



TAMPERE
UNIVERSITY OF
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Quench protection studies updated

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+ the magnet designers in WP5 team!*

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Outline

1. 40 ms protection delay at 105% of I_{nom}
2. Parametric analyses
3. Protection with heaters ($\cos\theta$)
 - Is the high current the most critical?
4. Failure scenarios and impact of uncertainties
5. Summary

Simulation methods

- Current decay and temperatures with Coodi
 - Adiabatic
 - Field map and inductance from ROXIE
 - Quench delays and propagation velocities are input
- Heater delays with CoHDA
 - 2-D simulation of heat conduction from heater to coil
 - Quench onset when cable temperature reaches T_{CS}
 - T_{CS} for cable maximum field, no degradation

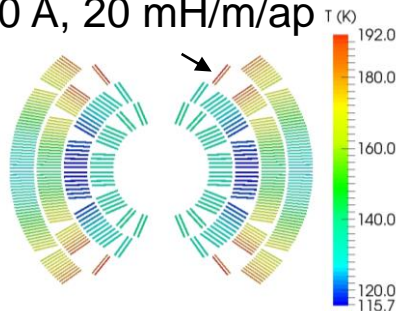
1. 40 ms uniform protection delay: Temperatures

Protection delay includes the detection, etc.

	T_{max} (K)	ΔT (incl. HS) (K)	ΔT (excl. HS) (K)
Cos θ	345	~140	~60
Block	356	~250	~80
CC*	353	~250	~120

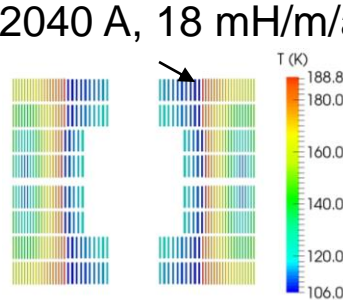
16T_22b-37-optd6f6

11790 A, 20 mH/m/ap



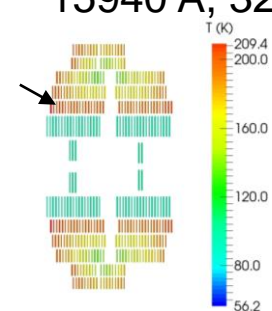
V20ar

12040 A, 18 mH/m/ap



V1h2

15940 A, 32 mH/m/2-ap



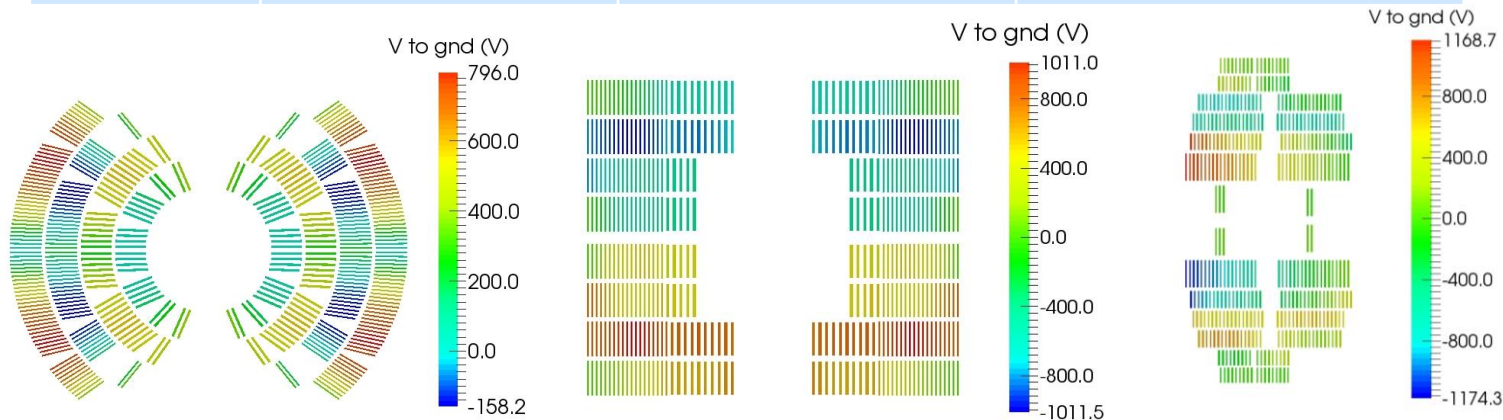
*CC winding order and induct. tbc



1. 40 ms uniform protection delay: Voltages

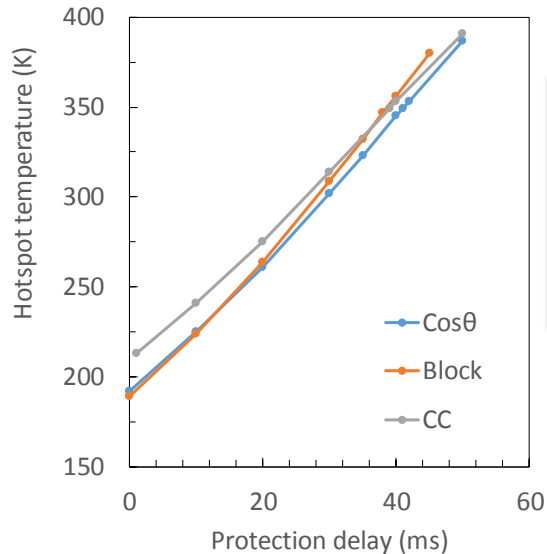
	Max to gnd (V)	Max btw turns (V)	Max btw layers (V)
Cos θ	800	90	970
Block	1010	70	880
CC*	1200	80	1860

Initial quench propagation excluded



2. Parametric analysis with uniform delay

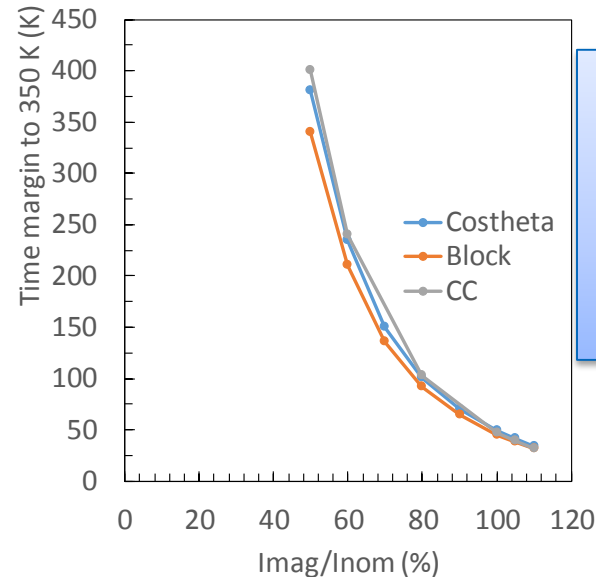
T_{max} vs. Protection delay at 105 %



Similar behaviour in all magnets

Time margin vs. current

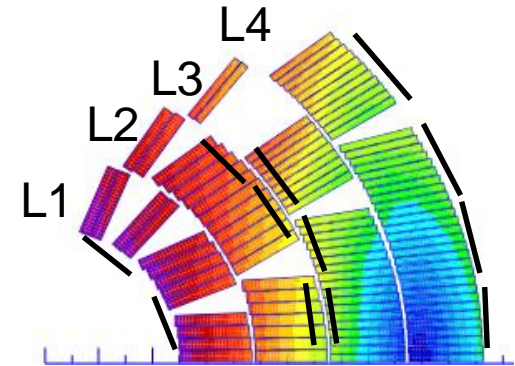
Time margin = protection delay that leads to given T_{max} (see E. Todesco, WAMSDO 2013)



Significant increase of reaction time at low current

3. $\cos\theta$ protection with heaters

- Realistic heater design, but not optimized
- Similar to LHC, LARP and HL-LHC technology:
 - 25 μm SS strips with Cu-plating
 - **75 μm polyimide insulation**
- Strip width: 10-14 mm
 - **Strips cover 70 turns out of 101**
- HS length: 3-6 cm, period: 15-35 cm
 - **HS cover 17-20% of turn length**
- **$P(t=0)$: 70 -100 W/cm², τ_{RC} : 30 ms**

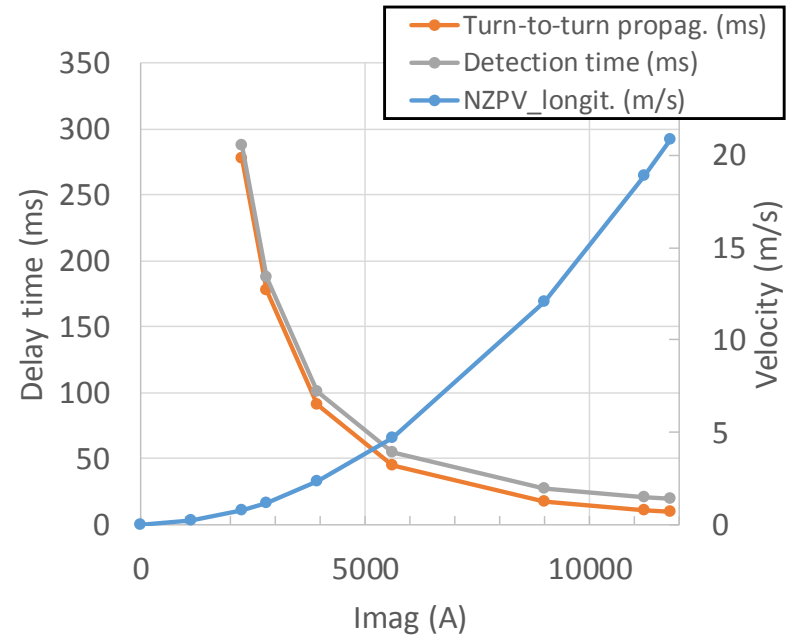


Approximate heater strip locations

HFU	450 V / 14 mF
Strips / coil	24
HFU circ. coil	8
Stored E / 2 ap.	45.4 kJ *
900 V units / 2 ap.	16

3. Hotspot temperature simulation assumptions

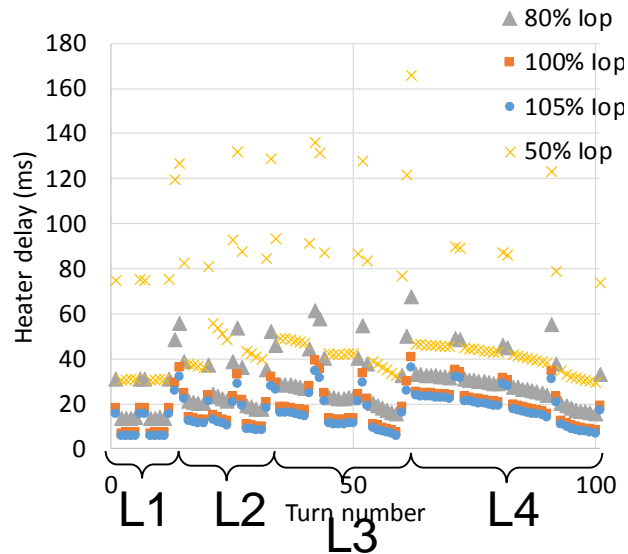
- 20 ms for quench detection (10+10ms)
- 20 m/s longit. NZPV, 10 ms turn-to-turn
 - QLASA: Average longit. 18 m/s, turn to turn: ~4-10 ms
 - Remember pre-heating from heaters!
- At lower current scaled proportionally to I_{mag}^2



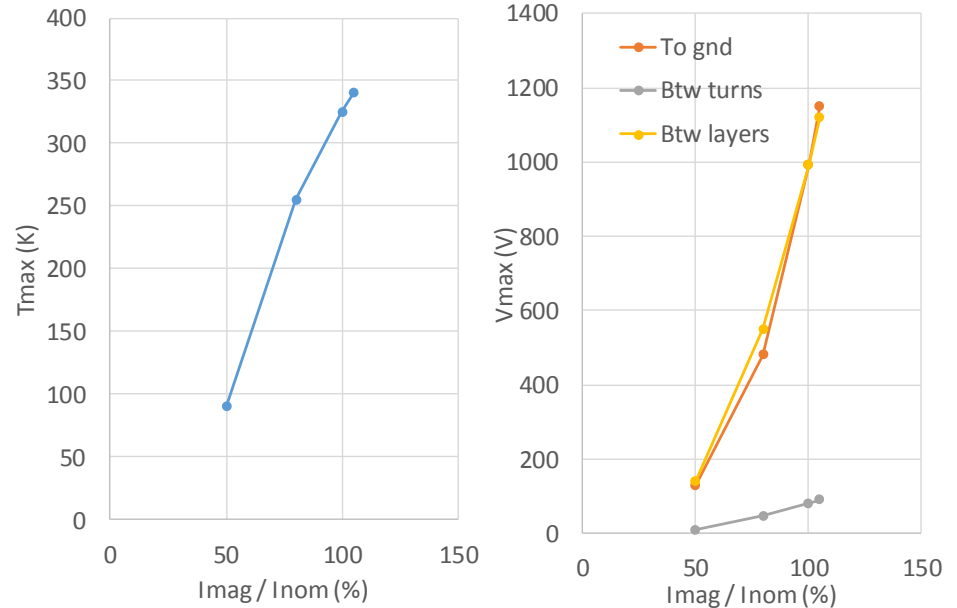
3. Results with heater based protection

Turn heater / quench delays

vs. I_{mag}



Hotspot temperature and voltages vs. I_{mag}

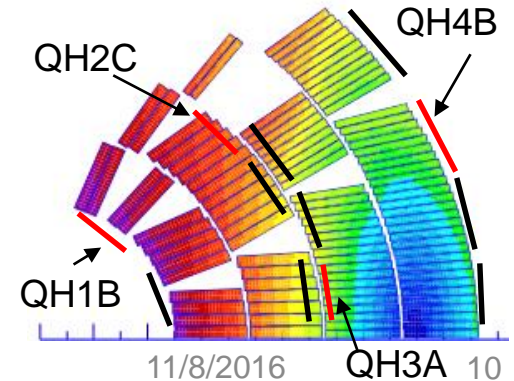


- ⇒ High current the most critical
- ⇒ Protection at all currents
- ⇒ Very small margin at high current

4. Failure scenarios at 105% I_{nom}

Failing strip in all coil halves	Strips failed	T_{max} (K)	V_{max} gnd (V)	V_{max} turns (V)	V_{max} layers (V)
Nominal	0	341	1150	90	1120
Fail1 QH1B	4	349	1070	100	1250
Fail2 All IL QH's	8	355	1000	100	1380
Fail3 QH2C	4	346	1100	100	1200
Fail4 QH2C and QH3A	8	366	1160	110	1110
Fail5 QH4B	4	355	1800	100	1100

If 4 strips / magnet fail: $T_{max} < 360$ K



4. Uncertainties...

- Heater delays:

- Assign heater delay to cable average field:

- $T_{max} = 364 \text{ K}$, $V_{\text{gnd}} = 1290 \text{ V}$, turns = 100 V, layers = 1360 V

- Material properties:

- Use MATPRO properties for current decay (NIST for heater delays):

- $T_{max} = 356 \text{ K}$, $V_{\text{gnd}} = 1480 \text{ V}$, turns = 110 V, layers = 1410 V

- Heater insulation:

- Increase heater insulation to 100 μm :

- $T_{max} = 356 \text{ K}$, $V_{\text{gnd}} = 1240 \text{ V}$, turns = 90 V, layers = 1050 V

Nominal:

$$\underline{T_{max} = 341 \text{ K}},$$

$$V_{max} \text{ to gnd} = 1150 \text{ V},$$

$$V_{max} \text{ btw turns} = 90 \text{ V},$$

$$V_{max} \text{ btw layers} = 1120 \text{ V}$$

4. ...Uncertainties

- Quench propagation velocity:

- NZPV longit. to 15 m/s:

- $T_{max} = 346 \text{ K}$, $V_{\text{gnd}} = 1160 \text{ V}$, turns = 90 V, layers = 1100 V

- NZPV longit. to 15 m/s AND turn-to-turn speed to 15 ms:

- $T_{max} = 353 \text{ K}$, $V_{\text{gnd}} = 1110 \text{ V}$, turns = 90 V, layers = 1090 V

Not enough margin...

Not easy to find significant improvements with small changes, but

Increasing NZPV longit to 40 m/s: $T_{max} = 334 \text{ K}$...
(Corrisponds to halving the periods)

Nominal:

$$\underline{T_{max} = 341 \text{ K}}$$

$$V_{max} \text{ to gnd} = 1150 \text{ V},$$

$$V_{max} \text{ btw turns} = 90 \text{ V},$$

$$V_{max} \text{ btw layers} = 1120 \text{ V}$$

To summarize

- Tmax vs. protection delay quite similar in all magnet options
 - **Time margin 40+/-2 ms in all options to 350 K at 105% I_{nom}**
 - Time margin increases exponentially at low current (340-400 ms at 50% I_{nom})
- In $\cos\theta$ heater-based protection shows potential, but a large number of HFU's may be needed for the redundancy and margin
- **To explore next: Heaters + CLIQ**
 - Heaters to complement CLIQ, analysis needed at all current levels
 - Waiting to use STEAM for this analysis

Appendix: Heater design

	Peak power, RC time constant	HS length / period	Strip width
QH3, QH2C	70 W/cm ² , 30 ms	6/30 cm	10 mm
QH4	100 W/cm ² , 30 ms	6/35 cm	14 mm
QH1 and QH2A-B	70 W/cm ² , 30 ms	3/15 cm	10 mm

4 HFU circuits:

- 1B || 1A || 2A || 2B
- 2A || 3A || 3B || 3C
- 4A || 4B
- 4C || 4D

