



# Parametric Study on the Thermal Performance of Beam Screen Samples of the High-Luminosity LHC Upgrade

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# Outline

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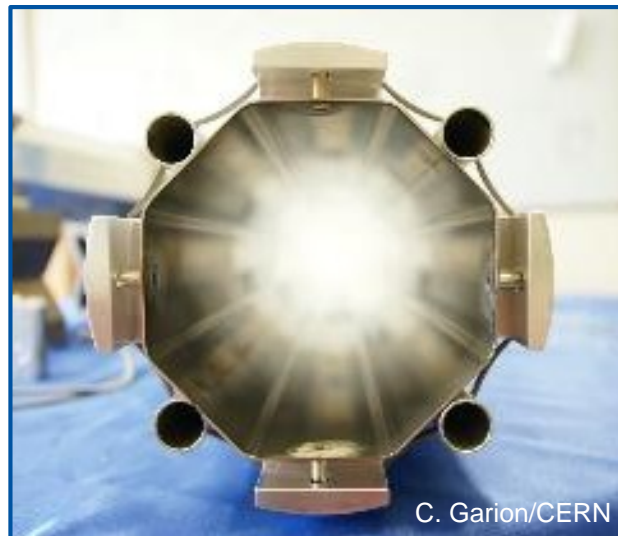
- High-Luminosity LHC upgrade
- Beam screens for the insertion regions
- Experimental test set-up
- Sample geometry
- Results: beam screen thermal pathways
- Results: supporting structure conductance
- Concluding remarks

# From the LHC to the HL-LHC



## LHC beam screen

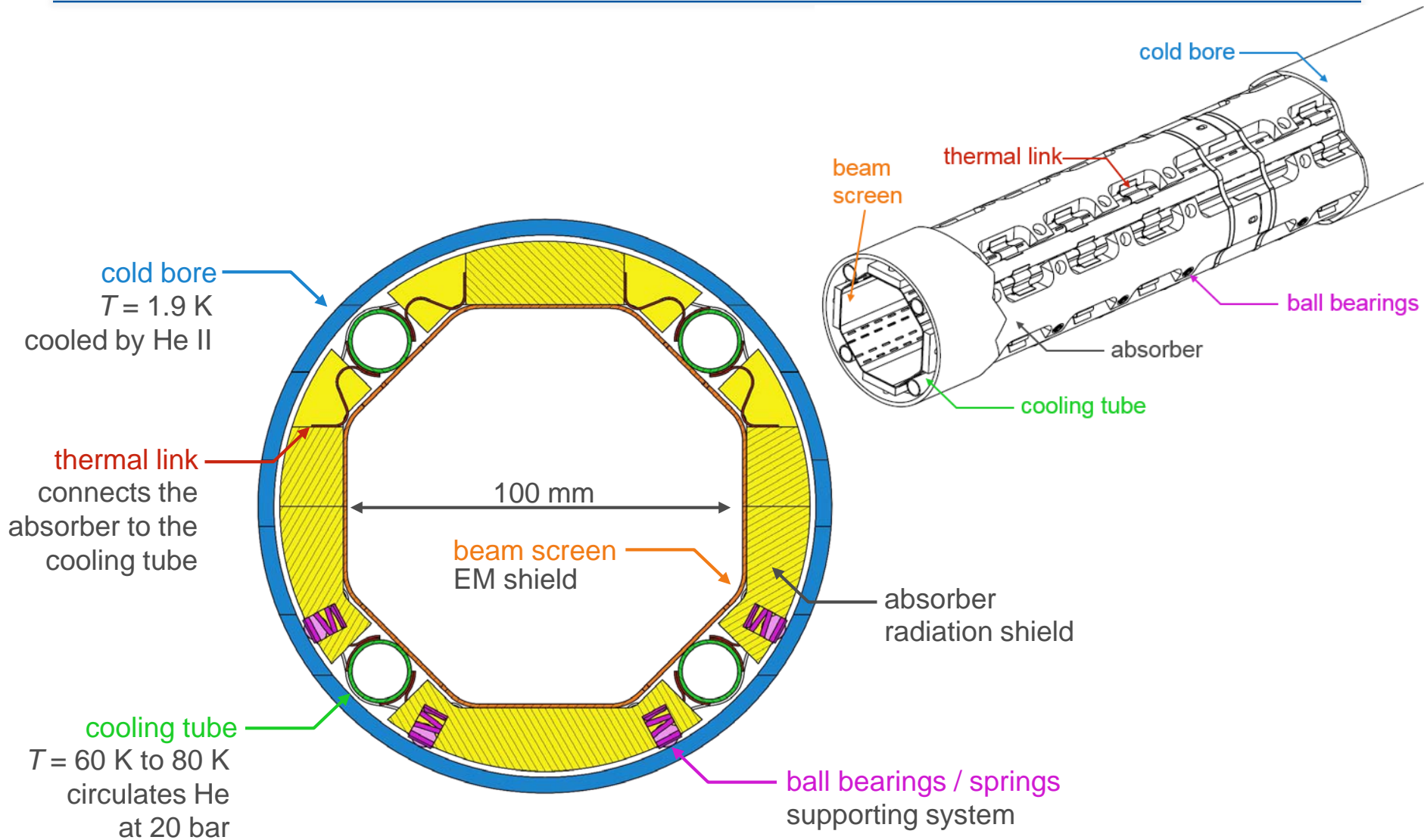
- 4 – 20 K operating  $T$
- Low mass flow (1 g/s)
- Supercritical He at 3 bar
- No absorber (just screen)



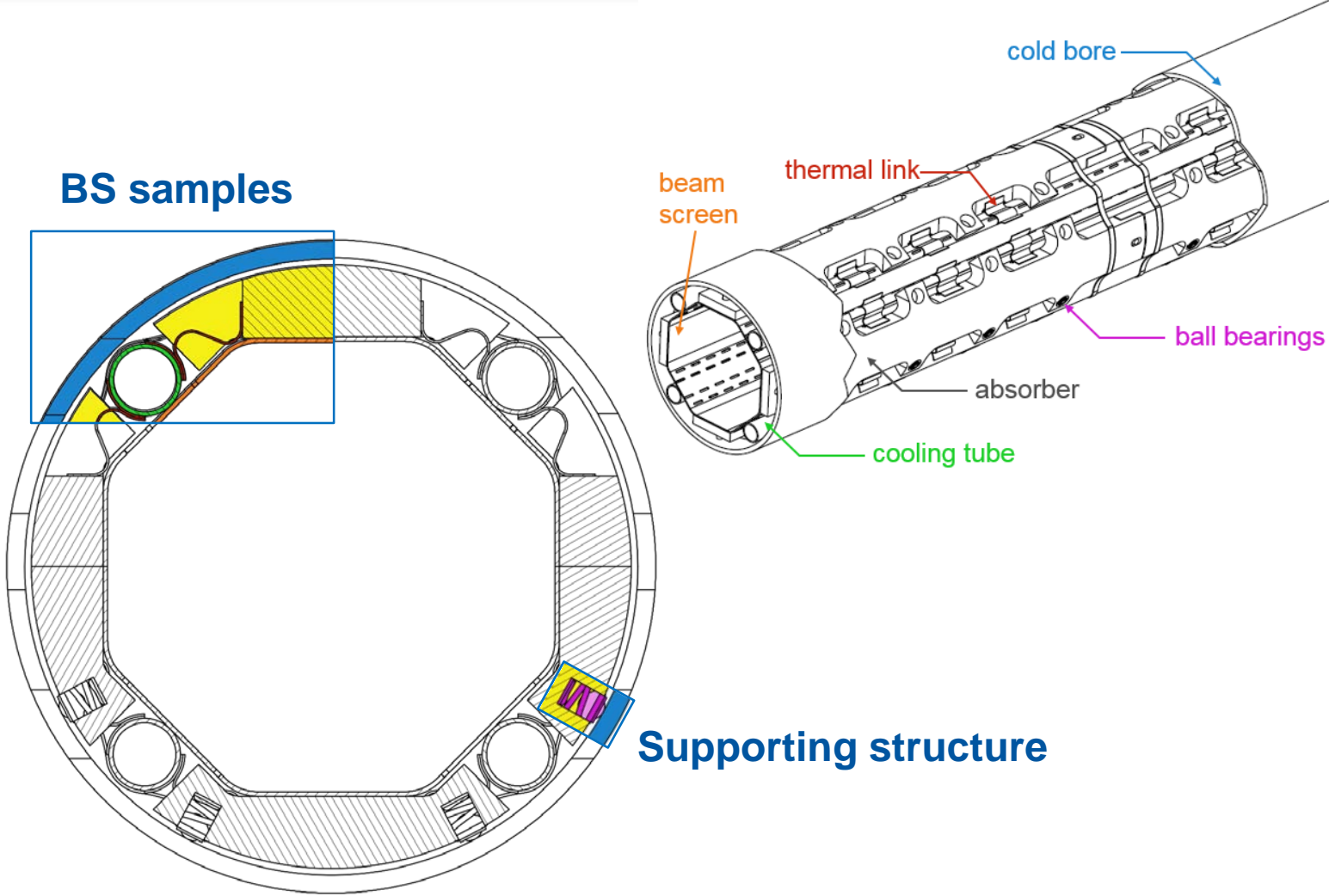
## HL-LHC beam screen

- 60 – 80 K operating  $T$
- High mass flow (10 g/s)
- Supercritical He at 20 bar
- Tungsten-based absorber

# HL-LHC beam screens



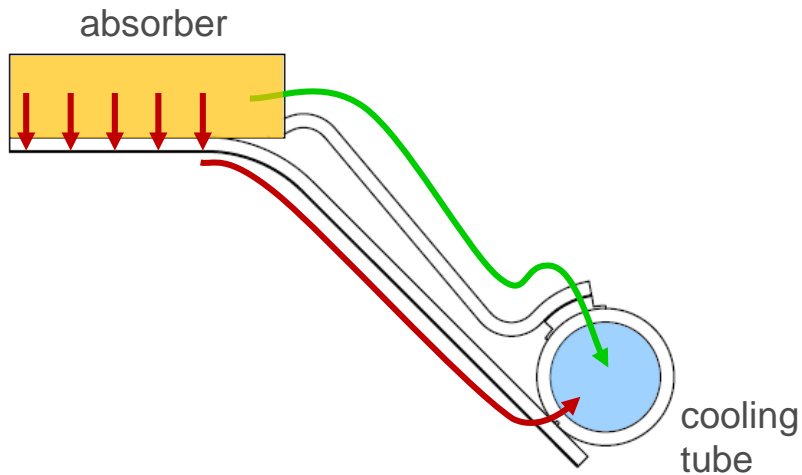
# HL-LHC beam screens



# Scope of thermal performance studies

## BS samples:

- Characterise two thermal pathways
  - Through the beam screen
  - Through the thermal link
- Requirements:
  - No max.  $T$  defined for absorber
  - Max  $\Delta T$  between heat sink and inner beam screen surface of 5 K

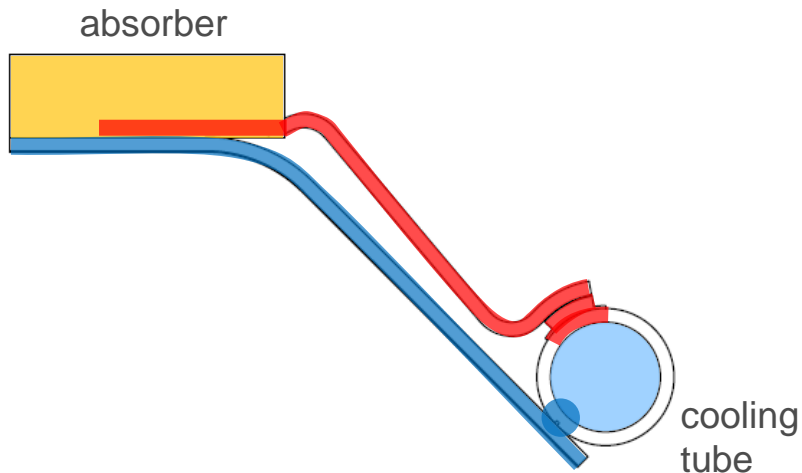


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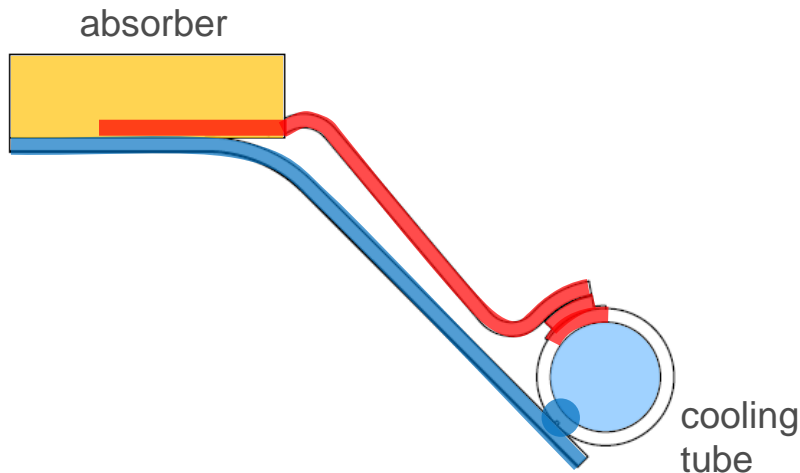




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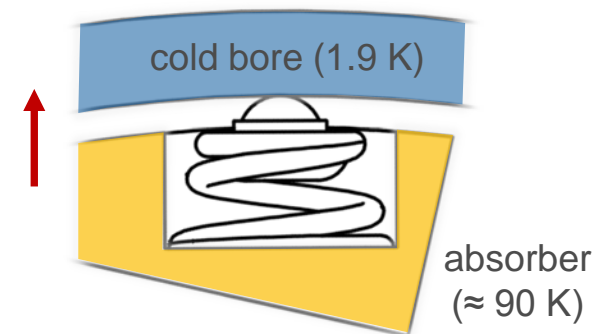
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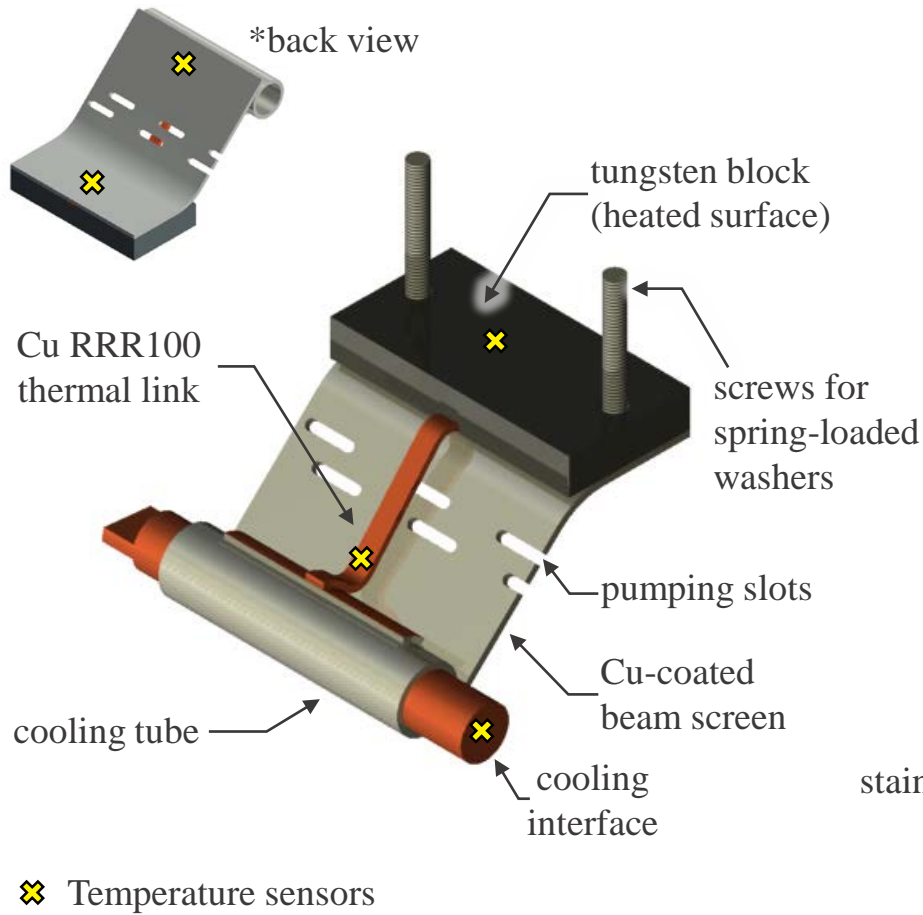


## Supporting structure:

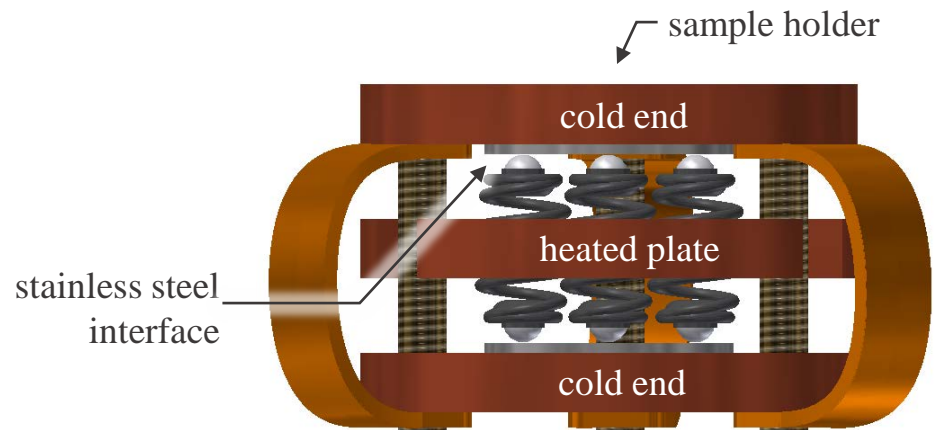
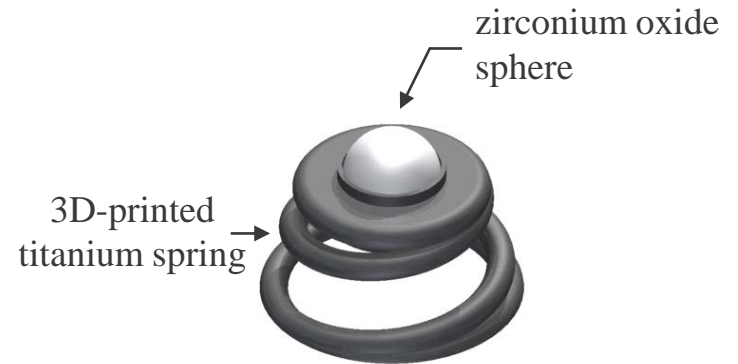
- Characterise heat transfer from beam screen to cold bore by conduction
- Requirements:
  - Total heat load transferred (conduction+ radiation)  $< 500$  mW/m of beam screen



# Sample geometries and test set-up

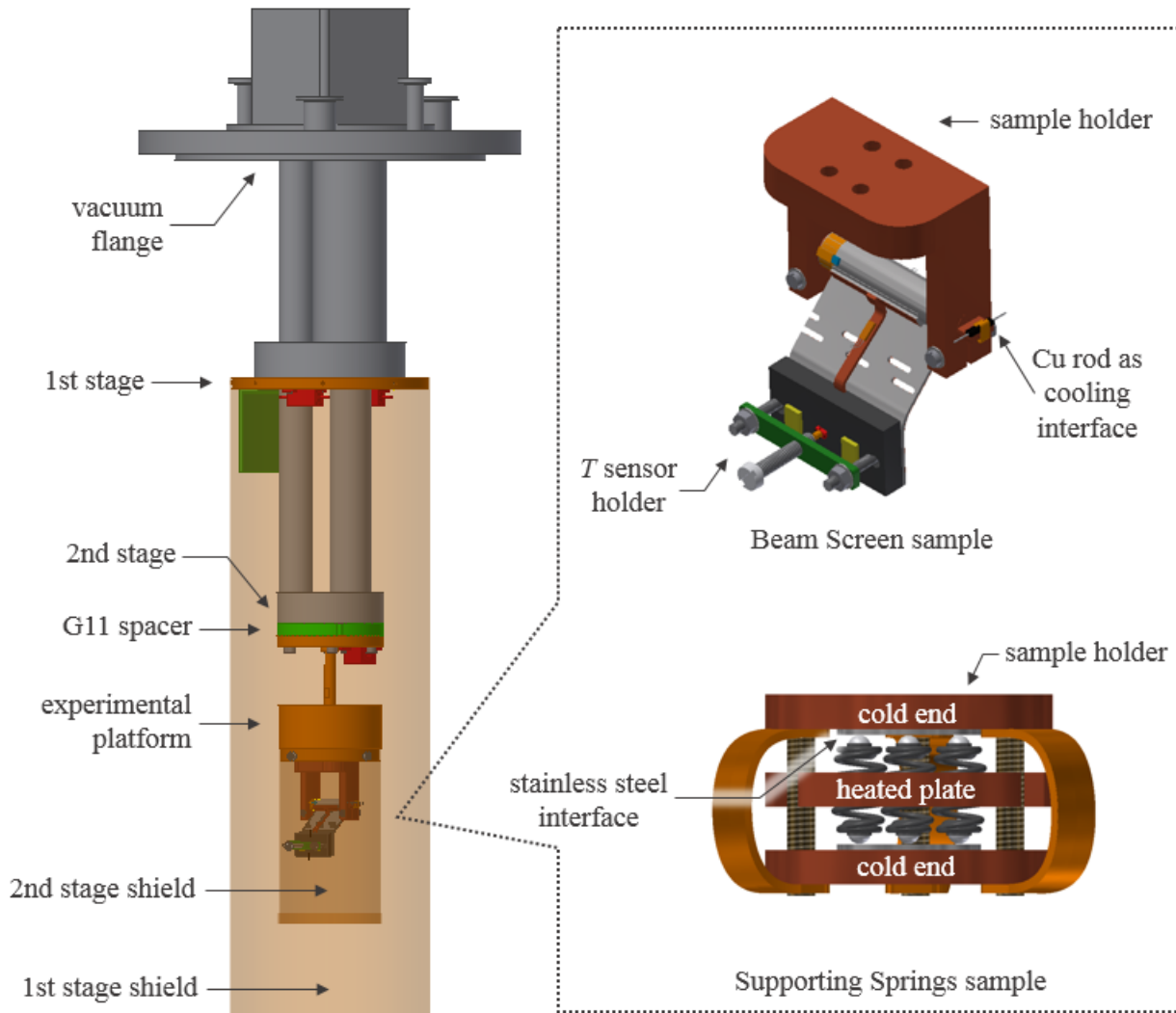


Beam Screen sample



Supporting Springs sample

# Experimental set-up



## BS samples:

- Base temperature varied from 50 K to 80 K
- Heat load varied from 0 to 400 mW (0 to 25 W/m)
- Tungsten block-beam screen compression 0 and 1.82 N

## Supporting structure:

- Base (cold) temperature kept between 2.7 K and 3 K
- Warm end heated up to 100 K
- 7.5 N (nominal) and 15 N compression

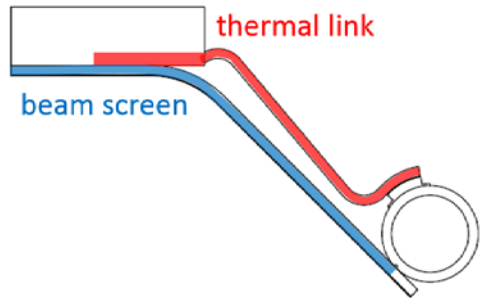
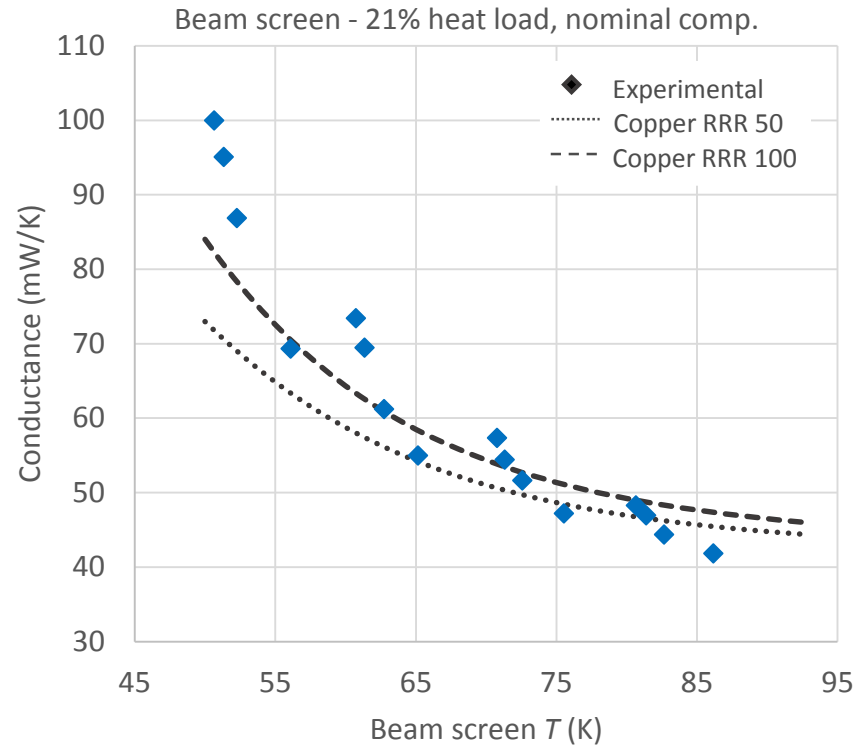
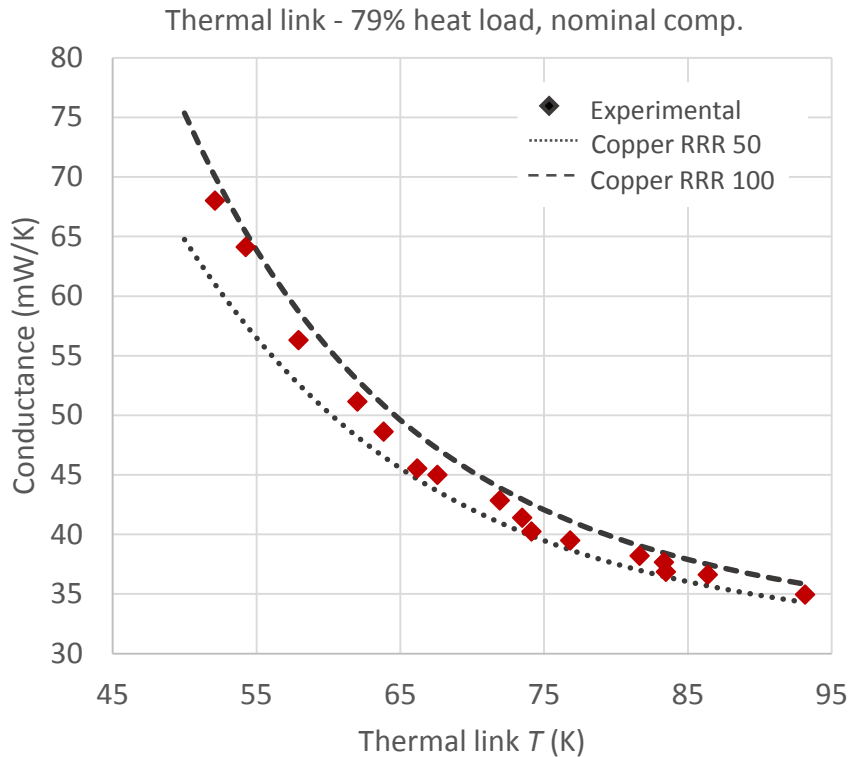
# Results – Beam screen sample

- Maximum temperature increase of relevant beam screen components was measured for a Q2-type magnet, heat load 15 W/m

	Nominal compression		No compression	
Base $T$ (K)	W block $\Delta T$ (K)	Beam screen $\Delta T$ (K)	W block $\Delta T$ (K)	Beam screen $\Delta T$ (K)
$60.00 \pm 0.16$	$14.00 \pm 0.06$	$3.20 \pm 0.04$	$13.50 \pm 0.06$	$2.20 \pm 0.04$
$75.00 \pm 0.23$	$14.00 \pm 0.09$	$3.40 \pm 0.03$	$13.50 \pm 0.09$	$2.30 \pm 0.03$

- Temperature difference between the inner surface of beam screen and the cooling source kept below the 5 K threshold
- Tungsten block reaches a maximum temperature of  $75 + 14 = 89$  K at the nominal heat load towards the high temperature end

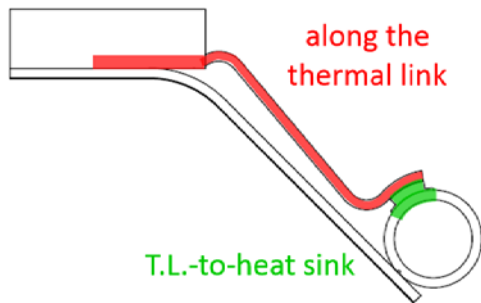
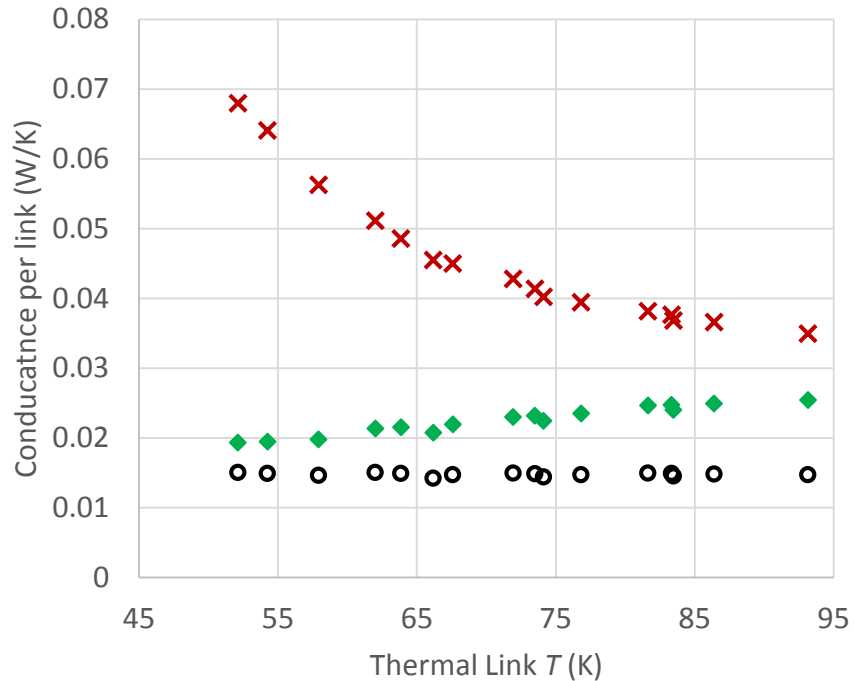
# Results – Beam screen sample



- Nominal compression: 79% heat load flows to the heat sink through the thermal link, 21% through the beam screen
- No compression: 89% through TL, 11% through BS

# Results – Beam screen sample

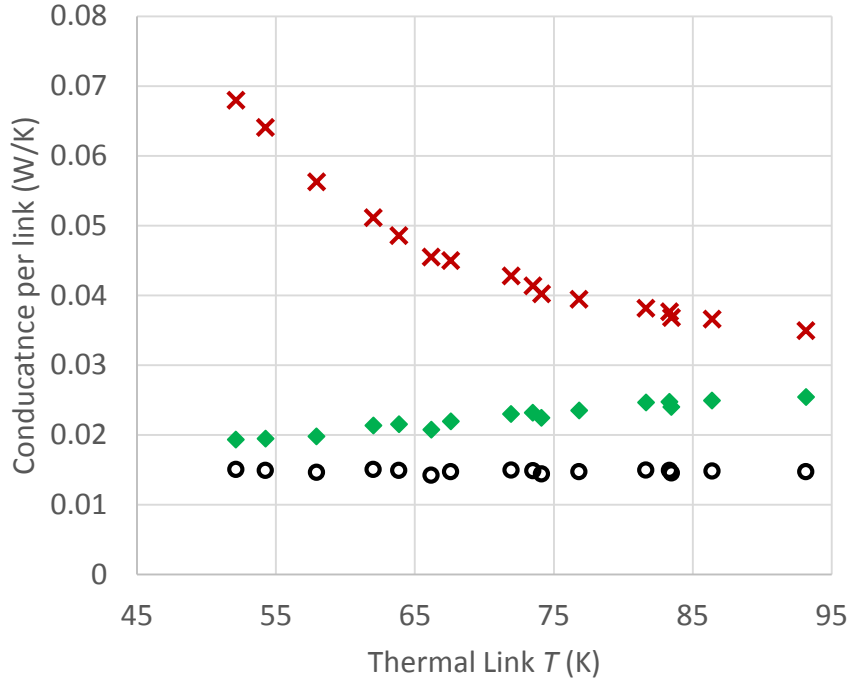
Thermal link pathway - 79% heat load, nominal comp.



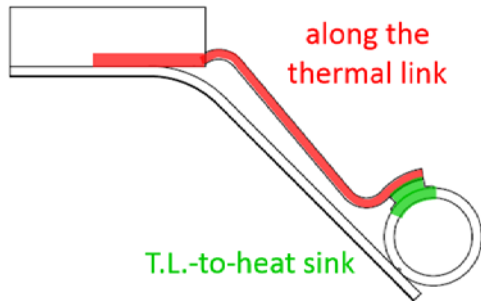
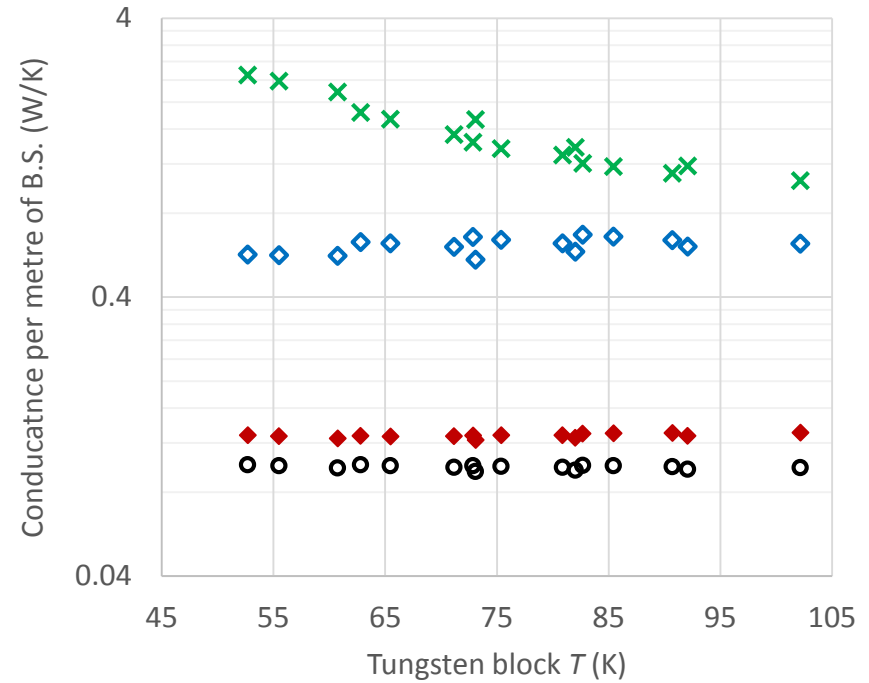
- ◇ Thermal link to heat sink
- × Along the thermal link
- Overall conductance

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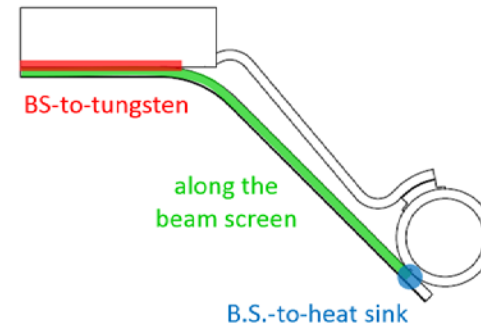
Thermal link pathway - 79% heat load, nominal comp.



Beam screen pathway - 21% heat load, nominal comp.

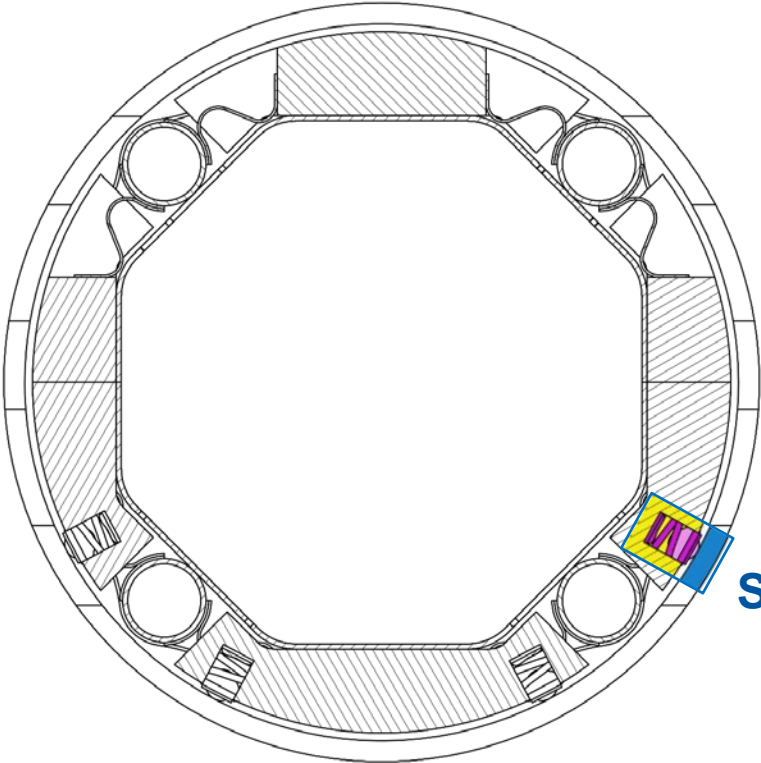


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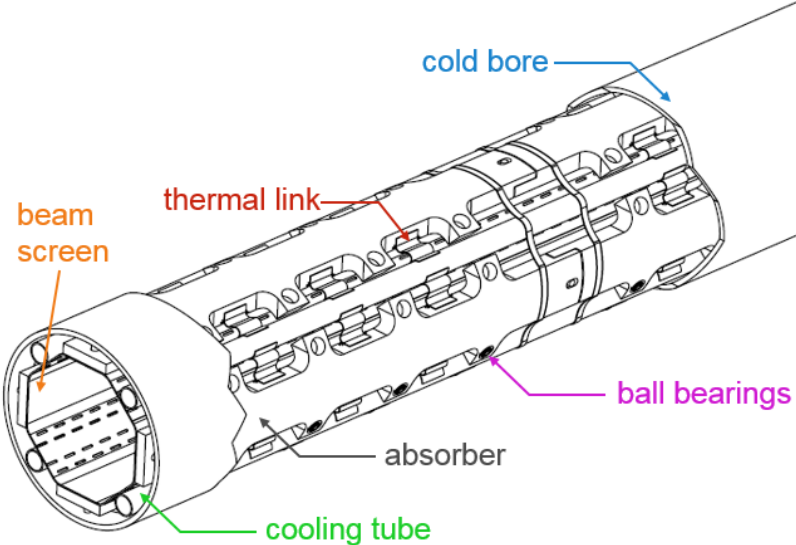


- ◇ B.S. to heat sink interface
- ◆ B.S. to tungsten interface
- × Along the beam screen
- Overall conductance

# Supporting structure – Q2 assembly

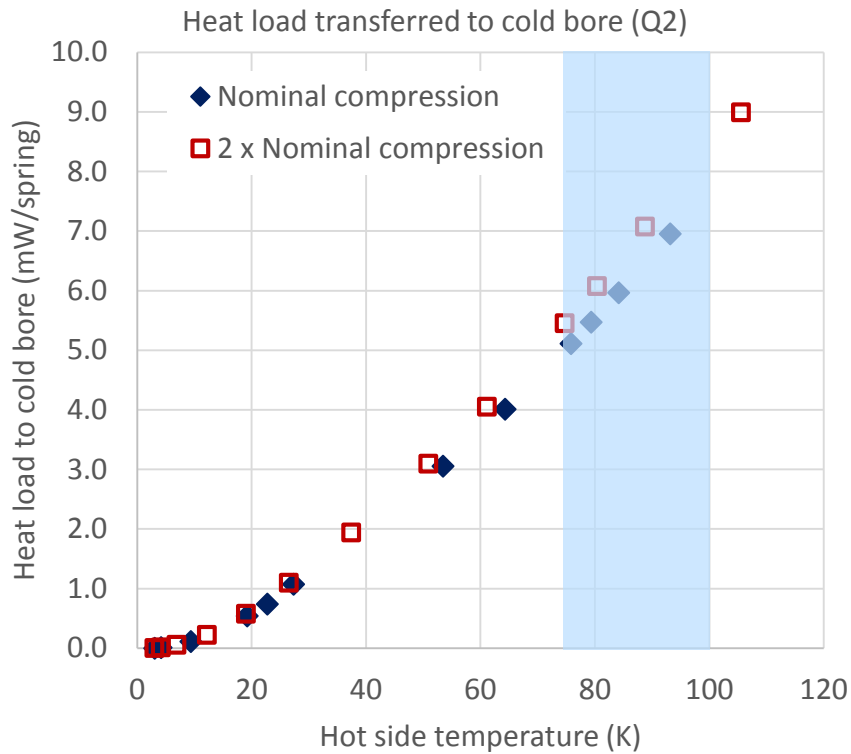


Supporting structure





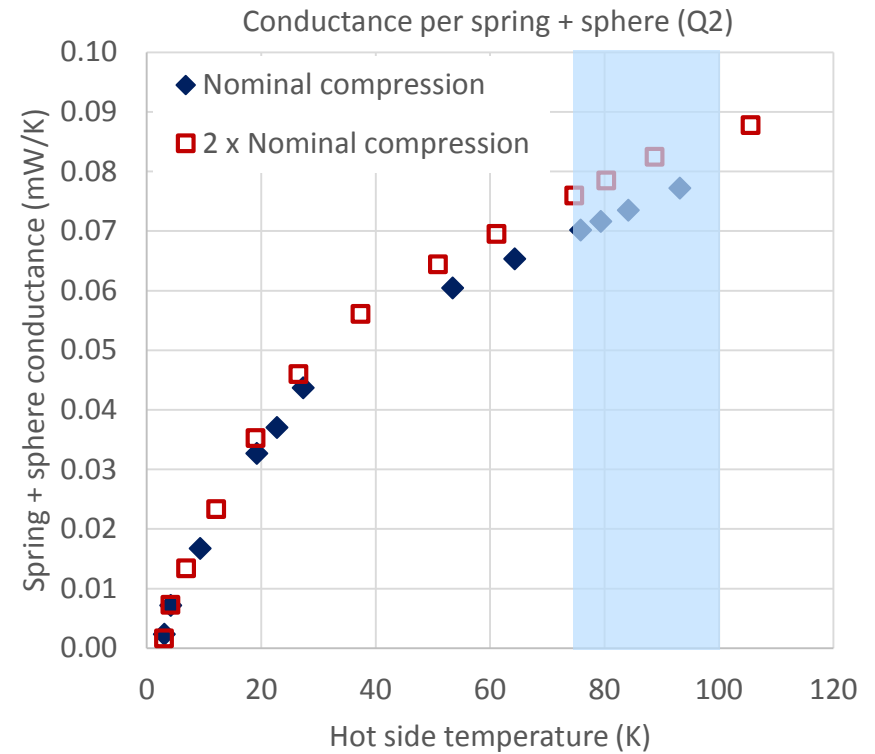
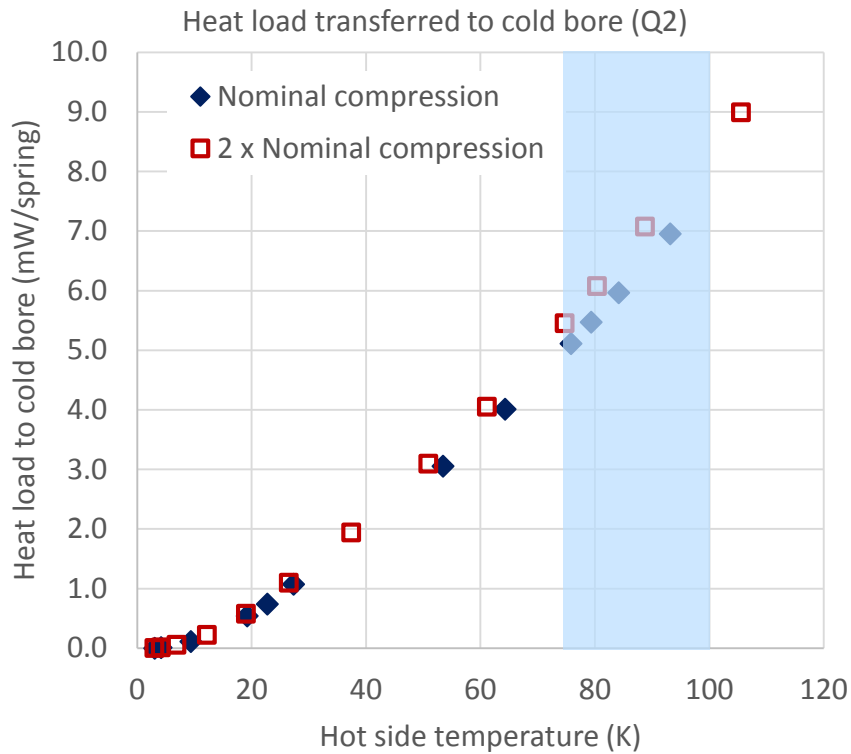
# Supporting structure – Results for Q2 assembly



- Nominal compression: 7.5 N
- 80 spring+sphere sets per metre of beam screen → 560 mW/m



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# Summary

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## Beam screen thermal link at the nominal heat load of 15 W/m:

- Maximum  $T$  of tungsten block is 89 K (14 K gradient to cooling tube)
- $\Delta T$  between the cooling fluid and the inner surface of the beam screen kept below 5 K
- Results similar for nominal (1.82 N) and no compression
- Major thermal pathways have been analysed and design validated, and agree with simulations

## Spring support structure to cold bore:

- Conductance around 0.08 mW/K for the 75 K – 95 K range to 3 K
- An average of 560 mW per metre of beam screen needs to be considered
- Little influence of compression force (less than 10%)



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