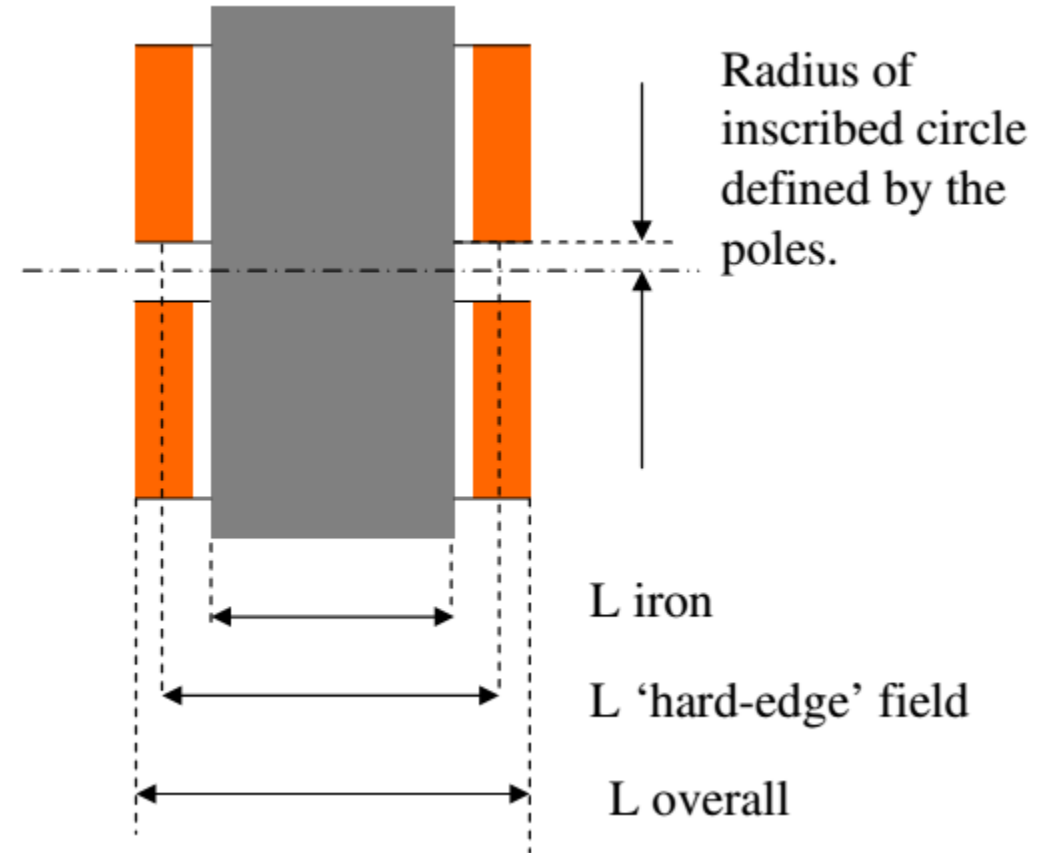
Main Specifications For Quadropole

- Magnet Length,[mm]=400
- Aperture diameter,[mm]=28
- Overall Length,[mm]=56.3720
- Liron,[mm]=0.3720
- Overall width,[mm]=7*28=196
- NI,[A]=16964.11

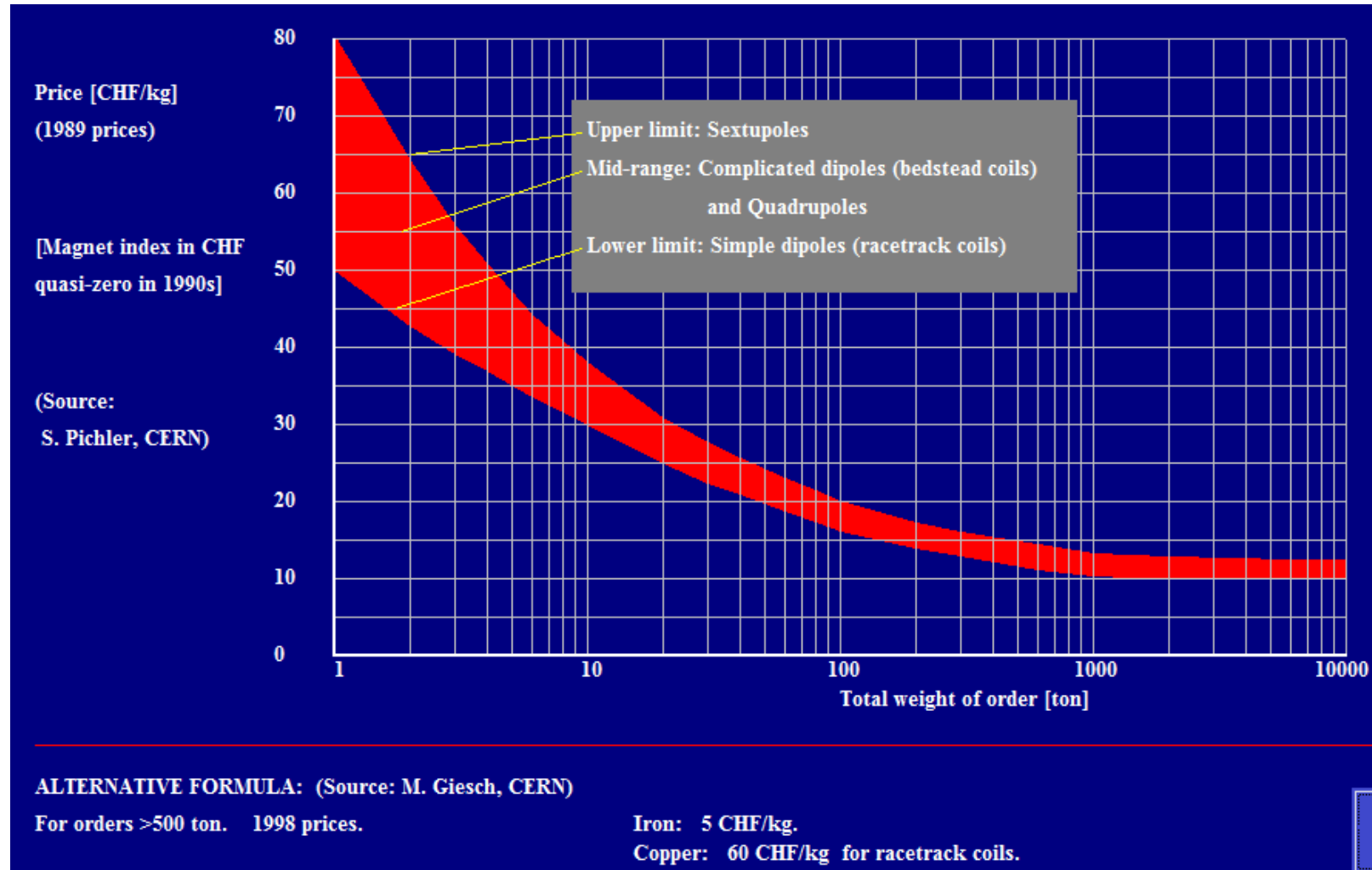
$$r_x \propto \sigma_x = \sqrt{\epsilon_x \beta_x}$$

$$r_y \propto \sigma_y = \sqrt{\epsilon_y \beta_y}$$

$$r = \max(r_x, r_y)$$



Magnet Cost





Aperture and Vacuum

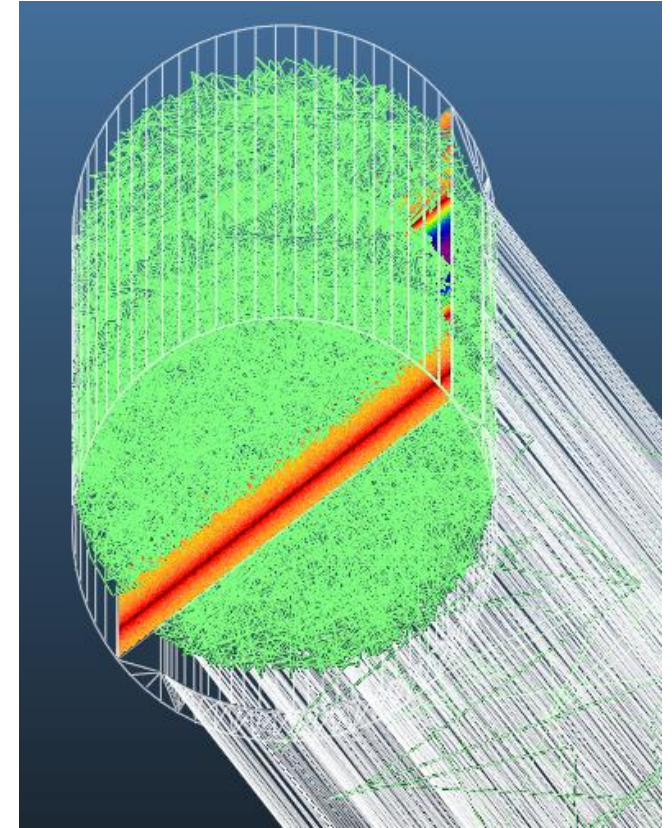
Nicolas Misiara

Vacuum & aperture

- Input parameters
 - Base vacuum pressure : **$1,33 \cdot 10^{-10}$ mBar** (10^{-10} torr)
 - Reference value of β function : **150m**
 - Induced $4,5\sigma$ minimum radius of the beam pipe : **21mm**

Vacuum & aperture

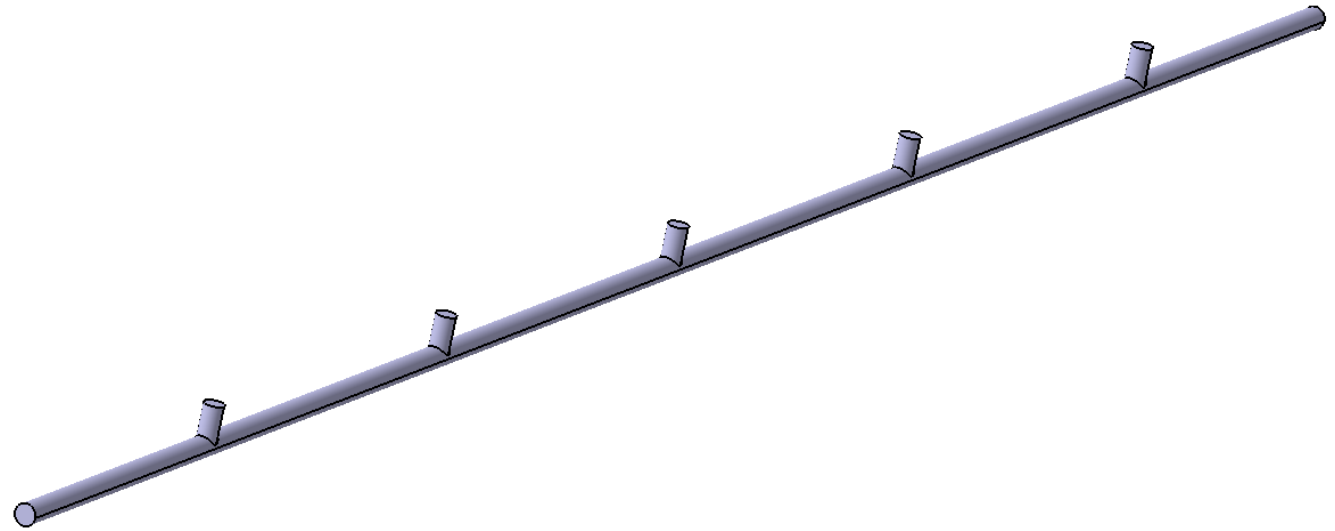
- Molflow (CERN) simulation software
 - Monte-Carlo statistical counting
 - Simulation without beam
 - No time-dependency



molflow.web.cern.ch

Vacuum & aperture

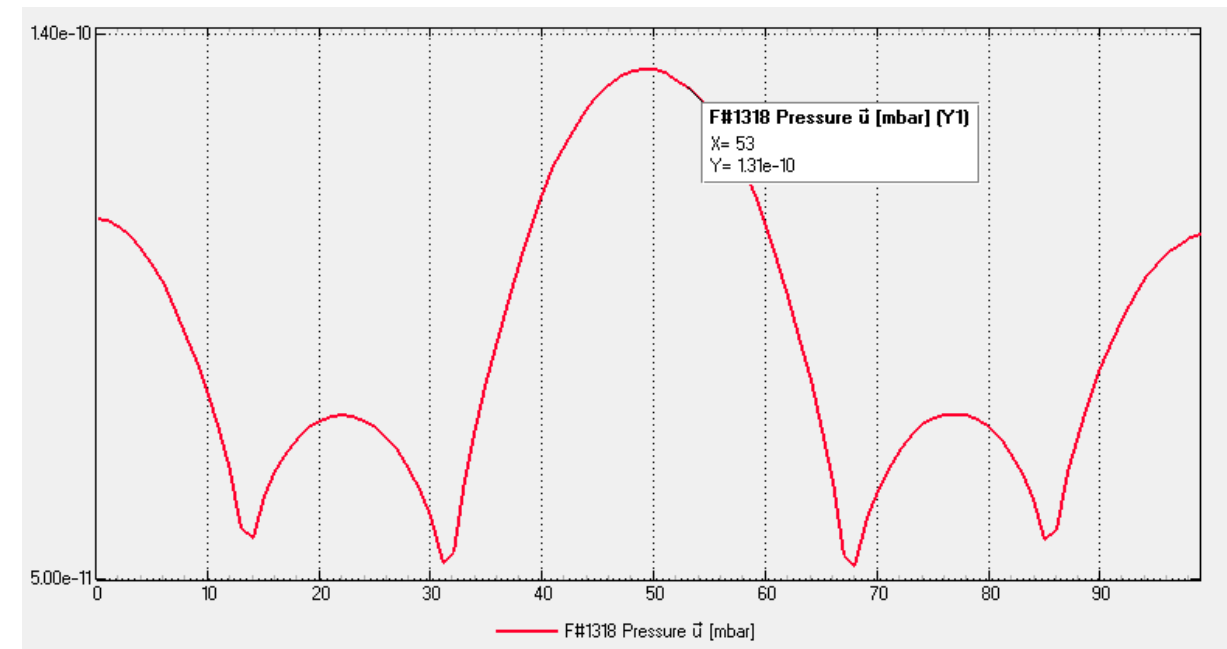
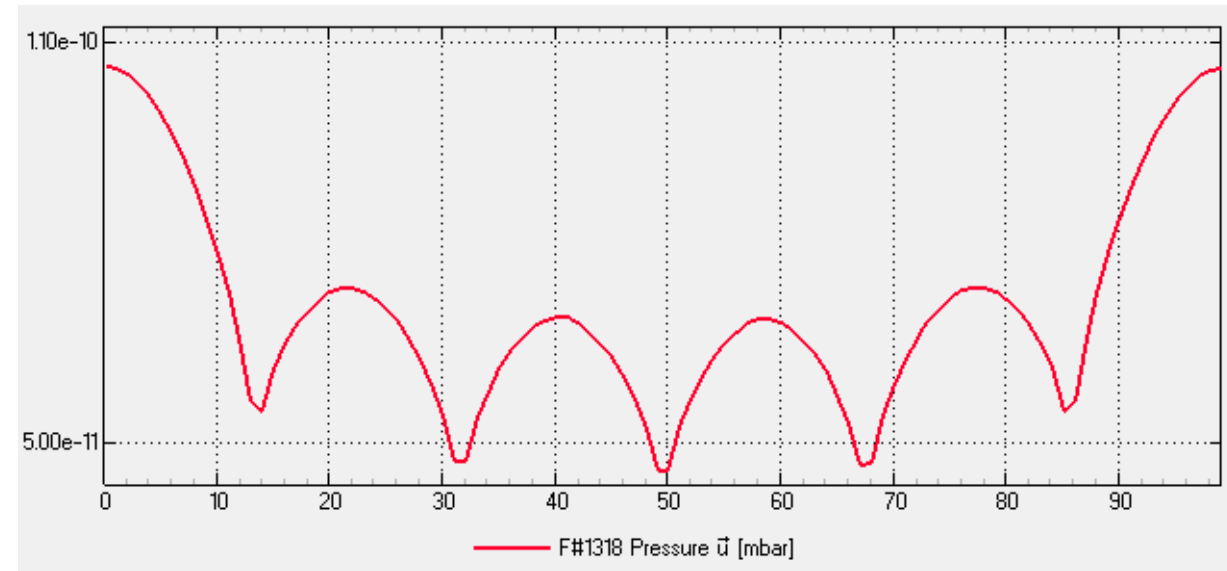
- Source of particle
 - Outgassing of the beam pipe ($1,3 \cdot 10^{-12}$ mBar.L/s/cm² for stainless steel)
- Sink of particle
 - Pumping systems (50 – 100 L/s)
- 5m cell
- Constant $\varnothing 42$ mm
- $\varnothing 40$ mm ports every 0,9m



Vacuum & aperture

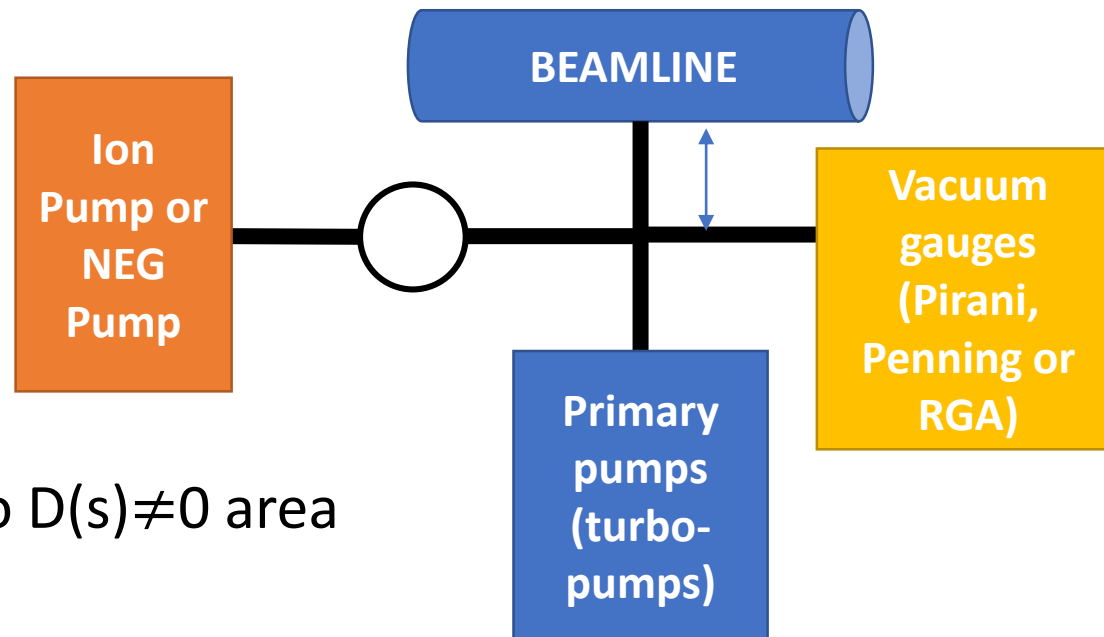
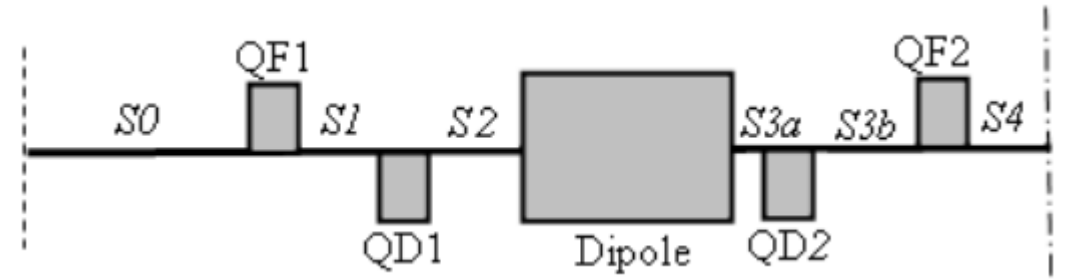
- 5 pumps every 0,9 m
- 50 L/s (50%)

- 50 – 75 – 0 – 75 – 50 L/s
- 1,8 m



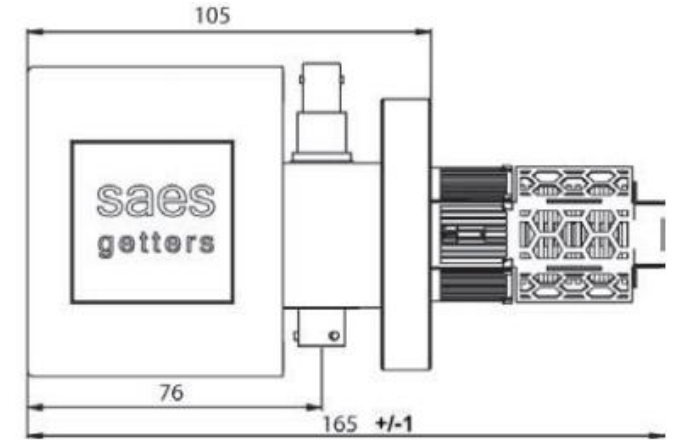
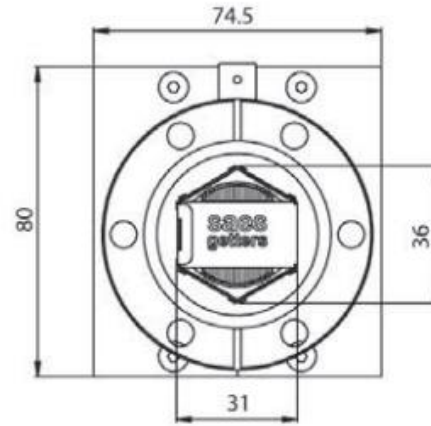
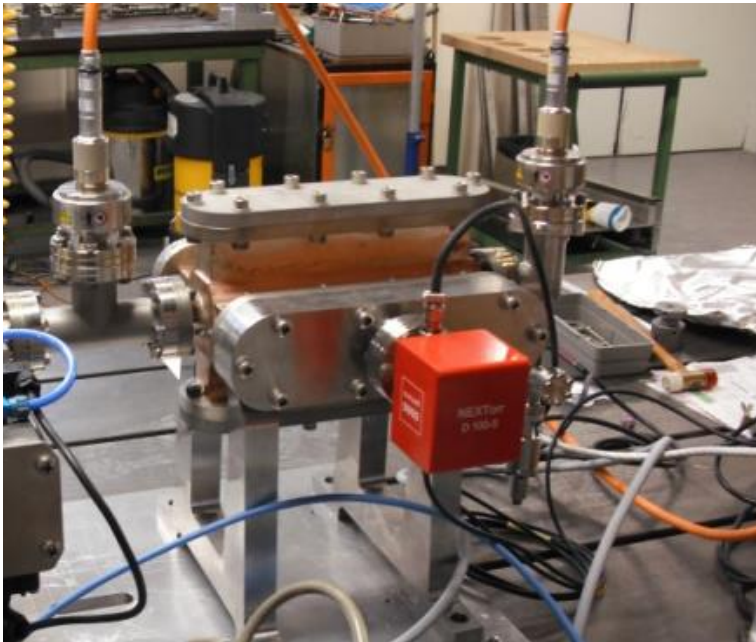
Vacuum & aperture

- Implantation on the beamline
 - Dipoles : 1,2 m long
- Pumping cell
 - MPS
- Photodesorption
 - Placing the pumps close to $D(s) \neq 0$ area



Vacuum & aperture

- Ex : NEG pump : SAES Getters NexTorr
 - 100L/s





Synchrotron radiation

Marco Diomede
Anna Pugelise

Goals

- Compute
critical frequency of bending;
energy loss per turn;
total power radiated;
- Install IDs to reach **5 keV**;
- Compute
tuning range;
energy loss per turn;
total power emitted by the IDs;
- Compute the **RF power** needed for 300mA;
- Install SCW for a UV wavelength.

✓ Compute **critical frequency** of bending, **energy loss per turn**, **total power radiated**;

Bending Radius ρ (m)	Energy (GeV)	Lorentz Factor Υ
9.167	3	5871

Critical Frequency

$$\omega_c = \frac{3}{2} \frac{c}{\rho} \gamma^3 = 9.93 \cdot 10^{18} \frac{\text{rad}}{\text{s}}$$

Critical Energy

$$\varepsilon_c = \hbar \omega_c = 6.5 \text{ keV}$$

**Energy Loss
per Turn
per electron**

$$U_0(\text{keV}) = \frac{e^2 \gamma^4}{3 \varepsilon_0 \rho} = 88.46 \frac{E(\text{GeV})^4}{\rho(\text{m})} = 781 \text{ keV}$$

**Total Power
Radiated**

$$P(\text{kW}) = \frac{e \gamma^4}{3 \varepsilon_0 \rho} I_b = 88.46 \frac{E(\text{GeV})^4 I(\text{A})}{\rho(\text{m})} = 235 \text{ kW}$$

✓ Install IDs to reach **5 keV**

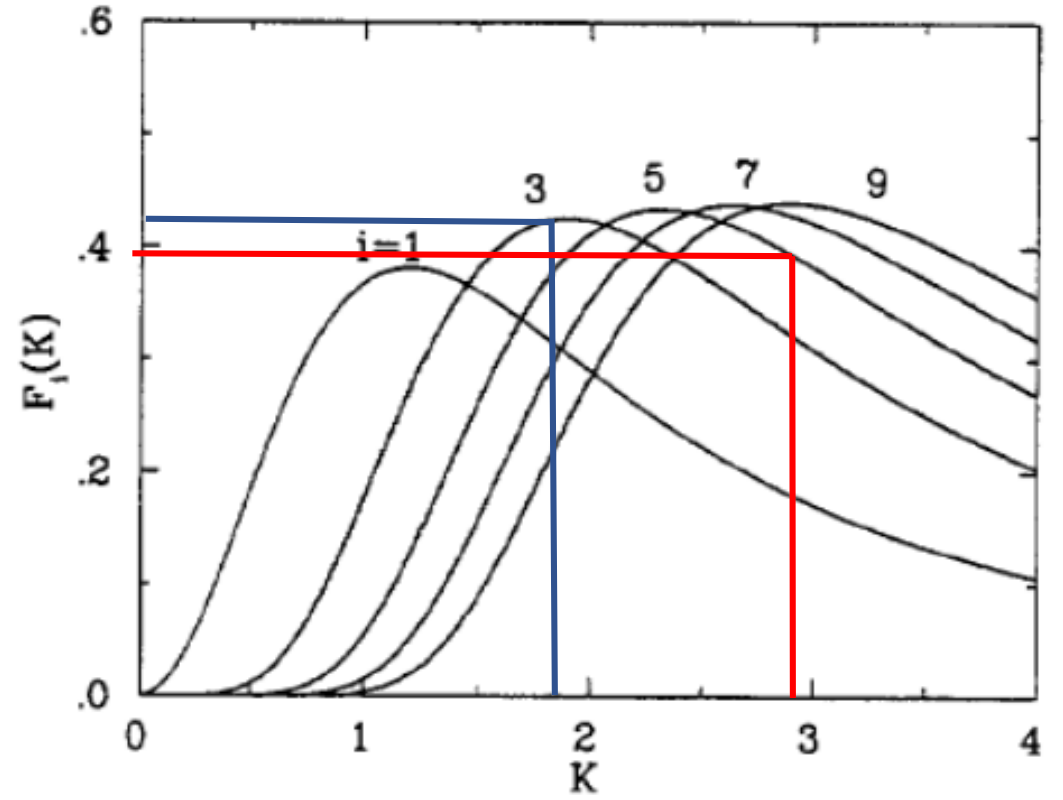
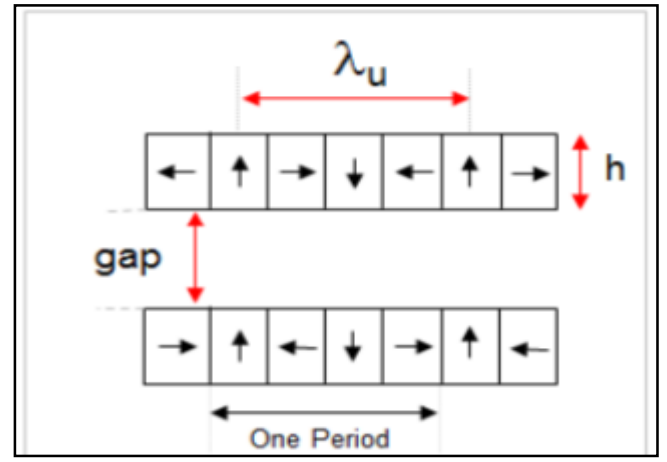
TYPICAL VALUES FOR AN UNDULATOR	
Pole Tip Field B_r (T)	Undulator Period λ_u (mm)
1.3	20

$\epsilon = \frac{hc}{\lambda} = 5 \text{ keV} \quad \longrightarrow \quad \lambda = 2.48 \cdot 10^{-10} \text{ m}$

$\lambda_n = \frac{\lambda_u}{2\gamma^2 n} \left(1 + \frac{K^2}{2} \right) \quad \longrightarrow \quad K = 1.77 \text{ for } n = 3$

$K = 0.168 B_r \lambda_u e^{-\frac{\pi \text{Gap}}{\lambda_u}} \quad \longrightarrow \quad \text{Gap} = 5.83 \text{ mm} > 4 \text{ mm}$
(Limit for an undulator)

For $n = 5 \quad K = 2,94 \quad \text{Gap} = 2.55 \text{ mm} < 4 \text{ mm}$



✓ Compute tuning range

$$K_{max}(Gap = 4mm) = 0.168 B_r \lambda_u e^{-\frac{\pi Gap}{\lambda_u}} = 2.33$$

$$\lambda_n = \frac{\lambda_u}{2\gamma^2 n} \left(1 + \frac{K^2}{2} \right)$$

$$0.5 \leq K \leq 2.33$$



$$\lambda_{@K=0.5} \leq \lambda \leq \lambda_{@K=2.33}$$

$$n = 1$$

$$K = 0.5$$

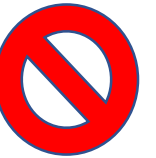


$$\begin{cases} \lambda_{@K=0.5} = 3.26 \cdot 10^{-10} m \\ \lambda_{@K=2.33} = 10.77 \cdot 10^{-10} m \end{cases}$$

$$K = 2.33$$

$$3.26 \cdot 10^{-10} m \leq \lambda \leq 10.77 \cdot 10^{-10} m$$

$$\lambda = 2.48 \cdot 10^{-10} m$$



$$n = 3$$

$$K = 0.5$$



$$\begin{cases} \lambda_{@K=0.5} = 1.09 \cdot 10^{-10} m \\ \lambda_{@K=2.33} = 3.59 \cdot 10^{-10} m \end{cases}$$

$$K = 2.33$$

$$1.09 \cdot 10^{-10} m \leq \lambda \leq 3.59 \cdot 10^{-10} m$$

$$\lambda = 2.48 \cdot 10^{-10} m$$



- ✓ Compute **energy loss per turn, total power emitted** by the IDs;

TYPICAL VALUES FOR AN UNDULATOR		
Pole Tip Field B_r (T)	Undulator Period λ_u (mm)	Undulator Length (m)
1.3	20	2

$$E_u \text{ (eV)} = 0.07257 \frac{E^2 \text{ (GeV)} \cdot K^2}{\lambda_u^2 \text{ (m)}} L_u \text{ (m)} = 10 \text{ keV}$$

$$\#cells = 20$$

$$E_{u,tot} = \#cells \cdot E_u = 200 \text{ keV}$$

$$P_{u,tot} = E_{u,tot} \cdot I = 60 \text{ kW}$$

- ✓ Compute the **RF power needed** for 300mA;

$$P_{RF} = P_{tot} = P_{u,tot} + P_{syn_rad} = 295 \text{ kW}$$

✓ Install **SCW** for a UV wavelength

TYPICAL VALUES FOR A WIGGLER		
Wiggler Parameter K	Wiggler Period λ_u (mm)	Wiggler Length (m)
20	40	2

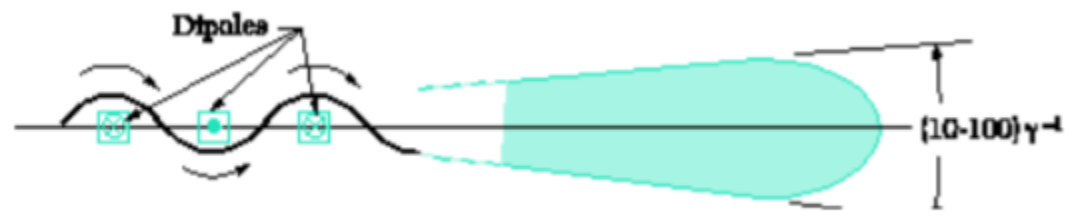
$$B_0 = \frac{K 2\pi mc}{e\lambda_u} = 5.35 \text{ T}$$

$$\lambda_1 = \frac{\lambda_u}{2\gamma^2} \left(1 + \frac{K^2}{2} \right) = 1.16 \cdot 10^{-7} \text{ m}$$

$$E_w = 326 \text{ keV}$$

$$P_{w,tot} = E_{w,tot} \cdot I = \#cells \cdot E_w \cong 2.0 \text{ MW}$$

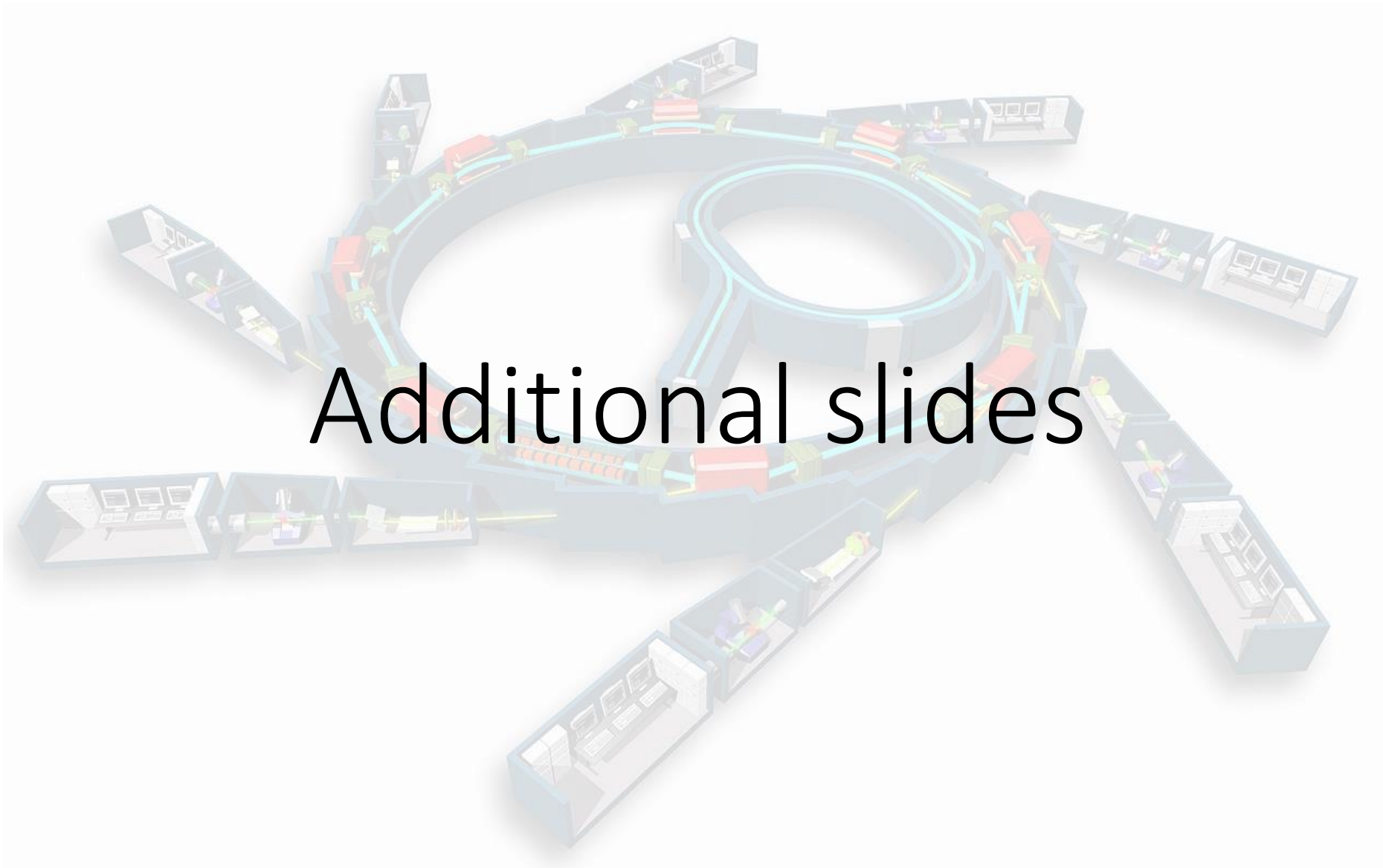
$$P_{tot} = P_{w,tot} + P_{syn_rad} = 2.235 \text{ MW}$$



wiggler - incoherent superposition $K > 1$



**Thank you for your
attention**



Additional slides

Phase shifter

Plotting the quadrupole strength vs phase shift, we observe a discontinuity.

