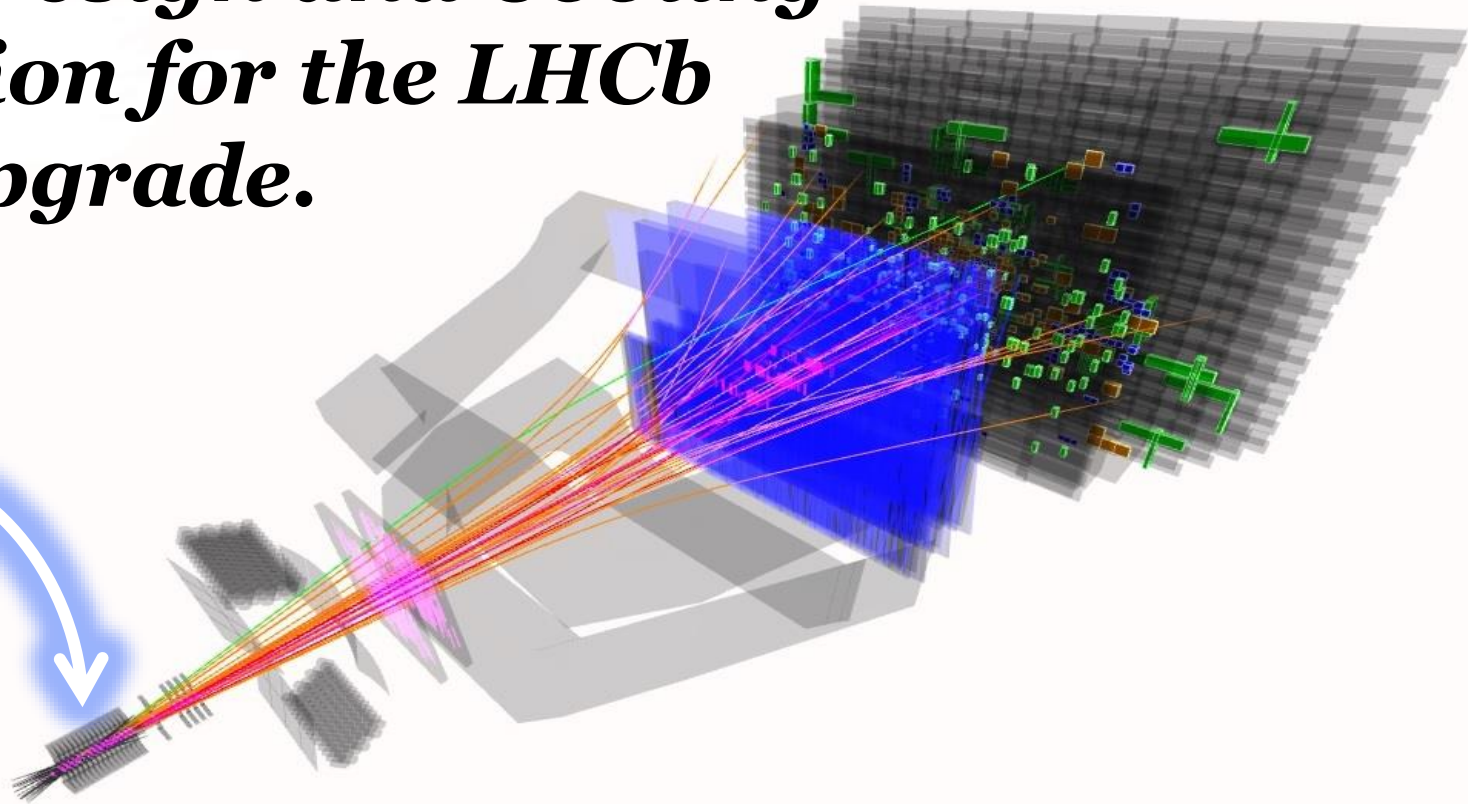


# *Module Design and Cooling Integration for the LHCb VELO Upgrade.*



**Wiktor Byczyński on behalf of the VELO group**

**Forum on Tracking Detector Mechanics  
Marseille 2017**

## Introduction:

### Current VELO and Upgrade:

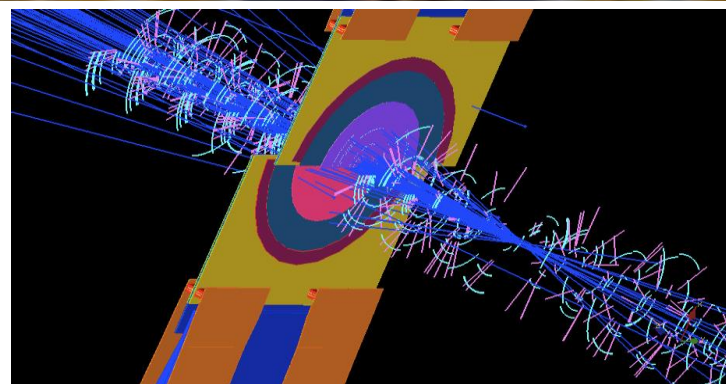
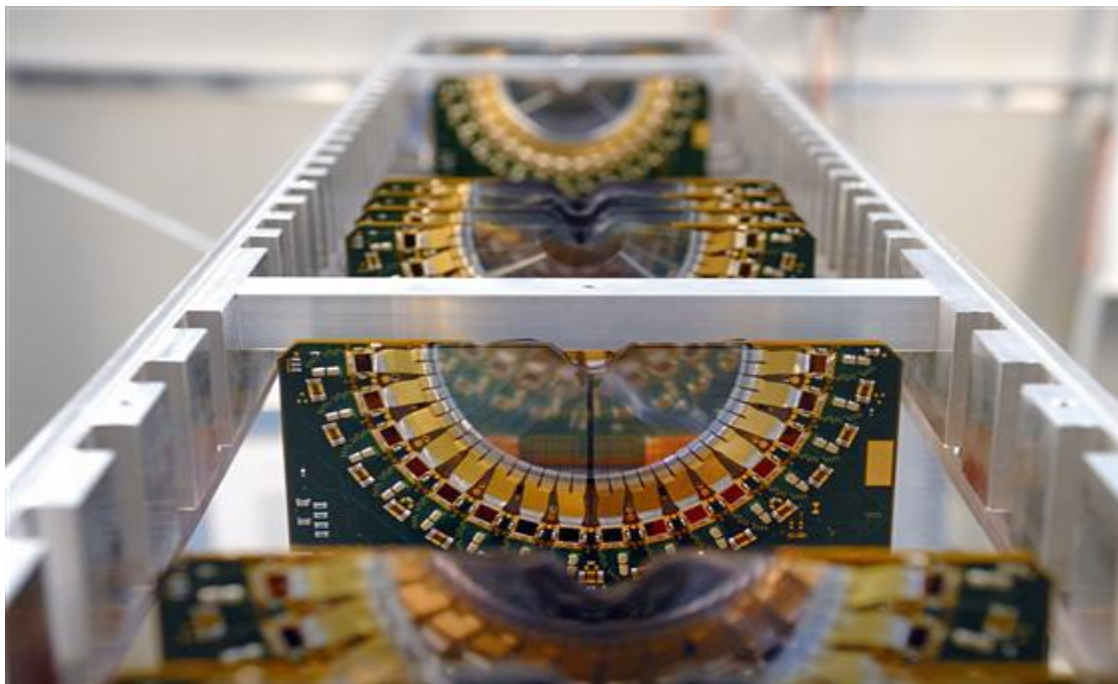
- **Module Design**
- **Cooling substrate:**
  1. **Microchannels:**
    - **Design**
    - **Attachment of the fluidic connector**
    - **Reliability tests of the solder joint**
    - **Fluidic characterization**
    - **Boiling stability**
  2. **Alternative plan: Ceramic substrate**
    - **Design**
    - **Constraint system**
    - **Fluidic characterization**

## Conclusion

# Current VELO Detector

## VELO:

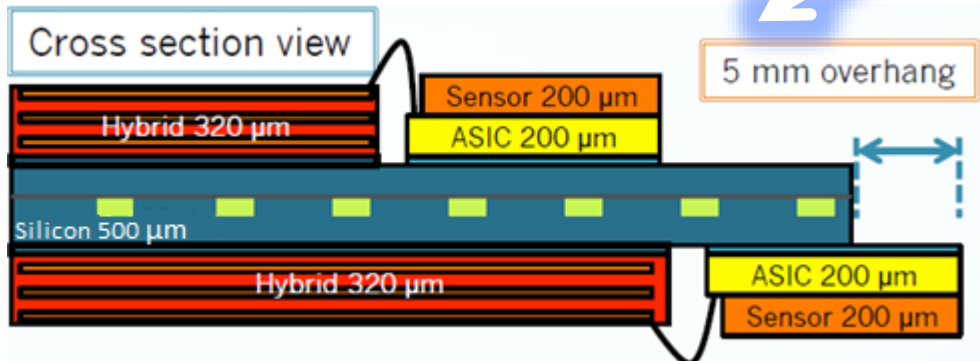
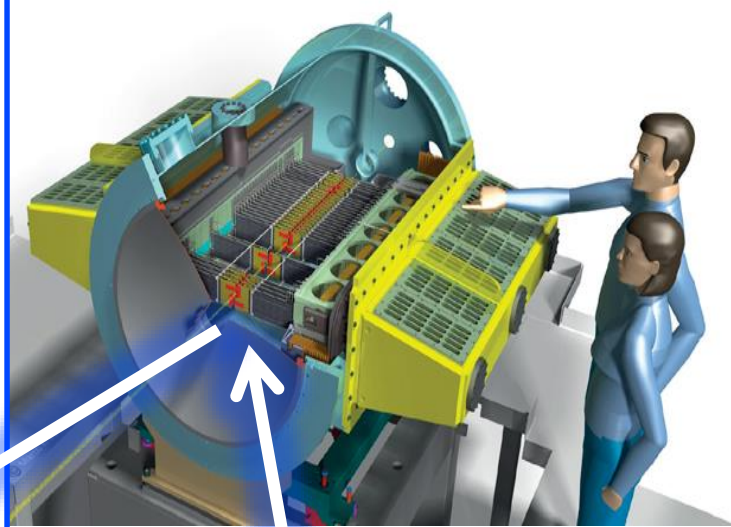
- Vertex reconstruction and tracking
- 88 Si-strip sensors surrounding the interaction point
- Modules are moved away during the beam injection
- Excellent impact parameter resolution (down to 11.6 [ $\mu\text{m}$ ])
- Excellent single hit resolution  $\sim 4$  [ $\mu\text{m}$ ]
- $\sim 16.5$  [W/module]



Performance of the LHCb Vertex Locator - arXiv:1405.7808

# New VELO Detector

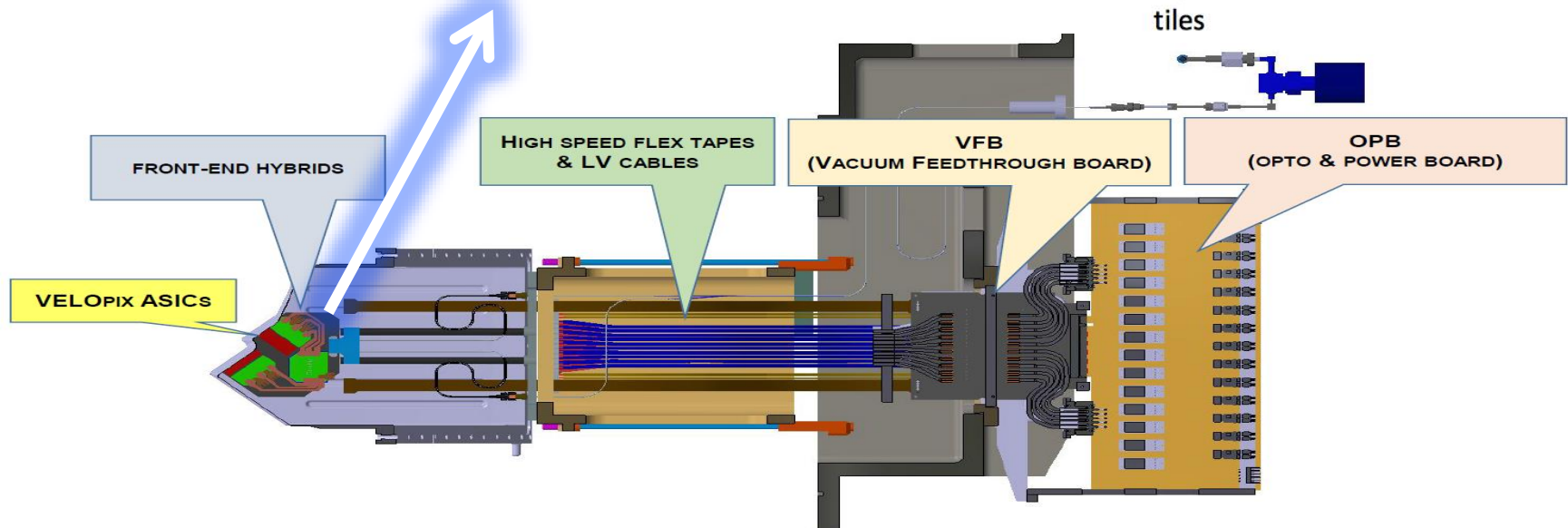
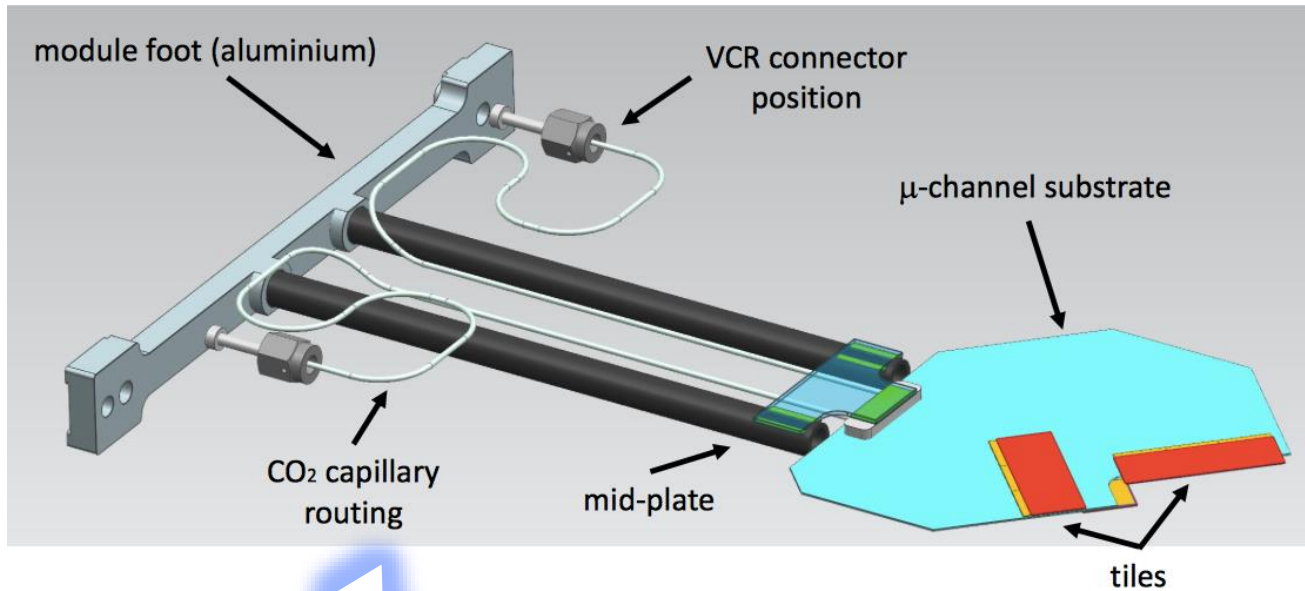
- The closest distance to LHC beam will be **5.1 mm** (down from 8.2 mm).
- Very high ( $8 \times 10^{15} n_{eq}/cm^2$  for  $50 fb^{-1}$ ), non-uniform radiation ( $\sim r^{-2}$ )
- Huge data bandwidth: up to  $\sim 15$  Gbit/s for central ASICs and 2.9 Tbit/s in total.
- Sensor temperature  $< -20^\circ C$  (CO<sub>2</sub> @  $-30^\circ C$ )
- Total maximum power dissipation/module is **~30 W**.
- Minimal material: cooling substrate is retracted 5 mm at the inner region.



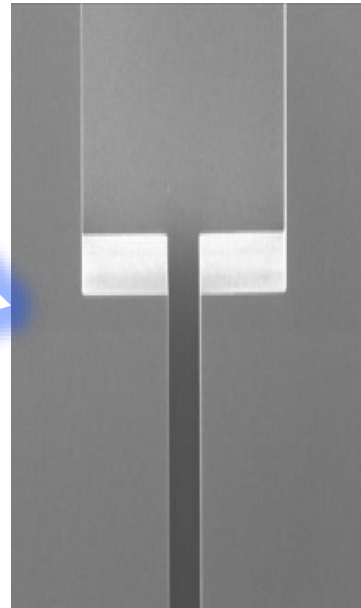
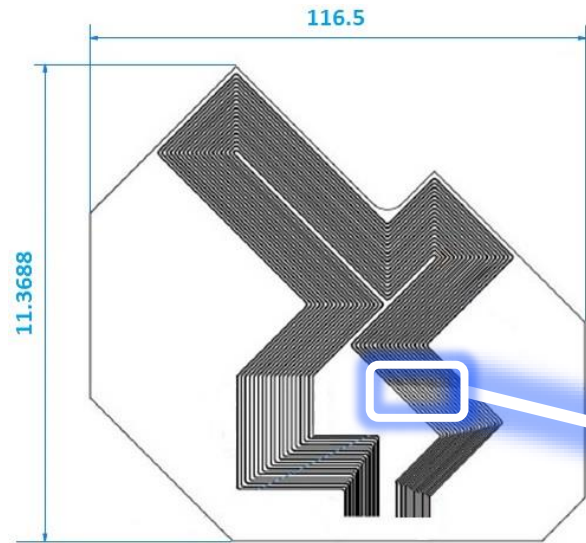
**52 Modules ( 26 per side)**



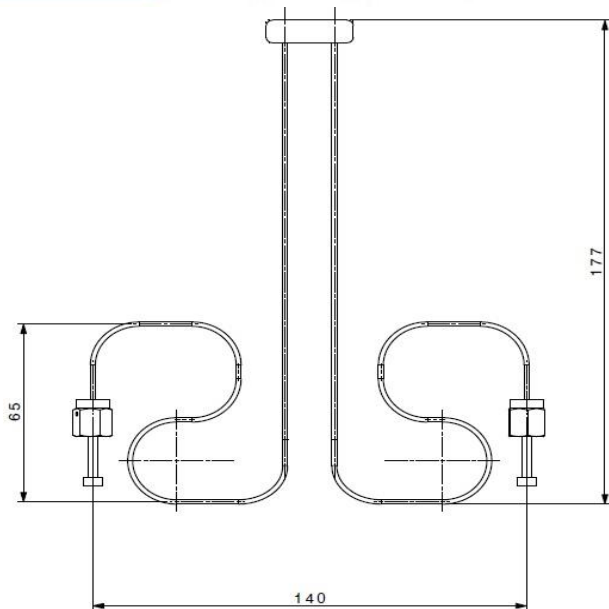
# Module design



# Silicon microchannel substrate design

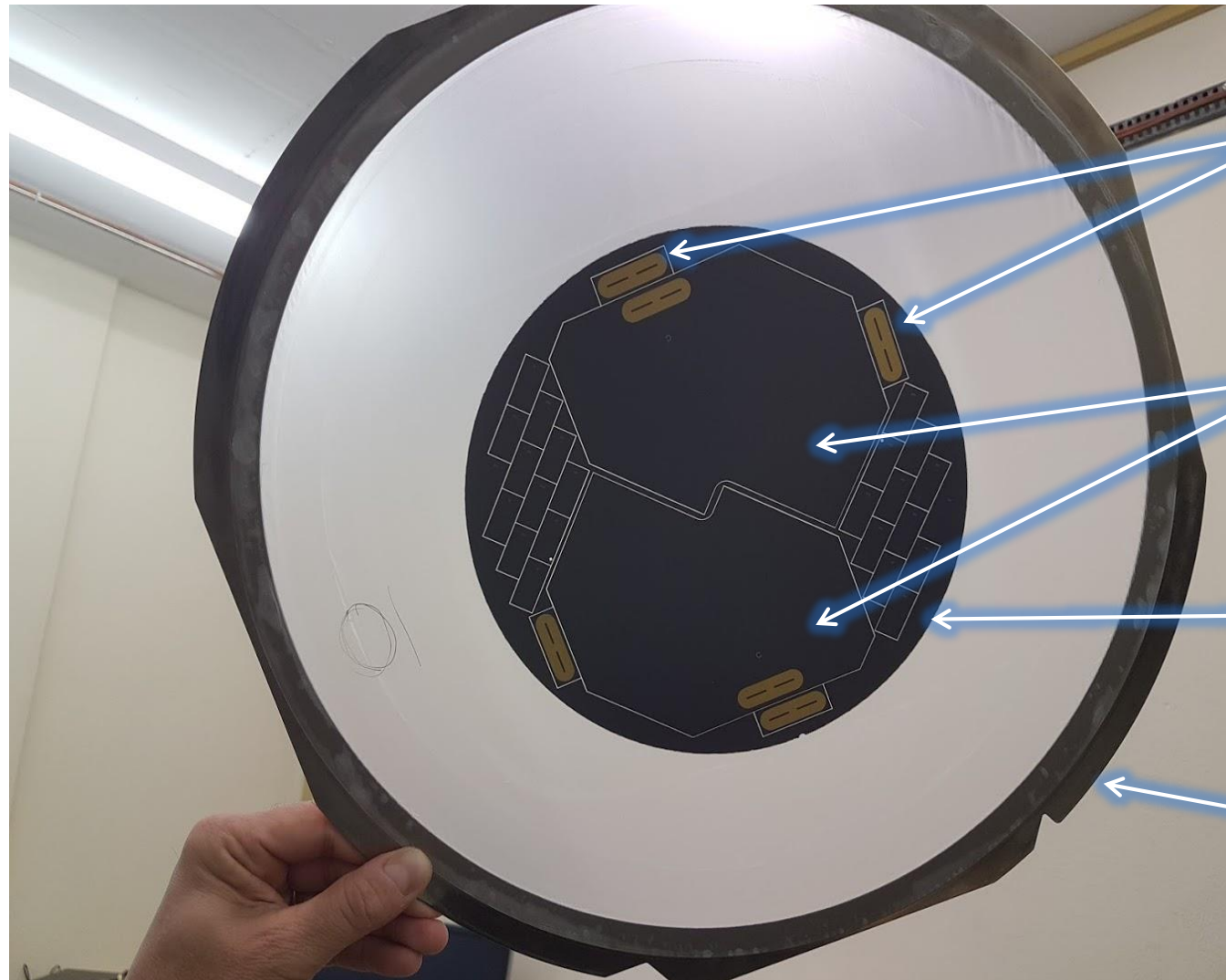


Channel	Restriction length [mm]	Main channel length [mm]
1	40.00	230.86
2	40.00	234.28
3	40.00	237.70
4	40.00	241.11
5	40.00	244.53
6	40.00	247.95
7	40.00	251.36
8	40.00	254.78
9	40.00	258.20
10	40.00	261.61
11	40.00	265.03
12	40.00	268.45
13	40.00	271.87
14	40.00	275.28
15	40.00	278.70
16	40.00	282.12
17	40.00	285.53
18	40.00	288.95
19	40.00	292.37



- Silicon thickness - 500 [μm]
- Main Channel 120 [μm] x 200 [μm]
- Restriction 60 [μm] x 60 [μm]

# Silicon microchannel substrates



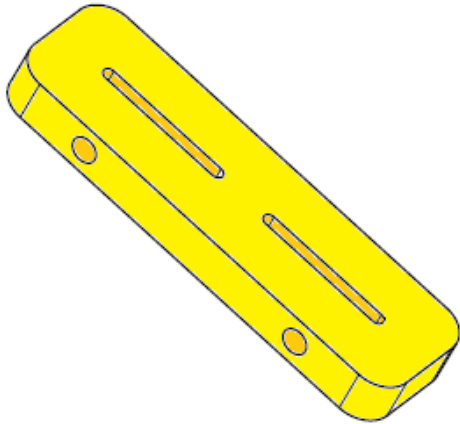
**Metallization samples**

**Silicon microchannel substrates**

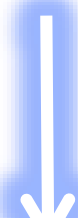
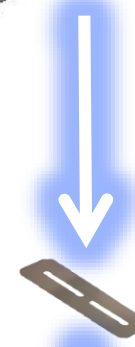
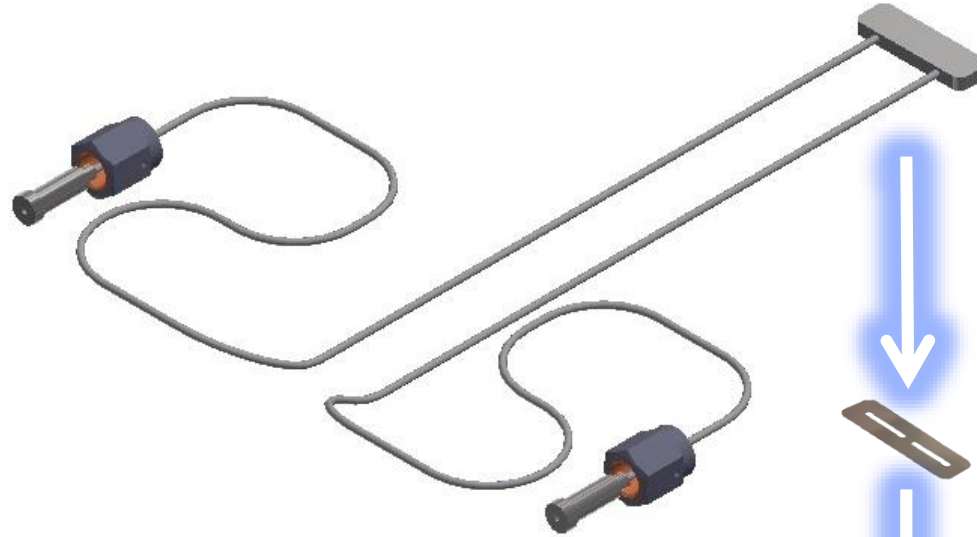
**Silicon Wafer 8"**

**Transport ring**

# Soldering Fluidic Connector



INVAR 36

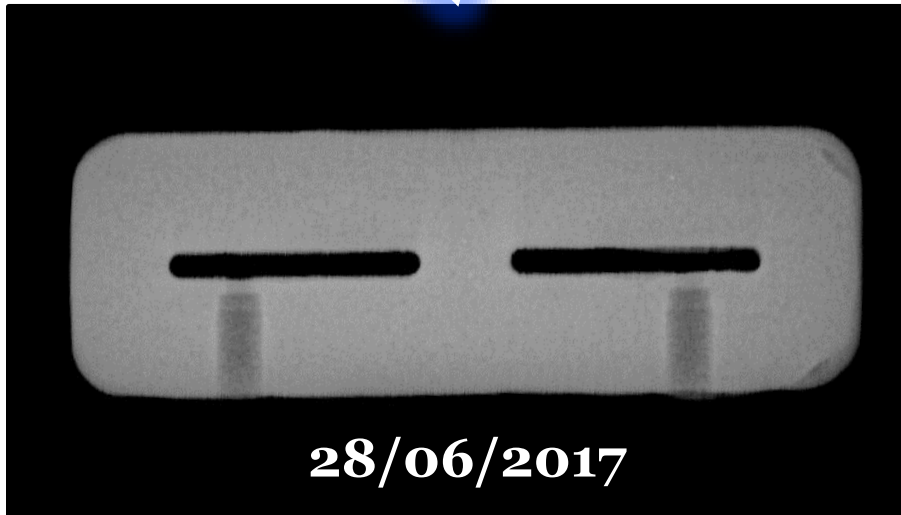


## Joint Requirements:

- **Reliable**
- **Leak tight (under vacuum)**
- **Able to withstand pressure of 186 [bar]**



# Soldering Fluidic Connector Results



**X-ray result of the solder joint in small sample**



**Full size – dummy substrate**

# Creep effect in the solder joint

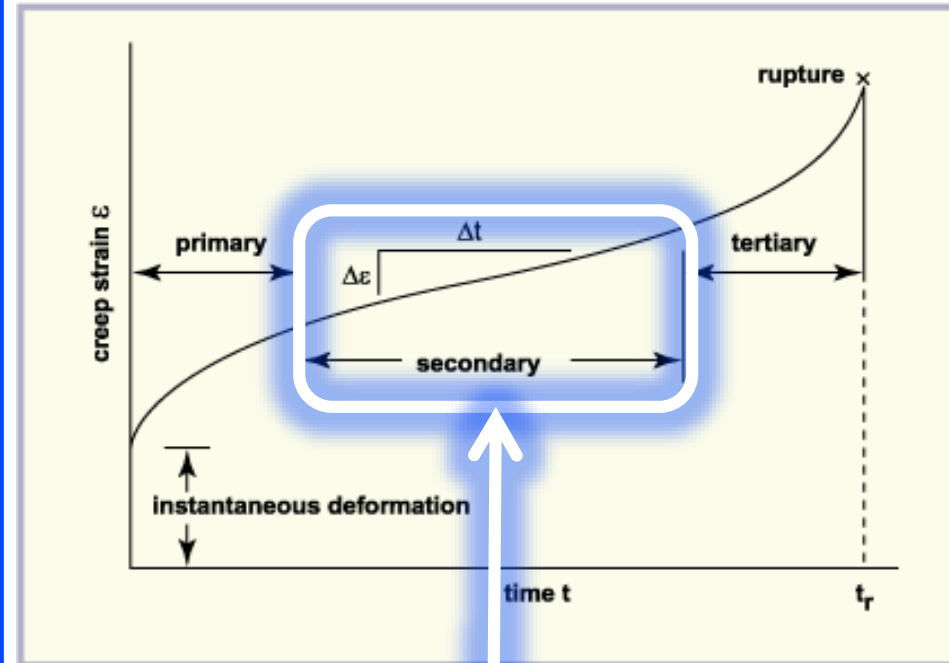
**“Plastic deformation of a material at very low mechanical stress levels”.**

- Present in many materials.
- Stress can be caused by its own weight (e.g. glaciers or glass windows).
- Can lead to failure after long time.
- Typically can be neglected only if:  
Temperature < T-critical

T-critical = 50% of absolute melting Temperature.

- For SnPb: T-critical = - 46 [°C].
- VELO should be at - 30 [°C], so expect very small creep effects.

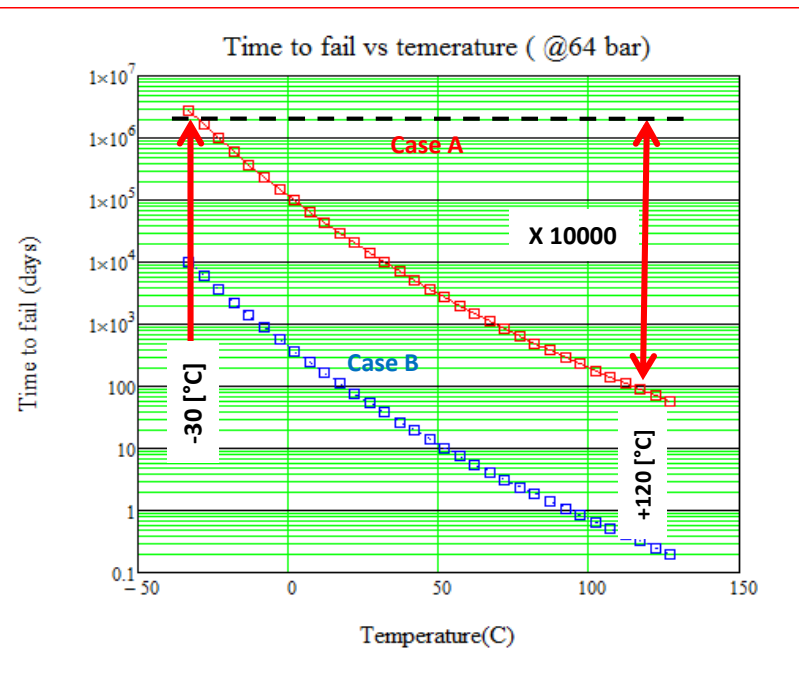
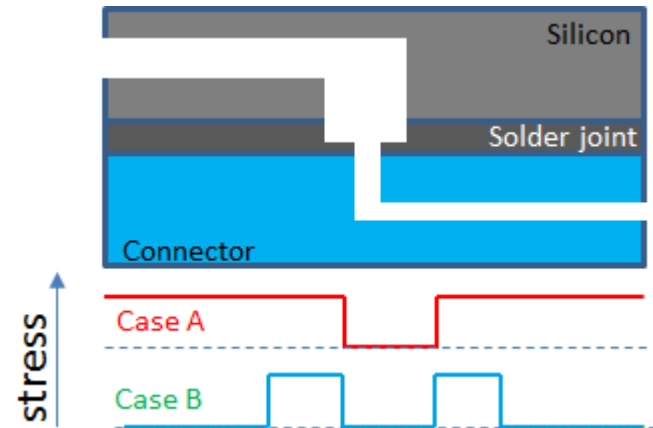
**CO2 pressure at -30 [°C] ~20 [bar]**



Models exist for linear (secondary) region :  
e.g. “**A new creep constitutive model for eutectic solder alloy.**” Shi, Wang, Zhou, Pang, Yang , 2002.  
Transactions of the ASME page 84, Vol124, June 2002.

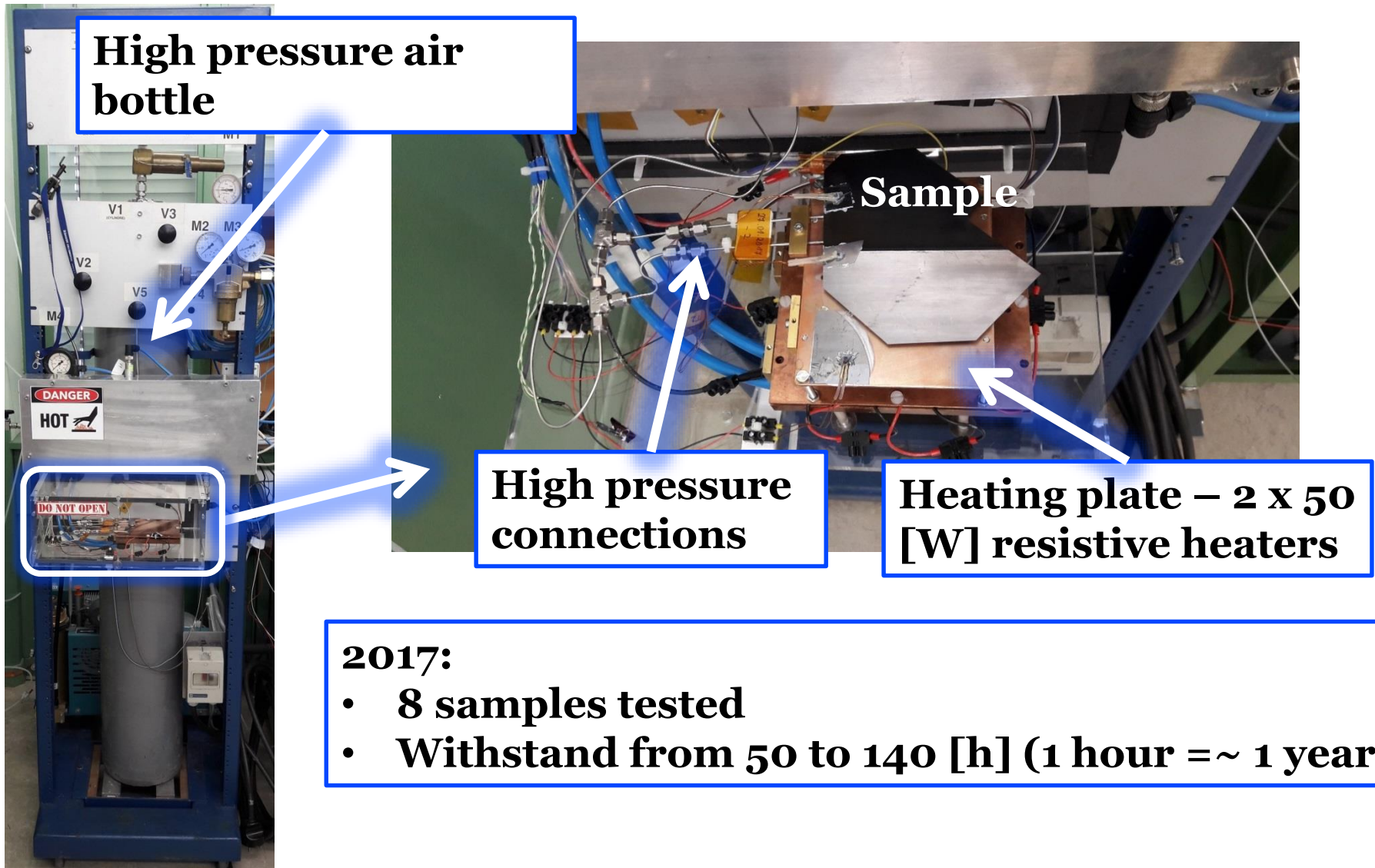
# Creep effect in the solder joint - simulation

- **Strain rate (=strain/sec) is function of Temperature (T) and stress ( $\tau$ ).**
- **Stress distribution is not well known: assume 2 extreme cases:**
  - **Case A: total force is spread uniformly over soldered surface.**
  - **Case B: total force is highly concentrated near the slits.**



*“A new creep constitutive model for eutectic solder alloy.”* Shi, Wang, Zhou, Pang, Yang, 2002. Transactions of the ASME page 84, Vol124, June 2002.

# Creep effect test stand



**2017:**

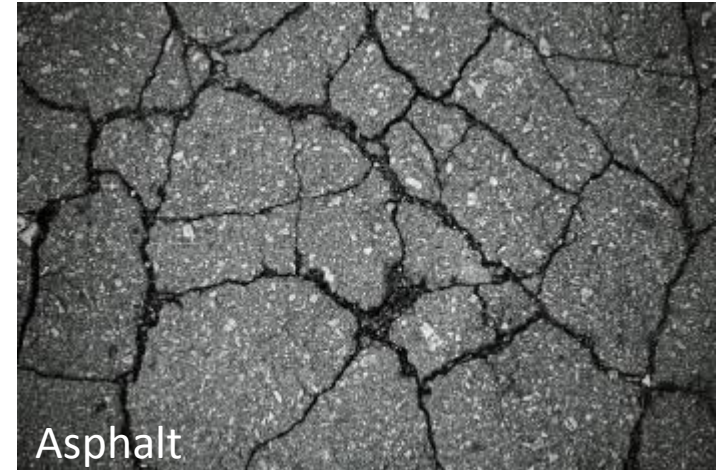
- 8 samples tested
- Withstand from 50 to 140 [h] (1 hour = ~ 1 year)



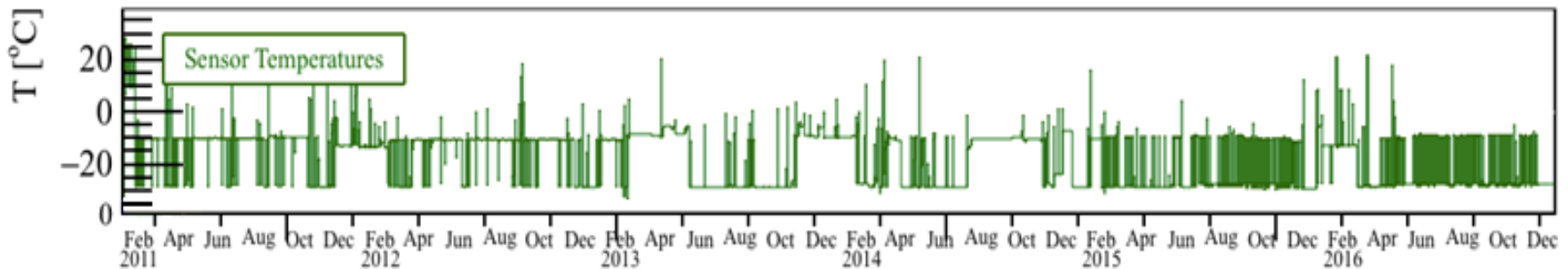
# Fatigue effect in the solder joint

***“Fatigue is the weakening of a material caused by repeatedly applied loads.”***

Effect occurs when a material is subjected to repeated loading and unloading.



Current Velo – Few hundred Temperature and Pressure Cycles (300 roughly)

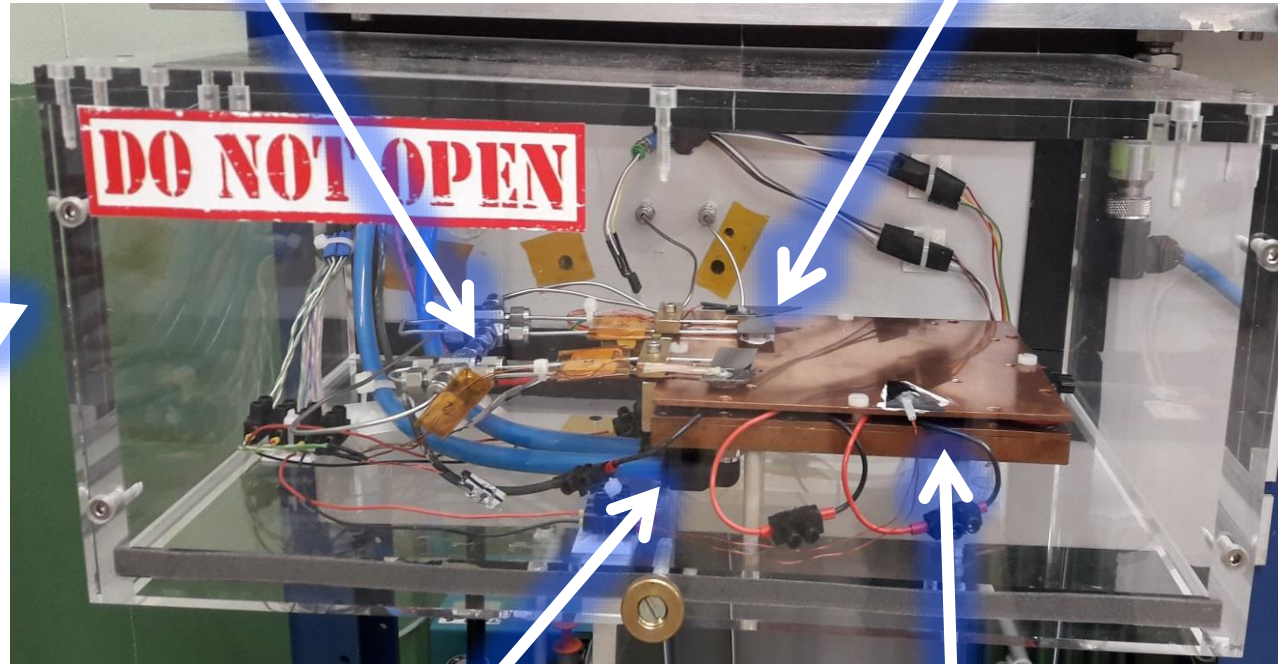


# Fatigue test stand



High pressure connections

Samples



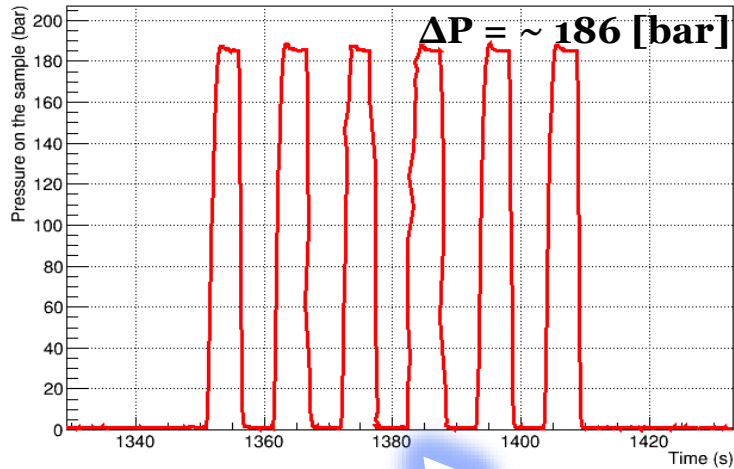
Bottom heat exchanger – glycol flow

Heating/Cooling plate – 6 x 40 [W] Peltiers

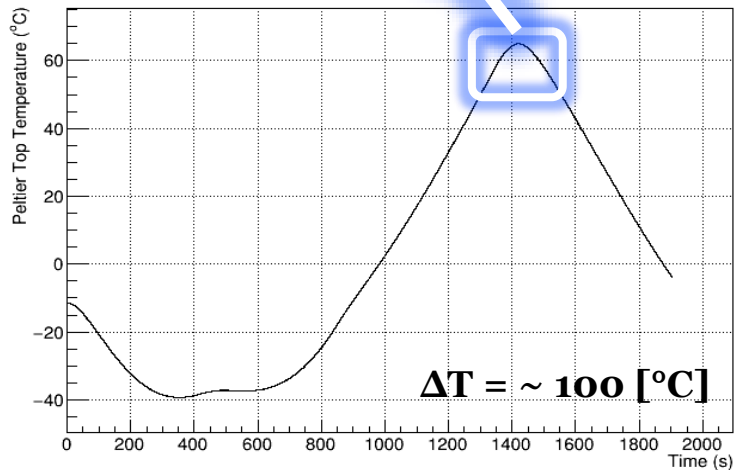
# Fatigue test results example

## Single cycle

Pressure on the sample

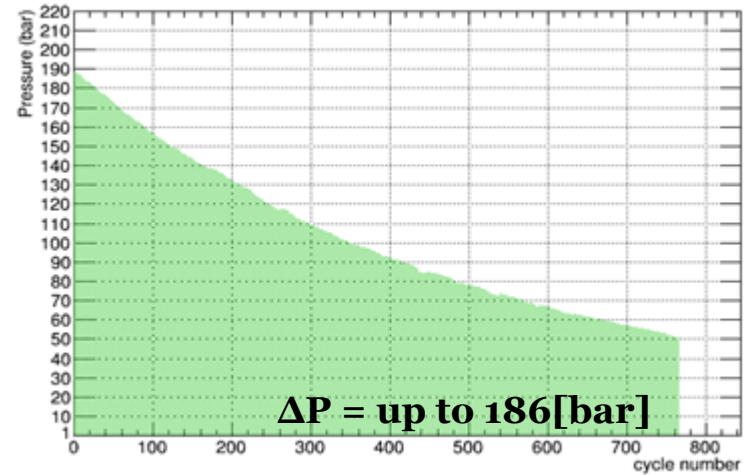


Sample temperature

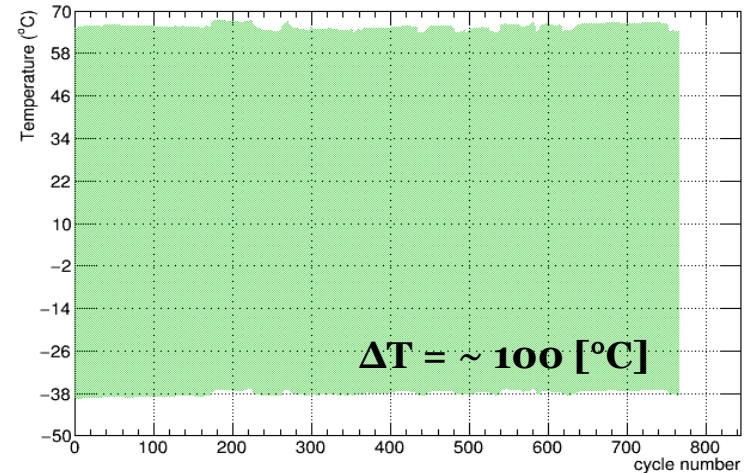


## Full test

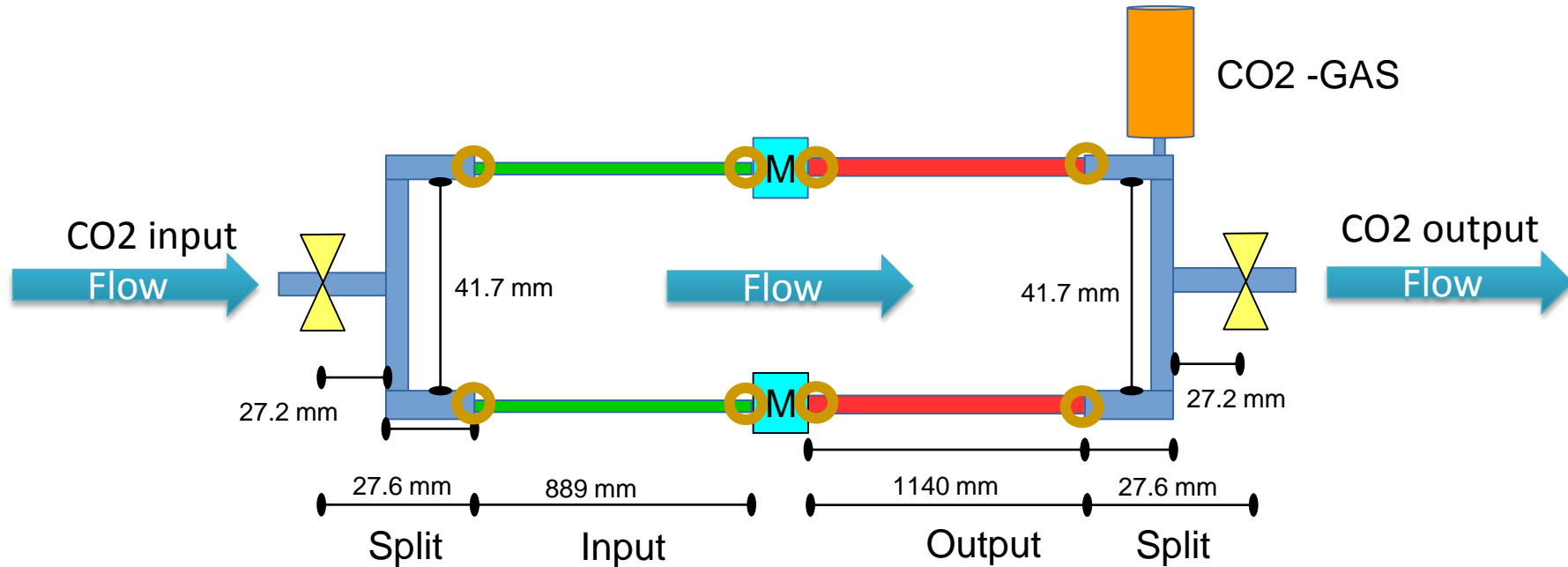
Max and Min Pressure on the Sample\_S74\_S75












Max and Min Temperature on the Sample\_S74\_S75



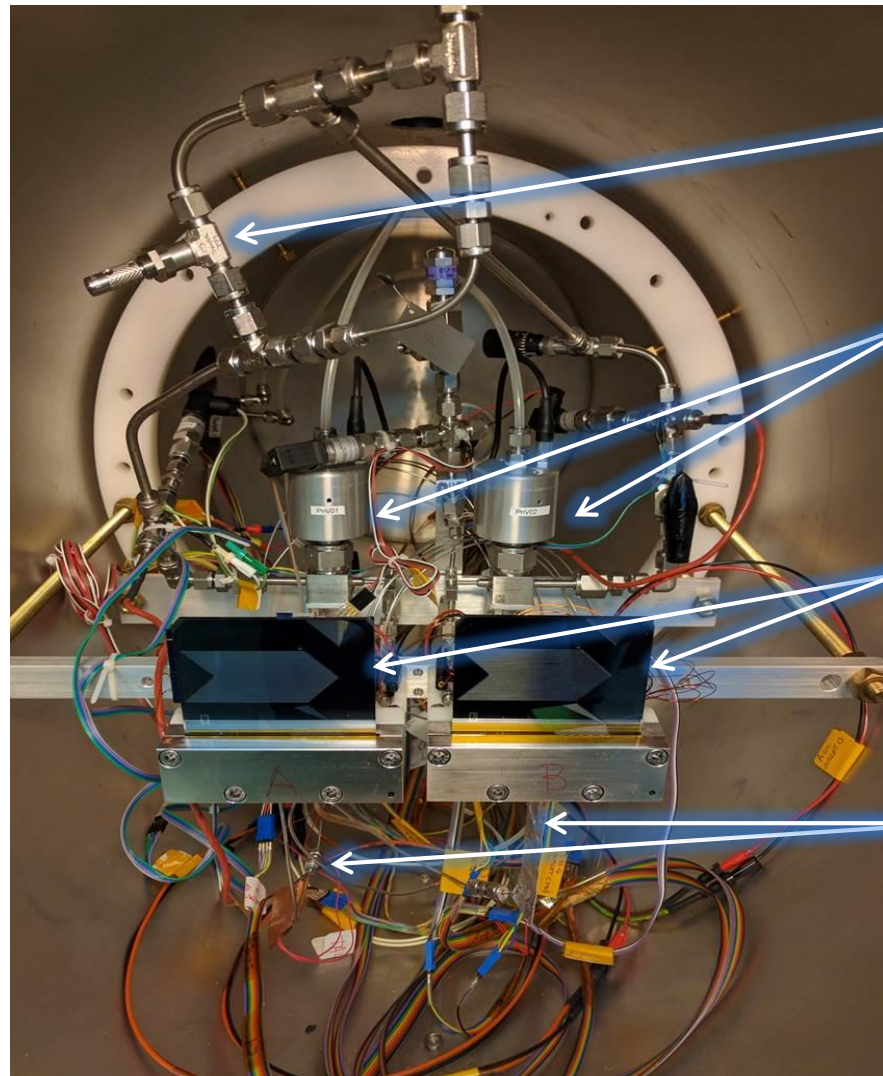
# Two microchannels in parallel



-  1/8" (ID 1.397 mm)
-  1/16" (ID 0.5715 mm)
-  1/16" (ID 0.8763 mm)
-  3/8" (ID 6.223 mm)
-  VCR connector 1/8" (~5mm)
-  1/2" (ID 9.398 mm)
-  Safety volume between the valves
-  Module - 2x320 mm 1/16" to the connector in the module (Microchannels – Input + output)
-  Safety valves (pneumatic)



# Fluidic characterization test stand



**Vacuum chamber view**

**Bypass  
 (metering  
 valve)**

**Safety Valves  
 (pneumatic)**

**Microchannel  
 substrates  
 silicon/pyrex**

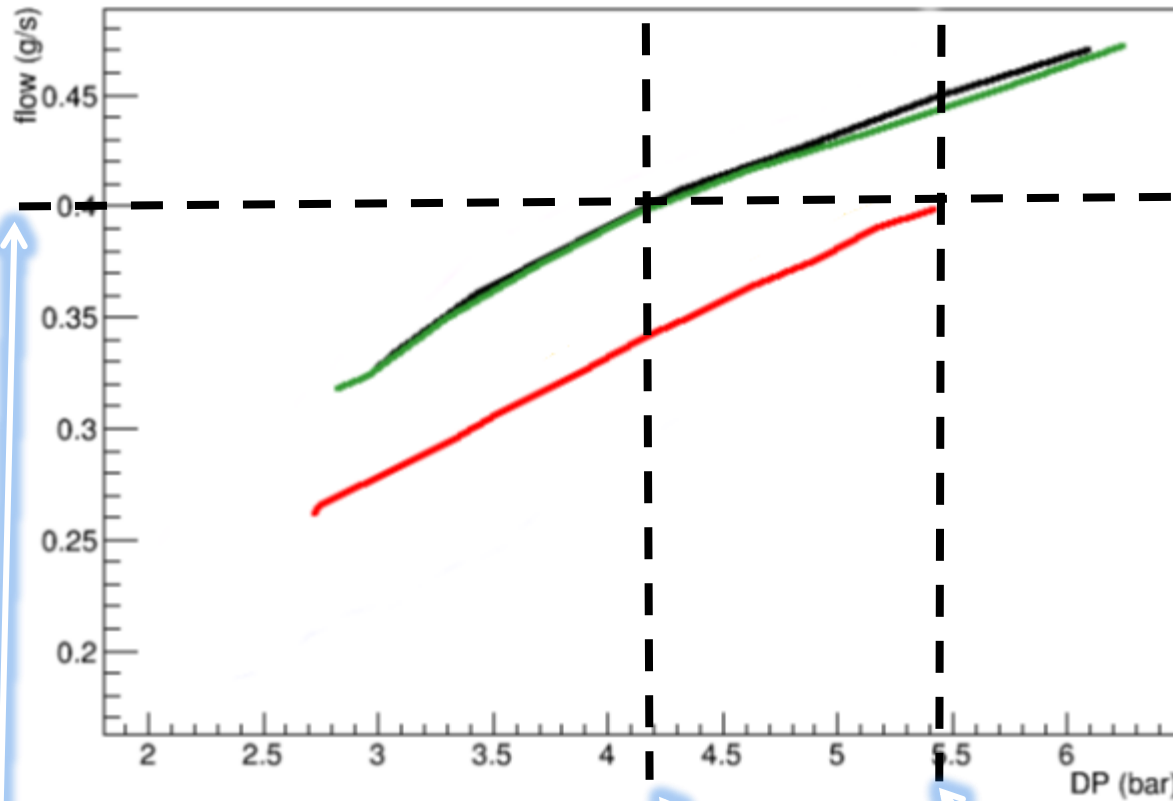
**Preheaters**

**Isolated  
 concentric  
 tube**



# Silicon substrate fluidic characterization

CO<sub>2</sub> Temperature -25 [°C]



Applied Power:  
 0W, (2016)  
 5W, (2016)  
 30W, (2016)

0.4 [g/s] - nominal flow

Min  $\Delta P = \sim 4.2$  [bar]

Max  $\Delta P = \sim 5.45$  [bar]

# Flow stability test

**There should be no interplay between the two modules in the same cooling loop.**

**Test procedure:**

- **Power one microchannel (A or B) with 30[W]**
- **Make cyclic changes of power on the other microchannel between 0-30[W]**

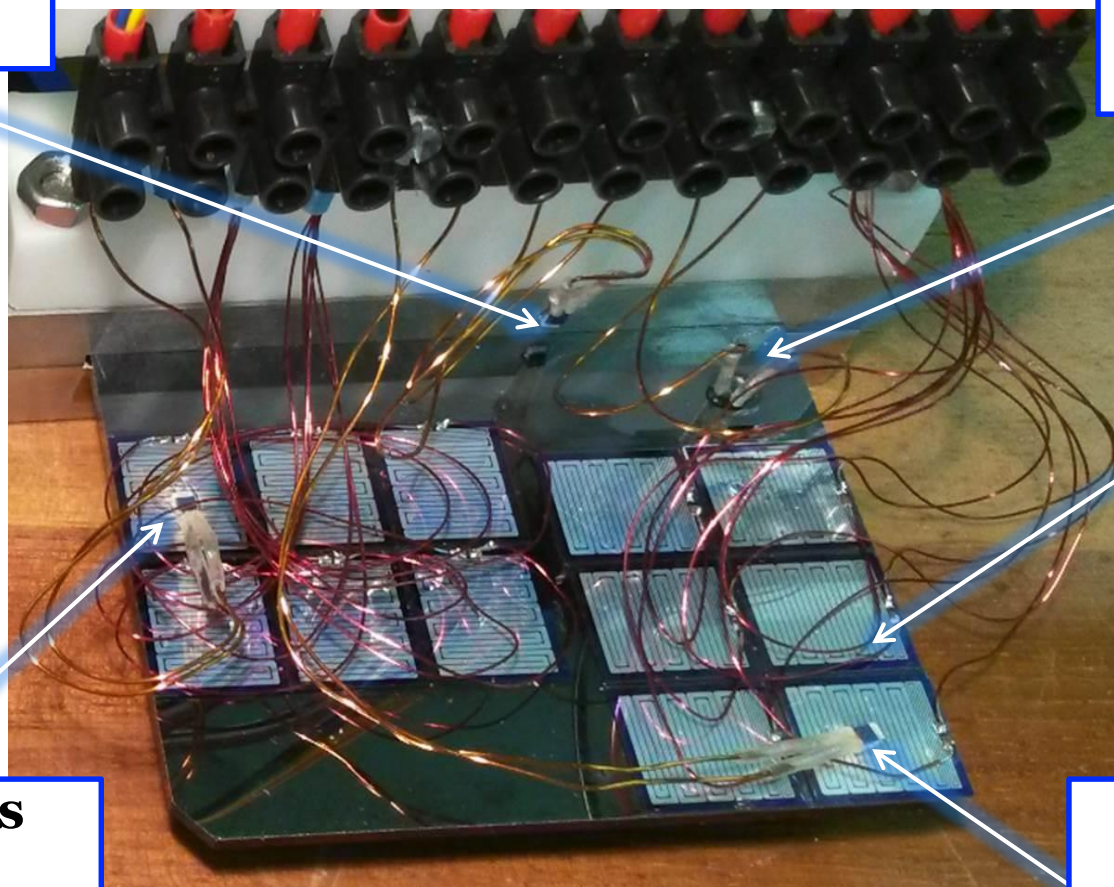
**Since the cooling plant will be flow driven, the flow is adjusted manually to  $2 * 0.4$  [g/s] (0.4[g/s] is the nominal flow per microchannel)**

**If the system is stable, the module with constant power should not be affected by the power variation on the second one.**

# Silicon substrate – temperature probes

Connector  
temperature  
(Con)

Microchannel  
Outlet  
temperature  
(MCOutput)



12 ASIC  
heat  
mockups

Inlet Asics  
Heaters  
temperature  
(MCinput)

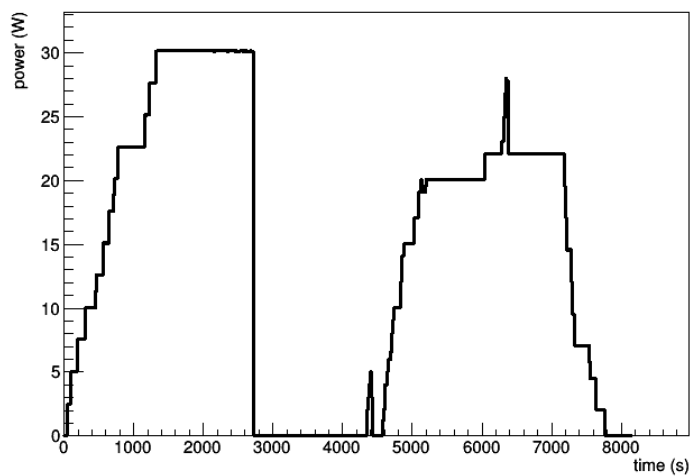
Outlet Asics  
Heaters  
temperature  
(OAH)



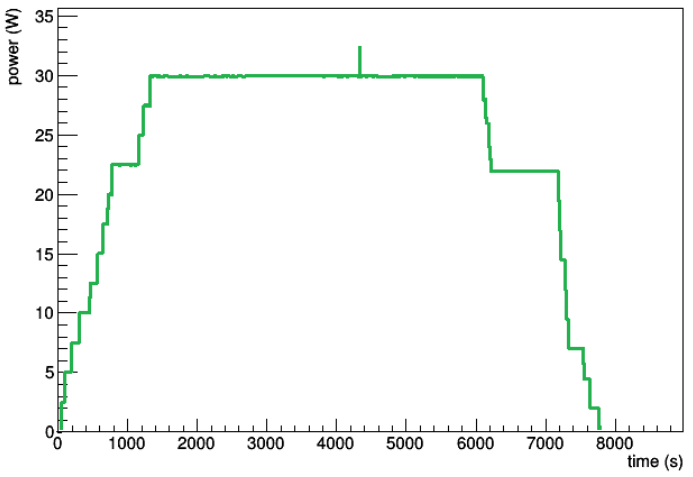
# Flow stability in parallel operation

**Total Flow ~ 0.8 [g/s]**

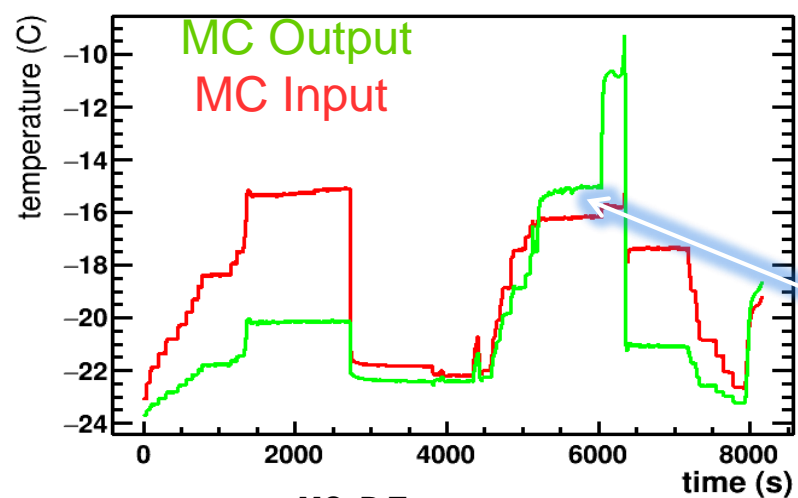
Total power A



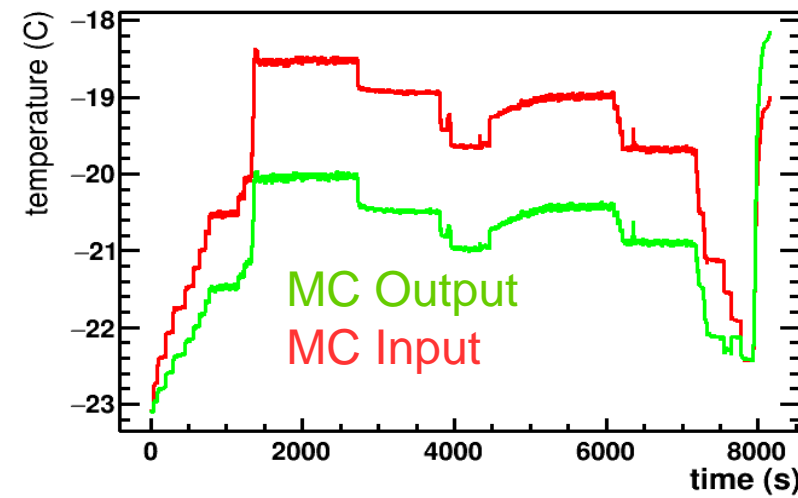
Total power B



MC A Temperatures



MC B Temperatures



**MCOutput warmer than MCInput!**

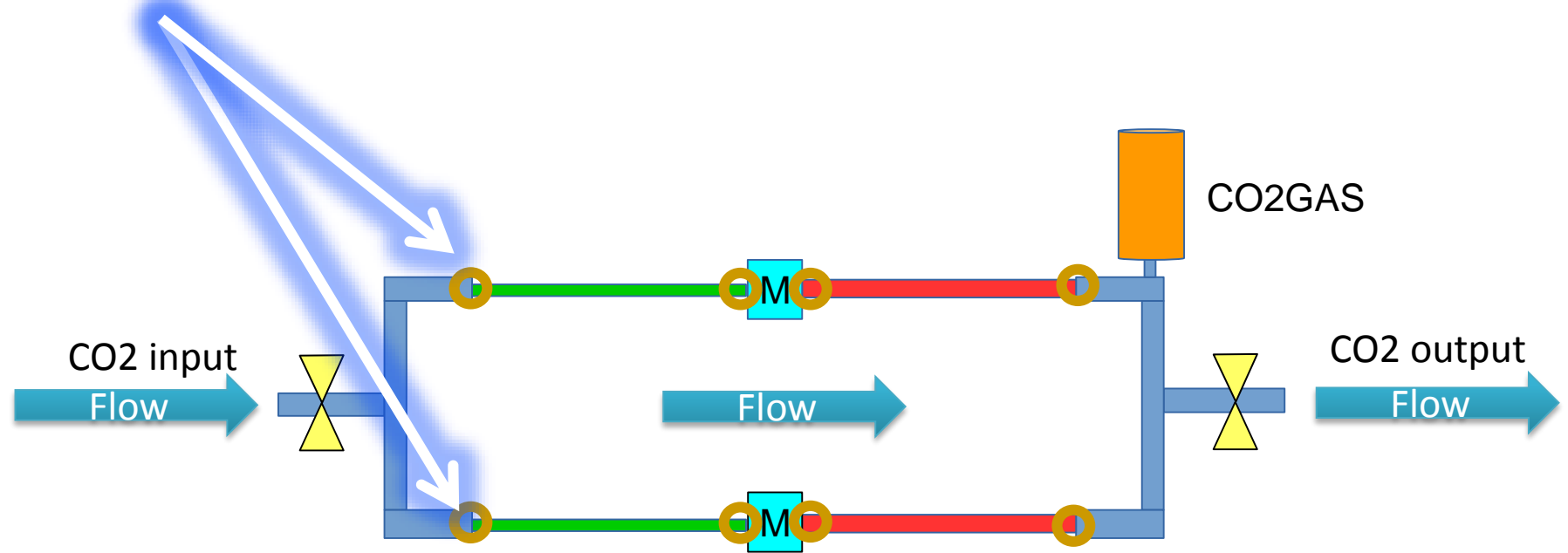
**Possible solutions**

**Gasket restrictors**

**Preheaters**

# Gasket Restrictors position

**VCR gaskets with orifices to create additional pressure drop**

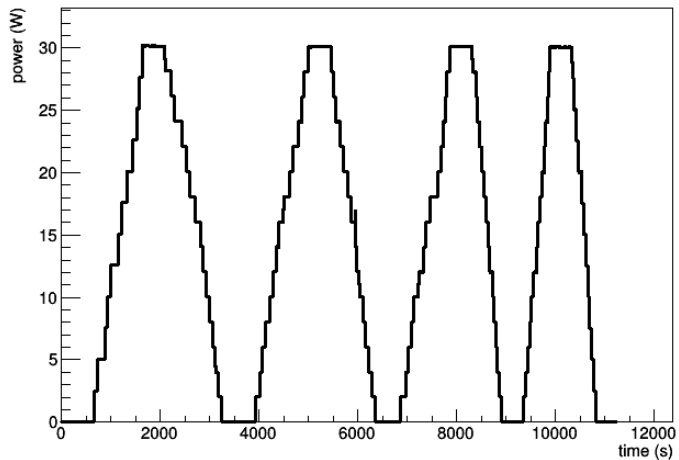


 VCR connector

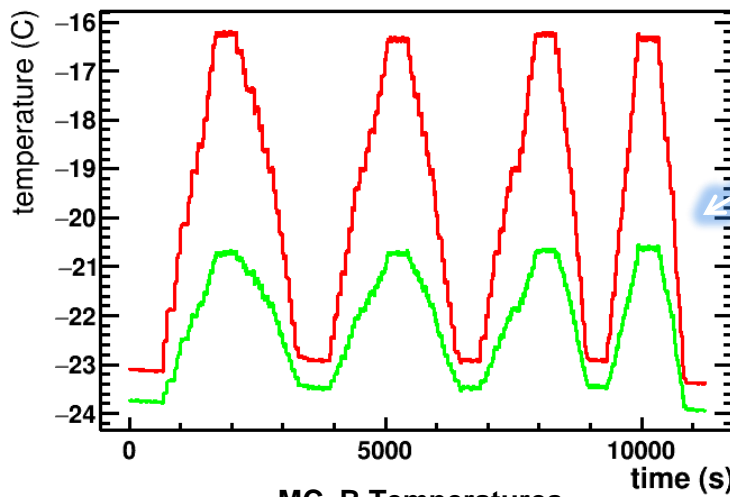
# Gasket Restrictor 0.150 [mm]

**Total Flow ~ 0.64 [g/s]**

Total power A

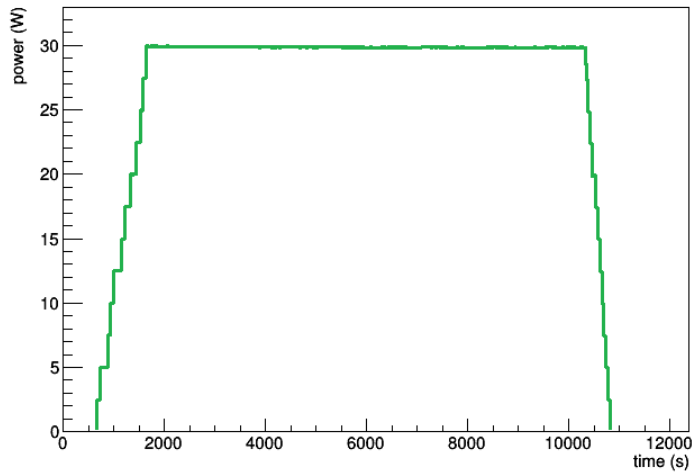


MC A Temperatures

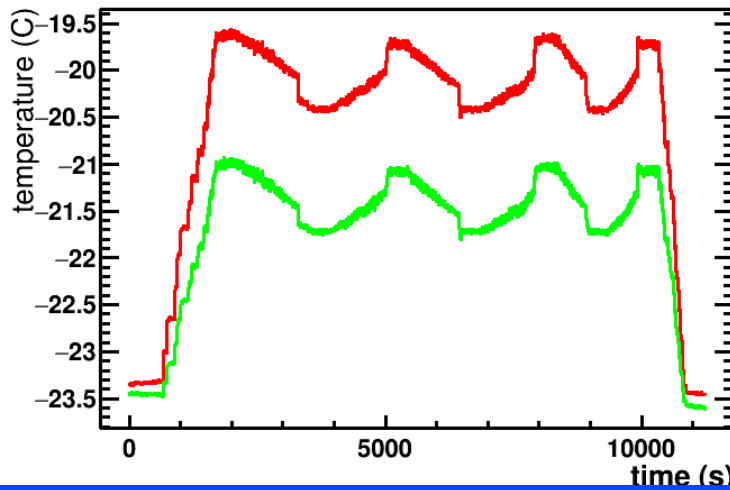


**MCOutput**  
colder  
than  
**MCInput**

Total power B



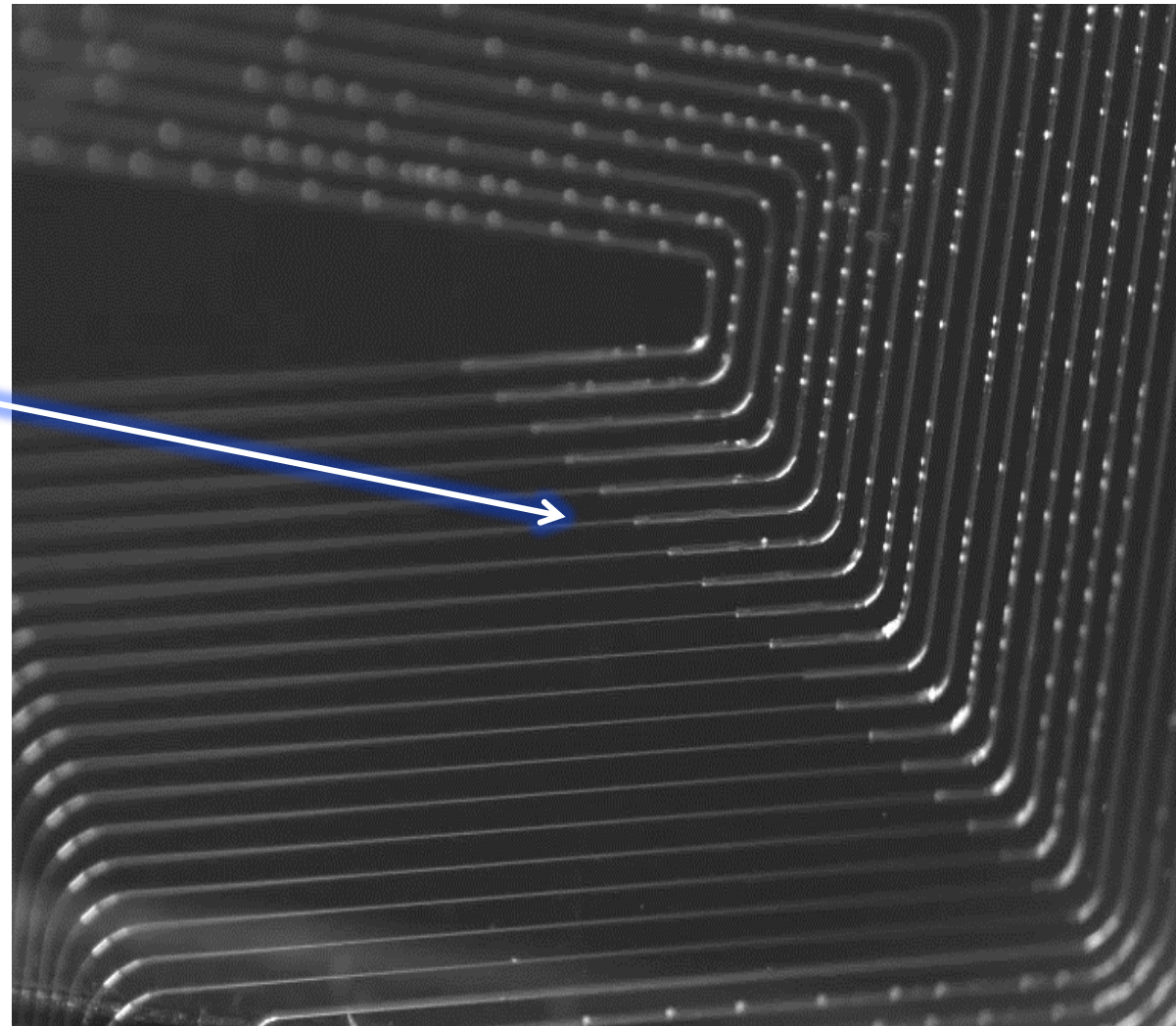
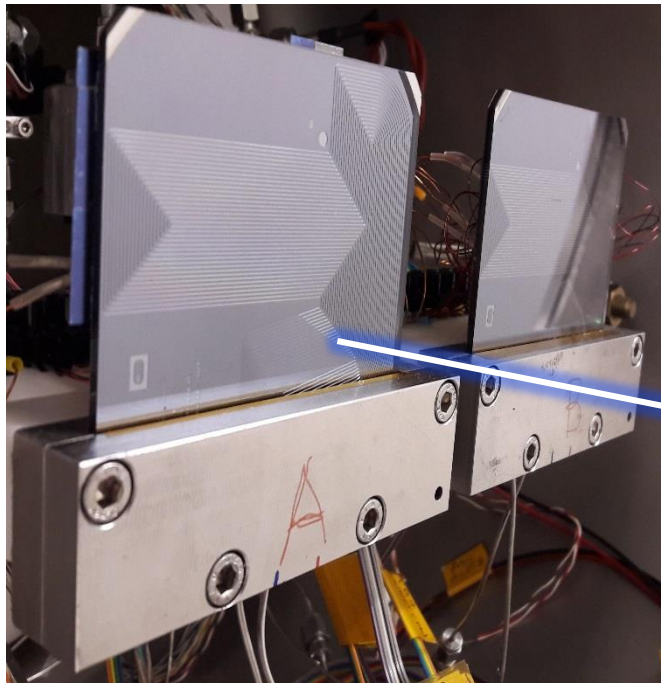
MC B Temperatures



**Stable**  
operation  
during  
power  
cycling

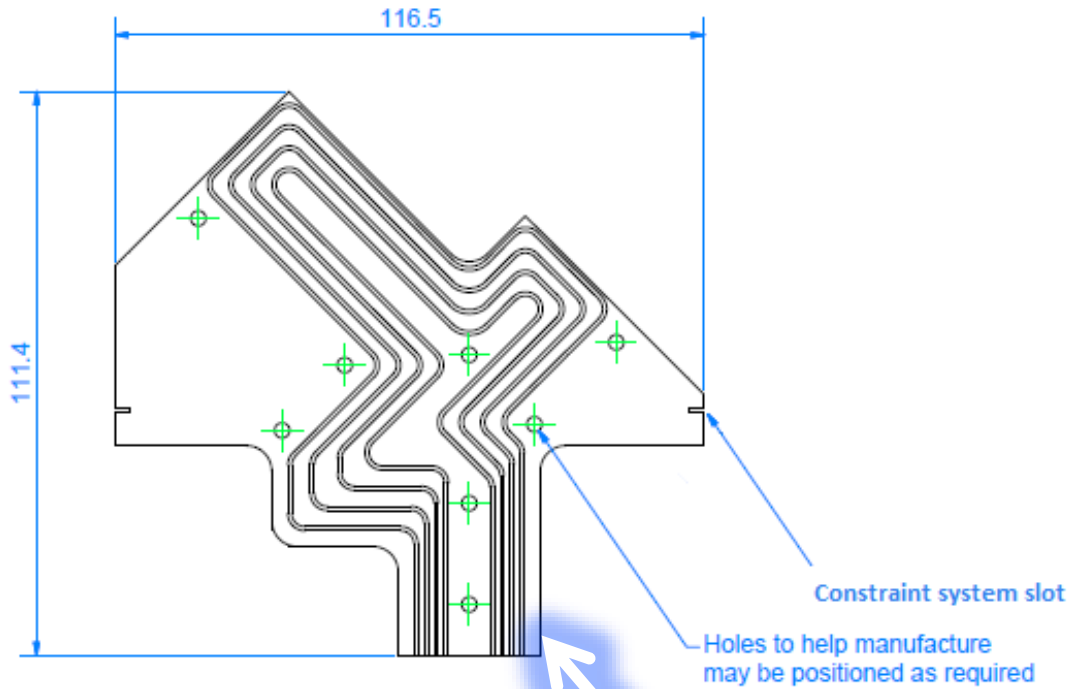


# Flow through silicon microchannel substrate



**Single CO<sub>2</sub> bubble  
speed – up to 1 [m/s]**

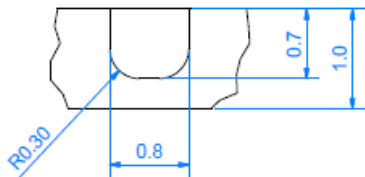
# Ceramic substrate design



Bending jig



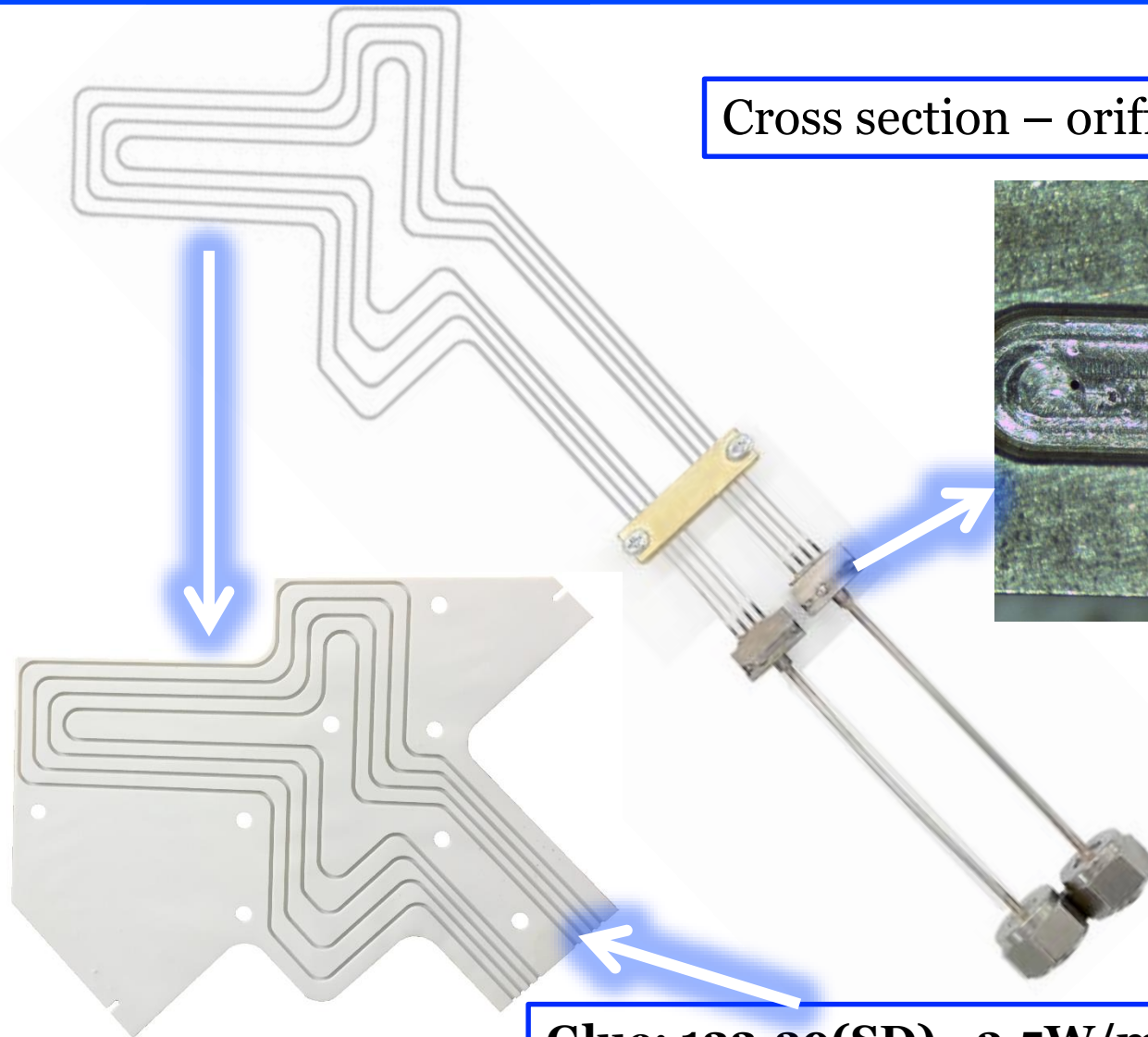
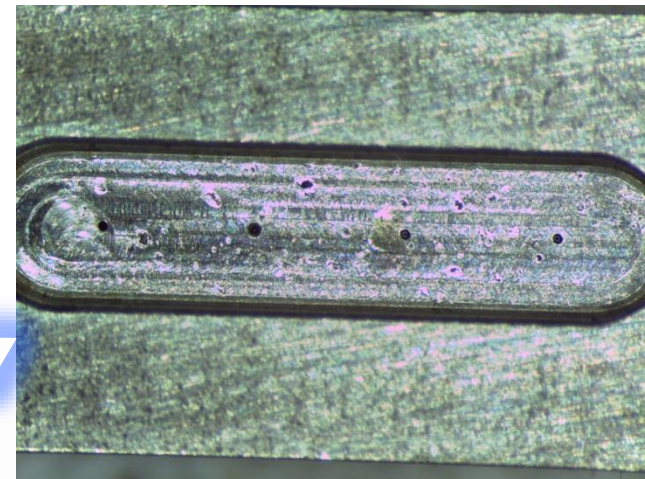
Detail of sheet thickness and channels



**Aluminum Nitride - Shapal**

# Ceramic substrate fabrication

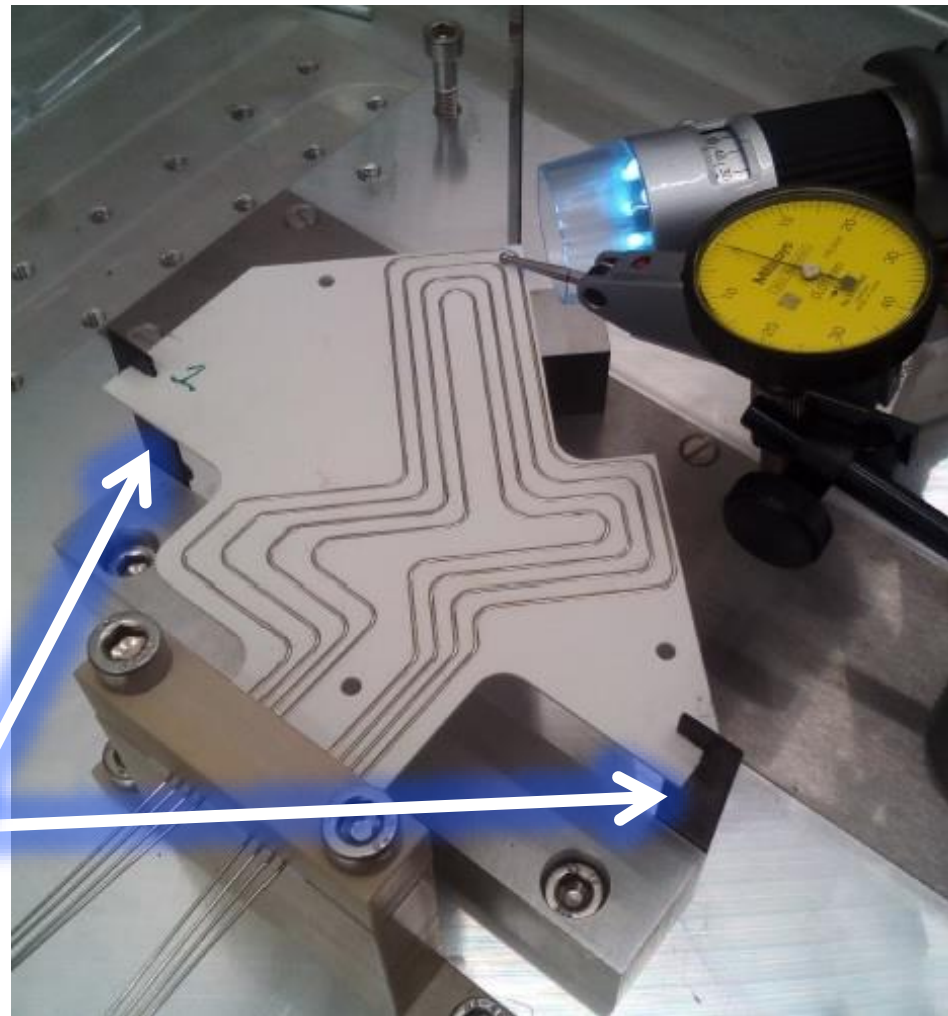
Cross section – orificies  $125 \pm 5 \text{ } [\mu\text{m}]$



**Glue: 122-39(SD) -  $3.5 \text{ W/mK}$  ( applied by robot)**



# Ceramic substrate constraint system



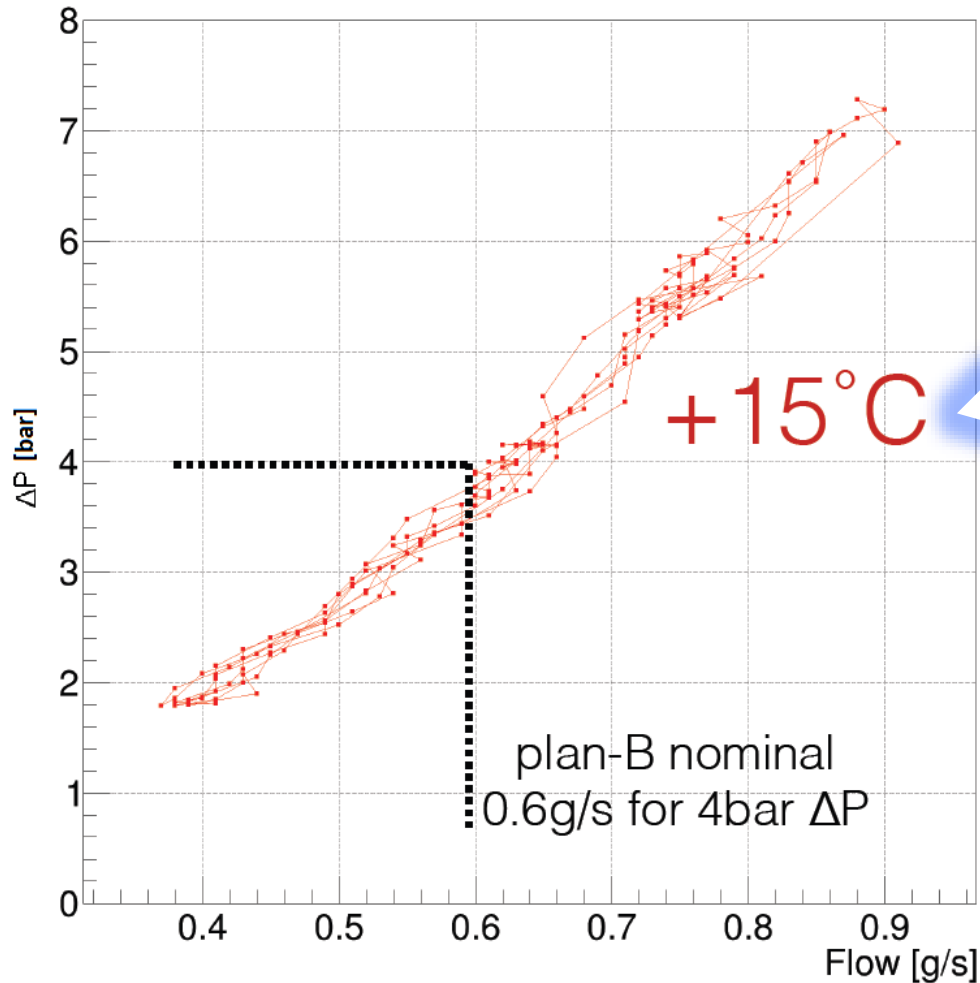
**Carbon fibre  
constraint  
system**

**Deflections < 100 [ $\mu\text{m}$ ] - due to temperature variation**



# Ceramic Substrate fluidic characterization

Capillaries 0.41 [mm] ID



CO<sub>2</sub> temperature

+15°C

## Microchannels:

- Better Physics performance due to less material
- No CTE mismatch between sensors and substrate
- High thermal conductivity (silicon)
- No fatigue or accumulated stress effects have been observed by doing cyclic stress tests
- The orifices approach is a quite promising technique to solve the boiling instabilities.
- Soldering technique is quite advanced. The first microchannels will be soldered in a few weeks.

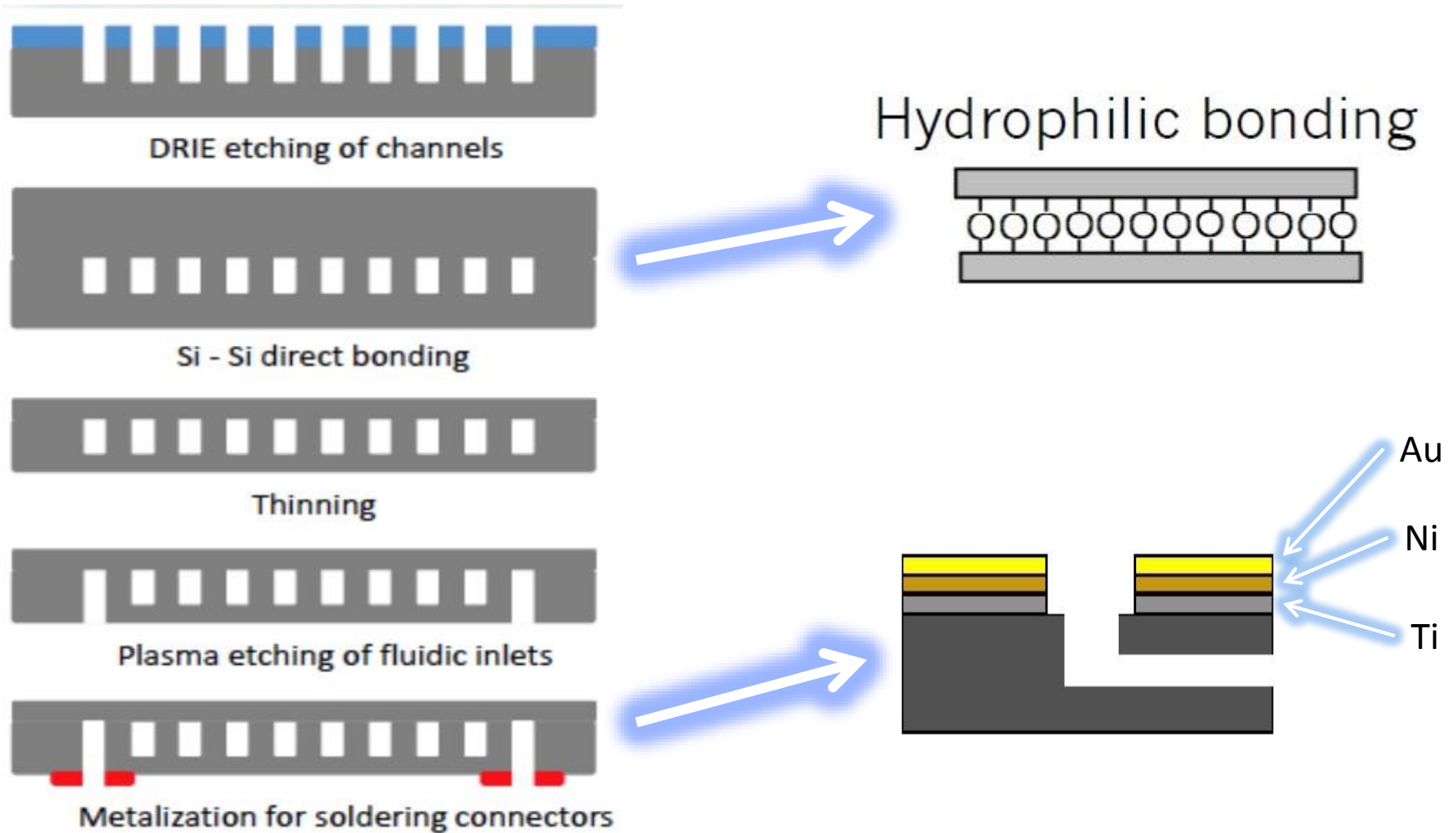
## Ceramic substrate:

- A more conservative approach is being developed in parallel
- Small deflection due to the thermal variations ( $< 100$  [ $\mu\text{m}$ ])
- Smaller fluidic resistance
- Reliability tests (pressure and temperature cycling) ongoing.

**The decision will be taken this summer.**

# Backup Slides

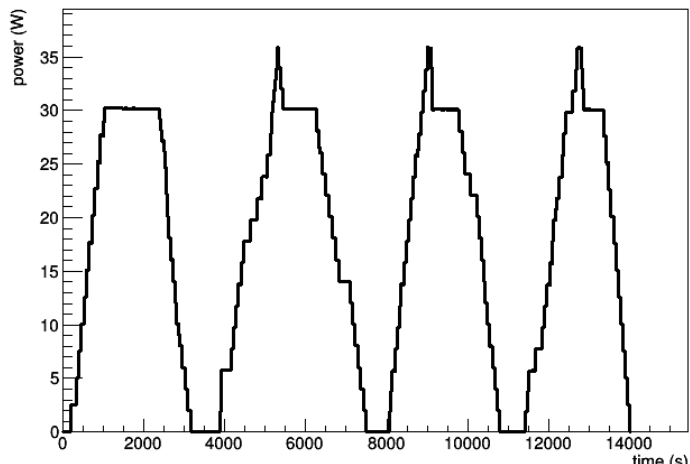
# Microchannels fabrication



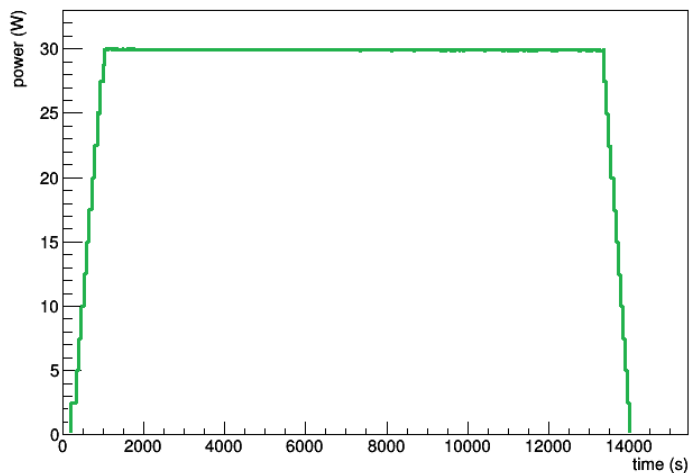
# Preheating

**Total Flow ~ 0.8 [g/s]**

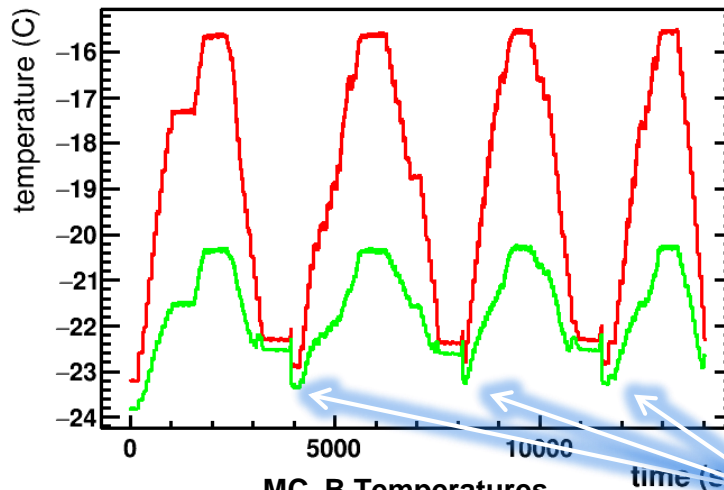
Total power A



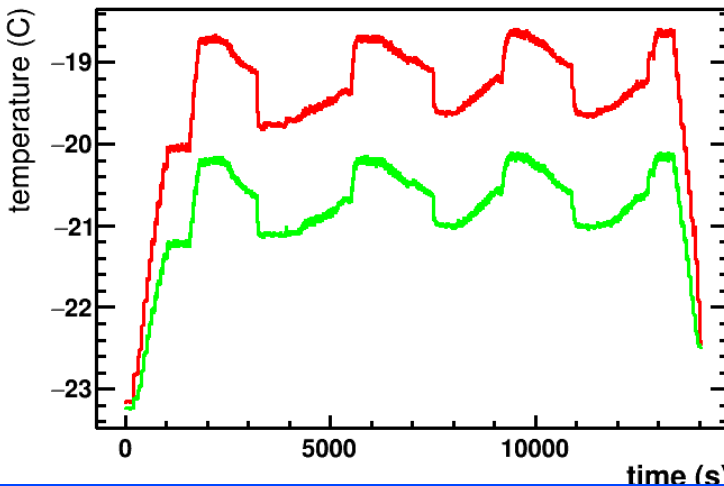
Total power B



MC A Temperatures



MC B Temperatures

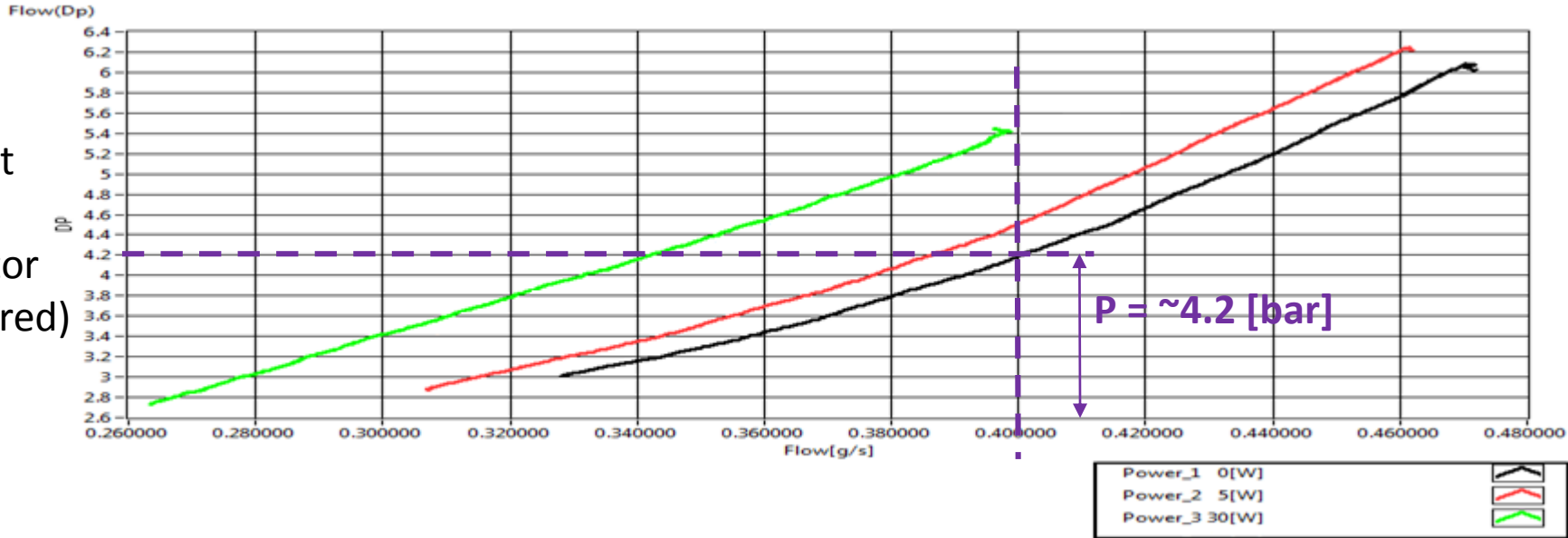


**Preheating applied at 0 [W] Load**

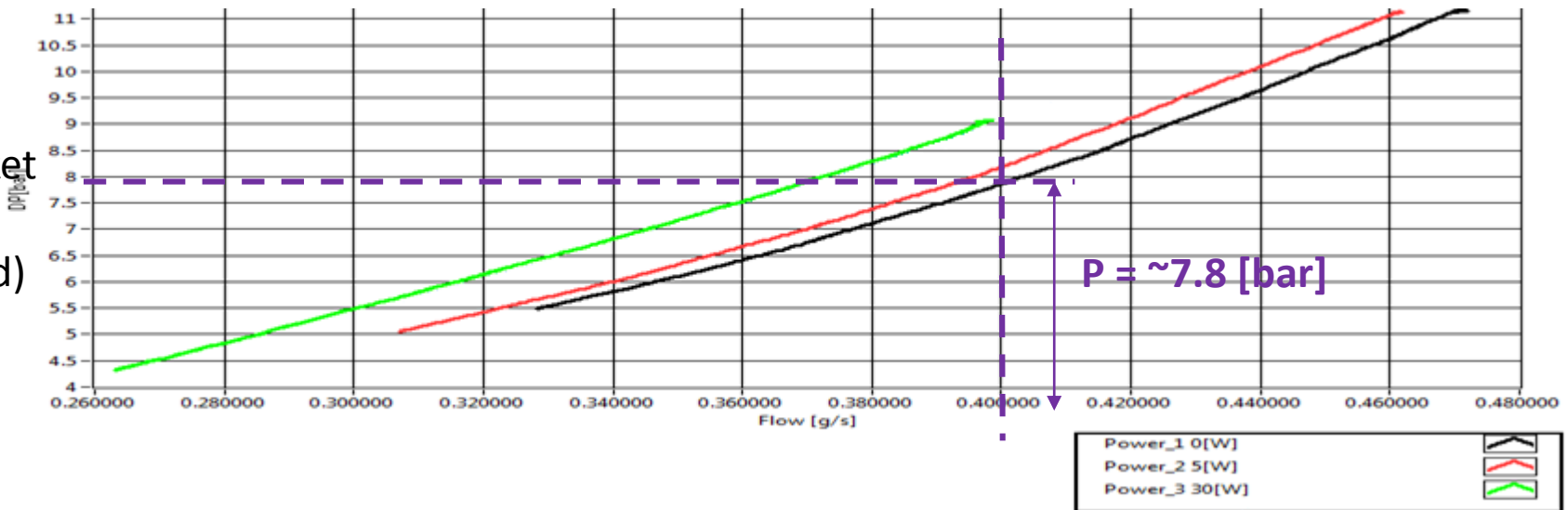


# Gasket Restrictor 0.150 [mm], CO<sub>2</sub> -25[°C]

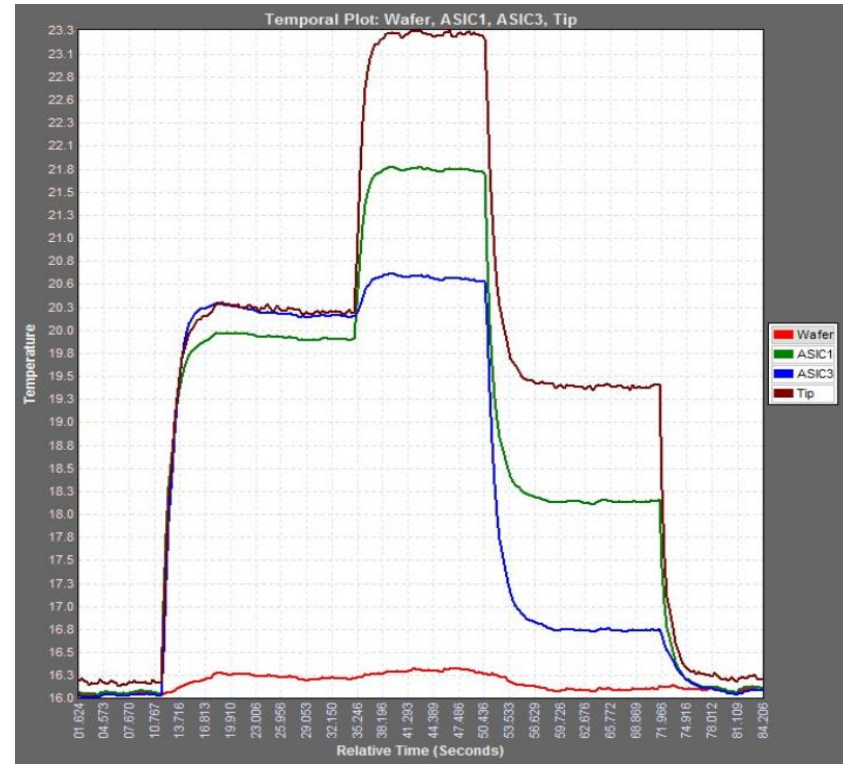
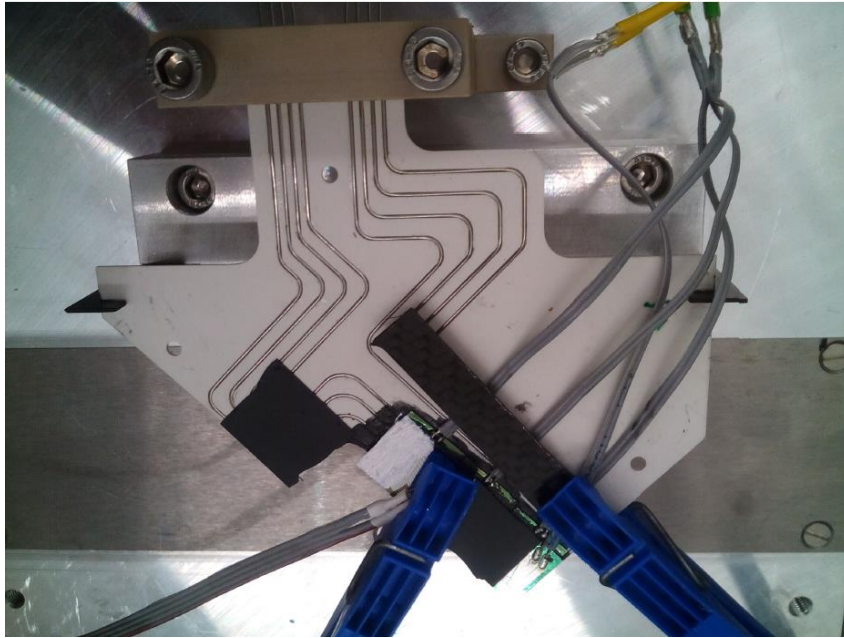
Without Gasket Restrictor (measured)



With Gasket Restrictor (calculated)



# Cooling performance



**CO<sub>2</sub> temperature set to +15[°C]**  
**Heaters mockups simulate the power dissipation due to the 2W/ASICs + 1W/sensor**  
**The measured DT is around [7° C]**