





PSB longitudinal painting: concept and control

Vincenzo Forte, TE/ABT/BTP

Acknowledgements: B. Mikulec, C. Carli, E. Benedetto, J. Sanchez





Outline

Longitudinal painting concept

- > The process
- Physical parameters
- Present hardware limitations
- > A longitudinal painting control algorithm
- Summary and next steps



The process

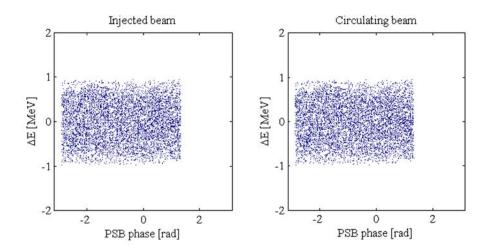


> Multi-turn **un-modulated energy** injection

- The L4 bunch trains arrive to the PSB with the same central energy E₀ = 160 MeV
- The rms energy spread δE is usually large (~400-450 keV) to compensate peaks of line density

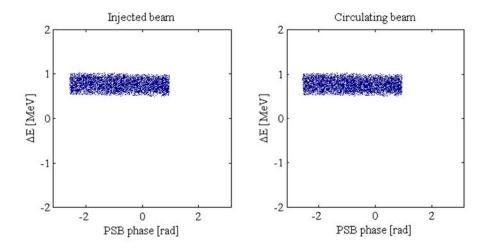
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> The chopping factor is fixed (~60%)



Multi-turn longitudinal painting

- The L4 bunch trains arrive to the PSB with different (turn-by-turn) central energy arou E₀ = 160 MeV
- The rms energy spread δE is fixed (120-250 keV)
- The chopping factor is varying to follow the longitudinal iso-Hamiltonian contours for a give longitudinal emittance.





The process

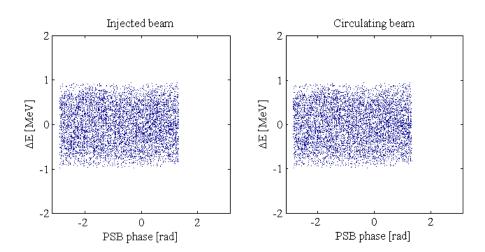


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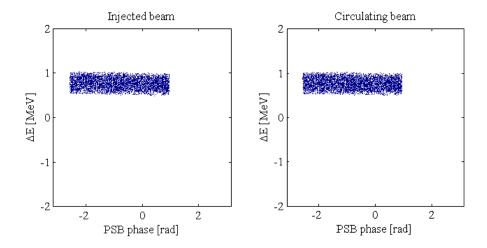
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Physical parameters



> The rms energy spread δE

- · Imposed by the de-buncher
- Fixed during the injection process

The central energy E₀(t)

- Imposed by the last two PIMS
- · Can be swept turn-by-turn at injection

The central energy sweeping rate dE₀(t)/dt

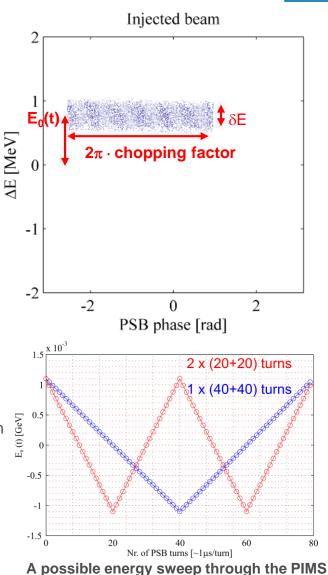
 Imposed by the last two PIMS → change of phase and, thus, power requested to the de-buncher

➤ The chopping factor (≤1)

- Imposed by the chopper
- · Rations the effective current/turn at the PSB entrance
 - I_{eff}(t) = chop. factor × unchopped current = chop. factor × 40 mA
- Can be modulated turn-by-turn at injection
- Determines the number of turns to be injected for any given target intensity

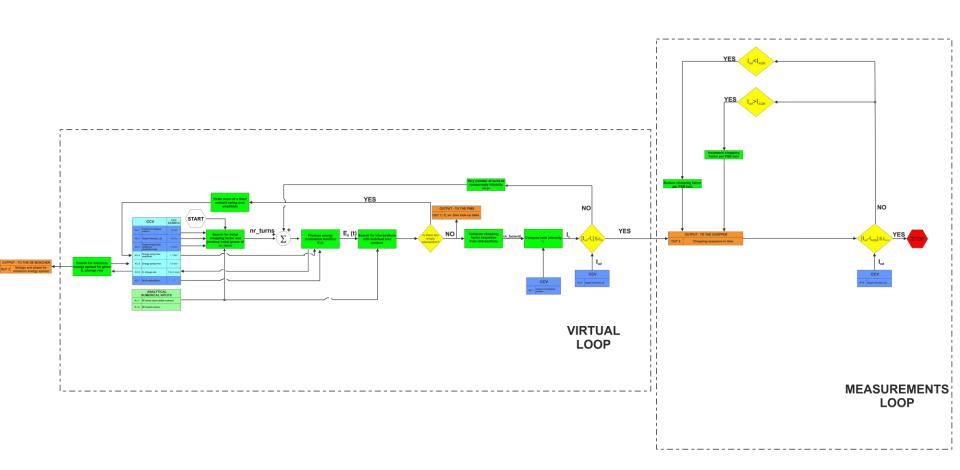
The number of injectable turns

• Is limited by the BI.DIS at <150 per PSB ring





A longitudinal painting control algorithm

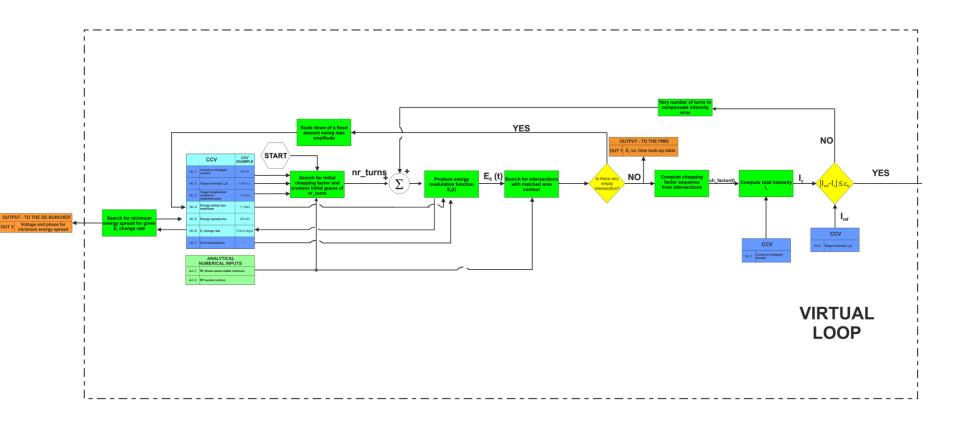


PSB Upgrade





- > The virtual loop, from the inputs, is an algorithm to set the HW through:
 - Chopping factor sequence (chopper)
 - Energy swing function (PIMS)
 - Energy-spread (de-buncher)



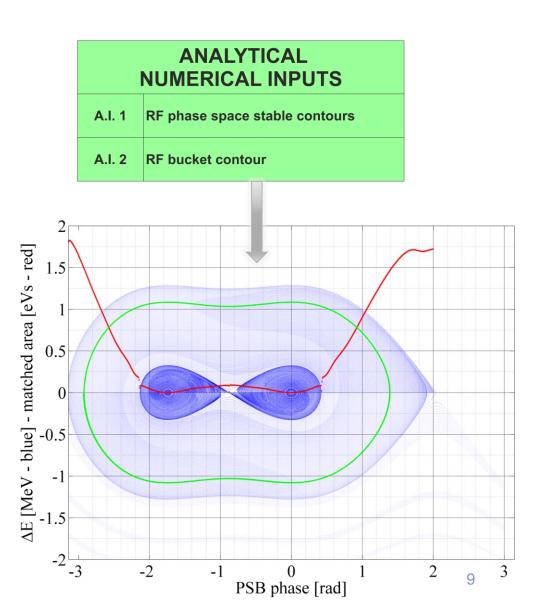




CCV		CCV EXAMPLE
H.I. 1	Linac4 un-chopped current	40 mA
H.I. 2	Target intensity I _{ref} (t)	1.6e13 p.
H.I. 3	Target longitudinal emittance (matched area)	1.5 eVs
H.I. 4	Energy swing max amplitude	1.1 MeV
H.I. 5	Energy spread rms	120 keV
H.I. 6	E₀ change rate	5.5e-6 deg/s
H.I. 7	Nr.of modulations	1

Fixed inputs Variable inputs

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HW outputs



OUTPUT - TO THE DE-BUNCHER OUT 3 Voltage and phase for

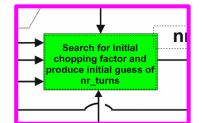
minimum energy spread

OUTPUT - TO THE PIMS

OUT 1 E₀ vs. time look-up table

OUTPUT - TO THE CHOPPER		
OUT 2	Chopping sequence in time	

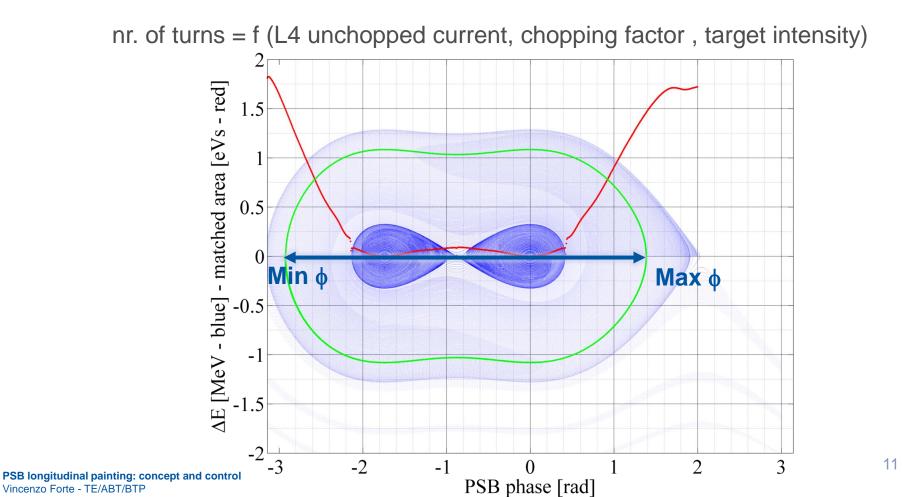




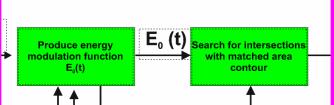


> First guess of the chopping factor \rightarrow initial nr. of turns (<u>under-estimated!</u>)

Initial chopping factor = $(Max \phi - Min \phi)/2\pi$







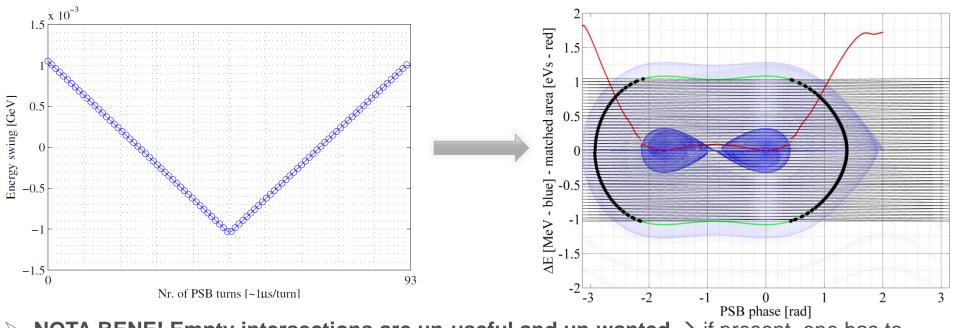


Estimation of the energy modulation function for the PIMS (e.g. triangular waveform)

energy_modulation= f(nr turns, nr of modulations, amplitude)

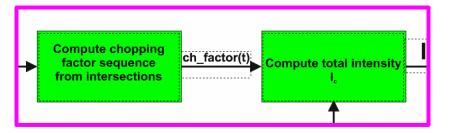
The intersections of the energy swing function with the target contour determines the portion of the L4 pulse that has to be retained at every PSB turn





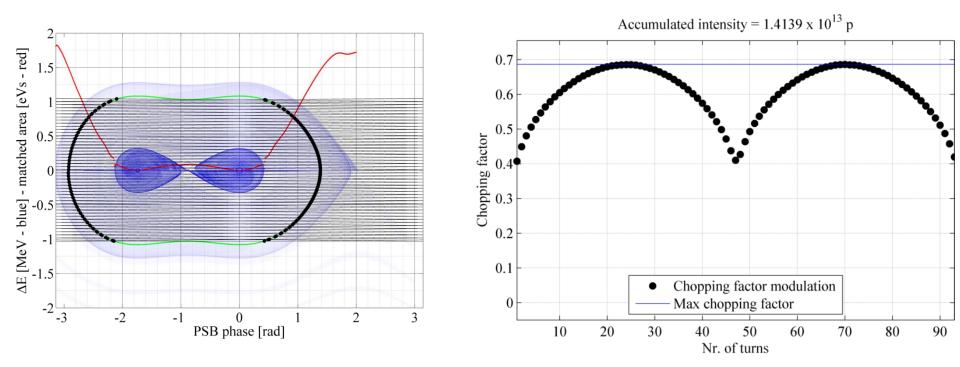
> NOTA BENE! Empty intersections are un-useful and un-wanted → if present, one has to scale down the PIMS amplitude in feed-back by a small amount



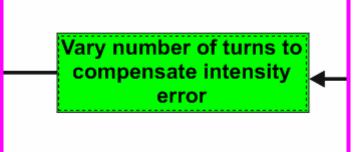




For convexity of the phase edges of the longitudinal iso-Hamiltonian contours, the chopping factor modulation causes the accumulated intensity to be lower than the reference intensity (1.4139e13 < 1.6e13 p.)</p>

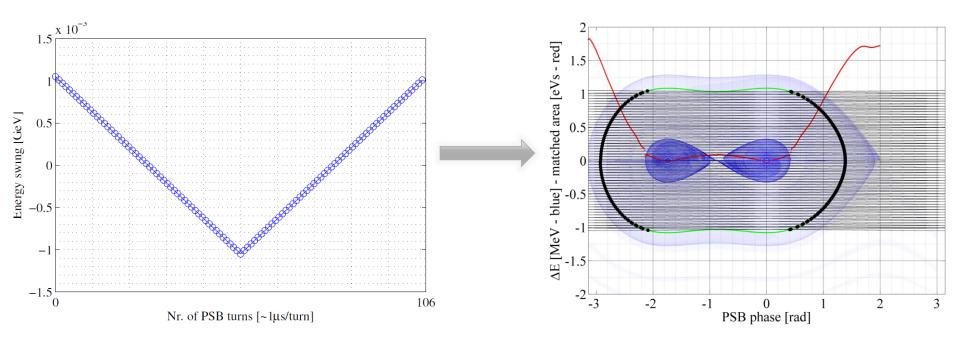




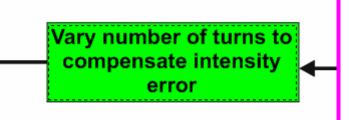




An iteration (feed-back) is needed to compensate the intensity difference → More turns are needed (from 93 to 106!) → Slower energy modulation



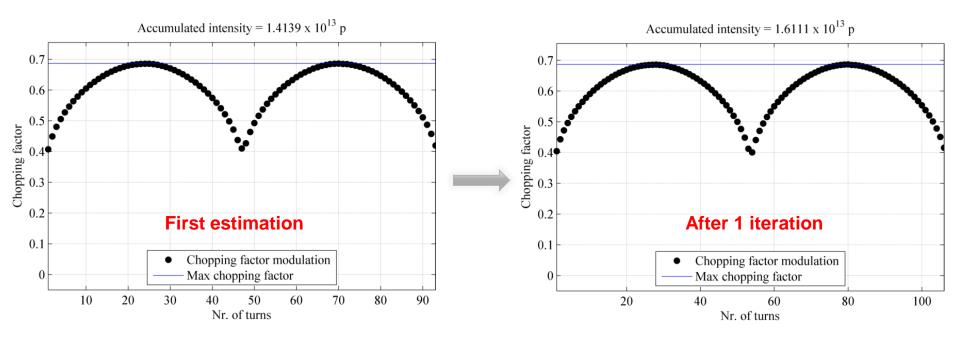






After 1 iteration the estimated intensity is reasonably close to the target value (1.6111e13 ~ 1.6e13 p.)

 \rightarrow The chopping factor pattern period becomes <u>slower</u>

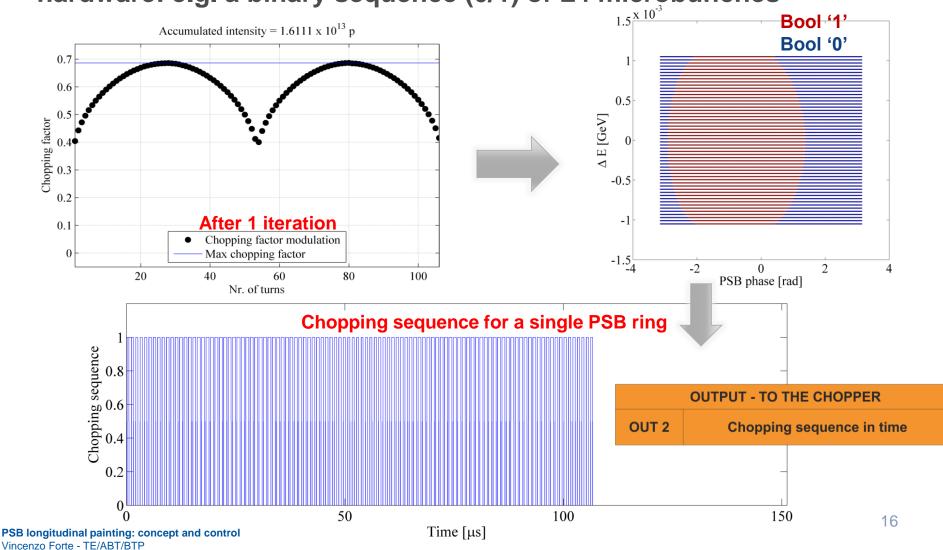




PSB Upgrade



The chopping pattern must be translated in information for the chopper hardware: e.g. a binary sequence (0/1) of L4 microbunches



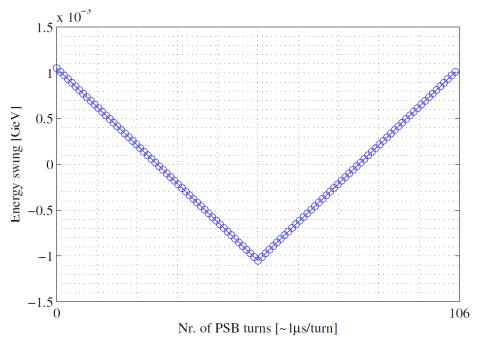




OUTPUT - TO THE PIMS

OUT 1 E₀ vs. time look-up table

The E₀ swing function could be translated in form of GFA (look-up table) for the PIMS cavities (11+12) regulations.



> The swing rate (dE_0/dt) depends on the wanted energy spread by the de-buncher and by the power (available) at the de-buncher cavity.





OUTPUT - TO THE DE-BUNCHER OUT 3 Voltage and phase for minimum energy spread

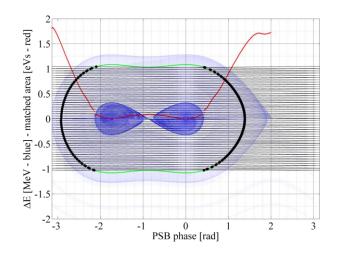
- The de-buncher is needed to generate different energy spreads at the entrance of the PSB.
- The voltage and the phase must be defined <u>once</u>, respecting the present hardware limitation constraints.
- The minimum energy spread achievable strictly depends on the E₀ sweep rate (imposed by the PIMS)
- NOTA BENE! For a finest painting, the smaller the energy spread, the better! → We aim to use ~100 keV rms at the entrance of the PSB
 → max E₀ sweep rate of 5.5 deg/s (limits the number of PSB turns to achieve given intensity)
- The correlation between de-buncher phase and energy spread at given voltage is foreseen during the commissioning in the LBS line.

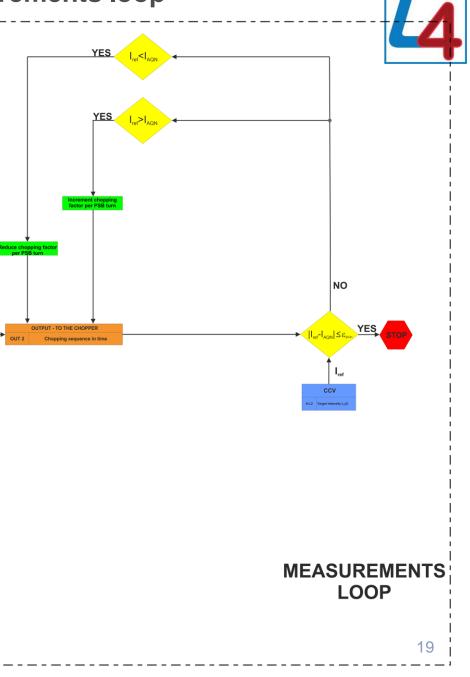
The measurements loop

PSB Upgrade

- The measurements loop acts in a smart way on the chopping factor sequence in case the measured intensity at a certain time marker soon after injection differs from the desired one
- E.g. 'Smart' way: random reduction or increment of the chopping factor per turn to minimize the mismatch with target contour.

From virtual loop







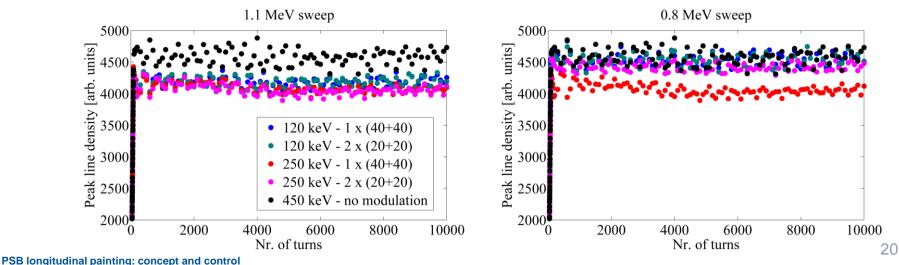
Next: longitudinal painting quality figures of merit



- The historical reasons for the painting in the PSB with L4 have always been related to space charge reduction.
- We might need another loop to control a specific figure of merit.
- Suggestion: instead of pointing at target longitudinal emittance, shall we point to the contour with lowest peak line density amplitude and beating in time?
- > Peak line density
 - An advantage of the longitudinal painting is to lead to a <u>SMALLER</u> peak line density (10%), compared to the un-modulated energy case.

$$\Delta Q_y = -\frac{r\lambda}{2\pi e\beta^2 \gamma^3} \oint \frac{\beta_y(s)}{\sigma_y(s) \left[\sigma_x(s) + \sigma_y(s)\right]} \, ds$$

Simulations for future ISOLDE beams



Vincenzo Forte - TE/ABT/BTP



Summary and next steps



- The longitudinal painting technique for the new L4 to PSB injection has been initially proposed by C. Carli and R. Garoby, as an elegant and efficient way to reduce longitudinal filamentation, thus bunch shape (bunching factor) beating from the very beginning.
- > An introduction to the longitudinal painting process and control has been given.
- > The longitudinal painting has the advantage to control the longitudinal plane with **high flexibility**, as we will do with the painting in the transverse plane.
- It gives the possibility to implement in a very controlled way different longitudinal (and also exotic, e.g. hollow bunches) beam phase spaces.
- A 'simple' control algorithm, totally generic (for any given RF bucket shape) has been proposed
- > <u>This algorithm could work also for the un-modulated injection</u>, as this last is a particular case of injection with $E_0(t)=0$
- The longitudinal painting is foreseen only at a late stage of the commissioning, so this is the moment to make brain storming and propose ideas for its realization.



Next steps



- > Missing implementative details:
 - > Timing
 - Control
 - >
- Control tolerances and quality indexes
- Interlocks
- Suggestions?



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